



This is a digital copy of a book that was preserved for generations on library shelves before it was carefully scanned by Google as part of a project to make the world's books discoverable online.

It has survived long enough for the copyright to expire and the book to enter the public domain. A public domain book is one that was never subject to copyright or whose legal copyright term has expired. Whether a book is in the public domain may vary country to country. Public domain books are our gateways to the past, representing a wealth of history, culture and knowledge that's often difficult to discover.

Marks, notations and other marginalia present in the original volume will appear in this file - a reminder of this book's long journey from the publisher to a library and finally to you.

Usage guidelines

Google is proud to partner with libraries to digitize public domain materials and make them widely accessible. Public domain books belong to the public and we are merely their custodians. Nevertheless, this work is expensive, so in order to keep providing this resource, we have taken steps to prevent abuse by commercial parties, including placing technical restrictions on automated querying.

We also ask that you:

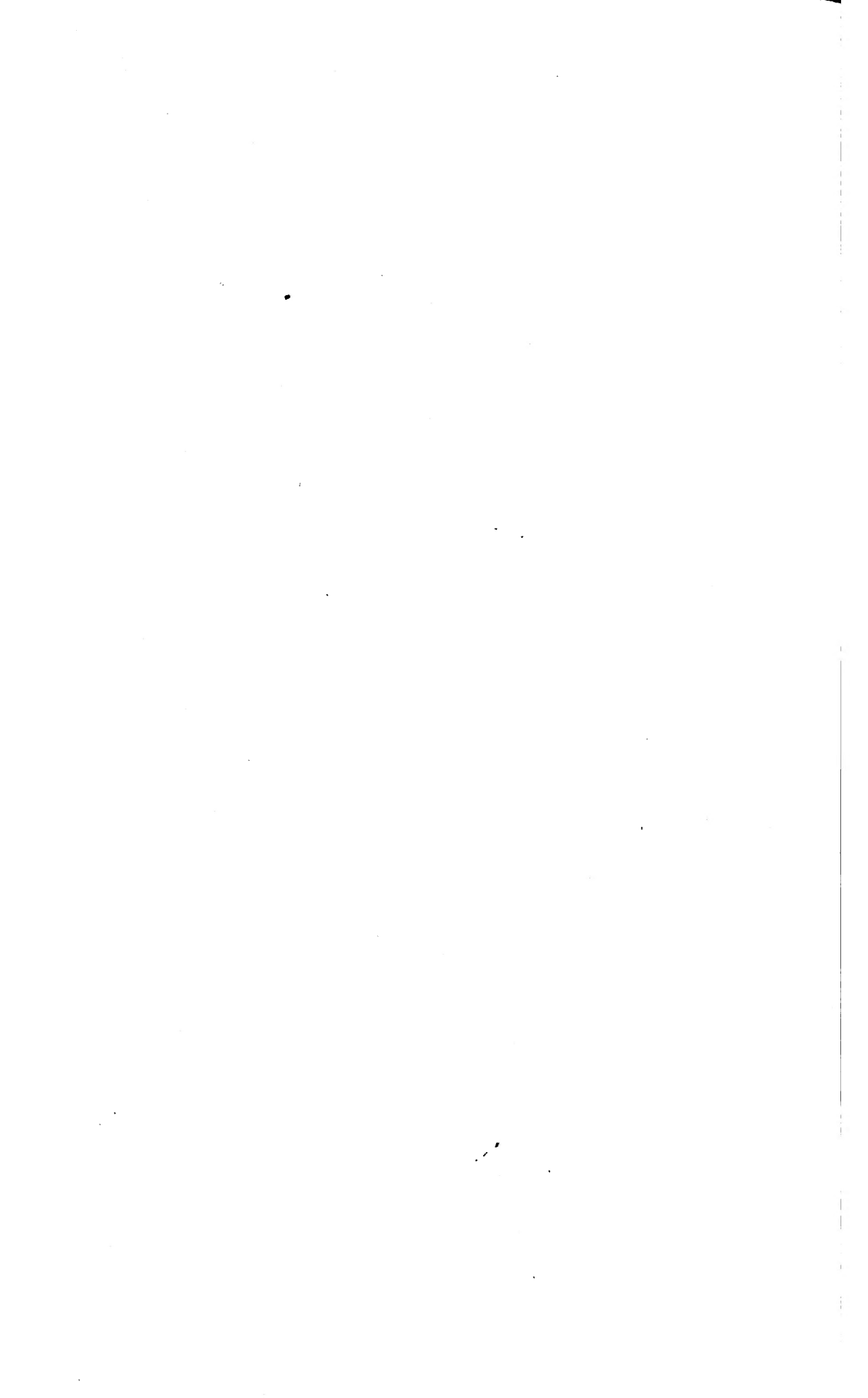
- + *Make non-commercial use of the files* We designed Google Book Search for use by individuals, and we request that you use these files for personal, non-commercial purposes.
- + *Refrain from automated querying* Do not send automated queries of any sort to Google's system: If you are conducting research on machine translation, optical character recognition or other areas where access to a large amount of text is helpful, please contact us. We encourage the use of public domain materials for these purposes and may be able to help.
- + *Maintain attribution* The Google "watermark" you see on each file is essential for informing people about this project and helping them find additional materials through Google Book Search. Please do not remove it.
- + *Keep it legal* Whatever your use, remember that you are responsible for ensuring that what you are doing is legal. Do not assume that just because we believe a book is in the public domain for users in the United States, that the work is also in the public domain for users in other countries. Whether a book is still in copyright varies from country to country, and we can't offer guidance on whether any specific use of any specific book is allowed. Please do not assume that a book's appearance in Google Book Search means it can be used in any manner anywhere in the world. Copyright infringement liability can be quite severe.

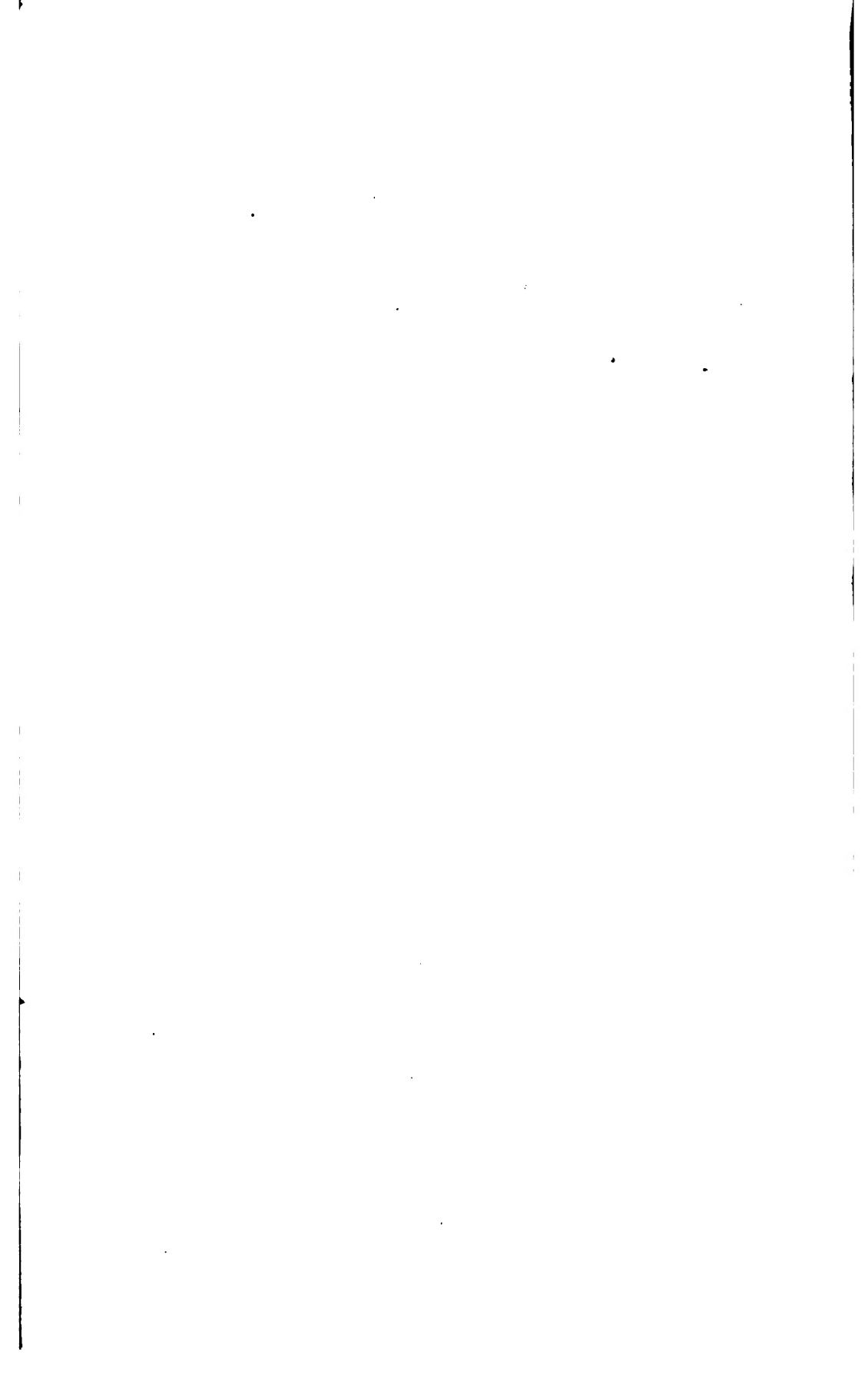
About Google Book Search

Google's mission is to organize the world's information and to make it universally accessible and useful. Google Book Search helps readers discover the world's books while helping authors and publishers reach new audiences. You can search through the full text of this book on the web at <http://books.google.com/>

LIBRARY
OF THE
UNIVERSITY OF CALIFORNIA.

Class





THE
PRACTICE OF NAVIGATION
AND
NAUTICAL ASTRONOMY.

THE
JOURNAL OF THE
ROYAL ANTHROPOLOGICAL INSTITUTE
OF GREAT BRITAIN AND IRELAND
VOLUME 100 PART 1 2000

THE
PRACTICE OF NAVIGATION
AND
NAUTICAL ASTRONOMY.

BY
HENRY RAPER, LIEUT. R.N., F.R.A.S., F.R.G.S.

NINETEENTH EDITION.

REVISED AND ENLARGED.

London:
PUBLISHED BY J. D. POTTER,
Admiralty Agent for Charts
145 MINORIES, E.
1908

Y-23

70 11/11
AMERICAN

TO

REAR-ADMIRAL SIR FRANCIS BEAUFORT,
K C.B.

HYDROGRAPHER TO THE ADMIRALTY.

SIR,

The eminent station which you occupy in the naval scientific world renders it highly gratifying to me to dedicate the following Work to you as a testimony of my regard and esteem; while the general accordance of my views on the subject with those of your more experienced judgment, gives me the greater confidence in laying my labours before the Public.

I have the honour to be,

Sir,

Your obedient Servant,

HENRY RAPER.

P R E F A C E

TO THE

F I R S T E D I T I O N .

THIS Work is intended for the use of all persons concerned either with the navigation of ships or with the determination of latitude and longitude on shore.

The present volume, which is devoted exclusively to the **PRACTICE**, contains all the rules and tables necessary in navigation, and for the determination of latitude and longitude by means of the sextant or reflecting circle. The study of its contents demands no previous attainments beyond the knowledge of the elements of arithmetic. Every endeavour has been made to render the whole easy of reference, and to adapt it to the use of those who may desire to instruct themselves. Rules which admit of more cases than one, as, for example, that for applying the equation of equal altitudes, are given in the form of *tables*; so that the several conditions involved, and their mutual connexion, being exhibited to the eye, the computer is relieved from the sense of complication, and the chance of a mistake is materially diminished. An ample alphabetical index is annexed, by which the reader is at once referred to all the information which the volume can afford him.

Those who have been brought up to the sea, and who have experienced the distaste for long calculations which that kind of life inspires, will not hesitate to admit that the only means of inducing seamen generally to profit by the numerous occasions which offer themselves for finding the place of the ship is extreme

brevity of solution. It is not, however, merely as a concession to indolence, that rules should be made as easy and simple as possible; the nature of a sea life demands that every exertion should be made to ~~bridge~~ computation, which has often to be conducted in circumstances of danger, anxiety, or fatigue, and so to separate the several points, that the seaman may be referred directly to what concerns his case, to the exclusion of all other matter. These considerations have been carefully kept in view in the rules, in the examples, and in the form and order of the tables.

Two kinds of solutions are employed, and, in general, two only; namely, an *approximate* method, and a complete, or, as it is called, *rigorous*, method. The former may often serve in cases of haste, or when precision is not necessary, and will also afford a convenient check against the effects of a mistake in the more elaborate method.

All the computations are effected by the well-known methods of inspection and logarithms; and as the former, it is presumed, leave but little to be desired in point of expedition, Gunter's scale, or other mechanical methods, are not employed.

Sailing on a Great Circle is, in this work, reduced, like Plane Sailing, to Inspection, by means of the SPHERICAL TRAVERSE TABLE.

Convenient rules are given for finding the distance of the land by its change of bearing, and by its altitude observed above the sea-horizon.

The seaman will find every necessary information on the subject of local magnetic deviation.

The highly useful problem of determining the latitude at sea, by the reduction of an altitude to the meridian, will be found greatly abridged; and a table is added for the purpose of shewing the limits within which the result may be depended upon when the time at ship is in error. This table will be found, it is presumed, of considerable utility, as it is perhaps from the want of some specific information as to the degree of confidence which it is safe to place in the result, no less than of a short and easy rule, that this excellent observation is almost entirely neglected; and, in consequence, the latitude, when the meridian altitude is not exactly obtained, is too often lost for the day.

The approximate solution of the double altitude, as a question of Time, will be found, it is hoped, well adapted to general use: since unless the latitude by account is very much in error this

method determines both the true latitude and the time at ship; and the computation of the time is one with which seamen are familiar in the next degree to that of the latitude by meridian altitude. The principle is not new, but rules have not hitherto been given for computing directly the error of the latitude by account.

The first approximate method of clearing the lunar distance is new, being effected, like many other problems, by the Spherical Traverse Table. The rigorous method is a modification of Borda's, and employs five logarithms, of which two only are taken out to seconds.

In a work in which many of the methods are new, I have felt it would be more satisfactory to the professional reader to find them illustrated by observations actually taken at sea. The examples are accordingly selected from the journals of Captain W. F. W. Owen, who kindly lent them to me for the purpose; though, necessarily, in proceeding by fixed rules, I could not introduce the solutions employed by that distinguished navigator. The remaining observations have been furnished to me by the Rev. G. Fisher, astronomer to Sir Edward Parry's expedition to the Polar Seas.

In order to enable the computer to judge of the degree of precision to which he attains, the *degree of dependance* to be placed on the result, or the limit of probable error, is indicated. This is the more important, as very indistinct and erroneous notions prevail among practical persons on the subject of accuracy of computation; and much time is, in consequence, often lost in computing to a degree of precision wholly inconsistent with that of the elements themselves. The mere habit of working invariably to a useless precision, while it can never advance the computer's knowledge of the subject, has the unfavourable tendency of deceiving those who are not aware of the true nature of such questions into the persuasion that a result is always as correct as the computer chooses to make it; and thus leads them to place the same confidence in all observations, provided only they are *worked* to the same degree of accuracy. By habitually following the short precepts laid down on this point, the computer will learn insensibly to estimate the value of his results; of which, since the limit of error is the sole criterion of the accuracy of any determination, he cannot otherwise be a judge. The degree of precision to which it is proper to carry the work in any case is observed, in general, in the examples.

In the Tables every endeavour has been made to render the

collection complete for the purposes required, and to compress the whole into small compass. For the sake of clearness, a different figure has been adopted for the argument and for the numbers in the body of each table. In the logarithms six places of figures only are employed, because a single result in which six places are necessary cannot be depended upon to the degree of precision obtained. On the same principle, some of the logarithms are given to three places only.

The log. sine square of half the arc, Table 61, universally familiar to seamen in finding the time, is given, for the convenience of this constant computation, to every second of the 12 hours. By means of this term tables of versed sines are dispensed with, all our solutions being either numeral or purely logarithmic.

I have not, either in the Rules or the Tables, aimed to make that additive which is in the nature of things subtractive. The precept *subtract* is as easy as the precept *add*; and when the student has the natural process before him he may be led to discover the reason of it; and must thus, by attention, always advance in knowledge of the subject. But an artificial process obstructs the exercise of the faculties, or leads the student, who reflects on what he does, to false conclusions.

The composition of the Table of MARITIME POSITIONS has been a very laborious task, and has caused great delay in the appearance of the Work. The numerous chronometric measures furnished of late years have rendered it necessary to deduce longitudes in a more systematic and accurate manner than that hitherto followed, which has chiefly consisted in modifying former determinations by means of those succeeding them. *Absolute*, or astronomical positions, and *relative* positions, being distinct things, and the latter being by far of the greater consequence to navigation, it is necessary, preparatory to a complete and final arrangement, to separate these two kinds of determinations. Accordingly, in a series of papers, some of which have been already published in the Nautical Magazine,* I have endeavoured to arrange the chronometric differences of longitude with reference to certain fixed points, convenient for the purpose, which it is proposed to call *Secondary Meridians*. These standard

* The *data* or evidence for the several positions being given in these papers, the value of each determination is easily appreciated; and accordingly, individuals in possession of one or more good watches may, by correcting defective measures, or by establishing new links of connexion, render material service to maritime geography. See Nautical Magazine, 1839, and following years.

positions, of which the number assumed is eighteen, being considerably distant from each other, are determined nearly enough for present purposes, and would, according to the system proposed, be finally settled by long series of astronomical observations.

An account of the principles adopted in this arrangement, and of the several voyages and surveys from which the materials have been taken, will be found, together with some suggestions for the advancement of the subject, in the *Nautical Magazine*. But it is necessary to state here, that the late determinations of the longitude of Madras have, from the importance of that position, occasioned a long and intricate discussion. Mr. Riddle and Mr. Maclear have compared observations of moon culminating stars made at Madras, with like observations made in Great Britain and at the Cape of Good Hope respectively. According to their computations, which agree very nearly, the received longitude, $80^{\circ} 17' 21''$, is about $3' 21''$ too great. The number and superior character of these observations, and the agreement of the results, have led me to adopt, without hesitation, $80^{\circ} 14' 0''$; while the magnitude of the correction has rendered it indispensable to trace its effects on the longitudes of the Eastern Seas.*

Precision in the Maritime Positions, especially in the longitudes, becomes, as navigation advances to perfection, a matter of increasing importance; because, where longitudes are well determined, the error of a chronometer may be ascertained on every occasion of making the land.

It will not be out of place to remark here that it is high time the chronometer should be found, like the compass, among the stores of every vessel beyond a mere coaster. It would be superfluous to attempt to prove that the hardships and privations consequent on missing a port, the losses of ships from being out in their reckonings, and the evils incident to navigation generally from the want of a ready means of checking the enormous errors to which the dead reckoning is liable, would, in many cases, have been prevented by a chronometer.

In urging this recommendation, it is, of course, taken for granted that they to whose hands the chronometer is entrusted are qualified to make a proper use of it. Employed merely as a check, a single chronometer cannot fail to prove of great service; but too firm a reliance on such an instrument would lead to the dangerous error

* The accepted Longitude of Madras, India Trigonometrical Survey, 1878 (see page 194), is $80^{\circ} 14' 51''$ E

of relaxing that vigilance which the known uncertainty of the dead reckoning keeps perpetually alive.

A list of times of high water, or, as they are now called, Establishments of Ports, is not given. The researches on the tides made of late years by Mr. Lubbock and the Rev. W. Whewell, have proved that the establishment cannot be truly deduced but from numerous observations, and consequently that a simple recorded time of high water is altogether insufficient. Moreover, if the establishment were correctly known, the time of high water, as also the height of the tide, cannot be determined without other elements, which, except in comparatively few places, are not afforded. But in navigation it is not the true instant of high or low water that is required so much as the time at which the flood or ebb stream turns, because this last affects every vessel when near the shore; and the proper place for information of this kind is, obviously, the Sailing Directions.

Although some results of the kind might be advantageously placed in a general work on navigation, yet the uncertainty of almost all that has been published, and the difficulty of collecting better materials, will, it is hoped, excuse the omission, at least for the present.

It may, however, be remarked, that under whatever form it may hereafter be found advisable to publish particulars of the tides, the observations required are so numerous, the discussions so tedious, and the whole subject so complicated, that no individual could undertake successfully to treat this branch of navigation unless in a work devoted exclusively to its consideration.

The subject of Maritime Surveying, usually treated in works of this kind, has been omitted. Surveying is no part of the navigation of a ship, and a survey having any pretensions to authority can scarcely be made by a person whose qualifications for the task are confined to the slender information contained in a few pages. A survey is a matter of too great consequence to the security of navigation to be received from incompetent hands; and the seaman who desires to acquire a knowledge of surveying should study works treating expressly of this branch of science.

The customary chapter on the Winds has likewise been omitted. The subject, generally, does not belong to the navigation of a ship; and, even if it did, the general information contained in a few pages, though interesting as a branch of natural philosophy, is

necessarily too vague to be effective in shaping the course. The same applies to Currents, and also to the Marine Barometer; which, though matters of important consideration in sea-voyages, are not concerned in the practice of navigation, since this term, in strictness, comprehends only the consideration of the place of the ship when her circumstances and destination are given.

The space gained by the omission of these collateral subjects, and other matters sometimes introduced, is appropriated to the numerous practical details of the proper subjects of such a treatise.

The Work will be completed by another volume, which will be entitled the **THEORY OF NAVIGATION**, and will contain the construction of the rules and tables, for the advantage of those who desire to confirm their practical knowledge by mathematical investigation. It will contain, likewise, those methods in which the transit and azimuth instruments are employed. The present volume being thus, in the ordinary practice of navigation, independent of the second, no notice of another volume appears in the title-page.

By the term Theory is commonly understood, in this particular subject at least, the scientific principles on which the rules are formed. Considerations of this kind are thus altogether excluded from the present volume; but, on the other hand, that *rationale*, or process of reasoning, which, in considering the nature of the case, is obvious to common sense or apprehension, is, in most cases, introduced, as necessary to a clear understanding of important points.

The theory and the practice are thus kept purposely distinct. The former is not always necessary to successful practice; and rules constructed for ready and general application approach to perfection in proportion as they leave less to individual judgment or skill. It is the custom, generally, to teach the theory first; the impression forced upon me is, on the contrary, that the practice is itself the best foundation for sound and rapid advancement in the theory. For he who has acquired the practice knows the nature and extent of the subject; and in proceeding to the theory he has a distinct perception of the object to be attained. This is not the place for a discussion on these points; but it was incumbent on me to state, in a few words, the grounds of the arrangement adopted.

It is manifestly the duty of a writer, who undertakes to treat a subject in a thoroughly practical manner, not only to discuss every point which presents itself, but also to pronounce a decided opinion in every case. It is proper to bring this point under the notice of

the reader, who, especially if he has more experience in these matters than myself, might otherwise be disposed to consider many things in this volume as laid down too positively.

I cannot close the preface to a work which has been some years in preparation, and in which I have endeavoured to reduce to a practical form every useful consideration which has been suggested by my own experience or by intercourse with eminent officers and men of science, without soliciting the indulgence of the reader to errors and to deficiencies. Absolute correctness, especially in tables, is scarcely attainable; and in a treatise which contains much that has not appeared before, I cannot reasonably flatter myself that, notwithstanding every care and attention, some small inaccuracies may not be found.

H. R

September 1840

ADVERTISEMENT

TO THE

THIRD EDITION.

IN the Advertisement to the Second Edition I had the satisfaction of being able to state that the Royal Geographical Society had conferred the flattering distinction of their gold medal on the first edition, and that the Lords Commissioners of the Admiralty had honoured my work by ordering it to be supplied to Her Majesty's Navy as ship's stores.

The present edition has been greatly augmented. Much of the work has been rewritten. Two approximate methods of determining the time, though of inferior value, are introduced, since a work aiming to be complete for practice should contain provision for extreme cases. Nos. 789, 791.

The introductory portion, it had often been suggested, was insufficient for the purposes of elementary instruction. It is easier to allege this, than to lay down a condition which is to determine the extent of such preliminary matter. An attempt, however, has been made to fix a limit, on the following grounds:—

The most general defect, perhaps, in the education of seamen, as regards the present subject, is an insufficient knowledge of arithmetic; by which I mean, not of the more advanced rules, but of the elements, and especially of proportion. Now all questions to which arithmetical processes are applied involve some *proportion*, which the operation is to bring out, or distinctly assign; and it appears, accordingly, a great omission in our education that we are not more exercised on this point, which is the sole object or end of the processes which we learn to practise mechanically.

Again, in geometry, it is not the variety of problems which benefits the practical man, but a well-grounded and familiar knowledge of a few comprehensive propositions, which he applies readily, and with confidence; and the geometrical knowledge which appears to me to suffice to our present purpose is comprised in,—1, the property of the square of the hypotenuse; 2, the measure of an angle at the circumference; 3, the similarity of plane triangles. The first is of general importance; the second includes the problem of fixing a station by means of two angles subtended by three objects; and the third is the basis of trigonometry.

In this edition, therefore, proportions and fractions are treated at some length, and illustrated by numerous examples which afford the student abundant exercise; and a short course of geometry is given, after the manner of Euclid, sufficient to establish the above important theorems.

These limitations, the reader will bear in mind, are intended to apply only to that particular quantity of elementary matter which is assumed to be necessary and sufficient for the scale of attainment contemplated in the present volume.

In the Table of Positions many points of information of consequence to seamen are expressed by means of a new system of Symbols. In these days little apology is required for introducing a scheme which a few years ago would have been deemed a rash innovation. But a growing tendency to the use of symbols manifests itself on all sides. Efforts have been made to represent, as far as possible, all matters of instruction under a form addressed to the eye;* and symbols effect this object in an eminent degree, for their distinct and conspicuous forms, contrasting with the monotonous aspect of alphabetic writing, arrest and fix the attention, while their extreme conciseness admits the insertion of matters to which, for want of room, no allusion could otherwise be made.

The employment of symbols, therefore, on a more extensive scale than we have yet been used to, and that at no distant period, may be considered inevitable; and the present system, which has occupied my attention for several years, is proposed as so far deserving consideration that it is constructed with rigid adherence to principles.† The number of signs which I have ventured to

* The Physical Atlas is an example.

† The necessity for a uniformity in hydrographic symbols has already shewn itself. Symbols similar in character denote, on the French charts, rocks *above* the water, and on the Russian charts rocks *below* the water.

introduce is small, since, in matters waiting the sanction of experience, it is better to move too slow than too fast.

The introduction of symbols has necessarily modified the original design of the work, as described in the preface, and has justified allusion to many matters which otherwise would not have found a place in it.

The chief labour of this edition (as, indeed, of the two former) has been the Table of Positions, which, in consequence of the numerous references made to my labours in this country and abroad, I was desirous to extend. The list now contains 8,800 places; and as the degree of accuracy is indicated wherever I have found the means of forming a judgment, and as many physical details are supplied,—such as the dimensions of islands, heights, and the depths of shoals,—the table may be considered as representing the state of maritime geography at this day. The number of voyages, charts, and surveys, which it has been necessary to consult,—the labour of digesting and comparing the mass of materials collected, and the introduction, by a new method, of numerous details important to navigation,—will, it is hoped, excuse the long delay in the appearance of this edition, and account for the work having remained out of print for nearly three years.

In conclusion, I gladly express my obligation to the draftsmen and other gentlemen of the Hydrographic Office, whose patience during many years I have sorely taxed in the inspection and re-examination of thousands of documents, and without whose active and disinterested assistance I must have left much in a very unsatisfactory state.

ADVERTISEMENT

TO

THE NINETEENTH EDITION.

THE revision and enlargement of this edition of the "Practice of Navigation and Nautical Astronomy" was undertaken with considerable diffidence, it being felt, that while it was possible to spoil, little could be done to improve, this best of practical works on Navigation at Sea.

Compiled in the golden age of practical Navigation and Nautical Surveying by an officer in constant communication with Beaufort and Horsburgh, and the Captains and Masters who served under these distinguished chiefs in England and India, Lieutenant Raper's labours are founded upon a thorough practical experience, and may be looked upon as the work of a Sailor for the use and benefit of Sailors at Sea.

One chapter alone required to be re-written. The use of iron in modern shipbuilding, by its natural effect on the Mariner's Compass, having greatly increased the difficulties of navigation at sea, some additions have therefore been made to what Raper had already written upon this important subject. This chapter, as well as all parts of the book referring to the variation and deviation of the compass, has been re-written by Captain W. Mayes, R.N., late Superintendent of Compasses at the Admiralty.

Captain Mayes has also assisted in making a careful examination of the whole work, which is sufficient guarantee for its having been thoroughly done.

This scrutiny showed how well and earnestly Raper had carried out the intention expressed in the Preface to his First Edition* (see p. v) of "inducing seamen to profit by the numerous occasions

* Sailors are earnestly requested to read the Preface to the First Edition.

which offer themselves for finding the place of the ship ;” by laying before them methods whose “ extreme brevity of solution abridged computation.” These short rules aid the prompt decision upon which the safety and success of a ship at sea so often depend. A brief study of the comprehensive index will call attention to “ the numerous occasions ” alluded to.

The key to most of the modern short methods for fixing the position of the ship will be found in Raper’s “ Practice of Navigation.”

Under the head of “ Degree of Dependance ” is placed before the navigator the amount of possible error, a thought which should never be absent from his mind in considering the estimated position of a ship, with the view of determining his future proceedings.

The sailor’s attention is earnestly called to the chapter entitled “ Navigating the Ship,” which contains what John Davis, the navigator, writing in 1607, aptly termed the “ Seaman’s Secrets.”

In this, the concluding chapter of the work, Raper shows clearly the never ceasing watchfulness that is required, in both fair and foul weather, in obtaining the observations, terrestrial as well as celestial, necessary to conduct a vessel in safety from one port to another.

The simplicity of its mathematical theory makes Navigation appear an easy matter to men teaching or using it on shore ; but Pilotage, common and proper, is a very different business when practised by sailors in a gale of wind, at night, or in hazy weather, on board a ship at sea. Proficiency in the science can never compensate for a lack of experience in the handicraft of navigation. This experience can be attained only by incessant practice at sea ; by a capacity for taking trouble, unceasing caution, and a desire to do well.

In such labours the sailor will find no better friend and assistant than Raper’s “ Practice of Navigation.”

No changes in the numbering of the paragraphs have been made, and great care has been taken to leave the book in the style in which it was originally written, so that old students will have no difficulty in finding the various methods with which they are familiar.

Some slight changes have been made in the Tables. Considering the great increase of speed attained by modern steamships, Table 1, formerly Table 2, has been enlarged from 300 to 600 miles of distance. The Table giving the Diff. lat. and Departure for every quarter point has been withdrawn.

Table 10, of Maritime Positions, upon which Raper bestowed a very large amount of labour, has been revised with great care from the latest Admiralty Charts, so that it may still "be considered as representing the maritime geography of this day" (see p. xv). These positions mainly depend on the Table of Longitudes accepted for Secondary Meridians, amended from telegraphic observations to 1887, published in the Admiralty "Instructions to Hydrographic Surveyors." This Table of Secondary Meridians has been inserted in the Explanation of Table 10.

Steam having in a great measure rendered Table 12 obsolete, it has been replaced by a Table of the navigable Mercatorial Distances between the principal ports and points of the world.

Tables 11 and 13 (Approximate Variation of the Compass, and Tide-hours, or Establishment of the Ports) have been taken out, as the Admiralty Charts, and Admiralty and Indian Tide Tables, published yearly; with the Chart of Curves of Equal Magnetic Variation (No. 2598), corrected up to date; always give the latest information. These tables have been replaced by others showing first: where docks &c. may be found and coals obtained; and second, the position and nature of the Time signals, in all parts of the world, for the correction and rating of chronometers.

Table 65, of natural sines, tangents, &c., to assist magnetic computations, has been inserted in lieu of that of log. sines, tangents, &c., to quarter points.

With these few exceptions the Tables retain the same numbers they held in former editions.

In conclusion, thanks are due to Captain John C. Almond, Nautical Inspector of the P. and O. Company, for his many valuable suggestions.

THOMAS A. HULL.

MAKER, HONOR OAK:
December 21, 1890.

In this reprint of the Nineteenth Edition, the Sun's declination, the Sidereal Time, and the Equation of Time have been given for the years 1901, 1902, 1903 and 1904, in Tables 60, 61, and 62. Table 60A, correction of Sun's declination in Table 60 to 1928, has been restored. Tables 10, 12, and 13 have been brought up to date. Table 38, Corrections of Altitudes of Sun and Stars, has been extended, and the gross corrections are given for 'Height of the eye' up to 60 feet. Table 47, Limits of the Reduction to the Meridian at Sea, has been recast. Table 70, Logarithms for computing the Reduction to the Meridian at Sea, has been extended to 35° of declination. Tables 41 and 52 have also been recast.

CONTENTS.

INTRODUCTION.

	PAGE
I. FRACTIONS	1
II. PROPORTION	10
III. LOGARITHMS	18
IV. PRACTICAL GEOMETRY	21
V. GEOMETRY AND PLANE TRIGONOMETRY	32
VI. METHODS OF SOLUTION.....	50
VII. SPHERICAL TRIGONOMETRY	55A

NAVIGATION.

CHAP I. DEFINITIONS	55
II. INSTRUMENTS OF NAVIGATION	63
I. THE COMPASS	63
" " VARIATION OF	70
" " DEVIATION OF	73
" " ADJUSTMENT OF	81
MAGNETIC MAPS	82
II. THE LOG AND GLASSES.....	104
SEXTANT, PROTRACTOR, AND STATION-POINTER	143 & 178
III. THE SAILINGS	106
I. PLANE SAILING, WITH TRAVERSE, CURRENT, AND WINDWARD SAILINGS.....	106
II. PARALLEL SAILING, WITH MIDDLE LATITUDE, AND MERCATOR'S SAILINGS	119
III. GREAT CIRCLE SAILING	129
IV. TAKING DEPARTURES	137
I. BY A SINGLE BEARING AND DISTANCE	137
II. DETERMINATION OF DISTANCE.....	137
III. METHODS BY THE CHART.....	143
V. CHARTS	145
I. USE OF MERCATOR'S CHART	146
" PROJECTION OF A GREAT CIRCLE.....	147
II. CONSTRUCTION OF MERCATOR'S CHART	149
III. PROPERTIES OF CERTAIN PROJECTIONS	149
VI. SOUNDING	151

	PAGE
CHAP. VII. THE SHIP'S JOURNAL	154
I. KEEPING THE SHIP'S JOURNAL	154
II. THE DAY'S WORK.....	155

NAUTICAL ASTRONOMY.

I. DEFINITIONS	161
II. INSTRUMENTS OF NAUTICAL ASTRONOMY	178
I. THE REFLECTING INSTRUMENTS, SEXTANT	176
II. THE ARTIFICIAL HORIZON	188
III. THE CHRONOMETER	191
III. TAKING OBSERVATIONS	193
I. OBSERVING ALTITUDES	193
II. OBSERVATIONS WITH AND WITHOUT ASSISTANTS ...	201
III. EMPLOYMENT OF THE HACK WATCH	202
IV. FINDING THE STARS	203
IV. SUBORDINATE COMPUTATIONS	205
I. THE GREENWICH DATE	206
II. REDUCTION OF THE ELEMENTS IN THE NAUTICAL ALMANAC	207
III. CONVERSION OF TIMES	216
IV. HOUR-ANGLES	218
V. TIMES OF CERTAIN PHENOMENA	224
VI. ALTITUDES	230
VII. AZIMUTHS	240
V. FINDING THE LATITUDE	243
I. BY THE MERIDIAN ALTITUDE	243
II. BY THE REDUCTION TO THE MERIDIAN	249
III. BY DOUBLE ALTITUDE OF THE SAME BODY	255
IV. BY DOUBLE ALTITUDE OF DIFFERENT BODIES	270
V. BY THE ALTITUDE OF THE POLE STAR	277
VI. FINDING THE TIME	278
I. BY A SINGLE ALTITUDE	278
II. BY DIFFERENCE OF ALTITUDE NEAR THE MERIDIAN	285
III. BY EQUAL ALTITUDES	287
IV. RATING THE CHRONOMETER	293

CONTENTS.

xxi

	PAGE
VII. FINDING THE LONGITUDE	297
I. BY THE CHRONOMETER	297
II. BY THE LUNAR OBSERVATION	301
III. BY THE MOON'S ALTITUDE	319
IV. BY AN OCCULTATION.....	322
V. BY ECLIPSES OF JUPITER'S SATELLITES	325
VIII. FINDING THE VARIATION OF THE COMPASS	326
I. BY THE AMPLITUDE	326
II. BY THE AZIMUTH	328
III. BY ASTRONOMICAL BEARINGS	331
IV. BY TERRESTRIAL BEARINGS.....	333
IX. THE TIDES	335
I. PHENOMENA OF THE TIDES	336
II. RULES FOR FINDING THE TIME OF HIGH WATER...	341
III. TIDE OBSERVATIONS	345

NAVIGATING THE SHIP.

I. SHAPING THE COURSE	347
II. PLACE OF THE SHIP.....	351
III. DETERMINING THE CURRENT	364
IV. MAKING THE LAND	366
EXPLANATION OF THE TABLES.....	377

TABLES.

NAVIGATION.

THE SAILINGS :—

TABLE	PAGE	Explanation	PAGE
1. Traverse Table to Degrees	432		377
3. Departure and Corresponding Difference of Longitude	522	"	381
4. Difference of Longitude and Corresponding Departure	523	"	381
5. Spherical Traverse Table	524	"	382
6. Meridional Parts	533	"	385

DEPARTURES :—

7. For finding the Distance of an Object, by Two Bearings and the Distance run between them	538	"	386
8. True Depression or Distance of the Sea Horizon	539	"	386
9. Number of Feet subtending an Angle of 1' at different Distances	539	"	387
10. Maritime Positions *	540	"	387
11. Places at which Docks may be found, Coals obtained, &c.	634	"	406
12. Navigable Mercatorial Distances	635	"	406
13. Time Signals	644	"	407

TIDES :—

14. Epacts	646	"	407
15. Semimenstrual Inequality	646	"	407
16. Approximate Rise and Fall of the Tide	646	"	407

NAUTICAL ASTRONOMY.

REDUCTION OF THE ELEMENTS IN THE NAUTICAL ALMANAC :—

17. For converting Arc into Time	647	"	408
18. For converting Time into Arc	647	"	408
19. Correction of the Sun's Declination, at Sea	648	"	408

* Table of Longitudes accepted for Secondary Meridians, 392.

CONTENTS.

xxiii

TABLE	PAGE	PAGE
20. Correction of the Equation of Time, at Sea	648	Explanation 408
21. For reducing Daily and Twelve-hourly Variations	649	" 408
21A. Logarithms for reducing Daily Variations	655	" 409
22. For reducing the Moon's Declination ...	657	" 409
23. Acceleration	659	" 409
24. Retardation	659	" 409
25. For finding the Equation of Second Differences	660	" 409

TIMES OF CERTAIN PHENOMENA:—

26. Apparent Time of the Sun's Rising and Setting	661	" 410
27. Approximate Apparent Times of the Meridian Passages of the principal Fixed Stars	664	" 410
27A. Correction of the Times in Table 27 ...	665	" 410
28. Correction of the Time of the Moon's Meridian Passage	665	" 410
29. Hour-angle and Altitude of a Body upon the Prime Vertical	666	" 411

ALTITUDE:—

30. Apparent Dip of the Sea Horizon	671	" 411
31. Mean Astronomical Refraction	671	" 412
32. Correction of the Mean Refraction for the Height of the Thermometer	672	" 412
33. Correction of the Mean Refraction for the Height of the Barometer	673	" 412
34. The Sun's Parallax in Altitude, and Semidiameter	673	" 413
35. Dip of the Shore Horizon	673	" 413
36. Corresponding Thermometers	674	" 413
37. Corresponding French and English Measures	674	" 413
38. Corrections of Altitude of the Sun and Stars	675	" 414
39. Correction of the Moon's apparent Altitude	676	" 414
40. Corresponding Horizontal Parallax and Semidiameter of the Moon	685	" 414

b

TABLE	PAGE	PAGE
41. Correction of the Moon's Equatorial Parallax for the Figure of the Earth .	685	Explanation 414
42. Augmentation of the Moon's Semidiameter	685	" 415
43. Correction for reducing the true Altitude of the Sun or a Star to the apparent Altitude	686	" 415
44. Correction for reducing the true Altitude of the Moon to the apparent Altitude	686	" 415
45. Parallax in Altitude of a Planet	686	" 415
46. Azimuth and corresponding Change of Altitude in One Minute of Time	687	" 415

LATITUDE :—

47. Limits of the Reduction to the Meridian at Sea	688	" 415
48. Value of the Reduction at which the Second Reduction amounts to 1'	688	" 416
49. For computing the Reduction to the Meridian in Seconds	689	" 416
50. For computing the Second Reduction in Seconds	691	" 416
51. Correction of the Altitude of the Pole Star	692	" 417
52. Reduction of Latitude	693	" 417

LONGITUDE :—

53. Correction of the Lunar Distance for the Contraction of the Vertical Semidiameter	693	" 417
54. Error of Observation arising from an Error of the Parallelism of the Line of Sight	693	" 418
55. For correcting the Lunar Distance for the Spheroidal Figure of the Earth... ..	693	" 418
56. For computing the Moon's Second Correction of Distance.....	694	" 418
57. Correction of the Greenwich Mean Time for the Second Difference of the Lunar Distance	695	" 419
58. Error of the Ship's Place in Nautical Miles, and of the Longitude in Time, corresponding to an Error of 1' in the Lunar Distance	695	" 419

CONTENTS.

XXV

VARIATION OF THE COMPASS :—

TABLE	PAGE	PAGE
59. Amplitudes.....	696-7	Explanation 419
59A. Correction of the Amplitude observed on the Horizon, for the Effect of Re- fraction	696-7	„ 420

TO SUPPLY THE PLACE OF THE NAUTICAL ALMANAC :—

60. Declination of the Sun.....	698	„ 420
60A. Correction of the Sun's Declination	700	„ 420
61. Sidereal Time and Right Ascension of the Sun	701	„ 421
62. The Equation of Time	703	„ 421
63. Mean Places of Stars	705	„ 421

LOGARITHMS :—

64. Logarithms of Numbers	706	„ 422
64A. Spheroidal Tables	724	„ 423
65. Natural Sines, Cosines, Tangents, Co- tangents, Secants, and Cosecants	725	„ 423
66. Log. Sines of small Arcs to each Second	726	„ 423
67. Log. Sines of small Arcs to Ten Seconds	735	„ 424
68. Log. Sines, Cosines, Tangents, Cotangents, Secants, and Cosecants.....	738	„ 424
69. Logarithm of the Square of the Sine of Half the Arc	828	„ 426
70. Logarithms for computing the Reduction to the Meridian, at Sea	893	„ 427
71. Logarithms for computing the Correction of the Latitude by Account.....	897	„ 428
72. Logarithms for computing the Equation of Equal Altitudes	899	„ 428
73. The Logarithmic Difference	900	„ 428
74. Proportional Logarithms.....	909	„ 429

ABBREVIATIONS ADOPTED ON ADMIRALTY CHARTS, WITH EXPLANATORY NOTES

GENERAL INDEX.....

MAPS OF BOTH HEMISPHERES *To be placed between pages 82 and 83*

DIAGRAM TO ILLUSTRATE SUMNER'S METHOD FOR FINDING THE
POSITION OF A SHIP AT SEA *To face page 363*

INTRODUCTION.

I. FRACTIONS. II. PROPORTION. III. LOGARITHMS. IV. PRACTICAL GEOMETRY. V. RAISING THE TRIGONOMETRICAL CANON. VI. METHODS OF SOLUTION.

1. *Vulgar Fractions.*

1. A NUMBER which is a portion of 1, or unity, is properly called a *fraction*; thus, if we divide a foot into 3 equal parts, each of such parts is the fraction called a *third*, and written $\frac{1}{3}$.

These numbers arise, in arithmetical operations, in division, when the dividend is not divisible by the divisor in whole numbers, or, as they are called, *integers*; thus, if we divide 10 feet into 3 equal parts, each will measure 3 ft. and one-third, or 10 divided by 3 gives the quotient 3, and 1 over—that is, 1 not divided like the rest; but proceeding now to divide this 1 by 3, we call the result or quotient $\frac{1}{3}$; that is, 1 *divided by* 3.

2. If we divide 1 into four equal parts, each is one-fourth, written $\frac{1}{4}$; if into 5 equal parts, each is one-fifth, written $\frac{1}{5}$; thus, the *name of the fraction* is that of the *number of parts* into which the unity or entire quantity is divided; and this number is hence called the *denominator* of the fraction.

3. If we take two of three equal parts of subdivision, or two-thirds, we write $\frac{2}{3}$; if we take three of four equal subdivisions, we write $\frac{3}{4}$; if we take three of seven equal subdivisions, we write $\frac{3}{7}$; and so on: the number 2, 3, in these examples, which shews or enumerates the number of fractional parts taken, is hence called the *numerator*.

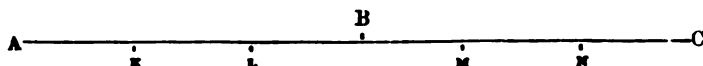
The term fraction is thus used to denote not only one part or subdivision, but any number of such.

4. In enumerating fractional parts we may go on, for example, $\frac{1}{3}$, $\frac{2}{3}$, $\frac{3}{3}$, $\frac{4}{3}$, $\frac{5}{3}$, $\frac{6}{3}$, &c. Here $\frac{3}{3}$ represents the whole, or entire quantity, since it enumerates as many parts as the whole is divided into; the fractions (so called) beyond this, as $\frac{4}{3}$, $\frac{5}{3}$, are all greater than 1, and are termed mixed or *improper* fractions.

5. The fractions to the left of $\frac{3}{3}$ are less than 1, and are *proper fractions*; hence, when the numerator is less than the denominator, the fraction is less than 1; when equal, the fraction represents 1; and when greater, it is greater than 1, and is capable of being resolved into a whole number with or without a fraction.

Hence also, the greater the denominator the smaller the fraction, and the smaller the denominator the larger the fraction.

6. If we take a line AB, and divide it into 3 equal parts by the points K, L; and another line BC equal to it, and divided similarly at M, N, then AL is $\frac{2}{3}$ of AB, or of 1.



Then the parts being all equal, AK and KL, are equal to LB and BM, and these to MN and NC; therefore AK and KL are $\frac{1}{3}$ of AC, that is, of 2. Hence AL is $\frac{2}{3}$ of 1, and $\frac{1}{3}$ of 2; or, $\frac{1}{3}$ of 2, and $\frac{2}{3}$ of 1 are the same thing. If AB is 1 yard, it is evident at once, since 2 ft. or $\frac{2}{3}$ of 1 yard are $\frac{1}{3}$ of 6 feet, or 2 yards.

7. The value of a fraction is not changed by multiplying the numerator and denominator by the same number.

The term one-half is equivalent to two-quarters, to four-eighths, and so on; that is $\frac{1}{2}$, $\frac{2}{4}$, $\frac{4}{8}$, &c. are all equal; since it is evident that the result is the same if we divide the whole into twice the number of parts, and take twice the number, or into 3 times the number of parts, and take 3 times as many of them. The above fractions are $\frac{1}{2}$, the numerator and denominator being both multiplied successively by 2.

Again, take $\frac{2}{3}$, multiply both numerator and denominator by 3, it becomes $\frac{6}{9}$: if now we take a line and divide it into 5 equal parts, and 15 equal parts, it will be the same thing whether we take two of the larger parts, or six of the smaller, which are $\frac{2}{3}$ the size.

8. The value of a fraction is not changed by dividing the numerator and denominator by the same number. This appears in exactly the same way as the above, in any case; thus, $\frac{6}{9}$, dividing both numerator and denominator by 3, gives $\frac{2}{3}$. The process is equivalent to dividing the unit into larger portions, and taking fewer of them in proportion.

Fractions are thus often simplified: example, $\frac{22}{33}$ is evidently reducible to $\frac{2}{3}$; $\frac{36}{48}$ to $\frac{3}{4}$.*

* A fraction is reduced to its simplest terms by finding their *greatest common measure*, that is, the largest number which will divide them both without a remainder. To find the greatest common measure of two numbers,

Divide the greater by the less. Consider the remainder as a new divisor to the former divisor as a dividend, and find the next remainder. Consider the last remainder as a new divisor, and find the next remainder, and so on. The last divisor is the number required.

If the last divisor is 1, the numbers have no common measure but 1, that is, are not further reducible.

Ex. 1. Find the greatest common measure of 24 and 124.

$$\begin{array}{r} 24 \overline{)124} 5 \\ \underline{120} \\ 4 \overline{)24} 6 \\ \underline{24} \\ 0 \end{array}$$

Ans. 4.

Ex. 2. Find the greatest common measure of 48 and 11.

$$\begin{array}{r} 11 \overline{)48} 4 \\ \underline{44} \\ 4 \overline{)11} 2 \\ \underline{8} \\ 3 \overline{)4} 1 \\ \underline{3} \\ 1 \end{array}$$

Ans.

[1.] *Reduction to a Common Denominator.*

9. Suppose it is required to add together $\frac{2}{3}$ and $\frac{1}{5}$; if we could at once express thirds in fifths, or fifths in thirds, we should then merely enumerate the number of parts; but as one of these fractions is no exact number of times greater than the other, (as may be seen by dividing a line into 5 parts and 3 parts), we cannot do this. But by multiplying the numerator and denominator of one by some number, and of the other by some other number, (which leaves the fractions unchanged in value, No. 6) we may select such multipliers as will produce the same number in the denominator; thus, multiplying the numerator and denominator of $\frac{2}{3}$ by 5, gives $\frac{10}{15}$, and multiplying the numerator and denominator of $\frac{1}{5}$ by 3 gives $\frac{3}{15}$, and the fractions $\frac{2}{3}$ and $\frac{1}{5}$ are thus reduced to 15ths.

Again, to reduce $\frac{1}{3}$ and $\frac{1}{4}$ to the same denominator, multiply the numerator and denominator of $\frac{1}{3}$ by 4, which gives $\frac{4}{12}$, and $\frac{1}{4}$ by 3, which gives $\frac{3}{12}$. These reductions are effected by multiplying each numerator by the *other* denominator, and the two denominators together; and the same applies to three or more fractions taken in succession. Hence the

Rule: Multiply the numerator of each fraction by every denominator, except its own, for the new numerator, and multiply all the denominators together for the new denominator.

Ex. 1. Reduce $\frac{2}{3}$, $\frac{1}{15}$, and $\frac{1}{7}$ $\frac{2 \times 15 \times 7}{3 \times 15 \times 7}$, $\frac{1 \times 3 \times 7}{3 \times 15 \times 7}$, $\frac{1 \times 3 \times 15}{3 \times 15 \times 7}$, or $\frac{210}{315}$, $\frac{21}{315}$, $\frac{45}{315}$.

Ex. 2. Reduce $\frac{11}{17}$, $\frac{1}{2}$, and $\frac{4}{7}$ $\frac{11 \times 2 \times 7}{17 \times 2 \times 7}$, $\frac{1 \times 17 \times 7}{17 \times 2 \times 7}$, $\frac{4 \times 17 \times 2}{17 \times 2 \times 7}$, or $\frac{154}{238}$, $\frac{119}{238}$, $\frac{136}{238}$.

Ex. 3. Reduce $\frac{2}{5}$, $\frac{5}{12}$, and $\frac{6}{7}$ $\frac{168}{420}$, $\frac{175}{420}$, $\frac{360}{420}$.

10. The process of reduction to a common denominator is often necessary in the comparison of two fractions, to find which of the two is the greater; thus, to compare $\frac{1}{3}$ and $\frac{1}{4}$, these become $\frac{4}{12}$ and $\frac{3}{12}$, hence $\frac{1}{3}$ is the greater.

11. Whole numbers are written in the fractional form by employing 1 as the denominator; thus 3 is written $\frac{3}{1}$, the 1 is in the place of the unit divided into 1 part (No. 2), that is, left entire, and the 3 denotes that 3 such parts are taken (No. 3).

12. By means of this last notation whole numbers are reduced to fractions with the same denominator, by the rule No. 9. Thus 11 and $\frac{1}{2}$, or $\frac{11}{1}$ and $\frac{1}{2}$ become $\frac{44}{2}$ and $\frac{1}{2}$.

[2.] *Addition.*

13. Reduce the fractions to a common denominator, add the numerators (No. 9), and under the sum place the common denominator.

Ex. 1. Add together $\frac{3}{17}$ and $\frac{2}{3}$. These become $\frac{3 \times 3}{17 \times 3} = \frac{9}{51}$, and $\frac{2 \times 17}{3 \times 17} = \frac{34}{51}$; the sum of which is $\frac{43}{51}$.

Ex. 2. Add together $\frac{1}{2}$, $\frac{1}{4}$, and $\frac{1}{8}$. Ans. $\frac{7}{8}$.

Ex. 3. Add $\frac{8}{10}$, $\frac{2}{7}$, and $\frac{3}{100}$. Ans. $\frac{7810}{7000} = 1\frac{81}{700}$.

Ex. 4. Add $\frac{3}{10}$, $\frac{2}{16}$, and $\frac{1}{3}$. Ans. $\frac{364}{480} = \frac{91}{120}$.

[3.] Subtraction.

14. Rule: Reduce the fractions to a common denominator, and subtract the lesser numerator from the greater for a numerator. Thus, suppose it required to subtract $\frac{1}{3}$ from $\frac{1}{2}$, these become $\frac{2}{6}$ and $\frac{2}{6}$, and $\frac{2}{6}$ from $\frac{2}{6}$ leaves $\frac{0}{6}$, the remainder required.

Hence it appears that the difference between $\frac{1}{2}$ part and $\frac{1}{3}$ part is $\frac{1}{6}$ of the whole.

Ex. 1 Find the difference between $\frac{3}{7}$ and $\frac{2}{5}$. These become $\frac{15}{35}$ and $\frac{14}{35}$, the difference of which is $\frac{1}{35}$.

Ex. 2. Subtract $\frac{1}{33}$ from $\frac{2}{11}$. Ans. $\frac{55}{363}$.

Ex. 3. Subtract $\frac{12}{13}$ from $\frac{11}{5}$. Ans. $\frac{83}{65} = 1\frac{18}{65}$.

[4.] Multiplication.

15. To multiply a fraction by a whole number is to repeat the fraction a given number of times; that is, to multiply $\frac{1}{3}$ by 3, or to take $\frac{1}{3}$ three times, gives $\frac{1}{1}$. Hence to multiply a fraction by a whole number is to multiply the numerator.

Hence a number multiplied by a (proper) fraction is diminished; thus, 3 multiplied by $\frac{1}{3}$, which is $\frac{2}{3}$, is less than 3.

16. To multiply a fraction by a fraction, as for example $\frac{1}{3}$ by $\frac{2}{5}$. Since $\frac{2}{5}$ is the same as twice one-fifth, we have to take $\frac{2}{5}$ of $\frac{1}{3}$, and double the result.

To take $\frac{1}{5}$ of $\frac{1}{3}$ is to divide $\frac{1}{3}$ into 5 parts and take one of them; now $\frac{1}{3}$ is $3 \times \frac{1}{9}$ (by No. 6), and dividing $\frac{1}{9}$ into 5 equal parts gives $\frac{1}{45}$, since 5 such parts repeated 7 times make up 1. Hence 3 of these parts (or $\frac{1}{3}$ divided into 5 parts) is $\frac{3}{45}$, which is therefore $\frac{1}{15}$ of $\frac{1}{3}$, and $\frac{2}{45}$ doubled, or $\frac{4}{45}$, is $\frac{2}{15}$ of $\frac{1}{3}$.

Now, the numerator 6 is the product of the two given numerators, 2 and 3 (as appears by the process); and the denominator 35 is the product of the denominators 7 and 5. If we had to multiply this result by a third fraction, the process would be the same; hence the

Rule. Multiply all the numerators together for a new numerator, and all the denominators for a new denominator.

Ex. 1. Multiply $\frac{1}{3}$, $\frac{2}{7}$, and $\frac{6}{7}$. Ans. $\frac{12}{105}$. Ex. 2. Multiply $\frac{32}{63}$, by $\frac{2}{7}$. Ans. $\frac{64}{441}$.

Ex. 3. Multiply $\frac{11}{16}$, $\frac{7}{3}$, and $\frac{1}{5}$. Ans. $\frac{77}{240}$.

17. If we multiply $\frac{2}{3}$ by itself, we have $\frac{4}{9}$, this again by $\frac{2}{3}$ gives $\frac{8}{27}$; now $\frac{8}{27}$ differs little from $\frac{8}{28}$, and $\frac{8}{28}$ is equal to $\frac{2}{7}$, which is very

much less than $\frac{1}{2}$. Again, $\frac{1}{2}$ multiplied by itself is $\frac{1}{4}$, and this multiplied again by $\frac{1}{2}$ is $\frac{1}{8}$.

Hence a proper fraction is diminished by continually multiplying it by itself.

[5.] *Division.*

18. To divide a fraction, as $\frac{1}{3}$, by a whole number, as 4, is to find a new fraction which, repeated 4 times, shall produce $\frac{1}{3}$: that is, we have to divide a third into 4 equal parts.

It will be at once seen, on dividing a line into 3 equal parts, that to divide each third into 4 equal parts, is to divide the whole line into 12 equal parts, and since 4 of such parts, or twelfths, constitute a third, $\frac{1}{12}$ is the required fraction. Hence, as similar reasoning applies to any other fraction or whole number, the most general rule for dividing a fraction by a whole number is to multiply the denominator by the given whole number; but if the numerator be a multiple of the divisor, it is better to divide the numerator as it leaves the result in a more reduced state.

19. To divide a whole number, as 3, by a fraction, as $\frac{1}{4}$. Dividing 3 by 1, that is, finding how often 1 is contained in 3, gives 3. Now, it is easily seen, since $\frac{1}{4}$ is 4 times *smaller* than 1, that it must be contained in 3, four times *oftener*, that is 12 times; and 12 is the product of 3 by the denominator 4.

To divide 3 by $\frac{2}{3}$. Since $\frac{2}{3}$ is twice $\frac{1}{3}$, we have to divide 3 by $\frac{1}{3}$, and take half the quotient; and we know that to divide by the product of two numbers, $2 \times \frac{1}{3}$, is the same thing as to divide by them separately, that is, 3 divided by $\frac{1}{3}$ is 3 multiplied by 3 (No. 18), and divided by 2; or $3 \div \frac{2}{3}$ is the same as $3 \times \frac{3}{2}$, or $\frac{9}{2}$.

Here $\frac{3}{2}$ is the fraction $\frac{2}{3}$ inverted.

As similar reasoning applies to any numbers and fractions, we have the

Rule. To divide by a fraction, invert the fractional divisor, and proceed as in multiplication.

20. To divide a fraction by a fraction. We have evidently to treat the dividend as a whole number, and apply to the divisor the rule above.

Ex 1. Divide $\frac{7}{12}$ by $\frac{2}{3}$. $\frac{7}{12} \times \frac{3}{2} = \frac{21}{24} = \frac{7}{8}$.

Ex. 2. Divide $\frac{3}{4}$ by $\frac{3}{5}$. Ans. $\frac{15}{8}$.

Ex. 3. Divide $\frac{2}{7}$ by $\frac{9}{11}$. Ans. $\frac{22}{63}$.

Hence it appears that the smaller the fractional divisor the greater is the quotient.

21. When a quantity is both multiplied and divided by the same number, it remains unchanged. Hence when the same number occurs in the numerator and denominator of a fraction, or of two or more fractions multiplied together, we simply omit or erase it; as,

$$\frac{1 \times 3}{3} = 1, \quad \frac{1}{4} \times \frac{4}{3} = \frac{1}{3}, \quad \frac{4}{7} \times \frac{7}{8} \times \frac{8}{16} = \frac{4}{16} \times \frac{1}{2} = \frac{1}{4} \times \frac{1}{2} = \frac{1}{24}, \quad 6 \times \frac{1}{6} = 1.$$

II. *Decimal Fractions.*

22. Tenths, hundredths (which are tenths of tenths), and so on, are called *Decimal Fractions*, and may be written as fractions, having for denominators 10, 100, &c., thus, one-tenth, $\frac{1}{10}$; three hundredths, $\frac{3}{100}$, &c. But as these quantities are counted by *tens*, like common numbers, it is simpler and more concise to write them in *continuation* with the common numbers, only taking care to put a dot, called the *decimal point*, where the whole number ends and the fraction begins; that is, between the unit and the tenth: thus, 21·32 signifies 21 and 3-tenths and 2-hundredths; 432·9 signifies 432 and 9-tenths; 33·05 signifies 33, no tenths, 5 hundredths.

23. In the fractional part beyond the dot, each figure may be read in its separate denomination, or the whole may be read in the denomination of the last: thus, ·32 is read either as 3-tenths and 2 hundredths, or as 32-hundredths; just as 32 is read either as 3 tens and 2 units, or as 32 units.

24. As ·5, (or 5-tenths) is the half of 1, so ·05 is the half of 0·1, or 5 hundredth-parts are the half of one-tenth; 5 thousandth-parts are the half of a hundredth-part. The half of 5 tenths is 2 tenths and half a tenth, that is, 2 tenths and 5 hundredths, or 0·25. Hence the fractions, *quarter*, *half*, and *three-quarters* are written in decimals, 0·25, 0·5, and 0·75.

All the preceding rules apply equally to decimal fractions, but as these last, from their denominators being multiplied by 10, are of a uniform kind, special rules have been made for them, relating, however, almost entirely to the placing of the decimal point.

[1.] *Addition and Subtraction.*

25. Place the quantities so that their decimal points shall be in the same vertical line; for then the quantities of the same denomination will stand together.

Then proceed as in the addition or subtraction of whole numbers.

Ex. 1. Add together 0·35, 47·4, and 9·12.

$$\begin{array}{r} 0\cdot35 \\ 47\cdot4 \\ 9\cdot12 \\ \hline \text{Sum } 56\cdot87 \end{array}$$

Ex. 2. Add together 72·99, 4·1, and 52·31.

$$\begin{array}{r} 72\cdot99 \\ 4\cdot1 \\ 52\cdot31 \\ \hline \text{Sum } 129\cdot40 \end{array}$$

Ex. 3. From 31·8 subtract 11·62.

$$\begin{array}{r} 31\cdot8 \\ 11\cdot62 \\ \hline \text{Rem. } 20\cdot18 \end{array}$$

Ex. 4. From 423·5 subtract 97·9.

$$\begin{array}{r} 423\cdot5 \\ 97\cdot9 \\ \hline \text{Rem. } 325\cdot6 \end{array}$$

[2.] *Multiplication.*

26. Multiply the numbers together as whole numbers, and point off as many decimal places in the product (beginning at the right) as there are decimal places in the multiplier and multiplicand together.

When the decimal places to be pointed off are more in number than the figures of the product, make up the proper number by prefixing ciphers to the product.

Ex. 1. Multiply $34\cdot11$ by $3\cdot72$.

$$\begin{array}{r} 34\cdot11 \\ 3\cdot72 \\ \hline 6822 \\ 23877 \\ 10233 \\ \hline \text{Ans. } 126\cdot8892 \end{array}$$

In $34\cdot11$ are two decimals; in $3\cdot72$ are two; therefore four decimal places are pointed off.

Ex. 3. Multiply $90\cdot01$ by $0\cdot034$. Ans. $3\cdot06034$.

Ex. 4. Multiply together $1\cdot3$, $1\cdot2$, and $0\cdot09$. Ans. $0\cdot1404$.

Ex. 2. Multiply $\cdot201$ by $\cdot06$.

$$\begin{array}{r} \cdot201 \\ \cdot06 \\ \hline \text{Ans. } \cdot01206 \end{array}$$

The product of 201 by 6 is 1206 ; in $\cdot201$ are three decimals, in $\cdot06$ are two; to make up five decimals, a cipher is prefixed to 1206 .

[3.] Division.

27. Divide as in whole numbers. The rule for placing the decimal point is, that the quotient and divisor together must contain as many decimals as the dividend.*

Ex. 1. Divide $17\cdot34$ by $3\cdot4$.

$$\begin{array}{r} 3\cdot4)17\cdot34(5\cdot1 \\ 170 \\ \hline 34 \\ 34 \end{array}$$

Here $17\cdot34$ contains two decimals, $3\cdot4$ contains only one; therefore $5\cdot1$ must contain the remaining one required, and be written $5\cdot1$.

Ex. 2. Divide $54\cdot1\cdot2$ by 66 .

$$\begin{array}{r} 66)54\cdot1\cdot2(8\cdot2 \\ 528 \\ \hline 132 \\ 132 \end{array}$$

Here $54\cdot1\cdot2$ contains one decimal, 66 none; hence $8\cdot2$ must contain one, and be written $8\cdot2$.

Ex. 3. Divide $2\cdot392$ by $4\cdot6$.

$$\begin{array}{r} 4\cdot6)2\cdot392(5\cdot2 \\ 230 \\ \hline 92 \\ 92 \end{array}$$

Here $2\cdot392$ contains three decimals, and $4\cdot6$ one, the remaining two required must therefore be obtained by pointing off both figures of $5\cdot2$ thus, $\cdot52$.

Ex. 4. Divide $338\cdot4$ by $9\cdot4$.

$$\begin{array}{r} 9\cdot4)338\cdot4(36 \\ 282 \\ \hline 564 \\ 564 \end{array}$$

Here the dividend has one decimal, and the divisor also one, or as many, and the quotient is therefore an integer.

28. When the dividend has no decimals, ciphers must be annexed, preceded by the decimal point.

Ex. 1. Divide 19 by $\cdot04$.

Annexing two ciphers to 19 , gives the complete quotient 475 .

Ex. 2. Divide 132 by $0\cdot7$.

Annexing five ciphers (decimals) gives quotient $188\cdot5714$. Then the number which added to one decimal in $0\cdot7$ to make up five, is four. Ans. $188\cdot5714$.

29. When the number of figures in the quotient is not sufficient to make up the required number of decimals, ciphers must be prefixed.

* It is always easy to verify the quotient, since multiplying it by the divisor should reproduce the dividend: thus, in Ex. 1, $5\cdot1 \times 3\cdot4$ gives (by No. 26) $17\cdot34$. The learner should also exercise his common sense on the results as a security against gross mistakes; thus, $17\cdot34$ divided by $3\cdot4$ will be near 17 divided by 3 ; that is, less than 6 (as $5\cdot1$ is). Again, $2\cdot392$ divided by $4\cdot6$, is not far from 2 divided by 4 , or a half (which is nearly $\cdot52$).

Ex. 1. Divide $\cdot 1734$ by $3\cdot 4$.

Here $\cdot 1734$ contains four decimals, and $3\cdot 4$ one; the quotient 51 (Ex. 1, above) contains only two figures, and three are required, hence 51 must be written $0\cdot 051$.

Ex. 2. Divide $2\cdot 392$ by 46 .

Here $2\cdot 392$ contains three decimals, and 46 none; the quotient (52) must contain three, and becomes $0\cdot 052$.

Ex. 3. Divide $27\cdot 9$ by $0\cdot 02$. Annexing one cipher, the quotient is 1395 .

Ex. 4. Divide $0\cdot 0296$ by $5\cdot 2$. Annexing two ciphers gives quotient 569 , which is $0\cdot 00569$, since the five in this added to one in $5\cdot 2$ make up six.

30. The division may always be carried to any degree of accuracy by annexing ciphers to the dividend, as is seen in Ex. 2, No. 28.

31. The decimal point may be removed altogether from both the divisor and dividend, by continually multiplying each by 10; for the quotient will thus remain unaltered, No. 7. The first decimal in the quotient will then appear only with the first cipher annexed to carry on the division.

Ex. Divide $27\cdot 9$ by $0\cdot 02$. Multiplied by 10 they become 279 and $0\cdot 2$; multiplied again they become 2790 and 2, the quotient of which is 1395.

This easy process furnishes a complete security against wrongly placing the decimal point in the quotient.

[4.] Reduction.

32. The great convenience of decimals makes it often desirable to reduce vulgar fractions to the decimal form.

To reduce a Vulgar Fraction to a Decimal Fraction.

Divide the numerator by the denominator, adding ciphers as required. The quotient is the decimal required.

Ex. 1. Reduce $\frac{1}{5}$ to a decimal fraction. Dividing 10 by 5 (the cipher being added) we find $\frac{1}{5}$ is $0\cdot 2$.

Ex. 2. Reduce $\frac{1}{3}$ to a decimal fraction. Dividing 10 by 3 gives 3; the next cipher added gives another 3, and so on continually. The fraction required is therefore $0\cdot 333$, &c.

Ex. 3. Find what decimal of 1 (nautical) mile is 700 feet.

There are 6080 feet, nearly, in 1 such mile; hence 1 foot is $\frac{1}{6080}$ of 1 mile, and 700 feet are $\frac{700}{6080}$ of 1 mile, which gives $0\cdot 115$ of 1 mile, nearly

Ex. 4. Find what decimal of 1 minute is 42 seconds.

1 second is $\frac{1}{60}$ of 1 minute, hence 42 seconds are $\frac{42}{60}$ or $0\cdot 7$ of a minute; or, as it may be written, $0\cdot 7$.

Ex. 5. Find what decimal of 1 foot is $8\frac{3}{4}$ inches.

First, $\frac{3}{4}$ is $0\cdot 75$ of 1 inch, hence $8\frac{3}{4}$ inches are $8\cdot 75$ inches. Then, 1 inch is $\frac{1}{12}$ of 1 foot hence $8\cdot 75$ inches are $\frac{8\cdot 75}{12}$, or $0\cdot 729$, of 1 foot.

Ex. 6. Find what decimal of 1 degree is $8' 37''$.

$37''$ are $\frac{37}{60}$ of $1'$, or $0\cdot 61$ of $1'$; then $1'$ is $\frac{1}{60}$ of 1° ; hence $8\cdot 61$ are $\frac{8\cdot 61}{60}$ of 1° , or $0\cdot 143$.

Ex. 7. Find what decimal of 1 day is $3^h 42^m$.

42^m are $\frac{42}{60}$ of 1^h , or $0\cdot 7$; and 1^h is $\frac{1}{24}$ of 1 day; hence $3\cdot 7$ is $\frac{3\cdot 7}{24}$ of 1 day or $0\cdot 154166$, &c.

33. Or, reduce the given quantity to the lowest of its denominations when there are more than one, and also the integer to which it is referred, to the same denomination; then divide the given quantity by the integer thus reduced.

Ex. 1. (Ex. 3, above.) The given quantity, 700 feet, being all in one denomination, requires no further reduction.

The integer 1 mile, reduced to the same denomination, is 6080 feet; then 700 divided by 6080 gives 0.115.

Ex. 2 (Ex. 5, above.) 8 inches and 3 quarters are 35 quarters; and 1 foot reduced to the same denomination, is 48 quarters; then 35 divided by 48 gives 0.729

34. To reduce a Decimal Fraction to a Vulgar Fraction.

Note the number of parts which the unit or integer of the given quantity contains of the next inferior denomination, and multiply the given decimal by this number; the product is the given quantity expressed in that denomination

If this product have a decimal part, multiply this decimal by the number of parts which the unit of the present denomination contains of the next inferior denomination to that just before employed: this product is the quantity which the given decimal contains of that *next denomination*.

Proceed (if there still be decimals), in like manner, to the lowest denomination in which the decimal is required to be expressed

Ex. 1. Find the number of feet in 0.115 of 1 mile.

The next inferior denomination to that of miles } 0.115
is here feet, of which the number in 1 mile is } 6080

Ans. (in the lowest denomination required) 699.4 feet.

Ex. 2. Find the number of seconds in 0.7 of 1 minute.

The next inferior denomination to that of minutes } 0.7
is seconds, of which the number in 1 minute is } 60

Ans. 42.0 seconds.

Ex. 3. Find the number of inches and eighths in 0.48 of 1 foot.

The next inferior denomination to that of feet } 0.48
is inches, of which the number in 1 foot is } 12

The next proposed inferior denomination to inches } 5.76 inches.
is eighths, of which the number in 1 inch is } 8

Ans. 5 inches and 6.08 eighths, or $\frac{6}{8}$ nearly.

Ex. 4. Find the number of minutes and seconds in 0.734.

The next inferior denomination to that of degrees } 0.734
is minutes, of which the number in 1° is } 60

The next inferior denomination to minutes } 44.040
is seconds, of which the number in 1' is } 60

Ans. 44' 24".

Ex. 5 Find the number of hours and minutes in 0.37 of a day.

The next inferior denomination to days is } 0.37
hours, of which the number in 1 d. is 24 } 24

The next inferior denomination to hours is } 8.88 hours.
minutes, of which the number in 1^h is 60 } 60

Ans. 8^h 52^m 2.

52.80 minutes.

35. When we propose to use the nearest whole number, rejecting the decimals, if the decimal is less than $\cdot 5$, we omit it, if greater than $\cdot 5$, we count it as a unit. For example, if we propose to take 31.3 as a whole number, we call it 31; if we propose to take 31.7 as a whole number, we call it 32. The reason is, obviously, that 31.3 is nearer to 31 than it is to 32, whereas 31.7 is nearer to 32 than it is to 31.

In like manner, we may abridge the decimals themselves when accuracy is not required: thus, for ex. 11.567 may, when two places only are required, be written 11.57, or when one place only, 11.6 *

II. PROPORTION.

36. By the term *ratio* we commonly understand the relative magnitude or quantity of two things of the same kind; thus, when we speak of the ratio of two numbers, 12 and 4, we mean their relative magnitude, or the result of comparing them together in respect of quantity.

37. The most distinct and intelligible notion which we can form of the degree in which one quantity or magnitude is greater than another, is the number of times one contains the other; that is, the quotient of one by the other is the *measure* of the ratio. Thus, to compare 12 and 4, we find that 12 contains 4 three times, or the quotient $\frac{12}{4}$, or the number 3, is the measure of the ratio of 12 to 4.†

* The following signs, or symbols, of arithmetical operations are often used for abbreviation.

(1.) The sign $+$, called *plus* (which is the Latin for *more*), signifies *additive*, or to be *added*.

(2.) The sign $-$, called *minus* (which is the Latin for *less*), signifies *subtractive*, or to be *subtracted*.

Ex. $+3$ signifies 3 to be *added*, -3 signifies 3 to be *subtracted*.

(3.) The sign \times signifies *multiplied by*.

Ex. 7×5 signifies 7 *multiplied by* 5.

(4.) The sign \div signifies *divided by*. The operation of division is also indicated by writing the divisor under the dividend, with a line between them.

Ex. $14 \div 2$ signifies 14 *divided by* 2; which is as frequently denoted thus, $\frac{14}{2}$.

(5.) The sign $=$ signifies *equal to* (or amounting to).

Examples of the preceding, with the results in each case, will stand thus:—

(1.) 14 and $3 = 17$, or $14 + 3 = 17$.

(2.) $10 - 3 = 7$.

(3.) $7 \times 5 = 35$.

(4.) $14 \div 2 = 7$, or $\frac{14}{2} = 7$.

These processes appear much more conspicuous to the eye than when written out in words at length.

† But, instead of saying that the absolute number 3 is the measure of the ratio 12 : 4, it is more correct to say that the measure is itself the ratio of 3 : 1; because, in all cases of measure, we employ a convenient quantity of the same kind as a unit, as 1 foot, or 1 mile. for length, 1 second for time, &c.; so the measure of ratio is itself a ratio, but of the simplest form that can be found

The ratio or proportion (for the terms are often used indifferently) of two numbers, as 12 and 4, is written thus, $12 : 4$, or, as above, $\frac{12}{4}$.

38. Suppose it required to find the ratio of 12 to 5. 12 contains 5 more than twice, but not three times. By actual division, $\frac{12}{5}$ gives $2\frac{2}{5}$; but this, instead of being simpler, is more complex than $\frac{12}{5}$. Hence, as we cannot simplify this fraction (12 and 5 having no common measure but 1), it remains as the measure, or represents the ratio of 12 : 5

39. In the same manner is represented the ratio of 4 to 12, in which the smaller term is taken first; for though 4 does not contain 12, yet it contains the third part of 12, so that there is still an exact relation between the numbers in this order: in other words, the ratio of 4 to 12 is the same as the ratio of $\frac{1}{3}$ to 1; but the ratio of $\frac{1}{3}$ to 1, or a third to the whole, is the same as that of 1 to 3, since each contains the other three times. Hence, $4 : 12$, or $\frac{1}{3} : 1$, is the same as $1 : 3$, or $\frac{4}{12}$ the same as $\frac{1}{3}$, which is the measure of $\frac{4}{12}$.

40. There is an employment of *ratio* or fractions which is often embarrassing to unpractised arithmeticians. If we increase 6 to 7, we add *1-sixth*, for 1 is $\frac{1}{6}$ of 6, and $6 + 1$ make 7; but, if we now diminish 7 to 6, we take away *1-seventh*, for $\frac{1}{7}$ of 7 is 1, and $7 - 1$ is 6. In the first case, we take a fraction of 6, in the second, a fraction of 7; and it is obvious that the same quantity cannot be the same fraction of two different numbers. In like manner 3 increased by $\frac{1}{3}$ of itself becomes 4; but to pass back again from 4 to 3, we must take away $\frac{1}{4}$ of 4.

41. It may be convenient to express the change of a quantity in any ratio, by means of the increase or diminution it undergoes, measured by a fraction of itself.

To increase a number in the ratio of $\frac{4}{3}$. $\frac{4}{3}$ is composed of $\frac{3}{3}$ and $\frac{1}{3}$, or 1 and $\frac{1}{3}$; hence the number is to be increased by $\frac{1}{3}$ of itself.

To diminish a number in the ratio of $\frac{4}{3}$. $\frac{4}{3}$ is equivalent to $\frac{2}{3}$, deducting $\frac{1}{3}$, or to $1 - \frac{1}{3}$; hence the number is to be diminished by $\frac{1}{3}$ of itself.

Ex. 1. A number is increased in the ratio of $\frac{71}{53}$, by what fraction of itself is it increased?
Answer, $\frac{18}{53}$.

Ex. 2. A number is diminished in the ratio of $\frac{23}{51}$, by what fraction of itself is it diminished?
Answer, $\frac{28}{51}$.

42. The first of two terms taken in order is called the *antecedent*, and the second the *consequent*: thus, in $12 : 4$, 12 is the antecedent, and 4 the consequent; in $4 : 12$, 4 is the antecedent.

1. Direct Proportion.

43. When two pairs of terms occur, each antecedent having the same ratio to its consequent, the four terms constitute an analogy, or proportion, as it is also called: thus, 18 and 6, 12 and 4, each pair

having for its measure the ratio $\frac{1}{4}$, form this proportion—18 is to 6 as 12 is to 4; or, as it is written for abbreviation, $18 : 6 :: 12 : 4$.

The same is also written thus: $\frac{18}{6} = \frac{12}{4}$, and read "the ratio of 18 to 6 is equal to the ratio of 12 to 4."*

44. In every proportion the product of the two extreme terms is equal to the product of the two mean (or middle) terms: thus, in $18 : 6 :: 12 : 4$, $18 \times 4 = 6 \times 12 = 72$.† This property affords the test by which we learn the various alterations that may be made in a proportion, the original proportionality being still preserved.

45. The following variations in the order of the four terms of a proportion occur the most frequently:—

Given form,	$18 : 6 :: 12 : 4$	In like manner,	$\left\{ \begin{array}{l} 4 : 6 :: 12 : 18 \\ 6 : 4 :: 18 : 12 \\ 12 : 18 :: 4 : 6 \\ 18 : 12 :: 6 : 4 \end{array} \right.$
Alternately,	$18 : 12 :: 6 : 4$		
Reversing,	$6 : 18 :: 4 : 12$		
Or,	$4 : 12 :: 6 : 18$		

46. In a proportion, either of the mean terms is equal to the product of the extremes divided by the other mean.

$$\text{Thus in } 18 : 6 :: 12 : 4, \quad 6 = \frac{18 \times 4}{12}, \text{ and } 12 = \frac{18 \times 4}{6}.$$

Also, either of the extremes is equal to the product of the means divided by the other extreme; as in

$$18 : 6 :: 12 : 4, \quad 18 = \frac{6 \times 12}{4}, \text{ and } 4 = \frac{6 \times 12}{18}$$

Hence, if any three terms of a proportion be given, the fourth may be found.

47. It is often required to increase or diminish a quantity in a *certain ratio*, or proportion. For example, to increase the number 12 in the ratio of 3 to 1, is to multiply by 3. For the increased quantity (which, being yet unknown, we will call x) is to be to the given quantity 12, as 3 to 1, or $x : 12 :: 3 : 1$. Whence (No. 44) $1 \times x = 12 \times 3$. Again, to reduce a number, as 13, in the ratio of 5 to 7, is to multiply it by 5 and then divide by 7, for the required number (x) is to be to the given number (13) as 5 is to 7, whence $x = \frac{13 \times 5}{7}$.

For example, if certain provisions last 122 men a given time, it is evident that, in order to last 146 men the same time, they must be *increased in the ratio* of 146 : 122; that is, multiplied by 146, and then divided by 122. Again, if certain provisions suffice 106 men, and they are required to serve only 74 men, they may be *diminished in the ratio* of 74 to 106; that is, $\times 74 \div 106$.

* Hence proportion is also described as being the equality of ratio.

† Hence, also, when the products of two pairs of numbers are equal, the four numbers may be written as a proportion. Ex. $22 \times 66 = 4 \times 363$; hence $22 : 4 :: 363 : 66$. Care must be taken in the order of the terms, which, though indifferent in a product is every thing in a proportion.

[1.] *Rule of Three, Direct.*

48. Numerous arithmetical questions occur in a form more or less like this: if 5 men do 20 yards of work, how many yards will 11 men do, in the same time, and under the same circumstances.*

(1.) The most obvious and natural method of solving such questions is the *Method of Unity*. Thus, if 5 men do 20 yards, 1 man alone will do 4 yards, and therefore 11 men will do 11 times 4 yards.

(2.) The *General Method* is to arrange the terms in the manner of a proportion, and then to find the unknown term from the other three, (No. 46). Thus, it is obvious that a constant proportion obtaining between the men and their work, we have

$$5 \text{ men} : 20 \text{ yards} :: 11 \text{ men} : \text{number of yards required.}$$

This process is called the Rule of Three.

(3.) They, however, who are practically familiar with ratio, or proportion, perceive, on considering the question, the ratio in which one of the given terms is to be changed, so as to suit the conditions; and thus the solution is effected at a single step. Thus, in the above question, it is evident that the given number of yards, 20, is to be increased in the ratio of 11 : 5; that is, in exactly the same ratio as the number of men is increased. The solution, therefore, is comprised in these figures, $20 \times \frac{11}{5}$, which gives 44.

49. Various precepts have been suggested for ensuring a correct order in the arrangement of the terms, or the *statement of the question*, as it is called; and one of such, which is often useful, is to consider the terms given as standing to each other in the relation of cause or agent, and effect (as, for instance, the men in the above example and their work). By this supposition (which, however, is arbitrary and unsatisfactory enough in many cases), the four terms are rightly *paired*, or the antecedents and consequents rightly taken. But the fact is, that no mechanical rules can so completely supersede the notion of proportionality as to absolve the mind from all necessity for estimating it; and, consequently, the student, if he clearly understands proportion, depends upon it alone; and if he does not, he cannot, from any number of precepts, feel the least confidence in the soundness of his result.

As a right apprehension of proportion is most essential to every one who has any thing to do with calculation, we have, for the sake of exercise, solved several examples in each of the above three forms.

Ex. 1. A steam-vessel consumes 13 tons of coal in $1\frac{1}{2}$ days; how long will 98 tons last?

(1.) Method of Unity: 13 tons in $1\frac{1}{2}$ d. or $\frac{3}{2}$ d., is 1 ton in $\frac{7}{4 \times 13}$ or $\frac{7}{52}$ d., and 98 tons in $98 \times \frac{7}{52}$ or $13\frac{1}{4}$ days, or 13 d. 5 h. nearly.

* In the application of the rules which follow, the circumstances are supposed to remain the same, that is, the change of the numbers does not imply any other change. If, for example, the increased number of men should be in each other's way, so as to interfere with their labour, this must be made a separate consideration.

(2.) General Method: $13 : 18d. :: 98 : d. \text{ req.} = 1.75 \times 98 + 13 = 13.2 \text{ days.}$

(3.) By Ratio: Here $1\frac{1}{2}$ (days) is to be increased in the ratio of 98 to 13.

$$1.75 \times 98 + 13 = 13.2.$$

Ex 2 If 13 men make 420 yards in 20 days; how much will they make in 11 days?

Note.—The number of men remaining the same, while the time and the *work* change, need not be noticed.

(1.) 420 yds. in 20 d. is 21 yds. in 1 d., and 11×21 , or 231 yds. in 11 days.

(2.) 420 yds. : 20 d. :: yds. req. : 11 yds. req. = $11 \times 420 + 20 = 231$ yds.

(3.) Here 420 is to be diminished in the ratio of 11 to 20.

Ex 3. A pump, A, delivers 1 ton in 5^m; another, B, 1 ton in 8^m; and a third, C, 1 in 15^m; how much water will they deliver in 1^h 10^m?

Ans. A, $\frac{20}{9} = 2\frac{2}{9}$ tons; B, $\frac{20}{8} = 2\frac{5}{4}$; C, $\frac{20}{15} = 1\frac{2}{3}$. Total, 27.4 tons.

Ex 4. A boat, A, lands 52 men in 28^m (going and returning); another, B, lands 68 men in 41^m; and a third, C, lands 20 men in 23^m; how long will all take to land 220 men?

At these rates, in 1^h, A lands $\frac{22}{7} \times 52$ men = 111.4; B, $\frac{22}{11} \times 68$, = 99.5; and C, $\frac{22}{23} \times 20$, = 52.2. Total in 1^h, 263.1 men. Now, as the number landed is proportionate to the time, we have $263.1 : 1^h :: 220 : 220 \times 1 \div 263.1$, or 0^h 84 nearly.

Ex 5. A boat, A, fills 8 tons of water in 3^h; another, B, fills 5 tons in 4^h; and a third, C, fills $1\frac{1}{2}$ ton in 1^h; in what time will they fill 107 tons?

(1.) In 1^h, A fills $\frac{8}{3}$ tons; B, $\frac{5}{4}$ tons; and C, $\frac{3}{2}$ tons; or altogether, $\frac{127}{12}$ tons. This is 1 ton in $\frac{12}{127}$ of 1^h, 107 tons in $28 \times 107 \div 123 = 24\frac{1}{2}$.

(3.) Having found the fraction expressing the joint effect for 1^h, or $\frac{127}{12}$ tons; 1^h is to be changed in that ratio, which will convert this into 1, ($\frac{12}{127}$ by Ex.), which gives the time for 1 ton; this is then to be increased in the ratio of 107 : 1.

Note.—Such questions as in Ex. 4 and 5 do not usually admit of exact solution; thus, in any whole number of trips that can be proposed, the boats carry too much or too little. Each boat performs a certain quantity in one particular interval of time, and not *continuously*, like a pump, or so much *per hour*; the reduction, therefore, to hourly rate, is not correct, but it is near enough for forming a tolerable estimate, which, in practice, is all that is wanted. To obtain as complete a solution as the question allows, we must take each boat's performance separately, and add them all up.

Ex. 6. The change of the sun's declination in 1 day is $18' 21''$; find the change for 1^h 34^m.

$24^h (1440^m) : 18' 21'' (1101'') :: 1^h 34^m (94^m) : x$
or, less exactly, $24^h : 18' 3'' :: 1^h 6^m : x$.

Ex. 7. In a Table, against 36° stands the term 27943, and against 37° stands 28504; find the term corresponding to $36^\circ 23'$.

36° 27943
 37° 28504
Diff. 561

Hence $60 : 561 :: 23 : x$

which added to 27943 (because the terms increase while the argument* increases), gives the term required.

Ex. 8. Against 11° in a Table stands 6726, and against $11^\circ 30'$ stands 6354; find the term corresponding to $11^\circ 37'$.

$11^\circ 0'$ 6726
 $11^\circ 30'$ 6354
Diff. 372

$30 : 372 :: 37 : x$

to be subtracted from 6726, which gives the term required.

50. The process of finding a term which falls between two given terms, or, as it is called, *Interpolation*, is sufficiently exemplified above; but it is important to remark that it is not always necessary to work proportions at length. It is enough, for most practical

* The *argument* is the quantity at the side or head of the Table, for which the terms or quantities in the body of the table are given.

purposes, to take a quantity, somewhere between the given terms, as half way, or a third of the way, between them, according to the case. The power of guessing the proportional part is acquired by practice, and saves time which otherwise would often be wasted in working to a superfluous degree of accuracy.

On the other hand, when extreme precision is required, this proportioning alone is not enough, but a correction is necessary, for which see the explanation of the Table for finding the Equation of Second Differences.

[2.] *Double Rule of Three, Direct.*

61. Questions in the Rule of Three occur also in a more complex form; thus, if 2 men do 7 yards of work in 3 hours, how many yards will 13 men do in 11 hours? in which the answer is required to correspond not merely to a certain number of men, but also to a certain number of hours.

This question resolves itself into two: 1st, if 2 men do 7 yds. how many will 13 men do in the same time, or 3 hours? The answer to which is 45·5 yds.; and, 2nd, if 13 men do 45·5 yds. in 3 hours, how many yds. will they do in 11 hours? Hence the solution of such questions is called the Double, or Compound Rule of Three.

Ex 1. The example above

- (1.) 1 man does $\frac{1}{2}$ of 7 yds., or 3·5 yds. in 3^h, and 13 men do 45·5 yds.
13 men do 45·5 yds. in 3^h, or 15·17 yds. in 1^h, and therefore 166·87 in 11 hours.
- (2.) The two statements as given above.
- (3.) 7 is to be increased in the ratio of 13 : 2, and then of 11 : 3.

Ex 2. If 9 men make 47 yds. in 4 days, how many yards will 17 men make in 31 days?

Ans. 622 yds.

Ex 3. If 5 men do 64 yds. in 11 days, in how many days will 14 men do 37 yds.?

- (1.) 1 man does 64 yds. in 55 days, or 1 yd. in 0·86 days, and
14 men do 1 yd. in $\cdot 86 \div 14$, and 37 yds. in 2·27 days.
- (2.) 5 m. : 64 yds. :: 14 m. : 179·2 yds. 179·2 : 11 :: 37 : 2·27 nearly.
- (3.) 11 is to be diminished in the ratio of 37 : 64, and then of 5 : 14.

Ex 4. A certain quantity of provisions lasts 170 men for 3 months; how much is required for 210 men for 2 months?

- (2.) 170 : 1 (whole) :: 210 : $x = 210 \div 170$. And $y : 210 \div 170 :: 3 : 2$.
- (3.) The quantity is to be increased in the ratio of 210 : 170, and diminished in the ratio of 2 : 3.

Ex 5. A steam-vessel has fuel for steaming 13 days at 11 hours a-day; how much must she take to steam 15 days at 18 hours a-day?

- (3.) The fuel must be increased in the ratio of 15 : 13, and then of 18 : 11. $\frac{15}{13} \times \frac{18}{11} = \frac{270}{143}$, which is $1\frac{126}{143}$, or $1\frac{1}{11}$ nearly, or nearly doubled.

Ex 6. Three boats fill 16 tons of water in 7 hours; how many boats, at the same average performance, will fill 78 tons in 10 hours?

- (1.) 3 boats fill 16 tons in 7^h, or $\frac{1}{7}$ of 16 = 2·3 tons in 1^h, and 23 tons in 10 hours. Then, since 23 tons employs 3 boats, 1 ton employs $\frac{3}{23}$ of 1 boat, and 78 tons will employ $\frac{78 \times 3}{23}$ or 10·2 boats.
- (2.) 7^h : 16 t. :: 10^h : x tons ($= 22\cdot9$) 22·9 t. : 3 b. :: 78 t. : 10·2 b.
- (3.) 3 is to be increased in the ratio of 16 : 78, and then diminished in the ratio of 10 : 7.

2. *Inverse Proportion.*

52. In direct proportion, as we have seen, more is always followed by more, and less by less. But when the nature of the question is evidently such that *more* will be followed by *less*, or *less* by *more*, the proportion is no longer direct. For example, if 5 men do certain work in 4 days, in how many days will 7 men do the same work? Here it is evident that the *greater* number of men will require *less* than 4 days. Again, if a ship going 8 knots, sails a certain distance in 5 hours, it is evident that, if she goes at a *greater* rate, she will perform the same distance in *less* than 5 hours.

53. In a question of work performed, the result is represented by the number of agents multiplied by the time each works; thus, 6×5 or 30, represents the labour of 6 agents working for 5 hours, the unit of work being that performed by 1 man. If now, the work remaining the same, we double the number of agents, we shall obviously halve the time, since 12 men will do the work of 6 in half the time, and $12 \times 2\frac{1}{2} = 30$. Or, again, trebling the number of agents, gives $18 \times \frac{5}{3}$ of 5, or $18 \times \frac{5}{3} = 30$. That is, while one factor of a given product is *increased* in the ratio of 3 : 1, the other must be *diminished* in the ratio of 1 : 3, which last ratio contains the same terms as the other, but in a reverse or *inverted* order. The four numbers constituting two equal products are hence said to be in *inverse proportion* to each other.

In the example, No. 52, the number of men is *increased* in the ratio of 7 : 5, and the time is accordingly to be *diminished* in the ratio of 5 : 7; hence 4 days becomes $4 \times \frac{5}{7}$, or $2\frac{2}{7}$ days.

[1]. *Rule of Three Inverse.*

54. In regard to the solution of these questions:

(1.) In the method of unity, the consideration of inversion does not present itself.

(2.) As a question of proportion, the solution may be effected thus. Suppose the proportion were direct, then (example above, keeping the antecedents and consequents in their given order) 5 men : 4 days :: 7 men : x days. Now, we require a direct comparison between the number of men in the two cases, and the times in the two cases; hence we alter this to 5 men : 7 men :: 4 days : x days. But this would give x greater than 4, as 7 is greater than 5, whereas we know it must be less; hence, inverting the last two terms, gives 5 : 7 :: x : 4, or $7 : 5 :: 4 : x = \frac{4 \times 5}{7} = \frac{20}{7}$, or $2\frac{2}{7}$ days. Hence the process (which is, perhaps, as little liable to mistake as may be expected in a question of some perplexity), is, 1, to write, in the form of a direct proportion, the given antecedents and their consequents; 2, to close terms of like denomination; 3, to invert the last two terms, and then to find the unknown term.

Ex. 1. If 7 men do certain work in 4 days, in how many days will 10 men do it?

(1.) 7 men in 4 days is 1 man in 28 days, and 10 men in 2.8 days.

- (2.) Direct form, 7 men : 4 d. :: 10 men : days required.
 Like terms, 7 : 10 :: 4 : days required.
 Inverting, 7 : 10 :: d. req. : 4. Ans. 2 3 days
 (3.) It is evident that 4 is to be diminished in the ratio of 7 to 10.

- Ex. 2. If 27 men do certain work in 14 days, how many men will do the same work in 4 days?
 (1.) 27 men in 14 days, is 1 man in 378 days; and $378 \div 4$ gives $94\frac{1}{2}$ men.
 (2.) Direct form, 27 m. : 14 d. :: men req. : 4 d.
 Closing like terms and inverting, men req. = $27 \times 14 \div 4 = 94\frac{1}{2}$ men.
 (3.) 27 is to be increased in the ratio of 14 : 4.

- Ex. 3. If 12 men do certain work, working 4 hours a-day; how many men will it take to do the same work, working 7 hours a-day?
 (1.) 12 men in 4 h. is 48 men in 1 h., and $\frac{48}{7}$ in 7 hours, or 7 men nearly.
 (2.) Direct form. 12 m. : 4 h. :: men required : 7 h.
 Closing like terms and inverting, $12 \times 4 \div 7 = 7$ men nearly.
 (3.) 12 is to be diminished in the ratio of 4 : 7.

- Ex. 4. Certain tons of fuel last a steam-vessel 11 days, steaming 4 hours a-day; how long will they last steaming 6½ hours a-day?
 (1.) 4 h. for 11 d. is at the rate of 1 h. a-day for 44 d., and therefore 6½ h. for $44 \div 6\frac{1}{2}$, or $88 \div 13$, which is $6\frac{7}{13}$ d., or 6 d. $18\frac{1}{2}$ h.
 (2.) Direct form, 11 d. : 4 h. :: x days : 6½ h.
 Closing like terms and inverting, $x = 44 \div 6\frac{1}{2} = 6\frac{7}{13}$ d.
 (3.) Here 11 days is to be diminished in the ratio of 4 to 6½.

- Ex. 5. A certain quantity of fuel lasts a steam-vessel 12 days, steaming day and night; how long will it last steaming 14 hours a-day? Ans. $20\frac{2}{7}$ days.

- Ex. 6. A pump, A, empties a cistern in 3 hours; another, B, in 2½ hours; in what time will they empty it both working together?
 (1.) In 1^h, A empties $\frac{1}{3}$ of it, and B empties $1 \div 2\frac{1}{2}$, or $1 \div \frac{5}{2}$, which is $\frac{2}{5}$. Hence in 1^h both together empty $\frac{1}{3} + \frac{2}{5}$, or $\frac{7}{15}$. Suppose, for greater convenience, the cistern to hold 10 tons; then in 1^h both empty $\frac{7}{15}$ tons, or 1 ton in $1\frac{1}{2} \div \frac{7}{15}$, or $1\frac{1}{2} \times \frac{15}{7}$, = $\frac{15}{7}$ of 1^h, which is 10 tons in $\frac{15}{7}$ of 1^h, or $1\frac{1}{2}$ h.
 (2.) Stating the question directly, we should say,
 $\frac{1}{3} + \frac{2}{5}$ (= $\frac{7}{15}$) : the whole, or 1 :: time required : 1^h.
 But, the greater the fraction representing the hourly work done, the smaller must be the time required for any given quantity of work.
 Hence $\frac{7}{15} : 1 :: 1\frac{1}{2} : \text{time required} = \frac{15}{7}$ of 1^h.
 (3.) Here 1^h, in which the fraction $\frac{7}{15}$ is done, is obviously to be increased in that ratio which will turn $\frac{7}{15}$ into 1, or the whole; and this ratio is $\frac{15}{7}$, for $\frac{7}{15} \times \frac{15}{7} = 1$.

- Ex. 7. A can do certain work in 8^h, and B the same work in 6^h; in what time will they both complete it together?
 (1.) In 1^h A does $\frac{1}{8}$, and B $\frac{1}{6}$, hence both together $\frac{1}{8} + \frac{1}{6}$, or $\frac{5}{24}$. Let the work be represented by 10, then in 1^h both do $\frac{5}{24}$, and therefore they do the unit of work in $1\frac{1}{2} \div \frac{5}{24}$, or $\frac{24}{5}$ of 1^h. Hence they do the whole in $10 \times \frac{24}{5} = \frac{240}{5}$ of 1^h, or 48^h.
 (2.) Direct form, $\frac{1}{8} + \frac{1}{6} : 1$ (whole) :: time required : 1^h = $\frac{24}{5}$.
 (3.) 1^h is to be increased in the ratio of 24 : 5.

- Ex. 8. Five pumps empty a cistern in 13 hours; how many must be put on to empty it in 3½ hours?
 (1.) 1 pump in 65 hours gives 13.6 in 3½ hours.
 (2.) 5 p. : 13^h :: x : 3½^h. Ultimately, $x = 5 \times 13 \div 3\frac{1}{2}$.
 (3.) 5 is to be increased in the ratio of 13 : 3½.

- Ex. 9. Four pumps empty a cistern in 10 hours; how long will 7 each pumps take?
Ans. $40 \div 7 = 5\frac{5}{7}$.

Ex. 10. A certain quantity of bread lasts 110 men 21 days; how long will it last 74 men?

(1.) 21 d. for 110 men is 1 d. for 2310 men, and $2310 \div 74$ gives 31.2 days.

(2.) Direct form, $110 \text{ m.} : 21 \text{ d.} :: 74 \text{ m.} : x \text{ d.}$

Closing like terms and inverting, $x = 21 \times 110 \div 74 = 31.2$ days.

(3.) It is evident that 21 is to be increased in the ratio of 110 : 74.

Ex. 11. A quantity of bread lasts a ship's crew 21 days at four-fifths allowance; how long will it last at two-thirds allowance?

(1.) $\frac{4}{5}$ lasts 21 d., $\frac{2}{3}$ will last 4×21 or 84 days, and $\frac{3}{4}$, or whole allowance, $\frac{4}{3}$ or 16.8 days. Hence $\frac{2}{3}$ allowance will last 3×16.8 d., or 50.4 d., and $\frac{3}{4}$, one half of this, or 25.2 days.

(2.) $\frac{4}{5} : 21 :: \frac{2}{3} :: x$ required days.

Closing and inverting, days required $= 21 \times \frac{4}{5} \div \frac{2}{3} = 25.2$ days.

(3.) 21 days are to be increased in the ratio of $\frac{4}{5} : \frac{2}{3}$, that is $21 \times \frac{4}{5} \div \frac{2}{3}$.

Ex. 12. If it takes 54 yds. at $\frac{3}{4}$ of a yard wide, to cover a surface; how many yards will it take at $\frac{1}{2}$ of a yard in width?

(1.) 54 yds. at $\frac{3}{4}$ wide is 3×54 , or 162 yds. at $\frac{1}{2}$ wide, or 40.5 yds. at 1 yd. wide. This is 5×40.5 or 202.5 yds. at $\frac{1}{2}$ wide, and $\frac{1}{2}$ of this, or 50.62 yds. at $\frac{1}{4}$ wide.

(2.) Direct form, $54 \text{ yds.} : \frac{3}{4} \text{ width} :: x \text{ yds. req.} : \frac{1}{2}$

Closing like terms and inverting, yds. req. $= 54 \times \frac{3}{4} \div \frac{1}{2} = 50.62$ yds.

(3.) Here 54 is to be diminished in the ratio of $\frac{3}{4} : \frac{1}{2}$, or of 15 : 16.

[2.] Double Rule of Three, Inverse.

55. As the inversion arises from a product remaining constant while both factors vary, questions of this kind may be solved directly by taking, in each of the two proportions necessary, those terms only which are directly proportional to each other. For example, in a question of agents, work, and time, the first proportion would include work and time, and the second, agents and work.

III. LOGARITHMS.

56. These are numbers calculated for the purpose of converting multiplication into addition, and division into subtraction.

1. Use of Logarithms.

57. Every logarithm consists of two parts, the *index* and the decimal part;* thus, in the logarithm 2.80618, the index is 2, and the decimal part .80618.

58. To find the Logarithm of a given number. Find in the Table of Logarithms of Numbers the decimal part (for which see also the Explanation of that table); and then apply the index by one of the two following rules:—

(1.) When the number consists of a whole number, with or without decimals, the index is 1 less than the number of figures in the whole number.

* This part is also called the *mantissa*.

Ex. 1. Find the log. of 522.

Against 522, in the Table, stands $\cdot 717671$; then, since there are three figures in 522, the index is 2; hence the log. is $2\cdot 717671$.

Ex. 2. Find the log. of $5\cdot 22$.

The log. of $5\cdot 22$ is $0\cdot 717671$, because there is one figure in the whole number, and one less than 1 is 0.

(2.) When the number consists of decimals only, count the number of ciphers between the decimal point and the first significant* figure after it, and subtract this number from 9; the remainder is the index.

Ex. 1. Find the log. of $\cdot 005814$.

The decimal part of 5814 is $\cdot 764475$; there are two ciphers before the 5, which 2 taken from 9 leaves the index 7: hence the log. is $7\cdot 764475$.

Ex. 2. The log. of $\cdot 5814$ is $9\cdot 764475$, for the number of ciphers before the $\cdot 5$ is nothing which leaves 9 for the index.

59. To find the natural number of a given Logarithm. Look for the decimal part of the given log. in the body of the table, and take out the number from the side column and top.

To place the decimal point. Add 1 to the given index of the log., and mark off to the left this number of figures; these will be whole numbers; the rest, if any, will be decimals.

If the index is 9, put the dot before the first figure; if it is 8, prefix one cipher to the first figure, and place the dot before the cipher; if it is 7, prefix two ciphers, and so on.†

Ex. 1. Find the number to the log. $1\cdot 717671$.

The number (to 4 places) to $\cdot 717671$ is 5220: adding 1 to the index 1, gives 2, which, marked off to the left, gives $52\cdot 2$, the number required.

Ex. 2. Find the number to the log. $8\cdot 581381$.

The number to 581381 is 3814; prefixing one cipher gives $\cdot 03814$, the number required.

When the number exceeds four figures, see the explanation of the table.

60. In using logarithms, it is proper to observe that the number (whether it contain decimals or not), and the decimal part of the logarithm, are in general true to the same number of figures, rejecting prefixed ciphers; thus, for instance, the log. $3\cdot 7575$ corresponds to the number 5721, and the log. $3\cdot 7576$ to 5722, nearly. So also, $8\cdot 7575$ to $\cdot 05721$, and $8\cdot 7576$ to $\cdot 05722$.

This remark should be kept in view, because it is mere waste of time to employ more figures than are required to insure a certain degree of precision in the result.

* That is, the first figure not a cipher.

† As the index of the log. is 1 less than the number of figures in the natural number itself, it would follow that the index of $\cdot 3814$ (for example) in which there are no significant figures, would be 1 less than nothing, the meaning of which is, that such a log. is reckoned on the opposite direction from a certain point, which need not here be further discussed. The index of such a log. is called *negative*; and as this is embarrassing to beginners, 10 is added to the index 0, whereby 1 less gives 9. But 9 is the index, properly, of a number consisting of 10 figures; however, as we have no such numbers to deal with, the ambiguity of the double meaning is not experienced.

61. The remark (No. 35) applies also to logarithms; thus, for example, if we propose to use only four figures of the log. $\cdot 881385$, we write $\cdot 8814$, which is evidently nearer to $\cdot 881385$ than $\cdot 8813$ would be. Again, if we take four figures of $\cdot 881343$, we write $\cdot 8813$.

62. To find the *arithmetical complement* of any number or logarithm.

Take every figure from 9, except the last, which take from 10. It is necessary to begin at the left.

Ex. 1. Find the arith. comp. of $1^{\circ} 37' 04\frac{1}{2}$
arith. comp. log. required $8^{\circ} 12' 957$

Ex. 2. Find the arith. comp. of $0^{\circ} 91' 350$
arith. comp. log. $9^{\circ} 08' 650$

63. A subtractive quantity is, by this means, made additive. The process is equivalent to subtracting the number from 10, and the reason of it is evident on considering that to add 3, for example, and subtract 10, is the same as to subtract 7. In like manner, instead of subtracting $47^{\text{m}} 32^{\text{s}}$, for example, we may add $12^{\text{m}} 28^{\text{s}}$ (the complement to 60), provided we subtract 1 hour (or 60); and thus any number of quantities, of which some are additive and some subtractive, may be rendered all additive, provided that the larger numbers which are employed in taking the complements be themselves subtracted.

2. Certain Arithmetical Operations by Logarithms.

[1.] Multiplication.

64. To multiply numbers together, add their logarithms together; the sum is the logarithm of the product required.

Ex. 1. Multiply $530^{\circ} 9'$ by $27^{\circ} 22'$.
 $530^{\circ} 9'$ log. $2^{\circ} 72' 5013$
 $27^{\circ} 22'$ log. $1^{\circ} 43' 4888$
Ans. 14451 . log. $4^{\circ} 15' 9901$

Ex. 2. Multiply $\cdot 079$ by $3^{\circ} 142$.
 $\cdot 079$ log. $8^{\circ} 29' 7627$
 $3^{\circ} 142$ log. $0^{\circ} 49' 7206$
Ans. $0^{\circ} 2482$ log. $9^{\circ} 39' 4833$

[2.] Division.

65. From the log. of the dividend subtract the log. of the divisor; the remainder is the log. of the quotient required.

If the logarithm of the dividend is the lesser of the two, increase its index by 10.

Ex. 1. Divide 4280 by 365 .
 4280 log. $3^{\circ} 63' 1444$
 365 log. $2^{\circ} 56' 2293$
Ans. $11^{\circ} 73$ log. $1^{\circ} 06' 9151$

Ex. 2. Divide $69^{\circ} 3'$ by $71^{\circ} 7'$.
 $69^{\circ} 3'$ log. $(+10)$ $1^{\circ} 84' 0733$
 $71^{\circ} 7'$ log. $1^{\circ} 85' 5519$
Ans. $0^{\circ} 9665$ log. $9^{\circ} 98' 5214$

[3.] Involution.

66. Involution is the process of multiplying a quantity by itself; the quantity thus multiplied is said to be *raised to a power*.

67. The *first power* is the number itself. The second power is the number multiplied by itself; this is also called the *square*. The third power is the number again multiplied by itself; this is also called the *cube*.

The number or quantity to be raised to a power is called the *root*; the number which indicates the power to which the quantity is raised is called the *index*.

68. To *square* a number. Multipliy the log. of the number by 2; the product is the log. of the number required.

When the number is a decimal fraction, subtract the index (after being doubled) from 10 multiplied by 2 (or 20), diminish the remainder by 1, and prefix the number of ciphers indicated by this remainder to the number corresponding to the logarithm.

Ex. 1. Square 12'39.

12°39'

log. 1.093071

Ans. 153°5.

log. 2.186142

Ex 2. Square '0592.

0592

log. 8.77232

Ans. '003505

log. 17°54'46"

17 from 20 leaves 3; deducting 1 gives 2;
2 ciphers are, therefore, prefixed to 3505.

69. To *cube* a number. Proceed by the above rule, only reading 3 for 2, and 30 for 20. In like manner, to raise a number to the *fourth power*, read 4 for 2, and 40 for 20, and so on.

[4.7] Evolution.

70. Evolution is the reverse of involution, and is the process of finding that number which, multiplied by itself a certain number of times, will produce the given number.

This number is called the *root* of the given number.

71. To extract the square root of a number. Divide the log. of the given number by 2, the quotient is the log. of the square root required.

¹ When the given number is a decimal fraction (that is, when the index of its logarithm is 9, 8, 7, &c.), increase the index by 10.

Ex. 1. Find the square root of 1.535.

1535

log. 0186108

2) 0.186108

1 2.9 Sq. root req.

0.093054

Ex. 2. Find the square root of .003505.

003505

log. 7°54469

I

2) 17.54469

0.0592 Sq. root req.

$$8.77234$$

72. To extract the cube root. Proceed by the above rule, only reading 3 for 2, and 20 for 10. To extract the *fourth* root, read 4 for 2, and 30 for 10, and so on for other roots.

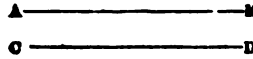
IV. PRACTICAL GEOMETRY.

1. Definitions.

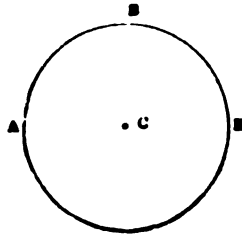
73. GEOMETRY is the name of that science which relates to the measures of space.

A PROBLEM is something required to be done.

PARALLEL LINES are lines so placed that the shortest distance between them is every where the same, as A B, C D. Such lines evidently never meet.



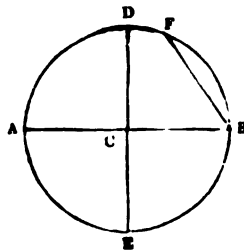
74. A **CIRCLE** is a figure bounded by a curve line called the *circumference*,* of which every point is at the same distance from a point within, called the *centre*. Thus, A B D is a circle, and C the centre.



75. The circumference is divided into 360 equal parts, called *degrees*, written thus, 360° ; each degree, into sixty equal parts, called *minutes* ($60'$); each minute into sixty seconds ($60''$); and also each second, into sixty thirds ($60'''$). Example, $11^\circ 19' 46''$, eleven degrees, nineteen minutes, forty-six seconds.

76. The circumference is also divided into 32 equal portions of $11^\circ 15'$ each, called *points of the compass*. These are again subdivided into half points and quarter-points. The term point is used indifferently for the arc of $11^\circ 15'$, and for a mere point of division of the circumference.

77. A straight line, A B, drawn through the centre, divides the figure into two equal parts, called *semicircles*, as A D B, A E B. The half circumference measures 180° .



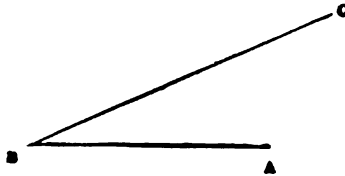
78. The line A B is called the *diameter*: it is evidently equal to twice the distance from the centre, C A, which is called the *radius*.

* In common language, circle and circumference are often used indifferently the one for the other, but circle is properly the *surface* or *area* of the figure included within the circumference.

79. If another diameter, D E, cross this, and divide each semi-circle into two equal parts, the four equal parts, A D, B D, B E, E A, are called *quadrants*, and each of such portions of the circumference measures 90° .

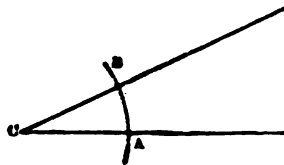
80. Any portion of the circumference is called an *arc*, and the line joining its extremes is called a *chord*: thus the line B F is the chord of the arc B F.

81. AN *ANGLE* is the inclination of two straight lines to each other; that is, the difference of the directions in which they lie: thus A B C, or B, is the angle contained by the two lines B A, B C which are called the *legs*.



An angle is not changed by increasing or diminishing the length of the legs, because the *length* of these lines has nothing to do with the *directions* in which they lie.

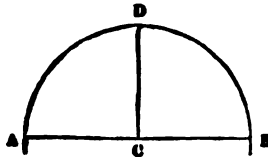
82. Since in describing a circle the radius moves round the centre C, exactly as the point of the compasses advances on the circumference, the angle A C B is measured by the number of degrees in the arc A B.



83. The arc A B is said to *subtend* the angle A C B.

84. An angle of 90° , as A C D (fig. in No. 77), which is subtended by a quadrant, as A D, is called a *right angle*. A circle contains four right angles, a semicircle two.

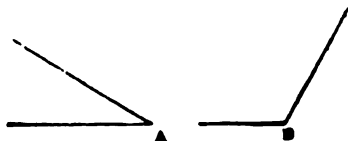
85. The angles A C D, B C D, being each 90° , are equal; and C D, which makes these adjacent angles equal, is said to be *perpendicular* to A B.



86. The difference between an angle and 90° is called its *complement*; the difference to 180° is called its *supplement*.

An angle less than 90° is called *acute*, as A.

An angle greater than 90° is called *obtuse*, as B.



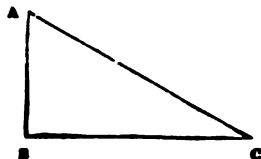
87. A **PLANE TRIANGLE** is a figure contained by three straight lines.

When the three sides are equal, the triangle is called *equilateral*; when two of them are equal, it is called *isosceles*.

88. When one of the angles is 90° , the triangle is said to be *right-angled*; when each angle is less than 90° , it is said to be *acute-angled*; when one is greater than 90° , it is said to be *obtuse-angled*.

Triangles that are not right-angled are called in general *oblique-angled*.

89. In a right-angled triangle, as A B C, the side A C, opposite the right angle is called the *hypotenuse*; one of the other sides, as B C, is called the *base*; and the third side, A B, the *perpendicular*.



90. A **SPHERE**, or **GLOBE**, is a solid figure bounded by a curve surface, of which every point is at an equal distance from the centre.

2. Geometrical Problems.

91. The instruments necessary in constructing the figures in these problems are, a pair of compasses and a straight edge of any kind, as of a ruler, or, when such cannot be had, the back of the fold made by doubling a piece of thick paper. Also the parallel rulers are convenient. These may be of the common form, which needs no description here, or those called Marquoi's Rulers.*

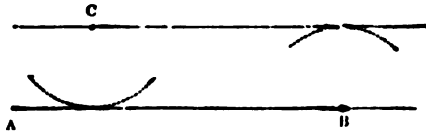
92. The accuracy of a straight edge is tested thus. Draw a line with a fine pointed pencil, or steel pen, along the edge, between two points near the extremities. Then turn the ruler over and draw another between the same two points: if the edge is perfect, the two lines will appear as one; if not, there will be a space between them.

* These last consist of a right-angled triangle, having one of its angles about 20° , and a flat ruler somewhat longer than the hypotenuse of the triangle, both of the same thickness. By sliding the triangle along the edge of the ruler, which is kept fixed, two sides of it move parallel to themselves. This parallel motion is perfect, which is not always the case with the common parallel rulers, especially after long use; and besides this, the triangle being right-angled, dispenses with the trouble of drawing perpendiculars by points.

93. PROBLEM. To draw a line through a given point parallel to another line.

C is the given point, AB is the line.

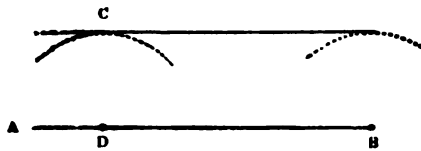
Take the shortest distance from C to AB in the compasses; set one foot on AB as at B , and describe a small arc; then the line drawn through C , so as to touch this arc, is the line required



94. PROBLEM. To draw a line parallel to another line at a given distance from it.

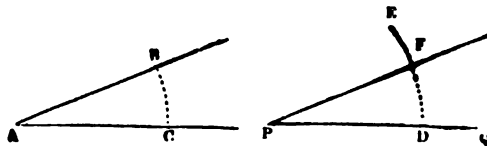
AB is the line, CD the given distance.

Take CD in the compasses, place one foot near each end of AB , and describe two arcs; the line drawn touching these arcs is the line required.



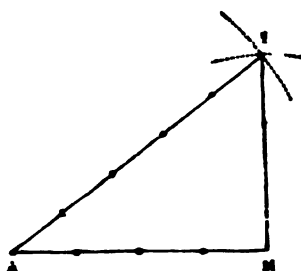
95. PROBLEM. At a given point in a line to make an angle equal to a given angle.

P is the point in the line PQ ; A is the given angle. From the centre A , with any convenient radius (the longer the more accurate), describe an arc, CB ; from the centre P , with the same radius, describe an arc, DE ; take the distance from C to B in the compasses, and put one foot on D and the other on the arc at F , and join PF : then the angle FPD is equal to BAC , their measures, FD and BC , being the same.



96. PROBLEM. From a point M , in a straight line AM , to draw a perpendicular to it (fig. p. 26).

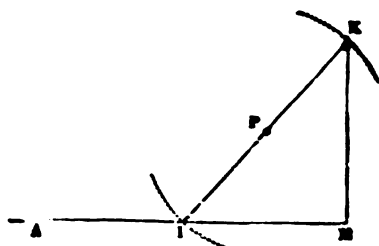
(1.) Draw a straight line any where, and set off by the compasses 5 equal parts upon it. With 3 of these parts in the compasses, as radius, describe from M , as a centre, an arc at I ; then lay off 4 parts from M to A ; with 5 parts, as radius, describe from the centre A an arc cutting the former arc at I ; join IM : this is the perpendicular required.



The following methods are also used :

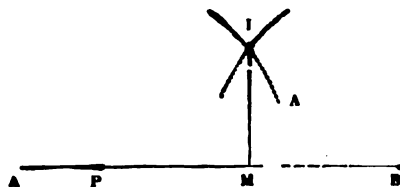
(2.) When the point M is at or near the end of the line.

Take a point P , such that a line supposed to join P and M may make the angle PMA about 45° ; and from P as a centre, with the radius PM , describe a small arc I , and another opposite, as K , draw the line IPK , and join the point where it crosses the arc K with M . KM is the perpendicular required.



(3) When the point M is not near the end of the line.

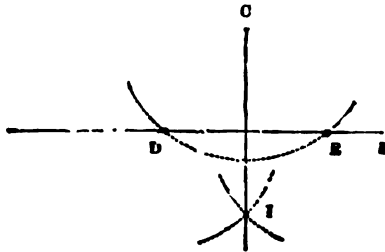
Take two points P, B , at equal distances, from M , and at P and B as centres with a radius exceeding PM , describe two arcs, cutting each other at I ; join IM . This line is the perpendicular required.



97. PROBLEM. From a given point without the line, as C , to draw a perpendicular to it.

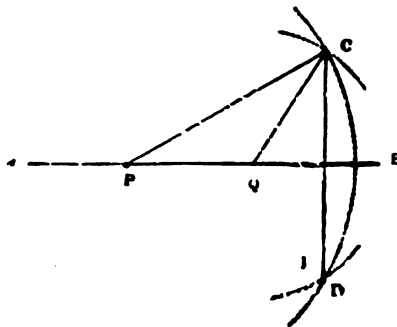
(1.) When the point is nearly opposite the middle of the line.

Take in the compasses a distance exceeding the distance from C to the line; and from C , as a centre, describe an arc, DE ; then, from D and E as centres, with a convenient radius, describe two arcs cutting each other at I . CI is the perpendicular required.



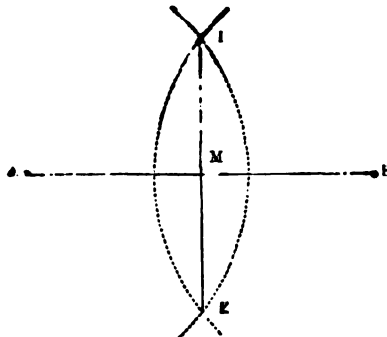
(2.) When the given point is towards the end of the line.

Take a point P as centre, and with P C as radius describe an arc C D. Take another point Q as centre, and with Q C as radius describe another arc cutting C D in I. C I is the perpendicular required.



98. PROBLEM To bisect a line A B, or to divide it into two equal parts.

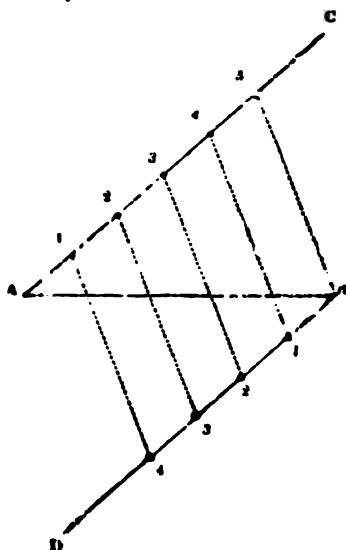
Take in the compasses a distance exceeding half the line, and from A and B, as centres, describe two arcs. The line I K, joining the points of their intersection, divides the line A B into two equal parts, A M, M B.



99. PROBLEM. To divide a line, A B, into any proposed number of equal parts, as five, for example.

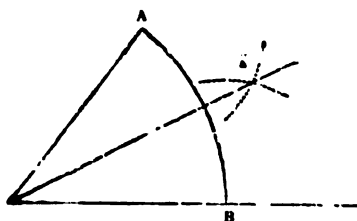
Draw a line A C, making about half a right angle with A B. Draw another line, B D parallel to A C. On A C and B D lay off

five equal parts; join the points 1 and 4, 2 and 3, &c.; these lines will divide AB into 5 equal parts.



In like manner, the line might be divided into any other number of equal parts.

100. PROBLEM. To bisect an arc AB , or an angle ACB .

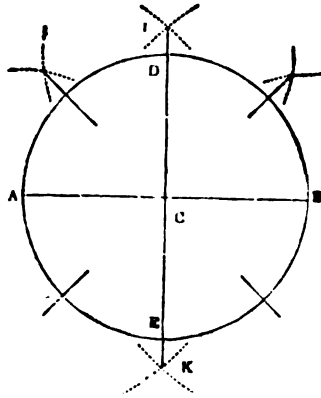


From the points A and B , as centres, with a radius exceeding half the distance AB , describe two arcs cutting each other in I , and draw the line CI ; CI bisects the arc AB , and the angle ACB . If the angle alone is given, and not the arc subtending it, describe this arc from C as a centre, with any convenient radius.

101. PROBLEM. To divide a circle into 2, 4, 6, &c. equal parts.

Draw the diameter AB ; this divides the circle into two equal parts. From A and B , as centres, with a radius exceeding half AB , describe the arcs I and K , cutting each other above and below AB ; join IK : the line ED is a diameter crossing AB at right angles, and dividing the circle into the four quadrants, AE , EB , BD , and DA . Bisect the arc AD (No. 100); draw the diameter through C : this will bisect BE also. Bisect, in like manner, BD and AE . The circle is now divided into 8 equal parts, of 4 points each; bisecting these last arcs divides the circle into 16 equal parts, of $22\frac{1}{2}^\circ$ each.

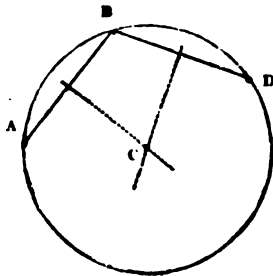
and again bisecting these divides it into the 32 points of the compass of $11^{\circ}\frac{1}{4}$ each.



An arc is divided into a number of parts not divisible by 2, as into 3, 5, 7, &c. parts, by trial.

102. PROBLEM. To find the centre of a circle, or circular arc.

Take two points, as A B, on the circumference, and join them; bisect the line A B (No. 98), and at the middle point draw a perpendicular (No. 96, 3d). Take a third point, D, join it with B; bisect the line B D, and draw a perpendicular at the middle point. The two perpendiculars will cross at the centre.



103. PROBLEM. To draw a circle through three given points.

Suppose the three points to lie in a circle, and proceed to find the centre as above.

It is easy to see that however three points may be placed, some one circle will always pass through them; for an infinite number of circles may be drawn passing through two points, and therefore some one of these must likewise pass through a third point wherever situated.

3. Use and Construction of the Scales.

104. These are flat, thin pieces of brass, ivory, or wood divided into certain portions by lines, and serve for measuring, or laying off *lines or distances*, and *angles*.

The common scale of equal parts has generally on one side four or five different scales for different measures, on each side of which one division is subdivided into 10 equal parts.

105. In the diagonal scale, the shorter lines dividing the length into equal portions (units) are crossed perpendicularly by 10 others extending the length of the scale. The end division, or unit, has its upper and lower edge subdivided into 10 equal parts, and diagonal lines are drawn from the beginning of one division to the end of the opposite one. This effects a further subdivision by 10, as an example will shew. To take the No. 5.28 from this scale by the compasses. Set one foot at 5, and the other at the second line on the lower edge of the subdivided unit,—this gives 5.2. Now follow up the diagonal line at the .2 to the eighth of the long parallel lines, and, fixing the point there, extend the other point to meet the line which rises at 5, crossing the breadth; and the number is taken.

The same process serves for tens and units, as for units and tenths, and so on; thus the No. 52.8, or 528, is taken as above.

By placing the points of the compasses *between*, instead of *on*, the 10 long parallel lines, we may obtain a still further subdivision.



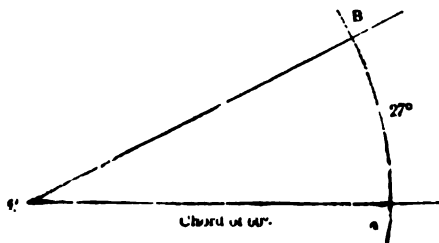
106. Angles are measured, or laid off, either by means of the lines marking the divisions of degrees, or half degrees, at the edge of the scale, and which are numbered at each 10° or 5° , or by means of the

Scale of Chords.



(1.) To measure an angle by the marked divisions. Place the middle point of the scale (which is strongly marked) upon the angular point, and lay the edge along one of the legs; the other leg, produced, if necessary, shews, on the graduated edge, the degrees which the angle contains.

(2.) To measure an angle by the scale of chords. Take in the compasses the chord of 60° off the scale, and describe an arc: take the distance from A to B in the compasses, and, placing one foot at



the beginning of the scale of chords, look how many degrees the other foot extends to. Thus, for example, if AB extends to 27° , the arc AB , or angle, C , contains 27° .

107. To lay off an angle from a given line, as, for example, 27° . Describe an arc AB (fig. 106), with the chord of 60° , from C , as centre, and set off the chord of 27° from A on AB ; join CB , and ACB is the angle required.

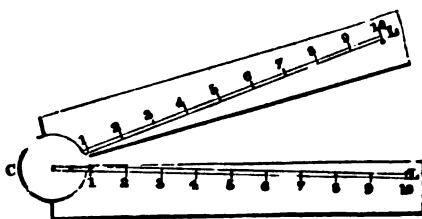
When the angle to be measured or laid off exceeds 90° , measure or lay off 90° , and then the excess above 90° .

108. The semicircle with a graduated edge is useful for this purpose; but the most convenient instrument, especially for using with the chart, is a transparent horn semicircle, with a long silk thread attached to its centre.*

109. To construct a scale of chords to any proposed radius. The radius is equal to the chord of 60° ; describe, therefore, a quadrant, divide it into portions of 30° , 20° , 10° , and so on; draw the several chords, and transfer them to the proposed scale.

4. The Sector.

110. The Sector is a ruler, or scale, which folds into half its length by moving round a large circular joint on which it is accurately centered. Several lines, or scales, are laid off from the centre to the extremity on both legs of the sector, as tangents, sines, &c., and others parallel to the edges. We shall refer here only to that one which is called the *line of lines* (marked CL in the figure), on account of the great convenience of the sector in reducing a plan, or a figure, to another on a different scale, dividing lines proportionally,† and in solving some simple questions which depend on proportion alone.



The line of lines is divided into 10 equal parts, and these again are similarly subdivided. The distance from the centre to any point in the line of lines is called the *lateral distance*; and that between any point in the line of lines on one leg, and the corresponding point on the other, the *transverse distance*.

* Such semicircles, made of horn or other transparent material, and having a long silk thread attached to the centre to extend a straight line to any point beyond the circumference, are most useful, especially for chart work. They are commonly called protractors.

† Another instrument, equally convenient and portable, but more expensive, is the *proportional compasses*. These compasses open on a movable centre, so that the opening of one pair of points may, by moving the centre, be made to bear any proportion to the opening of the other pair of points.

The following examples will illustrate the use of the Sector.*

Ex. 1. To divide a line into a number of equal parts, as for ex. 7.

Take the given line in the compasses; place one point on the division 7 on one leg of the sector, and open it till the other falls on the other 7. Then the transverse distance 1 to 1 is 1-7th, 2 to 2 is 2-7ths, and so on; or the line 7, 7 is equally divided into the parts 1, 1; 2, 2; &c.

Ex. 2. To reduce a plan on the scale of 3 inches to a mile, to another scale of 2 inches to a mile.

Take the lateral distances on the scale of the 3-inch plan. Take 2 in the compasses; place one point at the division 3, and open the sector till the other point falls on the other 3. Then the transverse distances will be the distances on the proposed plan.

Ex. 3. A line of a given figure measures 85; find the measure of another line in the same figure.

Take the given line 85 in the compasses and open the sector till their points measure the transverse distance 85, 85. Then any other line of the figure taken in the compasses is measured by finding the corresponding points in the two legs which exactly contain it, and multiplying the number shewn by 10.

* See J. F. Heather on Mathematical Instruments, Lockwood & Co., Ludgate Hill.

V. RAISING THE TRIGONOMETRICAL CANON

111. This term implies forming the proportions or analogies proper for the solution of problems concerning right-angled triangles.

Before, however, the student proceeds to the actual composition of these analogies, he should be acquainted with the few propositions of geometry which are given in the following section.

112. DEFINITION. An AXIOM is a proposition assumed to be so obvious as to require no demonstration.

The principal axioms which have been employed as the foundation of geometrical reasoning are the following:—

(1.) Geometrical magnitudes are said to be equal when one being placed on another coincides with, or exactly covers, it.

(2.) Two magnitudes which are each equal to a third, are equal to each other.

(3.) If equals be added to equals, the wholes will be equal.

That is, if two magnitudes be equal, and a third be added to each, the two sums will be equal.

(4.) If equals be taken from equals, the remainders will be equal.

(5.) If the same or equal quantities be added to unequals, the sums will be unequal.

(6.) If equals be taken from unequals, the remainders will be unequal.

(7.) The halves of equal things are equal.

(8.) The doubles of equal things are equal.

113. DEF. A GEOMETRICAL THEOREM is a proposition in which some property of a figure is demonstrated.

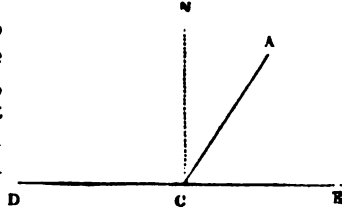
The term PROPOSITION includes both Problems and Theorems.

114. DEF. A COROLLARY is an obvious conclusion or necessary inference, from a proposition.

1. Theorems of Geometry.

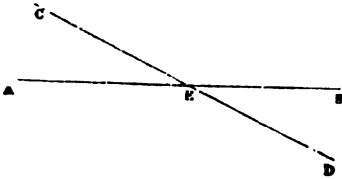
115. A straight line, as AC , standing on another, as DE , makes the adjacent angles, ACE and ACD , together equal to two right angles.

For, draw CN at right angles to DE ; then DCN and NCE are two right angles; that is, DCN , with NCA and ACE , are two right angles; and since DCN and NCA make up DCA , therefore, DCA and ACE are two right angles.



116. If two straight lines, as AB , CD , intersect or cross each other, the opposite and vertical angles, as CEA , BED , are equal.

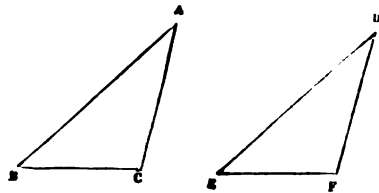
Since CE stands on AB , the angles CEA and CEB are equal to two right angles (No. 115). Again, since BE stands on CD , the angles CEB and BED are equal to two right angles. Hence CEA and CEB are equal to BED and CEB . Take away the angle CEB , common to both these sums, and the remaining angles CEA , BED are equal. (No. 112, 4).



117. If two triangles, as ABC , DEF , have two sides of the one, as AB , AC , equal to two sides of the other, as DE , DF , and have likewise the angles A , D , contained by those sides, equal, the two triangles are equal in all respects.

For if the point A be laid on D , and the line AB on DE , the point B will coincide with E because AB is equal to DE .

Also, since the angles A , D , are equal, the line AC will coincide with DF , and the point C of AC will coincide with the point F of DF , because AC is equal to DF .



Then since B coincides with E , and C with F , the base BC coincides with the base EF , and is therefore equal to it.

Since therefore the three sides of the triangles are equal, the triangles are equal, and either laid on the other (two equal sides being laid on two equal sides) will exactly cover it. Hence the two remaining angles must be equal, or B is equal E , and C to F ; or, the triangles are equal in all respects.

The above proves the method No. 100. For suppose A and I , B and I to be joined by lines, then the two triangles CAI , CBI , have the sides CA , AI equal to CB , BI , and the third side common. Hence they are equal, and the angles ACI , ICB being equal, each is half of ACB .

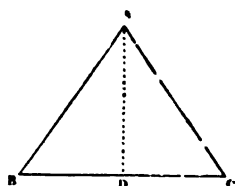
118. If two triangles ABC , DEF (fig. No. 117) have the angles B , C , in one, equal to two angles E , F , in the other respectively, and also the sides BC , EF , adjacent to the equal angles, equal to each other, the two triangles are equal.

Suppose the point B to be laid on E , and the side BC on EF , the points C and F will coincide because BC is equal to EF .

Again, since the angles B and E are equal, the side BA will fall on ED ; and because the angles C and F are equal, the side CA will fall on FD . Hence, as the point A belongs to both the sides BA and CA , and D to ED and FD , the point A will coincide with D , and the angles A and D are equal. Hence the two triangles are equal.

119. In an isosceles triangle, as ABC , the angles B , C , opposite the equal sides AB , AC , are equal.

Suppose the angle BAC bisected by the line AD . Then since AB and AC are equal, and the side AD common to the two triangles ADB , ADC , and the angle BAD equal to CAD , each being half of BAC , these two triangles are equal in all respects (No. 117), and therefore the angles B and C are equal.



COR. 1. Since the base BD is equal to the base CD , a line bisecting the angle contained by the two equal sides of an isosceles triangle likewise bisects the third side.

COR. 2. Also, since the adjacent angles ADB , ADC are equal, they are right angles, or the said line is perpendicular to the third side.

COR. 3. If the third side is equal to AB or BC , the angle A is equal to B or C ; or an equilateral triangle is equiangular.

This proves the method No. 97 (1); for supposing CD , DI , and CE , EI joined, the two CD , DI are equal to CE , EI , and CI is common; hence the triangles are equal. And the angles DCI , ECI are equal, and each is half DCE ; hence CI bisects DCE and is perpendicular to AB .

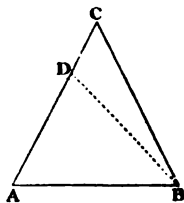
The like proof applies to No. 97 (2); for suppose PI , QI to be joined; then CP , CQ are equal to PI , QI , and PQ is common; hence CPQ is equal to IPQ , and PB which thus bisects CPI , is perpendicular to CD .

The same kind of proof applies to Nos. 96 (3) and 98.

120. Every triangle which has two angles, A , B , equal, is isosceles; or the sides CA , CB are also equal.

If CA is not equal to CB , let it be greater, and take a part of AC , as AD , equal to CB .

Then since DA , CB are equal, add to each of them AB , and the two DA , AB , are equal to the two CB , AB (No. 112, 3). Also, since DA is equal to CB , the angles DAB , CBA are equal (No. 119). Hence the triangle ADB , having the two sides DA , AB , and the included angle DAB equal to the sides CB , AB , and the angle CBA , is equal to the triangle CBA (No. 117), or the less to the greater, which is absurd. Hence AC , CB are not unequal, that is, they are equal.

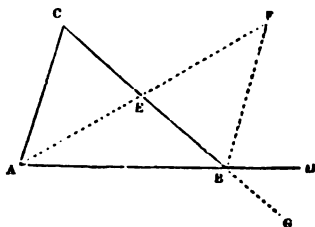


COR. If the third angle C is equal to A or B , the side AB must

In like manner be equal to CB , or to CA ; that is, every equiangular triangle is equilateral.

121. If a side of a triangle ABC , as AB , be produced, the exterior angle CBD is greater than either of the interior and opposite angles A and C .

Bisect CB in E , join AE and produce the line till EF is equal to AE ; and join FB .

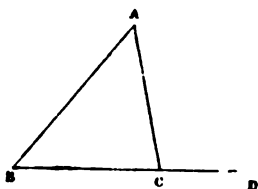


Then since AE is equal to EF , and BE to EC , and also the angle AEC to the angle BEF , the two triangles AEC , BEF have two sides and the included angle equal in each. Hence these two triangles are equal (No. 117), and therefore the angle C (opposite the side AE) is equal to the angle EBF (opposite the equal side EF). Hence CBD which contains CBF is greater than C .

In like manner, by producing CB to a point G , and bisecting AB , it would be proved that the angle ABG , or its equal CBD , is greater than A .

122. Any two angles of a triangle are together less than two right angles.

Produce the side BC of the triangle ABC , to D . Then the exterior angle ACD of the triangle is greater than the interior and opposite angle ABC (No. 121). Add to each angle ACB , then ACD and ACB , are greater than ACB and ABC (No. 112, 5); and since ACD , ACB are equal to two right angles, ACB , and ABC are less than two right angles. The same may be proved of the other angles by producing the other sides.



123. If a straight line AB meeting two other lines CD , EF , makes the alternate angles CGH , GHI equal, the two lines are parallel.

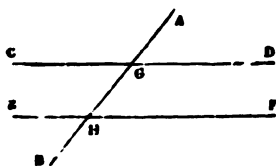


Fig. 1.

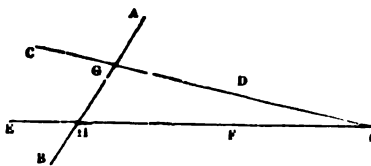


Fig. 2.

For if they are not, they will meet on one side of AB ; let them meet at I , then GHI is a triangle, and the exterior angle CGH is greater than the interior and opposite angle GHI (No. 121). But these angles are equal by the supposition, therefore the lines do not meet towards I .

In like manner it may be shewn that they do not meet on the

other side of AB , and hence that they do not meet at all; that is, they are parallel.

It appears by fig. 2, that the lines meet on that side on which the two interior angles are less than two right angles. For IGH , IHG are together less than two right angles (No. 122).

124. If a straight line AB (fig. 1, No. 123) falling on two lines CD , EF , make the exterior angle AGD equal to the interior and opposite angle GHF (on the same side of AB), the two lines are parallel. Also, if the two interior angles DGH , GHF , are equal to two right angles, the lines are parallel.

The angle AGD is by supposition equal to GHF , and AGD is equal to CGH (by No. 116); hence CGH and GHF are equal, and they are alternate angles, and CD , EF are parallel.

Again, since DGH , GHF are equal to two right angles by the supposition, and since CGH , DGH are equal to two right angles by No. 115, CGH , DGH , are equal to DGH , GHF ; take away the common angle DGH , and the remaining angle CGH is equal to GHF , and they are alternate angles, therefore CD , EF are parallel.

125. If a straight line AB (fig. 1, No. 123) fall on two parallel lines CD , EF , it makes

- (1.) The alternate angles CGH , GHF , equal;
- (2.) The exterior angle AGD equal to the interior and opposite angle GHF ;
- (3.) The two interior angles DGH , GHF , equal to two right angles.

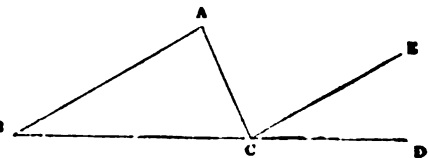
(1.) If CGH be not equal to GHF , let it be greater; add to each the angle DGH ; then the angles CGH , DGH are greater than the angles DGH , GHF , and CGH , DGH are equal to two right angles (No. 115); therefore DGH , GHF are less than two right angles. But, by fig. 2, No. 123, this is the case in which the two lines meet at I , whereas they are here parallel by the supposition; therefore CGH is not greater than GHF . In like manner it might be shewn that it is not less; it is therefore equal to GHF .

(2.) Since AGD is equal to CGH (No. 116), and CGH to GHF , therefore AGD is equal to GHF .

(3.) Hence, adding DGH to AGD , GHF , the two AGD , DGH are equal to the two DGH , GHF . But AGD , DGF are equal to two right angles; therefore DGH , GHF are equal to two right angles.

126. PROP. The exterior angle, as ACD , of a triangle (formed by producing one of the sides of the triangle), is equal to the sum of the two interior and opposite angles, ABC and BAC .

Produce the side BC to D , and draw CE parallel to BA . Then the angle ECD is equal to ABC since BD meets the



parallels BA and CE (No. 125). Again, the alternate angles BAC , ACE , formed by AC , which crosses the same parallels, are equal (No. 125). Hence ACE and ECD are together equal to BAC and ABC ; that is, ACD , which is made up of ACE and ECD , is equal to BAC and ABC .

127. **PROP.** The three interior angles of a triangle are together equal to two right angles (fig. No. 126).

By the above proposition, ACD is equal to the sum of ABC and BAC . Add to each ACB ; then ACD and ACB are equal to the three angles ABC , BAC , and ACB . (No. 112). But ACD and ACB are equal to two right angles, therefore the angles ABC , BAC , and ACB , are equal to two right angles.

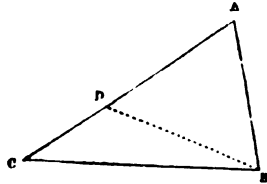
COR. 1. In a triangle which has one right angle, the other two angles make up a right angle; each of them, therefore, must be less than a right angle, and each is the complement of the other to 90° .

COR. 2. If two triangles have two angles in the one equal, respectively, to two angles in the other, they will also have the third or remaining angles equal.

128. **PROP.** The greater side of any triangle, as AC , is opposite to the greater angle ABC .

CA being greater than AB , make AD equal to AB , and join DB ; then since AD is equal to AB , the triangle ABD is isosceles, and the angles ADB and ABD are equal (No. 119). But ABD which is contained within ABC is less than ABC . Hence ADB is less than ABC . Now ADB is equal to the sum of ACB and CBD (No. 125); hence ADB is greater than ACB , that is ABD is greater than ACB , therefore ABC is greater than ACB .

In like manner, by taking CD equal to CB , it would be proved that the angle B is greater than the angle A ; and, by taking D on BC , and BD equal to BA , that the angle A is greater than the angle C .

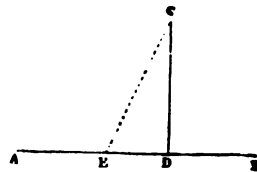


129. **PROP.** The line drawn perpendicularly from a given point C , to a right line AB , as CD , is the shortest that can be drawn from C on AB .

Take any point E in AB , and join CE . Then since in the triangle CED , CDE is a right angle, the angle CED is less than a right angle (No. 127, Cor. 1), and therefore (No. 128) CE is greater than CD .

The same proof applies to any point whatever taken in AB .

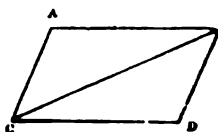
COR. As the angle CED is acute, wherever E may be taken, there is but one line which can be drawn perpendicular to AB from C .



130. **DEF.** A Parallelogram is a four-sided figure of which the opposite sides are parallel.

131. The opposite sides of a parallelogram, as AB, CD , are equal; also the opposite angles are equal; and the diameter, or diagonal, CB divides it into two equal parts.

Since AB and CD are parallel, and CB meets them, the alternate angles ABC and BCD are equal (No. 125). Also, since AC, BD , are parallel, and BC meets them, the alternate angles ACB, CBD are equal. Hence the two triangles ABC, BCD having two angles equal in each, and the side BC adjacent to them common, are equal (No. 118). Hence AB is equal to CD , and AC to BD ; also the third angle A to the third angle opposite, D .



Since the two triangles are equal, and make up the whole figure, each is half the parallelogram, or CB bisects AD .

132. The straight lines CA, BD (fig. No. 131) which join the extremities of two equal and parallel lines AB, CD are themselves both equal and parallel.

The triangles ACB, CBD , having the two sides AB, CD equal, and the side BC common, and also the included angles ABC, BCD equal, are equal; hence AC and BD are equal.

Again, since the other angles are equal, ACB and CBD are equal, and hence AC, BD are parallel.

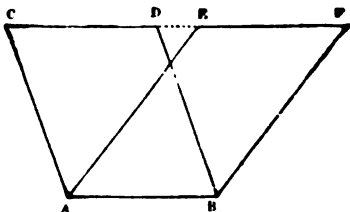
This proves the method No. 93; for the equal distances laid off from C and B perpendicular to AB , form two sides of a parallelogram, of which the other sides also are parallel.

And the like reasoning applies to No. 94.

133. Parallelograms, as $ABCD, ABEF$, on the same base AB and between the same parallels AB, CF , are equal to each other.

Since CD and EF are each equal to AB , they are equal to each other.

Add to each DE , then CD, DE , are equal to EF, DE (No. 112, 3), or CE is equal to DF . Also AC is equal to BD , and AE to BF ,



nence AC, CE are equal to BD, DF , and the angles ACE, BDF ,

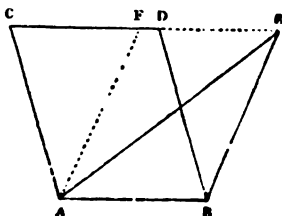
are equal, because AC is parallel to BD (No. 125). Hence the triangle ACE is equal to the triangle BDF (No. 117).

Take away the triangle ACE from the whole figure $ABCF$, and the remainder is $AEFB$; again, take away the triangle BDF from the same figure, and the remainder is $ABCD$; therefore since these triangles are equal the remainders are equal (No. 112, 4), or the parallelograms $ABCD, ABEF$ are equal.

COR. Parallelograms on equal bases, and between the same parallels, are equal. For since the bases are equal, either of them placed on the other will coincide with it, and the above proof applies.

134. A Parallelogram $ABCD$ is double of a triangle ABE on the same base, AB , and between the same parallels, AB, CE .

Draw AF parallel to BE , then $ABFE$ is a parallelogram, and it is equal to $ABCD$ (No. 133). Hence the triangle ABE , which is half of $ABFE$, is equal to half $ABCD$, or the parallelogram is double of the triangle.

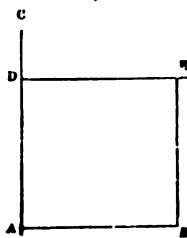


Cor. Triangles on the same or equal bases, and between the same parallels are equal. For parallelograms under these two conditions are, by No. 133, and Cor., equal, and the triangles being the halves of equal parallelograms, are equal.

135. DEF. A Square is a four-sided figure of which all the sides are equal, and all the angles right angles.

136. PROB. To describe a square, AE , on a given line, AB .

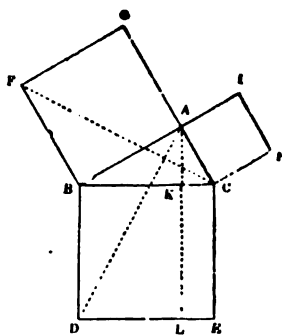
Draw AC perpendicular to AB , take AD equal to AB , and through D draw DE parallel to AB ; and through B draw BE parallel to AD (or take DE equal to AB , and join BE). Then $ADEB$ is a parallelogram, of which the opposite sides, being equal, are each equal to AB . Also since DE is parallel to AB , and AD meets them, the angles EDA, DAB , are equal to two right angles, and since A is a right angle, D is a right angle, and the opposite angles to these being equal to them are also right angles.



137. In any right-angled triangle, as ABC , the square BE , on the hypotenuse BC , is equal to the sum of the squares GB and CI on the other two sides.

Draw AKL perpendicular to BC , or parallel to BD , which is perpendicular to BC , and join FC and AD .

Then, since BD is equal to BC , and FB to BA (No. 135), the two sides FB, BC are equal to the two AB, BD (No. 112, 3). Also, the angles ABD and FBC are equal, since each contains a right angle and the common angle ABC . Hence the triangles ABD and FBC are equal (No. 117).



Now the triangle ABD is half the parallelogram BL , because they are on the same base BD , and between the same parallels BD, AL (No. 134). Likewise the triangle FBC is half the square BG , since GC and FB are parallel. Hence the parallelogram BL and the square BG are equal.

In like manner, by joining the points B, H , and A, E , it would

be proved that the parallelogram CL and the square CI are equal.

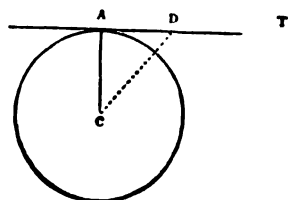
Hence the sum of the squares BG , CI , is equal to the sum of the parallelograms BL , CL , that is, to the square BE .

Hence in a right-angled triangle if we have two sides we can always find the third: thus, suppose the hyp. is 100, and the base 64, the squares of these are 10000, and 4096; the diff. of these squares, or 5904, is therefore the square of the unknown side, which is 76.8.

The theorem above proves that the triangle of the dimensions in No. 96 (1) is right-angled. For 3, and 4, squared, are 9 and 16, and the sum of these, or 25, is the square of 5, the third side.

138. The perpendicular on the extremity of the radius of a circle, as AT , is a tangent to the circle.

Take any point D in AT , and join CD ; then since CAD is a right angle, CDA is less than a right angle (No. 127), and therefore CD is greater than CA (No. 128) or falls beyond the circumference, that is, AT touches the circle at A only.



Cor. As only one line can be perpendicular to AT (No. 129), the centre of the circle must be in the line perpendicular to the tangent.

139. The angle at the centre of a circle, as ACB , is double the angle at the circumference, as ADB , both angles standing on the same arc AB .

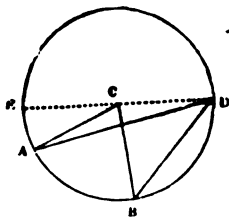


Fig. 1.

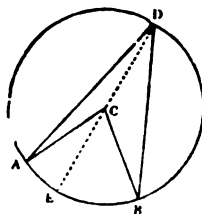


Fig. 2.

Join D on the circumference and C the centre, and produce the line DC to E ; then the exterior angle ACE of the triangle ACD is equal to the sum of the two interior and opposite angles CAD , and CDA (No. 126). But CAD is equal to CDA , because CA and CD being equal, ACD is an isosceles triangle (No. 119). Hence ACE at the centre is equal to twice ADE at the circumference.

Again, the exterior angle BCE of the triangle BCD is equal to the sum of CBD and CDB . But these angles also are equal, because CB and CD being equal, BCD is an isosceles triangle; hence BCE at the centre is equal to twice BDE at the circumference.

Now, in fig. 1 (where the diameter of the circle passes clear of the arc $A B$), $A C B$ is the difference of $B C E$ and $A C E$, and is double of $A D B$, the difference of $B D E$ and $A D E$.

When E falls on $A B$, as in fig. 2, $A C B$ is the sum of $A C E$ and $B C E$, and is double the sum of the angles $A D E$ and $B D E$, or the angle $A D B$.

140. The angle at the circumference is measured by half the arc subtending it (fig. No. 139).

As $A C B$ at the centre is measured by the arc $A B$, it is evident that $A D B$ at the circumference (which, by the prop. is half $A C B$), is measured by half $A B$. Thus, if $A B$ is 58° , the angle $A D B$ will be 29° , for any point of the circumference at which D may fall, except between A and B .

This proves the method No. 100, for, since $C A$, $A I$ (supposing A , I , and B , I , joined) are equal to $C B$, $B I$, and $C I$ common, the triangles $C A I$, $C B I$ are equal, — hence $A C I$ and $I C B$ are equal; each therefore is half of $A C B$, and is measured by half the arc $A B$.

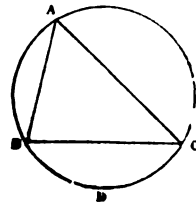
141. The angle in a semicircle is a right angle.

If the arc $A B$ increases to a semicircle, A moving to E and B to D , $A C$ and $C B$ (fig. 1, prop. 139) falling into the same line, form a diameter, the angle $A C B$ becomes two right angles or 180° , and then $A D B$, or half $A C B$, is 90° . Hence the angle in a semicircle is a right angle.

This theorem proves the method No. 96 (2), for since $I K$ is a diameter, the angle at M , a point on the circumference, is the angle in a semicircle.

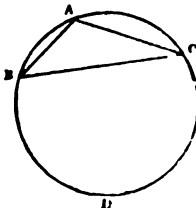
142. The angle in a segment greater than a semicircle is less than a right angle.

The segment $B A C$ of the circle being greater than a semicircle, the other segment $B D C$ must be less than a semicircle; and the angle $B A C$ in the greater segment being measured by half the arc $B D C$, that is, by a quantity less than half 180° (No. 140), is less than a right angle.



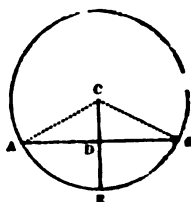
143. The angle in a segment less than a semicircle is greater than a right angle.

The segment $B A C$ being less than a semicircle, the segment $B D C$ must be greater than a semicircle, and therefore the angle $B A C$, which is measured by half $B D C$ (No. 140) is greater than half two right angles or than one right angle.



144. A line, $C D$, drawn from the centre of a circle bisecting any chord $A B$, is perpendicular to the chord.

Join CA , CB , then CA and CB are equal by the def. of a circle (No. 74). Also AD and DB are equal, each being half of AB , and CD is common to the two triangles CAD , CBD . These triangles, therefore, having their three sides equal, are equal; hence the equal angles CDA , CDB , opposite the equal sides CA , CB , being adjacent angles, are right angles.

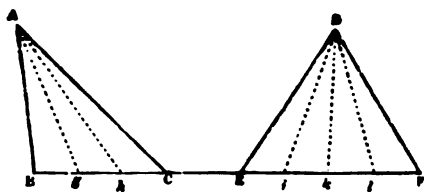


Cor. The line from the centre bisecting the chord bisects the arc AB . For since the two triangles, as above, are equal, the angles ACD and BCD , opposite the equal sides AD , DB , are equal, and being at the centre are measured by the arcs on which they stand.

The above proposition is the principle of the method of finding the centre of a circle, No. 102.

145. Triangles having the same altitude are proportional to their bases.

The altitude is the perpendicular distance of the vertex, or summit, from the base.



Let the base BC of the triangle ABC be divided into any number of equal parts, as three, Bg , gh , hC , and EF the base of the triangle DEF , into four like parts, Ei , ik , kl , lF , then BC is to EF as 3 to 4.

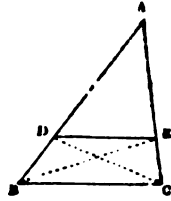
Join the points Ag , Ah , and Di , Dk , Dl . Then the triangles ABg , $Ag h$, $A h C$, and DEi , $Di k$, $Dk l$, $D l F$ are all equal, being on equal bases, and having the same altitude (No. 134, Cor.)

Hence the triangle ABC contains three parts, of which DEF contains four, and, therefore $ABC : DEF :: 3 : 4$, which is the ratio of the bases.*

146. A line DE parallel to a side BC of a triangle ABC divides the sides AB , AC , in the same proportion, that is, $AD : AB :: AE : AC$.

* If it be impossible to find a quantity, or measure, Bg , which shall divide BC and EF into an exact number of equal parts, as 3 and 4 above (that is, when BC and EF are said to be incommensurable) we must take a smaller quantity, and a greater number of triangles; and by taking this measure sufficiently small we may make the error of using it instead of the true proportion as small as we please.

Join BE, CD . Then the triangles BDE, CDE on the same base DE , and between the same parallels DE, BC , are equal (No. 134, Cor.) Add to each the triangle ADE , then the whole triangle ABE is equal to the triangle ADC (No. 114, 3). Hence the triangle $ABE : ABC :: ADC : ABC$.



Now triangle $ABE : \text{triangle } ABC :: \text{base } AE : \text{base } AC$, since they have the same altitude, viz. the perpendicular drawn from B on AC or AC produced (No. 145). Also, triangle $ADC : \text{triangle } ABC :: \text{base } AD : \text{base } AB$, And the triangle ABE is equal to the triangle ADC , hence the two proportions are the same, and $AE : AC :: AD : AB$.

In like manner, as the triangles ADE, EDB , have the same altitude, viz. the perpendicular drawn from E on AB , we have triangle $ADE : \text{triangle } EDB :: AD : DB$.

Also since the triangles ADE, EDC have the same altitude, viz. the perpendicular from D on AC ,

triangle $ADE : \text{triangle } EDC :: AE : EC$.

But the triangles EDC and EDB are equal, hence

$AD : DB :: AE : EC$.

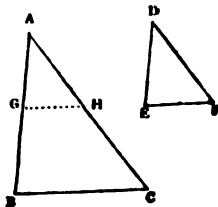
This proof applies to the sector. The line of lines on each leg is the side of an isosceles triangle, and the transverse distances 1, 1, 2, 2, &c., are the bases of so many isosceles triangles; the angles at these bases being equal, the bases are parallel, and the sides of the several triangles so formed are proportional.

147. DEF. Similar triangles are such as have the sides about the equal angles proportional.

148. Equiangular triangles, as ABC, DEF , have the corresponding sides about the equal angles proportional, that is $AB : AC :: DE : DF$.

Let the angles A and D be equal, as also B and E, C and F .

Place the triangle DEF on ABC , D being placed on A , and DE on AB , and let G be the point where E falls.



Then since the angles A and D are equal, and DE is on AB , DF will fall on AC ; let, therefore, H be the point where F falls. Then since AGH is equal to E , and B to E , AGH is equal to B , and the lines GH and BC , which make equal angles with AB , are therefore parallel. Hence, by No. 146, $AB : AC :: DE : DF$.

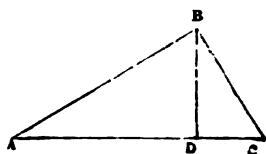
COR. Hence equiangular triangles are similar (No. 147.)

149. In a right-angled triangle ABC , a line BD drawn from the right angle perpendicular to the hypotenuse, divides the triangle into two similar triangles ABD, BDC .

The triangles ABC , ADB , having each a right angle, and the angle A common, have the third angle also equal (No. 127), they are, therefore, equiangular.

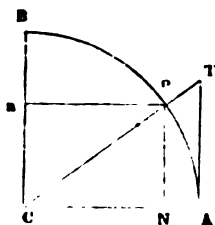
For the like reasons ABC and BDC are equiangular; therefore the two triangles ABD , BDC , are equiangular, and the sides about the equal angles are proportional (No. 148). Hence

- (1) $AC : AB :: AB : AD$.
- (2) $AC : CB :: CB : CD$.
- (3) $AB : AD :: BC : BD$.*



2. Terms of Trigonometry.

150. These terms occur in all calculations in which lines and angles are concerned.



151. PNC is a right-angled triangle; a quadrant is described with the radius CP , from the centre C ; CN and CP are produced, and AT is drawn parallel to PN .

152. The perpendicular PN , drawn from the extremity of the arc AP , upon the radius CA , is called the *sine* of the angle PCA (to which it is *opposite*).

When the arc is very small, or P very near A , PN and AP , or the arc and sine, nearly coincide. When the arc is 0 , the sine is 0 . When the arc is 90° , P falls at B , or the sine of 90° is equal to the radius. Thus the sine is always less than the radius, though near 90° it becomes very nearly equal to it.

153. The line CN , between the centre and the foot of the sine, is called the *cosine* of PCA (to which it is *adjacent*). It is called cosine because its equal Pn , is the *sine* of PCn , the *complement* of PCN .

When the arc is small, N falls near A , and CN falls nearly on CA , or the cosine of a small arc is nearly equal to the radius; for the arc 0 , they are equal. When the arc is near 90° , the cosine is very small; and the cosine of 90° is 0 . Thus the cosine is always less than the radius, though it may approach indefinitely near to it.

* By (1) $AC \times AD = AB \times AB$, or, as it is written, AB^2 , and read AB square; and by (2), $AC \times CD = CB^2$; hence the products $AC \times AD$ and $AC \times CD$ are together equal to AB square and BC square. But $AC \times AD$ and $AC \times CD$, is the same as $AC \times AD$ and CD , or as $AC \times AC$, which is called AC square; hence AC square is equal to AB square and BC square. The term square here denotes the number of units (in the line) multiplied by itself; thus, if AB is 3 , AB^2 is 9 , and this is the number of square units contained in the square described on AB . Hence this is another form of the propos. in No. 137.

154. The line AT , drawn from the extremity of one radius (as CA), touching the circle, and meeting the other radius produced, is called the *tangent* of the angle PCA , or arc PA .

When the arc is small, AT but little exceeds PN ; when the arc is 0 the tangent is 0; when the arc is small, the tangent and sine may be taken for each other, and for the arc. When the arc is 90° , the tangent is infinitely great. The tangent is less than the radius, according as the angle is less or greater than 45° .

The *cotangent* is the tangent of PCn , which is the complement of PCN , and would be drawn from the extremity of the radius CB , meeting CP produced.

155. The line CT meeting the tangent, is called the *secant*.

The *cosecant* is the secant of PCn , and meets the cotangent.

When the arc is 0, the secant is equal to the radius. When the arc is 90° , the secant is infinitely great. The secant is always greater than the radius, as is also the cosecant.

156. The line AN is called the *versed sine*.

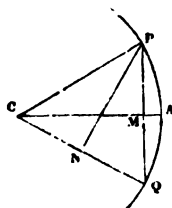
157. These quantities are calculated for a radius of the same constant length, and to each minute or smaller division of the quadrant, and are inserted in Tables. Then, since the sides of all right-angled triangles having the same angles are proportional (No. 148), the tables afford the means of finding the relations among the parts of a right-angled triangle, of any kind or dimensions, by simple proportion. For example, the sine of 30° is $\frac{1}{2}$ the rad. (see No. 159, Cor.), or 0.5, the log. of which, by No. 58 (2), is 9.698970, as inserted in Table 68.

These are the principles on which the Traverse Tables and the Trigonometrical Tables are constructed.

3. Propositions of Trigonometry.

158. The sine of an arc is half the chord of twice the arc.

Take the arcs AP , AQ equal to each other, and join PQ . Then the angles PCA , ACQ are equal (No. 82). And since $CP = CQ$, and CM is common to the two triangles CPM , CQM , these triangles are equal (No. 117); hence $PM = MQ$; therefore PM , the sine of AP , is half PQ , the chord of twice AP .



159. The chord of 60° is equal to the radius.

Let AP and AQ (fig. No. 158) be each 30° , then the arc PQ is 60° ; and since the three angles of the triangle PCQ are equal to 180° (No. 127), CPQ and CQP are together equal to 120° . Also, since $CP = CQ$, these two angles are equal (No. 119), and each, therefore, is 60° . The triangle is, therefore, equiangular, and consequently, equilateral, No. 120. Hence $PQ = CP$.

Cor. Since PM is half PQ , it is equal to half CP ; or the sine of 30° , which is the cosine of 60° , is half the radius.

160. The secant of 60° is equal to twice the radius.

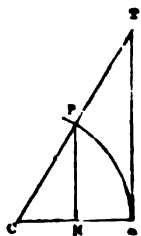
Since $P'N$ and AT are both perpendicular to CA , they are parallel (No. 124), and the triangles $CP'N$, CTA , are similar (No. 148), hence

$CT : CP' :: CA : CN$, that is, as $\text{rad.} : \cos.$
 60° , or as 1 to $\frac{1}{2}$, that is, as 2 : 1.

161. The tangent of 45° is equal to the radius.

Let $P'CA$ (fig. No. 160) be 45° , then CTA is also 45° (No. 127), hence the triangle is isosceles and the sides CA , AT are equal.

Cor. Hence also, by similar triangles, $CN = NP'$, or the sine and $\cos.$ of 45° are equal; as are also the tangent and cotangent.



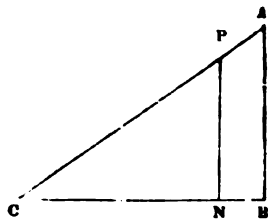
4. Constructing the Canons, and working them by Logarithms.

162. Take a right-angled triangle, as ABC , and suppose another similar to it, as $P'NC$, drawn in a quadrant, as in No. 151; then

$CA : AB :: CP' : PN$;

that is, $CA : AB :: \text{rad.} : \sin C$ (by 152).

The second triangle, $P'NC$, is, in fact, here referred to for illustration only; for it is evident, without it, that CA and AB themselves stand in the same relation to each other as that of *radius* and *sine*; hence



By No. 152. $CA : AB :: \text{rad.} : \sin C.$ (1.)

By No. 153. $CA : CB :: \text{rad.} : \cos C.$ (2.)

By No. 154. $CB : BA :: \text{rad.} : \tan C.$ (3.)

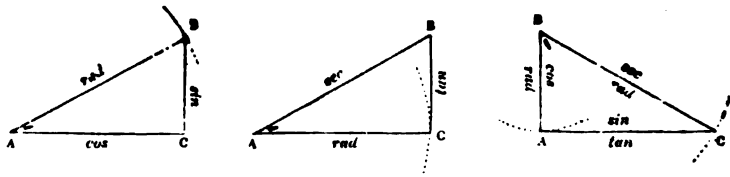
By No. 155. $CB : CA :: \text{rad.} : \sec C.$ (4.)*

163. It is easy to recollect these analogies, each of which begins with two sides, by observing these conditions.

1. One of the three sides must be made radius, and the analogy always begins with that side.

2. The other sides will then become sine, cosine, tangent, cotangent, secant, or cosecant, of one or the other of the two acute angles.

The figures below sufficiently illustrate the application of the terms.



* The learner will much more speedily apprehend the purposes which the expressions of trigonometry answer in the sciences of calculation by considering these proportions as representing the change of quantities in a certain ratio, as in No. 48 (3). Thus AB is CA diminished in the ratio of the sine of C to 1; CB in that of cosine to 1. AB is also CB diminished or increased in the ratio of $\tan.$ to 1, according as C is less or greater than 45° and CA is CB increased in the ratio of \secant to 1.

To employ rightly the terms *sine*, *cosine*, &c., observe—

3. That when the *hypotenuse*, or longest side (which is opposite the right angle), is made the radius,

The side *opposite* either of the acute angles is the *sine* of that angle; and the side *adjacent* to either angle is the *cosine* of that angle.

4. When either of the sides containing the right angle (or *legs*,* as they are called), is made radius, the other side becomes the *tangent* of the angle *opposite* to it; and the hypotenuse becomes the *secant* of that angle which is contained or included between *itself* and the *radius*.

The learner should be able to construct the above analogies (which he will find very easy) before he proceeds to the solution of any question, without regard to what is given or what is not given.

164. We now proceed to the calculation of a problem. The above analogies or proportions consist of four terms each. Hence, if three are given, the fourth may be found (No. 46). But the radius is assumed in the trigonometrical tables as 1 (which is the simplest of numbers), and hence, of the three remaining terms, if two are given, the third may be found.

Hence, in any right-angled triangle, consisting of three sides and two angles besides the right angle, if two parts which enter into any one of the above analogies are given, the third term of that analogy may be found.

165. The proportions may be solved by multiplication and division; thus, suppose, CA (fig. No. 162) measures 37 feet, and the angle C is $29^{\circ} 52'$, and we want to find AB.

We have by No. 162 (1), $CA : AB :: 1 : \sin. C$,

whence (No. 46) $AB = CA \times \sin. C$ (the 1 not being written).

Now the sine of $29^{\circ} 52'$, given in tables of natural sines (of which the *logs.* are given in Table 68) is 0.498 nearly, hence $AB = 37 \times 0.498 = 18.426$.

But in order to save such tedious processes, logarithms are employed in the manner described, Nos. 64 and 65. Thus, $AB = 37 \times \sin. C$, becomes $\log. of AB = \log. of 37 + \log. \sin. C$.

Again, if CA were required, and AB given, we should have $CA = AB \times 1 \div \sin. C$; or, (suppressing the 1).

$\log. CA = \log. AB - \log. \sin. C$.

The following rules are deduced from these principles.

The learner will do well to verify all his work by the *Traverse Tables*. This proceeding is described in the explanation to the *Traverse Tables*.

166. The rule for working any analogy by logarithms is very simple, and there are but two cases: 1. In which it is required to find one of the mean terms; and, 2. In which it is required to find one of the extreme terms.

* The two legs are also called the *base* and *perpendicular* (No. 89). These terms, being usually given to the sides which are horizontal and vertical, as the reader holds the figure before him, are employed entirely at convenience.

(1.) To find a *mean* term. Add together the logarithms of the two extremes, and subtract from the sum the logarithm of the other mean. The remainder is the logarithm of the term required.

(2.) To find an *extreme* term. Add together the logarithms of the two means, and subtract from the sum the logarithm of the other extreme. The remainder is the logarithm of the term required.*

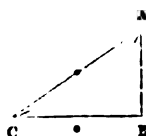
Note.—The log. of the *radius* (as employed in the analogies) is 10, this being used for convenience, as stated at p. 19, note †.

Case I. Given the angles and the hypothenuse, to find the two sides.

Ex. B is the right angle. The angle A is 50° (whence C is 40° , because the two acute angles are together 90°). (See No. 127, Cor.) CA is 28 feet. It is required to find BC and BA.

We must employ two sides, and one of them must be the unknown, or required side : hence,

to find CB,
we must take CA and C.



If CA, the hypothenuse, be radius, CB becomes the sine of A (No. 163), hence

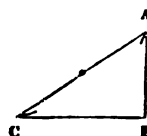
$$CA : CB :: \text{rad.} : \sin. A;$$

in which CB, a *mean* term, is required. Hence, by No. 166 (1), we have to add the logs. of CA and $\sin. A$, and subtract the log. 10.

CA 28	log. (tab. 64)	1.4472
A 50°	log. sin. (tab. 68)	9.8843
	log.	11.3315
	sub. 10.	
CB = 21.4	log.	1.3315

We might have used CB as $\cos. C$, that is, $CA : CB :: \text{rad.} : \cos. C$, otherwise $CB : CA :: \text{rad.} : \sec. C$.

to find AB,
we must take CA and A.



If CA, the hypothenuse, be radius, AB becomes the cosine of A (No. 163).

$$CA : AB :: \text{rad.} : \cos. A;$$

in which AB, a *mean* term, is required. Hence, by No. 166 (1), we have to add the logs. of CA and $\cos. A$, and subtract the log. 10.

CA 28	log. (tab. 64)	1.4472
A 50°	log. cos. (tab. 68)	9.8081
	log.	11.2553
	sub. 10.	
AB = 18.0	log.	1.2553

We might have used AB as $\sin. C$, that is, $CA : AB :: \text{rad.} : \sin. C$, otherwise $AB : AC :: \text{rad.} : \sec. A$.

* It is necessary to remark here that the process above differs from that followed by seamen in general, the object of which is simply that the required quantity may stand last.

The example in Case III. by that method stands thus :

To find the Angles.

As the hypoth. AB	2.3430
Is to radius	10.0000
So is the perp. AC	2.0082
	12.0082
	2.3430
To sine of angle B $27^\circ 33'$	9.6652
Hence, A is $62^\circ 27'$.	

To find the side BC.

As rad.	10.0000
Is to hypoth. AB	2.3430
So is sin. A	9.9478
	12.2908
	10.0000
To BC 195.4	2.2908

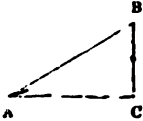
Now the method proposed is more natural than this last ; because, when the two sides are taken together, their trigonometrical relation to each other is immediately perceived, which, when they are separated, is not so apparent. Again, since the term sine, or cosine, is determined altogether by that side which we make radius, these terms should, according to the natural progress of ideas, *immediately follow* the term radius. The method followed is also shorter and more elegant. Moreover, the method just quoted, not being employed in

Case II. Given the angles and one leg, to find the hypotenuse and the other leg.

Ex. C is 90° . Angle A is $30^\circ 14'$, hence B is $59^\circ 46'$. BC is 171. Find AB and AC.

To find AB.

Take the two sides, AB, BC make AB the hypotenuse) radius; then, No. 163.



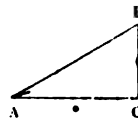
$$AB : BC :: \text{rad.} : \sin. A;$$

In which AB, an *extreme* term, is required. Hence, by No. 166 (2), we have to add the logs. of BC and rad., and subtract the log. of $\sin. A$.*

BC 171	log. + 10, 12'2330	
A $30^\circ 14'$	log. sine $\frac{-9'7020}{2'5310}$	
AB = 339'6		

To find AC.

Take two sides, AC, CB, make AC radius; then, by No. 163 (3).



$$AC : CB :: \text{rad.} : \tan. A,$$

in which AC, an *extreme* term, is required. Hence, by No. 166 (2).

CB 171	log. + 10, 12'2330	
A $30^\circ 14'$	log. tan. $\frac{-9'7655}{2'4675}$	
AC = 293'4		

This might, like Case I., be worked differently. Thus, to find AB, we may make BC radius; then $AB : BC :: \text{rad.} : \cos. B$. Again, to find AC; making BC radius, we have $AC : CB :: \text{rad.} : \tan. B$.

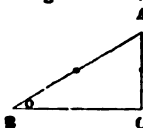
We might also, having found one of the unknown quantities, employ this quantity as a means of finding the rest; but in general it is better, when practicable, to depend only on the original quantities given.

Case III. Given the hypotenuse and one leg, to find the angles and the other leg.

Ex. Angle C is 50° , BA = 220'3, AC = 101'9; find the angle B, and then BC.

To find B.

Taking the two given sides, we have



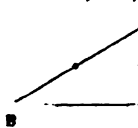
$$BA : AC :: \text{rad.} : \sin. B;$$

In which $\sin. B$, an *extreme* term, is required.

AC 101'9	log. + 10, 12'0082	
BA 220'3	log. $\frac{-2'3430}{9'6652}$	
B = $27^\circ 33'$		
Hence A = $62^\circ 17'$		

To find BC.

Taking the two sides, BC, CA, we have



$$BC : CA :: \text{rad.} : \tan. B;$$

in which BC, an *extreme* term, is required.

CA 101'9	log. + 10, 12'0082	
B $27^\circ 33'$	log. tan. $\frac{-9'7174}{2'2978}$	
BC = 195'4		
(Here, in computing by the canons, we are obliged to employ B, as found.)		

say any other scientific process, every seaman who may require to extend his scientific knowledge of these subjects will have to unlearn it and to adopt the other. The rules laid down above will be found, after very little practice, simpler and more intelligible, and therefore easier to recollect, than those of the old method.

* Instead of *subtracting* the log. sine, cosine, and tangent, it is the same thing to add the log. cosecant, secant, and cotangent, because these last are the arithmetical complements to the first. We have omitted this in the examples, to avoid confusing the learner.

Case IV. Given the two legs, to find the hypotenuse and the angles.

Ex. The angle C (fig. in Case III., only marking BC as given instead of BA) is 90° . $BC = 195.4$, $CA = 101.9$; find BA and the angle A.

To find angle A.

$$AC : BC :: \text{rad.} : \tan. A.$$

Hence, by No. 166 (2),

$$\begin{array}{rcl} BC & 195.4 & \log. + 10, 12.2909 \\ AC & 101.9 & \log. - 2.0082 \\ \hline A & = 62^\circ 27' & \log. \tan. 10.2827 \\ \text{and } B & = 27^\circ 33' & \end{array}$$

To find BA.

Making BC radius, BA will become the secant of B; hence,

$$BC : BA :: \text{rad.} : \sec. B.$$

Hence, by No. 166 (1),

$$\begin{array}{rcl} BC & 195.4 & \log. 2.2909 \\ B & 27^\circ 33' & \log. \sec. 10.0523 \\ \hline BA & = 220.3 & \log. 2.3431 \\ \text{As 10 is to be subtracted it is omitted in} & & \text{the index 12.} \end{array}$$

Ex. 1. The hypotenuse AC is 144, the angle A $39^\circ 22'$, whence C is $50^\circ 38'$, required AB and BC.

Ans. AB is 111.3, and BC 91.3.

Ex. 2. The hypoth. AC 250, the angle C $= 35^\circ 30'$; find CB and AB.

Ans. CB = 203.5, AB = 145.2.

Ex. 3. The perp. BC = 360, the angle A opposite $58^\circ 20'$; required the base and hypotenuse AC.

Ans. AB = 222, AC = 423.

Ex. 4. Given the base AB 208, and angle A $35^\circ 16'$; find the hypoth. AC and the perpendicular BC.

Ans. AC = 254.8, BC = 147.1.

Ex. 5. Given the hypoth. AC 272, and base AB 232, to find the angles A and C, and BC.

Ans. A = $31^\circ 28'$, C = $58^\circ 32'$, BC = 142.

Ex. 6. Given the hypoth. CA 980, and base BC 720, required the angles and remaining leg.

Ans. A $47^\circ 17'$, C $42^\circ 43'$, AB 664.8.

VI. METHODS OF SOLUTION.*

167. The solution of a question in which the result is required in numbers is obtained in three ways, namely, 1. Inspection; 2. Calculation or Computation; 3. Construction.

(1.) Inspection usually implies taking out, ready calculated, from a table, the result corresponding to the elements of the particular question proposed. The term has, however, a more general acceptance, being applied to the taking out, not merely of the result itself, but of quantities which compose it.

This method being easy and expeditious, is the best for general practice when precision is not required; but as the tables adapted to this kind of solution are necessarily limited, it is, on many occasions, not sufficient.

(2.) The general term Computation may be applied to every mode of solution by the composition of numbers only. Since, however, Inspection includes the simplest cases of this kind, namely, those in which either the required quantity itself, or the parts com-

* The matter in this section is, from its nature, adapted only to the reader who has made some progress in the subject.

THE SOLUTION OF OBLIQUE-ANGLED PLANE TRIANGLES.

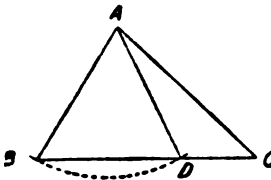
Case I. In any oblique-angled plane triangle, given two sides and an angle opposite to one of them, or two angles and a side opposite to one of them, the remaining angles and sides are found by the following simple proportions:—

As one of the given sides : sin. of its opposite angle
 \therefore the other given side : sin. of its opposite angle.

To find an angle, begin with a side opposite to a known angle.

Again, as sin. of one of the given angles : its opposite side
 \therefore sin. of the other given angle : its opposite side.

To find a side, begin with an angle opposite to a known side.



Ex. 1. In the triangle ABC , given $ACB\ 41^{\circ}\ 13'$, $AC\ 282$ yards, and $AB\ 210$ yards, to find the rest.

Now $AB\ 210$ being less than $AC\ 282$, the case is ambiguous, and there are two solutions.

At point C in the line BC make angle $BCA = 41^{\circ}\ 13'$, from C lay off $CA = 282$, and from A lay off $AB = 210$, cutting BC in B and D , join AD .

To find ABC and ADC .

As $AB\ 210$	log. 7.677781^*
$\therefore ACB\ 41^{\circ}\ 13'$	log. sin. 9.818825
$\therefore AC\ 282$	log. 2.450249
$\therefore ABC\ 62^{\circ}\ 14'$	log. sin. 9.946855

$$ABC = ADB, \therefore ADB = 62^{\circ}\ 14' - 180 = ADC\ 117^{\circ}\ 46'$$

$$ADC = 117^{\circ}\ 46' + ACB = 41^{\circ}\ 13' = 158^{\circ}\ 59' - 180 = DAC\ 21^{\circ}\ 1'$$

$$ACB = 41^{\circ}\ 13' + ABC = 62^{\circ}\ 14' = 103^{\circ}\ 27' - 180 = BAC\ 76^{\circ}\ 33'$$

To find BC .

As $ACB\ 41^{\circ}\ 13'$	log. cosec. 0.181175^*
$\therefore AB\ 210$	log. 2.322219
$\therefore BAC\ 76^{\circ}\ 33'$	log. sin. 9.987922
$\therefore BC\ 310'$	log. 2.491316

To find DC .

As $ACB\ 41^{\circ}\ 13'$	log. cosec. 0.181175^*
$\therefore AB\ 210$	log. 2.322219
$\therefore DAC\ 21^{\circ}\ 1'$	log. sin. 9.554658
$\therefore DC\ 114'$	log. 2.058052

* See note to p. 49 on the "Arithmetical Complement."

Case II. In any oblique-angled plane triangle, given two sides and the included angle, to find the rest.

As the sum of the given sides : their difference
 $\therefore \tan. \frac{1}{2}$ sum of the unknown angles : $\tan. \frac{1}{2}$ their difference.

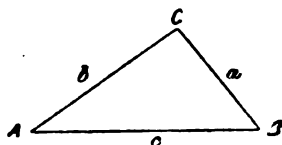
The $\frac{1}{2}$ difference being added to $\frac{1}{2}$ sum will give the greater angle, and being subtracted from it will give the less.

The greater angles will be opposite the greater side.

Ex. 2. In the triangle ABC, given $a = 512$ yards, $c = 907$ yards, and $B 49^\circ 10'$, to find the rest.

$$c 907 + a 512 = c + a 1419, \quad c 907 - a 512 = c - a 395,$$

$$B 49^\circ 10' - 180 = A + C 130^\circ 50' + 2 = \frac{A + C}{2} 65^\circ 25'.$$



To find A and C.

As $a + c 1419$	log. 6.848018*
: $a - c 395$	log. 2.596597
$\therefore \frac{A + C}{2} 65^\circ 25'$	log. tan. 10.339642
<hr/>	
: $\frac{A - C}{2} 31^\circ 19'$	log. tan. 9.784257

To find b.

As $A 34^\circ 6'$	log. cosec. 0.251345*
: $a 512$	log. 2.709270.
$\therefore B 49^\circ 10'$	log. sin. 9.878875
<hr/>	
: b 691	log. 2.839490

$$\frac{A + C}{2} 65^\circ 25' + \frac{A - C}{2} 31^\circ 19' = C 96^\circ 44', \text{ and } 65^\circ 25' - 31^\circ 19' = A 34^\circ 6'.$$

Case III. In any oblique-angled plane triangle, given the three sides, to find the angles.

From the half sum of the three given sides (S) subtract the two sides containing a required angle. To the logs. of these numbers add the arithmetical complement of the logs. of the sides; the sum of these 4 logs., rejecting 10 from the index, will be the log. sin. square, Table 69, of the required angle.

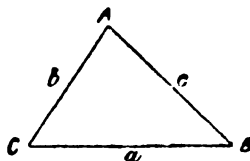
Ex. 3. In the triangle ABC, given $a = 6$, $b = 5$, and $c = 4$, to find the rest.

$$a + b + c = 6 + 5 + 4 = 15 + 2 = 7.5(S), \quad S 7.5 - b 5 = 2.5, \quad S 7.5 - c 4 = 3.5.$$

To find A.

$S - b 2.5$	log. 0.397940
$S - c 3.5$	log. 0.544068
$b 5$	Ar. Co. log. 9.301030
$c 4$	Ar. Co. log. 9.397940

$$A 82^\circ 49' \text{ log. sin. square } 9.640978$$



* See note to p. 49 on the "Arithmetical Complement."

posing it, are taken from tables, the term Computation will be employed in other cases, and always when precision is required and logarithms are concerned.*

(3.) Construction implies (in our present subject) drawing a figure of the actual case on a convenient scale, and in the proper proportions, the number of parts contained in the quantity required to be measured being taken from a scale adapted to the purpose.

This process is tedious, and not, in general, capable of much precision, but it is the most readily intelligible of the three methods, and is, therefore, the least open to mistake. The seaman should, accordingly, be able to produce a figure of every case that admits one, and should acquire the habit of referring to the figure, in the mind as the only real security against mistakes in his work.

The figure or natural representation of the case is, moreover, the foundation of the mathematical treatment of the question.

1. *Limits of Methods or Observations.*

168. In every process of calculation, the elements which enter into it, and which are either observed at the time by instruments, or taken from tables, are liable to error. Every result, therefore, is, to some extent, uncertain; but the *amount* of error of the final result

* Solutions of this kind are usually divided into "rigorous" and "approximate," or indirect, as the latter are also called. In all solutions, however, we either deal directly with the quantities themselves, as arcs, angles, &c., in their entire or *integral* state, or we compute a *difference* from a certain value assumed or given, and thence find the required quantity. This last process is indirect, but the former may be effected indirectly also. The terms Integral and Differential would then, it is presumed, be more satisfactory, for the degree of approximation obtained is altogether beside the question of the character of the solution. We do not, however, on the present occasion, depart from the usual terms. We shall merely add, as some indistinctness prevails as to the properties of these different solutions, that both are equally affected by errors of observation (as must of course follow, if they be both true), and thus the essential distinction between them, in practice, lies in the different numbers of figures which they respectively require.

There is another point on which we shall take the opportunity to make some remarks for the satisfaction of the scientific reader. In the present subject we are obliged, in most cases, to consider the required quantity, though really unknown, as if it were given, as it is an indispensable argument in reducing the elements;—thus, in finding the longitude by chronometer, by the sun, we must assume a longitude in order to deduce the declination and equation of time. Such solutions are, therefore, *solutions by assumption*, and the question naturally arises, What is the criterion by which to know whether the result is nearer the truth or further from it than the temporary value employed?

In general we have to solve, not the equation $u = f(x, y, z)$, but $u_1 = f(x, y, z, u)$, in which u is an assumed value of u , and u_1 a first approximation. The second approximation is $u_2 = f(x, y, z, u_1)$, and so on. Now, it is evident, without examining the successive differences $u - u_1, u_1 - u_2, \dots$ that the process is convergent, if u varies more slowly than u' , that is, when $\frac{du}{du'} < 1$. This is the case with all our problems within the limits assigned. When $\frac{du}{du'} > 1$, the process is divergent, or the results are worse and worse; and when $= 1$, the assumption is reproduced. Again, when $\frac{du}{du'}$ is positive, the results are all greater or all less than the truth; when negative, they are alternately too great, and too small. Hence, in general, it depends on the *data*, and not on the greatness or smallness of the error of assumption, whether the process converge or not. The above, however, applies, in strictness, only to small errors of assumption; for large errors higher terms must be considered.

caused by an error in any one of the *data* (or quantities given for the solution of the question) is very different under different circumstances, being in some cases scarcely perceptible, while in others it may far exceed the very error to which it is due.

If we agree beforehand that a probable error of observation shall not cause an error beyond a certain amount in the result, we must exclude all those cases in which it would produce a greater effect, and we thus assign *limits* to the method or observation.

169. Generally speaking, every element that enters into the computation is liable to error, and, therefore, each element will have its own independent influence in limiting the observation; that is, in strictness, there will be *different limits* for each separate element, but, for practical purposes, it is enough to assign the limits according to that element of which the error is most important. For instance, in finding the time by a single altitude of a celestial body, we employ its altitude and declination, and the latitude of the place. Now the latitude will often, and the declination sometimes, be correctly known, but the altitude can never, from various causes, be exempt from suspicion of inaccuracy; besides, in general, an error of altitude produces a greater effect on the result than an equal error in latitude or declination. Hence we limit the method of "time by an altitude off the meridian" in respect of altitude only; and assuming that 1' error of altitude shall not cause more than 10" error in the time, we limit, for the more frequented latitudes, the celestial body to a certain bearing.

2. Degree of Dependence.

170. The result of every computation is, as above remarked, No. 168, more or less uncertain. If we knew the error in one of the elements, we could easily find the effect it would produce on the result, by working the computation over again; and if, under the circumstances, such error in the data is not likely to exceed a certain quantity, we should thus find the *limit of probable error*;* for example, suppose in finding the time, the error of altitude is not likely to exceed 2', and that the effect of this in working over again is 9", we say that 9" is the limit of probable error.

171. Since all the elements are more or less uncertain, there is a limit of probable error or degree of dependence in respect of each. Hence the extreme probable error of the result is the sum of all these errors, supposing they lie on the same side. But, in practice, they will, in general, tend to neutralise each other, and it is enough to estimate the degree of dependence in respect of the most important of them.

172. In some cases a small error of observation will produce a very great error in the result; in others, a large error may not pro-

* The term "Degree of Dependence" is preferred here to "limit of probable error," because it describes in direct terms the application or use of that limit, which is, to point out how near the result may be depended upon.

duce a sensible effect. For example, an error of $1'$ in the lunar distance, causes an error of $30'$ or $40'$ in the longitude, while an error of several miles of latitude may not, in certain cases, produce an error worth notice in the time as found by an observation. As nicety in the mere working of the computation can, in any way, meet or counteract errors of observation, it is necessary, in forming a true judgment of the place of the ship, to try the effects of probable errors; in other words, to try the degree of dependance. Thus, in the example of the lunar alluded to above, a novice might conclude that his longitude was, to the exact minute and second, that found by computation; but a more experienced computer, knowing that all his elements are not absolutely correct, and that his result can scarcely be perfectly exact but by an accidental compensation of errors, makes an allowance for error; and assuming that the distance may be too much or too little by $30''$, for example, considers the observation as merely having established with certainty the ship's place within $15'E.$ or $W.$ of the position deduced.

173. But the degree of dependance, besides being indispensable to rightly judging of the true place of the ship, or, rather, of the space on latitude and longitude within which she is to be found, has another important application, as it governs the amount of labour bestowed on the computations. For example, if the latitude is uncertain several miles, it is at once evident, that to proceed with as much care and precision as if it were ascertained to a few seconds, is mere waste of time. Similar remarks have already been offered in the Preface, and they are particularly directed to the student's attention, who should be early impressed with the importance of improving his judgment by continual exercise, instead of trusting on all occasions to a mechanical routine of computation.

174. It is worth while to notice, that in working to a certain degree of accuracy, as, for example, to minutes, it is generally enough to employ the nearest whole minute; but when one of the quantities varies very rapidly, it may be proper to work closer; for it is easy to see that the inaccuracy of half a minute in a quantity which is multiplied by a number greater than 1, is increased, and appears as a whole minute.

[1.] *Personal Error.*

175. The several errors to which each observation is exposed, and which accordingly enter into the estimation of the degree of dependance, are described in their proper places; but there is one which, though sensible only in cases where a considerable step has been made towards precision, is of universal application, and is, therefore, properly noticed here.

It is found that different persons do not agree in the precise instant of observing the same phenomenon. Again, some persons are in the habit of observing more or less closely than others. The kind of error which is obviously present in such cases, is called the *personal error*, or *equation*.

Two observers have been found to differ $0^{\circ}.4$ in the sun's transit over the wire of a telescope.

176. When two images, in contact, lie stationary before two observers, it is difficult to understand why one of them should see them overlap, or the other open, or why they should not agree in the measure. But when the images are in motion, the observer's anxiety is roused lest he may miss the observation, and the excitement may lead him to think that he sees the contact before it really takes place. Hence there is reason to believe that the personal equation is, in some degree, a matter of temperament.

It also seems well ascertained that the personal equation is not the same for the same individual at all times, and that it is greatly influenced by fatigue, by the effort of observing, and, in fact, by every cause that affects the nervous system. It may, therefore, be advantageous to bear these circumstances in mind preparatory to undertaking observations in which much accuracy is required.

177. The existence of this error shews that when much precision is required, observations taken by different persons should not be mixed together until cleared of personal errors, since they may at the outset be presumed to be affected by unequal errors; and it is probable that many discrepancies are due to this cause, in observations whether by the same or different observers.

SPHERICS, DEFINITIONS AND PRINCIPLES

SPHERICS is that part of mathematics which treats of the positions and magnitudes of arcs of circles described on the surface of a sphere.

A **SPHERE** is a solid formed by the revolution of a semicircle about its diameter; this diameter is immovable during the motion of the semicircle.

THE **CENTRE AND AXIS** of a sphere are the same as the centre and diameter of the generating semicircle, and as a circle has an indefinite number of diameters, so a sphere may be considered to have an indefinite number of axes, round any one of which it may be conceived to be generated.

EVERY **SECTION** of a **SPHERE** made by a plane passing through its circumference is a circle.

A **GREAT CIRCLE** is formed by a plane passing through the centre of the sphere. A **SMALL CIRCLE** is formed by a plane that does not pass through the centre of the sphere. A sphere is therefore divided into two equal parts by the plane of every great circle, and into two unequal parts by the plane of every small circle.

THE **POLES** OF A **CIRCLE** of a sphere are those points on the surface of the sphere which are equally distant from the circumference of that circle. Thus the poles of a circle are the extremities of that diameter or axis of the sphere which is perpendicular to the plane of that circle. All points in the circumference of a great circle are equally distant from *both* its poles.

SMALL CIRCLES of the sphere are those circles which are unequally distant from both their poles.

THE **POLES** of every great circle are each 90° distant from that great circle on the surface of the sphere, and no two great circles can have the same poles.

THE **DIAMETER** of every great circle passes through the centre of the sphere, but the diameters of small circles do not pass through the centre. Thus the centre of the sphere is the common centre of all its great circles.

PARALLEL CIRCLES of a sphere are those small circles the planes of which are parallel to the plane of some great circle. All parallel circles have the same poles, and may be conceived to be concentric to the great circle they are parallel to.

A SPHERICAL ANGLE is the inclination of two great circles of the sphere meeting one another. It is measured by an arc of a great circle intercepted between the legs of that angle, 90° distant from the angular point.

A SPHERICAL TRIANGLE is a figure formed on the surface of the sphere by the intersection of three great circles.

THE SHORTEST DISTANCE between two points on the surface of a sphere is an arc of the great circle passing through those points.

THE STEREOGRAPHIC PROJECTION* of the sphere is such a representation of its circles upon the plane of some great circle, and thence called the plane of projection, as would appear to an eye placed in one of the poles of that circle, and thence viewing the circles of the sphere.

The place of the eye is called the projecting point or lower pole, and the pole opposite is called the opposite or exterior pole; also the projection of any point on the sphere is that point in the plane of projection through which the visual ray passes to the eye.

THE PRIMITIVE CIRCLE is that great circle on the plane of which the representation of all other circles is supposed to be drawn.

A RIGHT CIRCLE is one which is perpendicular to the plane of the primitive circle, and, if it be a great circle, its plane passes through the eye and it is seen edgewise, consequently it is represented by a straight line drawn through the centre of the primitive circle.

AN OBLIQUE CIRCLE is that which has its plane oblique to the eye, and is represented by a curved line.

SPHERICAL TRIGONOMETRY is the art of computing the measures of the sides and angles of such triangles as are formed on the surface of a sphere, by the mutual intersection of three great circles described thereon.

A SPHERICAL TRIANGLE has three sides and three angles.

A RIGHT-ANGLED SPHERICAL TRIANGLE has one right angle. The sides about the right angle are called legs; the side opposite the right angle is called the hypotenuse.

A QUADRANTAL SPHERICAL TRIANGLE has one side equal to 90° .

AN OBLIQUE SPHERICAL TRIANGLE has all its angles oblique.

THE CIRCULAR PARTS of a triangle are those arcs which measure its sides and angles.

Two spherical triangles are said to be *supplemental* to one another when the sides and angles of the one are supplemental of the sides and angles of the other, and one in regard to the other is called the supplemental triangle.

Two arcs or angles when compared together are said to be *alike* when both are less or greater than 90° . But when one is greater and the other less than 90° , they are said to be *unlike*.

In every spherical triangle equal angles are opposite equal sides, and equal sides are opposite equal angles.

* Stereographic means representing a solid on a plane surface.

Any two sides of a spherical triangle are together greater than the third side.

Each side of a spherical triangle is less than a semicircle or 180° .

In every spherical triangle the greater side is opposite the greater angle. The sum of the three sides of a spherical triangle is less than 360° .

The sum of the three angles of a spherical triangle is greater than two right angles and less than six, or always will fall between 180° and 540° .

In right-angled spherical triangles, the oblique angles and their opposite sides are of *like affection*; that is, if a leg is less or greater than 90° , its opposite angle is also less or greater than 90° .

In right-angled spherical triangles the hypotenuse is *less than* 90° when the legs are of a *like kind*; but *greater than* 90° when the legs are of a *different kind*.

In any spherical triangle

As sine of either angle : sine of its opposite side
 \therefore sine of another angle : sine of its opposite side,

RIGHT SPHERICAL.

The celebrated Lord Napier, inventor of logarithms, contrived a general rule, easy to be remembered, by which the solution of every case of right-angled spherical triangles is readily obtained.

In any right-angled spherical triangle there are five parts beside the right angle—viz., two legs, two angles, and the hypotenuse. The two legs, the complements of the two angles, and the complement of the hypotenuse are called circular parts.

In any case relating to right-angled spherical triangles three of these circular parts are concerned—viz., two given and one sought.

If the three concerned are all joined together, ignoring the right angle, the central one is called the middle, and the other two adjacent parts.

But if only two are joined together these are called the opposite, and the other the middle part.

These being known, all the cases of right-angled spherical triangles may be solved by Napier's rules.

1. The product of radius and sine of the middle part = the product of the tangents of the adjacent parts.

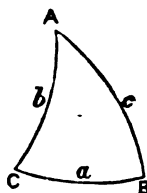
2. The product of radius and sine of the middle part = the product of the cosines of the opposite parts.

N.B.—As an aid to memory the letter *a* occurs in tangent and adjacent; and the letter *o* in cosine and opposite. In the following examples, instead of *subtracting* the log. sine, cosine, and tangent, it is the same thing to *add* the log. cosec., sec., and cot.; because these last are the arithmetical complements of the first (*see note, p. 49*).

Ex. 1. In the right-angled spherical triangle $A B C$, given $C 61^{\circ} 50'$, $B C (a) 40^{\circ} 30'$, $B 90^{\circ}$, to find the other parts.

To find A .

$$\begin{array}{l} \text{Rad. cos. } A = \sin. C . \cos. a \\ \cos. A = \sin. C . \cos. a \\ C = 61^{\circ} 50' \quad \log. \sin. 9.945261 \\ a = 40^{\circ} 30' \quad \log. \cos. 9.881046 \\ A = 47^{\circ} 54' \quad \log. \cos. 9.826307 \end{array}$$



To find $A C (b)$.

$$\begin{array}{l} \text{Rad. cos. } C = \cot. b . \tan. a \\ \cot. b = \cos. C . \cot. a \\ a = 40^{\circ} 30' \quad \log. \cot. 0.068501 \\ C = 61^{\circ} 50' \quad \log. \cos. 9.673977 \\ b = 61^{\circ} 4' \quad \log. \cot. 9.742478 \end{array}$$

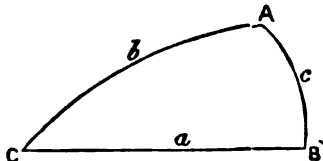
To find $A B (c)$.

$$\begin{array}{l} \text{Rad. cos. } b = \cos. a . \cos. c \\ \cos. c = \sec. a . \cos. b \\ a = 40^{\circ} 30' \quad \log. \sec. 0.118955 \\ b = 61^{\circ} 4' \quad \log. \cos. 9.684658 \\ c = 50^{\circ} 29' \quad \log. \cos. 9.803613 \end{array}$$

Ex. 2. In the right-angled spherical triangle $A B C$, given $A B (c) 50^{\circ} 40'$, $A C (b) 113^{\circ} 26'$, $B 90^{\circ}$, to find the other parts.

To find C .

$$\begin{array}{l} \text{Rad. sin. } c = \sin. b . \sin. C \\ \sin. C = \sin. c . \operatorname{cosec}. b \\ b = 113^{\circ} 26' \quad \log. \operatorname{cosec}. 0.037383 \\ c = 50^{\circ} 40' \quad \log. \sin. 9.888444 \\ C = 57^{\circ} 28' \quad \log. \sin. 9.925827 \end{array}$$



To find $B C (a)$.

$$\begin{array}{l} \text{Rad. cos. } b = \cos. c . \cos. a \\ \cos. a = \cos. b \sec. c \\ c = 50^{\circ} 40' \quad \log. \sec. 0.198027 \\ b = 113^{\circ} 26' \quad \log. \cos. 9.599536 \\ \quad 51^{\circ} 8' \quad \log. \cos. 9.797563 \\ \quad 180^{\circ} 0' \\ a = 128^{\circ} 52' \end{array}$$

To find A .

$$\begin{array}{l} \text{Rad. cos. } A = \tan. c . \cot. b \\ \cos. A = \tan. c . \cot. b \\ c = 50^{\circ} 40' \quad \log. \tan. 0.084711 \\ b = 113^{\circ} 26' \quad \log. \cot. 9.636918 \\ \quad 58^{\circ} 4' \quad \log. \cos. 9.723389 \\ \quad 180^{\circ} 00' \\ A = 121^{\circ} 56' \end{array}$$

NOTE.—In the triangle $A B C$, b the hypotenuse being greater than 90° , and c less than 90° , A is of unlike affection to C , or greater than 90° . Also A being greater than 90° its opposite side a must also be greater than 90° .

Quadrantal spherical triangles are also solved by Napier's rules reversed: using the quadrantal side as the right angle, the angles adjacent to it, the complements of the other two sides, and of the angle opposite to the quadrantal side, as circular parts.

OBLIQUE SPHERICS.

Case I. Given two sides and an angle opposite to one of them, to find the angle opposite to the known side.

$$\begin{array}{l} \text{As sin. of a given side : sin. of its opposite angle} \\ \therefore \text{sin. of the other given side : sin. of its opposite angle.} \end{array}$$

To find the 3rd side.

$$\begin{array}{l} \text{As sin. } \frac{1}{2} \text{ diff. of the two known angles} \\ \quad : \sin. \frac{1}{2} \text{ their sum} \\ \therefore \tan. \frac{1}{2} \text{ diff. of the two known sides} \\ \quad : \tan. \frac{1}{2} \text{ the third side.} \end{array} \quad \begin{array}{l} \text{Or, as cos. } \frac{1}{2} \text{ diff. of the two known angles} \\ \quad : \cos. \frac{1}{2} \text{ their sum} \\ \therefore \tan. \frac{1}{2} \text{ sum of the two known sides} \\ \quad : \tan. \frac{1}{2} \text{ the third side.} \end{array}$$

Case II. Given two angles and a side opposite to one of them, to find the side opposite to the known angle.

As $\sin.$ of a given angle : $\sin.$ of its opposite side
 :: $\sin.$ of the other given angle : $\sin.$ of its opposite side.

To find the 3rd angle.

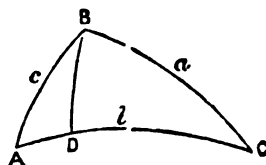
As $\sin.$ $\frac{1}{2}$ diff. of the two known sides : $\sin.$ $\frac{1}{2}$ their sum :: $\tan.$ $\frac{1}{2}$ diff. of the two known angles : $\cot.$ $\frac{1}{2}$ the third angle.	Or, as $\cos.$ $\frac{1}{2}$ diff. of the two known sides : $\cos.$ $\frac{1}{2}$ their sum :: $\tan.$ $\frac{1}{2}$ sum of the two known angles : $\cot.$ $\frac{1}{2}$ the third angle.
--	--

Cases I. and II. may also be solved by drawing a great circle from the unknown angle perpendicular to the opposite side. This divides the triangle into two right-angled triangles. The segments of the divided side may then be found by right-angled spherics.

In the spherical triangle ABC , given A $84^\circ 52'$, BC or (a) $67^\circ 5'$, and AB or (c) $55^\circ 38'$,

To find the other parts.

As $\sin. a$: $\sin. A$:: $\sin. c$: $\sin. C$.	
$a = 67^\circ 5'$	$\log. \operatorname{cosec}. 0.035706$
$A = 84^\circ 52'$	$\log. \sin. 9.998255$
$c = 55^\circ 38'$	$\log. \sin. 9.916687$
$C = 63^\circ 12'$	$\log. \sin. 9.950548$



From B draw a great circle BD perpendicular to AC . Angles A and C being of like affection, both less than 90° , BD falls within the triangle. Then by Napier's rules:

To find AC (b).

Rad. $\cos. C = \cot. a \cdot \tan. DC$ $\tan. DC = \cos. C \cdot \tan. a$	Rad. $\cos. A = \cot. c \cdot \tan. AD$ $\tan. AD = \cos. A \cdot \tan. c$
$a = 67^\circ 5'$ $\log. \tan. 0.373907$	$c = 55^\circ 38'$ $\log. \tan. 0.165033$
$C = 63^\circ 12'$ $\log. \cos. 9.654059$	$A = 84^\circ 52'$ $\log. \cos. 8.951696$
$DC = 46^\circ 51'$ $\log. \tan. 10.027966$	$AD = 7^\circ 27'$ $\log. \tan. 9.116729$
$AD = 7^\circ 27'$	
$b = 54^\circ 18'$	

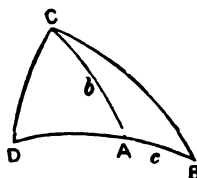
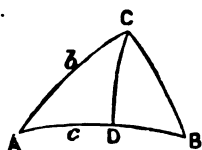
To find B .

As $\sin. a$: $\sin. A$:: $\sin. b$: $\sin. B$.	
$a = 67^\circ 5'$ $\log. \operatorname{cosec}. 0.035706$	
$A = 84^\circ 52'$ $\log. \sin. 9.998255$	
$b = 54^\circ 18'$ $\log. \sin. 9.909601$	
$B = 61^\circ 25'$ $\log. \sin. 9.943562$	

If A and C are of unlike affection—i.e. one greater and one less than 90° —the perpendicular will fall without the triangle, and the difference between AD and DC must be taken to find b .

This also will solve Case II., given two angles and a side opposite to one of them, to find the other parts

Case III. Given two sides and the included angle.



Let A , B , AC and the included angle A be given. From one of the unknown angles at C draw a great circle perpendicular to the opposite side. Then in the right-angled triangle ADC find AD . If the perpendicular falls within the triangle subtract AD from AB to find DB , and if the perpendicular falls without the triangle add AD to AB , and the sum is B .

To find BC .

$$\text{As } \cos. \text{ of } AD : \cos. \text{ of } BD :: \cos. \text{ of } AC : \cos. \text{ of } BC.$$

To find the unknown angles.

$$\text{As } \sin. \text{ of side just found} : \sin. \text{ of the given angle}$$

$$:: \sin. \text{ of either of the given sides} : \sin. \text{ of its opposite angle.}$$

Second Method.

To find $\frac{1}{2}$ sum of the unknown angles.

$$\text{As } \cos. \frac{1}{2} \text{ sum of the two given sides} : \cos. \frac{1}{2} \text{ their diff.}$$

$$:: \cot. \frac{1}{2} \text{ the included angle} : \tan. \frac{1}{2} \text{ sum of unknown angles.}$$

NOTE.—This $\frac{1}{2}$ sum of the unknown angles is of the same name as the $\frac{1}{2}$ sum of the sides.

To find $\frac{1}{2}$ diff. of the unknown angles.

$$\text{As } \sin. \frac{1}{2} \text{ sum of the two given sides} : \sin. \frac{1}{2} \text{ their diff.}$$

$$:: \cot. \frac{1}{2} \text{ the included angle} : \tan. \frac{1}{2} \text{ diff. of the unknown angles.}$$

The $\frac{1}{2}$ diff. being added to the $\frac{1}{2}$ sum will be the greater angle, and being subtracted from it will be the less.

In the spherical triangle ABC , given B $125^\circ 36'$, BC (a) $81^\circ 17'$, and, AB (c) $59^\circ 13'$, to find the other parts:

$$\begin{array}{rcl} a = 59^\circ 13' & a = 81^\circ 17' & B = \frac{125 \ 36}{62 \ 48} B \\ a = 81 \ 17 & c = 59 \ 13 & \\ \frac{140 \ 30}{70 \ 15} \frac{a+c}{2} & \frac{22 \ 4}{11 \ 2} \frac{a-c}{2} & \end{array}$$

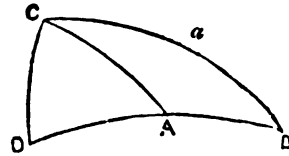
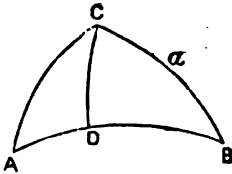
To find angles C and A .

$\frac{a+c}{2} = 70^\circ 15'$	log. sec. 0.471190	$\frac{a+c}{2} = 70^\circ 15'$	log. cosec. 0.026329
$\frac{a-c}{2} = 11 \ 2$	log. cos. 9.991897	$\frac{a-c}{2} = 11 \ 2$	log. sin. 9.281897
$\frac{B}{2} = 62 \ 48$	log. cot. 9.710904	$\frac{B}{2} = 62 \ 48$	log. cot. 9.710904
$\frac{A+C}{2} = 56 \ 11$	log. tan. 10.173991	$\frac{A-C}{2} = 5 \ 58$	log. tan. 9.019.30
$\frac{A-C}{2} = \frac{5 \ 58}{50 \ 13} C$		$\frac{A+C}{2} = \frac{56 \ 11}{62 \ 9} A$	

To find side b .

$$\begin{array}{rcl} C = 50^\circ 13' & \log. \text{ cosec.} & 0.114373 \\ c = 59 \ 13 & \log. \sin. & 9.934048 \\ B = 125 \ 36 & \log. \sin. & 9.910144 \\ b = 114 \ 38 & \log. \sin. & 9.958555 \end{array}$$

Case IV. Given two angles and the included side.



In the triangle ABC given angles B , C , and side BC , a : to find the other parts. Where two angles and an included side are given, a great circle may be drawn from one of the given angles perpendicular to the opposite side, and the angle BCD instead of the segment BD found. The difference between BCD and the given angle C will give ACD . Then

To find the 3rd angle.

$$\text{As } \sin. BCD : \sin. ACD :: \cos. B : \cos. A.$$

If the perpendicular falls within the triangle the angles B and A are of the same name; if it falls without the triangle they are of different names.

The Second Method is the same as in Case III., only for *cots.* of half included angle use *tans.* of half included side.

Case V. Given the three sides of a spherical triangle, to find the three angles.

Find the half-sum of the three sides. Take the difference between this half-sum and the side opposite to a required angle, then add together the log. cosecs. of the two sides containing the angle, the log. sines of the half-sum, and of the difference between the half-sum and the side opposite the required angle: Half the sum of these four logs will be the log. cos. of half the required angle.

In the spherical triangle ABC , given AB (c) $79^\circ 56'$, BC (a) $119^\circ 36'$, and AC (b) $64^\circ 5'$, to find angle B .

$$\begin{array}{rcl} a = 119^\circ 36' & \log. \text{ cosec. } & .060733 \\ c = 79 \ 56 & \log. \text{ cosec. } & .006738 \\ b = 64 \ 5 & & \\ \hline s & \frac{263 \ 37}{2} & \\ & 131 \ 48 \ 30 & \log. \sin. \ 9.872377 \\ & 67 \ 43 \ 30 & \log. \sin. \ 9.966318 \\ & & \hline & & 19.906166 \\ \frac{B}{2} = 26 \ 9 \ 20 & \log. \cos. & 9.953083 \left\{ \begin{array}{l} \log. \sin. \text{ square of} \\ 127^\circ 41' 20'', \text{ supple-} \\ \text{ment } B. \end{array} \right. \\ \hline B = 52 \ 18 \ 40 & & \end{array}$$

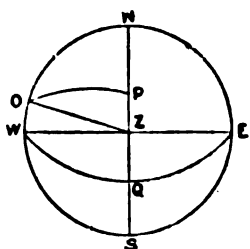
Case VI. The three angles being known, to find a side.

Add together the log. cosecs. of the two angles adjacent to the required side and the log. cosines of the half-sum of the three angles and the difference between the half-sum and the angle opposite the required side. Half-sum of these four logs. will be the log. sine of half the required side.

APPLICATION OF THE PRECEDING CASES IN SPHERICAL TRIGONOMETRY TO QUESTIONS IN NAUTICAL ASTRONOMY.

THE AMPLITUDE.

In these figures N E S W represents the horizon, S and N being its south and north points; N Z S the celestial meridian; O the place of the body observed on the horizon, O W the amplitude, P the pole of the heavens, P O the polar distance, less or greater than 90° , as the declination of the body observed is of the same or of a different name to the latitude; Z the zenith, W E the prime vertical, and W Q E the equator.



From Right Spherics, p. 57A.

In the problem to find the amplitude of a heavenly body, No. 884, there are given P N the lat. and P O the polar distance to find O W the amplitude.

Then in right-angled triangle P O N

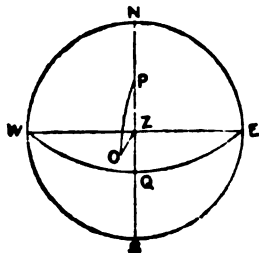
$$\begin{aligned} \text{Rad.} \times \cos. PO &= \cos. PN \cos. ON \\ \cos. ON &= \cos. PO \sec. PN, \text{ or} \end{aligned}$$

$$\begin{aligned} \text{Log. sec. PN (lat.)} + \log. \sin. \left\{ \frac{90^\circ - PO}{PO - 90^\circ} \right\} (\text{dec.}) \\ = \log. \sin. \left\{ \frac{90^\circ - ON}{ON - 90^\circ} \right\}; \end{aligned}$$

i.e. O W the amplitude.

The question can also be solved by the quadrantal triangle Z P O, where P Z O, and therefrom O W, may be found.

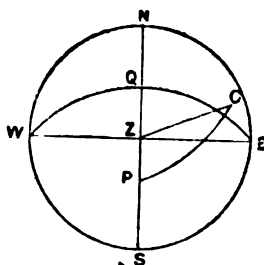
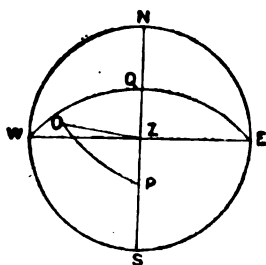
LATITUDE FROM REDUCTION TO THE MERIDIAN.



From Oblique Spherics, Case I., p. 58A.

Given Z P O the hour angle, P O the polar distance, and Z O the zenith distance, or two sides and an angle opposite to one of them, to find the remaining side P Z, or the colat. at the time of observation, see Nos. 700 to 704 and explanation of Table 70, page 427.

THE HOUR ANGLE AND AZIMUTH.



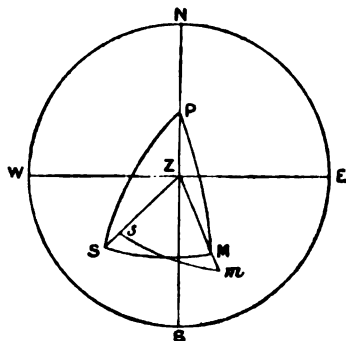
From Oblique Spherics, Case V., p. 61A.

Here are given: PZ the colat., PO the polar distance, and ZO the zenith distance, or the three sides of the triangle ZOP ; to find either ZPO the hour angle, or PZO the azimuth, *see* Nos. 614 and 674.

LUNARS.

From Oblique Spherics, Cases V. and III., pp. 61A and 60A.

The Lunar problem is fully treated upon (*see* Nos. 836 to 863). The figures of 837 show the solution by oblique spherics, where first, in the triangle sZm , three sides, the two apparent altitudes Zm and Zs , and the apparent distance ms are given, to find angle mZs ; and then in the triangle MZS , two sides, the two true altitudes ZM and ZS and the included angle Z are given, to find the true distance MS .



DOUBLE ALTITUDE.

From Oblique Spherics, Cases III. and V., pp. 60A and 61A.

For two altitudes of the same body the solution of this problem is fully given at No 757, and figure at p. 268, where right spherics

are used: *see* p. 57A. If different bodies are used, the problem is solved by oblique spherics.

Fig. 1 illustrates a double altitude where the observations are taken of the same body and right spherics are used. In this case, A and B are the places of the body in the two observations; PA, PB, the polar distances;

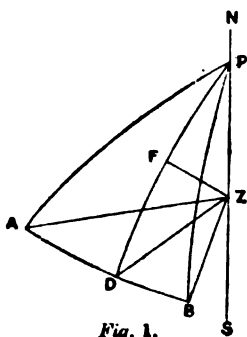


Fig. 1.

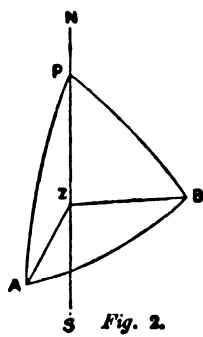


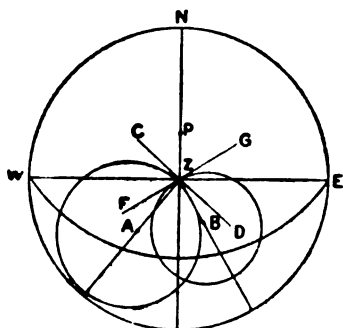
Fig. 2.

ZA , ZB the zenith distances; APB the polar angle or interval. PD is drawn perpendicular to AB , dividing APB into two equal parts; ZF is drawn perpendicular to PD .

Fig. 2 illustrates the problem where observations of two different bodies are taken, and the problem solved by oblique spherics. See No. 770, Note to pages 273, 274, and figure at page 268.

SUMNER'S METHOD.

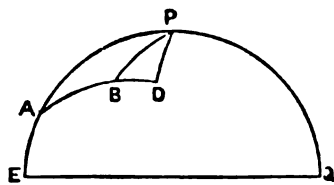
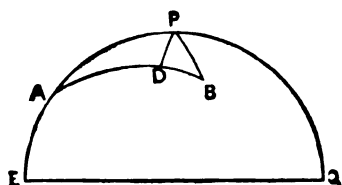
From two altitudes of the same heavenly body taken at a requisite interval apart, or two altitudes of different stars (having the requisite interval in azimuth) taken at the same time, two small circles (circles of position) may be described, the intersection of which * will be the place of the ship, allowing for her run in the interval.



In the figure A and B represent the places of the body or bodies at the time or times of observation. From these points as centres, with the zenith distances, small circles are drawn, the intersection of which will be the zenith of the observer, or place of the ship.

The intersection of these circles will be represented on the chart by the two straight lines CD and FG , drawn at right angles to ZA and ZB , the bearings of the body or bodies at the time of observation. Full explanation of this useful method, with an illustrative chart, will be found under Nos. 1009 to 1014.

GREAT CIRCLE SAILING.



From Oblique Spherics, Case III., p. 60A.

Given PA and PB the two colats. and APB the diff. long., to find AB the distance and A and B the courses from one place to the other; or given two sides PA and PB , and included angle APB , to find the other parts.

The position of the vertex D will be found from the right-angled triangles APD or BPD . This problem is fully treated upon in Nos. 336 to 347.

* A chartlet showing this intersection will be found in Lecky's Wrinkles, 9th edit. p. 502

NAVIGATION.

CHAPTER I.

DEFINITIONS.

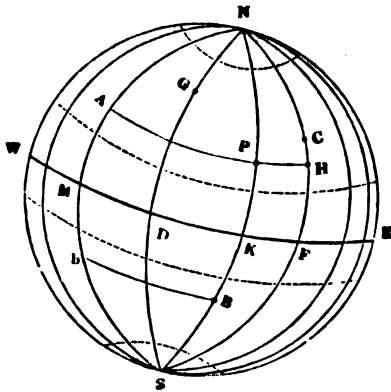
178. By the general term **NAVIGATION** is meant that science which relates to the determination of the place of a ship on the sea.

179. The place of a ship is determined by either of two methods, which are independent of each other: 1st, by referring it to some other place, as a fixed point of land, or a former place of the ship herself; 2d, by astronomical observation.

The first of these methods is treated under the head of **NAVIGATION**; the second, under that of **NAUTICAL ASTRONOMY**.

180. The earth is nearly a globe or sphere: this is proved in three ways. 1st. When a vessel is seen at a considerable distance on the sea, in any part of the world, the hull is partly or entirely concealed by the water, though the masts are visible. 2d. The shadow of the earth thrown on the moon when the earth is between the sun and the moon is, in all positions of the earth, circular. 3d. The earth has been sailed round.

The earth, however, is not exactly spherical, but of the figure called an oblate spheroid, which resembles an orange, the shortest diameter (that which joins the poles) being 7899 statute miles, and that of the fullest parts (about the equator) being nearly 26 more.



181. The earth turns once round in 24 hours. The line round which it revolves, and which is the shortest diameter, is called the **axis**, and its extremities are the **North and South POLES**, as **N, S**.

192. The EQUATOR, called also the Equinoctial Line, or vulgarly the Line, is a circle equidistant from both poles, as W M E, and dividing the globe into two half globes, or hemispheres, N W E and S W E.

At all places on this circle the sun rises at 6 A.M., and sets at 6 P.M., all the year round; the days and nights are thus equal, being 12 hours each.

183. A MERIDIAN is a semicircle joining the two poles, as N A S, N B S. Every portion of the meridian lies north and south; and places lying north and south of each other are said to be on the same meridian.

184. LATITUDE is the distance from the equator, measured on a meridian; thus the latitude of a place A is A M, the latitude of B is B K.

Latitude is named north or south, according as the place is north or south of the equator. Thus A is in north latitude, B is in south latitude.

185. The COLATITUDE is the complement of the latitude to 90° ; thus N A, S B, N C, are the colatitudes of the places A, B, C.

The colatitude reckoned from the other pole is the sum of the latitude and 90° ; thus the colatitude of A is also S A, which is $90^\circ + M A$ (the latitude of A): N B is the colatitude of B.

186. Latitude is measured in degrees, minutes, and seconds. A minute, or *nautical mile*, contains about 6082 feet, or 1013 fathoms, and therefore, a second is about 101 feet, or 17 fathoms nearly. See p. 104, note, and Spheroidal Tables, p. 724.

187. Circles parallel to the equator, that is, equidistant from it in every point, are *parallels of latitude*; as A P H, b B. Two places in the same latitude are said to lie on the same parallel.

188. The DIFFERENCE OF LATITUDE of two places is the portion of the meridian included between their parallels. Thus, A b is the difference of latitude of the two places A, B; C H is that between A and C.

The difference of latitude of the ship is, therefore, the distance she makes good in a north and south direction.

Difference of latitude is also called *Northing* and *Southing*, and is marked N. or S. It is then said to be one of these *names*.

189. It is evident, that when two places are on the *same* side of the equator, their diff. lat. is found by subtracting the lesser latitude from the greater; and that when they are on *opposite* sides of the equator, that is, when one place is in north latitude, and the other in south latitude, the *sum* of their latitudes is their diff. lat. Thus the diff. lat. of A and B, which is A b, is the sum of the north latitude A M, and the south latitude B K, or M b.

Ex. 1. Find the diff. lat. of Cape Clear and Cape Finisterre.

Cape Clear.....	$51^\circ 26' N.$
Cape Finisterre ...	$42 \quad 54 N.$
DIFF. LAT.	$8 \quad 32$

Ex. 2. Find the diff. lat. of Cape Verd and Cape St. Roque.

Cape Verd.....	$14^\circ 43' N.$
Cape St. Roque	$5 \quad 28 S.$
DIFF. LAT.	$20 \quad 11$

Ex. 3. A ship sails from lat. $50^{\circ} 19' N.$ to $48^{\circ} 12' N.$: find her diff. lat.	Ex. 4. A ship sails from lat. $1^{\circ} 11' N$ to $0^{\circ} 13' S.$: find her diff. lat
Lat. left $50^{\circ} 19' N.$	Lat. left $1^{\circ} 11' N.$
Lat. in $48^{\circ} 12' N.$	Lat. in $0^{\circ} 13' S.$
DIFF. LAT. $2^{\circ} 7'$ or 127 miles.	DIFF. LAT. $1^{\circ} 24'$ or 84 miles.

Examples for Exercise.

Required the diff. lat. between the following places :

1. Between a place A in lat. $42^{\circ} 21' N.$, and another place B in lat. $37^{\circ} 32' N.$
Ans. 289 miles.
2. Between Halifax and the Cape of Good Hope. Ans. 4716 miles.
3. Between Diego Ramirez and Cape Lopatka. Ans. 6447 miles.

190. When a ship in north latitude sails north she evidently increases her latitude; and so, likewise, when in south latitude she sails south; because, in these cases, she increases her distance from the equator, at which the latitude begins.

But if in north latitude she sails south, or in south latitude she sails north, she diminishes her latitude.

Hence, when one latitude and the diff. lat. are given, the other latitude is easily found.

Ex. 1. A ship from lat. $43^{\circ} 30' S.$ sails 219 miles south : required her lat. in.

Lat. left	$43^{\circ} 30' S.$
Diff. lat. 219'	$3^{\circ} 39' S.$
LAT. IN	$47^{\circ} 9' S.$

Ex. 2. A ship from lat. $43^{\circ} 11' N.$ makes 194 miles southing : required her lat. in.

Lat. left	$43^{\circ} 11' N.$
Diff. lat. 194' ...	$3^{\circ} 14' S.$
LAT. IN	$39^{\circ} 57' N.$

Ex. 3. A ship from lat. $1^{\circ} 3' N.$ sails 123 miles south : required her lat. in.

Lat. left	$1^{\circ} 3' N.$
Diff. lat. 123'	$2^{\circ} 3' S.$
LAT. IN	$1^{\circ} 0' S.$

The ship being in $1^{\circ} 3'$, or 63 miles N. of the equator, must evidently be in S. lat. after making 123 miles southing. Thus, in subtracting one of the quantities from the other, the difference takes the name of the greater.

Examples for Exercise.

1. A ship from lat. $59^{\circ} 27' S.$ sails southward until her diff. lat. is 374 : find her present lat. Ans. $65^{\circ} 41' S.$
2. Lat. left $48^{\circ} 2' S.$ diff. lat. 149 N. ; what is the lat. in ? Ans. $45^{\circ} 33' S.$
3. Lat. left $53^{\circ} 4' N.$ diff. lat. 122' N. ; find the lat. in. Ans. $55^{\circ} 6' N.$
4. Lat. left $0^{\circ} 0'$, diff. lat. $2^{\circ} 13' S.$; what is the lat. in ? Ans. $2^{\circ} 13' S.$

191. **LONGITUDE** is the distance measured on the equator between the meridian of a given place and another meridian, called the *first meridian*.* The first meridian with us is the meridian of Greenwich Observatory; thus, if G be Greenwich (fig. in No. 180), the longitude of A is DM, the longitude of B is DK.

The longitude of a place is named East or West, according as it is to the east or west of the first meridian; thus A is in west longitude, H is in east longitude.

* The first meridian is a matter of arbitrary choice amongst different nations; thus, the French refer to Paris. It is therefore necessary, in taking up a chart, to observe what meridian the longitude is reckoned from. See p. 395.

192. We may use either the longitude of one name or the supplement to 360° , with the contrary name; thus, instead of 166° W. we may say 194° E.

193. Longitude is measured either in *space* (or arc), that is, in degrees, minutes, and seconds; or in *time*, that is, in hours, minutes, and seconds, each hour being equal to 15 degrees; for the sun, which regulates the time, returns to the same meridian again, after describing a complete circle, or 360° , in 24 hours, and 15×24 is 360.

194. The DIFFERENCE OF LONGITUDE of two places is the portion of the equator included between their meridians; thus M F is the diff. long. of A and C, as also of A and H, and of b and C. To measure, therefore, the diff. long. of two places, we must follow down their meridians to the equator, and then take the included portion of the equator itself.*

195. When two places are on the *same* side of the first meridian, their diff. long. is found by *subtracting* the lesser longitude from the greater; thus the diff. long. of C and P, that is, the difference between D F and D K, is K F. But where the places are on *opposite* sides of the first meridian, that is, when one place is in east longitude and the other in west longitude, the *sum* of their longitudes is the diff. long.; thus the diff. long. of A and P, as also of A and B, is M K, which is the sum of M D and K D.

When one longitude being east and the other west, the sum exceeds 180° , take the supplement to 360° for the diff. long.

Ex. 1. Find the diff. long. of Ushant and the east point of Madeira.

Ushant.....	$5^\circ \quad 3' \text{ W.}$
E. point of Madeira	$16 \quad 39 \text{ W.}$
DIFF. LONG.	$11 \quad 36$

Ex. 2. Find the diff. long. of the Cape of Good Hope and Tristan d'Acunha.

Cape of Good Hope	$18^\circ \quad 29' \text{ E.}$
Tristan d'Acunha ...	$12 \quad 2 \text{ W.}$
DIFF. LONG.	$30 \quad 31$

Ex. 3. A ship sails from longitude $7^\circ 56' \text{ W.}$ to $18^\circ 32' \text{ W.}$: find her diff. long.

Long. left.....	$7^\circ \quad 56' \text{ W.}$
Long. in	$18 \quad 32 \text{ W.}$
DIFF. LONG.	$10 \quad 36$

Ex. 4. A ship sails from longitude $1^\circ 20' \text{ W.}$ to $2^\circ 17' \text{ E.}$: find her diff. long.

Long. left.....	$1^\circ \quad 20' \text{ W.}$
Long. in	$2 \quad 17 \text{ E.}$
DIFF. LONG.	$3 \quad 37$

Examples for Exercise.

Required the difference of longitude between the following places:

1. Between Halifax and the Cape of Good Hope.	Ans. $4924.$
2. Between Ushant and St. Michael's.	Ans. $1238'.$
3. Between Diego Ramirez and C. Lopatka.	Ans. $8071'.$
4. Between New York and Manila.	Ans. $9899'.$

196. When a ship in E. long. sails east, or in W. long. sails west,

* Since the meridians are all parallel at the equator and meet at the poles, the distance between any two meridians, measured east and west, is less as the latitude is greater; that is, the absolute number of miles, or of feet, in a degree of longitude, is less as the latitude in which they are measured is greater. Hence, also, a given number of miles between two meridians corresponds to a greater diff. long. as the latitude in which they are measured is greater. For example, two places in lat. 10° and distant 40 miles east and west from each other, have $40 \cdot 6$ diff. long. In lat. 50° two places similarly situated have $1^\circ 2' 2$ diff. long. Questions of this kind are solved by the rules of Parallel Sailing.

she evidently increases her longitude, or the distance from the first meridian. But if in E. long. she sails west, or in W. long. she sails east, she diminishes her longitude. Hence, when one longitude is given, and also the diff. long., the other longitude is easily found.

Ex. 1. A ship from long. $31^{\circ} 40'$ E. sails east $3^{\circ} 9'$: find the long. in.
 Long. left..... $31^{\circ} 40'$ E.
 Diff. long. $3^{\circ} 9'$ E.
 LONG. IN $34^{\circ} 49'$ E.

Ex. 2. A ship from long. $97^{\circ} 45'$ W. makes $1^{\circ} 11'$ easting: find the long. in.
 Long. left $97^{\circ} 45'$ W.
 Diff. long. $1^{\circ} 11'$ E.
 LONG. IN $96^{\circ} 34'$ W.

Ex. 3. A ship from long. $0^{\circ} 32'$ W makes $2^{\circ} 8'$ easting: find the long. in.
 Long. left $0^{\circ} 32'$ W.
 Diff. long. $2^{\circ} 8'$ E.
 LONG. IN $1^{\circ} 36'$ E.

Ex. 4. A ship from long. $178^{\circ} 54'$ W makes $3^{\circ} 4'$ westing: find the long. in.
 Long. left $178^{\circ} 54'$ W.
 Diff. long. $3^{\circ} 4'$ W.
 LONG. IN $181^{\circ} 58'$ W.
 Or (by No. 195) $178^{\circ} 2'$ E.

Examples for Exercise.

- | | |
|--|---------------------------|
| 1. Long. left $1^{\circ} 25'$ W. diff. of long. $85'$ E: what is the long. in? | Ans. $0^{\circ} 0'$ |
| 2. Long. left $0^{\circ} 0'$, diff. of long. $146'$ W: the long. in is required. | Ans. $2^{\circ} 26'$ W. |
| 3. Long. left $0^{\circ} 0'$, diff. of long. $122'$ E: what is the long. in? | Ans. $2^{\circ} 2'$ E. |
| 4. Long. left $160^{\circ} 20'$ W. diff. of long. $41^{\circ} 20'$ W: find the long. in. | Ans. $158^{\circ} 20'$ E. |
| 5. Long. left. $179^{\circ} 10'$ E. diff. of long. $34'$ E.: what is the long. in? | Ans. $179^{\circ} 26'$ W. |

197. The *COURSE steered* is the angle between the meridian and the ship's head. The *course made good* is the angle between the meridian and the ship's real track on the surface of the sphere.

The course is reckoned from the north, towards the east or west, when the ship's head is less than eight points from the north point. The same applies to the south point. The course is measured in *points* of $11^{\circ} 15'$ each, or in degrees and minutes.

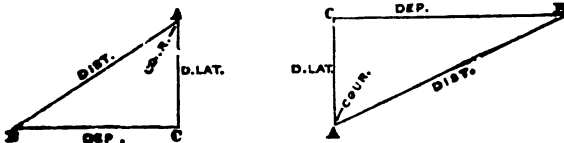
198. The track of the ship while preserving the same angle with all the meridians as she crosses them in succession, is called the *RHUMB LINE*.

199. The *DISTANCE* between two places, or the distance run by the ship on a certain course, is measured in *nautical miles* of 60 to the degree of latitude. See p. 104, note, and Table 64 A. Three such miles make a *nautical league*.

200. The *DEPARTURE* is the distance in nautical miles, made good by the ship due east or west; or the distance between two places measured along their parallel.

Departure is marked east or west, according as it is made good towards the east or west, and is accordingly called *easting* and *westing*; such easting and westing being, however, expressed in *miles*, and not, like longitude, in *arc*.

Thus, if a ship sails from a place A to another as B, A B is the



Distance; A C drawn N. and S., or in the meridian, shews the angle

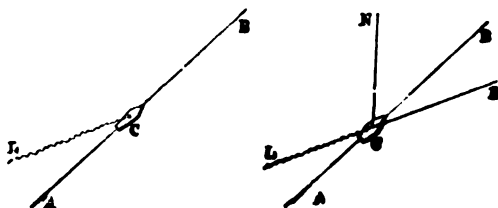
$C A B$ the *course*; $B C$ drawn E. and W., or perpendicular to $C A$, is the *departure*; and $A C$ is the *diff. lat.*

201. The **BEARING** of an object or place is the angle contained between the meridian and the direction of the object, and is the same thing as the course towards it.

Taking a bearing of an object is called *setting* it.

The bearings of two objects, taken from the same place, constitute *cross bearings*, the lines of direction of the two objects intersecting or crossing each other at the place of the observer.

202. **LEEWAY** is the angle included between the direction of the ship's keel and the direction of the wake she leaves on the surface of the water.



Thus the vessel C , while she moves through the water in the direction of her length, in the line $C B$, is at the same time pressed to leeward of this line by the force of the wind, supposed in the figures to blow on the vessel's left or port side; her wake, or actual path through the water, appears therefore to windward of the line which she endeavours to keep, as is represented by the line $C L$. The angle $A C L$ is the leeway.

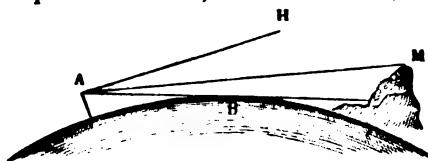
The course steered (No. 197) is the angle $N C B$, $N C$ being the meridian; the course made good is $N C D$, the line $C D$ being determined by producing $L C$.

203. The **DEAD RECKONING** is the account kept of the ship's place, without reference to astronomical observation. It is written *D. R.* for shortness.

204. The **VISIBLE**, or **SEA HORIZON**, is the apparent boundary of the surface of the water, which appears to the eye the circumference of a circle.

205. The **DEPRESSION**, or, as it is called by abbreviation, **DIP**, is the angle through which the sea horizon appears depressed, in consequence of the elevation of the spectator.

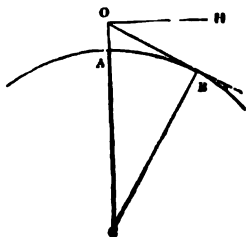
Suppose the spectator at A , above the sea, and $A H$ a line



perpendicular to the plumb-line at A , which tends to the centre; $A H$ is the true level, or horizontal line, and the angle $H A B$, included between it and the line $A B$, touching the sea, is the dip.

The dip depends on the distance in nautical miles of the visible horizon. Thus, to the eye 30 feet above the sea the true dip is 6', or the distance of the horizon itself is about 6 miles. This is easily proved thus,

Let C be the centre of the earth, O the place of the observer; then the line OB drawn touching the surface at B determines B the farthest point visible to him. Draw OH perpendicular to OC, then since OB touches the circle at B, the angle CBO is a right angle (No. 138, Cor.) Hence BCA is the complement of COB, and HOB is also the complement of COB ($\text{COH} = 90^\circ$), therefore ACB and HOB are equal.



The depression is given in Table 8.

206. The ALTITUDE of a terrestrial or celestial object above the sea horizon is the angle included between the line drawn from the eye to the object, and the line from the eye to the horizon. Thus, the angle MAB is the altitude of the summit M. The altitude here, in consequence of the great elevation of the spectator at A, about $\frac{1}{3}$ of the radius, or 330 miles, is less than the dip, or the summit M is really below the true horizontal line AH. This may take place when, from the small height of the object with respect to that of the observer, or its great distance, it is seen very little elevated; but in most cases AM will fall above AH.

207. The rays of light which pass from any distant object on the earth suffer a change in their direction, which is called the *terrestrial refraction*, by which the object appears in general higher than its true place. This effect is, on the average, about $\frac{1}{4}$ of the intercepted arc, or distance in miles, which are minutes of a degree very nearly. Thus, an object twenty-eight miles distant is raised about 2' above its true place. The sea horizon is thus raised by refraction, or the apparent dip (Table 30) is less than the true.

This proportion, however, is subject to great irregularity, and varies between $\frac{1}{3}$ and $\frac{1}{4}$ of the intercepted arc. The apparent elevations of the summits of high land are thus subject to great variations, depending on particular states of the air.

208. The apparent place of the sea horizon differs also in different temperatures of the sea and air. When the sea is *warmer* than the air, the horizon appears *below* its mean place, or that at which it appears when the air and water are of the same temperature, or the apparent dip is too small; when the sea is *colder* than the air, the horizon appears *above* its mean place,* or the apparent dip is too great.

* Admiral W. F. W. Owen informs me that he found on one occasion, in observing a star's altitude, a change of 4' in the place of the sea horizon, in the tropics, soon after sunset. Mr. Fisher observed a variation in the place of the horizon of 18' in the arctic regions. In summer the ice horizon was *elevated*, not depressed; in the winter it was depressed several minutes.— (*Appendix to Captain Parry's Voyage in 1821-3*, p. 187.) These observations, however, do not all follow the rule above. A table for correcting the apparent place of the sea horizon for the difference of temperature of the sea and the air, according to the height of the eye, would

Colonel Sabine gives a table of depressions observed from the gangway of H.M.S. Pheasant, at 15 ft. 1 in. above the sea, in the Gulf Stream, and after leaving it.* On Dec. 5, 1822, lat. $36^{\circ}\frac{1}{2}$ N., long. $72^{\circ}\frac{1}{2}$ W., at 10^h A.M., the temperature of the sea being 70° , that of the air 60° , the dip observed by Wollaston's dip sector was $4' 57''$, or $1' 6''$ more than the table. At noon the temperature of the water had changed to $62^{\circ} 4$, the air at 60° as before, the ship having passed from the warmer water of the stream to the colder water of the rest of the ocean, and the dip observed was $3' 37''$. From the result of his observations, Colonel Sabine considers that the navigator will be right nine times in ten in assuming that, when the sea is warmer than the air, the tabular dip is too small. In only one case, however, did this error ever amount to so much as $1' 56''$, the sea being then at 49° , and the air at 38° , or the difference 11° ; and it is important to remark that the error of the table is by no means proportional to the difference of these temperatures, which in one case was no less than 29° .

Numerous instances are on record, in the accounts of modern navigation, of errors of observation arising from variation in the place of the sea horizon.

209. Besides the vertical effect of refraction above described, some instances have been recorded of a sensible change in the *horizontal* direction of objects. Mr. K. B. Martin observed a change in the true direction of a point of land in the Azores, towards sunset. He also mentions an extraordinary change in the direction of C. Grisnez light as seen from Ramsgate at the close of a very hot day; on which occasion, also, distant objects were elongated horizontally till they seemed to separate into parts. ("Naut. Mag." 1847.)

Lieutenant Wilkes observed from the summit of Mowna Roa, the sun's horizontal diameter lengthened out to twice and a half the vertical one. ("Narrative of the United States Exploring Expedition," 1838-42.) In the Survey of the Isthmus of Tehuantepec, under Señor G. Moro, in 1842-3, the refractions at San Mateo on the Pacific, "especially the lateral ones," produced the strangest illusions.†

210. The TROPICS of CANCER and CAPRICORN are the parallels of latitude $23^{\circ} 28'$ N. and S. These are the dotted lines nearest the equator (fig. in p. 55). The sun is vertical at noon twice in the year to every place between the tropics, and never to any place outside of them. The space between the tropics is called the TORRID ZONE, on account of its heat.

211. The ARCTIC CIRCLE, or North Polar Circle, and the ANT-ARCTIC CIRCLE, or South Polar Circle, are parallels distant $23^{\circ} 28'$ from each pole, and are therefore in latitude $66^{\circ} 32'$. These are the dotted lines nearest the pole. Within these circles the sun does not set during part of the summer, nor rise during part of the winter.

The spaces within these circles are called the FRIGID ZONES, on account of the cold. The spaces between the tropics and the polar circles are called the TEMPERATE ZONES.

be useful; but there are scarcely any data for the construction of such a table, and the theory itself appears not to be complete.

The above variation of the place of the apparent horizon, with mirage, reflected images, and other optical illusions, were first discussed, generally as questions of unequal temperature alone, by M. Biot, *Mém. de l'Institut*, 1809.

* Account of Experiments to determine the Figure of the Earth. London, 1825, p. 454.

† It is easy to conceive, that if a mass of air of different density from the rest be interposed between the spectator and the object, and if also the sides or faces which he looks through be not exactly parallel, it will have the effect of a prism, and will seem to throw the object to the right or left of its true direction. If the surfaces are curved, the effect of magnifying or diminishing will occur at the same time.

CHAPTER II.

INSTRUMENTS OF NAVIGATION.

I. THE COMPASS. II. THE LOG AND GLASSES.

THE necessary instruments of navigation are the COMPASS, by the aid of which the course of the ship can be directed; and the LOG, which, with the help of sand-glasses for measuring small intervals of time, or a watch showing seconds, gives the velocity or rate of the ship, and thence the distance run in any interval of time.

I. THE COMPASS.

212. Before the invention of the Compass, the course of the ship was directed by reference to the land, or to the position of the heavenly bodies; but when those objects were obscured, the seaman must sometimes have been much perplexed.

The pointing or directive property of the magnet, on which the efficiency of the compass mainly depends, appears to have been known to the Chinese, and made use of by them in travelling by land and sea, in times of remote antiquity. The ancient Greeks and Romans, though familiar with the magnet, were not apparently aware of its directive property, nor were their descendants till the beginning of the thirteenth century. About that time the seamen of the Mediterranean gradually became acquainted with the fact, that a piece of magnetised steel, shaped like and commonly called a needle, would, if allowed to turn freely about its centre, always come to rest in the same direction, and that, by reference to its pointing, they could roughly check or direct the course of the vessel.

Thus, before the seamen of those days were two problems. First, the best means of giving to the needle freedom, to take up any horizontal direction, and of indicating the direction of the ship's head relative thereto. Second, to find the exact direction of the pointing of the needle, in relation to some known standard of direction. In other words, first the perfecting of the mariner's compass; second, a knowledge of what is now called its variation.

Apparently, the earliest means used to allow the needle to take up any position in azimuth, was by thrusting it through a piece of light wood or pith, forming with it a rectangular cross;

The points *next* the eight principal points (namely, N., S., E., W., and N.E., N.W., S.E., and S.W.) take the word *by* between the name of such point and the next cardinal point. Thus the point *next* to north, on the east side, is called North *by* East; that on the West side is called North *by* West. Thus, on inspecting the compass, it is easy to see the reason of the names E. by N., S.W. by W., &c.

A *half-point*, which is the middle division between two points, is called after that one of its adjacent points which is either a cardinal point, or is the nearest to a cardinal point. Thus the middle division between N. and N. by E. is called north-*half-east* (written N. $\frac{1}{2}$ E.). Half-points near N.E., N.W., S.E., and S.W., take their name from these points. Thus we say N.E. $\frac{1}{2}$ N., and N.E. $\frac{1}{2}$ E., and N.E. by E. $\frac{1}{2}$ E.

The same holds for a quarter and for three-quarters as for a half-point.

In speaking of these divisions of the card, brevity seems to have been the chief end, rather than the habitual reading of the card from left to right, or the reverse. Thus, we may say N.E. by E. $\frac{1}{2}$ E.; but continuing to the right, instead of E.N.E. $\frac{1}{2}$ E. and E. by N. $\frac{1}{2}$ E., it is usual to say E. by N. $\frac{1}{2}$ N. and E. $\frac{1}{2}$ N.

The name of the opposite point to any proposed point is known *at once*, without referring to the compass, by simply reversing the names or the letters which compose it. Thus the opposite of N. being S., and that of E. being W., the opposite point to S.W. by S. is at once known to be N.E. by N. The opposite of W. $\frac{3}{4}$ S. is E. $\frac{1}{4}$ N., and so on.

Dividing the circumference of the card, by successive halving, into points, half-points, and quarter-points, was well adapted to the time, not very distant, when many helmsmen were unable to read. The quarter-point was also considered the smallest division a man, sometimes under the blinding influences of wind, rain, and spray, could well distinguish. Now, however, the cards of steering compasses are frequently divided to degrees, in addition and external to the point divisions. In cards of nine or ten inches in diameter, the degrees are sufficiently large to be distinguished by men of ordinary sight. The degrees are always marked from North or South, towards the East or West; the courses, therefore, are read from left to right, and *vice versa*, in alternate quadrants. This is apt to cause mistakes in steering. For this reason, and for precision and brevity in speaking, writing, and signalling, there is much to be said in favour of marking the card from zero to 360 degrees, round by the right. Small compasses for shore work are thus marked generally.

Repeating the points in any order is called *boxing the compass*; to do this is, of course, one of the first things a seaman learns.

In becoming familiar with the points of the compass the

learner should bear in mind that their utility is far from being confined exclusively to navigation, and that in finding his way across a new country, or through the streets of a strange city, no impressions will be so distinct or so permanent as those grounded on the points of the compass.

213. As the ship's course, which is sometimes expressed in points and sometimes in degrees, is always reckoned from the north or south point, the seaman has to refer at once, in using the Tables, to the *number of points*, or *degrees*, in any course given by *name*. The following table, which exhibits the degrees, minutes, and seconds, in each quarter-point of the compass, will be convenient for reference :—

N—E	N—W	S—E	S—W	Pts.	° ' "
North.	North.	South.	South.		
N $\frac{1}{4}$ E	N $\frac{1}{4}$ W	S $\frac{1}{4}$ E	S $\frac{1}{4}$ W	$\frac{1}{2}$	2 48 45
N $\frac{1}{2}$ E	N $\frac{1}{2}$ W	S $\frac{1}{2}$ E	S $\frac{1}{2}$ W	$\frac{3}{4}$	5 37 30
N $\frac{3}{4}$ E	N $\frac{3}{4}$ W	S $\frac{3}{4}$ E	S $\frac{3}{4}$ W	$\frac{5}{8}$	8 26 15
N b E	N b W	S b E	S b W	1	11 15 0
N b E $\frac{1}{4}$ E	N b W $\frac{1}{4}$ W	S b E $\frac{1}{4}$ E	S b W $\frac{1}{4}$ W	$1\frac{1}{4}$	14 3 45
N b E $\frac{1}{2}$ E	N b W $\frac{1}{2}$ W	S b E $\frac{1}{2}$ E	S b W $\frac{1}{2}$ W	$1\frac{1}{2}$	16 52 30
N b E $\frac{3}{4}$ E	N b W $\frac{3}{4}$ W	S b E $\frac{3}{4}$ E	S b W $\frac{3}{4}$ W	$1\frac{3}{4}$	19 41 15
NNE	NNW	SSE	SSW	2	22 30 0
NNE $\frac{1}{4}$ E	NNW $\frac{1}{4}$ W	SSE $\frac{1}{4}$ E	SSW $\frac{1}{4}$ W	$2\frac{1}{4}$	25 18 45
NNE $\frac{1}{2}$ E	NNW $\frac{1}{2}$ W	SSE $\frac{1}{2}$ E	SSW $\frac{1}{2}$ W	$2\frac{1}{2}$	28 7 30
NNE $\frac{3}{4}$ E	NNW $\frac{3}{4}$ W	SSE $\frac{3}{4}$ E	SSW $\frac{3}{4}$ W	$2\frac{3}{4}$	30 56 15
NE b N	NW b N	SE b S	SW b S	3	33 45 0
NE $\frac{1}{4}$ N	NW $\frac{1}{4}$ N	SE $\frac{1}{4}$ S	SW $\frac{1}{4}$ S	$3\frac{1}{4}$	36 33 45
NE $\frac{1}{2}$ N	NW $\frac{1}{2}$ N	SE $\frac{1}{2}$ S	SW $\frac{1}{2}$ S	$3\frac{1}{2}$	39 22 30
NE $\frac{3}{4}$ N	NW $\frac{3}{4}$ N	SE $\frac{3}{4}$ S	SW $\frac{3}{4}$ S	$3\frac{3}{4}$	42 11 15
NE	NW	SE	SW	4	45 0 0
NE $\frac{1}{4}$ E	NW $\frac{1}{4}$ W	SE $\frac{1}{4}$ E	SW $\frac{1}{4}$ W	$4\frac{1}{4}$	47 48 45
NE $\frac{1}{2}$ E	NW $\frac{1}{2}$ W	SE $\frac{1}{2}$ E	SW $\frac{1}{2}$ W	$4\frac{1}{2}$	50 37 30
NE $\frac{3}{4}$ E	NW $\frac{3}{4}$ W	SE $\frac{3}{4}$ E	SW $\frac{3}{4}$ W	$4\frac{3}{4}$	53 26 15
NE b E	NW b W	SE b E	SW b W	5	56 15 0
NE b E $\frac{1}{4}$ E	NW b W $\frac{1}{4}$ W	SE b E $\frac{1}{4}$ E	SW b W $\frac{1}{4}$ W	$5\frac{1}{4}$	59 3 45
NE b E $\frac{1}{2}$ E	NW b W $\frac{1}{2}$ W	SE b E $\frac{1}{2}$ E	SW b W $\frac{1}{2}$ W	$5\frac{1}{2}$	61 52 30
NE b E $\frac{3}{4}$ E	NW b W $\frac{3}{4}$ W	SE b E $\frac{3}{4}$ E	SW b W $\frac{3}{4}$ W	$5\frac{3}{4}$	64 41 15
ENE	WNW	ESE	WSW	6	67 30 0
E b N $\frac{1}{4}$ N	W b N $\frac{1}{4}$ N	E b S $\frac{1}{4}$ S	W b S $\frac{1}{4}$ S	$6\frac{1}{4}$	70 18 45
E b N $\frac{1}{2}$ N	W b N $\frac{1}{2}$ N	E b S $\frac{1}{2}$ S	W b S $\frac{1}{2}$ S	$6\frac{1}{2}$	73 7 30
E b N $\frac{3}{4}$ N	W b N $\frac{3}{4}$ N	E b S $\frac{3}{4}$ S	W b S $\frac{3}{4}$ S	$6\frac{3}{4}$	75 56 15
E b N	W b N	E b S	W b S	7	78 45 0
E $\frac{1}{4}$ N	W $\frac{1}{4}$ N	E $\frac{1}{4}$ S	W $\frac{1}{4}$ S	$7\frac{1}{4}$	81 33 45
E $\frac{1}{2}$ N	W $\frac{1}{2}$ N	E $\frac{1}{2}$ S	W $\frac{1}{2}$ S	$7\frac{1}{2}$	84 22 30
E $\frac{3}{4}$ N	W $\frac{3}{4}$ N	E $\frac{3}{4}$ S	W $\frac{3}{4}$ S	$7\frac{3}{4}$	87 11 15
East.	West.	East.	West.	8	90 0 0

214. The Azimuth Compass is a compass of superior construction, especially adapted for observing bearings. It is fitted with

two vertical vanes. The one near the eye in observing, has a narrow vertical slit, with coloured shades for observing the sun. The other vane has a wider slit or opening, having a vertical thread in the middle of it. In front of this vane is a reflector, for observing objects elevated above the horizon. The line joining the slit in one vane, and the vertical thread in the other, should pass over the centre of the card. The cards of azimuth compasses are always marked to degrees, and frequently to smaller divisions.

In the Prismatic Azimuth Compass, a magnified image of the divisions of the card is read by reflection, in a prism attached to the fore side of the near sight vane. Azimuth compasses being required for taking bearings, are placed on a tripod for shore work, and on an elevated stand on board ship.

215. In the early part of the present century, when ships and instruments for navigation were rapidly improving, the compass was still a rude instrument, and not abreast of the requirements of the seaman. In 1820 Mr. Barlow reported to the Admiralty, that half the compasses he had at their request examined, belonging to the Royal Navy, were useless. It is probable that the compasses of the Mercantile Navy were no better. In 1837 their Lordships appointed a committee to inquire into the matter, and, if possible, to find a remedy for an evil so pregnant, as they said, with mischief. This step was taken for the benefit of the Royal Navy, and the improvement which took place, both in the design and in the workmanship of the compass, in consequence of the recommendations of the Admiralty compass committee, was of immediate and lasting benefit to the public service. The Mercantile Navy was not so immediately benefited, as the proceedings of that committee were not made public. But doubtless the fact of there having been such a committee stimulated compass makers to seek information, and to apply it to the improvement of the mariner's compass.

A great difficulty to be overcome, in a compass intended to be used on board ship, is the disturbance of the card caused by the motion of the ship. The Admiralty compass committee, while insisting on extreme lightness in the fly and fittings of the card, made considerable addition to its weight, by applying more needle power than would otherwise have been desirable, in order to secure steadiness. This was a fairly successful way of meeting the motion of ships at that date. But the violent and continuous motion, subsequently caused by the general adoption of the screw propeller, has been generally met, by suspending the compass bowl by springs or india-rubber.

The difficulty of getting a compass that would be steady in small vessels and boats, led to the introduction of the Liquid Compass; that is, a compass having the bowl filled with liquid instead of air. The first practical liquid compass was patented

by Mr. Crowe in 1818. It was subsequently improved by other makers, and is now, when well made, a very efficient compass for all purposes. It is especially adapted to stand severe vibration, and the shock of gun-firing. For these purposes, and for use in boats, it has not yet been excelled.

216. In 1876 Sir Wm. Thomson patented a compass, which is regarded with much favour by navigators. At the circumference of the card is an aluminium ring; the cap is held in the centre by radial silk threads, extending from it to the ring. Attached to the ring and threads is a disc of very light paper, its circumference having the usual compass graduations. All the central part of this disc is removed, still further to lessen the weight. Recognising the fact, that the power of a magnet increases relative to its weight, as the size decreases, the needles are very small. They are suspended under the card from its circumference. The entire card is not more than one-fifth to one-tenth of the weight of compass cards generally, of the same size. The friction on the pivot is, therefore, proportionally diminished.

By giving to the card no more needle power than would certainly overcome this much-diminished friction, it has a very slow period of vibration. The desirability of giving to a compass card a period of vibration that would not be isochronous with the roll of the ship, in order to maintain steadiness in a seaway, had already been pointed out by Mr. A. Smith, and by Mr. Towson. The bowl is protected from disturbance, also, by being suspended on a twisted wire gromet. This compass card, from the little friction on the pivot, is very sensitive at all times. From its slow period of vibration, it is steady when the ship is rolling; and, by reason of the suspension of the bowl, it has considerable immunity from the disturbances caused by vibration, shakes, and sudden shocks.

217. Though a compass, when supplied to a ship, should be accurate and efficient, it is desirable that the seaman should be able to satisfy himself on these points. The following essentials should be looked to, in steering and azimuth compasses, as far as they apply to each kind respectively.

The point of the pivot should always be in the same plane as the centre of the gimbals. The pivot should be sharp, or, when intended to be a little rounded, quite smooth; it should be free from rust. The cap should be sound—that is, not cracked nor perforated—and free from dust or dirt, which sometimes gets into it. Placing the card gently on the pivot, it should be deflected two or three times, through a small angle from its position of rest, to see if it always comes back to rest at the same point. This would show if the needle power is sufficient to overcome the friction on the pivot.

Select a position on shore, free from disturbances, from whence the bearing of some object is known. Measure horizontal angles

from it with a sextant, or other means, to three other objects, so selected that the correct bearing of four objects, about 90° apart, may thus be known. Now turn the compass round horizontally, so that the line from the centre of the card to the lubber-line coincides, in horizontal direction, with the line from the centre of the card to each object in succession. At each position of the compass, observe the bearing of the first object, by the sight vanes. Assuming that the card is regularly divided, these observations would show whether or not a course shaped, or a horizontal bearing taken, by the compass is correct.

Placing the compass on board ship in its binnacle, see that the bowl takes up its proper horizontal position in the gimbals; that the lubber-line is vertical, and that a line from the centre of the card to the lubber-line is exactly in the same horizontal direction as the fore-and-aft line of the ship. See that the thread in the sight vane is vertical, by testing it with a plumb line; and raise and lower the reflector, and see that the reflected image of the thread coincides with the thread itself. This will show that the bearing of an object at any elevation, whether taken by direct bearing or by reflection, is correct.

Metal pivots become blunted by wear, and steel pivots are also very liable to rust; jewelled caps naturally get worn and perforated by use, especially from the long-continued working of the screw propeller. They are also liable to be cracked by sudden concussion. Heavy cards are sometimes fitted with speculum metal caps, and work on jewelled pivots. Defective caps and pivots are a fruitful source of inefficiency in compasses, and require the especial attention of the navigator.

218. At a time when ships had no compass in an elevated position, all bearings had to be taken from the steering compasses. These were low down to the deck, and therefore inconvenient for that purpose. And subsequently, when most ships had an elevated compass, its position was frequently such, that an all-round view could not be obtained therefrom. The difficulty was met by the introduction of an instrument called a dumb card, or bearing-plate. It consists of a circular plate of metal, graduated like a compass card, and so gimballed that it may be revolved round a central pivot, in a horizontal plane. Adjacent to the circumference is a mark, similar to the lubber-line of the compass. It is fitted with sight vanes, shades, and reflector, for taking bearings.

The instrument may be placed in any position from whence the object, or objects, to be observed may be seen. The greatest care must be taken to see that the line from the centre of the bearing-plate to its lubber-mark is in the exact fore-and-aft line of the ship. This may be done by referring it to some mark in the ship, exactly in the fore-and-aft line; or to some mark, such as a bollard, which, from the position chosen for the

bearing-plate, is a known, small, and constant angle from the fore-and-aft line.

If the direction of the ship's head by the bearing-plate, be made to correspond with the direction of the ship's head by any compass, then the bearings taken by the bearing-plate will be the same as if they were taken by that compass. And, conversely, if the bearing-plate be turned round, so that the bearing of an object by it corresponds with its known correct bearing, the direction of the ship's head, as shown by the bearing-plate, is correct. This instrument, sometimes called a Pelorus, is extensively used.

Another instrument, called a Palinurus, is sometimes used for getting true bearings. It is, simply, the mechanical construction of the celestial sphere, with its great circles. By means of time, latitude, and declination of some heavenly body, a line in the instrument may be set to the true direction of that body. All the parts of the instrument, when that line is pointed to the body, will be in the true astronomical direction, and the bearings on the horizontal circle of the instrument will be true bearings round the horizon. A mark placed as the lubber-line will, of course, show the true direction of the ship's head. It will be seen that, with this instrument, no calculations or azimuth tables are required to get a true direction.

With respect to the use of such adjuncts to the compass, as have been briefly described, liability to secondary errors, both personal and instrumental, must be taken into account. To work directly, from a well-placed standard compass, appears by far the safest practice in navigation.

Variation of the Compass.

219. The second problem before the early navigators was, to find the direction in which the needle pointed (No. 214). When the directive property of the magnet was first brought into use by seamen, it is probable that they continued for some time to steer by the sun and stars, as before. It was only when those objects were obscured, that they had recourse to a rude form of compass, to enable them to maintain their course, till their accustomed and more reliable guides appeared again. What the compass needle was to the seamen of those days, it is to the navigator of to-day. By it he can preserve a course, without reference to the heavenly bodies, for a longer or shorter time, and with more or less accuracy, according to the perfection of his compass, and to the degree in which he is acquainted with the laws which govern its pointing.

The natural standard of direction is the meridian. The horizontal angle contained between the direction of the meridian

and the direction of the needle, is called the Variation of the Compass. It is termed easterly or westerly, according to which side of the meridian the north end of the needle points.

The approximate direction of the meridian was easily seen in the northern hemisphere, by the position of the pole star. It must, therefore, have been well known, to all who noted the pointing of the compass needle, with any degree of care, that its direction did not coincide with the direction of the meridian; or, in other words, that it did not, in all places, point to the north. This fact seems to have been brought most prominently into notice by Columbus. He found, on his first voyage, in 1492, when well over towards the West Indies, that the needle pointed to the westward of north. In the seas which Columbus had hitherto navigated, as far as can be now judged, it pointed to the eastward of north. At the port in Europe from which he sailed the variation was, apparently, not less than two points easterly. Probably, therefore, it was the change, and especially its going from easterly to westerly, rather than the existence of variation, which arrested the attention of Columbus.

The first good determination of the variation, in England, was made in 1580, when the direction of the north end of the needle was about one point to the eastward of the meridian. Since that time, the variation has been observed with increasing frequency and accuracy. The following is an outline of the change in the variation in England.

Commencing in 1580 at $11^{\circ} 15'$ easterly, the north point of the needle moved towards the meridian, and crossed it in 1657, moving westward at the rate of $10'$ annually. The north end of the needle continued to move westward, with a diminishing rate, till 1818, when it attained the limit of its western range, $24^{\circ} 38'$ westerly. Since that date the north point of the needle has moved to the east with an increasing rate. The variation in London is now $17^{\circ} 30'$ westerly, diminishing at the rate of $8'$ annually.

The first attempt to give a comprehensive view of the direction of the compass needle, in all parts of the world, was made by Halley, in a chart published in 1700. This chart embraced the results of a voyage made by Halley himself, and such other information as was at that time available. Joining, by a line, the points on the earth's surface where the variation was the same, he traced, on a Mercator's chart, a series of lines of equal variation, extending over the Atlantic and Indian Oceans, and as far east as the meridian of 150° . Several similar charts, more complete and accurate, as the materials for compiling them increased in quantity and value, have since been published. The latest variation chart published by the Admiralty is all that the seaman can desire. On it the annual change of variation is also shown, enabling the navigator to obtain the variation very closely, at any date subsequent to that of the publication of the

chart. Comparing Halley's chart with those which have since been made, it appears that changes in the variation, analogous to those observed in England, but of greater or lesser extent, have been going on nearly all over the world. The variation of the compass is thus shown to be a variable quantity, changing at a variable rate. Such being the case, the only way in which it is possible to make and maintain an accurate variation chart, is by the co-operation of navigators, in making and recording, for that purpose, observations of the variation of the compass, in all those parts of the world over which they may sail.

220. Besides the change in the variation, which reaches its limits in long intervals of time, and is called the secular change, there are smaller changes, called periodical. Such is the diurnal change, wherein the needle moves through a small angle to the westward during the day, and returns to the eastward during the night, in the northern hemisphere. In the southern hemisphere, a similar change takes place, but in an opposite direction. The needle is also disturbed by the aurora, and by phenomena called magnetic storms. These changes are, in the navigable parts of the globe, too small to be of any importance to the navigator. Neither is the pointing of the compass needle affected by atmospheric phenomena, such as fogs, rain, wind, or thunderstorms. But in cases where a ship has been struck by lightning, the directive property of the compass needle has sometimes been impaired or destroyed.

There is, however, one cause of disturbance of the needle which should interest the navigator. Humboldt, in the beginning of this century, observed that the needle, in certain places on land, was deflected from what may be called its normal direction, by some property in the ground. In previous editions of this work, several places are noted, where the variation was affected by the land, or by the ground in shallow water.* It is probable, from the practice of steering by the land when it is in sight, rather than by compass courses, that this disturbance of the compass needle has escaped notice in some places where it exists. It is, therefore, desirable that this unquestionable source of danger should be pointed out, that the seaman may be on his guard, when navigating near the land, or in shallow water, especially in volcanic regions. Methods of determining the variation of the compass are given in Chapter VIII.

221. To correct compass courses and bearings for variation.

The manner of doing this appears thus. Suppose one compass card to be placed directly over another, and the lower one to be true. Now suppose the north point of the upper compass to be drawn two points to the right of the true by easterly variation, then the North point of the upper or magnetic compass corresponds

* Commander W. U. Moore of H.M.S. Penguin reports a large local disturbance of the needle (55°) in 9 fathoms, 2 miles from the shore, off Port Walcott; on the N.W. coast of Australia. See Notice to Mariners, No. 43 of 1891.

to N.N.E. of the *true* compass, which point is to the right of N., and the South point corresponds to S.S.W. of the true compass, to the right of S., and so on. The contrary would take place with westerly variation; hence to correct a magnetic course or bearing we have this rule.

Rule. When the variation is *easterly*, apply it to the *right* of the compass course or bearing; when *westerly*, apply it to the *left*, looking from the centre of the card over the point to be corrected.

Ex. 1. Course by compass, S. $\frac{1}{4}$ W.; variation, $2\frac{1}{2}$ points easterly.
True Course, $2\frac{1}{2}$ points to the right of S. $\frac{1}{4}$ W., or S. $\frac{3}{4}$ points W., or S.W. by S.

Ex. 2. Course by compass, N. by E.; variation, 2 point westerly.
True Course, 2 points to the left of N. by E., that is, N. by W.

Ex. 3. Course or bearing by compass, N. 84° E.; variation, 19° W.
True Course, N. 65° E.

Ex. 4. Course by compass, S. 4° E.; variation, 17° E.
True Course, S. 13° W.

To reduce a true course or bearing to the compass course or bearing, apply the variation the *contrary way* to that directed above.

Ex. 1. True course, N.E. by E.; variation, 1 point easterly.
Course by Compass, N.E.

Ex. 2. True course, E. $\frac{1}{4}$ N.; variation, $1\frac{1}{2}$ point westerly.
Course by Compass, E. by S.

Ex. 3. True course, North; variation, 18° easterly.
Course by Compass, N. 18° W.

Ex. 4. True course, West; variation, 21° westerly.
Course by Compass, N. 69° W.

Deviation of the Compass.

222. From the earliest times it was known that if a magnet, or a piece of ordinary iron, were brought near to a compass, it would deflect the needle in its pointing, and so make the compass indications erroneous. Compasses on board ship, therefore, were not placed near to each other, and iron was rigorously kept away from their vicinity. With these precautions, though accidents sometimes happened from iron in the vicinity of the compass being overlooked, ships were navigated with a fair amount of security. But as iron became increasingly used in the construction of ships, and by the introduction therein of steam engines, with their boilers and funnels, it was no longer possible to navigate, without systematically allowing for the deflection of the compass needle caused thereby.

The horizontal angle, which the needle is deflected by the iron in or of the ship, is called the Deviation of the Compass. It is named easterly or positive (E. or +), when the north end of needle is deflected to the eastward; and westerly or negative (W. or -), when deflected to the westward. The mode of ascertaining and applying the deviation of the compass, is the next problem to engage the attention of the student of navigation.

Within half a century of the present time, many navigators doubted the existence of the deviation of the compass; or, while admitting its existence, denied that it was of any practical importance. And the belief was not uncommon, that it was a constant error—that is, that it was the same in amount with the ship's head in any direction. Those, however, who had studied the subject, or whom circumstances had made familiar therewith, acknowledged its importance, and recognised the necessity of ascertaining the deviation of the compass, with the ship's head in all directions.

223. There are three standards from which to reckon an angle of direction. First, from the meridian, the direction of which can always be ascertained astronomically. A course or bearing thus reckoned, is called a true course, or true bearing. Second, from the direction of the magnetic north; that is, from the direction of a magnetic needle, when uninfluenced by any contiguous iron, or by any such local disturbances as are mentioned in No. 220. A course or bearing thus reckoned, is called a magnetic course or bearing. Third, from the direction of the compass needle, as shown by a compass which is instrumentally correct, placed in any position. A course or bearing thus reckoned, is called a compass course or bearing.

The prefix correct may be placed to either of these quantities. The terms correct true, correct magnetic, correct compass, are used to distinguish the exact angles from those more or less approximate. The student must not confuse correct compass with magnetic. A correct compass course or bearing means a course or bearing accurately observed, with an accurate compass, regardless of any disturbance by which the compass may be influenced.

224. From the fact that compasses, in different parts of a ship, gave different indications, came the necessity for navigating by one especial compass, placed in a selected position. Such a compass is called the Standard Compass. It should be an azimuth compass, that is, one fitted for observing bearings; and one essential of its position is, that from it bearings can be taken all round the horizon, and at any altitude.

Turning a ship round, so as to place her head on all points of the compass in succession, for the purpose of ascertaining the deviation, is called swinging the ship. A ship may be warped or towed round, when lying at anchor or at moorings; or advantage may be taken of her turning with the tide. Wherever there is room, it may be convenient to steer a ship round under steam. It is in all cases desirable that the ship should be checked in her swinging, and steadied on the point on which it is desired to obtain the deviation.

As the variation of the compass is determined by comparing the true bearing of an object with its magnetic bearing,

so the deviation of the compass is ascertained by comparing the magnetic bearing with the compass bearing—the compass, at the time, being deflected by the iron in and of the ship only. Any other disturbance, such as from the proximity of other ships or masses of iron, or the irregular influence of the land, is not deviation according to the definition already given.

The first problem is, therefore, to determine the magnetic bearing of some object external to the ship. The sun is very commonly used; the true bearing is easily found, and the variation being applied thereto, gives its magnetic bearing. A distant mark on the land may also be used; its true bearing may be found by the chart, or by measuring and applying the horizontal angle or difference of bearing between it and the sun, and the magnetic bearing by further applying the variation. A third method is to have a correct compass in a convenient position on shore, where it is free from magnetic disturbances. Then the bearing of that compass being taken from the standard compass, and the bearing of the standard compass being simultaneously taken from the shore compass, the deviation of the standard compass is found by comparison.

These methods are spoken of as, swinging by the sun, swinging by distant mark, and swinging by shore compass. When using a distant mark, it should be so far away that the radius of the circle, along the circumference of which the standard compass moves as the ship goes round, subtends a smaller angle than is of practical consequence in navigating. Otherwise the bearings must be corrected for parallax.

There are many places where the true direction of lines, on which two known and conspicuous marks appear in one, are known. These lines, called transit lines, offer especial facilities for ascertaining the deviation.

Looking from the centre of the card, if the bearing shown by the compass is to the left of the magnetic bearing, the needle is obviously deflected to the right, and the deviation consequently called easterly. If the bearing shown by the compass is to the right of the magnetic bearing, the needle must be deflected to the left, and the deviation westerly.

225. Though the deviation of other compasses is not of so much importance as that of the standard, it is usual to note the direction of the ship's head, as shown by them, when it is on each point by the standard. The deviation is usually tabulated for reference, in some form similar to the following, which is commonly called a Deviation Table.

Head by Standard Compass	Deviation of Standard Compass	Direction of Head by other Compasses		
		Port Steering	Starboard Steering	Bridge Compass

The bearing-plate is frequently used in swinging. The vanes on the bearing-plate, being set to the known magnetic bearing of the sun, distant mark, or shore compass, the magnetic direction of head is shown by the lubber mark, when the plate is turned round so that the vanes point to the object. Thus, the deviation of the compasses on the magnetic points is shown, and may be tabulated as follows :—

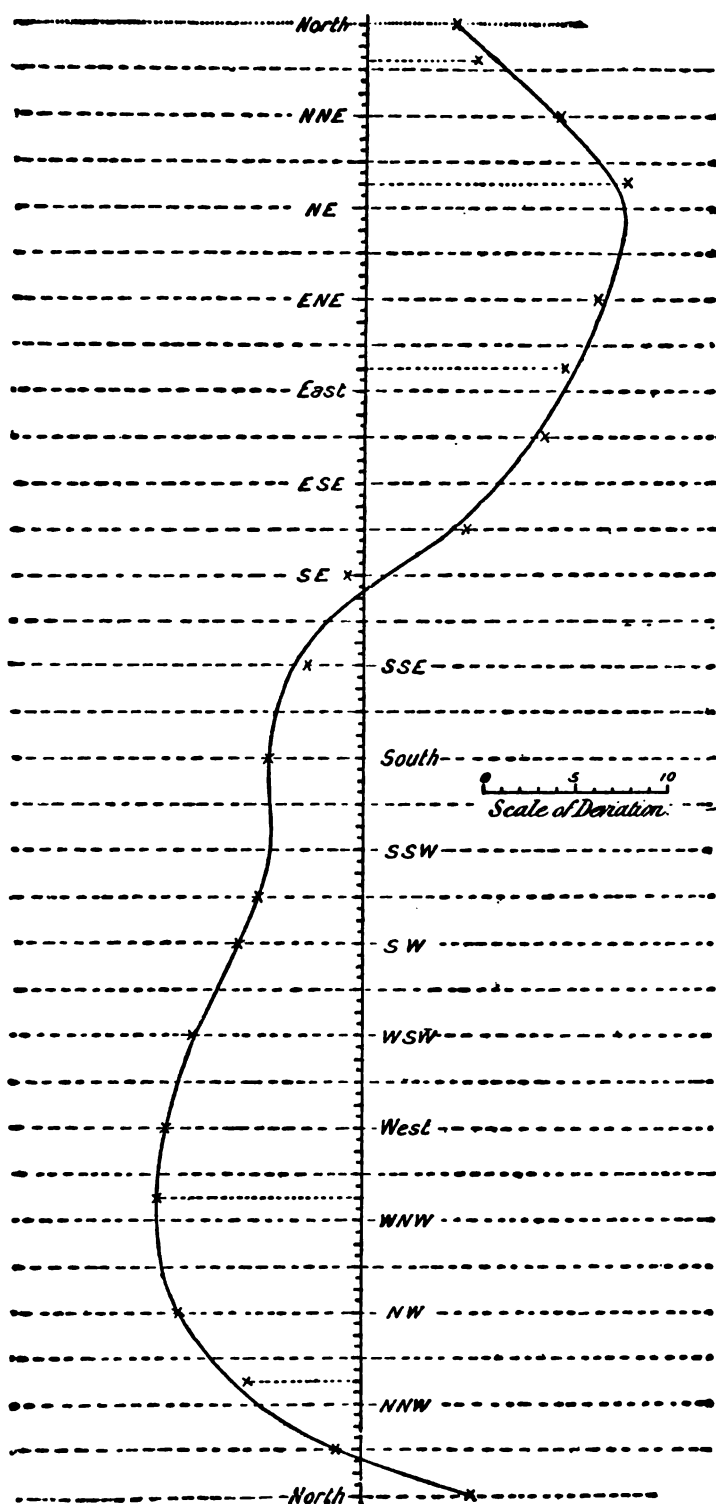
Head Magnetic	Direction of Head by Compasses			
	Standard	Port Steering	Starboard Steering	Bridge Compass

226. It is customary to form a deviation table from observations made on each point. But it may be convenient, or necessary, to form such a table with fewer observations, such as on every second or third point. Further, it may not be possible to get the observations exactly on the points. The problem, therefore, is to form a deviation table with few observations, irregularly distributed round the compass.

This is done by drawing a curve of deviations in the following manner. Draw a vertical line on paper, and divide it as a compass card is divided. The vertical line will thus represent the circumference of the card unrolled, and formed into a straight line. Through each compass point draw a line at right angles to the vertical line. On these lines, with any convenient scale, lay off the deviation found on each point. On parallel lines, passing through any intermediate degree or division of the point, lay off the deviation found thereon. Easterly deviation to be measured from the vertical line to the right, and westerly deviation to the left, marking, by a cross or otherwise, the positions thus determined. Now draw a line which, without being irregular in direction, passes most nearly through the several marks. This line, in practice, will always be a curve. The distance of the point of intersection of this curve with any point line, from the vertical line, will give the deviation on that point, using the same scale as before.

Example.—The following deviations having been observed, find the deviation on each compass point.

North	°	′	E	South	°	′	W
N $\frac{1}{2}$ E	6	0	E	SW b S	5	0	W
NNE	10	0	E	SW	5	30	W
NE $\frac{1}{4}$ N	14	0	E	WSW	8	0	W
ENE	12	0	E	West	10	0	W
E $\frac{1}{4}$ N	10	0	E	W b N $\frac{1}{4}$ N	11	0	W
E b S	9	30	E	NW	10	0	W
SE b E	6	0	E	NNW $\frac{1}{4}$ W	6	30	W
SE	1	0	W	N b W	1	0	W
SSE	2	30	W	North	5	0	E



227. Plotting these observations in the manner directed, and as shown in the foregoing diagram, the following table of deviations is obtained.

North	5 0 E	South	5 0 W
N b E	7 45 E	S b W	5 0 W
NNE	10 0 E	SSW	5 0 W
NE b N	12 15 E	SW b S	5 0 W
NE	13 30 E	SW	5 30 W
NE b E	13 30 E	SW b W	6 30 W
ENE	12 45 E	WSW	7 45 W
E b N	11 45 E	W b S	8 45 W
East	10 30 E	West	9 45 W
E b S	8 45 E	W b N	10 30 W
E b E	7 15 E	WNW	10 45 W
SE b E	4 30 E	NW b W	10 30 W
SE	0 45 E	NW	9 45 W
SE b S	2 0 W	NW b N	8 0 W
SSE	3 30 W	NNW	5 15 W
S b E	4 30 W	N b W	1 0 W

In the diagram shown, the vertical scale is made small as compared with the horizontal scale, in order to get it within the limits of the page. A sheet of ordinary ruled foolscap will be found very convenient for plotting deviations to form the curve.

228. The methods of ascertaining the deviation having been explained, the following are directions for applying the same to a compass course or bearing, so as to obtain the magnetic course or bearing.

The ship's head being on any compass point, and the deviation on that point being easterly, that deviation must be allowed to the right, to find the magnetic direction of the ship's head; and also to the right of any bearing taken by compass, to find the magnetic bearing. If the deviation on the compass course is westerly, it must be allowed to the left, to find the magnetic course or bearing.

Example.—Ship's head E.N.E. by compass, a point of land bore N. 10° W. What is the magnetic direction of the ship's head, and the magnetic bearing of the point, the deviation being as given in table 227?

The deviation on E.N.E. is 12.45 E., which allowed to the right of N. 67.30 E., gives N. 80.15 E. as the magnetic direction of the ship's head; and allowed to the right of N. 10.0 W., gives N. 2.45 E. as the magnetic bearing of the point. In the same way, head being N.W. and bearing S. 40 E., the deviation on N.W. is 9.45 W., which allowed to the left, gives N. 54.45 W. as magnetic direction of ship's head, and S. 49.45 E. as magnetic bearing of point.

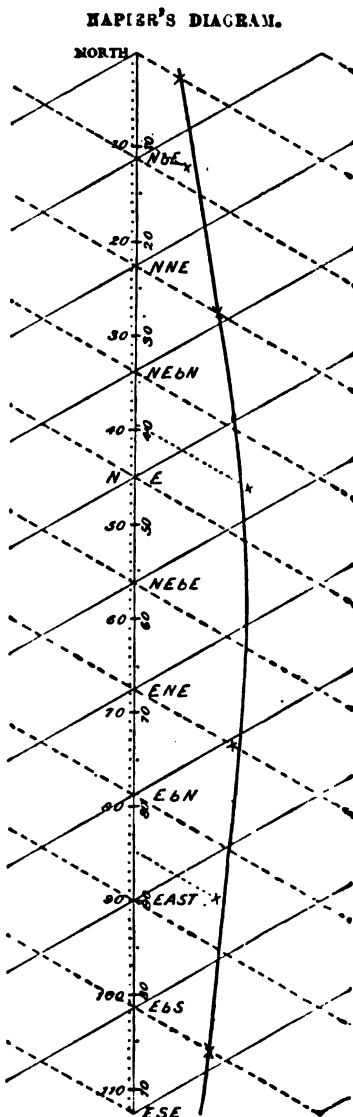
To turn magnetic courses or bearings into compass courses or

bearings, it is obvious that the deviation should be allowed the opposite way. That is, easterly deviation to the left, and westerly deviation to the right.

229. To facilitate turning compass courses or bearings into magnetic courses or bearings, and the reverse, certain graphic methods are sometimes used. The most common is one called, from its inventor, Napier's diagram. The example given, wherein are plotted, through a quadrant, the observations given in No. 226, shows the use of this diagram for the purpose named, as well as for forming a curve of deviations from few observations.

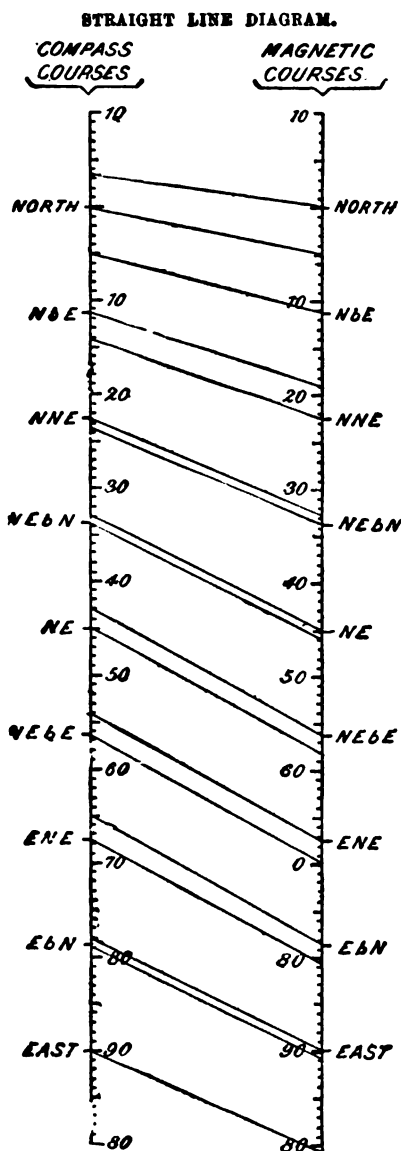
The dotted compass point lines intersect the vertical line, at an angle of 60° , and the vertical scale and deviation scale are equal. Therefore, if the deviation found on any compass point be laid off on one of the dotted lines, or on a line parallel thereto, and, from the point reached, a line be drawn making an angle of 60° with the compass point line, it will intersect the vertical line at the magnetic point. And, *vice versa*, if the deviation on a magnetic point be laid off on one of the plain lines, or on a line parallel thereto, the return line, drawn as before, will reach the vertical line at the compass point. The three lines form an equilateral triangle, of which the difference between compass and magnetic forms the base, the other sides being equal thereto, and to the deviation due to the direction of head, whether given by compass or magnetic.

230. Another method, called the straight line method, is due to Mr. Archibald Smith. It is only useful for showing, at a glance, the magnetic course equivalent to any given compass course, and *vice versa*, when the deviation is known. It consists merely of two parallel vertical lines, each divided as the circumference of a compass card is divided. Straight lines are



drawn, from the compass points on one line to the magnetic points on the other.

In the annexed example, the deviation table through one quadrant, given in No. 227, is thus treated.



If a ship be steering any compass course, shown on the left-hand column, the corresponding magnetic course is shown on the right-hand column. And if it is desired to steer any magnetic course, shown on the right-hand column, the required compass course is shown on the left-hand column.

231. A third method is to have two prints of compass cards, one laid on the other. The upper card somewhat smaller than the lower, and capable of being rotated about the common centre. The lower card, being fixed, may be considered as representing either true, or magnetic, courses or bearings.

Consider the lower card to represent true courses and bearings, and the north points of the two cards together. Conceive the north point of the upper card, moved through an arc equal to the variation, away from the north point on the lower card, to the right when the variation is easterly, and to the left when the variation is westerly. Magnetic courses and bearings on the upper card, and true courses and bearings on the lower card, will now be coincident.

Similarly, if the lower card be considered as showing magnetic courses or bearings, and the north points of the cards be separated by an arc equal to the

deviation, then the compass courses and bearings on the upper card, will coincide with magnetic courses or bearings on the lower card.

Diagrams on which curves of deviation can be drawn, so as to show indifferent observations, and thus eliminate their effects, or to form the curve from few observations, are of undoubted value to the seaman. But it is a question, whether any means such as have been described, for turning magnetic courses into compass courses, or the reverse, are of ultimate benefit. The habit of considering the effect on courses and bearings, of the north point, and consequently the whole circumference of the card, being turned right or left, from what may be considered its proper position, so as to have a clear conception thereof in the mind, will make the seaman independent of rules, and of all such semi-mechanical methods.

Adjustment of the Compass.

232. If the increase of iron put into ships had been limited to engines and boilers, it is possible that a compass might have been so placed, in most ships, that the deviation would have been comparatively small. Seamen might have continued to navigate with confidence, by ascertaining and applying the deviation. But when ships were built with iron beams, iron frames, or wholly of iron, it was no longer possible to evade a deviation so large as to be unmanageable; and steps had to be taken to correct, or, as it is now called, adjust, the compass.

This operation is generally performed by practised compass adjusters; but many rightly think this is essentially the duty of a seaman, and that he should also have sufficient knowledge of magnetism to enable him to select the best position for the compasses of a ship. In a book in which teaching navigation is the main object, magnetism can only be treated with brevity; but it is hoped that the navigator will find herein all that is required for his guidance.

The horizontal pointing of the compass needle has been shown to be of the utmost importance to the navigator. For the right understanding of the magnetism of iron ships, however, and its effect on the compass, some further knowledge of the pointing of the magnetised needle, and the cause thereof, is necessary.

In the year 1576, Robert Norman, a mathematical instrument maker, of London, discovered that a needle, however nicely balanced, would, after being magnetised, depart from the horizontal, and assume a position within 20° of vertical. By careful observations he found that the needle in London, at that date, pointed, with its north end downward, $71^{\circ}50'$ from the horizontal. Since that time, observations have been made nearly all over the world. It is found that the needle is horizontal only on a line round the earth, not far from the equator. Going from this line to the northward, the needle points with its north end downwards; and going to the southward, with its south end downwards. The angle of inclination, in both cases, increases, till in a position in

each hemisphere, about 18° from the earth's poles, the needle becomes vertical. These positions are called Magnetic Poles.

This angle of inclination to the horizontal is called the Dip. It is named positive, or +, when the end towards the north magnetic pole is the lower, and negative, or -, when the end towards the south magnetic pole is the lower. Like the variation, the dip is found to change with time, and other circumstances.

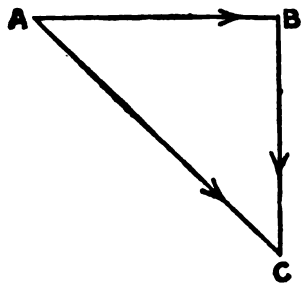
In the adjacent maps, lines of equal dip are drawn. The line whereon the dip = 0, is called the magnetic equator; and the lines of equal dip may be considered as parallels of magnetic latitude. The lines running nearly north and south show the horizontal direction the needle lies in, and may be considered as magnetic meridians. These lines converge to the magnetic pole in each hemisphere. For the use of seamen, there is no better way of giving the variation of the compass, than by lines of equal variation, as drawn on the variation chart (No. 238); but the lines here shown give a more direct representation of the pointing of the compass needle.

233. In the beginning of the present century it became known, chiefly through the researches of Humboldt, that the strength, or force, with which the needle points is not the same in all parts of the earth. It may be stated, generally, that this force is least about the equator, and, like the dip, increases towards the poles. Also, like the variation and dip, it is not constant in value at the same place.

The line whereon the magnetic force is least, coincides nearly with the magnetic equator; but there are apparently, in each hemisphere, two points where the force is greater than in the surrounding regions, neither of which coincides with the magnetic pole.

As the earth's force is not horizontal, except at the magnetic equator, it is convenient to reckon, or resolve, as it is called, that force in the horizontal and vertical directions. If the length of the line AC represents the earth's force, and the angle A be equal to the dip, then the horizontal line AB, and the vertical line BC, will in length represent, respectively, the horizontal and vertical components of the earth's force. These quantities are usually called the Horizontal Force, the Vertical Force, and the Total Force. Of these quantities and the dip, if any two are known, the other two may be found by the ordinary processes of trigonometry.

As previously stated, the dip and total force increase, going away from the magnetic equator; but it is evident that when the dip is 90° the horizontal force must vanish, whatever the total force may



Hemisphere from 60° W. to 120° E. Longitude.



Maps showing the **Magnetic Equator**, lines of **Equal Dip**, and **Horizontal Direction** of the **Compass Needle**. The parallels of latitude and the meridians are drawn at every fifteen degrees of latitude and longitude; the figures at the circumference denote the dip in degrees along the respective magnetic parallels; and the direction of the magnetic meridians, compared with the direction of the geographical meridians, shows the variation.

Hemisphere from 120° E. to 60° W. Longitude.



The points (©) to which the magnetic meridians converge are the magnetic poles, sometimes called, from the dip thereat being 90°, the poles of Verticity. The points (*) show the approximate position of the foci of maximum force. It is remarkable that these six points are within 160° of longitude.

These maps, and the following table of horizontal force, are based on the good work on this subject done by the late Sir F. Evans, R.N.

be. The dip and total force, therefore, increase together in such a manner that the horizontal force continually diminishes.

The horizontal force is the only part of the earth's force by which the compass card maintains its due position. The seaman is generally satisfied if this condition is fairly answered; but he must be sometimes painfully aware, from what is called the sluggishness of his compass, that this force is, at best, very feeble.

The following table gives the comparative value of the horizontal force, in different positions; the maximum value being considered as unity.

COMPARATIVE VALUE OF HORIZONTAL FORCE													
Maximum Value equal Unity													
Latitude	EAST LONGITUDE												
	0°	15°	30°	45°	60°	75°	90°	105°	120°	135°	150°	165°	180°
N 60°	0.40	0.41	0.43	0.44	0.44	0.43	0.42	0.43	0.44	0.45	0.47	0.49	0.48
50	0.49	0.52	0.55	0.57	0.58	0.58	0.58	0.57	0.57	0.59	0.60	0.60	0.59
40	0.60	0.64	0.68	0.70	0.73	0.75	0.75	0.75	0.74	0.73	0.71	0.70	0.68
30	0.71	0.75	0.79	0.83	0.87	0.89	0.90	0.89	0.87	0.84	0.82	0.80	0.76
20	0.78	0.81	0.86	0.90	0.94	0.97	0.97	0.96	0.94	0.92	0.89	0.86	0.84
10	0.82	0.85	0.88	0.90	0.93	0.97	1.00	1.00	0.99	0.97	0.94	0.92	0.90
0	0.79	0.79	0.80	0.83	0.87	0.90	0.96	1.00	1.00	1.00	0.98	0.97	0.95
S 10	0.70	0.70	0.70	0.72	0.76	0.82	0.88	0.92	0.96	0.98	0.98	0.97	0.96
20	0.61	0.59	0.59	0.60	0.64	0.71	0.77	0.82	0.87	0.90	0.91	0.91	0.90
30	0.56	0.54	0.52	0.53	0.54	0.58	0.62	0.68	0.71	0.75	0.78	0.81	0.82
40	0.55	0.51	0.49	0.48	0.49	0.50	0.51	0.54	0.55	0.57	0.62	0.65	0.68
50	0.54	0.50	0.47	0.44	0.43	0.42	0.41	0.39	0.38	0.39	0.43	0.47	0.52
60	0.53	0.49	0.46	0.42	0.39	0.36	0.32	0.27	0.20	0.20	0.24	0.30	0.37
Latitude	WEST LONGITUDE												
	0°	15°	30°	45°	60°	75°	90°	105°	120°	135°	150°	165°	180°
N 60°	0.40	0.37	0.33	0.29	0.22	0.12	0.10	0.20	0.29	0.38	0.43	0.46	0.48
50	0.49	0.45	0.41	0.37	0.34	0.32	0.36	0.43	0.49	0.54	0.55	0.57	0.59
40	0.60	0.55	0.50	0.48	0.47	0.50	0.56	0.60	0.64	0.65	0.65	0.66	0.68
30	0.71	0.66	0.62	0.61	0.65	0.71	0.77	0.80	0.80	0.77	0.74	0.74	0.76
20	0.78	0.74	0.72	0.72	0.77	0.85	0.90	0.90	0.88	0.85	0.82	0.82	0.84
10	0.82	0.79	0.77	0.79	0.84	0.89	0.94	0.95	0.92	0.89	0.89	0.90	0.90
0	0.79	0.78	0.77	0.80	0.83	0.89	0.92	0.93	0.92	0.90	0.92	0.93	0.95
S 10	0.70	0.71	0.73	0.76	0.80	0.84	0.87	0.88	0.89	0.88	0.91	0.93	0.96
20	0.61	0.65	0.68	0.70	0.74	0.79	0.82	0.84	0.85	0.87	0.88	0.90	0.90
30	0.56	0.60	0.63	0.67	0.70	0.76	0.77	0.78	0.78	0.80	0.81	0.82	0.82
40	0.55	0.59	0.63	0.67	0.71	0.74	0.75	0.73	0.71	0.70	0.70	0.70	0.68
50	0.54	0.59	0.63	0.69	0.72	0.73	0.72	0.68	0.63	0.61	0.59	0.56	0.52
60	0.53	0.58	0.63	0.68	0.71	0.71	0.67	0.60	0.55	0.50	0.46	0.42	0.37

234. In dealing with the subject of compass adjustment, it will sometimes be useful for the seaman to know the value of the force with which the needle points on board ship, compared with the force with which it points on shore; or the force with which

it points when the ship's head is in one direction, compared with the force with which it points when the head is in other directions. It is necessary, therefore, to show how comparative magnetic force is measured. If a magnetised needle, balanced on its centre, be disturbed from its position of rest, it will, like a pendulum, vibrate through diminishing arcs, till it again comes to rest. The speed of the needle is increased when the magnetic force is increased; the force being proportional to the square of the speed of the needle. That is, if the needle in one position makes 10 vibrations in any given time, and in another position makes 12 vibrations in the same time, the magnetic force in the first position is to the magnetic force in the second position as 10^2 is to 12^2 .

It is convenient to measure the horizontal force and the vertical force separately. The horizontal force is measured by means of a flat and pointed needle, about three inches long. It has a jewelled cap at its centre, which works on a sharp pivot. It must be used in a covered box, or compass bowl, to protect it from the motion of the air. It is brought horizontal by a small weight, counterbalancing the dip, and so vibrated in the horizontal plane.

Horizontal force may also be measured by deflection. If a magnet be placed at right angles to the direction of the needle, the magnet will deflect the needle through a certain angle, depending upon the strength of the magnet, compared with the horizontal force. The smaller the force, the larger the angle of deflection of the needle, the force being as the cosine of the angle of deflection. Or the deflecting magnet may be moved round, and kept at right angles to the compass needle, and the horizontal force measured by the maximum deflection the magnet is capable of producing, when thus applied.

Vertical force is measured by means of a Dip Circle. This is an instrument having a flat pointed needle, with an axle passing through its centre of gravity, about which it can rotate in a vertical plane; the axle being supported at the centre of a graduated circle. If the circle is placed in the vertical plane of the magnetic force, the needle will stand in the direction of that force, showing the dip, if it be acted on by the earth's force only. A small weight placed on the upper arm of the needle, bringing it horizontal, will be a measure of the vertical force.

If the circle is placed at right angles to the plane of the magnetic force, the needle will hang vertically, where there is any vertical force, and in this position may be vibrated, so as to measure that force.

Measuring either horizontal or vertical force by vibration, the initial arc should be the same, in any positions wherein it is desired to compare those forces. The effects of friction, and the resistance of the air, are to cause the needle to take a little more

time, in going through the larger arcs than the smaller, and ultimately to bring it to rest. The smallest arcs which can be conveniently used give the best results.

235. Studying the phenomena of the pointing of the magnetised needle on the earth's surface, and comparing them with the effects of one magnetised needle, or steel bar, on another magnetised needle, or steel bar, the conviction gradually gained ground, that the earth is, or has the properties of, a large magnet. Those properties are two. First, Attraction and Repulsion: the property by which one magnet will attract and repel another, according to definite laws. Second, Induction: the property by which a magnet can impart magnetism, and so convert into a magnet any piece of iron or steel, either by contact or mere proximity.

The property of attraction and repulsion may be shown, by bringing two compass cards near to each other. The north part of one card will push away or repel the north part, and attract or draw towards it the south part, of the other. The ends of magnets are called poles, and we express the law of attraction and repulsion by saying, like poles repel, and unlike poles attract, each other.

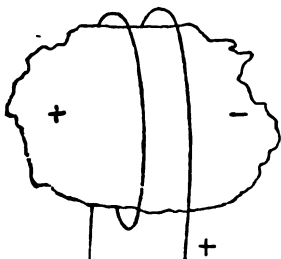
This attraction and repulsion may be due to two different kinds of magnetism in the poles, or to an excess of magnetism in one pole as compared with the other, or it may be a magnetic state, depending upon neither one cause nor the other. It will be convenient to speak of the magnetic state of the north pole of the compass needle as positive, indicating it by the sign +, and of that of the south pole as negative, indicating it by the sign —.

The pointing of the magnetised needle appears to be, the direction it takes up in obedience to the law of attraction and repulsion existing between it and the larger magnet, the earth. Also, the increasing strength, with which the needle is found to point as the latitude increases, appears due to the approach to the magnetic poles of the earth.

By the law of induction, a magnet when brought near to any piece of unmagnetised iron, induces magnetism therein; the near pole of the magnet, and the proximate part of the iron, having magnetism of opposite kinds. The similar magnetism to that of the near pole of the magnet is found in a remote part of the iron. Applying this law to the earth as a large magnet, the magnetism of iron and iron structures is apparently due to induction from the earth, and the end or part of iron which is towards the north will have positive magnetism.

In dealing with the magnetism of iron ships, this property of induction, hitherto little thought about by seamen, becomes of great importance. The earth's magnetic force, by inducing magnetism in the iron of a ship, is the source of all magnetic disturbances of the compass.

236. The question as to how the earth became magnetised will perhaps come into the mind—possibly it is, or was, magnetised by induction, from some far distant cause. But magnetism may be induced by electricity. If an insulated wire is passed round a piece of iron, and the wire be considered as conveying an electric current flowing from positive to negative, the iron will become magnetised, and have positive and negative powers, as shown in the figure.



If the trade winds flowing round the earth from the eastward, be considered as acting as a positive electric current, the earth would be magnetised with a negative pole to the north, and a positive pole to the south. Whether it is thus magnetised or not, the idea will aid the memory as to the magnetic state of the earth, show how magnetic forces may be generated by electricity, and suggest the possibility of compass disturbance, by the increasing use of electricity on board ship.

237. All iron is capable of receiving magnetism by induction from the earth. If the iron remain a long time in the same position, or if it be hammered or subjected to mechanical violence, part of the induced magnetism will remain. That is, the iron will show polarity in the same parts, after it has been moved into another position, relatively to the line of the earth's force.

All magnetism, therefore, may be called induced magnetism. That which instantly passes away, when the inducing cause no longer acts, is called transient magnetism. That which remains for a longer or shorter time, is generally called permanent magnetism. The term permanent, in this extended sense, means all magnetism that is not transient. The terms trans-permanent, sub-permanent, and permanent, may be used to indicate increasing degrees of permanency, if desired. It is, however, a question whether anything is gained by thus multiplying terms, as no definite line of separation can exist.

Speaking generally, iron will receive or part with magnetism more or less readily, according as it is soft or hard. Hard iron or steel, when magnetised, will retain its polarity for a very long time.

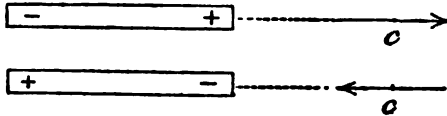
238. The disturbing effects of iron on a compass, being caused by magnetism induced in the iron by the earth's magnetism, the possibility of so placing iron about a compass on board ship as to counteract the effect of the iron of the ship, is the problem of compass adjustment.

Professor Barlow was the first to deal practically with compass adjustment, and the problem was subsequently completely solved by Professor Airy in 1839. That gentleman gave the results of his researches and experiments in the following words: 'By

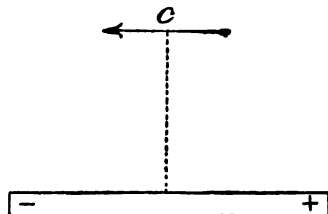
placing a magnet so that its action will take place in a direction opposite to that which the investigations show to be the direction of the ship's independent magnetic action, and at such a distance that its effect is equal to that of the ship's independent magnetism, and by counteracting the effect of the induced magnetism by means of the induced magnetism of another mass [according to rules which are given], the compass may be made to point exactly as if it were free from disturbance.' Briefly, this statement is to the effect, that the permanent magnetism of the ship may be counteracted by the permanent magnetism of steel magnets, and the transient magnetism of the ship by the transient magnetism of iron; the magnets and iron being placed near the compass, according to definite rules.

In order to be able to consider together, the disturbing effects of the iron of the ship on the compass, and the action of magnets and iron in counteracting the same, a brief explanation of the latter is necessary.

239. Magnets, when used to adjust a compass, are applied, generally, either end on, or, as it has been termed, broadside on. If a magnet be placed near a compass, so that the centre of the needle is in the line of the magnet, the effect of the magnet is to cause a force pushing away the north point of the needle, if the positive end of the magnet is presented, and drawing the north point of the needle towards the magnet, if the negative end is presented. In the figure, if c represent the centre of the compass needle, the arrows represent the direction of the force on its north end. This is called the end-on position of the magnet.



If a magnet be placed near a compass, so that the centre of the needle is in the same plane as the magnet, and on a line drawn from the middle of the magnet, perpendicular to its direction, the effect of the magnet is to cause a force parallel to itself, pushing the north end of the needle away from the positive end of the magnet. In the figure, if c be the centre of the compass needle, the arrow shows the direction of the force on its north end. This is sometimes called the broadside position of the magnet.



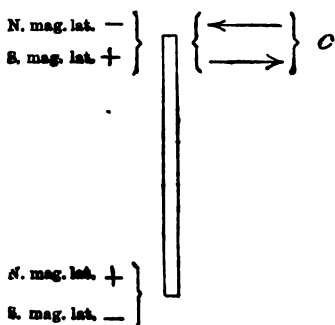
Magnets used for compass adjustment are made of hard steel, and well magnetised. Their magnetism may be considered as permanent. Thus, by means of a magnet, a permanent magnetic force can be produced, pushing the north end of the compass needle in any desired direction.

240. The iron used in adjusting compasses should be soft malle-

able iron, so that magnetism is readily induced therein by the earth's force, and readily parted with; that is, it does not become permanent.

It is used for two purposes. For one purpose, it is in the form of an upright bar, placed, generally, before or abaft the compass. For another purpose, masses of chain or scrap iron in boxes, cylinders, or spheres, are used. These are placed beside the compass, on the same level as the needle.

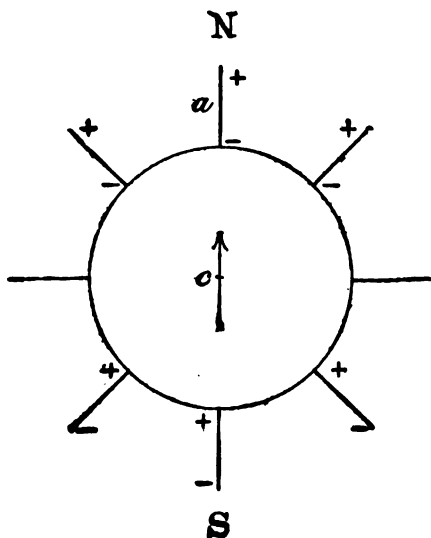
241. The action of the upright bar depends upon the earth's vertical force. In north magnetic latitude, the lower end has positive magnetism, and the upper end negative magnetism. On the magnetic equator the bar may be considered as unmagnetised. In south magnetic latitude, the lower end has negative magnetism,



and the upper end positive magnetism. Therefore a magnetic force in any direction can be produced, acting on the north end of the compass needle, varying in strength with the earth's vertical force, by placing the upper end of the bar in a suitable position. It is generally desired to make this force horizontal, as shown in the figure, where *c* is the centre of the compass needle. After Captain Flinders, R.N., who was the first to propose this, or, indeed, any mode of

counteracting the effect of the ship's iron on the compass, iron thus used is called a Flinders bar.

242. The action of iron placed beside a compass, is not



quite so simple as that of the Flinders bar. In the fig. let *c* be the centre of the compass needle, and the circle the outer circumference of the binnacle. Let *a* represent a horizontal iron rod, placed radially north of the centre of the compass. In this position it will be magnetised by induction from the earth—the north end of the rod with positive magnetism, and the south end with negative magnetism. It will cause no deflection of the needle, because the force is in the line of the needle. It will, however, increase the force with which the needle points.

Conceiving the rod to be moved round the needle to the right, as the spokes of a wheel move round its centre, it will be seen that the amount of magnetism in the rod will diminish as it goes round, till in the east position it may be considered as without magnetism. But as the rod leaves the north position, so the magnetic force of the rod, by being inclined to the needle at a greater angle, has a greater proportional effect in deflecting it. From the combined action of these two causes, the maximum deflection of the needle occurs when the rod is in the N.E. position.

Following the rod round, and noting the magnetism induced therein by the earth's magnetism, and the effect of the magnetic force, thus generated in the rod, in deflecting the needle, the following results will appear:—

Rod North or South of the centre of the needle. Increase of force, no deflection of the needle.

Rod N.E. or S.W. Increase of force, maximum easterly deflection of the needle.

Rod East or West. No effect on the needle.

Rod S.E. or N.W. Increase of force, maximum westerly deflection of the needle.

Thus it will be seen, that the effect of the rod is to cause a deflection of the needle, easterly and westerly in alternate quadrants, and to increase the mean magnetic force. It will also be seen, that the effect of two rods opposite to each other, is to double the effect of one.

243. Another instructive example of the effects of iron moving round a compass is that of a similar rod placed tangentially. Following the rod round, and noting the magnetism induced therein, and the effect thereof on the compass needle, as in the figure, the following results will be seen:—

Near end of the rod North or South of the centre of the needle. No effect.

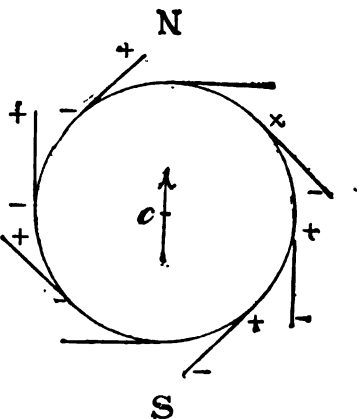
Near end of the rod N.E. or S.W. of the centre of the needle. Westerly deflection of the needle.

Near end of the rod East or West of the centre of the needle. Maximum westerly deflection of the needle.

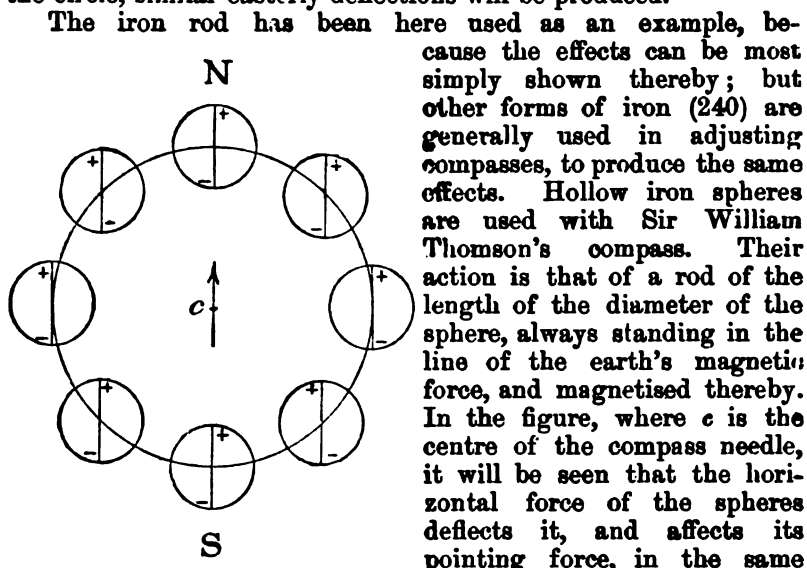
Near end of the rod S.E. or N.W. of the centre of the needle. Westerly deflection of the needle.

In this example, as in 242, the effect of two rods in opposite positions is to double the effect of one.

When two rods thus placed tangentially, having their near



ends at North and East, or in any positions 90° apart, revolve about the compass together, one rod will cause a maximum deflection of the needle, when the other rod has no effect thereon. As the effect of one rod increases, the effect of the other decreases; and the combined effect of the two rods, thus revolving together, is a constant westerly deflection of the needle. If the rods are placed in the opposite direction from their point of contact with the circle, similar easterly deflections will be produced.



manner as the iron rod in 242. When east and west of the centre, however, spheres diminish the directive force on the needle, more than the forms of iron commonly used.

Having briefly examined the means employed to counteract the ship's magnetic forces, the origin and effect of those forces, and the mode of applying the counteracting means, may now be considered.

244. An iron ship, in the course of construction, stands in the influence, or field as it is termed, of the earth's magnetism, and is consequently magnetised by induction. In north magnetic latitude, all upright iron structures, such as stern-post and frames, have positive magnetism in their lower ends, and negative magnetism in their upper ends. In south magnetic latitude, these conditions are reversed. In all latitudes, horizontal iron structures, such as beams and keel, have positive magnetism in their northern ends, and negative magnetism in their southern ends. The ship throughout is, in course of building, permeated with magnetism in the direction of the inducing force. Part of the magnetism thus acquired in building remains after the ship has been launched, causing a permanent magnetic force, in some direction in the ship.

This force tends to draw the north point of the compass towards that part of the ship which was south in building.

Besides this permanent magnetism, the ship, as she subsequently turns about with her head in different directions, takes up magnetism according to her varying positions. The amount of magnetism iron will thus receive by induction, within the limits of the change in the earth's force, varies as that force; the ends of beams, and other parts of the ship's structure, which are towards the north having positive magnetism, which changes and becomes negative when the direction of the ship's head is reversed. It is evident, however, that vertical iron will have magnetism which does not depend on the direction of the ship's head, but which will vary, in character and value, with the earth's vertical force only.

245. From these premises it will be seen, that there must be always a Constant force, and a Variable force, acting on the compass needle as the ship goes round. Therefore, if the direction and value of these forces are known, together with the law which governs the change in the variable force, the deviation of the compass could be found without swinging the ship. Generally, it is easier to deal with the deviation than with the forces which cause it; but a knowledge of the manner in which these forces act, facilitates very much the construction of a deviation table. Considering the commercial value of time, in all matters relating to shipping, this is a subject of no small importance.

246. It has been stated, that part of the magnetism acquired in building causes a constant force, in some direction, in the ship. The amount of deviation any force is capable of producing must decrease, as the force with which the needle points increases. Therefore, the deviation caused by the ship's permanent magnetism varies inversely as the earth's horizontal force.

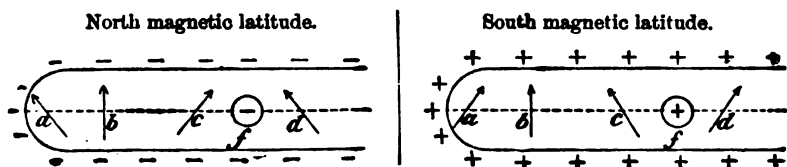
It is also clear, that, if the direction of the ship's permanent magnetic force is known, a permanent force by means of magnets (239) might be produced to counteract it; and if this magnetism of the ship, and of the magnets, were equally permanent, the adjustment would be perfect for all time and places.

The transient magnetism of vertical iron also causes a force which is constant in direction and value, as the ship goes round. This force, however, changes with change of place, as it depends on the earth's vertical force for its value. The liability of the needle to be deflected thereby varies inversely as the horizontal force. Therefore, the deviation caused by the transient magnetism of vertical iron will vary as,

$$\text{ver. force} \times \frac{1}{\text{hor. force}} = \tan. \text{ dip}$$

247. The following diagram will show how the compass is affected by the transient magnetism of vertical iron, and the manner in which Flinders' bar (241) counteracts that effect.

AFTER PART OF SHIP'S UPPER DECK. HEAD EAST.



In north magnetic latitude, the upper part of the ship's frames having negative magnetism, a compass in the position (a) would have its north point drawn to the westward. In south magnetic latitude, it would be drawn to the eastward. It is certain that no fixed magnet would meet this change. A Flinders bar, however, might be placed before the compass, so that its magnetism would exactly counteract that of the stern frames. The magnetism of the bar would change, exactly as that of the stern frames, when the ship went into south magnetic magnitude.

At a position (b), generally rather more than one-third of the distance between the stern and the funnel (f), the magnetism of the upper part of the boilers and funnel counteracts that of the stern frames, so that no bar is required.

At the position (c), the bar would be required abaft the compass; at the position (d), before the compass.

The position (b), when not otherwise objectionable, is chosen for the position of the standard compass in the Royal Navy. The position (d), being more convenient, is commonly used in the Mercantile Navy.

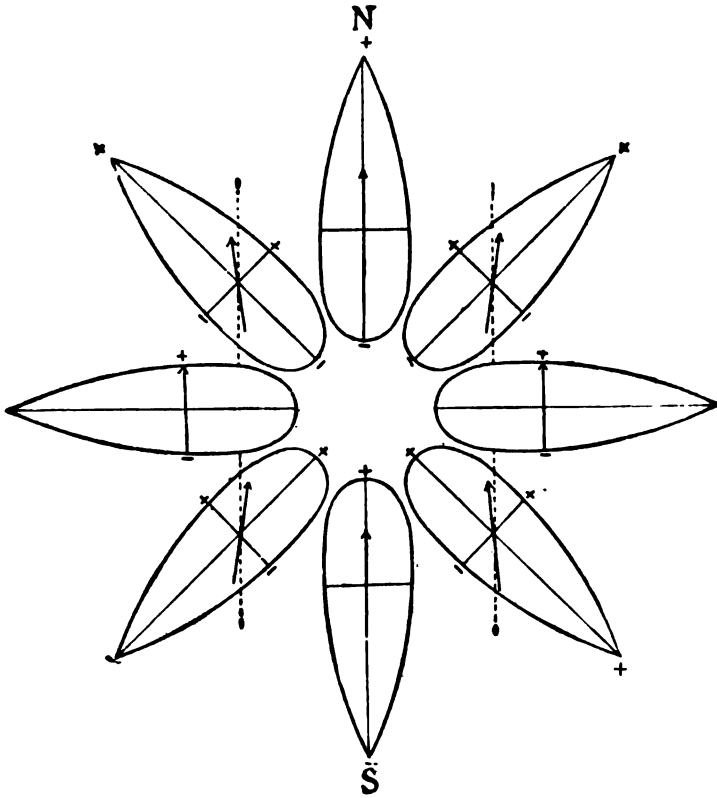
If a compass were placed out of the middle line, its north point would be drawn to the near side of the ship in north magnetic latitude, and repelled therefrom in south magnetic latitude. This effect would have its maximum value when the ship's head is north or south; and the Flinders bar must be towards the middle line, to counteract it.

248. The horizontal forces, from permanent magnetism and the transient magnetism of vertical iron, cause a deviation which is zero when the direction of the ship's head is such that the resultant of these forces is in the north and south line; and a maximum deviation when that resultant is in the east and west line. This deviation, from being easterly through one semi-circle, and westerly through the other, is called the Semicircular Deviation.

In correcting the semicircular deviation, such magnets as are commonly used should not be brought nearer than twice their length to the compass needles. And Flinders' bar should not be so near to the compass needles, or correcting magnets, as to receive magnetism by induction from them.

249. When the semicircular deviation has been got rid of, by

the means shown, there remains the deviation caused by the variable force. This force comes from the transient magnetism of horizontal iron; or, from the transient magnetism induced by the earth's horizontal force, in iron in any position. It causes a deviation which has four equidistant zero points, and is alternately easterly and westerly, in the intervening quadrants. It is for this reason called *Quadrantal Deviation*. The following diagram will show how it is caused, and why it takes that form.



Let the figures in the diagram represent the upper deck of a ship, in the several positions, and the fore-and-aft and thwartship lines thereon represent the horizontal magnetic axes of the ship, passing through the centre of the compass. Considering the magnetism of these axes to be positive in the ends presented to the north, it will be seen that, with the ship's head north, there will be no deviation; with the head N.E., the thwartship magnetism tends to deflect the needle to the right, while the fore-and-aft

magnetism tends to deflect it to the left. From the proximity of the poles of the thwartship magnetism, as compared with the poles of the fore-and-aft magnetism, the deviation is always easterly.

It is as well, however, for the student to recognise the possibility of its being westerly, as in the case of a very flat vessel, where the compass might be placed not much above the screw-shaft, or keel.

Following the vessel round in the several positions, it will be seen that there is a deviation, alternately easterly and westerly, having its zero points when the ship's head is on the cardinal points; and that there is always a diminution of the pointing force of the needle. No. 242 shows, that a quadrantal deviation of this kind could be corrected, and the pointing force of the needle increased, by placing iron on each side of the compass, directly athwartships.

The compass might be so placed, with reference to the iron about it, especially if it were out of the middle line of the ship, that the magnetic axes would be oblique in the ship. In that case, the zero points of the quadrantal deviation would not be at the cardinal points. No. 242 shows that any quadrantal deviation can be corrected, by placing iron beside the compass, at the same angle from the ship's head, as the zero points which have easterly quadrantal deviation on their left, are from the north point of the compass.

250. Besides the semicircular and quadrantal deviations, there is sometimes a residual deviation, which has the same value in whatever direction the ship's head may be, and is therefore called the Constant Deviation. No. 243 shows that if a compass were placed near iron, such as bulkheads, in somewhat the relative position of the corrector there shown, a positive or negative constant deviation might be caused, and that either one or the other can be corrected, by correctors placed tangentially.

251. Reverting to the force which is in some fixed direction in the ship, the deviation caused thereby must be the same in amount, but contrary in sign, when the ship's head is in opposite directions; or, when the deviation is small, in opposite directions by compass.

Looking at the cause of the variable force, whatever may be the position of iron about a compass, that force will be the same when the ship's head is in opposite directions. The deviation caused thereby will also be the same in amount, and have the same sign, when the semicircular deviation has been corrected, or is small.

These facts show how the deviation caused by the variable force may be separated from that caused by the constant force. Let the deviation on each point of the compass be tabulated in the following form:

Head	Deviation	Head	Deviation	Column I.	Column II.	Column III.
North	0 0	South	8 0 E.	0 0 E.	0 05 W.	0 57 E.
N. b E.	4 20 E.	S. b W.	8 30 E.	6 25 E.	2 0 W.	2 12 E.
N.N.E.	6 40 E.	S.S.W.	8 30 E.	7 35 E.	3 35 W.	2 0 E.
N.E. b N.	8 50 E.	S.W. b S.	7 40 E.	8 15 E.	4 25 W.	1 55 E.
N.E.	10 0 E.	S.W.	6 0 E.	8 0 E.	4 05 W.	1 57 E.
N.E. b E.	10 20 E.	S.W. b W.	3 10 E.	6 45 E.	2 50 W.	1 57 E.
E.N.E.	9 50 E.	W.S.W.	0 20 W.	4 45 E.	0 40 W.	2 02 E.
E. b N.	8 10 E.	W. b S.	3 50 W.	2 10 E.	1 40 E.	1 55 E.
East	7 0 E.	West	7 10 W.	0 05 W.	8 15 55 E.	
E. b S.	5 40 E.	W. b W.	9 40 W.	9 40 W.	Constant deviation } 2 0 E.	
E.S.E.	4 30 E.	W.N.W.	11 40 W.	3 35 W.		
S.E.E.	3 40 E.	N.W. b W.	12 30 W.	4 25 W.		
S.E.	3 40 E.	N.W.	11 50 W.	4 05 W.		
S.E. b S.	4 0 E.	N.W. b N.	9 40 W.	2 50 W.		
S.S.E.	5 30 E.	N.N.W.	6 50 W.	0 40 W.		
S. b E.	6 50 E.	N. b W.	3 30 W.	1 40 E.		

Take half the sum of the deviations, on each pair of opposite points, and insert it, with its proper sign, in column I. From what has gone before, this must be the deviation caused by the variable force, on each of the two points. That is, on the north and south points, there is 4° easterly deviation, on N. b E. and S. b W., $6^{\circ} 25'$ E., on N.N.E. and S.S.W., $7^{\circ} 35'$ E., from that force. So the deviation caused thereby can be ascertained on every point of the compass.

To find how much of column I. has the same value on every point, bring up its lower half into column II. Insert half the sum of the values in columns I. and II., with its proper sign, in column III. Each value in this column will be that of the mean of the deviation on four points 90° apart, and should be equal to each other, and to the mean constant deviation $2^{\circ} 0'$ E.

The deviation in column I., made up of the quadrantal and the constant deviations, has the same value in all parts of the world. Because, the disturbing force and the pointing force of the needle vary together, both depending on the earth's horizontal force. It also changes but little with time, losing about $\cdot 05$ of its value in a year, owing to the fact that iron slowly loses its capacity for receiving magnetism by induction. It may be worth noting here, that this quantity has nearly the same value, at compasses similarly placed, in ships nearly alike.

The correction by soft iron is also perfect for all time and places, if the magnetism of the correctors is derived from the earth's force only; but when the correctors are placed so near to compass needles, as to receive magnetism by induction from them, though it adds to their power as correctors, the correction is to that extent imperfect, the correctors having less effect when the horizontal force is increased. The soft iron correctors should on no account be less than the length of the needles, from their ends.

252. When a compass is placed on the upper deck, in the middle line of the ship, with the iron in about the same relative position on each side of it, and the usual height for taking bearings, the maximum quadrantal deviation is about 6° in a new iron ship. Its zero points are at the cardinal points, and there is no constant deviation. In compasses placed in very unfavourable positions, the constant deviation has amounted to 12° , and the quadrantal deviation to 24° , and possibly more.

It is not customary to correct the constant deviation by soft iron, as it occurs generally only in compasses not required for taking bearings. To meet it, the binnacle, or the compass in the binnacle, or the lubber-line itself, is so placed, that it points the value of the constant deviation, on the starboard bow, when positive, and on the port bow when negative. Thus, a course steered by a compass, having the lubber-line so placed, is unaffected by the constant deviation.

If the quadrantal and constant deviations were not corrected, or were only partially corrected, column I. (251), the sum of their values might be tabulated on each point of the compass, whenever opportunities occur of swinging the ship completely round. Bearing in mind what has been said (No. 251), this quantity should soon become very exactly known, leaving only the semicircular deviation to be ascertained.

253. The horizontal forces causing the semicircular deviation, are best considered as resolved in the fore-and-aft and in the athwartship directions. The fore-and-aft force causes a maximum deviation, when the ship's head is east or west. The athwartship force causes a maximum deviation, when the head is north or south. Looking at the deviation table (No. 251), and allowing for the value in column I., it is evident that in this case there is a force towards the ship's head, capable of producing a maximum deviation of $7^{\circ} 5'$, and that there is a force towards the ship's port side, capable of producing a deviation of 4° . Therefore, to adjust this compass, a force must be produced by magnets, or Flinders' bar, or both, towards the stern, leaving $5'$ westerly deviation on the east and west points; and towards the starboard side, leaving 4° easterly deviation on the north and south points. These residual quantities must be corrected by the means already explained, Nos. 249, 250.

Hence the law for correcting the semicircular deviation. Make the deviation zero on any two adjacent cardinal points. If it is known, or, from the position of the iron about the compass, suspected, that there is deviation on those points from the variable force, then the ship's head must be placed on the opposite cardinal points also, and half the deviation found thereon taken out.

254. The question naturally arises, as to how much of the semicircular deviation should be taken out by magnets, and how

much by Flinders' bar. At first, there is no other guide than the position of the compass (No. 247); but when a ship has gone into positions where there is much change in dip and horizontal force, a better judgment can be formed. At the magnetic equator, there can be no transient magnetism in vertical iron; all the semicircular deviation there found, must be caused by the ship's permanent force. Hence if, near the magnetic equator, the semicircular deviation be corrected by magnets, any deviation subsequently found, arising from change of place, should be corrected by Flinders' bar.

From the fact (No. 246) that one part of the semicircular deviation varies inversely as the horizontal force, and the other part as the tangent of the dip, the value of each of these parts can be ascertained, if the deviation is observed in two magnetic latitudes.

Example.—The steamship *Scotia*, having a standard compass in position *d* (No. 247), corrected by magnets in the Thames, soon after, in latitude 30° S., longitude 16° E., found 12° easterly deviation on the east point, and 10° westerly on the west point. How much of the deviation on those points should be corrected by Flinders' bar?

From map 232, and table 233:—

Thames, dip $67\frac{1}{2}^{\circ}$; Nat. tan. of dip 2.42 ; Hor. force $.48$.
 Lat. 30° S. } dip -51° , Nat. tan. of dip -1.24 ; Hor. force $.44$.
 Lon. 16° E. }

Let P = the deviation from permanent magnetism,
 and T = the deviation from transient magnetism of vertical iron.

$$(1) \text{ Thames } \quad \frac{P}{.48} + T \times 2.42 = 0.$$

$$(2) \text{ Lat. } 30^{\circ} \text{ S. } \left. \begin{array}{l} \text{Lon. } 16^{\circ} \text{ E.} \end{array} \right\} \frac{P}{.54} + T \times -1.24 = 11^{\circ} \text{ semicircular on east point.}$$

From (1) $P = -1.16 T$,
 substituting in (2) $-3.39 T = 11^{\circ}$ semicircular on east point.

$$\text{Therefore } T = -\frac{11^{\circ}}{3.39} = -3.25^{\circ} \text{ on east point.}$$

In the Thames $-3.25^{\circ} \times 2.42$ (the tan. of dip) $= -7\frac{1}{2}^{\circ}$.
 Lat. 30° S., Lon. 16° E. $-3.25^{\circ} \times -1.24$ (the tan. of dip) $= 4^{\circ}$.

Therefore, a Flinders bar should be placed before the compass, capable of deflecting the needle $7\frac{1}{2}^{\circ}$ in the Thames, and 4° at the southern position. These deflections, from the magnetism of the bar, will be in opposite directions, and will exactly correct the deviation caused by the transient magnetism of vertical iron. Clearly, the magnetism of the funnel, in this case, draws the north point of the needle aft, in north magnetic latitude; and forward, in south magnetic latitude. A convenient form of Flinders' bar is fitted to the binnacle of Sir Wm. Thomson's compass.

255. The value of the semicircular deviation, on the east or west point, is a key to the value of the deviation caused by the

force in the fore-and-aft line, on every point of the compass. Similarly, the value of the semicircular deviation, on the north or south point, is a key to the value of the deviation caused by the force in the thwartship line, on every point of the compass. As the deviation on any point is made up of that caused by the forces in these two directions, added to that caused by the variable force, it is evident, that if the latter be known (No. 252), and the semicircular deviation be ascertained on two adjacent cardinal points, the deviation table can be completed.

When the semicircular deviation is small, the following table will be useful for that purpose:—

Semicircular deviation on any cardinal point	Semicircular deviation caused by the same force, on each point, reckoned right and left from that cardinal point, through the adjacent quadrants							
	1st	2nd	3rd	4th	5th	6th	7th	8th
•	•	•	•	•	•	•	•	•
1	0 59	0 55	0 50	0 42	0 33	0 23	0 12	0 0
2	1 58	1 51	1 40	1 25	1 7	0 46	0 23	0 0
3	2 57	2 46	2 30	2 7	1 40	1 9	0 35	0 0
4	3 55	3 42	3 20	2 50	2 13	1 32	0 47	0 0
5	4 54	4 37	4 9	3 32	2 47	1 55	0 59	0 0
6	5 53	5 33	4 59	4 15	3 20	2 18	1 10	0 0
7	6 52	6 28	5 49	4 57	3 53	2 41	1 22	0 0
8	7 51	7 24	6 39	5 39	4 27	3 4	1 34	0 0
9	8 50	8 19	7 29	6 22	5 00	3 27	1 45	0 0
10	9 48	9 14	8 19	7 4	5 33	3 50	1 57	0 0

Example.—The deviation (table 251) having been observed to be 8° 0' E. on the south point, and 7° 10' W. on the west point, what is the deviation on the N.W. b W. point?

The semicircular deviation on the south point, allowing for the value in column I., must be 4° E. It is therefore 4° W. on the north point, and, from the above table, 2° 18' W. on N.W. b W., five points from north.

The semicircular deviation on the west point must be 7° 5' W., it is therefore 5° 53' W. on N.W. b W., three points from west. Therefore the whole deviation on N.W. b W. must be 2° 18' W. + 5° 53' W. + 4° 25' W. (the value in col. I.) = 12° 31' W.

The semicircular deviation being the same in amount, with contrary signs, on opposite points, the deviation on S.E. b E. is 8° 6' E. + 4° 25' W. = 3° 41' E. In the same manner, the deviation on every point of the compass can be estimated.

There may be circumstances where it would be convenient to ascertain the position of the correctors necessary to apply to a compass, by measuring hor. force (234). The most simple way of looking at the problem is, to consider a ship lying with her head in any known magnetic direction. By placing a horizontal magnet at right angles to the compass needle, and so keeping it, the needle may be made to stand in the direction of the magnetic

meridian. By placing another horizontal magnet in the line of the magnetic meridian, the force with which the needle points may be made equal to the force on shore. Thus, all the forces due to the ship's magnetism, may be counteracted with the ship's head in the one direction. But when the ship's head is moved round, the needle will move away from the magnetic meridian, by reason of the change in the variable force. When the head is in the opposite direction, the deviation will be nearly equal to twice that caused by the variable force, and the needle will point with a force which will differ from the horizontal force on shore, by twice the value of the component of the variable force in the direction of the needle, nearly.

Therefore, to counteract the force which causes the semicircular deviation, the distance of the magnets from the card must be so adjusted, that the needle points with the mean value of the force found with the ship's head in the two directions, and with half the deviation found in the second position.

Another way of dealing with the problem is suggested by considering the following facts. If the force with which the needle points is the same when the ship's head is east and west, there can be no constant force in the athwartship line. If it is the same when the ship's head is north and south, there can be no constant force in the fore-and-aft line. Therefore, when these conditions are fulfilled, there can be no semicircular deviation. Further, if the force is the same on the four cardinal points, there can be no quadrantal deviation.

Working by force is a more delicate operation than working by bearings, and, under the circumstances in which the seaman has generally to work, is scarcely capable of the same degree of accuracy. If advantage be taken of the known direction of docks, wharves, transit and other lines, there will be few occasions where it will be necessary to have recourse to measuring force. But with the two methods available, there should be no detention of ships in port for the purpose of compass adjustment.

256. Hitherto the effects of the vertical component of the ship's forces have not been considered, because a vertical force cannot deflect the compass-needle, right or left. But when a ship heels, a force previously vertical may be no longer so, and the position of the iron about a compass may be so changed, as to introduce a new magnetic force. The deviation, caused by this change in a ship's magnetic forces, is called the Heeling Error. To estimate or correct the heeling error with theoretical accuracy is not an easy problem; especially in certain positions in a ship, and with the semicircular deviation uncorrected. The following remarks must be considered as applying to a compass, in such a position as is usually selected for a standard compass, and having the semicircular deviation corrected. At a compass so situated, there will be a force upwards or downwards in the ship, caused by per-

manent magnetism. The value of this force will depend, mainly, upon the direction in which the ship was built, and the position of the compass in the fore-and-aft line. It may be counteracted by a magnet placed end on (239), and vertically below the centre of the compass. If it is not counteracted, it will, by coming partly on one side when the ship heels, draw the north point of the compass to one side or the other.

There will also be a force upwards or downwards in the ship, from the transient magnetism of vertical iron, depending for its value on the earth's vertical force, of which it is a constant fraction. This force, in north magnetic latitude, is that of a negative pole under the compass, changing to positive in south magnetic latitude, drawing the north point of the needle to the high side of the ship in the former case, and to the low side in the latter. This force evidently should not be counteracted by a fixed magnet, but by a bar of soft iron, having, in north magnetic latitude, negative magnetism in the end nearest to, and above, the compass. $\cdot 05$ of the earth's vertical force is about a mean value of the vertical force caused by induction therefrom; therefore, in correcting the heeling error by a vertical magnet, the vertical force of the earth and ship should be brought to about $1\cdot 05$ of the earth's vertical force, wherever the ship may be.

Sometimes the position of the funnel, or an iron mast, may be such, that its vertical transient magnetism counteracts that of the ship; this will probably be the case in a compass in such a position as *d* (247). Or it may be counteracted by putting the upper end of the Flinders bar, where one is used, above the level of the compass.

Looking at the magnetic condition of athwartship iron, such as beams, passing under the compass, when, from the ship heeling, it departs from the horizontal position, it is evident that the higher ends will have negative magnetism, drawing the north point of the compass-needle to the high side of the ship in north magnetic latitude. The reverse of this takes place in south magnetic latitude, therefore this force should not be counteracted by a fixed magnet.

If a soft iron bar were placed horizontally athwartship, on each side of the compass, the magnetism induced therein would, if they were of suitable size and distance from the compass needle, exactly counteract the magnetism induced in the athwartship iron of the ship. This condition is nearly fulfilled by soft iron so placed as to correct the quadrantal deviation, so that no separate corrector is required for this part of the heeling error.

Because the transient magnetism of horizontal fore-and-aft iron, below the compass, causes a vertical force which is zero when the ship's head is east or west, it is desirable to correct the heeling error when the ship's head is nearly on those points. Then, if the quadrantal deviation is corrected, and the vertical

force brought by a magnet to the same value as, or a little more than, the vertical force on shore, the heeling error will be practically corrected.

The forces which cause the heeling error, by drawing the north end of the needle to one side or the other, must have their maximum effect when the ship's head is north or south. When the ship is rolling, the north end of the needle being drawn to each side alternately, causes the card to be unsteady. This disturbance of the compass-card has probably been more trouble to the navigator, than the error produced by heel.

Thus, in dealing with compass deviation, there are two distinct problems: one, to ascertain its amount; the other, to get rid of it altogether. At first sight, one or the other of these processes appears unnecessary, and in the early days of iron ships some thought that, with a table of deviation, there was no need for correctors; others that, if the compass were corrected, there was no need for a table of deviation. Experience has long since shown that neither of these views was correct. Many iron ships could not be navigated unless the compass was, at least, partly corrected. On the other hand, though compasses are frequently so well adjusted as to be without deviation, there are small changes subsequently which cannot be safely disregarded, rendering a deviation table necessary.

Changes which are gradual can be met by the ordinary daily observations, which should never be omitted; but there are some changes which are sudden, against which the seaman must be on his guard. If a ship has been steering for some time on one course, she will acquire negative magnetism in the part of the ship towards the south. On first altering course, the north point of the compass is likely to be drawn, for a short time, towards that part of the ship which was previously south. This is especially the case in changing from courses near east or west to those near north or south. Of course, the same effects follow when a ship has been some time in dock.

Thin iron structures, such as funnels, funnel casing, or ventilating cowl, are liable to change their magnetic state from strains or concussion, and so affect the deviation of a compass placed near. Any shock or strain which causes iron to vibrate or bend, and so cause movement in its particles, facilitates magnetic change.

With the introduction of electric lighting on board ship, came a new form of compass disturbance. The magnetism of the large electro-magnets, in the dynamos at present used, may disturb a compass at the distance of sixty feet. Also, circling round the wires conducting electricity, and at right angles to their direction, is a magnetic force, going in one direction round the wire conducting the direct current, and in the opposite direction round the wire conducting the return current. Thus these forces counteract each other when the conducting wires

are together, but when they are separated cause a proportional disturbance to the compass.

The maximum value of this disturbance, for any speed of the dynamo, is apparent directly the dynamo is started at that speed. So, by starting and stopping the dynamo, with the ship's head on two adjacent cardinal points, and noting the effects, the value of the disturbance on every point of the compass can be ascertained. Table 255 will be useful for this purpose.

257. A method of measuring the effects of a ship's magnetic forces, in causing deviation, was introduced by the late Mr. Archibald Smith. He found that the deviation could be expressed, as in the following equation:—

$$\left. \begin{array}{l} \text{Deviation with ship's head on} \\ \text{any point} \end{array} \right\} = A + B \cdot \sin \zeta' + C \cdot \cos \zeta' + D \cdot \sin 2 \zeta' + E \cdot \cos 2 \zeta'.$$

The factors A, B, C, D, E, are called coefficients, and ζ' is the direction of the ship's head by compass, reckoned round the circle to the right. Therefore, in dealing with the equation, the seaman, who generally has to deal only with angles not greater than a right angle, must consider the sign of the direction of the head, as well as that of the coefficient, in each term.

A, the first term in the expression, is the value of the constant deviation (250). It may be found by taking the sum of the deviation on the four cardinal points, and dividing it by four.

B is the maximum value of the deviation caused by the force in the fore-and-aft line (253). It is + when the force is towards the ship's head, and - when towards the stern. It may be found by adding to the deviation on the east point, the deviation on the west point with its sign changed, and taking half that sum. Any constant force in the fore-and-aft line, which causes this deviation, must cause a deviation = $B \cdot \sin \zeta'$, the second term of the expression, on every point of the compass.

C is the maximum value of the deviation caused by the force in the athwartship line (253). It is + when the force is towards the ship's starboard side, and - when towards the port side. It may be found by adding to the deviation on the north point, the deviation on the south point with its sign changed, and taking half that sum. Any constant force in the athwartship line, which causes this deviation, must cause a deviation = $C \cdot \cos \zeta'$, the third term in the expression, on every point of the compass.

D is the mean value of the deviation on the inter-cardinal points, caused by the variable force (249). It may be found by adding to the deviation on the N.E. and S.W. points, the deviation on the S.E. and N.W. points with the sign changed, and taking the fourth part of that sum. A force varying regularly, and causing this deviation, must cause a deviation = $D \cdot \sin 2 \zeta'$, the fourth term of the expression, on every point of the compass.

E is the mean value of the deviation on the cardinal points,

caused by the variable force (249). It may be found by adding to the deviation on the north and south points, the deviation on the east and west points with the sign changed, and taking the fourth part of that sum. A force varying regularly, and causing this deviation, must cause a deviation $= E \cdot \cos 2\zeta'$, the fifth term of the expression, on every point of the compass. The existence of the E shows that the axes are oblique (249).

It is obvious that the foregoing statement of the effect of the forces in causing deviation is true only when each force is the only disturbing force on the needle; it is true enough when those forces are small: in that case the resulting deviation is also small, and the sum of the five terms is equal thereto; when the deviation is large, the coefficients must be determined with more exactness. With such deviations as are usually found, since the general adoption of compass adjustment, the method here given is sufficiently exact.

The student must not consider the coefficients as forces, or as in any way causing the deviation; they merely measure it, with more or less exactness. And by their means the parts of the deviation can be particularised, in speaking and in writing, and a record of its value kept in five terms, of which two are generally zero. Excepting for this purpose, the treatment of the subject by coefficients, especially laborious methods of determining their exact values, and of deriving the ship's magnetic forces therefrom, has never been greatly esteemed by navigators.

258. Professor Airy made use of the terms Red and Blue, to indicate the two kinds or states of magnetism, of the north and south ends of the compass needle respectively. These terms have been of great use, especially in making clear, by coloured diagrams, the distribution of magnetism in iron ships. The terms positive and negative have been used in this chapter, being in accord with the terms used in the kindred science of electricity, which is daily becoming of more importance to seamen.*

The subject of compass deviation and adjustment was thoroughly investigated by a body of scientific men, shipowners, and others, interested in the subject, called the Liverpool Compass Committee. The results of their labours were published, in language intelligible to seamen, in three most valuable reports to the Board of Trade, 1856, 1857, 1861.

* Professor (now Sir) George Biddell Airy, K.C.B., has lived to see his accurate and thoroughly practical method of adjusting compasses, devised half a century ago, overcome all opposition, and be now, and for many years past, universally adopted. He has in other ways furthered the science of navigation, but in facilitating the navigation of iron ships he is pre-eminent.

The following Notes are the result of recent theory and experience.

The numbers refer to Articles in the present edition.

Art. 215. The method of suspension by india-rubber has been discontinued, owing to its rapid deterioration when exposed to heat and wet.

216. In Lord Kelvin's (Thomson) compasses the outer graduation of the numerals is inverted in the Navigational or Standard Compass to enable the card to be read direct with the azimuth mirror. The average period of a Thomson's card varies from thirty seconds for a ten-inch card to thirteen and a half seconds for a four-inch one.

219. The Variation at Greenwich was (1899) $16^{\circ} 34'$ westerly, decreasing $7'$ annually.

220. The simultaneous appearance of auroras and disturbances of the magnetic needle (magnetic storms) are manifestations of the same cause. The late Father Secchi held that thunderstorms exercised a perceptible influence on the magnetic needle. The disturbing element of land on the compass needle is recognised to be submarine. Theory confirmed by experience show that if the rocks are the upper extremities of a ridge in north magnetic latitudes they would attract and in southern repel, the red (paragraph 239) end of a compass needle.

223. The prefix correct to true, magnetic and compass courses is being discontinued, a true course is a compass one corrected for variation and deviation; a magnetic course, the same corrected for deviation, and a compass course, one uncorrected for variation and deviation.

232. The Dip of the needle at Greenwich was (1899) $67^{\circ} 10'$, decreasing $1'7$ annually.

237. The expression, "magnetism by induction from the earth" is seldom used; the magnetism of both earth and soft iron are produced by the same lines of magnetic force.

239. To avoid ambiguity, the pole of a magnet that attracts the north-seeking end of the needle is called blue and the repelling one red, bearing in mind the pole in the north end of a compass needle is a true south pole, and that in the south end of a compass needle is a true north pole.

244. Read paragraph at 237. Gaussin error is often developed by magnetic induction in a ship's iron beams, more especially when proceeding east and west; in fast Atlantic liners a Gaussin error of 8° to 10° is not unusual during a voyage across the Atlantic.

249. A compass is usually corrected in the following order: the quadrantal error, the heeling error, and lastly the semi-circular error.

256. In merchant vessels arrangements are usually made to place

the navigational compass beyond the magnetic field of the dynamo, but the necessary arrangements in a man-of-war may prevent this being carried out. A compass if within the magnetic field of a dynamo will be disturbed, the error altering with change of azimuth.*

In the general type of dynamo supplied to H.M. ships, designed for 80 volts at the terminals, the minimum distance of a compass should be 60 feet from a 300-ampère machine, increased to 70 feet from a 400-ampère one. A 600-ampère machine being armour-clad and multipolar produces no disturbance on a compass 15 feet away. In the "Destroyers" the correction is made by an electro-magnet at the foot of the compass pedestal, with its poles reversed to those of the dynamo; in second class cruisers (*Apollo* class) by exciting the shunt coils of both dynamos, when only one is in use, the resulting disturbances are neutralised, provided the poles of the dynamos are symmetrical to the middle line.

In the electric lighting of a compass, the current is usually conveyed to a 16 c.p. lamp by a twin cable, protected by phosphor-bronze braiding. The best position is to place the lamp vertically above the axis of the compass needle; occasionally a disturbance arises from the inductive effect due to the current in the filament of the lamp itself.

A small electric light (half-candle power) is found useful for star azimuths at night or if fitted to a sextant for stellar observations.

* For detailed information see *The Mariner's Compass in an Iron Ship*, by Captain J. Whitley Dixon, R.N., sold by J. D. Potter, 146 Minories, London, E.

II. THE LOG AND GLASSES.

1. *The Log.*

259. The log consists of the *log-ship* and *line*. The log-ship is a thin wooden quadrant, of about five inches radius; the circular edge is loaded with lead, to make it float upright, and at each end is a hole. The inner end of the log-line is fastened to a reel, the other is rove through the log-ship and knotted; and a piece of about eight inches of the same line is spliced into it at this distance from the log-ship, having at the other end a peg of wood, or bone, which, when the log is hove, is pressed firmly into the unoccupied hole.

At ten or twelve fathoms from the log-ship a bit of buntin rag is placed, to mark off a sufficient quantity of line, called *stray-line*, to let the log go clear of the ship before the time is counted.

260. The log-line is divided into equal portions, called *knots*, at each of which a bit of string, with the number of knots upon it, is put through the strands.

The length of a knot depends on the number of seconds which the glasses measure, and is thus determined:

The No. of feet in 1 knot : No. of feet in 1 mile :: No. of seconds of the glass : 3600 (the No. of seconds in an hour).

The nautical mile being about 6080 feet,* we have, for the glass of 30 seconds, the knot = $\frac{6080 \times 30}{3600} = 50.7$ feet, or 50 feet 8 inches, for the glass of 28 seconds, the knot = $\frac{6080 \times 28}{3600} = 47.8$ inches, or 47 feet 4 inches; and so for any other glass.

261. The knot is supposed to be divided into eight equal parts, or fathoms (which they are very nearly). In the Royal Navy the knot is divided into tenths and the even fathoms only are reckoned, for the convenience of adding up the distance on the log-board.†

262. The log-line should be repeatedly examined, by comparing each knot with the distance between the nails, which are (or should be) placed on the deck for this purpose, at the proper distance. The line should be wet whenever it is required thus to remeasure it, or to verify the marks.

* The Geographical Mile is generally defined to be the length of a minute of arc in the earth's equator; but the Nautical Mile as defined by hydrographers is the length of a minute of the meridian, and is slightly different for every different latitude. (See Table 64A.) It is equal to a minute of arc in a circle, whose radius is the radius of the curvature of the meridian, at the latitude of the place.

† It is, of course, more systematic to divide the knot or mile into tenths, as in the Traverse Table, instead of eighths; but single tenths and fathoms may be used for each other without sensible error.

263. As the manner of heaving the log must be learned at sea, it is only necessary to remark, for reference, that the line is to be faked in the hand, not coiled; that the log-ship is to be thrown out well to leeward to clear the eddies near the wake, and in such a manner that it may enter the water perpendicularly, and not fall flat upon it; and that before a heavy sea the line should be paid out rapidly when the stern is rising, but when the stern is falling, as this motion slacks the line, the reel should be retarded.

264. (2) *Massey's Log* shews the distance actually gone by the ship through the water, by means of the revolutions of a fly towed astern, which are registered on a dial-plate. This log is highly approved in practice.*

265. When the water is shoal, and the set of the tides or current much affected by the irregularity of the channel, or other causes; and when, at the same time, either the ship is altogether out of sight of land, or the shore presents no distinct objects by which to fix her position, recourse may be had to the *ground log*. This is a small lead, with a line divided like the log-line; the lead remaining fixed at the bottom, the line exhibits the effect of the combined motion of the ship through the water, and that of the water itself, or the current; and therefore the course (by compass) and distance made good are obtained at once.†

Caution.—Logs, whether patent or common, are unsatisfactory instruments in these days of high speed. No patent log yet invented will stand the wear and tear of a fast ship for any length of time. To avoid this wear and tear they should be used only when coasting or in with the land. They will tell a different story in a head sea to what they do in a following sea. In slow steamers and sailing ships they are naturally more reliable. Still, logs must be used; but it must be remembered they are beset with *impediments*, and their indications must not be *implicitly* trusted in critical times.

By practice, seamen learn to estimate the rate of progress of the ship closely by the number of revolutions in a given time made by the engines; but this is only speed through the *water*; the sailor has to consider carefully what that *unstable* element has *also* been doing. ‡

Further, though ships may now better preserve a given course, and the distance run may be estimated more accurately than formerly, there are in modern iron ships elements of uncertainty about D.R. which still makes it perilous to close the land unless there are means of knowing with some certainty the ship's proximity thereto, especially where land has a bad reputation, as Ushant, C. Finisterre, C. Guardafui, Mocha I. in South America, &c.

* Other logs on this principle have since been invented and are in common use: notably, Walker's taffrail log. They should be well oiled, and stowed away clean.

† In numerous passages up and down the river Plate, where the above circumstances concur, Captain Gordon T. Falcon, in 1818-19-20, made constant use of this log.

‡ See Admiralty Current Charts, Tide Tables, and Sailing Directions, Nos. 951, 952.

266. (3) *The Glasses*.—The long glass runs out in 30^s or in 28^s; the short glass runs out in half the time of the long one.

When the ship goes more than five knots, the short glass is used, and the number of knots shewn is doubled.

267. The sand-glasses should frequently be examined by a seconds watch, as in damp weather they are often retarded, and sometimes hang altogether. One end is stopped with a cork, which is taken out to dry the sand, or to change its quantity.

268. When either the line or the glass is faulty, or when a line and glass not duly proportioned to each other are employed, the distance run is found as follows:—The number of feet in 1^h is to the number of feet run out in an observed number of seconds, as 3600 (seconds in an hour) are to the observed number of seconds.

Ex. Suppose 190 feet of line are run out in 22^s: required the rate.

The number of feet run out in 1^h: 190 :: 3600^s: 22^s; hence the number of feet

$$= \frac{190 \times 3600}{22} = 31090 \text{ feet; which, divided by 6000 (as near enough), gives 5.2 miles.}$$

CHAPTER III.

THE SAILINGS.

I. PLANE SAILING, WITH TRAVERSE, CURRENT, AND WINDWARD SAILINGS. II. PARALLEL SAILING, WITH MIDDLE LATITUDE, AND MERCATOR'S SAILINGS. III. GREAT CIRCLE SAILING.

269. IN considering the place of a ship at sea, with reference to any other place which she has left, or to which she is bound, these five things are involved: the Course, Distance, Difference of Latitude, Departure, and Difference of Longitude.

270. In practice these two general questions occur.

1st. The course and distance from one place in given latitude and longitude to another are given, and it is required to find the latitude and longitude of the other place.

2d. The latitudes and longitudes of two places are given, and it is required to find the course and distance from one to the other.

The methods of solution, that is, the rules of calculation, by which the answers to such questions are obtained, are commonly termed SAILINGS.

I. PLANE SAILING.

271. In Plane Sailing, as the term implies, the path of the ship is supposed to be described on a plane surface.

If the ship sails 1 mile on a given course, she makes a certain D. lat. and Dep.; in sailing a second mile, on the same course, she

makes good the same D. lat. and Dep. as before. Thus the D. lat. and Dep. for 2 miles of Dist. are twice those for 1 mile; for 3 miles of Dist. they are three times those for 1 mile, and so on; that is, the total D. lat. and Dep. made good are proportional to the Dist. on the sphere as they would be on a plane. Plane Sailing, accordingly, treats of the relations of the Course, Dist., D. lat., and Dep., and applies to right-angled triangles generally.

But each mile of Dep. which the ship makes good corresponds to a Diff. of Long. which is different according to the latitude in which the ship moves (Note, p. 58), that is, there is no *constant proportion* between the Dep. and Diff. Long. in two different latitudes, and therefore a question in which Diff. Long. is concerned is not within the province of Plane Sailing, except the case in which the ship is on or near the equator, where Dep. and D. Long. are the same thing.

272. (1.) The proportions, No. 162, p. 46, as adapted to the figures, No. 200, p. 59 (or to the third figure of No. 163, where the course is the angle ABC), give the proportions or *canons*, as they are called, of Plane Sailing. We employ the following:

$$\begin{array}{llll}
 \text{Dist. : Dep.} & :: \text{rad. (= 1) : sin. Co.,} & \text{whence, Dep.} & = \text{Dist.} \times \text{sin. Co.} & (1.) \\
 \text{Dist. : D. Lat.} & :: & 1 : \text{cos. Co.,} & \text{D. Lat.} & = \text{Dist.} \times \text{cos. Co.} & (2.) \\
 \text{D. Lat. : Dep.} & :: & 1 : \text{tan. Co.,} & \text{Dep.} & = \text{D. Lat.} \times \text{tan. Co.} & (3.) \\
 & & & \text{and tan. Co.} & = \frac{\text{Dep.}}{\text{D. Lat.}} & (4.) \\
 \text{D. Lat. . Dist.} & :: & 1 : \text{sec. Co.,} & \text{Dist.} & = \text{D. Lat.} \times \text{sec. Co.} & (5.) \\
 & & & \text{and sec. Co.} & = \frac{\text{Dist.}}{\text{D. Lat.}} & (6.)
 \end{array}$$

(4.) These equations put into logarithms by the rules Nos. 64 and 85, p. 20, become

$$\begin{array}{llll}
 \text{Log. Dep.} & = \text{log. Dist.} & + \text{log. sin. Co.} & - 10 & (1.) \\
 \text{Log. D. Lat.} & = \text{log. Dist.} & + \text{log. cos. Co.} & - 10 & (2.) \\
 \text{Log. Dep.} & = \text{log. D. Lat.} & + \text{log. tan. Co.} & - 10 & (3.) \\
 \text{Log. tan. Co.} & = \text{log. Dep.} + 10 & - \text{log. D. Lat.} & & (4.) \\
 \text{Log. Dist.} & = \text{log. D. Lat.} & + \text{log. sec. Co.} & - 10 & (5.) \\
 \text{Log. sec. Co.} & = \text{log. Dist.} + 10 & - \text{log. D. Lat.} & & (6.)
 \end{array}$$

Which logarithmic equations contain the rules employed.
On ordinary occasions four places are enough.

Case I. Given the course and distance, to find the difference of latitude and departure.

Ex. 1. A ship sails N.W. by N. 03 miles from lat. $49^{\circ} 30' \text{ N.}$; find the D. Lat. and Dep. and also the Lat. in.

273. *By Inspection.* Open Table 2 at 3 Points,* and against the Dist. 108 stand D. Lat. 85.6 and Dep. 57.2.

Then 85.6 or $1^{\circ} 25.6$ added to $49^{\circ} 30'$ gives Lat. in $50^{\circ} 55.6 \text{ N.}$

* Whenever the course is given in points or divisions of a point, it must be turned into degrees (213) before entering Traverse Table 1.

274. *By Computation.* (1.) For the D. Lat. To the log. cos. of the Course (Table 68) add the log. of the Dist. (Table 64); the sum (rejecting 10 from the index) is the log. of the D. Lat.

(2.) For the Dep. To the log. sine of the Course add the log. of the Dist.; the sum (rejecting 10) is the log. of the Dep.

Ex. above. Course 3 points, Dist. 103.

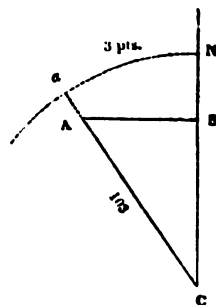
3 points, or $33^{\circ}45'$	log. cos. 9.9198
Dist. 103	log. 2.0128
D. LAT. $85^{\circ}6'$	log. 1.9326

(This is the Canon (2.) in No. 272.)

Course $33^{\circ}45'$	log. sin. 9.7447
Dist. 103	log. 2.0128
DEP. $57^{\circ}2'$	log. 1.7575

(This is the Canon (1.) in No. 272.)

275. *By Construction.* Draw a line CN towards the north for the meridian. From the centre C, with the chord of 60° as radius, describe an arc on the west side of CN, and lay off the chord of three points, or $33^{\circ}45'$ to *a* (No. 107). Through *a* draw *Ca*, this gives the angle N *Ca* equal to the Course, or three points; lay off from *a* scale of equal parts CA equal to the Dist. 103; draw AB perpendicular to CN, then CB will shew on the same scale the D. Lat. $85^{\circ}6'$, and AB the Dep. $57^{\circ}2'$.



Ex. 2 A ship sails S. 72° W. 216 miles from lat. $14^{\circ}11' N.$: required the D. Lat. and Dep., and also the Lat. in.

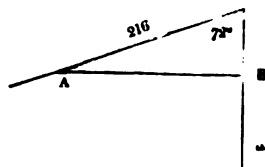
By Inspection. The Course 72° and Dist. 216 give D. LAT. $66^{\circ}7'$ and DEP. $205^{\circ}4'$. Then $66^{\circ}7'$, or $1^{\circ}6'7''$, subtracted from $14^{\circ}11' N.$ leaves Lat. in $13^{\circ}4'3'' N.$

By Computation.

Course 72°	log. cos. 9.4900
Dist. 216	log. 2.3345
D. LAT. $66^{\circ}7'$	log. 1.8245

Course 72°	log. sin. 9.9782
Dist. 216	log. 2.3345
DEP. $205^{\circ}4'$	log. 2.3127

By Construction. Draw a line CS to the southward for the meridian. By the chord of 60° lay off the arc 72° to the westward, and draw CA equal to 216; draw AB perpendicular to CS, then CB is the D. Lat. $66^{\circ}7'$, and AB the Dep. $205^{\circ}4'$.



These two examples of construction are sufficient for all varieties of Case I. When the course is to the eastward, CA is drawn on the right side of the meridian CN or CS instead of the left side.

Case II. Given the course and difference of latitude, to find the distance and the departure.

Ex. 1. A ship sailing W.S.W. makes 47 miles D. Lat.: find the Dist. run and the Dep.

276. *By Inspection.* Enter Table 1 with the Course 6 points look in the D. Lat. column for 47; the nearest to 47 is $47^{\circ}1'$, against which stand the Dist. 123 and Dep. 113.6.

The Lat. of the ship is, from the nature of the case, already given.

277. By Computation. (1.) For the Dist. To the log. sec. of the Course add the log. of the D. Lat.; the sum (rejecting 10) is the log. of the Dist.

(2.) For the Dep. To the log. tan. of the Course add the log. of the D. Lat.; the sum (rejecting 10) is the log. of the Dep.

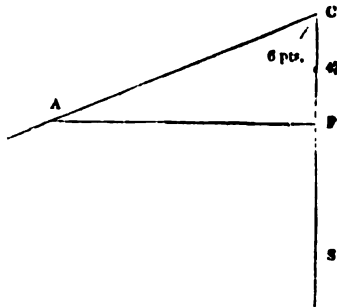
6 points, or $67^{\circ} 30'$	log. sec. 0.4172
D. Lat. 47	log. 1.6721
Dist. 122.8	log. 2.0893

(This is the Canon (5.) in No. 272.)

Course $67^{\circ} 30'$	log. tan. 0.3828
D. Lat. 47	log. 1.6721
Dep. 113.5	log. 2.0549

(This is the Canon (3.) in No. 272.)

278. By Construction. Draw the meridian line CS; lay off the course, or angle SCA, 6 points (No. 107); from C lay off CB the D. Lat. 47; draw BA perpendicular to CS, then CA is the Dist. and AB the Dep.



This example will suffice for all varieties of Case II. When the course is to the northward, CN is drawn upwards instead of CS downwards; and

when the course is to the eastward, CA is to be drawn on the right side of the meridian instead of the left side.

Ex. 2. A ship sails N. 54° E. and makes 119 miles D. Lat.: required the Distance run and the Departure.

By Inspection. Course 54° in Table 1, and D. Lat. 119.3, give the Dist. 203 and Dep. 164.2, nearly enough in practice.

Case III. Given the difference of latitude and departure, to find the course and distance.

Ex. A ship makes 91 miles northing and 34.7 Dep. (easting): find her Course and Distance.

279. By Inspection. Look in Table 1 for 91 in the D. Lat. column, and 34.7 in the Dep. column; the nearest are 90.6 and 34.8, which give the Course 21° (N. 21° E. in this example) and Dist. 97 miles.

280. By Computation. (1.) For the Course. From the log. of the Dep. (adding 10 to its index if necessary) subtract the log. of the D. Lat.; the remainder is the log. tan. of the Course.

(2.) For the Dist. Find the Course; then to the log. sec. of the Course add the log. of the D. Lat.; the sum is the log. of the Dist.

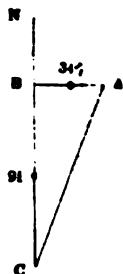
Ex. Dep. 34.7	log. 1.5403
D. Lat. 91	log. 1.9590
Course $20^{\circ} 52'$	log. tan. 9.5813

(This is the Canon (4.) No. 272.)

Course $20^{\circ} 52'$	log. sec. 0.0295
D. Lat. 91	log. 1.9590
Dist. 97.4	log. 1.9885

(This is the Canon (5.) No. 272.)

281. *By Construction.* Draw the meridian CN . Take CB , the D. Lat. 91, and through B draw BA perpendicular to CN , and equal to 34.7; join CA ; then BCA , the Course, measures 21° (No. 106, 2), and CA , the Dist. measures 98.



This example will suffice for all varieties of the case.

Case IV. Given the distance run and the difference of latitude, to find the course and departure.

Ex. A ship sails 101 miles between south and east, and makes 52 miles D. Lat. : find the Course and Dep.

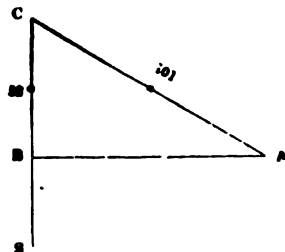
282. *By Inspection.* In Table 1, 101 in the Dist. column, and 52 in the D. Lat. column, occur over Course 59° (S. 59° E. in this example), and against the Dep. 86.6.

283. *By Computation.* (1.) For the Course. From the log. of the Dist. subtract the log. of the D. Lat. ; the remainder is the log. sec. of the Course.

(2.) For the Dep. Find the Course ; then to the log. sine of the Course add the log. of the Dist. ; the sum is the log. of the Dep.

Ex. Dist. 101	log. 2.0043	Course $59^\circ 1'$	log. sin. 9.9331
D. Lat. 52	log. 1.7160	Dist. 101	log. 2.0043
Course $59^\circ 1'$	log. sec. 0.2883	Dep. 86.6	log. 1.9374
(This is the Canon (6.) No. 272.)		(This is the Canon (1.) No. 272.)	

284. *By Construction.* Draw the meridian CS . Take CB , the D. Lat. 52, and through B draw BA perpendicular to CS . From C as centre, with the Dist. 101 as radius, describe an arc cutting BA in A ; then the Course, SCA , measures 59° , and BA , the Dep., measures 86.6.



This one example of construction will be sufficient.

Examples for Exercise.

Ex. 1. A ship sails from Flamborough Head, in $54^\circ 7' N.$, E. by N. $\frac{1}{4} N.$ 264 miles : required her Lat. in, and Dep.

Ans. D. LAT. $76.6 N.$, LAT. IN, $55^\circ 24' N.$; DEP. 252.6.

Ex. 2. A ship from Lat. $49^\circ 57' N.$ sails S.W. by W. 244 miles : required her Lat. in, and Dep.

Ans. LAT. IN $47^\circ 41' N.$; DEP. 202.9.

Ex. 3. A ship sails S.E. by E. from Lat. $1^\circ 45' N.$, until she arrives in Lat. $0^\circ 31' S.$: required her Dist. and Dep.

Ans. DIST. 244.8 ; DEP. 203.5.

Ex. 4. A ship from St. Helena in Lat. $15^\circ 55' S.$ sails N.W. $\frac{1}{4} W.$ till she is in Lat. $13^\circ 1' S.$: find the distance she has run, and the Dep.

Ans. DIST. 274.3 ; DEP. 212.

Ex. 5. A ship makes 135 miles northing, and 87.7 miles of Dep. westing : required her Course and Dist. made good.

Ans. COURSE N. $33^\circ W.$; DIST. 161 miles.

Ex. 6. A ship sails 210 miles between N. and E., and makes $160^{\circ}9'$ D. Lat. : find the Course and Dep.
 Ans. COURSE N. 40° E.; DEP. 135 miles.

Ex. 7. A ship sails 244 miles between S. and W., and makes $136'$ D. Lat. : find the Course and Dep.
 Ans. COURSE S. $56^{\circ}8'$ W.; DEP. $207^{\circ}6'$.

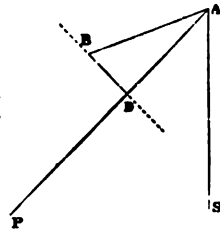
1. Resolution of one Course upon another.

285. It is sometimes required to resolve the distance run upon a given course into the distance upon a proposed course.

Ex. A ship is making good S. 70° W. $5\frac{1}{2}$ miles an hour : at what rate is she nearing a port bearing S.W. ?

Draw the meridian, A S, of the ship at A. Lay off the bearing of the port, S.W., and the Course S. 70° W., and take A B to represent the rate per hour (or for a smaller interval), as $5\frac{1}{2}$ knots. B then is the place of the ship at the end of this interval.

The distance, A P of the port, being very great, as compared with A B, a circle B D, described from P as a centre, is nearly a right line, and perp. to A P, and cuts off A D, the dist. by which the ship has neared P in an hour. Now A D is the D. Lat. to the Dist. A B, and the angle B A D as Course. B A D equal to $70^{\circ} - 45^{\circ}$, or 25° , and Dist. $5\frac{1}{2}$, give A D equal to 5 knots, the rate required, and A D is A B resolved in the direction A P.



When the number of degrees between the given and proposed courses exceeds 90 , the ship is increasing her distance from the port instead of closing it.

It is proper to observe, that the change in the distance of the port, made by the ship when not steering directly for it, is true only for its present bearing, and therefore holds only for a short time.

2. Traverse Sailing.

286. This is a variety of plane sailing in which the ship makes two or more courses in succession.

The process of reducing several courses, with the distances run on each, to the single course and distance which the ship would have made good if she had sailed at once from the place she first left, to the place at which she last arrived, is called *working a traverse*.

287. To work a Traverse. (1.) Draw six vertical lines. Head the space to the left Courses, the first column Distances, the next two columns D. Lat.; marking the first N. and the second S.; head the last two columns Dep., marking one E. and the other W. This forms a skeleton Traverse Table.

(2.) Set down the Courses, and the Distances against them, in order; look out in Table 1, the D. Lat. and Dep. to each Course and Distance. When the ship makes northing (that is, when the Course has an N. in it), set the D. Lat. in the N. column, otherwise in the S. column. When the ship makes easting (that is, when the Course has an E. in it), set the Dep. in the E. column, otherwise in the W. column.

(3.) Add the D. Lats. in each column; write the lesser of the two sums under the greater, and take their difference. Do the same with the Departures.

(4.) These differences are the D. Lat. and Dep. made good on the whole, and each takes the name of the column it stands in.

The course and distance are then found by No. 279.

It may be advisable for a beginner, before he proceeds to take out the quantities from the Traverse Table, to write a *dash* in all places *not* to be occupied by a D. Lat. or a Dep., in order to avoid writing a quantity in the wrong column. The first example only is thus marked, because such helps are useless to an expert computer.

Ex. A ship sails S.W. by S. 24 miles; N.N.W. 57 miles; S.E. by E. $\frac{1}{2}$ E. 84 miles; and South 35 miles: find the Course and Distance made good.

Courses	Dist.	D. Lat.		Dep.	
		N.	S.	E.	W.
S.W. by S.	24	—	20°0	—	13'3
N.N.W.	57	52°7	—	—	21'8
S.E. by E. $\frac{1}{2}$ E.	84	—	39°6	74°1	—
South.	35	—	35°0	—	—
		52°7	94°6	74°1	35°1
			52°7	35°1	
			41°9	39°0	

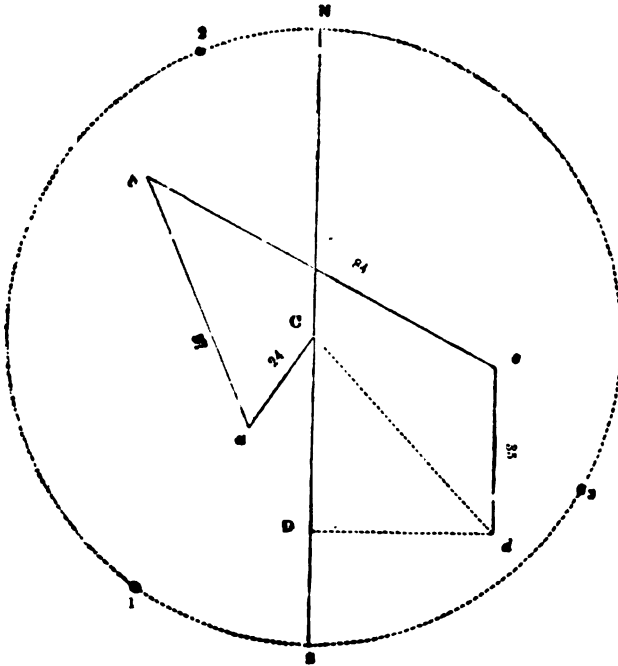
The D. Lat. 41°9 and Dep. 39°0, are found at 43° against the Dist. 57. Hence, since the ship has by the Traverse Table made southing and easting upon the whole, the COURSE is S. 43° E., and DIST. 57 miles.

By Computation. Each portion of the process having already been separately considered in plane sailing, nothing remains to be added here.

288. *By Construction.* With the chord of 60 describe a circle; draw the meridian NS, and mark the centre C. By means of the scale of chords lay off S 1, equal to 3 points, or S.W. by S., for the first course. Lay off N 2, equal to 2 points, or N.N.W., for the second course. Lay off S 3, equal to 5½ points, or S.E. by E. $\frac{1}{2}$ E., for the third course. The fourth course, or south, is already laid off, being on the meridian.

Now lay the edge of the ruler on C and on the point 1, and lay off by the compasses, or a scale of equal parts, the first distance, Ca, 24. Place the edge of the ruler on a, laying it parallel to the line joining C and the point 2, and lay off the second distance, ab, 57. Place the ruler on the point b, laying it parallel to the line joining C and the point 3, and lay off the third distance, bc, 84. Lay the ruler on c, parallel to the meridian, and lay off cd, the fourth distance, 35. The point d is therefore the place at which the ship has arrived. Join Cd, then SCd is the course, 43°, and Cd the distance, 57. Also, drawing Dd perpendicular to CS, gives

DC the D. Lat., and Dd the Dep. which will be found to measure 41.9 and 39.0.



The circle is here drawn outside the traverses altogether, without regard to the dimensions of the scale of chords, merely to shew the process more clearly.

This example, after the practice which the learner will have already had in drawing the figures in the preceding articles, will be sufficient for any case that may occur.

Ex. 2. A ship sails N.N.E. 11 miles; N.E. $\frac{3}{4}$ E. 39 miles; E. $\frac{1}{2}$ N. 14 miles; West, 10 miles; N.N.W. 4 miles: required the Course and Distance made good.

Courses	Dist.	N.	S.	E.	W.
N.N.E.	11	10°2		4°2	
N.E. $\frac{1}{2}$ E.	19	23°2		31°3	
E. $\frac{1}{2}$ N.	34	1°4		13°9	
West.	19				19
N.N.W.	4	3°7			1°5
		38°5	0	49°4 20°5	20°5
				28°9	

The D. Lat. 38.5 in the N. col., and Dep. 28.9 in the E. col give COURAGE N. 37° E., Dist. 48 miles.

289. The D. Lat. made good on the whole, as thus found, being applied to the Lat. left, gives the Lat. in. Thus, suppose in the above example the ship left Lat. $38^{\circ} 40' S.$; then $38^{\circ} 5$ northing places her in Lat. $38^{\circ} 1' 5 S.$ *

Examples for Exercise.

- Ex. 1. A ship from Cape St. Vincent, in lat. $37^{\circ} 3' N.$, sailed E.S.E. 45 miles, S.W. by W. 43 miles, S.E. by S. 64 miles, and N.N.E. 22 miles: find the Course and Distance made good, and also her Latitude in.
Ans. COURSE S. $34^{\circ} E.$; DIST. 89 miles; LAT. IN $35^{\circ} 49' N.$
- Ex. 2. A ship from Cape Amber (N.E. extremity of Madagascar), in lat. $11^{\circ} 5' S.$, sailed as follows:—S.S.E. $\frac{1}{4} E.$ 33 miles, S.W. by W. 40 miles, S.E. by S. 44 miles; N. 36 miles, S.W. by S. 44 miles, S.E. by E. 40 miles, S.S.W. $\frac{1}{4} W.$ 33 miles: required the Course and Distance made good, and also what Latitude she is in.
Ans. COURSE due South; DIST. 140 miles; the LAT. IN is $14^{\circ} 17' S.$
- Ex. 3. Yesterday, at noon, we were in lat. $28^{\circ} 34' N.$, and since then we have sailed N.E. $\frac{1}{4} E.$ 62 miles, N. by E. 16 miles, E. $\frac{1}{4} N.$ 40 miles, N.E. $\frac{3}{4} E.$ 29 miles N. by W. 30 miles, and N. $\frac{1}{4} W.$ 14 miles: what Course and Distance have we made good, and what is our present Lat.?
Ans. COURSE N. $43^{\circ} E.$ or N.E. $\frac{1}{4} N.$; DIST. 158 miles; LAT. IN $30^{\circ} 29' N.$
- Ex. 4. Yesterday, at noon, we were in lat. $44^{\circ} 10' N.$, and since then we sailed the following courses (all true): S. $69^{\circ} W.$ 4 miles, S. $58^{\circ} E.$ 15 miles, S. $66^{\circ} E.$ 8 miles, S. $65^{\circ} W.$ 12 miles, S. $1^{\circ} E.$ 6 miles, S. $55^{\circ} W.$ 2 miles, N. $21^{\circ} E.$ 2 miles, S. $55^{\circ} W.$ 23 miles, S. $32^{\circ} E.$ 14 miles, S. $55^{\circ} W.$ 4 miles: find what Course and Distance the ship has made good, and what is her present Lat.
Ans. COURSE S. $15^{\circ} W.$; DIST. 550 miles; LAT. IN $43^{\circ} 17' N.$

3. Current Sailing.

290. A current is named after the point *towards* which it runs or *sets*: thus, a current setting towards S.E. is called a south-east current. The mode adopted in speaking of the wind, which is named according to the point *from* which it blows, is thus reversed in speaking of a current.†

The term *set*, which is used to describe the direction of the current, is employed in the same way as in taking a bearing (No. 201); but it is necessary for the complete description of the current to state also its *drift*, that is, the distance through which the ship is carried or driven by its action.‡

291. When the rate of a current per hour is known, the drift for any number of hours is found by multiplying the rate by the number of hours.

In like manner, when the drift in a number of hours has been

* The beginner will proceed now to parallel sailing, because, though current sailing be strictly a branch of plane sailing, yet some of the examples, for the convenience of arrangement, involve the consideration of longitude.

† It is easy to conceive that people would name a wind according to the quarter it blows from, as bringing heat or cold, rain, &c., and a current according to the quarter to which it carries them.

‡ These terms have not in general been employed with sufficient precision. The term "drift" has been defined as the distance run per hour, or rate of the current. But as a second term for rate is superfluous, and as it is convenient to have a term expressive of the distance through which the ship has been carried by the current in any interval of time, we have used the word *drift* in the latter sense only. Thus the terms *set* and *drift* are used in speaking of the current as *course* and *distance* are in speaking of the ship.

a. certained, the rate is found by dividing the number of miles of the drift by the number of hours.

Ex. 1. A current runs 2.2 knots: required its drift in 13 hours.

Ans. $2.2 \times 13 = 28.6$ miles, the Drift.

Ex. 2. A ship is found to have drifted by the current 42 miles in 21 hours: required its rate.

Ans. $\frac{42}{21} = 2$ miles per hour, the Rate.

292. Since the current sets the ship in a certain direction and at a certain rate, while the ship herself is going through the water in another direction and at another rate, the course of a ship affected by a current becomes in general a case of traverse sailing, in which there are two courses and distances.

Thus current sailing is analogous to traverse sailing, the two courses, instead of following in succession, being here considered as taking place at the same time.

The subjects for consideration in this section are, finding the place of a ship affected by a current; determining the course under a particular condition; and, lastly, finding the motion of the current itself.

Case I. Given the course steered, and dist. run by the log, with the set and rate of the current, to find the course and distance made good.

Ex. A ship runs N.E. by N. 18 miles in three hours, in a current setting W. by S. two miles an hour: required the Course and Dist. made good.

N.E. by N. 18 m. gives	D. Lat. 15° 0' N.	Dep. 10° 0' E.
W. by S. 6 m.	D. Lat. 1° 2' S.	Dep. 5° 9' W.
	13° 8' N.	4° 1' E.

The Course is, therefore, N. by E. $\frac{1}{2}$ E.; Dist. 14 miles.

The Construction of this example is the same as that of a case of traverse sailing, in which the courses and distances to be laid off are N.E. by N. 18 miles, and W. by S. 6 miles.

293. When a ship steering for a port is drifted by a current, it is evident that, unless it be exactly with her or exactly against her, it will throw her out of her intended course. Since the course to be shaped in any case depends on the rate of sailing of the ship, and as this cannot be foreseen for any future hour, the course must, when it is proposed to take into consideration the effect of the current, be determined by the present rate of sailing, and independently of the distance of the port.

Case II. Given the bearing of the port, and the set and rate of the current: it is required to shape the course so as to keep the port on the same bearing.

294. *By Inspection.* When the bearing of the port and the set of the current are in *adjacent* quarters of the compass, take their *sum*; when in the *same* or *opposite* quarters, take the *difference*.

With this sum (or its supplement to 16 points, or 180°, if it exceeds 90°), or difference, as a course, and the rate of the current as a distance, find the Dep.

With this Dep. as Dep. and the rate of the ship as Dist. find the Course.

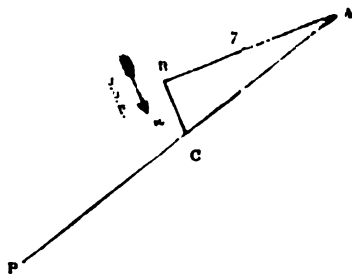
This course being applied to the bearing of the port on the *opposite* side to that towards which the current is drifting the ship, gives the course to be steered.

Ex. 1. The port bears S. 52° W., the current sets S.S.E. two miles an hour; the present rate of sailing 7 knots: shape the course so as to keep the port on the same bearing.

By Inspection. S. 52° W. and S.S.E. are in *adjacent* quarters; the *sum*, therefore, of 52° and $22^{\circ}\frac{1}{2}$ is $74^{\circ}\frac{1}{2}$. This course, with the Dist. 2, gives dep. $1^{\circ}9'$. The dist. 7 and dep. $1^{\circ}9'$ give the course 16° . This $16'$ applied to the *right* (because, in facing towards S. 52° W. S.S.E. lies to the *left*), gives the Course $52^{\circ} + 16^{\circ}$, or S. 68° W.

N.W.	N.E.
S.W.	S.E.

295. *By Construction.* Take a point B, any where, and from it lay off the set and rate of the current, as BC, S.S.E. two miles; through C draw a line AP, S. 52° W., for the direction of the port; from B lay off BA, 7, the rate of sailing, meeting PA in A; then CAB is the angle 16° , which the ship is to steer to the right of the port.



It is evident, in the present case, that while the ship is running along AB, looking to windward of the port, the current is setting her to the left towards the proposed line, AP. Attention to this point will ensure marking A on the proper side of BC; for if a line were drawn from B towards a point between C and P, to represent the ship's course, it is evident that while on it she would be looking to leeward of the port, while the current was also drifting her to leeward.

This example will serve for all cases. Thus, while the port bears as above, suppose the current sets N.N.W. 2 miles; then the point B and the line AB would lie on the S.E. side of AP instead of the N.W. side, the angle A would be 16° as before, but the distance AC made good by the ship in the direction of the port, would be different.

Ex. 2. The port bears N. 42° W., the current runs south 3 knots; rate of sailing, 5; shape the Course as required by the condition.

By Inspection. South giving no angle, the first course is 42° at once, which, with Dist. 3, gives Dep. 2. The Dist. 5 and Dep. 2 give Course 24° , to be applied to the *right*, because in facing towards N. 42° W., south is to the *left*.

Ex. 3. The port bears E., the current sets S.W. by S. 3 knots; rate of sailing, 4.

East is 8 points, or 90° , which is one of the *opposite* quarters to S.W.; the diff. of 8 points and 3 points, or 5 points as Course, and Dist. 3, give Dep. $2^{\circ}5'$. The Dep. $2^{\circ}5'$, and Dist. 4, give Course 39° , which, applied to the left of E., gives the Course to be steered N. 51° E.

Ex. 4. The port bears S. 82° E., the current sets N. 5° W. 4 knots; rate of sailing, 3.

S.E. and N.W. being opposite quarters, the diff. of 82° and 5° , or 77° , is the Course; which, with the Dist. 4, gives Dep. $3^{\circ}9'$. This Dep. $3^{\circ}9'$ being greater than the Dist. 2 (the ship's rate) which is impossible, shews that the ship cannot maintain the bearing of the port.

296. When the current sets at right angles across the line of direction of the port, the ship's velocity must evidently be equal, at least, to that of the current, that she may be able to stem it, and to preserve both the bearing and distance of the port unchanged.

Hence, if the current tend in any degree to set the ship away from her port, she will not be able to preserve the required position unless her velocity exceed that of the current.

Case III. Given the Course and Distance run by account from a well-determined place, and the true position of the ship, to find the Current.

297. *By Inspection.* Having the D. Lat. and Dep., both by account and as deduced from observation, take the difference between the two D. Lats. and the two Deps.; if the D. Lats. are of different names, take their sum, and the same of the Deps.

When the true lat. of the ship is to the north of the account, mark the diff. or sum of the D. Lats. N., otherwise S.; and when the true longitude of the ship is to the E. of the account, mark the diff. or sum of the Deps. E., otherwise W. Find in the Traverse Table the course and distance corresponding to the said differences, as D. Lat. and Dep. these are the set and drift of the current.

Ex. 1. A ship in lat. 37° N., sails S. 57° E., 48 miles, by account, and is found to have made good $31^{\circ}6'$ D. Lat. (S.), and $44^{\circ}7'$ Dep. (E.): find the current.

D. Lat. by account	$26^{\circ}1'$	Dep. by account	$40^{\circ}3'$
Do. true	$31^{\circ}6'$	Do. true	$44^{\circ}7'$
Diff. of D. Lats.	$5^{\circ}5'$ S.	Diff. of Deps.	$4^{\circ}4'$ E.

The D. Lat. $5^{\circ}5'$ S., and Dep. $4^{\circ}4'$ E., give Course S. 39° E., Dist. 7.1, the SET and DRIFT of the current in the time. Suppose the time eight hours and a half, then the RATE is 0.8 of a mile per hour.

Ex. 2. A ship from lat. $38^{\circ}20'$ S., and long. $31^{\circ}15'$ W., sails S. 40° E., 170 miles, by account, when she is found by observation to be in lat. $40^{\circ}54^{\circ}5'$ S., and long. $30^{\circ}44^{\circ}8'$ W.: find the current.

The lat. by account, is $40^{\circ}30'$ S.; the long. by account, $28^{\circ}55'$ W.

Lat. left	$38^{\circ}20'$	Long. left	$31^{\circ}15'$
Lat. in	$40^{\circ}54^{\circ}5'$	Long. in	$30^{\circ}44^{\circ}8'$
True D. Lat.	$2^{\circ}34^{\circ}5' = 154^{\circ}5'$	True D. Long.	$30^{\circ}2'$

The mid. lat. 40° as Course, and Dist. $30^{\circ}2'$, give D. Lat. $23^{\circ}0'$. (See No. 318.)

D. Lat. by account	$130^{\circ}2'$	Dep. by account	$109^{\circ}3'$
Do. true	$154^{\circ}5'$	Do. true	$23^{\circ}0'$
Diff. of D. Lats.	$24^{\circ}3'$ S.	Diff. of Deps.	$86^{\circ}3'$ W.

The D. Lat. $24^{\circ}3'$ S., and Dep. $86^{\circ}3'$ W. give Course S. 74° W., Dist. 90 miles, the SET and DRIFT of the current in the given time.

Ex. 3. (By bearings and dist. of land.) A ship at sunset sets a point of land, N. 58° E., 11 miles. Next morning having, as supposed, made good S. 40° E. 14 miles, the point bears N. 76° E. 20 miles: required the current.

The Bearing at sunset, considered as a Course from the land or S. 58° W., Dist. 11, and S. 40° E. 14, give whole D. Lat. by account, between the ship and the point, $16^{\circ}5'$ S. and Dep. $0^{\circ}3'$ W. The Bearing and Dist. in the morning give the D. Lat. $4^{\circ}8'$ S., and Dep. $19^{\circ}4'$ W.

D. Lat. by account	$16^{\circ}5'$	Dep. by account	$0^{\circ}3'$
Do. true	$4^{\circ}8'$	Do. true	$19^{\circ}4'$
	$11^{\circ}7'$		$19^{\circ}1'$

The D. Lat. $11^{\circ}7'$, and Dep. $19^{\circ}1'$, give Course or SET 58° and Dist. or DRIFT 22; the set is evidently (from the two bearings) between N. and W.

The complete construction of this last case, in which longitude is involved, requires the use of Mercator's Chart. No further directions are, however, necessary than to lay off the place of the ship by D.R. and her true position; the line joining these two points shews the set of the current, and its drift.

298. The last example leads to the remark that, unless the ship's head be the same way at the taking of each bearing, as well as during the whole interval between the observations, the resulting set of the current will be mixed up with local deviation; and the current accordingly cannot be truly determined, unless the effect of local deviation be removed.

In this subdivision* rules have been laid down for working certain questions in current sailing. Other matters relative to the current, which present themselves for consideration in shaping the course, and also in determining the current itself by experiment, are treated in the division of the work entitled "Navigating the Ship."

4. *Windward Sailing.*

299. In windward sailing the vessel bound to a port has a foul wind. As she is thus compelled to make more courses than one, the case is one of Traverse Sailing; but as the course on either tack is determined by the circumstances, the inquiry is limited to the consideration of the time at which it is proper to tack.

The general principle, supposing the wind to remain unchanged, is to near the port as much as possible from instant to instant. Now the ship nears the port fastest on that tack on which she looks the best up for it; if, therefore, she looks up for the port better on her present tack than she would on the other, she should stand on; if not, she should go about. Hence it follows, that the ship should constantly keep the port in the wind's eye; but, as working up on this line would require the vessel to be continually tacking, which is practically impossible, the limits within which the rule should be followed must be determined by circumstances.

The advantage of working up nearly in the stream of the wind towards any object, whether fixed or moving, is, that the wind cannot be worse, and, therefore, every change must be for the better.†

300. The distance run, or the ground actually gone over, is the same whether the ship makes two boards or a greater number, pro-

* As it is convenient occasionally thus to refer by name to the several parts into which, from the classification adopted, the contents of this volume are divided, it may be stated briefly that the principal portions, as the Introduction, Navigation, &c., are here termed *divisions*, which, when necessary, are divided into *chapters*. The parts of a division or of a chapter, distinguished by capital letters, are termed *sections*; the parts of a section in large italics, *subdivisions*, and the further division of these, in small italics with figures in brackets, *subsections*, the prefix *sub* being thus applied to the smallest divisions.

† The question of closing another vessel belongs to tactics, and not to our present subject, which relates solely to the place of the ship on the sea. It may not be useless, however, to notice here, that in working up to a vessel to windward, it is proper to keep as near the stream of the wind as circumstances permit; because from the time that the chase has drom to the weather beam of the chaser, the latter, however great her superiority of sailing, ceases to near the chase. See Naut. Mag. 1838, Art. "Chasing," p. 446.

vided that no ground or time is lost in stays: the application of the above rule, therefore, depends entirely on the probability of a change of wind.

In this subdivision we consider merely the general principle of sailing with a foul wind. Other points involved in Shaping the Course, as the combination of a current with a foul wind, the selection of such a course as may, in certain cases, convert a foul wind into a fair one, the effects of local deviation which have been observed while sailing on different tacks, will be treated in the Chapter on Navigating the Ship, under the heads "Shaping the Course," "Error of the Course."

II. PARALLEL SAILING.

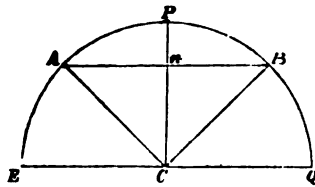
301. When two places lie on the same parallel of latitude, or due east and west of each other, the distance between them, estimated along a parallel, or E. and W. (which is all departure), is converted into difference of longitude; or, on the other hand, their difference of longitude is converted into distance,—by the rules of PARALLEL SAILING.

The principles of Parallel Sailing are contained in the two following propositions.

302. PROP. A parallel of latitude is a circle of which the radius is proportional to the cosine of the latitude.

Let EPQ be part of a meridian, P the pole, EQ a diameter of the equator, A a place whose latitude is the arc AE.

Take BQ equal to AE; then B is the opposite point to A on the same parallel. Join AB crossing CP in n .



Suppose now a ship to move from A round the polar axis CP, preserving the same lat., or the angle PCA constant; then at the end of half a revolution she will be at B, and PCB will be equal to PCA.

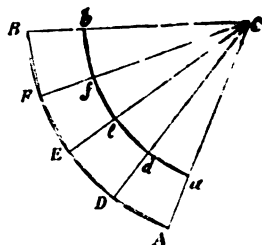
Then CA and CB being equal, each being a radius, and the angles PCA, PCB, equal, and Cn common to the two triangles ACn, BCn, these are equal (No. 117). Hence An is equal to Bn; and this holds for every point of the parallel.

Hence A and B are on the circumference of a circle whose centre is n, in the line or diameter joining any two opposite points.

Now An (see fig. p. 44) is equal to the cosine of the arc AE, CE being radius; hence CE : An :: rad. (= 1) : cos lat., which was to be proved.

303. PROP. The length of a circular arc is proportional to its radius. Or, the length of AB : the length of ab :: CA : Ca.

C is the common centre of the arcs AB, ab . Divide the angle C into any number of equal parts, as for ex. four, by the lines CD, CE, CF; join the points A and D, &c. by the chords AD, DE, &c. Then the sides CA, CD, &c. being equal, and the angles ACD, DCE, &c. being equal, the bases AD, DE, &c. are all equal. (No. 117.)



In like manner the chords ad , de , &c. are all equal.

Now the triangles CAD, Cad , being isosceles, and having one angle ACD common, have the remaining angles equal; they are thus equiangular, and therefore similar (148 cor.), and their sides are proportional (146); hence $AD : ad :: CA : Ca$.

We may multiply both terms of the ratio $AD : ad$ by any number without altering its value (Nos. 37 and 7), whence $4AD : 4ad :: CA : Ca$. Now $4AD$ is the sum of the four equal chords AD, DE, &c., and $4ad$ is that of the chords ad , de , &c. Hence,

The sum of the equal chords of AB : sum of the same number of equal chords of $ab :: CA : Ca$.

This proportion is evidently true, whatever be the number of equal parts into which the angle C is divided. It would therefore hold equally for an immensely increased number of diminished chords, as for ex. of $1'$, or $1''$, or a millionth of $1''$, or infinitely less; it therefore holds of the arc itself, which we may conceive to be composed of an indefinitely great number of indefinitely small portions, each of which is arc or chord indifferently,* or arc AB : arc $ab :: CA : Ca$.

(1). If AB be the equator, and ab a parallel, then $CA : Ca :: 1 : \cos \text{ lat.}$ Whence $AB : ab :: 1 : \cos \text{ lat.}$

And since Diff. Long. is an arc of the equator, and an arc measured parallel to it in any other latitude is called Dep., we have,

$$\text{D. Long.} : \text{Dep.} :: 1 : \cos \text{ lat.}, \quad \text{whence Dep.} = \text{D. Long.} \times \cos \text{ lat.} \dots (1)$$

$$\text{Dep.} : \text{D. Long.} :: 1 : \sec \text{ lat.}, \quad (162 (2) (4)) \quad \text{D. Long.} = \text{Dep.} \times \sec \text{ lat.} \dots (2)$$

These are the equations for Parallel Sailing.

(2). These equations, in logarithms, become

$$\log \text{ Dep.} = \log \text{ D. Long.} + \log \cos \text{ lat.} \dots (1)$$

$$\log \text{ D. Long.} = \log \text{ Dep.} + \log \sec \text{ lat.} - 10 \dots (2)$$

Case I. Given the distance run on a given parallel of latitude, to find the difference of longitude.

304. *By Inspection.* (1.) Enter the Traverse Table with the latitude as a course, and look in the D. Lat. column for the given distance; the Dist. against this is the Diff. Long. required.

* As, from the nature of the case, the sum of all the chords can never surpass the arc, though it may approach indefinitely near it, the arc is said to be the *limit* of the sum of the chords increased indefinitely.

Ex. A ship runs 143 miles due W. in Lat. $38^{\circ} 11'$: required the diff. long. she makes good.

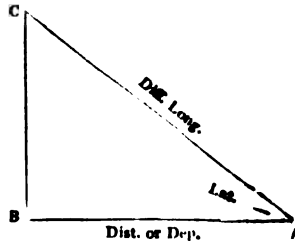
The lat. 38° as course, and 143 in the D. Lat. column, give the Dist. 181, or $3^{\circ} 1'$: the Diff. Long. required.

(2.) Or employ Table 3, as directed in the Explanation of the Tables.

305. *By Computation.* To the log. sec. of the Lat. add the log. of the Dist.; the sum (rejecting 10) is the log. of the Diff. Long.

Ex. above.	Lat. $38^{\circ} 11'$	log. sec. 0.1046
	Dist. 143	log. 2.1553
	Diff. Long. 181.9	log. 2.2599

306. *By Construction.* Draw a line A B east and west, and lay off 143 on it; lay off the angle B A C equal to the Lat. or 38° in this case; draw B C perpendicular to A B, and meeting A C in C. Then A C is the Diff. Long. required.



Case II. Given the Diff. Long. of two places on the same parallel, to find their distance as measured along the parallel.

307. *By Inspection.* (1.) Enter the Traverse Table with the Lat. as course and the Diff. Long. as distance; the D. Lat. is the distance required.

Ex. The diff. long. of two places in the parallel of $53^{\circ} 20'$ is $12^{\circ} 14'$: required their distance as measured along their parallel.

The lat. 53° as Course, and Dist. 734, give in the D. Lat. column 442 nearly: the distance required.

(2.) Or employ Tab. 4, as directed in the Explanation of the Tables.

308. *By Computation.* To the log. cos. of the Lat. add the log. of the Diff. Long.; the sum (rejecting 10) is the log. of the distance required.

Ex. above.	Lat. $53^{\circ} 20'$	log. cos. 9.7761
	D. Long. 12 14 or 734	log. 2.8657
	Dist. 438.3	log. 2.6418

309. *By Construction.* Draw a line A B (fig. No. 306) of any length; lay off at A the angle B A C equal to the latitude 53° ; take A C equal to the Diff. Long. 734; from C draw C B perpendicular to A B; then A B is the Dist. required, and measures 442.

310. In parallel sailing the Distance and Departure are identical. When the course is nearly, though not exactly, on a parallel, the distance run and the departure are very nearly equal; hence it is evident that parallel sailing will apply, nearly enough for common purposes, to cases in which the course is not exactly east or west.

311. In lats. below 5° , when the distance does not exceed 300 miles, the Dep. may at once be taken as the Diff. Long., as the greatest error will scarcely exceed $1'$.

1. *Middle Latitude Sailing.*

312. This is a method (founded on the principle of parallel sailing) of converting the Departure into Difference of Longitude, and the Difference of Longitude into Departure, when the ship's course lies obliquely across the meridian; that is when, besides Departure, she makes Difference of Latitude.

Suppose a ship make 100 miles departure in going, on the same course, from lat. 38° to lat. 41° ; this departure, if made good altogether in lat. 38° , would give 127 Diff. Long. by No. 304; and again, if made good in lat. 41° , it would give 132.5 Diff. Long. Now, since the ship has sailed between these two parallels, and not on either of them exclusively, her real Diff. Long. must be between 127 and 132.5; and therefore we may conclude it to be not far from that which would result from a departure made good altogether in the *middle parallel*; hence the name of the sailing.

313. Middle latitude sailing has thus the same two cases as parallel sailing; and, accordingly, the rules for inspection, computation, and construction, already given, Nos. 304, &c., apply equally to this sailing, observing merely to read *middle latitude for latitude*.

314. When the latitudes of the two places are of the *same* name, the middle lat. is half their *sum*.*

In using the Traverse Tables, it is enough to take the latitudes to the nearest degree.

Ex. 1. A ship sails from lat. $51^{\circ} 33' N.$ to $49^{\circ} 9' N.$: find the Mid. Lat.

Lat. left	52°
Lat. in	49
	101
Mid. Lat.	50

Ex. 2. A ship sails from lat. $2^{\circ} N.$ to lat. $1^{\circ} S.$

The ship moving near the equator, the consideration of middle latitude is omitted, and the Dep. taken as the Diff. Long.

When the latitudes are of *contrary* names, no sensible error can arise from taking the Dep. itself, made good from day to day, as the Diff. Long. But in greater distances between places in opposite latitudes it is proper to convert the Dep. made good in N. lat. into Diff. Long. by means of the north mid. lat., that is, half the N. latitude, and that made good in S. lat. by half the S. lat.

When, on the other hand, the Diff. Long. is to be converted into Dep., this rule does not apply. It will be near enough for common purposes, when the latitudes are either very nearly equal or very unequal, to employ, as the mid. lat., half the greater latitude. In

* The rule which directs half the difference of the latitudes of two places on opposite sides of the equator to be employed as their middle latitude, is erroneous. The error will be readily perceived in considering a case. Suppose a ship sails S.E. from lat. $10^{\circ} N.$ to $10^{\circ} S.$; it is evident that her diff. long. will be exactly the same as if, on reaching the equator, she returned to the same N. lat., steering N.E., since her course is the same, and she moves in the same lats. in both cases. Thus the mid. lat., which is the average of all the latitudes passed through, or the half sum of the first and last, and is here 5° , is independent of the distinctions of N. and S. The common rule gives 0 for the mid. lat.; whence it would follow that the diff. long. made good by a ship in ranging through all the latitudes between $10^{\circ} N.$ and $10^{\circ} S.$, or any other equal latitudes, however great, would be the same as if she made good her departure altogether on the equator — a conclusion manifestly erroneous.

an intermediate case we may combine the two mid. lats., giving the greater weight to that which corresponds to the greater latitude.

Ex. 1. Find the mid. lat. between 30° N. and 29° E.

The lats. being nearly equal, half of 30° , or 15° , may be taken as the MID. LAT.

Ex. 2. Find the mid. lat. between 30° N. and 2° S.

Half of 30° , or 15° , may be taken as the MID. LAT.

Ex. 3. Find the mid. lat. between 30° N. and 15° S.

The N. mid. lat. is 15° , the S. mid. lat. is 7° nearly; now the mid. lat. 15° corresponds to 30° of lat., and the other, or 7° , to only half as much. Instead, therefore, of dividing the sum of the two by 2, we give to the first double the weight of the other, and divide by 3; thus, $15 + 15 + 7$, or 37 divided by 3, gives 12° , the MID. LAT. required, nearly.

Case I. Given the departure, to find the difference of longitude.

Ex. 1. A ship from lat. $51^{\circ} 9'$ N. sails S.W. by W. 216 miles: required her Lat. in and Diff. Long.

315. *By Inspection.* Find the D. Lat. and Dep., and the Lat. in. Find the Mid. Lat.; then, with the Mid. Lat. as Course, look for the Dep. in the *D. Lat. column*, the corresponding Dist. is the D. Long. required.

By Case I. of Plane Sailing, S. 5 points, Dist. 216, give D. Lat. 120 and Dep. $179^{\circ} 6'$; hence the Lat. in is $49^{\circ} 9'$ N.

Lat. left $51^{\circ} 9'$ N.

$100^{\circ} 18'$ Mid. Lat. 50°

Then Course 50° and Dep. $179^{\circ} 6'$ in the D. Lat. column give Dist. 279 or $4^{\circ} 39'$, the Diff. Long. required.

316. *By Computation.* Having found the Dep. and the Mid. Lat., add together the log. sec. of the Mid. Lat. and the log. of the Dep.; the sum (rejecting 10) is the log. of the Diff. Long.

Ex. above. Dep. $179^{\circ} 6'$ Mid. Lat. $50^{\circ} 9'$

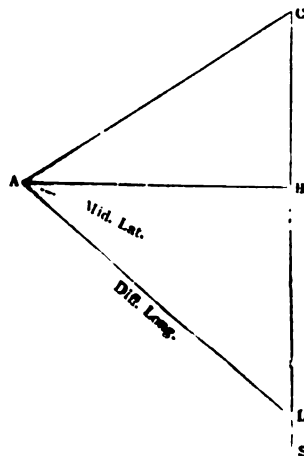
Mid. Lat. $50^{\circ} 9'$ log. sec. $0^{\circ} 1933$

Dep. $179^{\circ} 6'$ log. $2^{\circ} 2543$

Diff. Long. $280^{\circ} 3'$ ($4^{\circ} 40^{\circ} 3'$) log. $2^{\circ} 4476$

317. *By Construction.* (Ex. 1.) Lay off SCA the Course 5 points, and take CA the Dist. 216; draw AB perpendicular to CS. The figure is thus far complete for plane sailing, Case I.

Lay off the angle BAL equal to the Mid. Lat. 50° , and AL meeting CS is the Diff. Long. 280.



Ex. 2. A ship from Lat. $29^{\circ} 40'$ N. sails F.N.E. till she makes 72 miles D. lat.: required the Dist. run and Diff. Long.

By Inspection. By No. 276, Course 6 points and D. Lat. $71^{\circ} 9'$ give Dep. $173^{\circ} 7'$; and 72 miles northing give lat. in $30^{\circ} 52'$ N.

Lat. left $29^{\circ} 40'$ N.

Lat. in $30^{\circ} 52'$ N.

$60^{\circ} 32'$

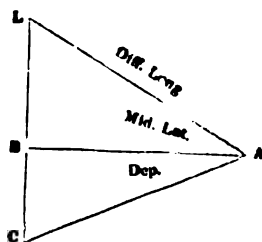
Mid. Lat. $30^{\circ} 16'$

Course 30° (Mid. Lat.) and Dep. $173^{\circ} 7'$ as D. Lat. give Dist. 201 or $3^{\circ} 21'$, the Diff. Long. required.

By Construction. C B A represents the fig. for plane sailing.

Lay off B A L equal to the mid. lat. 30° ; and A L is the Diff. Long. and measures 201.

These two examples of construction are sufficient for the case.



Ex. 3. A ship from lat. $44^\circ 58' N.$ runs 230 miles, and makes 56 miles southing: find the Course and Diff. Long.

By Case IV. of Plane Sailing, p. 86, the Dist. 230 and D. Lat. 56 stand together over the Course 76° and against the Dep. 223.2; then 56' southing gives Lat. in $44^\circ 2' N.$

The Lat. left 44° and Lat. in 45° give the Mid. Lat. $44\frac{1}{2}$ or 44° .

Course 44° (Mid. Lat.) and Dep. 22.3 in D. Lat. column give Dist. 31: hence the Diff. Long. is 310, or $5^\circ 10'$.

Case II. Given the latitudes and longitudes of two places, to find the departure, and thence the course and distance between them.

Ex. Find the Course and Dist. between C. Sierra Leone, in lat. $8^\circ 30' N.$, long. $13^\circ 8' W.$, and C. St. Roque, lat. $5^\circ 28' S.$, long. $35^\circ 17' W.$

318. *By Inspection.* Find the Mid. Lat. and the Diff. Long. of the places; open the Traverse Table at the Mid. Lat. as a course, look for the Diff. Long. in the Dist. column, and take out the D. Lat.: this is the Dep. required.

The Dep. and given Diff. Lat. between the places give the Course and Dist. by Case III. Plane Sailing, p. 109.

C. Sierra Leone, lat.	$8^\circ 30' N.$	Long.	$13^\circ 18' W.$
C. St. Roque	$5^\circ 28' S.$		$35^\circ 17' W.$
D. Lat.	$13^\circ 58'$	Diff. Long.	$21^\circ 59'$
Or	838 miles	Or	1319 miles.

The Mid. Lat. of $8^\circ 30'$ is $4^\circ 15'$, that of $5^\circ 28'$ is $2^\circ 44'$, or 4° and $3'$ nearly. As 4° corresponds to the greater lat., we may adopt it as the Mid. Lat. (Assigning the relative weights with some further precision gives $3^\circ 40'$ as the Mid. Lat.)

Course 4° (Mid. Lat.) and Dist. 132 give 131.7 in the D. Lat. col.; this as Dep., and D. Lat. 83.8, give Course $57\frac{1}{4}$, Dist. 1570 miles.

319. *By Computation.* Find the Diff. Long. and the Mid. Lat., to the log. cos. of the Mid. Lat. add the log. of the Diff. Long.: the sum is the log. of the Dep.

Ex. above.	D. Lat. 838, D. Long. 1319, Mid. Lat. $3^\circ 40'$.	
	Mid. Lat. $3^\circ 40'$	log. cos. 9.9991
	Diff. Long. 1319	log. $3^\circ 1202$
		DEP. 1316
		log. $3^\circ 1193$

The Dep. being now found and the D. Lat. given, the Course and Dist. may be found. (No. 279.)

Construction. Construct the triangle for turning the Diff. Long. into Dep., as in No. 306 (reading Mid. Lat. for Lat.). Then having the D. Lat. and Dep. the process is completed by drawing the figure as for Case III. of Plane Sailing, p. 109.

320. When the Mid. Lat. is below 5° , and Dist. under 300 miles, see No. 311.

Examples for Exercise.

- Ex. 1. If a ship from Tynemouth Castle, in Lat. $55^{\circ} 1' N.$ and Long. $1^{\circ} 25' W.$, sails S.E. by S. 296 miles: what is her present latitude and longitude?
 Ans. Lat. in $50^{\circ} 55' N.$; Diff. Long. 273m.; Long in, $3^{\circ} 8' E.$
- Ex. 2. A ship from Cape Clear, in Lat. $51^{\circ} 26' N.$ and Long. $9^{\circ} 29' W.$, sails S.W. 263 miles: required her Lat. and Long.
 Ans. Lat. $48^{\circ} 20'$; Diff. Long. 288.7; whence the Long. in is $14^{\circ} 18' W.$
- Ex. 3. Find the Course and Distance between Tynemouth and the Naaze of Norway.
 Ans. Course N. $57^{\circ} 43' E.$; Distance, 331.3 miles
- Ex. 4. Required the Course and Distance from a place A, in Lat. $51^{\circ} 25' N.$ and Long. $9^{\circ} 29' W.$, to a place B, in Lat. $36^{\circ} 57' N.$ and Long. $25^{\circ} 6' W.$.
 Ans. Course S. $37^{\circ} 45' W.$; Distance, 1098 miles.
- Ex. 5. Required the Course and Distance from a place A, in Lat. $56^{\circ} 12' N.$ and Long. $2^{\circ} 36' W.$ to a place B, in Lat. $57^{\circ} 58' N.$ and Long. $7^{\circ} 3' E.$.
 Ans. Course N. $71^{\circ} 23' E.$; Distance, 332 miles.
- Ex. 6. Required the Course and Distance from A to B; Lat. of A $53^{\circ} 18' N.$; Long. of A $0^{\circ} 55' E.$; Lat. of B, $57^{\circ} 58' N.$; Long. B $7^{\circ} 3' E.$.
 Ans. Course N. $36^{\circ} 34' E.$; Distance, 349 miles.

2. Mercator's Sailing.

321. This sailing is employed for exactly the same purposes as middle latitude sailing; but it is a perfect method, which the other is not.

The calculations are performed by the help of a table of Meridional Parts, Table 6.

322. To find the *Meridional Difference of Latitude*. When the latitudes are of the *same* name, take the *difference* of the meridional parts for the two latitudes; when of *contrary* names, take the *sum*.

Case I. Given the course between two places, and their latitudes, to find their difference of longitude.

Ex. 1. (Lats. *same* name.) A ship from lat. $51^{\circ} 9' N.$ sails S.W. by W. 216 miles; required the Lat. in and Diff. Long.

323. *By Inspection.* Having found the Lat. in, take out the meridional parts (Table 6) for it, and for the Lat. left; find the Meridional Diff. Lat. (No. 322).

With the Course, and Mer. D. Lat. in the D. Lat. column, find the Dep.; this is the Diff. Long.

By Case I. No. 273, the Course 5 points and Dist. 216 give D. Lat. 120 and Dep. $17^{\circ} 6'$; this D. Lat. subtracted from $51^{\circ} 9'$ gives Lat. in, $49^{\circ} 9' N.$

Lat. in	$49^{\circ} 9' N.$	Mer. parts	3396
Lat. left	$51^{\circ} 9'$		<u>3583</u>
		Mer. D. Lat.	187

The Course 5 points and D. Lat. 187 give Dep. 28° , or $4^{\circ} 40'$ the Diff. Long

324. *By Computation.* Find the Lat. in, and the Mer. D. Lat. To the log. tan. of the Course add the log. of the Mer. D. Lat.; the sum (rejecting 10) is the log. of the D. Long.

Ex. above. Lats. $49^{\circ} 9'$ and $51^{\circ} 9'$, Course 5 points.

	5 points	log. tan.	$10^{\circ} 1751$
Mer. D. Lat.	187	log.	<u>$2^{\circ} 2718$</u>
Diff. Long.	$279^{\circ} 8$, or $4^{\circ} 39' 8$	log.	$2^{\circ} 4469$

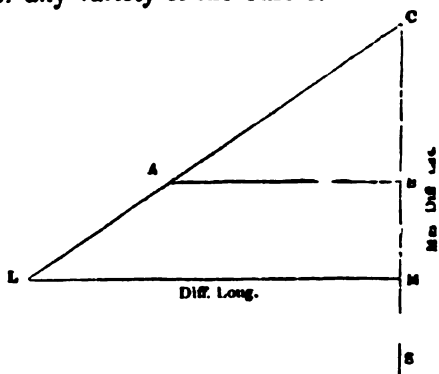
(This is the canon (3) No. 272. It will be sufficiently understood by observing that, in the fig. below, CM is the Mer. D. Lat., and ML the Diff. Long., and $CM : ML :: \text{rad.} \cdot \tan. MCL$ the course.

This example is sufficient for any variety of the Case I.

325. *By Construction.* Lay off the course MCA, S 5 points W.; take CA 216 the Dist.; draw AB perp. to CS: the fig. CAB is, thus far, the case for plane sailing.

Now lay off CM the Mer. D. Lat. 187, and draw ML parallel to AB meeting CA produced: ML is the Diff. Long. and measures 280.

This example of construction is sufficient for Case I.



Ex. 2. A ship from lat. $29^{\circ} 40'$ N. sails E.N.E. till she makes 72 miles D. Lat.: find her Diff. Long.

By Inspection. Course 6 points and D. Lat. 72 give Dist. 188 miles: the Lat. in is $30^{\circ} 52'$.

Lat. left $29^{\circ} 40'$	Mer. parts 1865
Lat. in $30^{\circ} 52'$	—
	1949
	Mer. D. Lat. 84

Course 6 points and D. Lat. 84, give Dep. 203, or $3^{\circ} 23'$, the Diff. Long.

Case II. Given the latitudes and longitudes of two places to find the course and distance between them.

Ex. Find the Course and Distance between Ushant, in lat. $48^{\circ} 28'$ N. long. $5^{\circ} 3'$ W., and St. Michael's, lat. $37^{\circ} 44'$ N. long. $25^{\circ} 40'$ W.

326. *By Inspection.* Take out the mer. parts for the two lats.: find the Mer. D. Lat. and the Diff. Long.

Enter the Traverse Table with the Mer. D. Lat. as D. Lat. and the D. Long. as Dep.: this gives the Course.

Then with this Course and the true D. Lat. find the Dist., which is the distance required.

Ushant, lat. $48^{\circ} 28'$ N.	Mer. parts 3334	Long. $5^{\circ} 3'$ W.
St. Mich. $37^{\circ} 44'$	2448	$25^{\circ} 40'$ W.
$10^{\circ} 44'$	Mer. D. Lat. 886	$20^{\circ} 37'$
True D. Lat. 644		Diff. Long. 1237

Then 886 as D. Lat. and Dep. 1237 give Course 54° ; and D. Lat. 644 gives 1095 miles, the Dist. required.

327. *By Computation* (1.) For the Course. Find the Mer. Diff. Lat. and the Diff. Long. From the log. of the Diff. Long. (adding 10 to the index if necessary) subtract the log. of the Mer. D. Lat.: the remainder is the log. tan. of the Course.

(2.) For the Distance. Find the course; then to its log. sec. add the log. of the true D. Lat.: the sum is the log. of the Distance.

Ex. above.	M. D. Lat. 886	D. Long. 1237	true D. Lat. 644.		
Diff. Long.	1237	log. $3^{\circ} 0924$	Course $54^{\circ} 24'$	log. sec. $0^{\circ} 2350$	
Mer. D. Lat.	886	log. $2^{\circ} 9474$	Tr. D. Lat. 644	log. $2^{\circ} 8089$	
Course $54^{\circ} 24'$		tan. $0^{\circ} 1450$	Dist. 1106	log $3^{\circ} 0439$	

328. *By Construction.* Draw the meridian CS* through one of the places, say Ushant, and on it lay off the Mer. D. Lat., 886 from C to M. Draw ML perpendicular to CS and equal to the Diff. Long. 1237; join CL, and SCL is the Course.

Lay off CB the true D. Lat. on CS, draw BA parallel to LM and CA is the Dist. 1106.

329. When the lat. is below 5° and the dist. less than 300 m., see No. 332.

Examples for Exercise.

Ex. 1. A ship, in Lat. $36^{\circ} 40'$ S. and Long. $16^{\circ} 20'$ E., sails W.N.W. until she arrives in Lat. $33^{\circ} 10'$ S.: find the Diff. of Long. and also the Long. come to.

Ans. Diff. Long. $620' 4''$ W.; whence the Long. come to is $6^{\circ} 8'$ E.

Ex. 2. A ship from Lat. $42^{\circ} 25'$ N. and Long. $15^{\circ} 6'$ W. sails N.E. by E. for several days, and then finds by observation she is in Lat. $46^{\circ} 40'$ N.: find what Diff. of Long. she has made; also find her Long. in.

Ans. Diff. Long. 536; whence her Long. in is $6^{\circ} 10'$ W.

Ex. 3. A ship, in Lat. $42^{\circ} 30'$ N. and Long. $58^{\circ} 51'$ W., sails S.E. by S. 300 miles: find the Diff. Long., and also the Long. in.

Ans. Diff. Long. 219 miles; Long. in $55^{\circ} 12'$ W.

Ex. 4. Find the Course and Distance between Tynemouth and the Naes of Norway.

Ans. Course N. $57^{\circ} 40'$ E.; Distance, 331.4 miles.

Ex. 5. Required the Course and Distance between Tynemouth and Helgoland.

Ans. Course S. $81^{\circ} 8'$ E.; Distance, 324 miles.

Ex. 6. Required the Course and Distance from Diego Ramirez, in Lat. $56^{\circ} 29'$ S., Long. $68^{\circ} 43'$ W., and C. Lopatka, in Lat. $51^{\circ} 2'$ N., Long. $156^{\circ} 46'$ E.

Ans. Course N. $46^{\circ} 21'$ E.; Distance, 934.6 miles.

3. Selection of Mid. Lat. or Mercator's Sailing.

[1.] Finding the Diff. Long.

330. The difference of longitude found by Mid. Lat. is true at the equator, and very nearly true for short distances in all latitudes, especially when the course is nearly E. or W. In high latitudes, when the distance is great and the course oblique, the error becomes considerable; but the result may be made as accurate as we please by subdividing the distance run into small portions, and finding the Diff. Long. for each portion separately.

331. The Diff. Long. deduced by Mid. Lat. sailing is too small: an estimate of the error for places on the same side of the equator may be formed by the help of a few cases. Suppose the course 4 points or 45° , and the D. Lat. 10° or 600 miles; then if this D. Lat. is made good in any latitude below 30° the error of the D. Long. will not exceed $2'$; if made good between the parallels of 40° and 50° the error will be about $3'$; and between 60° and 70° , about $19'$, or $\frac{1}{4}$ of a degree. For smaller distances the errors will be much

* The figure in the preceding page will, after the various examples given, serve sufficiently well to illustrate generally the construction of this case. The learner will merely observe, that if the other place was to the northward of Ushant, the Mer. Diff. Lat. CM would be laid off to the northward of C. In like manner, if the other place was to the eastward of Ushant, the D. Long. ML would be laid off to the eastward, or to the right of the meridian.

less, and for greater distances much greater, as they vary in much more rapid proportion than the distances.*

332. It is proper to remark that when the Course is large, that is, near seven or eight points, the D. Long. should be found by middle latitude in preference to Mercator's Sailing; because, although the latter is mathematically correct in principle, yet a small error in the Course may, when the Course is large, produce a considerable error in the Difference of Longitude.

The reason of this is easily shewn. In mid. lat. sailing we convert the *departure* into D. Long. The process increases the Dep. in a proportion which is less than 2 to 1 in all latitudes below 60° , and exceeds 3 to 1 in latitudes beyond 70° . The error of the Dep., increased in the same proportion, becomes thus the error of the D. Long. Now when the course is nearly E. or W. the Dep. is nearly the same as the distance, and an error of some degrees in the course does not affect the Dep. sensibly; hence in this case the error of the D. Long. depends on that of the Dist. alone.

But in Mercator's Sailing, on the other hand, we convert the *Mer. Diff. Lat.* into D. Long., and the process, when the Course is large, converts a given Mer. Diff. Lat. into a D. Long. much greater than itself; and thus increases the error of the Mer. Diff. Lat. in the same proportion. Thus, for example, at the course 80° the D. Long. exceeds the Mer. Diff. Lat. in the proportion of 6 to 1; at the course 85° this proportion is 11 to 1. Now when the course is large a slight change in it sensibly affects the D. Lat., and also the Mer. Diff. Lat., which is deduced directly from it.

In high latitudes the Mer. parts vary rapidly, and the error of the D. Long. is aggravated accordingly; hence the precept more especially demands attention in high latitudes.

[2.] *Finding the Course or Bearing.*

333. The bearing of the port is truly deduced in low latitudes and at short distances by the method of Mid. Lats.; but the result cannot be rendered accurate in high latitudes by subdividing the distance, which is unknown, into small portions: such cases are truly solved by Mercator's sailing.

When the bearing is large, or near 90° , the method of Mid. Lats. should be preferred to Mercator.

334. The course or bearing computed by mid. lat. sailing is too great. The error, however, in ordinary cases, will be much less than that to which the ship's course itself is liable.

335. The Course as reduced by Traverse sailing, from several courses, does not afford accurately whether by Mercator's or Middle Latitude Sailing, the Diff. Long. made good by the ship, because the

* The proper mid. lat. to employ should be somewhat greater than the mean of the lats. A Table has been given, by Workman ("Navigation Improved," London, 1805), shewing the correction to be added to the mean of the latitudes, in order to obtain true results. But for common purposes the usual method, of which the recommendation in practice is its great convenience, would seem to be near enough, and when more precision is required the complete solution by Mercator's Sailing is effected with very little more labour. (See No. 334.)

Diff. Long. made good on any Course depends entirely upon the latitude in which the ship actually moves.

Ex 1. A ship sails from Lat. 70° N.; 1st, N.E. 400 miles to Lat. $74^{\circ} 43'$, then S.E. 400 miles, when she returns to the parallel of 70° , having made Dep. 556 miles, and D. Long. $31^{\circ} 18'$.

Ex. 2. She sails 556 miles on the parallel of 70° , making D. Long. $27^{\circ} 34'$.

Ex. 3. Starting from 70° , as above, she sails S.E. 400 miles to Lat. $65^{\circ} 17'$, then N.E. 400 miles to 70° , having made 556 miles of Dep. and D. Long. $24^{\circ} 54'$.

The 1st and 3d case, reducing the two courses to one by the Traverse Table, give the same Course and Dist. made good as in Case 2, viz. East 556 miles, or Dep. 556m., and D. Long. $27^{\circ} 34'$, which is erroneous. In Case 1, this Dep. is made good in the average lat. of $72^{\circ} \frac{1}{2}$; in Case 2, in 70° ; and in Case 3, in 68° .

It may appear perplexing to the student that the ship should return to the *same parallel*, after having made a *given Dep.*, and yet that her long., that is, her position in the parallel, should be different in different cases; but he must bear in mind that the Dep. has not been made good *on the parallel*, except in Case 2. If he lays off a case of the kind on the globe, he will perceive clearly the nature of the question.

To obtain accurately the Diff. Long. each course should therefore be separately considered. But, in general, except in very high lats., the distances are not large enough to introduce much error on this account.

III. GREAT CIRCLE SAILING.

336. When the ship sails on a rhumb line (No. 198), her track cuts all the meridians as she passes them in succession, at the same angle; and thus, while steering a course, her head is kept on the *same point of the compass* until she reaches her intended port. This condition, namely, keeping the course constant, is the most convenient in practice, and, besides, produces in all the calculations in which the place of the ship is concerned the utmost simplicity of which they are capable. But the track on the rhumb line is not the *shortest distance* measured directly over the surface of the sphere from one place to another, or the distance "as the crow flies," except when the course is due north or south, or east or west on the equator. The shortest distance between two points on the surface of a sphere is the portion or arc which they include of the circle passing through both the points and the centre of the sphere. Such a circle is called a *great circle*,* as distinguished from other circles whose centres do

* The great circle passing through two places may be found on a globe by stretching a thread evenly between them; or, by turning the globe about till the two places fall on the upper edge of the wooden rim, or horizon of the globe, which thus marks the circle. The distance between the points may be measured at once by laying the thread along the equator of the globe. The courses are found by measuring the angles between the thread and the meridians; the most convenient instrument for which is the horn semicircle, or protractor, as it is also called (No. 108). In order to compare the great circle with the rhumb line the latter must be projected on the globe.

not coincide with the centre of the sphere; as, for instance, the parallels of latitude, of which the centres are in the axis between the centre and the pole, and which are called *small circles*. Hence sailing on a circle of the former kind is called **GREAT CIRCLE SAILING**.* On this course, and on this course alone, the ship steers for her port as if it were in sight.

The three arcs joining two points on the surface of a sphere with each other, and with a third point, and having for their common centre the centre of the sphere, constitute a Spherical Triangle. In the problem under consideration the two places are the two points, and the third point is the pole, and the triangle is formed by the distance between the places and their colatitudes. Some of the rules in this section may be employed accordingly in other problems of spherical trigonometry.

337. Great Circle Sailing is adapted principally to the second only of the two cases, No. 270, or Shaping the Course; because the ship, even when moving on a great circle, must necessarily be kept on the same course (that is, on a rhumb line) for a short distance at a time, and her place may then be deduced by the rules already given in the preceding section with incomparably greater convenience than it could by any rule in which the distance made good was rigorously considered as described on a circle. Although this sailing is thus restricted to one case, we shall, for the sake of clearness, divide the problem of finding the course by *Inspection* into two cases, namely, Case I. in which the places are on the *same* side of the equator, and Case II. in which they are on *opposite* sides.

Case I. *By Inspection*. (The places on the *same* side of the equator.)

(1.) For the Dist. With the two lats. enter the Spherical Traverses Table (Table 5), and take out M and N.

With the complement of the Diff. Long. as a Course and Dist. 100 (Table 2), find the Dep., and write it under N.

When the Diff. Long. is *less* than 90° , *add* this Dep. to N.; when the Diff. Long. is *greater* than 90° , take the *diff.* of the Dep. and N.

With this sum (or diff.) as D. Lat. and M as Dist. find the arc in Table 2: this is the Distance required in degrees of 60 miles each.

(2.) For the Course. Having found the Distance. With the lat *in*, and the compl. of the Dist. in degrees, find M. and N (Table 5.)

With the lat. *to* as Course and M as Dist. (Table 2), find the Dep., and write it under N. When the Diff. Long. is *less* than 90° , take the *diff.* between this Dep. and N. When the Diff. Long. exceeds 90° , take the *sum* of the Dep. and N.

With this diff. (or sum) as D. Lat. and Dist. 100 (Table 2), find the Course.

* Parallel sailing, for a like reason, is sailing on a *small* circle.

The Course is to be reckoned according to the following rule:

Dist. less than 90° (or 5400 miles).		Dist. greater than 90° (or 5400 miles).
Dep. less than N.	Dep. greater than N.	Course to be reckoned
Course to be reckoned	Course to be reckoned	
in N. lat. from S. in S. lat. from N.	in N. lat. from N. in S. lat. from S.	

Ex. 1. Find the Distance between St. Helena, in lat. $15^{\circ} 55' S.$, long. $5^{\circ} 44' W.$, and Cape Horn, in lat. $55^{\circ} 59' S.$ and long. $67^{\circ} 16' W.$, and the Course from each place to the other.

The D. Long. between $5^{\circ} 44' W.$ and $67^{\circ} 16' W.$ is $61^{\circ} 32'$; compl. 28° .

For the Distance.

16° and 56° (the lats.) give	M 186.0	N 42.5
28° (co-diff. long.) and Dist. 100 give		Dep. 46.9
(D. Long. less than 90° .)		Sum 89.4

The Dist. 186.0 and D. Lat. 89.4 give 61° nearly, or Dist. 3660 miles. The complement of 61° is 29° .

For the Course from St. Helena.

16° (Lat. in) and co-Dist. 29°	
	M 118.9 N 15.9
56° (Lat. to) and Dist. 118.9	Dep. 98.6
(D. Long. less than 90° .)	Diff. 82.7

Dist. 100 and D. Lat. 82.7 give 34° , which is S. $34^{\circ} W.$, the Course required, because the Dist. is less than 90° , the Dep. greater than N, and the Lat. is south.

For the Course from C. Horn.

56° (Lat. in) and co-Dist. 29°	
	M 204.5 N 82.2
16° (Lat. to) and Dist. 204.5	Dep. 56.3
	Diff. 25.9

Dist. 100 and D. Lat. 25.9 give 75° , which is N. $75^{\circ} E.$, the Course required, because the Dist. is less than 90° , the Dep. less than N, and the Lat. is south.

By Mercator's Sailing the Course is 50° from either place to the other, and the Distance 3740 miles.

Ex. 2. Find the Distance between Madeira, in lat. $32^{\circ} 38' N.$, long. $16^{\circ} 55' W.$, and Bermuda, in lat. $32^{\circ} 20' N.$, long. $64^{\circ} 51' W.$, and the Course from Madeira.

The D. Long. is $47^{\circ} 56'$; the compl. 42° .

For the Distance.

32° and 33°	M 140.6	N 40.6
42° (co-D. Long.) and 100		Dep. 66.9
		Sum 107.5

Dist. 141 and D. Lat. 107.5 give 40° , or 2400 miles, the Dist. required.

For the Course.

33° (Mad.) and co-Dist. 50°	
	M 185.5 N 77.4
32° (Berm.) and 185.5	Dep. 98.3
	Diff. 20.9

Dist. 100 and D. Lat. 20.9 give 78° , which is N. $78^{\circ} W.$, the Course required, because the Dist. is less than 90° , the Dep. greater than N, and the Lat. north.

Ex. 3. Find the Distance between a point in long. 180° on the equator, and another in lat. $40^{\circ} N.$, long. $140^{\circ} W.$, and the Courses between these points.

For the Distance. Lats. 0° and 40° give M 130.5 and N 0. Then 50° (the co-D. Long.) and Dist. 100 give Dep. 76.6; the sum of N and this is 76.6, and Dist. 130.5 with D. Lat. 76.6 gives 54° , or Dist. 3240 miles.

For the Course from Lat. 0° . 0° and the co-Dist. 36° give M 123.6, N 0; 40° and 124 give Dep. 79.7; Dist. 100 and D. Lat. 79.7 give 37° , which is N. $37^{\circ} E.$, the Course required.

For the Course from Lat. 40° . 40° and 36° give M 161.4, N 61.0 ; 0 and Dist. 161 give Dep. 0; Dist. 100 and D. Lat. 61.0 give 52° , which is S. $52^{\circ} W.$, the Course required as the Dep. 0 is less than N.

338. Case II. *By Inspection.* (The places on *opposite sides* of the equator.)

(1.) For the Distance. With the two lats. take out M and N. (Table 5.)

With the complement of the D. Long. as Course (Table 2), and Dist. 100, find the Dep.

When the D. Long. is *less* than 90° , take the *difference* between this Dep. and N; when the D. Long. is *greater* than 90° , take the *sum*.

With this diff. or sum as D. Lat. and M as Dist. find the Course or arc in Table 2.

When the D. Long. is *less* than 90° . If the Dep. is *greater* than N, this arc is the Dist. required; if the Dep. is *less* than N, take the supplement.

When the D. Long. is *greater* than 90° , take the supplement of the arc.

(2.) For the Course. Having found the Distance, with the Lat. and the complement of the Dist. to 90° , find M and N.

With the Lat. to as course and M as Dist. (Table 2), find the Dep.

When the D. Long. is *less* than 90° , take the *sum* of this Dep. and N; when the D. Long. is *greater* than 90° , take the *difference*.

With this sum or diff. as D. Lat. and Dist. 100 (Table 2), find the Course, which is to be reckoned as follows:—

Dist. <i>less</i> than 90° (or 5400 miles.)	Dist. <i>greater</i> than 90° (or 5400 miles)	
Course to be reckoned in N. lat. from S. in S. lat. from N.	Dep. <i>less</i> than N.	Dep. <i>greater</i> than N.
	Course to be reckoned in N. lat. from N. in S. lat. from S.	Course to be reckoned in N. lat. from S. in S. lat. from N.

Ex. 1. Find the Distance between C. Palmas, in lat. $4^\circ 22' N$. long. $7^\circ 44' W.$, and C. Frio, in lat. $23^\circ 0' S$. long. $41^\circ 57' W.$, and the Course from each place to the other.

The D. Long. is $34^\circ 13'$; the complement is 65° .

For the Distance.

4° and 23° (lats.) give M 108.9 N 3.1
 56° (co-Diff. Long.) and 100 Dep. 82.9
 (D. Long. *less* than 90° .) Diff. 79.9

Dist. 109 and D. Lat. 79.9 give 43° , or Dist. 2580 miles; the compl. is 47° .

For the Course from C. Palmas.

4° (C. Pal.) and 47° M 147.0, N 7.5
 23° (C. Frio) and 147 Dep. 57.4
 (D. Long. *less* than 90° .) Sum 64.9

Dist. 100 and D. Lat. 64.9 give 49° , which is $S. 49^\circ W.$, the Course required, because the Dist. is *less* than 90° and the Lat. is north.

For the Course from C. Frio.

23° (C. Frio) and 47° M 159.3, N 45.5
 $4\frac{1}{2}^\circ$ (C. Pal.) and 159 Dep. 12.5
 Sum 58.0

Dist. 100 and D. Lat. 58.0 give 55° , which is $N. 55^\circ E.$, the Course required, because the Lat. is south.

Ex. 2. Find the Courses and Distance between Diego Ramirez, in lat. $56^\circ 29' S$. long. $68^\circ 43' W.$, and C. Lopatka, in lat. $51^\circ 2' N$. long. $156^\circ 46' E$. The D. Long. is $134^\circ 31'$, the co-D. Long. 45° .

For the Distance. 51° and $56\frac{1}{2}^\circ$ give $M\ 288.0$, $N\ 186.6$. Then $44\frac{1}{2}^\circ$ and Dist. 100 give Dep. 70.1 ; the sum of N . and Dep., or 256.7 as $D.$ Lat., and Dist. 288 , give 27° . or Dist. 153° , or 9180 miles: the co-dist. is 63° .

For the Course from Diego Ramirez. $56\frac{1}{2}^\circ$ and 63° give $M\ 399.1$, $N\ 296.6$; 51° and 399 give Dep. 310.0 ; the diff. 13.4 and Dist. 100 give 82° : COURSE, $N. 82^\circ W.$

For the Course from C. Lopatka. 51° and 63° give $M\ 350.0$, $N\ 242.4$; $56\frac{1}{2}^\circ$ and 350 give Dep. 291.8 ; the diff. 49.4 and Dist. 100 give 60° : COURSE, $S. 60^\circ E.$

339. To find the Courses and the Distance between the places by *Computation*. Find the co-latitudes of the places. If the places are on different sides of the equator, add 90° to the latitude of one of them for its co-latitude. Find the $D.$ Long., and take half of it.

(1.) For the Courses. Take half the sum of the colats. and half their diff. Add together the log. cot. of half the $D.$ Long., the log. sec. of the half sum, and the log. cos. of the half difference: the sum (rejecting tens) is the log. tang. of half the sum of the two courses.

When the half sum of the colats. exceeds 90° , take the supplement of the resulting arc for the half sum required.

To the same log. cot. add the log. cosec. of half the sum of the colats., and the log. sine of half their diff.; the sum (rejecting tens) is the log. tan. of half the difference of the two courses.

The sum of the half sum and half diff. of the two courses is the course from the place in the *smaller* of the two co-latitudes to the other; the *difference* of the said half sum and half diff. is the other course.

The course is to be reckoned from the $N.$ point in north latitude, and from the $S.$ point in south latitude.

Ex. 1. Find the Courses on the great circle, between St. Helena, in lat. $15^\circ 55' S.$, long. $5^\circ 44' W.$, and C. Horn, in lat. $55^\circ 59' S.$, long. $67^\circ 16' W.$

The $D.$ Long. is $61^\circ 32'$; half $D.$ $30^\circ 46'$.

Colat. $34^\circ 5'$ (C. Horn)	$30^\circ 46'$	cot. 0.2252		0.2252	
Colat. $74^\circ 5'$ (St. Helena)					
Sum $108^\circ 6'$	half sum $54^\circ 3'$	sec. 0.2313	cosec. 0.0918	cos. 9.7687	
Diff. $40^\circ 4'$	half diff. $20^\circ 2'$	cos. 9.9729	sin. 9.5347	sin. 9.7089	
	$69^\circ 35'$	tan. 0.4294	$35^\circ 24'$	tan. 9.8517	$69^\circ 35'$ sec. 10.4574
	$35^\circ 24'$			$30^\circ 34'$	cos. 9.9350

COURSE, $S. 104^\circ 59' E.$ from C. Horn, or $N. 75^\circ 1' E.$ 2

COURSE, $S. 34^\circ 11' W.$ from St. Helena. $61^\circ 8' = 3668 m.*$

Ex. 2. Find the Courses on the great circle between Diego Ramirez, in lat. $56^\circ 29' S.$, long. $68^\circ 43' W.$, and C. Lopatka, in lat. $51^\circ 2' N.$, long. $156^\circ 46' E.$

The $D.$ Long. is $134^\circ 31'$; the co-lats. $33^\circ 31'$ and $141^\circ 2'$. The half sum of the required courses is $79^\circ 8'$, and the half diff. $18^\circ 42'$. The sum of these is the COURSE from colat. $33^\circ 31'$, or Diego Ramirez, $S. 97^\circ 50' W.$, or $N. 82^\circ 10' W.$; the diff. is the COURSE from C. Lopatka, or $S. 60^\circ 26' E.$

(2.) For the Distance. By *above method*,* or take the supplement of the Diff. Long. to 12^h or 180° . Add together the two co-lats.

Add together the log. sine square of the said supplement, and the log. sines of the co-latitudes: the sum (rejecting tens) is the log. sine square of an auxiliary arc x .†

Write x under the sum of the colats., and take the sum and difference, and the half sum and half difference.

Add together the log. sines of the last two terms: the sum (rejecting tens) is the log. sine square of the Distance required.

† Log sine square is identical with the log. haversine of Inman's tables.

Ex. Find the Distance between St. Helena, in lat. $15^{\circ} 55' S.$, long. $5^{\circ} 41' W.$, and C. Horn, in lat. $55^{\circ} 59' S.$ and long. $67^{\circ} 16' W.$

Diff. Long.	$61^{\circ} 32'$		
Suppl.	$118^{\circ} 28'$ log. sin. sq.	9'868247
Colat.	$34^{\circ} 1'$ log. sin.	9'747749
Colat.	$74^{\circ} 5'$ log. sin.	9'983022
Sum	$108^{\circ} 6'$		
Arc x	$78^{\circ} 8'$ log. sin. sq.	9'599018
Sum	$186^{\circ} 14'$		
Diff.	$29^{\circ} 58'$		
$\frac{1}{2}$ Sum	$93^{\circ} 7'$ log. sin.	9'999357
$\frac{1}{4}$ Diff.	$14^{\circ} 59'$ log. sin.	9'412524
Distr. $61^{\circ} 4'$, or 3664 miles.		log. sin. sq.	9'411881

The Distance by Mercator's Sailing (No. 327) is 3736 miles, or 72 more.

340. The course on the rhumb line,* from one of two places to the other, is exactly the opposite of the course to that place from the other; while, on the great circle, as appears from the preceding examples, these courses are very different. The ship, while on the rhumb line, is always changing the direction of her head with respect to her port, for which she never steers exactly until it is in sight, because this track cuts all the meridians at the same angle, and the meridians themselves are not parallel to each other; but on a great circle she steers directly for her port, while, as the angle made by her track with the meridians is perpetually varying, the direction of her head appears by the compass to be continually changing. This track, accordingly, is the only one on which the ship nears her port by the whole amount of distance which she makes good from instant to instant.

Great circle sailing includes the case of sailing on a meridian or due N. and S., and on the equator, because the meridians and equator are great circles.

341. While sailing at the same rate on the same rhumb, the ship always changes her latitude by the same quantity; but while sailing at the same rate on the great circle she may change her latitude, not only by unequal quantities, but in opposite directions. For example, suppose the polar seas navigable, then the shortest way for the ship to go from a point in the arctic circle (or any other parallel of north latitude) to another point 180° of longitude from it, and in the same latitude, would be to cross the pole; in which case she would first steer north and then south, whereas on the rhumb line she would constantly steer east or west.

342. The track on the great circle and that on the rhumb line differ most widely from each other in high latitudes, and between places on nearly the same parallels. On the other hand, when the places are on opposite sides of the equator, the great circle and rhumb line intersect each other, and the difference between them is not so conspicuous. In low latitudes, and in all latitudes when the course is nearly on a meridian, the two curves nearly coincide.

343. If the arc of the great circle passing through the two places (not being both on the same meridian or on the equator) be pro-

* Also called the loxodromic curve.

duced beyond them, and carried round the globe, it will pass through two points diametrically opposite in latitude and longitude, which we have called *vertexes*, each of them being the highest point in latitude N. and S., passed through by the circle. The vertex is 90° from the point where the great circle between the places (or produced beyond them) cuts the equator.

When the course shaped on the great circle from each place is less than 90° (reckoning both courses from the nearest pole), the vertex falls between the places. At this point the ship, neither increasing nor diminishing her latitude for a time, steers E. or W. But when the course from one of the places exceeds 90° , the vertex of the circle falls outside the arc joining them.

344. To find the Latitude and Longitude of the Vertex.

(1.) For the Latitude. To the log. cos. of the lat. of one of the places add the log. sine of the course, on the great circle, from this place to the other: the sum is the log. cos. of the lat. required.

(2.) For the Longitude. Add together the log. cosec. of the latitude already employed, and the log. cot. of the course already employed: the sum is the log. tan. of the D. Long. between the vertex and the place worked from.

Ex. 1. Find the vertex of the great circle passing through Rio de Janeiro, in lat. $22^\circ 55'$ S. long. $43^\circ 9'$ W., and the Cape of Good Hope, in lat. $34^\circ 22'$ S. long. $18^\circ 30'$ E.

The Course from Rio is S. $63^\circ 12'$ E., that from the Cape S. $84^\circ 54'$ W.; each of these courses, reckoned from S., being less than 90° , the vertex falls between the places.

Latitude.			Longitude.		
Rio, lat.	$22^\circ 55'$	cos. *9.9643	$22^\circ 55'$	cosec.	0.4096
Course	$63^\circ 12'$	sin. 9.9506	$63^\circ 12'$	cot.	9.7034
LAT. $34^\circ 42'$		cos. 9.9149	D. Long. $52^\circ 23'$	tan.	0.1130
			Rio	$43^\circ 9'$ W.	
			LONG.	$9^\circ 14'$ E.	

Ex. 2. Find the vertex on the great circle passing through St. Helena and C. Horn.

By Ex. No. 339, the Course from St. Helena is S. $34^\circ 12'$ W., that from C. Horn is S. $104^\circ 58'$ E.; since one of these courses exceeds 90° , the vertex falls without.

Ans. Lat. $47^\circ 17'$ S.; Long. $85^\circ 10'$ W.

345. When the ship sails on a great circle between two places on the same side of the equator, she is always in a *higher latitude* than if she had sailed on the rhumb line; hence, since both tracks coincide at their extremities, there must be a point in the great circle at which its distance from the rhumb line, measured on a meridian, is greater than anywhere else; this point we shall call the point of *Maximum Separation in Latitude*.

When the ship crosses the equator, there are two such points, the one being to the northward of the rhumb line in north latitude, and the other to the southward of the rhumb line in south latitude.

346. The track of the great circle between any two points

* As none but the logarithmic sines, cosines, &c. are employed in this work, except in No. 254, we shall henceforth, for brevity, dispense with the abbreviation *log.* in the examples.

may be conveniently shewn, by determining the latitude of its point of intersection with each of a certain number of intervening meridians, the degree of exactness being increased according to the number of meridians taken.

To find the latitude of the point where the great circle passing through two places intersects any given meridian,

Find the position of the vertex (No. 344).

To the log. tan. of the lat. of the vertex add the log. cos. of the difference of long. between it and the given meridian, and the sum is the log. tan. of the required latitude.

Ex. Find the latitude of the point where the great circle passing through St. Helena and Cape Horn intersects the meridian of 30° W.

Vertex (Ex. 2. 344) lat. $57^{\circ} 17'$ S., long. $85^{\circ} 10'$ W.

Latitude $57^{\circ} 17'$ tan. 0.922

Diff. Longitude $55^{\circ} 10'$ cos. 9.7568

Required Latitude $41^{\circ} 39'$ tan. 9.9490

The log. tan. of the lat. of the vertex being constant, the lats. of the points of intersection of the great circle with any desired number of meridians may thus be rapidly computed.

347. To facilitate the practice of Great Circle Sailing, Mr. J. T. Towson in 1847 devised a method by which, using a diagram and a table, the successive courses on the great circle can be found without the labour of calculation.*

The manner of projecting the track, and of measuring the distance on Mercator's chart, are described in Chap. V. Other matters demanding consideration when it is proposed to make a voyage on a great circle, are treated in the division of the work appropriated to Navigating the Ship.†

* Towson's Tables for facilitating Great Circle Sailing. Sold by J. D. Potter, 145 Minories, London, E.

† The Azimuth and Star-azimuth Tables of Burdwood and Davis also facilitate Great Circle Sailing. The lat. in being taken as the Lat., the lat. of the port bound to as the Dec., and the diff. long. as the Hour-angle, gives the Azimuth, which will be the True Course. From these the Great Circle Course may be projected on the Chart. See Burdwood and Davis' Azimuth Tables, published by Potter, 145 Minories.

Ex., a ship bound from Cape King, entrance of Yedo Bay, to San Francisco. Cape King, lat. $34^{\circ} 54'$ N., long. $139^{\circ} 53'$ E. San Francisco, lat. $37^{\circ} 48'$ N., long. $122^{\circ} 29'$ W. Diff. long. $97^{\circ} 38'$, or $6^{\text{h}} 30^{\text{m}} 32^{\text{s}}$.

Lat. in.	Lat. bound to.	Diff. long. as Hour-angle.	Azimuth or True Course.	Cutting Mer. of
35°	38°	$6^{\text{h}} 30^{\text{m}}$	N. 54° E.	150° E in lat 41°
41	38	5 50	N. 61 E.	160 E. " 45
45	38	5 10	N. 68 E.	170 E. " 48
48	38	4 30	N. 75 E.	180 " 49
49	38	3 50	N. 83 E.	170 W. " 50
50	38	3 10	N. 91 E.	160 W. " 50
50	38	2 30	N. 100 E.	150 W. " 49
49	38	1 50	N. 109 E.	140 W. " 47
47	38	1 10	N. 119 E.	130 W. " 43
43	38	N. 131 E.	San Francisco.

CHAPTER IV.

TAKING DEPARTURES.

I BY A SINGLE BEARING AND DISTANCE. II. DETERMINATION OF DISTANCE. III. METHODS BY THE CHART.

348. DETERMINING the place of the ship with reference to a point of land, or other position of known latitude and longitude, is called *Taking a Departure*.

The position of the ship with respect to a point of land or other fixed and conspicuous object is defined by the *direction* in which she lies, and her *distance* from it.

The *direction* or bearing of the ship from the land, being the opposite of the bearing of the land from the ship, is furnished at once by the compass, or it may be found by observation of an *Astronomical Bearing*; but the *distance* from the point, when it cannot be estimated or guessed with sufficient precision, must be deduced by means of some further observation, taken at the same time as the bearing, or after an interval.

When a former position of the ship herself is adopted as a point of departure, the direction (or course) and the distance are deduced from the reckoning.

I. BY A SINGLE BEARING AND DISTANCE.

349. The object being set by the compass, its distance is estimated by the eye.

This, which is the common method of taking departures, is near enough when the distance is small; but the error or uncertainty in the estimation of the distance, which, perhaps, may be stated generally at one-fifth of the whole, becomes considerable when the distance is great. Distances thus estimated are generally overrated.

II. DETERMINATION OF DISTANCE.

1. *By two Bearings of the same Object.*

350. When the ship's path lies across the line of direction of the object, the distance can be obtained by two bearings and the distance run by the ship in the interval of time between them

Take the bearing of the object, and note the number of points contained between it and the ship's head. After the bearing has altered not less than two or three points, note the number of points in the same angle again.

NOTE. The course and distance between the positions must be those actually made good.

(1.) To find the distance when the *last* bearing was taken.

Enter Table 7 with the first number of points at the top and the second number of points at the side; take out the number corresponding, and multiply it by the number of miles made good by the ship: the result is the dist. in miles at the time the *last* bearing was taken.*

Ex. The Eddystone bore N.W. by W.; after running W. by S. 8 miles, it bore N.N.E.: required its Dist. at this last bearing.

The number of points between N.W. by W. and W. by S. is 4; that between N.N.E. and W. by S. is 11; under 4 at the top and against 11 at the side stands 0.72, which multiplied by 8 (miles), gives 5.8 miles, the Dist. required.

The student can easily supply a figure.

(2.) To find the distance when the *first* bearing was taken.

Enter the Table with the supplement (or difference from 16 points) of the second number of points at the top, and the supplement of the first number of points at the side; take out the multiplier, and proceed as above directed.

Ex. Find the Distance of the Eddystone at the time the first bearing (or N.W. by W. above) was taken.

The second number of points is 11, the supplement of which is 5; the first number is 4 points, the supplement of which is 12; then 5 at the top and 12 at the side give the number 0.85, which multiplied by 8 gives 6.8 miles, the Dist. required.

When the number of points between the object and the ship's head at either observation is 8, that is, when the bearing is at right angles to the course, the distance may be found by the Traverse Table, by entering the table with the number of points at the other observation as a course, and the distance run as D. Lat.; the corresponding Dep. is the distance of the object when observed at 90° from the course.

351. If the time be noted when an object is 4 points on the bow, and again when it is right abeam, the distance run in the interval on the same course is evidently equal to the distance off the object when abeam. This case is called the *Four-point bearing*. It is, however, only a case of the general problem. If a ship having a point of land or other object at any angle on the bow, proceeds steering the same course till a position is reached where the angle on the bow is doubled, the distance from the object at the last position is equal to the distance between the two positions. The case is most favourable when from the positions chosen the object is 30° before and 30° abaft the beam; the triangle is then equilateral.

* This Table was constructed at the suggestion of Sir F. Beaufort, and first appeared in the *Nautical Magazine*, vol. i. p. 208

The error of the required distance produced by an error in the dist. run, is a matter of simple proportion. For example, if the dist. run be $\frac{1}{10}$ of itself in error, the distance required will also be $\frac{1}{10}$ of itself in error. Hence the dist. run should not be much less than the distance required.

2. By Sound.

352. An excellent mode of determining the distance is obtained by noting the number of seconds elapsed between seeing the flash of a gun and hearing the report. Sound travels, in a calm, about 1130 feet in one second at a temperature of 66° Fahr.; hence it is easy to deduce the following approximate rule.

Divide the seconds elapsed by 5, and subtract from the quotient $\frac{1}{3}$ of itself; the result is the Dist. in miles very nearly.

Ex. The mean of the intervals given by 4 guns fired from O. Shilling was 14 $\frac{1}{2}$ required the Dist. of the ship.

$$\begin{array}{r} 5) \ 14\frac{1}{2} \\ \underline{2\frac{8}{2}} \\ 1\text{-twelfth of } 2\frac{8}{2} \\ \underline{} \\ \text{Dist. } 2\frac{6}{2} \end{array}$$

This method is capable of much precision when the gun and the ear are at the same temperature and at the same height.* A moderate breeze in the direction of the sound causes a variation of about 20 feet a second in the velocity; a strong breeze more.

3. By the Altitude of High Land.

[1.] *When the Object is seen on the Sea-Horizon.*

353. The distance of the visible horizon from the spectator is equal to the true depression or dip of the eye in Table 8, increased by about $\frac{1}{3}$ of itself.† Thus, if the eye be twenty feet above the sea, the horizon is distant five miles and about half a mile more.

When, therefore, the sea-horizon is seen beyond the object, the distance of the latter is less than the depression.

354. When the summit, or any other point of known height of an object situated beyond the sea-horizon is seen *on this line*, its distance is at once known; for since the eye, the horizon, and the object are in the same straight line, the same horizon corresponds to both the height of the eye and that of the object; the distance, therefore, between these two points is, by No. 205, the sum of the depressions corresponding to the two heights.

Ex. From the mast-head, 87 feet above the sea, the Lizard Light, the height of which is 123 feet above low-water mark, is seen on the horizon: required its distance.

The dip (Table 8) to 87 feet is 10', that to 223 is 16'; the sum 26 increased by $\frac{1}{3}$ of 26, or 2', is 28 miles the Dist. required.

* The uncertainty to which this method is liable (though not worth notice in navigation) may, when precision is required, be removed, in the ordinary state of the atmosphere, by firing a gun at each extremity of the line, and taking the mean of the observed intervals.

† In this and the following rules $\frac{1}{12}$ is used instead of $\frac{1}{3}$ (see No. 207), because 12 is an easier divisor than 14. The difference is not worth notice.

This method will often be useful, but from the great uncertainty of terrestrial refraction it is impossible to assign with precision the degree of dependance.

[2.] *When the Object is seen above the Sea-Horizon.*

355. Case I. When the height of the summit, or other point of high land, is known, its distance is found by means of the altitude observed above the sea-horizon with a quadrant or sextant.*

356. *The Observation.* Observe the altitude of the summit, and estimate its distance in miles.

When the altitude exceeds 3° see No. 359.

357. *The Computation.* Alt. under 3° . (1.) Correct the alt. for index error (No. 496), and subtract from it $\frac{1}{2}$ of the estimated distance; the remainder is the true alt.

When the height of the eye exceeds 30 feet, add $\frac{1}{2}$ of the corresponding Depression; the sum is the true altitude.

(2.) From the true alt. subtract the true Depression to the height of the eye, Table 8: note the remainder.

To the square of the Depression corresponding to the height of the summit add the square of the remainder (which is found at once in the column headed "Square," against the remainder as a Depression). Look for the sum in the column headed "Square," and take out the Depression corresponding; from this take the remainder: the result is the distance of the summit in miles.†

Ex. 1. The alt. of a hill 2000 feet high is observed $56'$; corr. for index error, $-3'$; the height of the eye, 20 feet; estimated Dist. 8 leagues, or 24 miles: required its Distance.

Deducting $\frac{1}{2}$ of 24, or $2'$, and $3'$ error, leaves true alt. $51'$.

True alt.	51'	Square of Depr. to 2000 ft.	2304
True Depr. to 20 ft.	$-\frac{5}{46}$	Ditto of Rem. $46'$	+ 2116
Rem.	46	Depr. $67'$ Square	4420
		Rem. -46	
		Dist. required	$21'$ or miles.

Ex. 2. April 19th, 1829, Mr. Fisher observed from the poop of H.M.S. Spartiate, 74, the alt. of Mount Etna, $1^{\circ} 26' 30''$; index corr. $+ 1' 30''$; height of eye, 30 feet; estimated dist. 20 leagues: required its Distance. Height of Etna, 10900 feet.

$\frac{1}{2}$ of $60'$, $-5'$	$1^{\circ} 26'$	Square of Depr. to 10900 ft.	12321
Ind. cor. $+ 2$	-3	Ditto of Rem. $77'$	+ 5929
Alt.	1 23	Depr. $135'$ Square	18250
True Dep. to 30 ft.	-6	Rem. -77	
Rem.	1 17 or $77'$	Dist. required	$58'$ or miles.

The distance by the chart was 57 miles.

358. When the distance is too great for estimation, and the altitude low, the computation must be repeated.

Ex. Captain Beechey observed from H.M.S. Sulphur, the Peak of Teneriffe clearly defined against the setting sun; mean of 3 alts. on the arc, $19' 32''$; off the arc, $19' 50''$: the

* In this instance, reference is necessarily made to the use of instruments which belong principally to Nautical Astronomy, and are, therefore, described in that subject, Chap. II.

† When the height of the eye exceeds 30 feet, subtract from the sum of the two squares (above) the square of the corresponding Depression. From the nature of the observation, it is enough to work to minutes only.

mean, 19 41; height of the eye, 18 feet; height of the Peak, 12172 feet: required its Distance.

Alt.	20'	Square of Depr. to 12200 ft.	13689
Depr.	— 4	Ditto of Rem. 16'	+ 256
Rem.	16	Depr. 118'	Square 13944
		— 16	
		Dist. required 102' or miles.	

Using this now as an *estimated* distance, and repeating the work, gives 109 miles. It was found next day by the chronometers to have been 115 miles.

359. When the altitude is great, or above 30° , the following rule for the computation is preferable to No. 357:—

(1.) Correct the altitude for index error, subtract from it $\frac{1}{2}$ of the estimated distance in miles, subtract further the true Depr. of the eye (Table 8), and note the remainder.

When the height of the eye exceeds 30 feet, increase the remainder by $\frac{1}{2}$ of the depression.

(2.) Add the log. cos. of this remainder to the log. cos. of the Depr. corresponding to the height of the mountain; the sum (rejecting 10) is the log. cos. of an arc. From this arc take the said remainder, this leaves the Dist. of the summit in miles.

Ex. Mr. Fisher observed the altitude of Mount Etna, $5^\circ 15'$; height of the eye, 30 feet; estimated distance, 8 leagues, or 24 miles: required its Distance.

Alt.	$5^\circ 15'$	Etna, ht. 10900 ft. Dep.	$1^\circ 51'$	cos.	9.999774
$\frac{1}{2}$ of 24	— 2	Remainder 5 8	cos.	9.998255
Depr.	— 5	Remainder $5^\circ 27'$	cos.	9.998029
			Remainder 5 8		
			Dist.		19 miles.

360. *Degree of Dependence.* To judge of this, repeat the computation, using a new altitude, varied from the former by a number of minutes equal to the extent of the probable uncertainty.

For example. Suppose in Ex. 1, No. 357, the altitude doubtful, or in error, 5'; repeating the work, with the altitude $46'$, gives the distance 23 miles, instead of 21: hence we infer that, supposing 5' to be in this case the utmost probable uncertainty in the altitude, the distance may be depended upon to 2 miles.

The greater the altitude the more accurate is the result.

361. Case II. When the height of the land is not known, the distance may be found while standing directly towards it, or from it, by means of two altitudes, and the distance run in the interval between them.

If the course is not more than two points out of the direction of the object, the distance run may be reduced to the change of distance of the object by means of the Traverse Table.

362. *The Observation.* Observe the altitude. After a considerable change in the altitude, observe a second altitude at the same height of the eye. Note the rate of sailing. Estimate the distance at each observation.

363. *The Computation.* Find the true altitudes, No. 357. (1.) Find from the rate of sailing the dist. run, and reduce it when necessary to the change of distance made good in the direction of the object, thus,—enter Table 1 with the difference between the ship's

coarse and the bearing of the object as a Course, and the Dist. run as Dist.; the corresponding D. Lat. is the change of distance required.

To the lesser altitude add half the change of distance, and subtract the Depr. corresponding to the height of the eye; call this the first remainder. From the greater altitude subtract the lesser altitude, and the change of distance; call this remainder the second remainder.

Multiply the first remainder by the change of distance, and divide the product by the second remainder; the quotient is the distance in miles when the *greater* altitude was taken.

Ex. 1. Observed altitude of Mount Etna, $1^{\circ} 28'$; estimated distance, 20 leagues. When 38 miles nearer, observed the altitude $5^{\circ} 15'$; height of the eye, 30 feet: required the Distance.

$1^{\circ} 28'$, deducting $\frac{1}{2}$ of 60 miles or 5', is $1^{\circ} 23'$; $5^{\circ} 15'$, deducting $\frac{1}{2}$ of 22 miles or 2', is $5^{\circ} 13'$.

Lesser Alt.	$1^{\circ} 23'$	Greater Alt.	$5^{\circ} 13'$	then $\frac{96 \times 38}{192} = 19$ miles, the Dist. required.
$\frac{1}{2}$ Dist. run	+ 19	Lesser do. $1^{\circ} 23'$	- 2 1	
Depr.	- 6	Dist.	+ 38	
1st rem.	$\frac{1 \ 36}{96}$	2d rem.	$\frac{3 \ 12}{192}$	
or	$\frac{1 \ 36}{96}$	or	$\frac{3 \ 12}{192}$	

Ex. 2. Observed the altitude of Dunnose $41'$, estimated distance 4 leagues or 12 miles. After running $7\frac{1}{2}$ miles directly from it observed the alt. $20'$. Height of the eye, 10 feet.

The 1st alt. reduced is $18'$; the 2d, $40'$. The 1st rem. is 18.7 ; the 2d, 14.5 : the Dist. required 9.7 miles.

364. *Degree of Dependence.* This may be estimated by repeating the work with a new lesser alt., and also with a new change of distance, differing from those used before by $1'$, and comparing these two results with the first. If they do not differ much, the case is evidently but little affected by small errors; if, on the contrary, they differ more than $1'$, it is shewn that errors of observation are increased in the result.

Thus an error of $1'$ in the lesser alt. produces in Ex. 1, above, only 0.3 of a mile error in the distance required, while in Ex. 2, the latter error is 1.2 .

Again, an error of 1 mile in the change of distance produces in Ex. 1 only 0.7 of a mile in the result, while in Ex. 2, it produces 2.4 miles.

In ordinary cases an error of $1'$ or $2'$ is more likely to occur in an alt. than an error of 1 or 2 miles in the change of distance; and as precision is of less consequence in the greater than in the lesser alt. the value of the result will depend principally on the lesser altitude.

The less the 1st rem. is with respect to the 2d, the less is the effect produced by the above errors on the result.

Thus, in Ex. 1, the 1st rem. is to the 2d, or 96 is to 192, as 1 to 2 nearly, and the case is good. In Ex. 2, on the contrary, the 1st rem. 18.7 , is greater than the 2d, 14.5 , and the result could not be depended upon within 2 or 3 miles.

365. Since these rules suppose the object to be referred to the sea-horizon, they apply to all cases in which the observer, though near the land, can descend so near the surface of the water as to obtain a perfect sea-horizon.

On the other hand, when the land is very distant, or the altitude

very small, the methods in this section must not be too confidently depended upon, especially in a calm, or when, from heat, vapour, or other cause, there is anything unusual in the appearance of the horizon.

Useful tables of *Vertical Danger Angles* of heights from 50 to 18,000 feet, to distances off; from one cable to 110 miles, have been calculated by Lieut. S. T. S. Lecky, R.N.R. Published by George Philip & Son, London and Liverpool, 5th Edition, 1890.

III. METHODS BY THE CHART.

1. *Cross Bearings.*

366. The *true* bearings of two points of land being obtained, draw lines through them on the chart in the directions of the bearings; these lines cross in the place of the ship.

Or a *true* bearing of one of the points of land may be obtained, and an angle measured by the sextant (Nos. 485-504) between it and a second point, when the second point cannot be conveniently seen from the compass.

367. When the difference of bearings is near 90° , this is the most complete of all methods; but if the difference is small, as for example, less than 10° or 20° , or near 180° , the ship's position will be uncertain, because a small error in the bearing will then cause a great error in the distance.

2. *By Two Angles between Three Objects.*

368. When the ship's place is required to considerable accuracy, as, for example, in recovering a lost anchor, verifying the soundings on the chart, or other purposes, it should be determined by means of two angles observed between three objects on shore.

(1.) A convenient method of laying down on the chart the angles observed, is to draw with a pencil on tracing or transparent paper, or on paper oiled for the purpose, lines containing the observed angles; then, laying this paper on the chart, and moving it about until the lines drawn pass over the respective objects. The angular point where they meet will shew the true place of the observer.

The horn protractor (No. 108) may sometimes be conveniently employed, as lines may be drawn on it with a pencil.*

369. *By Construction.* The observer is always on a circle passing through his own place and any two objects (No. 103); also the angle

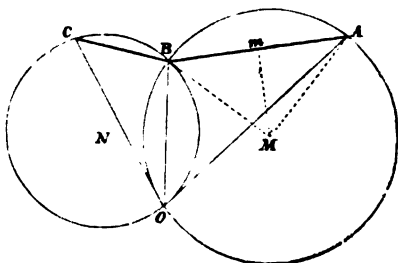
* The Station-pointer, an instrument used in this case to fix a ship's position, consists of three flat rulers, two movable from a common centre right and left of the third, which is fixed. The angular distance at which the movable rulers are required to be placed on either side of the fixed ruler being measured by an attached circular arc.

subtended by the two objects is the same at all points of the circumference on one side of the objects (No. 140). Hence, by observing this angle and laying it off, he can draw the circle on which he is, but cannot determine his position upon it. If now he adds a third object, he can draw a second circle passing through this and either of the other two, and his place is the intersection of the two circles.

Ex. 1. Let ABC be three objects on the chart; the angle between A and B , formed at O , the observer, is 46° ; that between B and C is 30° .

Join AB, BC ; lay off the angles BAM, ABM , each equal to the complement of 46° , or 44° ; then the intersection of the lines AM, BM , is the centre of the circle ABO .

In like manner lay off BCN, CBN , each equal to the complement of 30° , or 60° ; then N is the centre of the circle BCO , and O is the place of the observer.

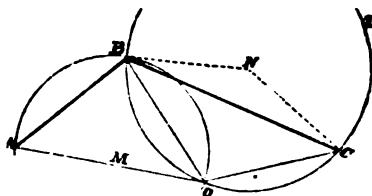


The drawing of the figure is materially simplified, in practice, by the bearing of the middle object, as this shews where the lines must fall.

Ex. 2. The angle between two objects A, B , is 47° , that between B and C is 107° .

Lay off ABM, BAM , each equal to 43° ; M is the centre of ABO .

Lay off CBN, BCN , each equal to the complement of 107° , or 17° , then N is the centre of BCO .



370. Demonstration. Having laid off two equal angles ABM, BAM , and described a circle from M the point of intersection of AM, BM , bisect AB (fig. Ex. 1) in m , and join mN ; also take a point O any where in the circumference, and join OA, OB .

Then Mm is perp. to AB (No. 144), and also bisects the angle AMB (cor.) or AMm is half AMB . Also AOB at the circumference is half AMB at the centre (No. 139); hence, AOB and mMA are equal, and mMA the complement of AMm is also the complement of AOB . A circle therefore has been described which has the given angle at the circumference.

The same proof applies when the angle at O exceeds 90° . Thus, in fig. Ex. 2, $BOC, 107^\circ$, is measured by half the arc BDC (supposing the circle completed, and BD, DC , joined), which is therefore 214° . Hence the arc BOC is $360^\circ - 214^\circ$, or 146° , and the angle BDC measured by half this, is 73° ; BNC is $2 \times 73^\circ$, or 146° , and NBC (or NCB its equal), which is the complement of half BNC , is $90^\circ - 73^\circ$, or 17° , which is the complement of 107° .

371. It is evident that the place of O is most distinctly marked when the circles cross each other at a considerable angle; and, on the other hand, that the result is unsatisfactory when the two circles nearly coincide, or when their centres are near together. These conditions govern the choice of objects.

372. In thus fixing the ship by two angles observed between

three well-known objects on shore, the centre object should always be the nearest; for if the ship should happen to be on the circumference of the circle passing through the three selected points, her position cannot be obtained by the means of two angles only. A *true bearing* of one of the objects is therefore desirable.

It will readily be seen that in war time, when the compass may be knocked away, or ride-fire may make it undesirable to expose the person more than necessary, a sextant offers great advantages, as angles can be obtained from any position whence the objects are visible. It is this contingency that makes it especially desirable that sailors should become expert in the method of fixing a ship's position with the sextant.

3. *By the Soundings.*

373. When the depth of water is not great, and also varies sensibly with the distance from the point of land set, this distance may be found from the chart by means of the soundings.

4. *By a Bearing, and the Lat. or Long. of the Ship.*

374. When the lat. of the ship is known, the true bearing of a well-fixed point, less than 4 points from the meridian, or not much more, affords a very accurate departure. In like manner, when the long. of the ship is known, the bearing of a given point more than 4 points from the meridian, or not much less, affords the departure.

In certain cases the bearing (alone) of a point of land may be determined from the long. by chronometer. See Sumner's Method, p. 363.

CHAPTER V.

CHARTS.

I. USE OF MERCATOR'S CHART. II. CONSTRUCTION OF MERCATOR'S CHART. III. PROPERTIES OF CERTAIN PROJECTIONS.

375. A CHART is a map or plan of a sea or coast. It is constructed for the purpose of ascertaining the position of the ship with reference to the land, and of shaping a course to any place.

376. In charts, the upper part, as the spectator holds it, is the north, and that towards his right hand the east, as on the compass card; latitude is accordingly measured between the upper and lower edges, and longitude between the right-hand and left-hand edges.

Parallels of latitude and meridians are drawn at convenient divisions of latitude and longitude. Compasses are described, by means of which a line can be readily drawn in any proposed direction; and the variation is marked where convenient. The depth of water, at low water springs, is denoted, as also, in some places, the quality of the bottom. The directions and velocities of currents are expressed, and on some occasions the prevailing winds are marked.*

* Charts are also constructed for special purposes, as *variation charts*, to exhibit the variation, as well as *current charts*, *wind charts*, and *ice charts*.

Caution.—In purchasing Admiralty charts care should be taken to see that they are corrected up to date. The dates of large corrections are noted on the middle of the lower edge; and of small corrections, in the lower left-hand corner of the chart.

377. Besides charts employed in general navigation, *plans* of harbours, ports, islands, or small districts, are constructed on a different scale, for reference when the ship is close in with the land. On these plans are inserted, besides the above particulars, the leading marks for channels or for avoiding certain dangers, anchorages, places convenient for landing, and for watering, with numerous other details proper to maps. Plans of these kinds are often inserted, for convenience, in a corner of the general chart.*

378. As the surface of the globe is round, while that of the paper is flat, every chart exhibiting any extent of surface is necessarily an artificial construction, or, as it is called, *projection*, of the real state of things. The charts used in navigation are those on Mercator's projection, because on this alone the track of a ship always steering the same course appears a straight line.

379. On Mercator's Chart all the meridians are parallel, and the degrees of longitude are all equal, being the same as those of the *true* difference of latitude. The degrees of latitude are unequal, being extended at each latitude beyond their proper lengths, in the same proportion as the degrees of longitude on the globe are diminished; they are consequently greater as the latitude is greater.

For Ex. the degree of lat. 60° , that is, between $59\frac{1}{2}^\circ$ and $60\frac{1}{2}^\circ$, is double of 1° at the equator, being increased in the ratio of the sec. lat. : 1.

I. USE OF MERCATOR'S CHART.

1. *Positions on the Chart.*

380. To find the latitude and longitude of a point on the chart.

Through the given point lay a ruler parallel to the nearest parallel of latitude, and look at what degree and minute the edge cuts the graduated meridian at the side, on which the latitude is marked. In like manner lay the ruler parallel to the nearest meridian, and see where the edge cuts the graduated parallel of latitude at the upper or lower edge, on which the longitude is marked.

Or measure, by the compasses or otherwise, the distance of the given point from the nearest parallel of latitude, and setting off this distance from the same parallel on the graduated meridian at the side, note the degree and minute there expressed.

In like manner, for the longitude, refer the point to the nearest meridian, along the graduated parallel at the upper or lower edge.

381. To find the bearing or course on the rhumb line between two places. Lay the edge of the ruler on the places, and refer it to the nearest compass.

Or, hold the thread of the horn protractor (No. 108) on one of the places, and placing the centre and the zero on a meridian, slide

* The paper on which charts are printed has to be damped. On drying distortion takes place, from the inequalities of the paper. This distortion varies greatly with different paper. It does not affect navigation; but angles taken at different points will not always agree when carefully plotted, especially if the lines to the objects be long. The larger the chart, the greater the amount of this distortion.

it with the other held up or down till the thread covers both the places; the bearing then will be read off on the graduated edge.

382. To find the distance on the rhumb line between two places.

(1.) When the places are on the same meridian. Find, by means of the ruler, where their parallels of latitude meet the graduated meridian at the side: the Diff. Lat. they include is the distance.

(2.) When the places are on a parallel of latitude. Take one or more divisions of the graduated meridian at the parallel in the compasses, and measure with this the distance of the places; or proceed as directed in (3).

(3.) When the places lie obliquely. Take the distance between them by a pair of compasses, and lay it on the graduated meridian so as to be middled by the *middle* parallel between the places: the D. Lat. is the distance.

Of the above modes of measuring distances on the chart the first is accurate. The other two are only approximate, though near enough for common purposes.

When precision is required, the 2d case, which is Case II. of Parallel Sailing, must be solved by No. 307, 308, or 309, as the chart affords no facility. In like manner, if the places are nearly E. and W., the distance should be found by Case II. of Mid. Lat. Sailing, p. 100. In the 3d case, the construction described in No. 328 must be employed. For this the chart is particularly adapted, as it shews the Mer. D. Lat. The true D. Lat. is to be taken from the scale of longitude.

383. To lay off a point on the chart in a given lat. and long. Lay a ruler through the lat. at the side, and parallel to a parallel of lat. draw a pencil line. Do the same with the longitude.

384. The course and distance of the ship on the rhumb line being given from any point, to find her place on the chart.

Lay the ruler through the given point, in the direction of the course. Take the given dist. in degrees and minutes from the graduated meridian, so that the parallel of lat. which the ship is upon shall middle it; lay off this distance along the edge of the ruler from the given point, and the ship's place is determined.

385. To lay down on the chart the position of the ship as given by observation. Lay off the given latitude and longitude as directed, No. 383.

To lay down on the chart the position of the ship by D. R., that is, by her course and distance from a given point of departure; as, for example, her place at last noon.

Lay off the course and distance as directed in No. 384.

Marking the ship's position on the chart is called *pricking* the ship off.

2. *Projection of the Voyage on a Great Circle.*

386. The Great Circle track between any two places may be accurately traced on a Mercator's Chart, by determining the latitudes of its points of intersection with any desired number of intervening meridians. These lats. may be computed (346), or found by the aid of Towson's Tables or Davis's Azimuth Tables (347).

387. But since the course and distance are liable to irregularities of which the Dead Reckoning can take no account, a sailing ship especially cannot be kept for any length of time upon a prescribed track; and since, when she has once deviated from the intended line, the course must be shaped anew, it is evident that the accurate projection of a proposed voyage on a great circle sometimes would be waste of labour. It will accordingly be sufficient, in general, to project the track roughly.

388. The following method by Professor Airy, for drawing on a Mercator's Chart the arc of a great circle between positions on one side of the Equator, is very simple and sufficiently accurate for practical purposes generally.

1.—Join the two points, between which it is required to project the great circle, by a straight line. Bisect this line, and from the point of section erect a perpendicular to the line on the side next the Equator, continuing it, if necessary, beyond the Equator.

2.—With the middle latitude (between the two places) enter the following table, and take out the "corresponding parallel."

3.—The centre of the arc of the great circle, required to be drawn, will be the intersection of this parallel with the perpendicular.

Middle Latitude.	Corresponding Parallel.	Middle Latitude.	Corresponding Parallel.
20°	81° 13'	58°	4° 0'
22	78 16	61	9 15
24	74 59	62	14 32
26	71 26	64	19 50
28	67 38	66	25 9
30	63 37	68	30 30
32	59 25	70	35 52
34	55 5	72	41 14
36	50 36	74	46 37
38	46 0	76	52 1
40	41 18	78	57 25
42	36 31	80	62 51
44	31 38		
46	26 42		
48	21 42		
50	16 39		
52	11 33		
54	6 24		
56	1 13		

N.B.—If greater accuracy is required the curve of the Great Circle should be drawn by the methods of Godfray, Towson, or by computation.

389. Godfray's Great Circle Chart and Course and Distance Diagram answer all the conditions of great circle sailing as completely and as simply as Mercator's Chart does for sailing on a Rhumb. The track is a straight line which may be drawn and examined; then the various courses and the distances to be run upon each course are obtained, as also the distance from the ship to her destination, by a mere inspection of the diagram.*

3. Figures of Different Tracks.

390. The track of a ship by Mercator's or by Middle Latitude Sailing, appears, as before stated (No. 378), a straight line on Mercator's Chart, on which the meridians and parallels of latitude are represented as straight lines. But on the globe such a course, unless it be N. or S., is really a *spiral*, winding towards one of the poles, which it can never reach. A ship's keel cannot pass over a point which is kept at any angle on the bow.

* See Chart to facilitate the practice of Great Circle Sailing, with accompanying Diagram for the determination of Courses and Distances: by Hugh Godfray, Esq., M.A. sold by J. D. Potter, 146 Minories, London, E.

The track by Parallel Sailing, on a circle on which the ship always maintains the same distance from the pole, also appears a straight line upon the chart.

The track by Great Circle Sailing, except when on a meridian, appears on Mercator's Chart as a curve line. It may at first seem inconsistent that a curve line can, in any case, represent a shorter distance than a straight line; but every point of this curve line is nearer the pole than a point in the same longitude on the track by Mercator: and accordingly, if we divide the curve into small portions, and measure each portion as in No. 382 (2), or (3), in its own latitude, we shall find that the whole distance measures absolutely less than the length of the rhumb line joining the places.*

II. CONSTRUCTION OF MERCATOR'S CHART.

391. The following instructions are merely general: practice will supply details.

In N. Lat. draw a line along the foot of the paper for the parallel of lowest latitude. In S. Lat. draw the line along the top. Divide this line into degrees and parts, as 30', 15', 10', or 5'. Draw at the sides two perpendiculars to this line, for the graduated meridians. Find, by Table 6, the Mer. D. Lat. between the lowest parallel and 1°, or 30', &c. above it. Take with the compasses this Mer. D. Lat. from the equally divided parallel, and set it off from this line on the meridian to be graduated. Find, in like manner, the Mer. D. Lat. between the said parallel and 2°, or 1°, &c. above it. In this way the meridians are graduated.

Parallels and meridians being drawn at convenient intervals, and the points of the coasts laid down, the coast-line is filled in by hand.

III. PROPERTIES OF CERTAIN PROJECTIONS.

392. Since a small portion of a globular surface may be considered, in a practical sense, as a plane, charts of coasts, and maps of

* In order to verify, on a globe, the results of calculations relating to the great circle and the rhumb line, the latter must be projected on the globe. To do this, note on the chart the latitude and longitude through which the rhumb line passes, at each 4° or 5°, or less, according to the degree of precision required; then lay off these points on the globe, in their several lats. and longs. by means of the moveable meridian. A curve traced by hand through the points laid off will represent the rhumb line nearly enough.

If the rhumb line between any two places, differing considerably in latitude and longitude, be produced on the chart, and transferred thus to the globe, its spiral figure will be distinctly perceived.

districts of limited extent, constructed from a scale of equal parts, exhibit, like the plan of a building or an estate, the relative *directions* and *distances* of the places upon them very nearly. On this projection, divisions of latitude and longitude may be laid off in their due proportions by means of parallel and perpendicular lines, drawn at proper distances. In drawing these lines the minute or mile of latitude is taken as the unit of measure (Nos. 186, 199), and the parallels of latitude drawn through certain divisions. The length of a minute of longitude being to that of a minute of latitude as the cosine of the latitude to the radius, is determined by No. 304, 305, or 306. On a small portion of the surface the minutes of longitude are nearly equal, and the meridians are therefore drawn parallel; but if the extent of latitude be increased, the meridians will converge sensibly towards the polar side of the chart (No. 194, note *) and the character of the projection changes.*

393. On Mercator's Chart the figure of each small district or portion of surface is truly represented, as in No. 392 above; but, as the mile or minute of latitude, which is the unit of measure, is of a different magnitude in every different latitude, if we take a greater extent of latitude we introduce a new scale of measurement. A small island, for example, near the pole, is represented, in regard to its shape, as truly as another near the equator, but on a larger scale: hence, though each small portion is truly figured, portions in different latitudes cannot be directly compared. The appearance of distortion of the countries on Mercator's Chart arises, therefore, from the distances in each latitude being drawn to a different scale.

This projection represents, with perfect accuracy, the relative positions of places as respects a rhumb line; it does not, however, exhibit the relative distances between places, which, when required with precision, must be found by the proper construction, No. 328.

The projections here described become identical at the equator.

394. Every bearing, obtained either by means of the magnetic needle or astronomical observation, is a horizontal angle on the surface of the sphere, formed at the eye, and contained between the meridian of the observer and a line drawn from the eye to meet a plumb-line passing through the point set. Such angle is the same thing as the course on a great circle. Hence observed bearings are never, unless due N. or S., or E. and W. on the equator, identical with bearings taken from Mercator's Chart. The difference is not, indeed, perceptible on common occasions, on account of the smallness of the portion of the sphere within the view of the spectator; but in charts of high latitudes, graduated with much precision, it becomes manifest, and must be taken into consideration when it is

* In the *Plane Chart* the degrees of latitude and longitude are all made equal. This projection represents very nearly the relative directions and distances of places near the equator, and serves for plans of ports and seas in those regions; but in higher latitudes it exhibits truly no directions but E. and W., N. and S., and no distances but those on a meridian. Hence the figure of every portion of surface, however small, is distorted. These charts are no longer used.

required to employ the observed bearing of a distant mountain for any purpose in which precision is necessary.*

A distant object cannot, accordingly, be correctly laid down on the chart, from its observed bearing and distance, except in low latitudes; it must therefore be laid down in lat. and long. as determined by Spherical Trigonometry. The line drawn from the observer's place to this position laid down is then the bearing on the chart,—not the *direction* of the object, but the course which a ship must preserve in approaching it while crossing all the meridians at the same angle.

It follows, in like manner, that three objects which lie in the same great circle (not the merid. or the equator), and therefore, when seen in a certain direction, appear in one, form, on the chart, an elongated triangle, the middle object of the three being on the polar side of the line joining the extremes. Thus the summit of Mount Athos, which lies a little ($0^{\circ} 39''$) to the N. of the great circle passing through Mount Olympus and the summit of Imbros, appears, on the chart of the Archipelago, nearly $2'$ to the N. of the straight line joining the two latter places.

395. The bearing of a distant object, as taken from the chart or computed by Mercator's or Mid. Lat. Sailing, may be converted, approximately, into the true azimuth, as it would be observed, thus:—

Find half the Diff. Long. between the place of observation and the object, and also the Mid. Lat. between them.

To the log. sine of half the D. Long. add the log. sine of the Mid. Lat.; the sum is the log. sine of the corr. required. Apply the corr. to the N. in N. Lat., and to the S. in S. Lat.

Ex. The observer in N. lat. $40^{\circ} 2'$ sees a peak in lat. $40^{\circ} 9' N.$, and $1^{\circ} 54' W.$ of him: required the true azimuth, as deduced from the rhumb course?

The Course by Mercator's Sailing, is N. $85^{\circ} 26' W.$

N. Long. 114', half do. 57'	sin. 8°21'96		Rhumb bearing	85° 26'
Mid. Lat. 40° 5'	sin. 9°8'88		Sub.	37
Corr. 37'	sin. 8°02'84		TRUE AZIM.	84 49

CHAPTER VI.

SOUNDING.

396. SOUNDING is ascertaining the depth of the water. This is commonly done by a lead attached to a line marked at certain divisions.

* This point, and also some considerations relative to the projection of the great circle on Mercator's Chart by rectangular co-ordinates, are treated in the "Traité de Géodésie à l'Usage des Marins," par P. Bégat. Paris, 1839.

397. The soundings marked on the chart are taken at low-water spring-tides; the depth is noted in fathoms, and, in small depths, in feet, and the nature of the bottom is specified. The "low water" of the charts is, generally, the *average* of the spring low water.*

Since the ship's place on the chart can thus be determined, within certain limits, by the soundings, it is always a proper precaution, however correctly the reckoning may be kept, to sound on approaching the land. In like manner, in a fog or during the night, the navigation is often made to depend upon the lead alone.

398. Two leads are employed for sounding, the *hand-lead* weighing 14lbs. and attached to about 25 fathoms of line, and the *deep-sea lead*, weighing 28lbs. and attached to 100 fathoms or more of line wound on a reel. A small lead of five or six pounds is sometimes used. The quality of the bottom is ascertained by fixing a lump of tallow, called the *arming*, on the lower end of the lead before it is thrown into the sea.

399. In using the hand-lead, the leadsman, standing at the vessel's side, or in the channels, throws the lead as far forward as he can, swinging it once or even twice over his head to give it increased force, and endeavours to draw the line tight from the lead at the instant the ship by her progress places him perpendicularly over it. The hand-lead descends about 10 fathoms in the first six seconds, according to some trials made by Capt. Bullock; hence, when the vessel is going fast, it is often difficult to get soundings.

The line is marked at 3, 5, 7, 10, 13, 15, 17, and 20 fathoms.† These depths are called *marks*, and the intermediate ones *deeps*; for example, in obtaining 10 fathoms the leadsman cries, with a peculiar song, "By the mark ten;" in 9 fathoms he cries, "By the deep nine." On some occasions the leadsman describes the bottom as hard or soft.

The only fractions of a fathom used are a half and a quarter; thus, $7\frac{1}{2}$ fathoms are called, "And a half seven;" $7\frac{3}{4}$ fathoms are called, "A quarter less eight."

400. In heaving the deep-sea lead, the lead is carried to the fore part of the ship, as the weather cathead or fore-chains, or the lee cathead, if the ship is making much leeway, the line being passed along outside. The ship's way being reduced when necessary, the lead is dropped and the soundings are observed by an experienced seaman at the quarter. The deep-sea line is marked at each 10 fathoms by the corresponding number of knots, and with a single knot at each five. The error of the soundings is generally in excess, because the line can rarely be stretched straight from the lead.

401. In sounding in deep water in small vessels, which drift to leeward rapidly upon losing their way, it is generally advisable to drop the lead before the headway ceases, and to cause the vessel to

* As this average height is not indicated by nature, the seaman should bear in mind that the water may, under the influence of strong winds, fall quite a foot below this average.

† These divisions require to be measured or rectified from time to time; when this is done, the line should be thoroughly wetted.

gather sternway so as to pass over the lead, which will thus have descended through a considerable depth perpendicularly.

402. The interruption to the voyage, and the inconvenience of rounding the ship in order to allow time for the deep-sea lead to descend to the bottom, have led to the invention of instruments for sounding without stopping the ship's way.*

Burt's buoy and nipper is a simple and well-known instrument. The line being rove through a spring-catch in the buoy, the lead is hove, and the buoy afterwards dropped into the water; the line then continues to run through the catch till the lead reaches the bottom, or is checked by a pull, when the catch firmly seizes the line, attaching the buoy to it at the depth descended through by the lead.

Massey's machine registers the depth by wheelwork set in motion by a fly.—Ericcson's machine measures the depth by the space into which the contained air is compressed.

Sir W. Thomson's Sounding Machine consists of a drum on which is wound about three hundred fathoms of steel piano-forte wire. This is kept at intervals between the casts in a box filled with lime water, which entirely protects the wire from rust.

A brake, partially self-acting, is arranged by a cord round a groove in the circumference of the drum, with two weights attached, one of lead (3 lbs.), the other a long iron weight (56 lbs.).

When ready to take a sounding, the brake is released by holding up the heavy weight and allowing the small one to hang freely in a recess in the heavy one. This opposes a slight resistance to the wire when running out, and when the sinker reaches the bottom the brake is put on by easing down the heavy weight gradually until it is supported by the small one.

Between the sinker (which is of iron, with a hollow at the bottom to receive the arming of tallow) and the depth gauge there is a two-fathom length of *plaited* rope, and the same between the depth gauge and the wire. It is important that *plaited* rope should be used, *not twisted*.

The depth gauge consists of a brass case about 2 feet long, containing a glass tube coated inside with a chemical preparation; this tube is open at one end, and is placed in the brass case with the open end downwards. As the sinker descends, the increased pressure drives the water up the glass tube, and the height is registered by the mark made by the combination of the water and the coating of the tube; this mark, when applied to the graduated boxwood scale, shows at once the depth that has been reached. There is also a counter attached to the wheel that shows approximately the number of fathoms of wire run out.

The instructions sent with the apparatus are ample, and the use of this simple machine is easily learnt; but men should be drilled at it in fine weather, so as to be able to handle it readily in bad. An officer and two men can with ease take soundings in 100 fathoms every quarter of an hour from a vessel going at any ordinary speed.

* Recently an instrument has been introduced wherein the depth is indicated by hydrostatic pressure.

CHAPTER VII.

THE SHIP'S JOURNAL.

I. KEEPING THE SHIP'S JOURNAL. II. THE DAY'S WORK.

I. KEEPING THE SHIP'S JOURNAL.

403. As the keeping of the log or journal, in the Royal Navy and in the merchant service, is a matter strictly professional, and as no one would be intrusted with it whose experience did not qualify him to know what matters to insert and how to express them,—and, moreover, as the log-board, from which the ship's log is copied, is ruled in an established form, the following remarks are inserted merely for reference, and not as a complete description for the instruction of the learner, who must acquire this knowledge with that of the rest of his duty.

404. The time in the ship's log-book is reckoned from midnight, as civil or common time; the first hour is, therefore, 1 o'clock in the morning, and the hours are carried on to 12, or noon, and then to 12, or midnight. The log-board, however, is copied into the log-book each day at noon.*

405. At noon, if the ship is in sight of land, a point or object of known latitude or longitude is set, and its distance estimated. This method of taking a Departure, which, from its convenience, is in general use (No. 349), is sufficiently accurate when the ship is very near the land; but when the land is distant, or enveloped in haze, and when, in consequence, the estimation of distance is liable to great uncertainty, some other method should, if practicable, be adopted in preference, or at least employed as a check. If there is no particular object in sight, the extremes of the land are set; and thus, in case of a fog coming on, the ship is secured, by keeping outside of the bearings of these extremes, from approaching the land.†

* The log-board, on which were painted the necessary divisions, and the record made in chalk, has long passed away. A log-slate or deck log-book is kept instead.

† Since, when the ship is in sight of land, her place is determined with reference to the land alone, it is customary, during this time, to discontinue heaving the log, and therefore to omit the insertion of the courses and distances on the log-board. It is sometimes, however, proper to keep up the account when in with the land, as it affords the means of discovering a permanent current, or the direction, strength, and time of change of the tide-current.

If the ship is out of sight of land, the Course and Distance made good in the last 24 hours, the Latitude and Longitude by Dead Reckoning, as also by Observations if they are obtained, are inserted, together with the Bearings and Distance of the port or of the land worked for.

406. It often happens, from change of long., that the day of 24^h has expired before the sun has attained the meridian. In this case, the hours having been truly measured, and the hourly distances rightly assigned, the reckoning is truly registered up to the running out of the last glass, and an increased distance must therefore be marked against the last hour or half-hour.

In like manner the day may really have expired by observation before the 24 hours are completed. In this case a diminished distance must be marked at the last hour or half-hour.

407. The Leeway should always be marked on the log-board, since it is impossible for any one to know what leeway the ship may be making in bad weather when he is not on deck.

408. At the end of every watch, at the close and dawn of day, and at the coming on of a fog, the land is set; so that, in case of losing sight of it, a Departure may always be secured at the latest period.

409. The Weather is described at the end of each watch, or oftener, as occasion may suggest. In order to mark the strength of the wind, and the description of the weather, with more distinctness than the terms in general use among seamen are capable of expressing, Sir F. Beaufort has proposed the following system of numbers and letters, which has been adopted by order of the Lords Commissioners of the Admiralty, dated Dec. 28, 1838, in Her Majesty's ships:—

FIGURES to denote the FORCE OF THE WIND.

0 — Calm.		
1 — Light Air	Or, just sufficient to give steerage way.	
2 — Light Breeze	Or, that in which a well-conditioned man-of-war, with all sail set, and clean full, would go in smooth water from.....	1 to 2 knots.
3 — Gentle Breeze ...		3 to 4 knots.
4 — Moderate Breeze		5 to 6 knots.
5 — Fresh Breeze	Or, that to which she could just carry in chase, full and by	Royals, &c.
6 — Strong Breeze ...		Single-reefed topsails and top-gallant sails.
7 — Moderate Gale....		Double-reefed topsails, jib, &c.
8 — Fresh Gale.....		Triple-reefed topsails, &c.
9 — Strong Gale ...		Close-reefed topsails and courses.
10 — Whole Gale	Or, that with which she could scarcely bear close-reefed main-top-sail and reefed foresail.	
11 — Storm	Or, that which would reduce her to storm-staysails.	
12 — Hurricane	Or, that which no canvas could withstand.	

LETTERS to denote the STATE OF THE WEATHER

b—Blue sky; whether with clear or hazy atmosphere.	q—Squally.
c—Cloudy; but detached opening clouds.	r—Rain; continued rain
d—Drizzling rain.	s—Snow.
f—Foggy—f, Thick fog.	t—Thunder.
g—Gloomy dark weather.	u—Ugly threatening appearance of the weather.
h—Hail.	v—Visibility of distant objects, whether the sky be cloudy or not.
l—Lightning.	w—Wet dew.
m—Misty hazy atmosphere.	.—Under any letter indicates an extraordinary degree.
o—Overcast; the whole sky being covered with an impervious cloud.	
p—Passing temporary showers.	

By the combination of these letters, all the ordinary phenomena of the weather may be recorded with facility and brevity. Examples:—b c m, Blue sky, with detached opening clouds, and a misty atmosphere. g v, Gloomy dark weather, but distant objects remarkably visible. q p d l t, Very hard squalls with passing showers of drizzle, and accompanied by lightning with very heavy thunder.

410. When a heavy sea is running, or when a swell rises without corresponding wind, the circumstance is noted.

A swell is named after the point of the compass *from* which the waves proceed, like the wind that produces them. To denote, however, a south-westerly swell (for example) as “a swell from the S.W.” removes all ambiguity.

411. The variation of the compass, when observed, is inserted in the remarks; as also the results of occasional observations, as the latitude by double altitude, by the moon, planets, or stars, the longitude by lunar, &c., the exact time of observation being specified.

412. In general, besides the details proper to the particular service on which a vessel may be employed, all matters relating to her *place* are inserted in the log, not only for the safety or convenience of the present voyage, but as matter of intelligence or of evidence in the case of future inquiry. Hence the circumstance of seeing or speaking a vessel is always noticed.

No form of log has been universally adopted in merchant-ships, but several neat forms are in common use. The precise form is not material, as long as the ship's proceedings are exactly and conveniently recorded.

A separate journal, called in the Royal Navy the engine-room register, is generally kept in steam-ships. In this is recorded the revolutions of the engines, the pressure of steam, the consumption of fuel and other materials, the temperature of the engine-room, stoke-holes, coal-bunkers, &c. Generally, it is a record of all matters relating to the performance and state of the engines, and the employment of the engine-room staff.

413. The following is the form in which the logs of her Majesty's ships are at present kept by order of the Board of Admiralty, 1879.

H.M.S. _____, _____ day of _____, 18 ____.													
From _____, to _____, or at _____.													
Initials of Officer of Watch	Hour	Knots	Tenths	Standard Compass Courses	Leeway, Points	Winds		Weather	Deviation of Standard Compass	Height of		Temperature of Sea	Remarks
						Direction	Force			Bar.	Ther.		
	1												A.M.
	2												
	3												
	4												
	5												
	6												
	7												
	8												
	9												
	10												
	11												
	12												
Course	Distance		Latitude	Longitude	Variation	Water Remains		True Bearing and Distance		No. on			
	made	through	DR.	DR.	allowed					Sick-bed			
	good	the water				Daily Expend							
Current	miles	miles	Obs.	Ohro.		Distilled since yesterday							
	1												I.M.
	2												
	3												
	4												
	5												
	6												
	7												
	8												
	9												
	10												
	11												
	12												
Signals {						Coal expended during 24 hours		For engines		For ship		For distilling	

II. THE DAY'S WORK.

417. This is the process of finding the place of the ship, with reference either to her place at yesterday's noon, or to a departure taken since, and comprises,

1st, The Course and Distance made good ;

2d, The Lat. and Long. in ;

3d, The Bearing and Distance of some port, which is either to be steered for directly, or is an intermediate point of land, with reference to which the course is to be shaped, so as to make it or to avoid it.

418. To work a day's work. (1.) Take the courses, with the distance run on each, from the log-board.

When a departure has been taken, consider it is a course and distance in the *opposite direction*.

Correct each course for deviation of the compass, 229, or p. 159.

If the variation has changed since the departure was taken, correct each course separately, No. 221 ; if not, defer this correction.

Every course affected by leeway must be corrected accordingly. The quantity, if not marked on the board, must be estimated from the circumstances. When the ship is on the *starboard* tack, allow the leeway to the *left* ; when on the *port* tack, allow it to the *right*, the observer being supposed in the centre of the compass. When the ship is hove-to, take the middle point between that to which she comes up and that to which she falls off, for the compass course, and correct this for leeway.

(2.) Having corrected the Courses thus far, take out to each the D. Lat. and Dep. from the Traverse Table, and find the Course and Distance made good by Traverse Sailing, No. 287, or by Traverse Tables (Table 1.)

If the variation has not been allowed for, apply it to the resulting course, No. 221.

(3.) Apply the D. Lat. to Lat. left : the result is Lat. in, No. 190.

With the Lat. left and Lat. in, and the Course, find the D. Long. by Case I. of Mid. Lat. or Mercator's Sailing (No. 315 or 323), or by Traverse Table. If the Course is due E. or W., then proceed by Case I. of Parallel Sailing (No. 304) or by Traverse Table.

Having the Long. left and Diff. Long., find the Long. in, No. 196.

(4.) Having now the Lat. and Long. of the ship, and those of the port to be worked for, find its Bearing and Distance ; if in the Lat. of the ship, by Case II. of Parallel Sailing, No. 307 ; otherwise by Case II. of Mid. Lat., or Mercator's Sailing, No. 318 or 326 ; or by Traverse Table. To this Bearing apply the Variation and Deviation of the Compass, and so obtain from the True Course, the *Course to be steered*.

To find the Course on a Great circle, *see* No. 337 or 338.

It is mere waste of time to work the Course nearer than to the whole degree ; for even if the compass could be depended upon to 1°, the ship cannot generally be steered within that quantity.

Ex. 1. The ship while hove-to for the first two hours, with light north-easterly winds, came up to E., and fell off S.S.E.; taking S.E. by E. as the middle course, allowing 2 pts. leeway, and 3 miles distance, gives S.E. by S. 3 miles, after which the courses and dists. follow as below. Lat. left $29^{\circ} 26' N.$, long. left $127^{\circ} 42' E.$; var. $3^{\circ} E.$; find the Lat. and Long. in; also set of current in the 24 hours. Position by observation being Lat. $27^{\circ} 55' N.$, Long. $128^{\circ} 43' E.$

Courses.	List.	N.	S.	E.	W.
S.E. by S.	3		2.5	1.7	
S.S.E. $\frac{1}{2}$ E.	23		20.3	10.8	
S.S.E.	49		45.3	18.8	
S. by E. $\frac{1}{2}$ E.	24		23.0	7.0	
S. by E.	6		5.9	1.2	
S.W. by S.	8		6.7		4.4
S.W.	7		4.9		4.9
S.W. by W.	7		3.9		5.8
W. by N.	5	1.0			4.9
S. $\frac{1}{2}$ E.	6		6.0	0.6	
		1.0	118.5	40.1	20.0
			1.0	20.0	
			117.5	20.1	

The D. Lat. 117.5 and Dep. 20.1 give Course by Compass S. $10^{\circ} E.$ Dist. 119 miles.

Applying 3° (var.) to the right gives Course S. $7^{\circ} E.$ true. Then 7° and Dist. 119 give D. Lat. 118.1, and Dep. 14.5.

In the foregoing example, the deviation of the compass has not been mentioned. From what has been said in Chapter II. it must be evident that the bearing taken for departure and the courses steered must be corrected for deviation, where there is any. As the deviation changes when the direction of head is changed, it is obvious that each course must be corrected separately.

To correct the Compass for Variation or Deviation.

Course by Compass given.

If Var. or Dev. East, allow to right.
If Var. or Dev. West, allow to left.
Will give true course.

True Course given.

If Var. or Dev. East, allow to left.
If Var. or Dev. West, allow to right.
Will give magnetic course.

To Correct the Compass Courses.

Easterly Variation or Deviation is + to all points between N. and E.....S. and W.
Westerly Variation or Deviation is - from all points between N. and E.....S. and W.
Easterly Variation or Deviation is - from all points between N. and W.....S. and E.
Westerly Variation or Deviation is + to all points between N. and W.....S. and E.

To Convert a True Course or a Correct Magnetic Course into a Compass Course.

Easterly Variation or Deviation is - from all points between N. and E.....S. and W.
Westerly Variation or Deviation is + to all points between N. and E.....S. and W.
Easterly Variation or Deviation is + to all points between N. and W.....S. and E.
Westerly Variation or Deviation is - from all points between N. and W.....S. and E.

In the following examples the Deviations from table of No. 227 have been applied to the Compass Courses, to obtain the Correct Magnetic Courses.

D. Lat. 118 $1^{\circ} 58' S.$
Lat. left D.R. $29^{\circ} 26' N.$
Lat. in, D.R. $27^{\circ} 28' N.$

Lat. left 29° and Lat. in 27° give Mid Lat. 28° .

Then 28° and D. Lat.
 14.5 give Dist. $16' E.$
Long. left $127^{\circ} 42' E.$
Long in, D.R. $127^{\circ} 58' E.$

To determine approximate current see Nos. 290 to 297, and 1015.

Position by
Obs. Lat. $27^{\circ} 55' N.$, Long. $128^{\circ} 43' E.$

Position by
D.R. Lat. $27^{\circ} 28' N.$, Long. $127^{\circ} 58' E.$
 27 45

In Lat. 28° Diff. Long. $45 =$ Dep. 39.7 .

Then D. lat. 27 and Dep. 39.7 gives Course N. $56^{\circ} E.$, Dist. 48 m., set of CURRENT in 24 hours.

Probable; the ship being in the Kuro Siwo, or Japan Stream.

Ex. 2. The Departure is taken from the Eddystone, bearing N.N.E. 12 miles. Ship's head S. by E. The ship ran S. by E. 14 (miles), S. by W. 10, and S.W. by W. 8. Allow 25° westerly variation. Find the Bearing and Distance of Ushant, and Course to be steered.*

The Departure gives a Course S.S.W. (No. 418 (1)). Correcting this and the other Courses from the Deviation Table, No. 227, S.S.W. becomes S. 18° W. (No. 228), S. by E. becomes S. 16° W., S. by W. becomes S. 6° W.; and S.W. by W. becomes S. 50° W.

Compass Courses.	Dist.	Correct Magnetic Courses.	N.	S.	E.	W.
S.S.W.	12	S. 18° W		11.4		3.7
S. by E.	14	S. 16° E		13.5	3.9	
S. by W.	10	S. 6° W.		9.9		1.0
S.W. by W.	8	S. 50° W.		5.1		6.1
				39.9	3.9	10.8
						3.9
						6.9

Eddystone Lat. $50^{\circ} 11' N.$

D. Lat. $40 S.$

Lat. in, D.R. $49^{\circ} 31' N.$

Lat. left 50° and Lat. in $49\frac{1}{2}^{\circ}$ give Mid Lat. 50° .

Then 50° and 10.6 as D. Lat. give Dist. 16', the D. Long.

Eddystone Long. $4^{\circ} 16' W.$

D. Long. $16 E.$

Long. in, D.R. $4^{\circ} 0' W.$

Lat. in $49^{\circ} 31'$ Long. $4^{\circ} 0'$

Ushant $48^{\circ} 29'$ $5^{\circ} 4'$

$1^{\circ} 2 = 62'$ $1^{\circ} 4 = 64'$

Mid. Lat. 49° .

D. Lat. $39' 9$ and Dep. 6.9 give Co. S. $10^{\circ} W.$, Dist. 41. Applying 25° to the left gives Course S. $15^{\circ} E.$ true. Then Course 15° and Dist. 41 give D. Lat. 39.6 and Dep. 10.6 .

Then Course S. $34^{\circ} W.$ + Var. $25^{\circ} W.$ gives S. $59^{\circ} W.$ + Deviation $7^{\circ} W.$ give S. $66^{\circ} W.$, Course to be steered for Ushant.

Ex. 3. A ship from lat. $0^{\circ} 5' N.$, and long. $0^{\circ} 17' W.$, sails S.W. by S. 7 miles, S. by E. 22, S.S.W. $\frac{1}{2} W.$ 8, and N.E. by E. 20. Var. $19^{\circ} W.$ Position by Obs. Lat. $0^{\circ} 15' S.$, Long. $0^{\circ} 20' W.$ Find Compass Course to be steered,* and the Dist. to C. Palmas; also current experienced in the 24 hours.

Compass Courses.	Dist.	Correct Magnetic Courses.	N.	S.	E.	W.
S.W. by S.	7	S. $29^{\circ} W.$		6.1		3.4
S. by E.	22	S. $16^{\circ} E.$		21.1	6.1	
S.S.W. $\frac{1}{2} W.$	8	S. $23^{\circ} W.$		7.4		3.1
N.E. by E.	20	N. $70^{\circ} E.$	6.8		18.8	
			6.8	34.6	24.9	6.5
				6.8	6.5	
				27.8	18.4	

D. Lat. 27.8 and Dep. 18.4 give Co. S. $33^{\circ} E.$, Dist. 33 miles. Applying 19° var. W. to the left, gives Course S. $52^{\circ} E.$ true. Then Course 52° and Dist. 33 give D. Lat. 20.3 and Dep. 26.

To determine approximate Current, see Nos. 890 to 297, and 1015.

Lat. Obsd. $0^{\circ} 15' S.$ Long. $0^{\circ} 20' W.$

Lat. D.R. $0^{\circ} 15' S.$ Long. $0^{\circ} 9' E.$

Approximate Current West 29 m.

Lat. from $0^{\circ} 5' N.$

D. Lat. $0^{\circ} 20' S.$

Lat. in, D.R. $0^{\circ} 15' S.$

Near the equator Dep. is D. Long. No. 311; hence,

Long. from $0^{\circ} 17' W.$

D. Long. $26 E.$

Long. in, D.R. $0^{\circ} 9' E.$

By Obs.

Lat. $0^{\circ} 15' S.$ Long. $0^{\circ} 20' W.$

C. Pal. $4^{\circ} 22' N.$ $7^{\circ} 44' W.$

$4^{\circ} 37' = 277'$ $7^{\circ} 24' = 444'$

D. Lat. 277 and Dep. 444 give Course N. $58^{\circ} W.$, and Dist. 523 miles; Course N. $58^{\circ} W.$ Then

— Var. $19^{\circ} W.$ = N. $39^{\circ} W.$

— Dev. $8^{\circ} W.$ = N. $31^{\circ} W.$, Compass Course to be steered.

N.B.—On this course allow for crossing the EQUATORIAL and GUINEA CURRENTS.

* In shaping the Course, consider the direction and force of the tide or current that may be found, between the position of the ship and the port steered for.

NAUTICAL ASTRONOMY.

CHAPTER I.

DEFINITIONS.

419. THIS branch of the subject, as already defined under the head Navigation, No. 179, relates to finding the place of the spectator on the surface of the earth by observation of the heavenly bodies.

420. To the spectator at the surface of the earth the heavens appear to form a vault, or the upper half of a hollow sphere, of which he is the centre; the earth itself, or the ground or sea on which he stands, occupying the lower half. Any two points on the apparent concave or celestial surface, as two stars, for example, may be supposed to be connected by an arc of a circle drawn on that surface: and thus the apparent celestial sphere may be conceived to be marked with circles like the terrestrial globe.

421. The spectator stands with his feet towards the centre of the globe; that is, a plumb-line, which is vertical, passes through the spectator and this centre;* and thus the spectator always conceives himself on the summit of the globe.† Suppose him now to descend the above line to the centre, and then suppose the upper half of the earth or globe to be cut off horizontally, that is, parallel to the horizon, or perpendicular to the plumb-line. The surface of the lower half-globe, or hemisphere, so exposed, being produced on all sides to meet the concave celestial surface, is called the RATIONAL

* The earth is here supposed to be a globe; the plumb-line does not exactly pass through the centre of the spheroid, but the difference is not worth notice here.

† This is the principle of rectifying the globe, or placing the globe to shew the relative position of the spectator and the heavens.

To rectify the globe, as, for ex., for Greenwich, in 51° N. Lat. Place the globe on a level surface, so that the broad rim, or horizon, shall be horizontal. Take hold of the brass meridian, and turn the globe round in its stand (upwards or downwards) until the N. pole is 51° above the rim.

Direct the N. point of the rim (now under the pole) to the true north. Turn the globe round its axis till Greenwich passes under the meridian; Greenwich will now be the uppermost point.

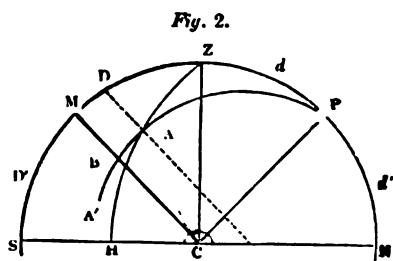
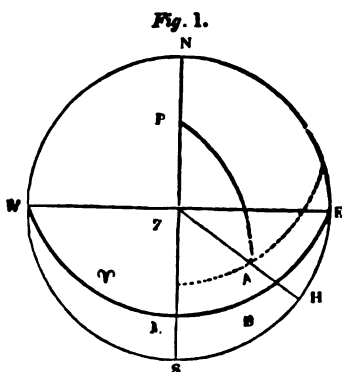
The axis of the globe now makes the same angle with the wooden horizon that the axis of the heavens (or line joining the centre and the poles) makes with the horizon of the spectator.

HORIZON. Every point of the earth's surface has thus a different rational horizon, but all these horizons have the same centre.

422. It becomes, in general, necessary, for considerations which will appear hereafter, to reduce celestial observations taken at the surface of the earth to what they would have been if taken at the centre; in the following figures, therefore, the observer is supposed to be at the centre of the earth. The dimensions of the earth are so small in comparison with the vast distances of the stars, that the above change of place of the spectator from the surface to the centre, or to any other point, would produce no change whatever in the apparent places or directions of the stars; and, accordingly, the magnitude of the earth, in drawing figures for general purposes, is neglected, the earth itself being considered as a mere point in the centre of the great sphere which circumscribes the stars. In the case of nearer bodies, as the sun and some others, and especially the moon, which, when viewed with delicate instruments, appear in different directions when seen from different points of the surface of the earth, this apparent change of place is allowed for by a special calculation. (See Parallax, No. 435)

423. The **ZENITH** is the point vertically over the spectator, and distant 90° from the rational horizon at every point.

The point opposite the zenith, or under the spectator's feet, on the other side of the centre, is called the **NADIR**.



In fig. 1, N W S E represents the Rational Horizon; N S, the Meridian of the observer; N, S, E, W, the North, South, East, and West points; Z, the Zenith, which is seen directly over, or in one with the centre. This figure is drawn on the plane of the rational horizon, and shews the several circles as they would appear to an eye looking down vertically from a point at a great distance above the zenith.

Fig. 2 is drawn on the plane of the meridian, and shews the several circles of the upper or visible half of the sphere, as they would appear to the eye situated at a great distance due east of the sphere. In this figure the circle N W S E, or the horizon, appears as a straight line NS being seen edgeways; while the meridian,

which in fig. 1 is the straight line NS , appears here as the semicircle $NPZS$. The E and W points are seen in one with the centre.

Of these two figures, that one would naturally be preferred which would best illustrate a proposed case. Fig. 1 may generally be employed to exhibit the hour-angle and azimuth; and fig. 2 the altitude, when the celestial body is near the horizon.*

424. P , the **POLE** of the heavens, is the point which remains fixed, whilst the rest of the celestial surface seen above the horizon appears to revolve.

The pole P is here represented as the North pole; the other extremity of the axis round which the sphere appears to revolve is the South pole, and takes the place of P when the figure is drawn for S . Lat. This pole is called the *elevated* pole.

425. The circle EMW , 90° from the pole, is the **CELESTIAL EQUATOR**. The plane of the earth's equator, EMW , fig. p. 55, No. 180, being extended to the heavens, marks on the sphere the celestial equator.

426. A **CELESTIAL MERIDIAN** is a semicircle passing through the pole of the heavens; PZS is the celestial meridian of the spectator. The plane of the terrestrial meridian extended to the heavens marks on the sphere the celestial meridian.

427. **CIRCLES OF ALTITUDE** are circles passing through the zenith, and vertical at the place of the spectator. Thus ZAH is the circle of altitude passing through a star A . Such, also, are ZMS , ZPN .

428. The **PRIME VERTICAL** is the vertical circle EZW passing through the E . and W . points. In fig. 2, EZW does not appear, being in one with CZ , a radius joining the centre and zenith.

When the observer is on the equator, the celestial equator and prime vertical coincide.

429. **ALTITUDE** is measured on a circle of altitude from the horizon; thus AH is the altitude of A .

The arc AH is the measure of the angle $A\hat{C}H$, which would be formed at the centre by two straight lines, CH and CA . The alt. of a body M on the meridian is MS , which is the measure of the angle $M\hat{C}S$.

430. *Parallels of Altitude* are circles parallel to the horizon.

431. **ZENITH DISTANCE** is the arc included between the zenith and the celestial body, or the angular distance of a body from the zenith of which that arc is the measure. The zenith distance is, therefore, the complement of the altitude to 90° , as ZA .

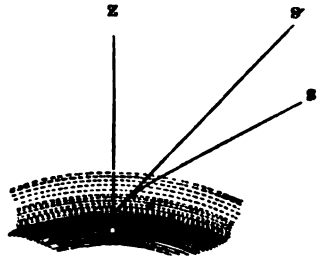
432. The altitude of a celestial body, as seen from the surface of the earth, is called the *apparent* altitude; as seen from the centre, the *true* altitude.

A ray of light, proceeding from the body, when not in the zenith, to the eye, in traversing the earth's atmosphere, which is heavier, or denser, as it is nearer the surface, is bent more and more as it

* In like manner the figure may be drawn in the plane of the equator (as in Nos. 472, 473), in that of the prime vertical, or any other circle.

approaches the earth, towards the perpendicular direction ; and as the spectator sees any object, not always in its true direction, but in that direction in which the light from it finally enters his eye, a celestial body appears higher than its true place. Thus, the ray SA , which proceeds from a star, is more and more bent towards the vertical line AZ as it approaches the surface, whereby the spectator sees the star in the direction AS' , and therefore higher than its true position.

The ray AZ , which traverses the atmosphere perpendicularly, undergoes no refraction. Thus to the eye supposed at the centre all rays would proceed without any deviation ; because lines drawn towards the centre of the sphere are perpendicular to its circumference, parallel to which the atmosphere is disposed.



433. This alteration in the apparent place of a celestial body, caused by the atmosphere, is called the **ASTRONOMICAL REFRACTION**.

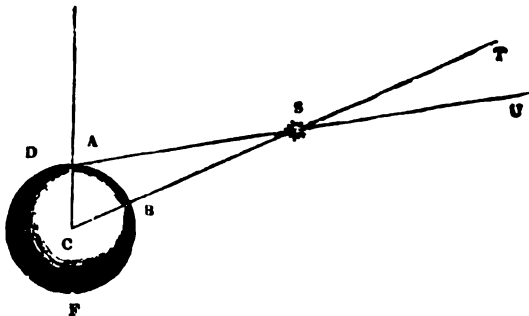
The astronomical refraction is 0 at the zenith, and about $34'$ at the horizon ; hence a celestial body, when really on the horizon, appears elevated $34'$ above it, and is seen on the horizon when really $34'$ below it. From the same cause all the celestial bodies rise earlier and set later than they would were there no atmosphere.

The refraction varies with the density or weight of the air, being greater when the barometer is high, or the air cold, and less when the barometer is low, or the air warm. The *mean refraction*, or that in the average state of the atmosphere, is given in Table 31, and corrections for different states of the air in Tables 32 and 33.

Since refraction causes the object to appear too *high*, it is to be *subtracted* from the apparent altitude in reducing it to the true altitude.

434. **TWILIGHT** is the effect of the illumination of the upper regions of the atmosphere by the sun, before he has risen or after he has set, at the place of the spectator. Twilight continues, generally, while the sun is less than 18° below the horizon.

435. **PARALLAX IN ALTITUDE** is the angular depression of a celestial body, in consequence of its being seen from the surface instead of the centre of the earth, thus :



The body *S*, which is vertical to the spectator (who always stands with his feet towards the centre) at *B*, in the line *CS*, appears at *T*, being seen in the direction *CST*; while to a spectator at *A* the same body appears below *T* at *U*, or in the direction *ASU*; the angle *ASC*, or *TSU*, which is equal to *ASC*, No. 116, is the *parallax in altitude*. (Tables 34 and 45.)

The spectator at *B* sees *S* in the same line as if he were at the centre; that is, a body in the zenith has no parallax. To a spectator at *D*, to whom *S* appears in the horizon, the depression, or parallax, is greater than at any other point.

The parallax at the horizon is called the **HORIZONTAL PARALLAX**.

Since parallax makes the object appear too *low*, it is to be *added* to the apparent altitude, in reducing it to the true altitude.

436. It is evident, by the fig. No. 435, that the farther off a celestial body is, the less parallax it will have; and the nearer, the more. The sun has about 9" hor. par.: the moon has about 1°. Parallax is matter of actual observation, and determines definitively the distances of the sun, moon, and planets.

437. The parallax will obviously be less if the earth's radius is less. Now, the earth being shaped like an orange, the radius, or line from the centre to the surface, in any latitude, is less than at the equator; hence the moon's hor. par. in the Nautical Almanac, which is the *equatoreal* hor. par., is too great for any latitude. The reduction is given in Table 41.

438. Since the apparent altitude is too great on account of refraction, and too small on account of parallax, the diff. between these quantities is the diff. between the true and apparent altitudes. This difference, or the combined effect of parallax and refraction, is called the *Correction of Altitude*.

The moon's Corr. of Alt. is given in Table 39; that of a star is merely its refraction.

439. The **SEMI-DIAMETER** of a celestial body is half the angle subtended by the diameter of the visible disc.

Thus to a spectator at *S* the semi-diameter of the body is half the angle subtended by the diameter *DF*, or contained between the lines *SD*, *SF*, supposed to be drawn from *S* to *D* and *F*; the half of this angle is *SDC* or *CSF*, and is called the semi-diameter.

It is evident that the semi-diameter will be greater as the body is nearer, and smaller as it is farther off. Thus the variations in the semi-diameter of the sun prove that the distance between the sun and the earth varies at different times of the year. (Table 34.)

440. When the body *S* is in the zenith, it is nearer to the spectator by half the earth's diameter, *CB*, than when it is on the horizon; hence it appears larger when in the zenith. This increase of apparent dimensions due to increase of altitude is sensible in the case of the moon only, and is called her **AUGMENTATION**.* This is given in Table 42.

* The apparent increase of the magnitudes of the sun and moon when near the horizon is a mere optical illusion, whatever explanation may be given of it; 'or the instruments by

441. The **DECLINATION** of a celestial body is the portion of the meridian between the equator and the body; it is reckoned from the equator, and is either north or south. Thus, A B, fig. 2, p. 162, is the Declin. of A, and is north.

Since the declination is measured on the celestial meridians, these are called also declination circles.

442. *Parallels of Declination* are circles parallel to the equator, as the dotted line through A, in both figures, p. 162.

Thus declination is reckoned from the celestial equator as latitude on the surface of the earth is reckoned from the terrestrial equator; and as both these circles are in one and the same plane, declination and terrestrial latitude correspond: that is, a star in 28° N. Decl. passes every day vertically over all places in 28° N. Lat.

443. **POLAR DISTANCE** is the arc of the celestial meridian between a celestial body and the pole, or the angular distance of a body from the pole. When the Lat. and Decl. are of the *same* name, the pol. dist. is the *compl.* of the Decl. to 90° , because the distance from the pole to the equator is 90° ; when the lat. and decl. are of *different* names, the pol. dist. is the *sum* of the decl. and 90° . Thus the pol. dist. of A is PA; that of A' in S. decl., fig. 2, is PA', which is the sum of 90° and A'B.

444. The **AZIMUTH** of a celestial body is the angle at the zenith contained between the meridian of the place of the spectator and the circle of altitude passing through the body. It is reckoned to begin from that part of the meridian which is on the polar side of the zenith, that is, from the N. in north latitude; thus, the angle PZA is the azimuth of A.

The angle MZA is the supplement of the azimuth to 180° . This is often used for convenience; thus, instead of N. 132° E., we say S. 48° E.

445. The angle NZA or PZA is the same thing as an angle NCH on the horizontal plane, contained between the north and south line CN, and a line from the eye at C to the foot of the circle of altitude H,* which is the "point of the compass" on which A is seen. Now the angle NCH is measured by the arc NH; the azimuth, accordingly, is measured by the arc of the horizon between the meridian of the place and the circle of altitude of the body. The ship's course is the azimuth of the ship's head; so, also, the bearing of an object is its azimuth; and difference of bearing is difference of azimuth.

When a body is on the prime vertical, its azimuth is 90° .

Since refraction and parallax take place vertically, they do not affect the azimuth of a body.

446. The **AMPLITUDE** is the arc of the horizon between a celestial body at rising or setting and the E. or W. point, and is the com-

which the angles subtended by the discs are measured discover no change of magnitude. The constellations, as the Great Bear, Orion, &c., appear in like manner, when near the horizon, to occupy a vast space in the heavens, but when near the zenith much less.

* This cannot be distinctly represented to the eye by figs. 1 and 2, because in fig. 1 the points Z and C coincide, and in fig. 2 the horizon N W S E appears as a straight line.

plement of the azimuth; thus EH is the amplitude of a body rising at H . Amplitude is reckoned from the E . or W .; thus, if EH is 27° , the amplitude of H is $E. 27^\circ S$.

(1.) The great refraction at the horizon affects sensibly the apparent amplitude. Thus, suppose the spectator in north lat. facing the east, EQ part of the equator, EZ part of the prime vertical, A' a star having north decl. then EA' is the *apparent* amplitude at the instant of rising; but the star is known to be raised, that is, brought into view, in this case, by refraction, and therefore has not yet, in its revolution, arrived at the horizon; A' is consequently to the *left* of the place A , where it would rise were there no atmosphere. Hence the arc $A'A$ is applied to the right of the compass-bearing on which A' is observed, in order to correct the apparent place of the star for the effect of refraction. This quantity is given in Table 59 A.

In facing the west the line EQ (which would become WQ) would lie on the other side of the prime vertical, and the star would be seen to set to the *right* of its true place.

In south lat. the figure drawn above answers to setting, putting W . for E .

(2.) As the elevation of the observer depresses the sea-horizon while it does not affect the place of the star, it produces a further effect of the same kind as that of refraction.

In the case of the moon, as her parallax exceeds the refraction, the opposite effect is produced; that is, when she appears to rise, she has already, to an eye at the centre, passed the rational horizon: thus A would be the apparent place of the moon at rising, to the *right* of the true place A' .

447. The latitude, or distance of the observer from the equator, is measured, on the celestial sphere, by the distance of his zenith from the celestial equator; or ZM is the measure of the latitude, figs. p. 162.

Suppose now D , a star of N . decl., on the meridian at D ., then MD is its decl. and ZD its zenith distance; here ZM , the Lat., is the *sum* of the decl. and zen. dist.

If D' be a star of S . decl., ZM is the *diff.* of ZD' and MD' .

If a star d be between Z and P , the lat. ZM is the difference of Md and Zd .

448. When the object is to the south of the observer, that is, when his zenith is to the north of the body, the zen. dist. is commonly called N .; when his zenith is to the south of the body, the zen. dist. is called S . In fig. 2, ZD and ZD' are therefore called North; Zd is called South.

It appears, hence, that when the Decl. and Zen. Dist. are of the *same* name, their *sum* is the latitude; when of *different* names, their *difference* is the latitude.

But when the star is below the pole, as at d' , the Lat. ZM is

the Diff. of $M\alpha'$ and $Z\alpha'$, and $M\alpha'$ is the sum of MP and $P\alpha'$ or of 90° , and the compl. of the decl.

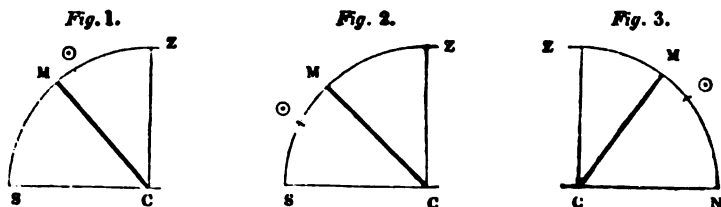
449. MZ being the lat., PZ is the Colat., since PM is 90° . Also ZN being 90° , PN is the compl. of PZ , and therefore equal to MZ ; or the elevation of the pole is equal to the lat. of the place.

450. The altitude of the uppermost point of the equator on the meridian, or MS , is equal to the colatitude, because ZS is 90° . By noting this, and also that the equator passes through the E. and W. points, it is easy, in looking towards the heavens, to figure in the mind, roughly, the position of this circle. This is often useful.

451. In high latitudes, P in the figure falls near Z ; in low latitudes, P falls near N . On the equator, Z and M coincide, the celestial equator there passing over the spectator's head.

In S. Lat. the letters N and S in the figures are changed; also the direction of the celestial motions (which we in N. lat. consider from left to right) is there reversed, because in S. lat., in looking towards the equator, the E. is on the right hand.

452. By the help of the preceding considerations (No. 447 and following) it is easy to construct a figure, in any case, to exhibit at once the manner in which the latitude is obtained from the meridian altitude and the declination.



Ex. 1. The Mer. Alt. of the sun, observed to the southward, is 58° ; his Decl. 14° N

Fig. 1. Draw a quadrant ZCS by means of the chord of 60° (No. 107). Lay off, by the scale of chords, the Alt. $S\odot$, 58° , or the zen. dist. $Z\odot$, 32° . Lay off the Decl. 14° to the southward of the sun, as $\odot M$, since he is to the northward of the equator; then M is on the equator, and ZM is the LAT. north, and measures 46° .

Ex. 2. The Mer. Alt. of the sun, south of the observer, is 29° ; his Decl. 18° S.

Fig. 2. Lay off $S\odot$, 29° , and $\odot M$, 18° to the N. of the sun; then M is the place of the equator, and ZM , the LAT. north, measures 43° .

Ex. 3. The Mer. Alt. of the sun, north of the observer, is 38° ; his Decl. 14° N.

Fig. 3. Lay off $N\odot$, the Mer. Alt. 38° , and $\odot M$ the Decl. 14° to the S. of \odot ; then ZM is the LAT. south, and measures 38° .

These figures, which are varieties of fig. 2, p. 162, are of the simplest kind. The point Z being marked on the quadrant, the place of the sun at \odot , north or south of the observer, is given by the observation; his declination gives M the place where the equator cuts the meridian; whence it is at once seen whether Z is north or south of M , that is, whether the Lat. is N. or S.*

* After a little practice the observer will perceive, at the time of observation, how to deduce the latitude from the mer. alt. and decl. independently of the distinctions of names above (No. 448), which are adopted for the purpose of forming a general rule.

453. The passage of a celestial body over any particular point or circle is called *TRANSIT*; as the transit of the meridian, or the prime vertical, of a planet over the sun's disc, &c.

454. *CULMINATION* is another term for transit of the meridian. The transit of the meridian below the pole, whether above or below the spectator's horizon, is called the lower culmination; the other transit is called the upper culmination.

455. *OCCULTATION* is the disappearance or hiding of a celestial body by the intervention of another. Thus the stars in the moon's path are occulted by her, and the satellites of a planet by the body of the planet.

456. *ECLIPSE* is the disappearance of a celestial body in the shadow of another. In an eclipse of the moon, she disappears wholly, or partly, in the shadow of the earth, the earth being then in a line between the sun and moon. In an eclipse of the sun, the moon, being then in a line between the sun and the earth, conceals from us, for a time, the whole or part of the sun.

457. Celestial bodies are said to be in *Conjunction* when in a line together, as seen from the centre of the earth. Bodies having the same Right Ascension are said to be in *Conjunction* in Right Ascension (No. 469).

Two bodies are said to be in *Opposition* when in diametrically opposite points of the heavens.

458. It will be perceived, on attending to the circumstance, that stars which are visible in the west soon after sunset, disappear after some days in the solar light; and, in like manner, that stars which are faintly seen in the east, before sunrise, become more distinct from day to day. Hence the sun, besides revolving daily with the fixed stars* from east to west, has an apparent yearly motion amongst them in the contrary direction, or from west to east, completing the circuit of the heavens in the course of a year.

459. The path on which the sun appears to move, or the great circle which he seems to describe in the heavens, is called the *ECLIPTIC*.

460. The ecliptic is divided into twelve *SIGNS*, or portions of 30° each, called the *Signs of the Zodiac*, which term originally meant a space or belt of 8° wide on each side of the ecliptic, to which the planets† are confined. The signs, taken in the order in which the

* The stars are bodies which shine by their own light, and astronomers conclude, from every analogy yet detected, that they are suns. They are called "fixed," because to the eye they appear always in the same relative positions with respect to each other. The distance of the stars is so great that the difference of angular position, as seen from opposite points of the earth's orbit, a distance of a hundred and ninety millions of miles, has been found, in the case of one star only, to amount to so large a quantity as $2''$, according to Mr. Henderson's determination of the parallax of *a Centauri*. At this star, therefore, the sun, which to us appears under an angle of above half a degree, would subtend an angle of only two hundredths of a second.

† The planets are bodies which, like the moon, shine by light received from the sun and reflected to us; they revolve round the sun in the same direction as the earth, but in different periods of time. Mercury ☿, the nearest to the sun, revolves in 88 days; Venus ♀, the next, in 225 days. These moving in orbits inside that of the Earth, are called *inferior*

sun moves through them, that is, in the contrary direction to the apparent diurnal motion, are as follow:—

♈ <i>Aries</i> (the Ram).	♎ <i>Libra</i> (the Balance).
♉ <i>Taurus</i> (the Bull).	♏ <i>Scorpio</i> (the Scorpion).
♊ <i>Gemini</i> (the Twins).	♐ <i>Sagittarius</i> (the Archer).
♋ <i>Cancer</i> (the Crab).	♑ <i>Capricornus</i> (the Goat).
♌ <i>Leo</i> (the Lion).	♒ <i>Aquarius</i> (Water Bearer).
♍ <i>Virgo</i> (the Virgin).	♓ <i>Pisces</i> (the Fishes).

461. Besides this perpetual motion from west to east, the sun is always changing his declination, which varies between $23^{\circ} 28'$ N. and $23^{\circ} 28'$ S. He crosses the equator twice in the year, namely, about the 20th of March, in coming up to us in N. lat. from the southward, and again about the 23d of Sept. in going to the southward.

462. When the sun crosses the equator, he rises and sets at six o'clock in all parts of the world;* at these times, therefore, the days and nights are every where equal.

463. The two points in which the ecliptic, or sun's path, thus cuts the equator, are called the *Vernal*, or spring, *Equinox*, and the *Autumnal Equinox*.

464. The sun attains his greatest N. decl. about June 21st, and the greatest S. decl. about Dec. 22d. The points at which the sun seems at these times to be stationary in declination before he diminishes it, and at which the ecliptic and equator are most widely separated, are called the *Summer* and *Winter Solstices*.

465. As the light and heat received from the sun at any place vary with his altitude, and the time during which he remains above the horizon, and as both of these depend on the declination, the succession of seasons depends on the changes of the declination of the sun. The common or civil year, as most convenient for the affairs of life, includes the succession of the seasons. It is, therefore, the interval in which the sun leaves any parallel of declination and returns to it again, and is called a *tropical year*. Its length, that is, the average length of a number of such years, is $365^{\circ} 5^{\circ} 48'' 51''.6$, of common or mean time.†

planets. Mars ♂ revolves in nearly 2 years; Jupiter ♃, in nearly 12 years; Saturn ♄, in 29 years; Herschel ♃, in 82 years; and Neptune ♆, in 165 years. These last are called *superior planets*. Besides these there are numerous small planets [287 known in 1890] whose orbits lie between those of Mars and Jupiter. Some of the planets have satellites, or moons: Mars has two, Jupiter four, Saturn eight, Herschel six, and Neptune one.

* The observed times differ a little from 6h on account of refraction, No. 445.

† If the tropical year contained exactly 365 days, the arrangement of the calendar would be perfectly simple; but the necessity of counting by entire days in the affairs of life has introduced arbitrary expedients for checking the errors accumulated from time to time, from neglecting the excess over the last complete day. For example, suppose the year ends at midn ght on Thursday, then new year's day begins at the same instant, that is, at 0h on Friday morning, while the old year is really not yet out by nearly 6 hours. Next year 6 hours more of the new year will be anticipated, that is, new year's day will be reckoned 12 hours too soon; so that at the end of 4 years the beginning of the new year is anticipated by a whole day. By adding 1 day to the fourth year this error is removed, and the commencement of the calendar year is carried back to its true place nearly

The period of the commencement of the year, which has been adopted differently at different times, is at present (as established in this country by act of parliament) on January 1st, which is about 11 days after the winter solstice.

466. Since it is summer on that side of the equator on which the sun is, and winter on that on which he is not, the seasons in south latitude are reversed.

467. In the continual apparent revolution of the heavens round the earth, the circles of declination are perpetually describing angles round the poles, which are called, from the division of time into hours, HOUR-ANGLES.

468. An hour-angle, or horary angle (sometimes called also Meridian Distance), is the angle at the pole contained between the meridian of the place and the celestial meridian passing through the body; thus, ZPA is the hour-angle of A (figs. p. 162). An hour-angle is measured by the arc of the equator contained between the meridian of the place and that of the body; thus MB , fig. 2, measures ZPA .

The hour-angle is thus measured on the celestial equator in the same way as longitude is measured on the terrestrial equator.

469. The RIGHT ASCENSION of a celestial body is the arc of the equator included between the first point of *Aries* and the celestial meridian of the body: it is reckoned from west to east. Thus, if γ be the first point of *Aries*, fig. 1, p. 162, the arc γMB is the Right Ascension of the body A . The 360° of the celestial equator are divided into 24^h of R.A.

Thus R.A. is reckoned on the celestial equator exactly as the longitude of places on the earth is reckoned on the terrestrial equator. But as the stars do not preserve that constant position with respect to the meridians which they do with respect to the equator, there is not that correspondence between R.A. and longitude which there is between declination and latitude.

470. The apparent revolution of the stars is perfectly regular, and is the only motion of the kind known.

One revolution of the earth round its axis, or, which is the same thing, the return of the same fixed star to the meridian after completing the circle, constitutes a *sidereal day*; this day consists of $23^h 56^m 4^s$ of common or mean time, as measured by clocks and watches. It is divided into 24 hours, called sidereal hours, and these into sidereal minutes and seconds. Thus a sidereal day is about 10^s

But the excess above 365^d does not amount to 6^h by $11^m 8^s$ nearly; hence at the end of the fourth year an error of the contrary kind is introduced of $44^m 32^s$, which amounts to nearly 3 days in 4 centuries. This error led to the reformation of the calendar by Pope Gregory XIII., in 1582, when the vernal equinox, which at the Council of Nice, in 325, had taken place on the 21st March, fell on the 11th. Hence, leaving 10 days out of the calendar, which was effected by calling the 4th of October, 1582, the 15th, brought matters right again. The error had amounted to 11 days when the change was adopted in this country in 1751.

This error is prevented for a long period in future by the Act 24 Geo. II., which directs the leap-years 1800, 1900, 2100, and so on, to be considered as common years, and 2000, 2400, 2800 as leap-years.

an hour shorter than a common or mean day; and the sidereal hours, minutes, and seconds, in the same proportion.

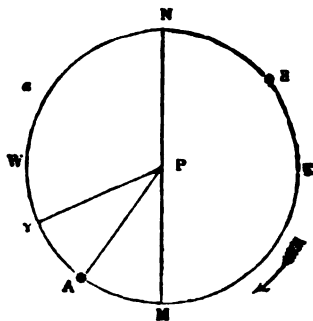
The sidereal day being thus, in round numbers, 4^m shorter than the mean day, a star that passed the meridian last night at 9 P.M. will pass this evening at 8^h 56^m, and so on, till after a few months it will pass at noon. (See Table 27.)

471. **SIDEREAL TIME** begins (that is, a sidereal clock, regulated to sidereal time, shews 0^h 0^m 0^s) when the first point of *Aries* is on the meridian, and is counted through 24 hours, till the same point returns again; the hour-angle of this point is accordingly sidereal time.

The hour-angle of the first point of *Aries* is the right ascension of the meridian, No. 469, which is accordingly sidereal time. Difference of R.A. may, in like manner, be considered as a portion of sidereal time.

472. P is the pole, the circle N W M E the celestial equator, to which the measures of all hour-angles are referred. The bent arrow shews the direction of the apparent diurnal motion of the celestial bodies, reckoned from east to west supposing the spectator to face the south. M N is the observer's meridian.

A is any celestial body, as a star, which has passed the meridian at M, then A P M is the *hour-angle* of A, of which the arc A M is the measure.



(1.) B is a star to the eastward of the meridian, which it has passed at N; its hour-angle, reckoned westwards, is measured by M W N B. We may, however, employ also B M, the measure of the hour-angle reckoned eastwards. Thus, instead of 14^h 11^m W. we may call it 9^h 49^m E. As in dealing with hour-angles we refer directly to the number of hours which they contain, and which are measured on the equator, it is unnecessary to form the hour-angle of B by joining B and the pole.

(2.) Let the first point or beginning of *Aries* be at γ , having passed the meridian before the star A; then γ M is the *right ascension* of the meridian, that is, sidereal time. The R.A. of A is γ A; that of B is γ M B, reckoned always from west to east, or opposite to the diurnal motion; and γ N B is the supplement of the R.A. of B to 24 hours.

(3.) The *sidereal time* γ M is the sum of the arcs γ A and A M, that is, of the hour-angle and R.A. of the star A. Again, γ M is the difference between the arcs a M and a γ , that is, between the hour-angle of the star a and the supplement of its R.A. In the case of the star B, the sid. time is the difference between its R.A. γ M B, and its hour-angle M B.

Hence it is easy, when the hour-angle of a star of known R.A. is given, at any instant of time, to construct the figure to shew the sidereal time, thus:—Having drawn a circle, with the meridian, lay

off, by a scale of chords, the star's hour-angle; the position of the star being now given, lay off its R.A., reckoning from the *star* in the *same direction* as the apparent diurnal motion (for thus the R.A. reckoned back again from this point γ will agree with the place of the star). This gives the place of γ , the hour-angle of which, reckoned westward, is the sid. time required.*

Ex. 1. The hour-angle of a star is $2^h 28^m$ W.; its R.A. $3^h 47^m$.

Lay off $2^h 28^m$, or 37° , to the W. of M, and $3^h 47^m$, or $56^\circ 45'$, further on towards the west: then the sid. time measures $93^\circ 45'$, or $6^h 15^m$.

Ex. 2. The hour-angle of the moon is $9^h 13^m$ W.; her R.A. $18^h 34^m$.

Lay off 6^h , or 90° (No. 107), and $3^h 13^m$, or $48^\circ 15'$, from M, westwards. Then lay off 3 times 6^h , or 90° , and 34^m , or $8^\circ 30'$, further: the sid. time measures $56^\circ 45'$, or $3^h 47^m$.

Ex. 3. The hour-angle of a star is $14^h 11^m$ W., or $9^h 49^m$ E.; its R.A. $5^h 21^m$.

The sid. time is $10^h 32^m$.

All hour-angles, which are differences of R.A. of the meridian and a celestial body, may be considered as portions of sidereal time. The *interval of time* in which a body of variable R.A. *describes* an hour-angle depends on the rate at which its R.A. changes.

473. The earth's motion round its axis being perfectly uniform, becomes the real standard of uniform measures of time; but as any star passes the meridian nearly 4^m earlier every night, the beginning of the sidereal day has no connexion with that of the common or civil day, as determined by light and darkness.

474. The hour-angle of the sun, reckoning always westward from the meridian, is APPARENT TIME. Thus, when the sun's meridian has passed over 48° of the celestial equator to the westward of the meridian of the place, it is said to be $3^h 12^m$ apparent time. This is the time shewn by the sun-dial.

475. The interval between the sun's passing the meridian on one day and the next, or the *apparent solar day*, is not always of the same length, the difference being sometimes half a minute between one day and the next. Apparent time serves well enough in cases where this irregularity does not appear, or is of no importance; as for example at sea, where, from the continual change of longitude, the time must be obtained by observation: but where account of the time is to be kept by mechanism alone, it must necessarily be divided into portions of invariable length.

The time for general use must, accordingly, unite the two advantages of being regulated by the sun, and of being perfectly uniform. The mean or average day of 24 hours must therefore be an average taken of all the days in the year, that is, such a day as the sun would regulate if he moved uniformly in R.A. This average day is called

* In the questions which this figure illustrates, motion round the pole only is considered; since, therefore, the place of a celestial body on its meridian is unconnected with the motion of the meridian itself round the pole, no regard is had to declination.

As the spectator will naturally refer the hour-angle of a star to the elevated pole of the place, in south latitude the figure will appear reversed, since the diurnal motion there appears from right to left in facing the equator. The figure, however, may be drawn in that manner which may appear the clearest, the only point essential to be kept in view, being that the R.A. is reckoned the opposite way to the apparent diurnal motion.

the *mean solar day*, and time thus regulated is called *mean solar time*, or **MEAN TIME**, which is that shewn by clocks and watches.

476. The sun being generally either behind or in advance of the position which he would have occupied if he had moved uniformly, mean time is in general either fast or slow, on apparent time. The correction for this irregularity, that is, the difference between the sun-dial and the mean solar clock, is called the **EQUATION OF TIME**. Mean time is, therefore, deduced from apparent time, by applying the equation of time. See the *Nautical Almanac*, p. 1. or 11., or Table 62.

477. **THE SIDEREAL TIME AT MEAN NOON** is the right ascension of the meridian at the instant when the sun, if he moved uniformly, would be on it.

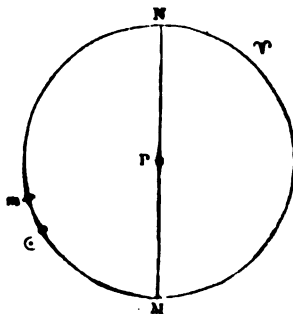
It is evident that this element, from its nature, varies uniformly; now, since the sun's R.A. varies irregularly, and since the equation of time, which is the correction that removes this irregularity, must also vary irregularly, it follows that the unequal variations of the equation of time and the sun's R.A. are together equivalent to the single and uniform variation of the sid. time at mean noon; and herein consists the great convenience of employing the sidereal time at mean noon, which has been given in the *Nautical Almanac* only since 1834.*

478. (1.) Let \odot be the place of the sun, at about 4 P.M., m the place where he would be if he always moved uniformly; then $\odot M$ is *apparent time* (No. 474), $m M$ is *mean time*, and $m \odot$ is the *equation of time*. The equation is here *additive* to app. time, as is the case from January to March, and from July to August. (See Table 62.)

(2.) Let γ be the first point of Aries; then, while the sun and γ revolve, the sun moves contrary to the diurnal rotation, or is always *increasing* his R.A., or the arc $\gamma N \odot$, by nearly 1° a-day. The complete revolution of γ constitutes a *sidereal day*; that of \odot , an *apparent solar day*; and that of m , a *mean solar day*.

After 24 sidereal hours the sun has still to describe about 1° , or one 360th part of the circle to complete it; the time necessary for which is about one 360th of 24 sidereal hours, or 4 sidereal minutes. Thus the solar day is longer than the sidereal day by about 4^m . The *mean solar day* being divided into 24 hours, the sidereal day is $23^h 56^m 4^s$ of such a day.

(3.) When m is on the meridian at M , the a.c. $M m \gamma$, or the



* This element, which is the R.A. of a mean, or imaginary sun, is a very different thing from the R.A. of the sun at *mean noon*, with which it has been confounded: the latter can differ only a few seconds from the R.A. \odot at *apparent noon*, but may differ from the *Sidereal Time at mean noon* by the whole amount of the equation of time, or sixteen minutes.

sun's mean R.A., is the *sidereal time at mean noon*. When m has arrived at m in the figure, this quantity has changed by an amount proportional to the mean time $M m$.

The \odot moves sometimes more quickly, at others more slowly; the point m (which is merely an imaginary situation of \odot , deduced by calculation, from knowing the limits within which the irregularities of its motion are confined) moves equably. Hence $m \odot$, the difference of these two, changes unequally.

(4.) By No. 472 (3) the sidereal time, or place of the point γ , is obtained from the hour-angle of any celestial body. By applying to the place of γ the sid. time at mean noon, we obtain the place of m , or mean time.

Thus Mean Time is found from the hour-angle of a star.

479. Since the sun m passes over 15° of the circle in one mean hour, he arrives at the meridian of a place 15° west of N M one hour after he has passed N M, that is, at one o'clock of the time at any place, or all places, of which N M is the meridian. In like manner he passes a meridian 15° east of M one hour before he arrives at M, that is, when the time on M is 11 o'clock in the forenoon, or 23 hours after the noon of the day before.

Thus the beginning of the day, and therefore the hour or time of the day, at one place differs from that of another place by the difference of longitude of the places; the time at the easternmost of the two being in advance of, that is, greater than, the time at the other. Hence when the times proper to two places at the same instant are known, their diff. long. is determined, or the relative positions of their meridians.*

480. The Civil Day is dated from midnight, and the twelve hours are computed twice over; the Astronomical Day is dated from noon, and runs through the twenty-four hours.

Ex. 1. October 3d, 3^h 18^m P.M., civil time, is the same astronomical time.

Ex. 2. January 3d, 4^h 25^m A.M. civil time, is reckoned January 2d, 16^h 25^m astronomical time.

Ex. 3. April 1st, 11 A.M. is, astronomically, March 31st, 23 hours.

481. The GREENWICH DATE is the time at Greenwich corresponding to any given time elsewhere.†

* The diff. long. is found as well by means of the motion of a star as of the sun, that is, by means of a clock or chronometer regulated to sidereal time, as well as by one regulated to mean time. For although the absolute interval of time employed by a star in moving from one meridian to the other is less than that employed by the sun, yet it is divided into the same number of hours, minutes, and seconds, but which are of smaller magnitude and thus the difference of time results, in numbers, the same.

† Here terminates all requisite description of the terms used in the rules in the present volume. The other terms which occur in the Nautical Almanac will be described in the *Theory*.

In this chapter we have sometimes spoken of the earth as fixed and the heavens as movable, although this is contrary to fact, because the appearances alone furnish us with the measures of time, without any regard to the actual state of things.

Again, we have considered the earth as a sphere instead of a spheroid (No. 180). The consequences of the oblateness, in an astronomical point of view, are that the planes of the

482. It will be found a useful exercise of what has preceded to verify the following remarks:—

(1.) No star of which the pol. dist. is less than the lat. can set; and no star of which the pol. dist. exceeds 90° plus the colat. (S M, fig. p. 162) can be visible.

(2.) When the pol. dist. is less than the lat. the star passes the meridian both above and below the pole.

(3.) When the pol. dist. is less than the colat. the star passes the meridian between the zenith and the pole, and does not pass the prime vertical.

(4.) When the declin. is 0, or the pol. dist. 90° , the body rises and sets in the E. and W. points. The hour-angle at rising and setting is 6^h , and the body is seen raised on the prime vertical by the effect of refraction; unless it is the moon, which, from her parallax being greater than her refraction, is not seen at the precise time of her rising and setting.

The object is above the horizon for 12 hours, and 12 hours below it.

In this case the amplitude is 0, except from the effect of refraction.

(5.) When the pol. dist. exceeds 90° , the celestial body rises and sets on that side of the E. and W. points which is farthest from the elevated pole; the hour-angle at rising and setting is less than 6^h : the time during which the body is above the horizon is less than 12 hours, while it is more than 12 hours below the horizon. The body does not pass the prime vertical above the horizon; and the amplitude is reckoned towards the S. in N. lat., and towards the N. in S. lat.

(6.) When the pol. dist. is less than 90° , the celestial body rises and sets on the same side of the E. and W. points as the elevated pole; the hour-angle at rising and setting is greater than 6^h . The body is more than 12 hours above the horizon, and less than 12 hours below it. The amplitude is reckoned towards the N. in N. Lat., and towards the S. in S. Lat.; the body passes the prime vertical twice. The hour-angle at the passage of the prime vertical is less than 6^h . (See Table 29.)

(7.) A star having a certain declination always rises and sets in the same points, and passes the meridian and prime vertical, or any other circle of altitude at the same altitude, without regard to its R. A.

circles of altitude (excepting the meridian) do not pass through the centre, and that the length of the radius, or line drawn from the centre to the place of the observer, is different in different latitudes. The first of these conditions produces no sensible effect in practice, because the Time is not affected by it, and the same Latitude (though differing from the latitude on a sphere by the quantity in Table 52) results alike from all observations, of whatever kind, of a body not affected by parallax,—and thus the oblateness, however great, would always be neglected in determining a place by observation of the stars or the sun. By the second condition the parallax of the moon is affected, and a further correction of her apparent place becomes necessary.

We have also described the first point of γ as fixed, whereas it has a very slow motion. The stars, also, though called fixed, have slow proper motions. These and other points not necessary to our present subject will be treated more at large in the *Theory*.

(8.) As the place of a star or any celestial body is determined by its R. A. and Decl., and as, at the place of the spectator, the position of the celestial equator, to which both these are referred, is fixed, it is easy to know whereabouts any star is to be looked for at any time. When, as is commonly the case, the time (mean or apparent) is given, the sun's hour-angle is known; and therefore, when he is invisible, his place on the equator may be estimated. By means of the sun's place, and his R. A., the place of the first point of Aries may be estimated; then the star's R. A. gives the place of its meridian on the equator, and its declination the place of the star with respect to the equator. When the sidereal time is given, the place of the first point of γ is at once known, just as the place of the sun is known from the apparent time.*

* The position of the equator, and the relations among the Latitude of the place, the Time, and the Hour-angle, Altitude, and Azimuth of a celestial body, are best illustrated by a celestial globe. The broad horizontal rim represents the Rational Horizon (No. 421). The brass meridian of the globe being laid N. and S., and the Pole elevated, by the degrees marked on it, to the latitude (No. 449), the globe represents the celestial sphere as shewn in figs. 1, 2, p. 162. The position of the sun is found by marking the sun in his place in R. A. and Decl., by the help of the divisions on the globe, and then setting the sun at his proper hour-angle by means of the hour-circle near the pole. The Alt. or Zen. Dist. is measured by a graduated slip of brass, or by a thread, as in the note, p. 129. It is unnecessary to enter further into details, as the reader who well understands the definitions above will find no difficulty in solving any useful "problem on the globe" which can be proposed, without burdening his memory with technical rules.

In the absence of a globe, distinct ideas may be obtained of the actual positions of the celestial bodies by a circular card, as a compass-card, having the hours marked on the edge, and an axis, as a pencil, put through the centre perpendicular to the card. If this axis be laid N. and S., and the north end (in north lat.) raised up till it is inclined to the horizon at an angle equal to the latitude, it will represent the polar axis round which the celestial bodies revolve, the card representing the equator. The 0^h being brought up to the meridian, the hour of the day at the edge will shew the place of the sun's meridian at the time. If the 0^h be made the first point of γ , the hours become hours of R. A.; if, then, the \odot be marked on the edge, on its proper R. A., and then turned round to the position proper to the hour of the day, the place of the first point of γ is seen.

Suppose, now, a small telescope were placed on the axis making an angle with the plane of the equator, or the card, equal to the declination of some star, then, while this star revolves parallel to the equator, the telescope, kept at the same angle, could at any time be directed towards the star by merely turning the axis round. A large instrument is constructed on this principle, and is called an *Equatoreal*!

CHAPTER II.

INSTRUMENTS OF NAUTICAL ASTRONOMY.

I. THE REFLECTING INSTRUMENTS.

II. THE ARTIFICIAL HORIZON. III. THE CHRONOMETER.

I. THE REFLECTING INSTRUMENTS.

483. THESE are instruments for measuring angles between two objects, by bringing the reflected image of one of them to coincide with the other seen directly. They are necessary for observing altitudes of the heavenly bodies at sea, where the spectator has no fixed point of reference except in the horizon. On shore, and often on a field of ice, the fixed point required in observing altitudes is obtained by means of the artificial horizon.

484. The instruments of this class which are in most common use are the quadrant, sextant, and reflecting-circle. For convenience, we shall describe the adjustments generally under the two former; and as every person in possession of an instrument will be instructed by the maker or some expert person in the names of the different parts, and also in the mode of handling it, and packing it in the case without danger of distortion, we shall confine ourselves merely to matters of general reference.

1. *The Quadrant and Sextant.*

485. The quadrant contains an arc of more than 45° , and measures a few degrees more than 90° ; it is usually made of wood, and the graduated arc, which is ivory, reads to minutes, and sometimes to $30''$. The sextant measures a few degrees more than 120° ; it is made of brass, and sometimes reads to $10''$. The quadrant serves for common purposes at sea, but the sextant is required for taking a lunar observation.

The observer should be in the habit of employing good instruments of their kind, as inferior instruments naturally induce careless and imperfect observation.

486. The sextant made of a very small size, and thence called the Pocket Sextant, is adapted to the use of surveyors, travellers and others, on occasions in which minute accuracy is not necessary.

[1.] *Manner of Using.*

487. To take the sun's altitude at sea. Set the index at 0, put down a screen before the central mirror, hold the instrument in a vertical position, and direct the sight, through the sight-vane and horizon-glass, to that part of the horizon which is exactly under the sun. Now move the index on with the left hand, and the image of the sun will appear to descend towards the horizon. Vibrate the instrument round the line of sight, and make the lower limb touch the horizon: this gives the *observed altitude of the lower limb*.

488. This last altitude is sometimes near enough; but for accuracy, having made a rough contact as above, put in the telescope, previously set to distinct vision by looking through it at the horizon; the image being now magnified, the contact is made more correctly. In general the telescope should not be fixed till a rough contact has been made, because it narrows the field of view, and increases the difficulty of bringing the images together.

The contact must be made in the centre of the field: if it is too near the plane of the instrument, or too far from it, the angle will be too great by the quantity in Table 54.*

489. When there is a tangent-screw, clamp the index, and make the contact perfect by turning the screw,—some further remarks on which will be made in the proper places.

The tangent-screw should be kept nearly middled when not in use.

490. To take the altitude of a star. Set the index to 0, direct the sight to the star, hold the instrument vertically, and move the index onwards: the image of the star will be seen to descend. This method is proper to avoid bringing down the wrong star, but should not be practised with the sun, as it exposes the eye to an intense light, which may derange it for the whole observation.

491. The shades, or coloured glasses, placed before the two mirrors, tend to equalise the brightness of the object and the image, and sometimes distinguish one from the other by the difference of colour. The shades require to be particularly well ground, because, if the surfaces are not strictly parallel, the rays in passing through the glass are turned out of their former direction: hence, when a defective shade is placed before each of the mirrors, the angle is affected by the sum or the difference of the errors due to the shades. It is advisable, therefore, in general, to employ a dark glass at the eye-end of the telescope, by which the shade before one or both of the mirrors may be dispensed with. Also, if this glass is not perfect, the rays from the object and the image are affected alike, and the angle between them remains unchanged.

A card screen, to slip over the eye-end of the telescope, is useful in protecting the eye from accidental glare.

492. The observer acquires, by attention, the power of estimating

* Mr. Hartnup, director of the observatory at Liverpool, acquaints me that he has constantly found sextant observations to come out more accurately in proportion as he narrowed the field by closing the wires.

the proper angle at which to set the index for a rough contact, and thus saves time. It also effects some saving of time to have the tubes of the telescope marked at the observer's focus.

493. When the angular distance between two objects is to be measured, the plane of the instrument is held in the line joining them, and the sight is directed to the fainter of the two. When, therefore, the brighter object is to the right, the instrument is held face upwards, and the image of the right-hand object brought to touch the left-hand object seen directly; but when the brighter object is to the left (as in observing the distance between the sun and moon in high north latitudes in the forenoon), the instrument must be held face downwards, the sight being directed to the right-hand object. The contact must be made in the centre of the field, as directed above.

[2.] *Reading off the Angle.*

494. The angle having been observed, its measure is to be read off. The arc being divided into degrees, and these subdivided into halves, thirds, &c., the smallest division contains several minutes, and the angle can thus be read, but roughly, from the arc itself.

In order to read to $1'$, or a fraction of $1'$, a scale called a *vernier* is applied to the arc; this is a portion of an arc having the same centre, and divided into *one part more* than an equal portion of the arc itself. The manner in which a more minute reading is obtained may easily be understood from the following example:—Suppose a division on the arc to be $\frac{1}{3}$ of 1° , or $20'$, and the vernier to be equal in length to 19 divisions, or $6^\circ 20'$, but divided into 20 equal parts; then each of the divisions on the vernier is $\frac{1}{20}$ of $6^\circ 20'$ or $380'$, that is $19'$, and therefore the difference between one division on the arc and one on the vernier is $1'$.

Suppose the beginning of the vernier and that of the arc to coincide, as in Fig. 1; then the first of the dividing lines of the vernier falls short of the first dividing line of the arc by $1'$; therefore, if we make these lines coincide, we advance the vernier $1'$. Again, to make the second dividing lines of each coincide, we must move the vernier through $2'$, and so on.

In Fig. 2 the 0 of the vernier stands between $20'$ and $40'$ after the division at 3° , and the first coincidence is at 9; hence the arc measured is $3^\circ 29'$.

Fig. 1.

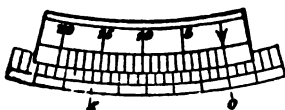


Fig. 2.



Fig. 3.



When the index is moved the contrary way, the 0 of the vernier goes off the arc, as seen in Fig. 3. As the 20 of the vernier stands at $6^{\circ} 20'$ when the two zeros coincide, if we move it 1' to the right, the coincidence will occur at 19, and at 18 if we move it 2', and so on. Hence, to measure an angle *off the arc*, we must read from the *end* of the vernier. The arc shown is 32' off the arc.

[3.] *Adjustments.*

495. (1.) The Index-Glass, or central mirror, must be perpendicular to the plane of the instrument.

Set the index about 60° ; then, if the image of the arc in the mirror appear in perfect continuation with the arc itself, the adjustment is perfect; if the reflection seem to droop from the arc itself, the mirror leans back; if it rise upward, the mirror leans forward. The position is rectified (in quadrants only) by the screws on the back. This adjustment generally rests with the maker, but it should be occasionally verified by the observer.

(2.) The Horizon-Glass, or fixed mirror, must be perpendicular to the plane of the instrument.

Set the index to 0, hold the instrument horizontally, look through the glass at the sea-horizon, or other distant object, and give the instrument a small nodding motion: then if the reflected image appear neither above nor below the real object, the adjustment is perfect; if the *image* be the *lower*, the glass stoops *forward*; if it be the *higher*, the glass leans *backward*. The position is rectified by the screws.

(3.) The line of sight of the telescope must be parallel to the plane of the instrument in which the index moves.

Place the two wires of the telescope parallel to the plane of the instrument. Select two distant objects from 100° to 120° apart, as two stars, or the sun and moon, and make an exact contact at the lower wire, or that nearest the instrument. Now move the instrument so as to throw the images in contact upon the upper wire; if the contact is still perfect (the images having overlapped in the middle of the field), the adjustment is perfect; if they have separated, the object-end of the telescope droops; if they overlap, it rises. The position is rectified by the screws in the collar. When this adjustment is defective, the observed angle is always *too great*. (See Table 54.)

[4.] *Index-Error.*

496. The graduation of the arc should commence at a certain point; when this is not the case, the Index-Error, as it is called, must be measured.

The point at which the graduation of the arc is supposed to begin, is that at which the index stands when the mirrors are parallel, as is the case when the image of a distant object is seen to coincide with the object itself. The index-error, therefore, is merely the error of the place of the *beginning* of the divisions, and affects all angles alike.

To find the Index-Error. (1.) By the Horizon Hold the instrument vertically, and make the image of the horizon coincide with the horizon itself as accurately as possible. If the 0, or zero of the

index, now stand at 0, there is no index-error; if it stand *on* the arc, the index-correction is so much *subtractive*; when *off* the arc, *additive*.*

Ex. The horizon and its image being made to coincide, the reading is 3' on the arc. Then 3' is the INDEX CORRECTION to be *subtracted* from every angle observed.

Any distant object, or a bright star, answers the purpose.

(2.) By the Sun. Measure the sun's horizontal diameter, † moving the index forward on the divisions; read off the measure which will be *on* the arc; then cause the images to change sides by moving the index back; take the measure again, and read off; this reading will be *off* the arc: half the difference of the two readings is the index-correction.

When the diameter *on* the arc is the *greater*, the correction is *subtractive*; when the *lesser*, *additive*.‡

Ex. 1.	On the arc	32' 10"
	Off	29 50
		<u>2 60</u>
IND. CORR.	<i>subtract</i>	1 10

Ex. 2.	On the arc	30' 10"
	Off	33 40
		<u>3 30</u>
IND. CORR.	<i>add</i>	1 45

In consequence of the spring or elasticity of the index-bar, the error will be different for the *onward* and for the *backward* motion of the index. It has been recommended, therefore, to turn the tangent-screw right and left alternately, in making successive contacts, by which a partial compensation is obtained. This source of discrepancy is, however, effectually removed by taking all observations, including that for index-error, with the same motion of the index-bar. The *onward* motion being adopted as the most natural, the tangent-screw is always employed to close the object and the reflected image, and is thus always turned in the same direction.§

One-fourth of the sum of the two readings should be equal to the sun's semi-diameter in the Nautical Almanac. This affords a test of the accuracy with which the observation has been made.

497. The adjusting screws are *never to be touched except from*

* When the mirrors are parallel, a very distant object is exactly covered by its image; but at a near object the distance between the mirrors subtends a sensible angle, or has sensible *parallax*, and this coincidence does not take place. The parallax of a 12-inch sextant at half a mile distance is about 21", and is smaller for smaller dimensions and greater distances, in simple proportion. Hence, for the purposes of adjustment, distances exceeding this should be employed.

Captain Beechey suggests a method of adjustment by parallel rays. Naut. Mag. 1844. p. 505.

† As the refraction increases towards the horizon, the lower limb is more raised than the upper limb, and the vertical diameter is shortened. This, at very low altitudes, produces a flattened or oval form in the sun and moon.

‡ If both readings are on the arc, which can only occur when the index-error is nearly half a degree, the ind. corr. is the mean, and subtractive; if off, additive.

§ Sir F. Beaufort, to whom I am indebted for the suggestion, acquaints me, that from the sensible influence of the spring of the index-bar in nice observation he uniformly adhered to this plan, and caused it to be followed by his officers.

The late Captain Basil Hall informed me that he made it his practice to obtain the index-error both for the onward and the backward motion of the index employing the former error in all observations by the onward motion, such as the lunar distance when increasing, and the latter in observations by the reverse motion, as for the lunar distance when decreasing.

necessity, and then with the greatest possible caution.* When two screws work against each other, care must be taken, in tightening one, to loosen the other if necessary.

498 Besides errors from these causes, there are others which are neither detected nor remedied so easily: the divisions on the arc are liable (though in these days in a very slight degree) to inaccuracy, and the centering of the arc is not always perfect.†

In order to test the accuracy of the arc in either of these respects, in different places, it has been proposed to measure the distance of two stars, comparing the distance with that shewn by a circle, or by an approved sextant, or deduced from calculation.‡ The absolute error being thus found for certain places on the arc, the correction for any angle may be inferred by proportion.

499. As the two sides of the coloured glasses are not always exactly parallel, the shades may vitiate the angle. (No. 491.) Some observers find, by actual trial, the error due to any shade or combination of shades. The shade in the eye-piece, as before stated, has not this defect;§ but an image-shade is generally indispensable in taking a lunar observation.

[5.] *Methods of Increasing the Efficiency of the Sextant.*

500. The necessity, under certain circumstances, of observing large angles, and the difficulty of measuring them, arising from the obliquity with which the rays of light, in such cases, fall on the central mirror, have led to the suggestion of various plans for extending the powers of the sextant.

Capt. Fitzroy has employed an additional fixed horizon-glass, placed at a constant angle with the ordinary one, by means of which the image of an object above, or to the right-hand of another in the

* Particular attention is called to this point, because it is a common failing of "overhandy gentlemen" (to use Troughton's language) to "torment" their instruments. It is better that error should exist, provided that it is allowed for nearly, than that mischief should ensue to the instrument from ignorant attempts at a perfect adjustment; and the skilful observer, instead of implicitly depending upon the supposed perfection of his instrument, will endeavour to avail himself of those cases in which errors, if they exist, will destroy each other.

† It is also necessary that the two surfaces of the central mirror should be exactly parallel. This parallelism can be tested only by observing an angle between two objects 120° or 130° apart, and then repeating the observation with the mirror in a reversed position. Half the difference, if there is any, between the two results is the angle between the surfaces. As in the best instruments the mirror is fixed, this cannot be put in practice, and the consideration is therefore omitted from the adjustments in the text. This error, however, when it exists, is obviated by the method described in the next sentence of the text.

‡ The stars for this purpose must be taken from the Nautical Almanac, as the places are required with precision. The true distance may then be computed by the rule No. 339 (2), using the Diff. of the stars' right ascensions for D. Long., and their polar distances for the colatitudes. The true distance may then be reduced to the apparent (which is that measured by the instrument), by No. 842, substituting one of the stars for the moon, omitting the second corr., and applying the other star's correction the *opposite way* to that laid down in the tabulated directions for the star.

§ Working with the artificial horizon, the eye-piece of the inverting tube should, if possible, be used instead of the shades of the sextant; if shades are used, endeavour always to use the same. The meridian altitude of the sun should, if possible, be observed with the eye-piece, as the latitude obtained from it can then be measured more satisfactorily with that determined by the stars.

line of sight, is seen in the field when the index is at 0, and thus a portion of the angle is measured in addition to that on the arc.

501. Admiral Beechey had a sextant constructed with a second central mirror over the usual one, and working on the same pivot, the arc of which, being concentric with the usual arc, is divided by the same stroke. Both index-glasses are adapted to the same horizon-glass.*

Any angle is measured by putting one index forward upon the arc to any convenient number of degrees, and moving the other until both reflected images are seen in the horizon-glass.

Each arc has its proper index-error.

502. Mr. C. George, R.N., has constructed a double pocket-sextant, by joining two small sextants by the face. This instrument, which scarcely exceeds the box-sextant in size, possesses for various approximate purposes, and for surveying, the advantages of the double sextant.†

503. The double sextant has some important advantages; it affords two alts. of the same or different celestial bodies in quick succession: this is a point of much consequence when the body appears for short intervals only, as between flying clouds, and also in observing at night, as it saves the disturbance to the eye caused by reading off; it measures the angular distance between opposite points of the horizon,‡ and thus serves as a dip sector; it measures two terrestrial angles at the same instant, and thus serves as a director.

The index-error of a compound angle measured by a double sextant is composed of the errors proper to each arc.

The error of parallelism (No. 495) in a compound angle is materially reduced, since in practice each portion is less than 90° .

504. In observing altitudes at sea by the double sextant, set any angle on the upper sextant; then, facing that part of the horizon which is opposite the sun, find his image, and bring up the horizon to the lower limb, by moving the lower index: the sum of the two readings is the suppl. of the alt. of the upper limb, affected by the dip and the index-error.

Now unclamp the indexes, set the upper one to an angle less than the alt., find the image under the sun, and bring up the horizon to the lower limb: the sum of the readings is the alt. of the lower limb, affected by the dip and the index-error.

Half the difference of the two sums is the app. zen. dist. cleared of the dip, semi-diameter, and index-error.

* Admiral Beechey acquainted me that he constructed this sextant for the purpose of obtaining the measures of the angles between two terrestrial objects at the same instant and by one observer: a point of considerable importance in surveying, or in laying down soundings, while the observer himself is in motion. A further advantage afforded by the construction is, that when the right-hand object is too faint to be reflected, the sextant does not require to be inverted. The instrument is constructed by Cary.

† Made by Cary.

‡ The difference between this angle and 180° is twice the apparent dip. Thus, if this angle, measured downwards, is $179^\circ 48' 30''$, the apparent or actual dip is $5' 45''$. The dip sector, being inconvenient and little used, is not described in the text.

2. *The Repeating Reflecting Circle.*

505. On this circle the measure of the angle observed by reflection, as in a sextant, is carried over any part or the whole of the circumference: this is effected by making the horizon-glass itself movable round the centre, and attaching to it a vernier. By thus *repeating* the same angle on different parts of the divided edge, the errors of the index, of the coloured shades, and of the centering, are nearly, if not altogether, removed; also, since the indexes follow each other round the circle (each mirror alternately acting the part of the fixed horizon-glass), the angle finally registered is the sum total of all the repetitions; and thus one reading alone contains the result of any number, however great, of separate observations. The arc read off, divided by the number of observations, gives the measure of the required angle.

506. When the angle changes during the observation, the arc finally registered is not the mere repetition of the same angle, but the sum total of *different angles*; it is therefore necessary to understand how the *time* is to be noted.

Suppose, for example, at $5^h 20^m$ the angle is 45° , and at $5^h 26^m$ it is 46° (neither being read off); now, at $5^h 20^m$ the first index would shew 45° , and at $5^h 26^m$ the second index would shew the sum of 45° and 46° , or 91° , *half* of which, or $45^\circ 30'$, in this case obviously corresponds to the *middle time*, $5^h 23^m$.

The same appears generally thus: the last arc read off measures the first angle, the repetition of the same angle, and the change upon it during the interval of the two observations; therefore half the arc measures the angle, and half the change upon it, supposed uniform, which corresponds to the middle time.

If, now, a second pair of angles, as before, be observed, a second angle with its time is obtained, and so on; hence, as long as the change of the angle is *uniform*, the arc read off, being divided by the number of observations, corresponds accurately to the mean of the times.

The time is therefore to be noted at each contact.

507. The Circle is made in various forms: we shall confine ourselves here to the description and use of those known by the names of Borda's and Dollond's Circles.* Figures are purposely omitted, and the general description will be easily followed with the instrument itself.

In using the circle, care must be taken to push the crooked handle out of the way of the telescope.

* Troughton's Reflecting Circle, which does not repeat, is capable of great precision; but it does not seem so well adapted to general practice, especially at sea, as the repeating circle: for the three indexes aggravate the inconvenience and tediousness of reading off; and the instrument, instead of facilitating, like the repeating circle, the multiplication of observations, affords merely a correct measure of an angle which, from the motion of the ship, is itself observed inaccurately.

[1.] *Borda's Circle.*

508. In Borda's Circle, the horizon-glass and telescope revolve together round the centre, like the central mirror, carrying a vernier, which we shall call A.

Sometimes another vernier is placed opposite to A, and moves with it. The central mirror carries, like a sextant, a vernier, which we shall call B. The circle is divided into 720° .

The horizon-glass and telescope are attached to an inner circular arc divided to degrees, which is called the *finder*, as it enables the mirrors to be set to contain any angle, and the objects can thus be at once brought into contact roughly. When B is set to 0 at the middle of the finder, the mirrors are parallel. The divisions on the finder are reckoned in both directions from the 0.

509. To use the circle as a sextant. Before this can be done we must know the reading of B when the mirrors are parallel. To find this, set A accurately to 720° ,* and clamp it. Set B to 0 on the finder, nearly, and measure the sun's horizontal diameter: read off. Cross the reflected image to the other side of the sun, and read off: the mean of the two readings is the *constant angle* required, and is clear of index-error.

To observe, move B as in a sextant.

After observation, examine the setting of A, as any error in this is so much index-error.

510. By moving the index opposite ways, observations may be taken backwards and forwards, from the same point on the arc; but the real efficiency of the repeating circle consists in what is called the *cross-observation*, to which we shall now proceed.

To observe an Altitude by the cross-observation. Set A† accurately at 720° (or at 360°); set B to 0 on the finder roughly; observe the alt. with B as with a sextant; read off B roughly on the finder; unclamp A, and move it on the finder, in the order of the divisions on the circle, till the 0 on the other side of B stands at the angle read off. Turn the circle over, hold it in the other hand, and complete the contact by turning the tangent-screw of A.

The vernier A now registers the *first pair*, or *double* the altitude required.

To proceed with the repetition. Unclamp B, set it on the finder at the same angle as before; hold the instrument as for the first observation; complete the contact. Unclamp A, move it onwards as before till the 0 stands at the angle read off; complete the contact. This is the *second pair*, or *four times* the required altitude.

* This index will, in some circles, stand at 360° , and may require to be moved backwards; 360° would then be subtracted from every angle measured by this index alone. The above instructions will, with a trial or two, be found sufficiently intelligible.

† It is usual to fix first the index called here B, as directed by Borda himself, and repeated by other writers; but it is immaterial which index is first fixed, or at what part of the circle, provided the vernier be read off. The index A is recommended here in order to assimilate as much as possible the use of the circle to that of the instruments with which we are already more familiar. Inaccuracy in this setting is diminished as the number of repetitions is increased.

The next reading of A will be six times the required altitude, and so on.

511. To observe Angular Distance by the cross-observation. Proceed as directed above, reading distance for altitude.

512. If there is not light enough to read the finder, the reflected image must be actually carried across the other object by moving the index through twice the angle first measured.

513. The last pair completed being registered by the vernier A, the disturbing of B at any time is immaterial, since it does not affect the reading of A; but if A is moved, and the observation is interrupted before the new pair is completed, the whole is lost.

514. Two altitudes, of the same or different bodies, may be obtained by reading both verniers;* thus, set A to 720° , observe one alt. with B, as in No. 509. Unclamp A, move it to 0 on the finder, hold the circle in the other hand, and observe the other altitude.

Read off B, and subtract from it the constant angle: the remainder is the first alt. For the second alt. subtract the first alt. from A.

Ex. B $252^{\circ} 2'$; A $98^{\circ} 11'$; const. $213^{\circ} 35'$. The FIRST ALT. is $38^{\circ} 27'$; the SECOND is $59^{\circ} 44'$.

515. We shall now consider the effects of errors. The index-error is obviously removed by measuring the same angle, either on opposite sides of a fixed zero, or between any two points on the arc. Now, after B has been clamped, and the angle is to be repeated by moving A, the horizon-glass passes from one side of the perpendicular upon the central mirror through the same angle on the other side; the angle, therefore, is measured by the motion of A from one point of the arc to another, and the exact point 720° is assumed merely for convenience in reading.

When a coloured shade is defective, it breaks the direct course of the ray from the central mirror to the horizon-glass, and the broken part inclines towards the same side of the horizon-glass, whether the circle is inverted or not. Therefore, if the angle formed on one side of the perpendicular on the fixed mirror is too great, the angle formed on the other side will be too small, by the same quantity, and this error disappears.

The inclination of the line of sight upon the plane of the circle, No. 495 (3), produces the same effect upon the angle formed upon either side of the perpendicular to the central mirror; this error therefore remains.

The error of the eye, and therefore the personal equation (No. 175), likewise remains.

The error of centering is removed by carrying the angle round the whole circumference.

* This may be found convenient in taking a lunar at night, since the lamp would be required but three times for reading, in obtaining the four altitudes required and the several pairs of distances. Rules might easily be given for repeating both altitudes to any extent, but an allowance would be necessary for the motion in altitude of the second body observed.

[2.] *Dollond's Circle.*

516. Dollond's Circle consists of two concentric circles, the inner one of which, in revolving within the other, carries the horizon-glass and telescope, and a vernier called A, of which the clamp and tangent screw are attached near the telescope. The inner circle is cut to degrees only; the central mirror carries a vernier called B, as in a sextant.

The inner circle answers the purpose of the finder above described. From the position of the telescope, this circle is held, in taking altitudes, exactly like a sextant, which is a convenience. From the general resemblance between the two instruments, it is unnecessary to enter into further details.*

II. THE ARTIFICIAL HORIZON.

517. The Artificial Horizon is a small shallow trough, a few inches in length, containing quicksilver or any other fluid, the surface of which affords a reflected image of a celestial body. The fluid is protected from the disturbing effects of the air by a roof, of which the two opposite sides contain plate-glass. This roof is often made to fold up for the sake of portability. The trough should be so thick as to raise the quicksilver to a level with the lower edges of the glasses.

A piece of talc, which substance splits into thin parallel plates, may be laid on the trough as a substitute for the roof. In some cases a piece of thin cloth, as muslin, sufficiently transparent to allow a bright object to be seen through it, protects the fluid from the wind.

518. The image of a celestial object reflected from the surface of a fluid at rest appears as much below the true horizontal line as the object itself appears above it; the angular distance measured between the object and its image is therefore double the altitude. An advantage resulting from this is that in halving the angle shewn by the instrument we halve, at the same time, all the errors of observation. The reflected image in the fluid is always less bright than the object, but as it is perfectly formed, and as the surface is truly horizontal, the artificial horizon, when it can be employed, is always to be preferred to the sea-horizon.

* It is the opinion of some competent judges that circles should be made much smaller, for the sake of lightness and portability, and that they should accordingly be cut to minutes only, as Borda's Circle formerly was; because, by repetition, the minute or nearest half-minute read off is speedily reduced to quantities smaller than can be measured in the observation.

The case of a sextant, or circle, should be made to receive the instrument permanently with the index in any position, as the reading off, which is always difficult in defective light, might thus be deferred to a more favourable opportunity. It would also be useful for reference in cases of error or doubt in the reading, especially at night, to leave the index undisturbed till the result had been worked out.

When the altitude exceeds 60° , the altitude by reflection exceeding 120° falls without the limits of the sextant. In low latitudes, therefore, it is often impossible to observe with the quicksilver except by a sextant with additional powers.* On the other hand, when the altitude is low, the observer is obliged to increase his distance from the quicksilver, by which it becomes difficult to keep sight of the image reflected in the fluid; and for altitudes less than 12° or 15° the observation is generally impracticable.

519. The roof should generally be placed upon a sheet of some thin material, impervious to vapour, which, condensing on the glass, obscures the image. A leaden stand about the size of an octavo volume, on three legs, and covered with cloth, into which the roof sinks and excludes the external air, is convenient.

520. The film, or scum, which forms on the quicksilver, is prevented from running into the trough by holding the bottle inverted while it is poured out. A wooden scraper, fitting close to the inner breadth of the trough, has been found to remove the scum, which adheres to the wood.

521. The fluid proper for the purposes must possess the qualities of giving a bright image, and of quickly subsiding to a perfect level after being disturbed, such as quicksilver, water, spirit, and others.

An ingenious, handy, and portable mercurial horizon by the late Captain George, R.N., made by Cary, 181 Strand, is recommended. It consists of a disc of glass floating on mercury, in a vessel which it nearly fits, and it has an arrangement by which the mercury is introduced, ready filtered from an attached reservoir, and afterwards withdrawn, in a manner which saves a great deal of trouble. The glass floats without touching the sides of the trough, and the whole of the mercury below is serviceable. Another advantage is, that the edges of the trough cut off proportionally less of the field of view, hence very low altitudes may be observed with this instrument. The glass must necessarily be of the best workmanship.

When the air is calm, a piece of water, or a puddle large enough merely to exhibit the image, is often a complete substitute for the quicksilver.†

522. As the celestial bodies are sometimes distinctly visible when the sea-horizon is enveloped in mist,‡ attempts have been made to

* To remedy this defect, it has been proposed to use a reflecting surface, inclined at a constant angle to the horizon, movable on a level surface or floating in quicksilver. Also, a sextant has been fixed, with its plane vertical, to a pillar turning on an upright axis, and the telescope laid nearly horizontal by a spirit-level, the image of the body being brought down to a horizontal wire in the telescope.

† A small piece of plate-glass levelled by a bubble is sometimes used, but the performance of this instrument is not always satisfactory.

‡ Capt. Scoresby ("Journal of a Voyage to the Northern Whale Fishery," p. 159), remarks, that fogs often cover the sea in the polar regions to the depth only of 150 or 200 feet, while the sky is perfectly clear.

Her Majesty's sloop Zebra was a week without interruption in a dense fog, to the southward of the Snares, during the whole of which time no observation could be taken, though the sun often shone brightly (Naut. Mag. 1844). The like circumstances occur in "the Smokes," on the coast of Africa.

obtain an artificial horizon adapted to be used on board ship, by means of the surface of a viscid fluid, and a mirror attached to a pendulum, which, by its weight, hangs vertically.*

The objections to the first of these have already been stated. With regard to the motion of a pendulum, it is important to observe that when the ship comes to the end of her roll or lurch, it does not at once rest in the vertical position, but continues to move onwards, or to swing, with the velocity which it had before the ship's motion was destroyed; hence the pendulum moves through greater angles than the ship. By combining, however, the viscid fluid and the pendulum, Commander Becher has obtained a method of measuring altitudes at sea, independently of the horizon, which appears, from the reports made upon it, to afford sufficient accuracy for common purposes, when the motion of the ship is not very great.† Outside the horizon-glass of the sextant is a small pendulum, an inch and a half long, suspended in oil; to this is attached a horizontal arm, carrying at the inner end a slip of metal, the upper edge of which, when seen in a certain position, is the true horizon.

The error is determined by observation of a known altitude, or by the help of another sextant, and is the same for all altitudes. It should be frequently examined.

A lamp is attached for observing at night.

523. Admiral Beechey fitted, within the telescope of the sextant, a balance carrying a glass vane, one half of which is coloured blue, to represent the sea-horizon, and to which the celestial object is brought down. The amount of oscillation above and below the level is indicated by divisions on the glass, the values of which are determined by the maker.

The instructions for using this instrument are as follows:—Bring down the object, as the sun's limb, to the edge of the blue and leave it there. As the ship rolls, catch with the eye the upper and lower divisions reached by the object, and call them out to an assistant, who writes them down with the time against each. When two or more such readings have been taken, read off the alt. and write it down. Take the mean of the readings of the vane and turn it into arc according to the scale furnished. When the mean is *above* the edge, *add* it, when *below*, subtract it. Apply the maker's index-error; the result is the apparent alt. being clear of dip.

Ex. Took an alt., and readings as follows; the divisions 12' each:—

h m s			Divis.	} the blue edge		o ' "		
10	50	0	(+1) above		Observ. Alt.	20	25	20
50	30		(-1½) below		Mean of Div.		- 6	
50	50		(+1½) above			20	19	20
51	20		(-2) below		Maker's Ind. Corr.		- 40	
Mean 10 50 40 (-½), 2½ above, 3½ below; diff. 1 below; the half is ¼ of 12' or 6' to be sub.					App. Alt.	20	18	40

* It has also been attempted, but without success, to employ the principle upon which a top while spinning tends to preserve a vertical position, by balancing a horizontal mirror on a pivot, and causing it to revolve with great velocity.

† See Naut. Mag. 1844, p. 291. Several reports, with observations made by this instrument, will be found in the Naut. Mag. of 1839, 1842, 1844, &c.

Care is to be taken to observe as near the centre of the field as possible, and exactly under the sun; the elbow should rest on some firm support.

With practice the instrument affords considerable accuracy; and in smooth water the mean of some alts. will be within 2'.

A lamp illuminates the telescope at night.*

524. An instrument for this purpose, indispensable when the horizon cannot be seen, will also be of great service as a check, when haze or fog, by its partial distribution, produces the appearance of the horizon where it is not.† The same applies to the uncertainty in the place of the sea-horizon which is often experienced in moonlight nights.

These instruments are very convenient on shore.

III. THE CHRONOMETER.

525. The chronometer is a superior kind of watch, furnished with an apparatus by which the changes in the rate arising from the expansion or contraction of the materials by heat and cold are nearly obviated.

Chronometers should be kept near the centre of gravity of the ship, which is a little below the water-line, and not far from the middle of the length, not so much because the motion here is less than elsewhere, as because the temperature below is not liable to sudden changes. In ships in which great attention is paid to the chronometers, they are usually kept in a small apartment abaft the mainmast, on a table, in cases lined with cushions of soft wool, which defend them from the jerks and vibrations of the ship. The table is secured to a beam of the deck below, and in small vessels sometimes rests on a stanchion rising from the keelson. Large chronometers are placed in jimbals, in order to preserve a horizontal position, as inclining a watch from this position affects its rate. They have also been hung, perhaps with the view of obtaining both these objects together, in swing trays; but as this method is found to be very unfavourable, it has been discontinued.‡

The chronometer-table has been itself placed in jimbals. It has also been supported by springs to diminish still further the effect of shocks.

526. When a chronometer is placed on board it should always remain in the same position, that is, with the XII towards the same

* Made by Cary.

† Adm. Bayfield acquaints me that he has been completely deceived in the place of the horizon at the coming on of a fog.

‡ Mr. Fisher acquaints me that he has found an acceleration of seven seconds a-day produced by suspending a chronometer in a cot with five inches' swing.

part of the ship, since it has been found that disturbing the positions has altered their rates.*

When a chronometer is transported from one place to another, it should be compared, before and after moving, with another chronometer or a good watch, in order to ascertain whether its regularity has been disturbed.

527. A chronometer should be wound up at regular intervals, in order that the same parts of the machine may undergo the same constant action; it should, therefore, be wound up at the same hour every day. In winding, the key should be turned steadily, and about half a turn taken each time, and the watch should be wound close up. After winding, the chronometer should be examined, to ascertain that it has not stopped.

In winding up a watch, the key alone should be moved, as to turn the watch itself is to increase the velocity of winding.

When a chronometer is wound up after running down, it is set a-going by giving it a small horizontal circular motion.

When a chronometer stops, it generally alters its rate.

528. It seems generally admitted that the principal cause of the variation of the rates of chronometers is change of temperature,† and accordingly, in some ships, the temperature of the chronometer-room has been regulated by lamps.

When the ship changes her climate, the rates do not change at the same time with the temperature, but some time afterwards.‡

529. It has been found that magnetism affects the rates of chronometers (see a paper by Mr. Fisher. *Nautical Magazine*, 1837). Hence it follows, that the magnetism of an iron vessel may produce similar effects. Their rates will certainly be affected by the proximity of apparatus generating or conveying electric currents.

530. Chronometers are generally found to perform best at the

* This depends, however, chiefly on the position of the arm of the balance.

† Captain R. Owen, while employed in surveying in the West Indies, found a fall of 14° in Fahrenheit's thermometer (from 82° to 68°) accelerated the rates $1^{\text{h}} 5$ a-day, and a fall of 20° (from 82° to 62°) accelerated them two seconds a-day.

‡ Admiral Fitzroy, who employed in his surveys of South America the unusual number of twenty-two chronometers, observes, that the ordinary motions to which chronometers are subjected, both from the incessant action of the sea and in transferring them from one vessel to another, scarcely affect the rates of good watches; and that, in general, temperature is the only cause of the alteration of rate. (*Journal of the Royal Geographical Society*, vol. vi.)

Sir E. Belcher, however, when engaged in the survey of the west coasts of North America, found the chronometers of H.M.S. *Sulphur* very materially deranged by the jerking produced by a looseness about the rudder-head and from towing the *Starling*, her tender; and observes, that when these causes were removed the watches performed admirably.

In the *Instruction Réglementaire pour les Bâtiments de la Marine Royale, &c.* (*Annales Maritimes*, 1840), it is recommended that the chronometers should be held in the hand during the firing of guns, and that in transporting a watch from one place to another it should be carried in both hands, in order to avoid giving it suddenly a circular motion, which may be communicated by taking it up by a handle, or becket, at the top of the case.

M. Givry considers that the rates of the chronometers of *La Coquille* frigate, commanded by M. Duperrey on a scientific expedition, were altered by the severe thunder-storms experienced on the coast of Timor, in August 1823.—*Mémoire sur l'Emploi des Chronomètres à la Mer*, par A. P. Givry, extracted from the *Annales Maritimes*, Paris, 1840.

It has been surmised that the hot and moist climate of the coast of Africa has speedily disturbed the rates of chronometers; but Adm. Vidal and Sir E. Belcher, in several years' experience, have recognised no such effect.

beginning of a voyage;* many subsequently become useless from irregularity, and some fail altogether. They are liable, also, to change their rates suddenly, and then to reassume the former rates in a few days.†

531. Since there seems no reason why any cause which alters the rate of one chronometer should not alter the rate of another in the same manner, the agreement of any number of chronometers, however great, cannot be unreservedly admitted as evidence for the truth of the time which they shew. Their irregularities, however, in this respect contribute to the security of navigation; for since one chronometer often gains while another, under exactly the same circumstances, loses, the discrepancies prevent the danger of trusting too confidently to any single result.

CHAPTER III.

TAKING OBSERVATIONS.

- I. OBSERVING ALTITUDES. II. OBSERVATIONS WITH AND WITHOUT ASSISTANTS. III. EMPLOYMENT OF THE HACK WATCH. IV. FINDING THE STARS.

532. In treating of observations with reflecting instruments we shall refer chiefly to altitudes, as most convenient for the purposes of illustration. If, however, for the *horizon*, we substitute a celestial body or any other point, what is said of altitudes will apply, with certain obvious exceptions, to angular distance generally. The details proper to the particular observations will be found under their respective heads.

I. OBSERVING ALTITUDES.

533. The observer will do well to accustom himself to obtain a single sight with accuracy, and not to depend upon the accidental compensation of errors due to want of care. It sometimes happens that a single sight only can be obtained, and no good estimate of its

* Advantage was taken of this circumstance in the late survey of part of the west coast of Africa by Admiral Vidal, who, by direction of the Hydrographer, proceeded at once to run down the coast from Sierra Leone to Corisco Bay, and returned to Sierra Leone as quickly as possible. The whole Diff. Long. between these points, as measured in both runs, agreed within 1".

† Captain R. Owen remarks, that most of his chronometers took thus a jump of one or two seconds in the daily rate, more than once during his surveys in the West Indies. Other officers have made similar remarks.

value can obviously be formed if the observer knows his observations by their general result only.

1. *At Sea.*

[1.] *Above the Sea Horizon.*

534. The instrument must be vibrated or swung, so that the image may skim the horizon, for the altitude must be measured to the point vertically under the body,* No. 487.

535. When the altitude is above 60° , it may be observed both from the opposite point of the horizon and from that under it, by the common sextant. Half the difference of the two readings is the apparent zen. dist., No. 432. By this means the dip, with the uncertainty to which it is liable, and the index error, are removed. As the apparent dip is always uncertain, and as the rules given in No. 208, though generally true, do not always hold good for small differences of temperature, it will be advisable, whenever precision is required, to attend to this consideration.

536. It is, in general, taken for granted that the dip is in the same state all round the horizon.

This supposition M. Arago, in discussing the observations made by Sir E. Parry in his first polar voyage, by Capt. B. Hall in the China Sea. and by M. Gauttier in the Mediterranean and Black Seas, thinks there is no reason to doubt. (*"Conn. des Tems,"* 1827.)

Capt. Fitzroy found however a difference of $16'$ on one occasion; and Capt. Bayfield informs me that he has often observed the dip not to be the same all round the horizon, more particularly on the coast of Labrador and in the Straits of Belleisle, where currents of unequal temperature prevail. See also note *, p. 196.

When circumstances allow, alts. should accordingly be observed at opposite points of the horizon. The mean of two alts. in such cases may not, indeed, be exactly true, but it is probably nearer the truth than one of them alone might be. For the same reason it is advisable to select stars on opposite bearings.

When both the alt. and its supplement are thus measured, and the alt. is in a state of change (as will always be the case except when the object is on the meridian), the time must be noted at each of the two contacts; and the half difference of the alt. and its suppl. is the apparent zenith distance of the centre corresponding to the mean of the times.

When the altitude is below 60° a sextant of additional powers, or a circle, is in general necessary for this observation. (See No. 504.)

537. When the altitude of a body is near 90° , it is proper, before attempting to bring down the reflected image, to ascertain, by re-

* When the 4th Adjustment. No. 495 (3), is not perfect, we look at a point of the horizon not directly under the sun. Hence a tube should be used to insure the eye and the contact of the images being at equal distances from the plane of the instrument. On the same ground, Dr. Maskelyne recommends the observer, when without a tube, to turn on his head while causing the image to skim the horizon. (*Nautical Almanac*, 1774.)

ference to the zenith, or the compass, the precise point over which the body is vertical.

538. When fog obscures the sea-horizon from the deck, a new horizon may often be obtained by descending the ship's side, or from a boat. See No. 550, note.

539. When the limbs of the sun or moon are indistinct, altitudes of the centre are obtained by bisecting the hazy or cloudy disc upon the horizon.*

540. In observing the moon's altitude there is a choice of the upper or lower limb when she is at the full, and also when the line of cusps, or horns, is vertical. At other times her illuminated limb, whether it be the upper or lower one, must be brought down to the horizon.

Mistakes may arise in observing the moon's altitude at sea by night. When the sky under the moon is unclouded, the upper edge of the illuminated part of the sea is the horizon; but at other times long dark shadows are projected on the water, which render it difficult, and sometimes impossible, to discern the horizon.

When the moon's alt. and its supplement are both measured, if she is full, or if the line of cusps is vertical, her alt. may be observed as directed in No. 535. But in other cases the same limb must be referred to the point of the horizon under her and to that opposite; half the difference is then the app. zen. dist. of the limb observed, and the semidiameter must be applied accordingly.

When the horizon under the moon is unfavourable for observation, and the supplement of the alt. alone is employed, correct the angle observed for index-error and dip, take the suppl. of the result to 180° , and apply the semidiameter as to the alt. taken directly.

541. The obscurity of the sea-horizon in a dark night renders it difficult to observe the altitudes of stars or planets; but in the twilight, when the sky is clear, the boundary of the sea exhibits a strong dark edge, most favourable for observation.

The difficulty of reading off at night is easily overcome by having a well-trimmed dark lanthorn, and a handy assistant.†

When the alt. of a star or a planet is measured both from the horizon under it and opposite to it, half the diff. of the two angles is the app. zen. dist. If the supplementary arc alone is employed, correct it for index-error and dip; the supplement of the result is the apparent altitude.

542. When a telescope is used the unemployed eye must be closed, but when the plain tube is used it should, when convenient, be kept open, because the image being seen by both eyes under the same magnitude, one assists the other.

This should be practised in observing stars at night.

La Caille recommends keeping the eye some minutes in complete

* Mr. Fisher tells me that he has repeatedly employed, with complete success, altitudes of the sun faintly seen through watery clouds, when those who had been used to depend solely upon the perfectly defined disc had despaired of an observation altogether. In such cases the altitudes have not greatly differed from each other, and the mean of several has been quite equal to an ordinary observation of the limb.

† A small electric light (half candle power) is found useful.

darkness before observing stars at night. (Guépratte, "Problèmes d'Astron. Naut." &c., tom. i. p. 20, 1839.)

543. Different powers suit different eyes. Too low a power does not magnify enough; too high a one makes it difficult to keep the object in the field on the least motion of the instrument. The observer, therefore, will employ those powers only in which the advantage gained by a larger image exceeds the disadvantage of increased unsteadiness.

A plain tube, however, should be used in all other cases, both for directing the sight to the proper point of observation, and for defence against disturbing lights.

544. All observed angles are vitiated by the errors of the instrument enumerated in the last Chapter, Nos. 495, 498, and 499. Again, each observer has in general some peculiarity in the manner of observing, or in the quality of the eye itself, which gives rise to a *personal* error, the correction for which is called the *personal equation*. No. 175.

545. Besides these errors, altitudes taken at sea are subject also to others which change with circumstances.

1st. The running of the waves causes the horizon to be in continual motion; 2d. The rise and fall of the observer, both from the lifting of the vessel by the waves, and by her rolling, cause the dip to be in continual change.

The effects of these alternating motions will, in taking two or three altitudes, in part disappear.

3d. The place of the visible horizon changes with the temperature of the sea and the air. See No. 208.* Also, since the sea-horizon is formed by the eminences of the waves, it should be higher in bad weather.†

Besides these distinct causes of error, the motion of the ship disturbs the attention and efforts of the observer.

546. The height of the eye should be ascertained with some precision, that is, within two or three feet, because an error in the dip causes an error of the same amount in the altitude. This is of most importance when the observer is very near the water, as the dip then changes most rapidly; thus, it appears in Table 30, that a change of three feet in the height produces, near the beginning of the table, a change of more than 1' in the dip, but near the end only

* M. Givry observes ("Mémoire sur l'Emploi des Chronomètres," p. 23), that when the sea is shoal near the horizon, the relation of the temperatures of the sea and the air being different from that at places where the water is deeper, may produce extraordinary refraction: and he attributes to this cause errors amounting to 8" in the time deduced from some altitudes taken near the mouth of the Jéba, in 1818, although circumstances appeared at the time in every respect favourable for observation.

M. Givry remarks, further, that extraordinary refraction sometimes takes place in the neighbourhood of sandy plains, the heated air of which, passing over the sea, produces partial inequalities of temperature; and he adds, that small undulations in the horizon are always indicative of irregular refraction.

† It is stated, "Voyage autour du Monde," 1840, by M. Du Petit Thouars, in the *Vénus* French frigate, that the observations shewed this. It is probable, however, that the errors of observation due to the motion would, in general, far exceed that due to the above cause.

4". An altitude observed at the top of a heavy sea will differ considerably from another taken at or below the mean level.*

If the altitude be observed above the deck, as in the top for instance, the horizon will appear better defined, and the variations of the dip by the ship's motion will be less sensible; also the difference of temperature of the sea and the air appears to affect the place of the visible horizon less as the observer is more elevated. Hence it would appear that altitudes should be taken from aloft when convenient.

547. Some observations on the heights, distances, and velocities of waves have been put on record of late years. Sir G. Grey,† in his voyage home from Australia in 1837-8, obtained numerous measures of the distance and velocity of waves, amongst which are the following:—

Dist. 121 ft.	Vel. 14½	Naut. miles.	Dist. 211 ft.	Vel. 19½ miles.
178	18·7		234	20·5
201	22·5		326	22
205	20·6		338	28

Lieut. Wilkes ("U.S. Exploring Expedition") found the highest waves in a heavy sea off Madeira from 14 to 25 feet high, and their velocity 23 miles an hour; and at another time and place, with a remarkably high and regular sea, 32 feet, with a velocity of 26 miles.

The highest waves observed by Sir Jas. C. Ross, in the North Atlantic, were 36 feet high. The highest sea seen by M. Lazarev, in the Russian Expedition of Admiral Bellingshausen, 1819, was in 56° S. and 103° E., but he does not state the height.

In the Naut. Mag. 1848, p. 228, are the following observations taken near the Cape of Good Hope:—

Height 17 f.	Dist. 35 fath.	Vel. 22 miles.
20	43 to 50	24
22	55 to 57	26 to 27

548. When the spectator nears or recedes from the celestial body, by the progress of the ship, the effect produced on the altitude is the same as that of a motion in the body itself, since exactly the same appearances result from the motion of either while the other remains fixed. Accordingly, in all observations, in which, from the sensible change of altitude, the time requires to be noted at each sight, the progress of the ship is included in the observed change of altitude; and the *place* to which the observation corresponds is that at which the ship was at the mean of the times.

* The height of waves is ascertained by placing one's self at such a height on the vessel, or her rigging, that the tops of the highest waves which pass near the ship may be seen on with the distant well-defined horizon, at the instant when the ship is at the bottom of the hollow between two heavy seas. The height of a wave thus observed, that is, the difference of level between the summit and the bottom of the hollow (which difference is *twice* the height of the summit above the *mean level*), is very nearly the height of the eye above the bottom of the same hollow, the ship at the instant of observation being upright. The distance is measured, when before the wind, by a line with marks on it.

† Governor of New Zealand. I am indebted to the author for these observations, of which I had a few only reduced for the course and rate of sailing of the ship.

[2.] *Altitudes above the Shore Horizon.*

549. It often happens that the horizon is concealed by the intervention of land, while the level surface of the water marks on the shore a distinct horizontal line, which is a substitute for the sea-horizon, and is called a *shore-horizon*.

When the distance of the shore-horizon is known, enter Table 35 with this distance and the height of the eye, and use the correction therein instead of the dip in Table 30.

Ex. From the height 20 feet, observed
merid. alt. $28^{\circ} 18'$, above a shore-horizon,
2 miles and a quarter distant.

Alt.	$28^{\circ} 18'$
Corr.	$- 7$
Alt. corrected for dip	$28^{\circ} 11'$

550. When the distance of the shore-horizon, or water-line, is not correctly known, it may be found by means of two altitudes, the one being observed from the deck, and the other as high as possible, at the same time.

Divide the difference of the heights in feet by the number of minutes in the diff. of alts.; the quotient is the number of feet subtending an angle of $1'$ at that distance. Look in Table 9 for this number of feet, and the corresponding distance is the distance required.

Ex. An observer, at the height of 91 feet above the sea, observed the sun's alt. $41^{\circ} 37'$ above the water-line of the sea; another observer, at the height of 22 feet, observed it $41^{\circ} 25'$ and the distance of the water-line, and correct the alt. for dip.

The diff. of the heights, 69 feet, divided by 12 (the minutes in the diff. of alts.), gives 5.7 feet, which answers, in Table 9, to 3 miles, the Dist. required. Then the cor. in Table 35 to 3 miles, and height 22 feet, is $5'$, which subtracted from the alt. taken at 22 feet, gives $41^{\circ} 20'$, the ALT. CORRECTED FOR DIP.

But as this result, like the preceding, becomes uncertain when the distance is very small, it is always advisable in such cases to endeavour to find, by descending, a natural horizon.*

2. *Observing Altitudes on Shore.*

551. Altitudes are well observed above the sea-horizon from a hill or cliff of known height. Nos. 544, &c. apply, with certain obvious exceptions, to altitudes of this kind taken on shore.

552. In taking the altitude of the *lower* limb in the quicksilver, the *lower* limb of the object is made to touch the *upper* limb of the image in the quicksilver, as reflection inverts the object. In taking the altitude of the *upper* limb, the image of the body is in like manner brought below the quicksilver image altogether. Hence, when the sun is *rising*, and the *lower* limb is observed, the images are continually *separating*; but when the upper limb is observed, they are continually *overlapping*; and the contrary when the sun is falling.

It is useful to attend to this, as it is sometimes doubtful, especially with the inverting telescope, which limb was observed.

* This is the practice recommended, on his own experience by Dr. Scoresby, "Voyage to the Northern Whale Fishery. 1822, London," p. 441.

553. It is advisable, when circumstances permit, to move the index a little too much, whether forwards or backwards, and clamping it, to wait the instant of contact while the instrument is in a state of repose, in preference to making the contact by moving the tangent screw up to the instant of observation, because the material always springs more or less. Again, moving the tangent screw diverts a portion of the attention which should be devoted to the contact alone. At sea this is rarely practicable in any observation on account of the motion of the ship.

554. The roof of the quicksilver should be reversed at each set of three or five altitudes, in order to remove the effects of errors in the glasses; one face is accordingly marked A and the other B, and these letters marked against the altitudes.

The roof should obviously be used only when it cannot be dispensed with.

555. A stand for the sextant or circle, on shore, is a great convenience, and allows a higher power to be used; practice is, however, necessary, in order to derive the full advantage from it.

556. The accuracy with which a set of altitudes has been observed may, in part, be inferred from their agreement with each other. For since the change of altitude in small intervals of time is nearly proportional to the intervals (unless the object is near the meridian), any considerable irregularity must be a consequence of an error of observation.

The comparison of the differences of altitude, with their respective intervals, may easily be made by means of the Traverse Table, as in the following example:—

Ex. Observed altitudes of Arcturus in the artificial horizon.

Time	10^h	5^m	43^s	Diff.	Alt.	78°	$59'$	$20''$	Diff.
	10	8	17	$2^m 34^s$		78	14	30	45'
	10	11	29	3 12		77	17	30	57
	10	14	20	3 51		76	33	40	44

In Table 2, $2^m 34^s$, or 154^s , as D. Lat., corresponds to 44 as Dep. at 16° . On the same page $3^m 12^s$, or 192^s , as D. Lat., corresponds to 55 as Dep., which is near enough. $2^m 51^s$, or 171^s , as D. Lat., corresponds to Dep. 49, the Diff. 44' is therefore in error, and the 3d alt. about 5' too great.

557. Several altitudes are taken in immediate succession, on the supposition that they are liable to errors of opposite kinds; for, in this case, if one altitude be observed a little too great, and another a little too small, the mean of the two will be nearer the truth than either of them separately; and thus, by increasing their number, the effects of irregularities of observation will be much diminished in the general result.

558. But if the portion of time during which the altitudes are taken be too long, an error of a new kind will arise from the unequal variation of the altitude itself, which never, strictly speaking, varies at the *same rate* at the beginning, middle, and end of an interval.

If a series of alts., at observed equal intervals of time, be cleared of errors, and the differences between them be taken in succes-

sion, these differences will generally afford, in like manner, differences among themselves, which are called *second differences*; and if the observations be prolonged, third differences will appear, and so on. When the 2d diff. is insensible, $\frac{1}{2}$ the sum of 2 alts., or $\frac{1}{3}$ the sum of 3 alts., or $\frac{1}{4}$ the sum of 5 alts., corresponds exactly to the middle of the time occupied in the observation; but when the 2d diff. is considerable, the arithmetical mean is in error by a quantity which is as follows:—

The half sum of two alts. at the beginning and end of the interval differ from the alt. proper to the middle instant of the interval by $\frac{1}{2}$ of the 2d diff. proper to the whole interval. The third of the sum of the three alts. at the beginning, middle, and end of the interval, differs from the same alt. by $\frac{1}{3}$ of the whole 2d diff.; and the fifth of the sum of 5 alts. at four equal intervals, by $\frac{1}{5}$ of the 2d diff.

Ex. Lat. $51^{\circ} 30' N.$ Decl. $22^{\circ} 20' N.$

	Hour-Angles.	Alts.	Diff.	2d Diff.
1st.	$0^h 16^m 0^s$	$60^{\circ} 40' 8''$	$5 \ 33''$	
2d.	$0 \ 20 \ 0$	$60 \ 34 \ 35$	$6 \ 43$	$1' \ 10''$
3d.	$0 \ 24 \ 0$	$60 \ 27 \ 52$	$7 \ 54$	$1 \ 11$
4th.	$0 \ 28 \ 0$	$60 \ 19 \ 58$	$9 \ 6$	$1 \ 12$
5th.	$0 \ 32 \ 0$	$60 \ 10 \ 52$		

The mean 2d Diff. is $1' 11''$ for 4^m ; hence, as the 2d Diff. varies as the square of the interval (that is, is 4 times greater when the interval is doubled, 9 times greater when it is trebled, and so on), the whole 2d Diff. for 16^m is 4 times 4, or 16 times $1' 11''$, which is $18' 56''$. Then the mean of the 1st and 5th Alts. is $60^{\circ} 25' 30''$, which differs from the 3d Alt. by $2' 22''$, or $\frac{1}{8}$ th of $18' 56''$.

The mean of the 1st, 3d, and 5th Alts. is $60^{\circ} 26' 18''$, which differs from the 3d by $1' 35''$, or $\frac{1}{12}$ th of $18' 56''$.

The mean of the 5 Alts. is $60^{\circ} 26' 41''$, which differs from the 3d by $1' 11''$, or $\frac{1}{16}$ th of $18' 56''$.

The error cannot be materially diminished by further increasing the number of alts.

The correction for this error cannot be given in a concise and convenient form.* But in practice the intervals are not exactly equal; and even if they should be, the errors of observation will often conceal the 2d diff. When, therefore, from circumstances, altitudes can be obtained only at considerable intervals, it is proper to deduce a separate result from each.

The 2d diff. of alt. disappears in two cases: 1st, when the object is E. or W.; 2d, when its motion is vertical.

559. The effect of the elevation of the spectator upon the altitude observed in the quicksilver, is insensible in practice, since, even in the case of the moon, an elevation of a mile does not produce a change of $1''$ in her horizontal parallax.

* The change of altitude in a very small portion of time depends on the latitude, and on the azimuth of the object (see No. 669); but the 2d Diff., or *variation* of the change of alt., which becomes conspicuous in a longer interval, depends, further, upon the altitude itself. To exhibit this correction, therefore, a table of *treble entry* would be required.

II. OBSERVATIONS WITH AND WITHOUT ASSISTANTS.

560. When the arc observed is in a state of continual change, the quantity measured corresponds to a particular instant of time. When, therefore, the complete observation consists of various elements whose measures are required at the same instant, either the observer must have assistance, or he must himself obtain the several measures in succession, and these must be reduced afterwards to the same instant by calculation.

When two or more altitudes at sea are required at the same instant, assistants have been employed to observe them. The impropriety of this custom will, however, appear on considering the nature of the errors of altitude (No. 545); for it is obviously impossible for an observer to keep the motion of the index so exactly adjusted to the irregular and often violent motion of the ship, as to be able to seize the altitude at command.

561. The assistant is useful chiefly in noting the time. An observation of a set of altitudes, with their times, for example, is conducted as follows:—

(1.) The observer sets the index to the estimated alt. (No. 492); about $\frac{1}{2}$ of a minute before he expects to complete the contact, he cries, "Look out!" at the instant of contact, he cries, "Stop!" on which the assistant writes down the second, the minute, and the hour. The observer then reads off the degree, minute, and division of the seconds, as $10''$, $20''$, $30''$, &c., which the assistant writes down. Three, five, or more altitudes make, generally, a set of *sights*.

When the assistants have watches shewing seconds, each takes his altitudes at leisure, and the whole is reduced to the same instant by calculation.

(2.) The times are then added together, and the sum divided by the number of alts. The alts. are then in like manner added together, and the sum divided by their number is, when the second difference is not considerable (No. 558), the alt. corresponding to the mean of the times. When the number of alts. is odd, and the intervals are nearly equal, the means will not differ much from the middle time and its corresponding altitude.

562. When two sets of observations are taken by different persons, nearly at the same time, they are reduced to the same instant thus:—

The difference or change of altitude (or other angular measure) in the time occupied by the observation is given; then the interval between the given mean of the times, and that to which it is proposed to reduce the observation, being found, the quantity to be applied to the altitude is determined by proportion. For accuracy, the change of alt. must be properly computed by No. 669 or 671.

563. The observer should, however, take the whole observation himself, and he will then learn to estimate his results at their real

value, of which he can be no judge when they are taken by other persons.

When the observer takes his own time, he holds his watch in his hand, or places it either where he can obtain sight of it readily, or where he can hear it tick plainly. In the latter case, the first beat after the instant of contact he counts 1, the next 2, &c.; then, looking at the watch, he counts on till the second hand arrives at a marked number of seconds, as 10, 15, &c.; he then writes down these seconds, and after them the number of beats counted, to be *subtracted*.

If the observer can count 10 or 20 seconds without an error of more than 1^s or 2^s, he may put the watch wherever it is most convenient to inspect the face, and thus avoid the principal difficulty in taking the entire observation himself, especially at night.

He then reads off the alt., and sets it down.

The sum of the beats is to be deducted before the mean of the times is taken.

Most watches beat 5 times in 2^s, or each beat counts 0^s.4.

Ex. After the instant of contact, 14 beats are counted; the second-hand is then at 30^s, the min. 42, and the hour 10, and so on, as follows:—

10 ^h 42 ^m 30 ^s	subtract	14 beats.
10 44 10		32
10 46 0		11
132 40		57
— 22.8	(corres. to	57 beats.)
3) 132 17.2		
Mean 10 44 5.7		

III. EMPLOYMENT OF THE HACK WATCH.

564. This is a portable chronometer, or good watch, used for observation, to save moving the standard chronometer. Since the watch and chronometer will not in general go exactly together, they must be compared both before and after observation, in order to find what time the chronometer shewed when the observation was taken. Thus,

Within 5 or 10 seconds of a whole minute by the watch the observer tells the assistant to “look out” on the chronometer. At the minute he cries “Stop!” when the assistant writes the times, and takes their differences. This should be repeated two or three times, and the mean result employed. The observer can compare alone, by counting the beats of the chronometer till the expiration of the minute.

If the difference between the watch and the chronometer be the same before and after observation, the time of observation by the chronometer is at once deduced from that by the watch; if not, a correction must be applied, as in the following example:—

	Before Obs.		After Obs.		Intervals.
Watch	3 ^h 1 ^m 0 ^s		4 ^h 3 ^m 0 ^s		0 ^h 52 ^m 0 ^s
Chron.	10 31 18.4		11 23 21.7		0 52 3.3
Diff.	7 20 18.4		7 20 21.7		3.3

Time of observation by watch, 3^h 32^m 37^s: required the time of do. by chron.

The watch here has *lost* 3^m 3 on the chron. in 52^m. The observation taking place 21^m 37^s by watch, after the first comparison, we have 52^m : 3^m 3 :: 21^m 37^s : 1^m 4, the *loss* of the watch on the chron. at the time of observ.; this, *added* to 21^m 37^s, gives 21^m 38^s 4, which, add'd to 10^h 31^m 18^s 4, gives 10^h 52^m 56^s 8, the TIME BY CHRON. required.

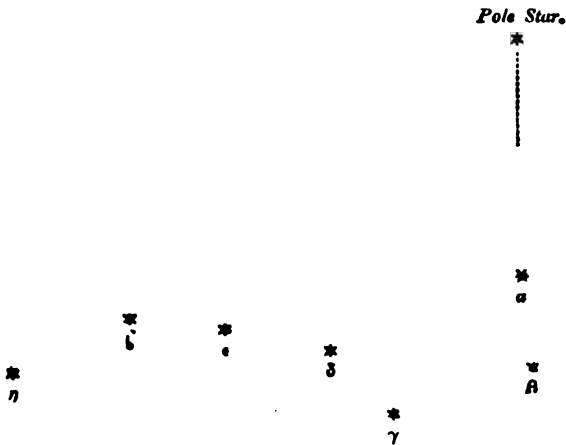
565. When the times by watch are separated by considerable intervals, and the rate of the watch is large, each time may require to be thus corrected for its proper gain or loss.

IV. FINDING THE STARS.

566. The most conspicuous stars have been designated, from remote antiquity, by names; besides which, the stars in each constellation or group are distinguished, for reference, by letters and numbers. The letters chiefly used for this purpose are the small letters of the Greek alphabet, which, with their names, are written as follows:—

α alpha	ζ zeta	λ lambda	π pi	φ phi
β beta	η eta	μ mu	ρ ro	χ ki
γ gamma	θ theta	ν nu	σ sigma	ψ psi
δ delta	ι iota	ξ ksi	τ tau	ω omega
ε epsilon	κ kappa	ο omicron	υ upilon	

567. In finding any star in the heavens, it is necessary to refer to some one star or constellation as known: the Great Bear, called also by the Latin name *Ursa Major*, a constellation of the figure shewn below, in the northern part of the heavens, and consisting of seven principal stars, is the most convenient for the purpose.



The two stars α and β point nearly to the POLE STAR (or *Polaris*), and are hence called the Pointers. This star will not easily be mistaken, as it appears always in the same place.

A line from *Polaris* through η (the last of the tail) passes, at 31° beyond η , through ARCTURUS, one of the brightest stars.

A line drawn from *Polaris* perpendicular to the line of the Pointers, and on the opposite side to the Great Bear, passes, at 48° distance, through CAPELLA, one of the brightest stars.

In this same line, about the same distance on the opposite side of the pole, is α *Lyræ*, or the bright star in the Harp, called also *Vega*, and also by seamen *Lyra*, a large white star.

At one-third of the distance from Arcturus to α *Lyræ* is ALPHACCA, the brightest of a semicircular group called the Northern Crown (*Corona Borealis*).

A line drawn from δ (the faintest of the Great Bear) through *Polaris*, passes through the constellation of *Cassiopeia*.

About 23° to the eastward of α *Lyræ*, and about the same distance as this star from *Polaris*, is the bright star in the Swan (or α *Cygni*). DENEK.

A line from *Polaris* passing between this last and α *Lyræ*, produced to an equal distance beyond them, passes through ALTAIR (α *Aquilæ*), a bright star between two small ones, the three lying in the direction of α *Lyræ*.

The line of the Pointers, carried through the pole to about 62° beyond it, passes through β *Pegasi*, called also SCHEAT, and about 13° further, through MARZAB (α *Pegasi*).

A line from *Polaris*, drawn between Capella and a star near it to the eastward, passes to the westward of the constellation Orion. The two northern stars of the four at the corners are the shoulders, the northernmost of which is BETELGEUSE, or α *Orionis*. The brightest of the two southern stars, the feet, is called RIGEL. In the middle are three small stars forming the belt, the northernmost of which is nearly on the equator.

About 25° to the northwestward of the belt, and not far out of the direction in which it points, are the *Hyades* and *Pleiades* in *Taurus*; in the former cluster lies the red star ALDEBARAN.

A line from Aldebaran through the belt passes, at about 20° on the other side, through SIRIUS, the brightest of the stars.

Sirius, the eastern shoulder, and PROCYON (to the northward of *Sirius* and eastward of Orion), form an equilateral triangle.

Nearly midway between Orion and the Great Bear are the Twins, CASTOR and POLLUX (the southern and brightest), about 4° apart. The line from *Polaris* to *Procyon* passes between them.

A line from *Rigel* through *Procyon* passes, at an equal distance beyond, to the northward of REGULUS. δ and γ *Urs. Maj.* serve as pointers for *Regulus*.

A line drawn from *Procyon* through *Regulus*, at nearly an equal distance beyond it, passes through β *Leonis*, or DENEbola.

A line from δ *Urs. Maj.* through *Regulus*, passes, at $30'$ beyond, through COR HYDRÆ.

A line from *Polaris* through ζ *Urs. Maj.* passes, at 70° distance, through SPICA VIRGINIS.

A line from the last star in the tail of the Great Bear through ARCTURUS will lead to α and β *Libræ*.

Arcturus, *Spica*, and *Denebola* form an equilateral triangle.

A line from *Regulus* through *Spica* passes, at 45° distance, through ANTARES, a very bright and reddish star.

A line from α *Orionis* (*Betelquese*) through *Aldebaran* passes, at 30° distance, through α *ARIETIS*, not a very distinct star.

The Southern Cross is about as far from the South Pole as the Great Bear is from the North Pole; α is the foot, and γ the head.

To the left of the Cross when on the meridian and pointing towards it are α and β *Centauri*, both of the first magnitude.

A line from *Scheat* through *Markab* passes, at 45° from *Markab*, through FOMALHAUT, a very bright star.

Scheat and α *ANDROMEDÆ*, called also *Alpheratz*, form the north side of a square; *Markab* and ALGENIB on the south side.

ACHERNAR, *Fomalhaut*, and CANOPUS, are in a line, and nearly equidistant, being about 40° apart.

568. When a few stars are known, the rest are easily found by the times of their Meridian Passages, Table 27, and their Declinations, Table 63, as described in No. 482 (8).

A star may also occasionally be identified by means of its altitude, or azimuth, computed roughly.

CHAPTER IV.

SUBORDINATE COMPUTATIONS.

- I. THE GREENWICH DATE. II. REDUCTION OF THE ELEMENTS IN THE NAUTICAL ALMANAC. III. CONVERSION OF TIMES. IV. HOUR-ANGLES. V. TIMES OF CERTAIN PHENOMENA. VI. ALTITUDES. VII. AZIMUTHS.

569. Such parts of computations as are common to more operations than one are collected, both to avoid repetition and for facility of reference, in this chapter, which contains also some smaller computations not relating directly to the principal divisions of the subject.*

* Certain computations in this chapter, though not of immediate application in the present volume, may be found useful for the purposes of verification.

I. THE GREENWICH DATE.*

1. *Conversion of Arc and Time.*

570. To turn Degrees and Minutes into Time.

By Inspection.—(1.) To the whole second. Enter Table 68 or 69 with the given arc, and take out the hour, minute, and second.

Table 68 shews the time to the nearest two seconds.

(2.) To parts of seconds. Take out of Table 17 the hours, minutes, seconds, and parts corresponding to the given degree, min., and sec.

Ex. 1. Turn $36^{\circ} 11'$ into Time.

In Table 68, or 69, $36^{\circ} 11'$ is seen to be $2^h 24^m 44^s$ in TIME.

Ex. 2. Turn $101^{\circ} 41' 45''$ into Time.

Ans. by Table 69, $6^h 46^m 47^s$ in TIME.

Ex. 3. Turn $134^{\circ} 52' 9'' \cdot 7$ into Time.

In Table 17, 130° ,	$8^h 40^m 0^s$
4	16
52'	3 28
9"	0 6
0'7	05
TIME required	8 59 28'65

571. *By Computation.*—Multiply the arc by 4; this turns the degrees into minutes of time, the minutes (') into seconds of time, and the seconds (") into thirds of time.†

Ex. $36^{\circ} 11'$ multiplied by 4, is $144^m 44^s$, or $2^h 24^m 44^s$ in TIME.

572. To turn Time into Degrees, Minutes, and Seconds of Arc.

By Inspection.—(1.) To the nearest second or two seconds. Employ Table 68 or 69.

(2.) To parts of seconds. Take out of Table 18 the deg., min., and sec. corresponding to the hours, mins., and secs. of time.

573. *By Computation.*—Turn the hours into minutes, and divide by 4; the quotient is the deg., min., and sec.

Ex. 1. $2^h 24^m 44^s$ are $144^m 44^s$, which, divided by 4, gives $36^{\circ} 11'$ in Arc.

Ex. 2. $5^h 20^m$ are 320^m , which divided by 4 gives 80° in Arc.

2. *Deduction of the Greenwich Date.*

574. The Civil Date begins at midnight, No. 480; the Astronomical Date begins at noon: thus the civil date Oct. 1st, 3 P.M., is the astronomical date Oct. 1st, 3^h; but 11 A.M. on this day, civil date, is the astronomical date Sept. 30th, 23^h.

In most cases it is necessary to refer to the astronomical time at Greenwich, or the *Greenwich Date*, No. 481, because it is for the time at this meridian that the elements of astronomical calculations, which are in perpetual change, are given in the Nautical Almanac.

The Greenwich Date is always *mean time*, unless the contrary be expressed. At sea, however, it is often convenient to deduce the Greenwich Date in App. Time.

* The term *Greenwich Date*, used always by Dr. Inman, is preferable to *Greenwich Time*, because it is essential to note the day as well as the hour.

† The reason of these rules will appear on considering that dividing 360° into 24^h gives 15° for 1 hour, $15'$ for 1^m, and $15''$ for 1^s; and further, that to multiply by 60, and at the same time to divide by 15, is the same as to multiply by 4; and to multiply by 15 and to divide by 60 is to divide by 4.

575. To find the Greenwich Date by the Chronometer:—

Since the chronometer is regulated to Greenwich mean time, apply the gain or loss up to the time proposed. No example is necessary, as this is no more than the common process of allowing for the error of a watch.

576. To find the Greenwich Date without the Chronometer:—

(1.) In W. Long. Find the Astron. Date, No. 574; *add* to it the Long. converted into time, No. 570. If the sum amounts to or exceeds 24^h , deduct 24^h and reckon the time on the *next day*.

Ex. 1. June 3d, at $3^h 30^m$ P.M., long. 31° W.: find the Greenwich Date.

Astron. Date, June 3d,	$3^h 30^m$
31° ,	$+ 2 \frac{4}{5}$
GREENWICH, JUNE 3d,	5 34

Ex. 2. June 4th, $5^h 18^m$ A.M., long. 130° W.: find the Greenwich Date.

Astron. Date, June 3d,	$17^h 18^m$
130° ,	$+ 8 \frac{40}{58}$
GREENWICH, JUNE 4th,	1 58

(2.) In E. Long. Find the Astronomical Date, No. 574; *subtract* from it the Long. in time: the remainder is the Greenwich Date. If the Long. be greater than the Astron. Date, add 24^h to this last, and reckon the time on the *preceding day*.

Ex. 3. April 15th, $4^h 17^m$ P.M., long. 28° E.

Astron. Date, 15th,	$4^h 17^m$
28° ,	$- 1 \frac{52}{25}$
GREENWICH, APRIL 15th,	2 25

Ex. 4. Dec. 31st, $6^h 57^m$ A.M., long. 40° E.

Astron. Date, 30th,	$18^h 57^m$
40° ,	$- 2 \frac{40}{17}$
GREENWICH, DEC. 30th,	16 17

(3.) When it is noon at the place. In W. Long. the Greenwich Date is the Long. in time. In E. Long. take the Long. in time from 24^h : the remainder is the Greenwich Date on the *preceding day*.

Ex. 5. February 13th, noon, long. 122° W.

GREENWICH, FEB. 13th, $8^h 8^m$ P.M.

Ex. 6. March 31st, long. 91° E.

Long. $6^h 4^m$
GREENWICH, MARCH 30th, 17 56

577. It is easy to perceive, on all occasions, what the Greenwich Date must be, by proceeding from noon at the place.

Thus, in Ex. 2, when it is noon in 130° W., it is $8^h 40^m$ *later* at Greenwich; hence, when it is $6^h 42^m$ *before* noon at this place, it is $6^h 42^m$ before $8^h 40^m$, or $1^h 58^m$ P.M. at Greenwich, on the same day.

Ex. 4. When it is noon in long. 40° E., it is $2^h 40^m$ *before* noon at Greenwich; hence, when it is $6^h 57^m$ A.M., or $5^h 3^m$ before noon at this place, it wants $2^h 40^m$ and $5^h 3^m$, or $7^h 43^m$ of noon at Greenwich on this day; or it is $16^h 17^m$ on the day before.

II. REDUCTION OF THE ELEMENTS IN THE NAUTICAL ALMANAC.

578. This Reduction is effected by Inspection, or by Logarithms. No. 597. When extreme precision is required, a further correction is necessary, on account of 2d Differences, No. 598.

1. *Reduction by Inspection.*[1.] *The Sun's Declination.*

579. *At Sea.*—(1.) At noon. Take out of the Nautical Almanac, p. I., or Table 60, the sun's decl. at noon of the day, and note whether it is increasing or decreasing; take out of Table 19 the correction for long., and apply it, as there directed, to the decl. at noon.

If the correction, when *subtractive*, exceed the decl. at noon in the table, the difference is the decl. of the *contrary* name.

Ex. 1. Nov. 13th, 1902, long. 64° W.:
find the decl. at noon.

Sun's decl. 13th, noon, 17° 48' S. (*incr.*)
64° W. Table 19 + 3
RED. DECL. 17 51 S.

Ex. 2. March 20th, 1902, long. 178° W.:
find the Sun's decl. at noon.

Decl. 20th, noon 0° 25' S. (*decr.*)
178° W. Table 19 - 12
RED. DECL. 0 13 S.

Ex. 3. June 20th, 1902, long. 120° W.:
find the decl. at noon.

Decl. 20th, noon, 23° 26' N. (*incr.*)
120° W. Table 19 0
RED. DECL. 23 26 N.

Ex. 4. Sept. 22d, 1902, long. 167° W.:
find the Sun's decl. at noon.

Decl. 22d, noon, 0° 35' N. (*decr.*)
167° W. Table 19 - 11
RED. DECL. 0 24 N.

Ex. 5. Aug. 6th, 1902, long. 85° E.:
find Sun's decl. at noon.

Decl. 6th, noon, 16° 54' N. (*decr.*)
85° E. Table 19 + 4
RED. DECL. 16 58 N.

Ex. 6. March 20th, 1902, long. 80° W.:
find Sun's decl. at noon.

Decl. 20th, noon, 0° 25' S. (*decr.*)
80° W. Table 19 - 5
RED. DECL. 0 20 S.

When the declination at noon at Greenwich is 0° 0' in *east* long., the correction is the decl. of the same name as that of the day *before*; in *west* long. the correction is the decl. of the same name as that of the day *after*.

(2.) At a given hour. Correct for long. as above, and then apply the correction for the hour.

Ex. 1. March 21st, 1902, long. 123° W.
at 3^h P.M.: find the decl.

Decl. 21st, noon, 0° 1' S. (*decr.*)
123 W. + 8' }
3^h + 3' } + 11
RED. DECL. 0 10 N.

For 3^h A.M. the corr. will be for 9^h, or 9', *subtractive*, and the DECL. is 0° 2' S.

Ex. 2. Feb. 12th, 1902, long. 78° E. at
7^h 50^m P.M.: find the decl.

Decl. 12th, noon, 13° 54' S. (*decr.*)
78° E. + 4' }
7^h 50^m - 6' } - 2
RED. DECL. 13 52 S.

For 7^h 50^m A.M. the corr. is that for 4^h 10^m, or 3', *additive*, and the DECL. is 14° 1' S.

580. *Accurately.*—(1.) Find the Greenwich Date.* Take out of the Nautical Almanac, p. II., the decl. for noon of the same and the next days, and take the diff. between them, or the Daily Variation.

When the declination changes its name, the daily variation is the *sum* of the two declinations.

(2.) With the Greenwich Date and daily variation take out the proportional part from Table 21.

* When the Greenwich Date is given in Apparent Time, the Sun's decl., &c., are taken from p. I. of the Naut. Alm. instead of p. II.; the computation in other respects is the same.

The reduction of the elements in the Nautical Almanac can also be effected by using the Hourly Variation given on p. I. of each month: taking care always to use the elements for the noon or hour nearest to the Greenwich Date. Several examples given under Nos. 579-584, and 592 are thus worked:—

1. Reduction by Hourly Variation in Nautical Almanac.

579.

[1.] *The Sun's Declination.*

Ex. 1. Nov. 13th, 1878, long. 64° W.:
find the decl. at noon.
Long. 64° W. = $4^h 16^m = 4^h 3'$
Hourly Var. $39'' \cdot 7 \times 4 \cdot 3 = 171''$ or $+ 3'$.
Sun's decl. 13th, noon, $18^{\circ} 1' S.$ (incr.)
 64° W. Table 19 $\frac{+3}{+3}$
RED. DECL. $18 \quad 4 \quad S.$

Ex. 4. Sept. 22d, 1878, long. 167° W.:
find the Sun's decl. at noon.
Long. 167° W. = $11^h 8^m = 11^h 1'$
Hourly Var. $58'' \cdot 5 \times 11 \cdot 1 = 649''$ or $- 11'$.
Decl. 22d, noon, $0^{\circ} 16' N.$ (decr.)
 167° W. Table 19 $\frac{-11}{-11}$
RED. DECL. $0 \quad 5 \quad N.$

(2.) At a given hour.

Ex. 1. March 21st, 1878, long. 123° W.,
at 3^h P.M.: find the decl.
Long. 123° W. = $8^h 12^m + 3^h = 11^h 12^m = 11^h 2'$.
Hourly Var. $59'' \cdot 1 \times 11 \cdot 2 = 663''$ or $+ 11'$.
Decl. 21st, noon, $0^{\circ} 18' N.$ (incr.)
 123° W. $+ 8'$ } $+ 11$
 $3^h \quad + 3'$ }

RED. DECL. $0 \quad 29$

For 3^h A.M. the corr. will be for 9^h , or
 $9'$, subtractive, and the DECL. is $0^{\circ} 17' N.$

Ex. 2. Feb. 12th, 1878, long. 78° E., at
 $7^h 50^m$ P.M.: find the decl.
Long. 78° E. = $5^h 12^m - 7^h 50^m = 2^h 38^m = 2^h 6'$.
Hourly Var. $50'' \cdot 1 \times 2 \cdot 6 = 130''$ or $- 2'$.
Decl. 12th, noon, $13^{\circ} 38' S.$ (decr.)
 78° E. $+ 4'$ } $- 2$
 $7^h 50^m \quad - 6'$ }

RED. DECL. $13 \quad 36 \quad S.$

For $7^h 50^m$ A.M. the corr. is that for
 $4^h 10^m$, or $3'$, additive, and the DECL. is
 $13^{\circ} 45' S.$

580. (3.)

Ex. 1. May 9th, 1878, at $11^h 30^m$ mean
time at Greenwich: find the Sun's declin.
Hourly Var. $39'' \cdot 5 \times 11^h 30^m$ or $11^h 5' = 454'' \cdot 3$
 $= + 7' 34'' \cdot 3$
Decl. 9th, at noon, $17 \quad 23 \quad 58 \quad 9 \quad N.$
RED. DECL. $17 \quad 31 \quad 33 \quad 2 \quad N.$

Ex. 2. March 21st, 1878, $15^h 27^m$ mean
time at Greenwich: find the Sun's decl.
 $15^h 27^m - 24^h = 8^h 33^m$ or $8^h 55'$.
Hourly Var. 22d, $59'' \cdot 2 \times 8^h 55' = 506'' \cdot 2$
 $= - 8' 26'' \cdot 2$
Decl. 22d, at noon, $0 \quad 41 \quad 42 \quad 6 \quad N.$
RED. DECL. $0 \quad 33 \quad 16 \quad 4 \quad N.$

582.

[2.] *The Sun's Right Ascension.*

Ex. 1. June 6th, 1878, at $8^h 11^m$ A.M.,
mean time, long. 17° W.: required the Sun's
R.A.

Astron. Time, June, $5^d 20^h 11^m$
Long. 17° W. $+ 1 \quad 8$
Green. Time, June, $5 \quad 21 \quad 19$
 $21^h 19^m - 24^h = 2^h 41^m$ or $2^h 7'$.
Hourly Var. 6th, $10^{\circ} 31' \times 2^h 7' = - 27^{\circ} 8'$
R.A. 6th, $4 \quad 57 \quad 26 \quad 4$
RED. R.A. $4 \quad 56 \quad 58 \quad 6$

Ex. 2. March 22d, 1878, at $2^h 20^m$ P.M.,
mean time, long. 43° E.: required the Sun's
R.A.

Astron. Time, March, $22^d 2^h 20^m$
Long. 43° E. $- 2 \quad 52$
Green. Time, March, $21 \quad 23 \quad 28$
 $23^h 28^m - 24^h = 0^h 32^m$ or $0^h 53'$.
Hourly Var. 22d, $9^{\circ} 09' \times 0^h 53' = - 4^{\circ} 8'$
R.A. 22d, $0 \quad 6 \quad 24 \quad 7$
RED. R.A. $0 \quad 6 \quad 19 \quad 9$

583.

[3.] *The Equation of Time.*

Ex. 2. Nov. 29th, 1878, long. 103° E.
at apparent noon: find the Equation of
Time.

Astron. Time, Nov. $29^d 0^h 0^m$
 103° E. $- 6 \quad 52$
Green. App. T., Nov. $28 \quad 17 \quad 8$
 $17^h 8^m - 24^h = 6^h 52^m$ or $6^h 9'$.
Hourly Var. 29th, $0^{\circ} 89' \times 6^h 9' = + 6^{\circ} 1'$
Equation 29th, at noon, $- 11^m 30 \quad 0$
RED. Eq. OF T. $- 11 \quad 36 \quad 1$

Ex. 3. Dec. 25th, 1878, long. 18° W. at
 $5^h 0^m$ A.M. (app. time): find the Equation
of Time.

Astron. Time, Dec. $24^d 17^h 0^m$
 18° W. $+ 1 \quad 12$
Green. Time, Dec. $24 \quad 18 \quad 12$
 $18^h 12^m - 24^h = 5^h 48^m$ or $5^h 8'$
Hourly Var. 25th, $1^{\circ} 25' \times 5^h 8' = - 7^{\circ} 3'$
Equation 25th, at noon, $+ 0^m 20 \quad 0$
RED. Eq. OF T. $+ 0 \quad 12 \quad 7$

[To face p. 208.]

(3.) When the first decl. is *increasing*, add this prop. part to the decl. at noon; when *decreasing*, subtract it.

If the prop. part, when *subtractive*, exceed the decl. itself, the difference is the decl. of the *contrary name*.

Ex. 1. May 9th, 1878, at 11^h 30^m mean time at Greenwich: find the Sun's declin.

9th, Page II., N.A. 17° 23' 58"·9 N.
10th, 17 39 47·4 N.

Daily Var. 15 48·5
11^h 30^m, var. 15' 30" 7 25·6
18·5 8·9

+ 7 34·5
9th, at noon, 17 23 58·9 N.

RED. DECL. 17 31 33·4 N.

Ex. 2. March 21st, 1878, 15^h 27^m mean time at Greenwich: find the Sun's declin.

21st, Page II., N.A. 0° 18' 2"·4 N.
22d, 0 41 42·6 N.

Daily Var. 23 40·2
15^h 0^m, var. 23' 30" 14 41·2
10·2 6·4

27^m, 23 40 26·6
+ 15 14·2

21st, at noon, 0 18 2·4 N.

RED. DECL. 0 33 16·6 N.

The sun's decl. changes nearly 1' an hour, or 1" in 1^m, in March and Sept.; hence, to ensure it to 1" in the extreme case, the Greenwich Date must be true to 1^m.

The 2d. diff. (see No. 598) is 26" a-day in June and December. The greatest error of omitting it is then $\frac{1}{8}$ of 26", or 3".

[2.] *The Sun's Right Ascension.*

581. *Approximately*.—Find it in the Nautical Almanac, or from Sidereal Time in Table 61, for noon. See Note to p. 211 and p. 421.

Ex. 1901, April 21st, find the Sun's Right Ascension. Sidereal Time, April 21st, 1^h 55^m·4 – 1^m·2 Equation of Time = 1^h 54^m·2, Sun's R.A.

582. *Accurately*.—(1.) Find the Greenwich Date. Take out of the Nautical Almanac, p. II., the R.A. for noon of the same day and the next. Take the difference between them, which is the Daily Variation.

When the first R.A. has 23^h and the second 0^h, add 24^h to the second, and subtract the first from it: the remainder is the Daily Variation.

(2.) With the Greenwich Date and the Daily Variation find the proportional part from Table 21.

(3.) Add this prop. part to the first R.A.: if the sum exceed 24^h, reject 24^h.

Ex. 1. June 6th, 1878, at 8^h 11^m A.M., mean time, long. 17° W.: required the Sun's R.A.

Astron. Time, June, 5^h 20^m 11^s
Long. 17° W. + 1 8

Green. Time, June, 5 21 19

R.A. 5th, Page II., N.A., 4^h 53^m 19^s·2
6^h, 4 57 26·4

Daily Var. 4 7·2

21^h 0^m, var. 4^m 0^s 3 30

7·2 6·3

19^m, 4 7 3·3

Corr. + 3 39·6

5th. R.A. 4 53 19·2

RED. R.A. 4 56 58·8

Ex. 2. March 22d, 1878, at 2^h 20^m P.M., mean time, long. 43° E.: required the Sun's R.A.

Astron. Time, March, 22^h 2^m 20^s
Long. 43° E. – 2 52

Green. Time, March, 21 23 28

R.A. 21st, Page II., N.A., 0^h 2^m 46^s·4
22d, 0 6 24·7

Daily Var. 3 38·3

23^h 0^m, var. 3^m 30^s 3 21·2

8·3 8·0

28^m, 3 38 4·2

+ 3 33·4

21st, noon, 0 2 46·4

RED. R.A. 0 6 19·8

When the R.A. in the tables is 0, the prop. part is R.A. required.

The greatest daily change of R.A. is $4^m 30^s$ in December; the smallest, $3^m 30^s$ in September.

[3] *The Equation of Time.*

583. *At Sea.*—(1.) Find the Greenwich Date. Take out the equation of time from the Nautical Almanac, p. I., or Table 62, for the same day and the next. When both the equations are directed to be added, or both to be subtracted, take their difference: if one is to be added and the other subtracted, take the sum: the result is the Daily Variation.

(2.) With the Greenwich Date and the Daily Variation find the correction or proportional part by Table 21.

(3.) When the first Equation is *increasing*, add the prop. part; when *decreasing*, subtract the lesser from the greater.

If the prop part, when subtractive, exceed the first Equation, their diff. is the Reduced Equation, and is *additive* or *subtractive* according to the direction for the second Equation.

Ex. 1. June 25th, 1902, long. 41° W. at $3^h 28^m$ P.M. (app. time): find the Equation of Time.

Astron. Time, June,	$25^d 3^h 28^m$
41° W.	$+ 2 \ 44$
Green. Time, June,	$25 \ 6 \ 12$
Eq. T. 25th,	$+ 2^m 11^s \cdot 0$
26th,	$+ 2 \ 24 \ 0$
Daily Var.	$13 \ 0$
$6^h 12^m$, var. 13^s	$+ 3 \ 0$
25th, noon,	$2 \ 11 \ 0$
RED. Eq. or T.	$+ 2 \ 14 \ 0$

Ex. 2. Nov. 29th, 1902, long. 103° E. at apparent noon: find the Equation of Time.

Astron. Time, Nov.	$29^d 0^h 0^m$
103° E.	$- 6 \ 52$
Green. App. T. Nov.	$28 \ 17 \ 8$
Eq. T. 28th,	$11^m 50^s \cdot 0$
29th,	$11 \ 29 \ 0$
Daily Var.	$21 \ 0$
$17^h 8^m$, var. 21^s	$- 15 \ 1$
28th, noon,	$- 11 \ 50 \ 0$
RED. Eq. or T.	$- 11 \ 34 \ 9$

Ex. 3. Dec. 26th, 1902, long. 18° W. at $5^h 0^m$ A.M. (app. time): find the Equation of Time.

Astron. Time, Dec.	$25^d 17^h 0^m$
18° W.	$1 \ 12$
Green Time, Dec.	$25 \ 18 \ 12$
Eq. T. 25th,	$- 0^m 8^s \cdot 6$
26th,	$+ 0 \ 21 \ 3$
Daily Var.	$0 \ 29 \ 9$
$18^h 12^m$, var. $29^s \cdot 9$	$- 22 \ 7$
25th, noon,	$- 0 \ 8 \ 6$
RED. Eq. or T.	$+ 0 \ 14 \ 1$

Ex. 4. Sept. 1st, 1902, long. 84° E. at $4^h 34^m$ A.M. (app. time): find the Equation of Time.

Astron. Time, Aug.	$31^d 16^h 34^m$
84° E.	$- 5 \ 36$
Green. App. T. Aug.	$31 \ 10 \ 58$
Eq. T. 31st,	$+ 0^m 28^s \cdot 3$
32d,	$0 \ 9 \ 7$
Daily Var.	$18 \ 6$
$10^h 58^m$, var. $18^s \cdot 6$	$- 8 \ 5$
Eq. T. 31st,	$0 \ 28 \ 3$
RED. Eq. or T.	$+ 0 \ 19 \ 8$

As the Equation of Time is generally required for a particular hour, the above method by Table 21 is more convenient than that by Table 20, in which the correction is given corresponding to the longitude, and the time at ship, without reference to the time at Greenwich. The first example worked by Table 20 will stand thus (no

further explanation being necessary, as the table is entered precisely like Table 19):—

Ex. 1. June 25th, 1878, long. 41° W.
at $3^h 28^m$ P.M.

Eq. T. 25th, p. I., N.A. $+ 2^m 18^s \cdot 5$
26th, $+ 2^m 31^s \cdot 2$

Daily Var. $12^s \cdot 7$

41° W. $+ 1^m \cdot 4$ } $+ 3^m \cdot 2$
 $3^h 28^m$ $+ 1^m \cdot 8$ }

Eq. 25th. $+ 2^m 18^s \cdot 5$

RED. EQ. OF T. $+ 2^m 21^s \cdot 7$

Ex. 2. March 26th, 1878, long. 109° E.
at $7^h 42^m$ A.M. (app. time).

Astron. Time, March 25^d 19^h 42^m
Eq. 25th, $+ 6^m 4^s \cdot 2$
26th, $+ 5^m 45^s \cdot 7$

Daily Var. $18^s \cdot 5$

$12^h 0^m$ $- 9^s \cdot 2$ } $- 9^s \cdot 5$
 $7^h 42^m$ $- 5^s \cdot 9$ }

109° E. $+ 5^m \cdot 6$

25th, noon, $+ 6^m 4^s \cdot 2$

RED. EQ. OF T. $+ 5^m 54^s \cdot 7$

584. *Accurately*.—Proceed as directed in No. 583, with more attention to precision in the several quantities.

Ex. 1. Green. Date, June 25th, 1878,
 $6^h 11^m$ (app. time): find the Equation of Time.

Eq. 25th, page I., N.A. $2^m 18^s \cdot 5$
26th, $2^m 31^s \cdot 2$

Daily Var. $12^s \cdot 7$

$6^h 0^m$, var. $12^s \cdot 7$ $3^s \cdot 2$

11^m , do. 1^s

$+ 3^s \cdot 3$

Eq. 25th, $+ 2^m 18^s \cdot 5$

RED. EQ. OF T. $+ 2^m 21^s \cdot 8$

Ex. 2. Green. Date, Dec. 24th 1878,
 $15^h 49^m$ (app. time): find the Equation of Time.

Eq. 24thh. N.A. $- 0^m 10^s \cdot 0$
25th, $+ 0^m 20^s \cdot 0$

Daily Var. $30^s \cdot 0$

$15^h 30^m$, var. 30^s $19^s \cdot 4$

19^m , do. 4^s

$- 19^s \cdot 8$

24th, Eq. $- 0^m 10^s \cdot 0$

RED. EQ. OF T. $- 0^m 9^s \cdot 8$

[4.] *The Sidereal Time.**

585. Take from Table 23 the Acceleration corresponding to the hours, minutes, and seconds of the Greenwich Date; *add* them to the Sidereal Time at the preceding mean noon, from N.A. or Table 61.

When the sum exceeds 24^h , reject 24^h .

Ex. 1. Green. Date, Nov. 1st, 1901,
 $3^h 41^m 39^s$: find the Sid. Time. By
Tables 61 and 23.

Sid. T. mean noon, Nov. 1st, $14^h 40^m \cdot 3$

Accel. 3^h 5^s

41^m 1^s

39^s 0^s

RED. SID. TIME $14^h 40^m \cdot 9$

Ex. 2. Green. Date, March 23rd, 1901,
 $20^h 36^m 57^s$: find the Sid. Time. By
N.A.

Sid. T. mean noon, March 23d, $0^h 1^m 7^s \cdot 0$

20^h $3^m 17^s \cdot 1$

36^m $5^s \cdot 9$

57^s 2^s

RED. SID. TIME $0^h 4^m 30^s \cdot 2$

[5.] *The Moon's Horizontal Parallax.*

586. *At Sea*.—As the Moon's Horizontal Parallax does not change more than $27''$ in 12 hours, it may be, in most cases, taken out of the Nautical Almanac at sight.

587. *Accurately*.—(1.) Find the Greenwich Date. When the Greenwich time is less than 12^h , take out the hor. par. for the noon and midnight of the given day; when it exceeds 12^h , take out the quantities for the midnight of the same day and the noon of the next. Take the difference between them, which is the variation in 12 hours.

* The Sun's Right Ascension may be found roughly thus:—To the Sidereal Time in Table 61 apply the Eq. of Time from Table 62, as there directed: for ex., the Sidereal Time on Nov. 1st, 1901, is $14^h 40^m \cdot 3$, the Eq. of Time is $16^m 3^s$ sub.; hence, *subtracting* $16^m 3^s$ from $14^h 40^m \cdot 3$, gives $14^h 24^m$, the Sun's R.A. required.

(2.) Enter Table 21 with the Greenwich Time and the 12-hourly var., and take out the proportional part. When the horizontal parallax is *increasing*, *add* this prop. part; when *decreasing*, *subtract* it from the horizontal parallax at the preceding noon or midnight.

Ex 1. Green. Date, Jan. 15th, 1878,
5^h 11^m: required the Hor. Par.

H.P. 15th, noon,	57' 45''·2
15th, midn.	58 12 ·7
Var. in 12 ^h ,	27 ·5
5 ^h 11 ^m , var. 27''·5	+ 11 ·9
15 ^h h. noon,	57 45 ·2
RND. HOR. PAR.	57 57 1

Ex 2. Green. Date, Aug. 12th, 1878,
15^h 28^m: required the Hor. Par.

H.P. 12th, midn.	54' 56''·9
13th, noon,	54 45 ·9
Var. in 12 ^h ,	11 ·0
3 ^h 28 ^m , var. 11''·0	- 3 ·2
12th, midn.	54 56 ·9
RND. HOR. PAR.	54 53 ·7

When necessary to correct for latitude (No. 437), see Table 41.

[6.] *The Moon's Semi-diameter.*

588. As the variation in 12^h does not exceed 8'', the semi-diameter may be taken out of the Nautical Almanac at sight. In general the hor. par. is required at the same time, and the semid. corresponding is then taken at once from Table 40.

[7.] *The Moon's Declination.*

589. *At Sea.*—(1.) Find the Greenwich Date. Take out of the Nautical Almanac the decl. corresponding to the hour of the Greenwich Time, and also the diff. for 10^m.

(2.) Enter Table 22 with this diff. and the minute of the Greenwich Date, and take out the prop. part at sight to the nearest minute.

(3.) When the declination is *increasing*, *add* this prop. part to it; when *decreasing*, *subtract* the lesser from the greater. If the prop. part, when subtractive, exceed the decl., their diff. is the decl. of the *contrary* name.

Ex. 1. Green. Date, Feb. 16th, 1878,
11^h 56^m: find the Moon's declin.

Decl. 11 ^h ,	14° 39' N. decr. D. 154''
56 ^m , D. 154''	- 14
RND. DECL.	14 25 N.

Ex. 2. Green. Date, April 24th, 1878,
10^h 47^m: find the Moon's declin.

Decl. 10 ^h ,	18° 15' S. decr. D. 108''
47 ^m D. 108''	- 8
RND. DECL.	18 7 S.

Ex. 3. Green. Date, June 25th, 1878,
6^h 50^m: find the Moon's declin.

Decl. 6 ^h ,	18° 33' N. incr. D. 105''
50 ^m ,	+ 9
RND. DECL.	18 42 N.

Ex. 4. Green. Date, Sept. 22nd, 1878,
9^h 37^m: find the Moon's declin.

Decl. 9 ^h ,	18° 34' N. decr. D. 122''
37 ^m ,	- 8
RND. DECL.	18 26 N.

When the decl. for the given hour is 0, the prop. part is the decl. of the name of the next hour.

590. *Accurately.*—Employ the decimals of the diff. for 10^m as whole seconds, taking care to divide the prop. part corresponding by 10, or by 100. Proceed as above directed in No. 589, (1) and (3); also take the seconds of the Greenwich Date as minutes, taking care to put the minutes of the prop. part into the place of the seconds,

and the seconds into that of thirds : it is near enough to work to the fraction of 1^m.

Ex. 1. Green. Date, Aug. 16, 1878, 17^h 38^m 20^s : find the Moon's declin.

Decl. 17^h, 8° 10' 3'' 2 N. *incr.* D. 130'' 28
10^m : 130'' 28 :: 38^h + 8 19 '4

RED. DEC. 8 18 22 '6 N.

Ex. 2. Green. Date, Jan. 221, 1878, 4^h 31^m 45^s : find the Moon's declin.

Decl. 4^h, 0° 15' 27'' 7 N. *dec.*
10^m : 170'' 92 :: 31^h - 9 2 '7

RED. DEC. 6 25 '0 N.

The greatest change of decl. in 1 hour is 17' ; hence, to obtain the decl. in the extreme case, true to 1', the Greenwich Date must be true to 4^m, or 1° of long. ; and to obtain it to 1'', the Greenwich Date must be true to 4^s, in the extreme case.

17 ^m , 2 3 3	2 4	17 ^m , 5 9 3	8 4
	1 4		3 6
	I 1 3		4 53 2
R.A. Sept. 11th,	11 37 18 8	R.A. May 5th,	5 17 49 3
R <small>ED.</small> R.A.	11 36 17 5	R <small>ED.</small> R.A.	5 22 42 5

The greatest daily change of R. A. is 6^m.

(2.) Enter Table 21 with the Greenwich Time and the 12-hourly var., and take out the proportional part. When the horizontal parallax is *increasing*, add this prop. part; when *decreasing*, subtract it from the horizontal parallax at the preceding noon or midnight.

Ex 1. Green. Date, Jan. 15th, 1878,
5^h 11^m: required the Hor. Par.

H.P. 15th, noon,	57' 45''·2
15th, midn.	58 12 ·7
Var. in 12 ^h ,	27 ·5
5 ^h 11 ^m , var. 27''·5	+ 11 ·9
15 ^h , noon,	57 45 ·2
RED. HOR. PAR.	57 57 ·1

Ex 2. Green. Date, Aug. 12th, 1878,
15^h 28^m: required the Hor. Par.

H.P. 12th, midn.	54' 56''·9
13th, noon,	54 45 ·9
Var. in 12 ^h ,	11 ·0
3 ^h 28 ^m , var. 11''·0	- 3 ·2
12th, midn.	54 56 ·9
RED. HOR. PAR.	54 53 ·7

When necessary to correct for latitude (No. 437), see Table 41.

592.

[9.] *Right Ascension of Venus.*

Ex. 3. Green. Date, Sept. 11th, 1903,

11^h 47^m: find Venus' R.A.

R.A. Sept. 11th, noon 11^h 37^m 18^s·8

Hourly Var.* 11th,

5^m·1 × 11^m·8 1 0 ·2

RED. R.A. VENUS 11 36 18 ·6

Ex. 4. Green. Date, May 5th, 1903,

22^h 47^m: find Venus' R.A.

R.A. May 5th, noon 5^h 17^m 49^s·3

Hourly Var.* 5th,

12^m·9 × 22·8 4 54 ·1

RED. R.A. VENUS 5 22 43 ·4

593.

[10.] *Declination of Venus.*

Ex. 1. Green. Date, Sept. 11th, 1903,

11^h 47^m: find Venus' Declination.

Hourly Var.* Sept. 11th

23''·9 × 11^h 47^m = -4' 42''·0

Decl. Venus, Sept. 11th, 6° 51' 30''·0

RED. DECL. VENUS 6 46 48 ·0

Ex. 2. Green. Date, Sept. 11th, 1903,

11^h 47^m: find Venus' Declination.

Decl. Sept. 11th, 6° 51' 30''·0

" Sept. 12th, 6 41 53 ·7

Daily Var. 9 36 ·3

11^h 30^m, var. 9 30 4 33 ·1

6^h 3 2 ·9

17^m, 9 36·3 6 ·9

Decl. Venus, Sept. 11th, -4 42 ·9

6 51 30 ·0

RED. DECL. VENUS 6 46 47 ·1

* The Hourly Variations are taken from the Planetary Ephemerides at Transit in the Nautical Almanac.

[To face p. 213.

of the name of the next hour.

590. *Accurately.*—Employ the decimals of the diff. for 10^m as whole seconds, taking care to divide the prop. part corresponding by 10, or by 100. Proceed as above directed in No. 589, (1) and (3); also take the seconds of the Greenwich Date as minutes, taking care to put the minutes of the prop. part into the place of the seconds,

and the seconds into that of thirds : it is near enough to work to the fraction of 1^m.

Ex. 1. Green. Date, Aug. 16, 1878, 17^h 38^m 20^s : find the Moon's declin.

Decl. 17^h, 8° 10' 3''·2 N. *incr.* D. 130''·28
10^m : 130''·28 :: 38½^m + 8 19 '4

RED. DEC. 8 18 22 '6 N.

Ex. 2. Green. Date, Jan. 22d, 1878, 4^h 31^m 45^s : find the Moon's declin.

Decl. 4^h, 0° 15' 27''·7 N. *dec.*
10^m : 170''·92 :: 31½^m - 9 2 '7

RED. DEC. 6 25 '0 N.

The greatest change of decl. in 1 hour is 17' ; hence, to obtain the decl. in the extreme case, true to 1', the Greenwich Date must be true to 4^m, or 1° of long. ; and to obtain it to 1'', the Greenwich Date must be true to 4^s, in the extreme case.

[8.] *The Moon's Right Ascension.*

591. Take the diff. of R.A. for 1^h. To the const. 9·5229 add the prop. log. of the diff. for 1^h, and the prop. log. of the minutes and seconds of the Greenwich Date : the sum is the prop. log. of the proportional part, always *additive*.

When the sum exceeds 24^h, reject 24^h.

Ex. 1. Green. Date, Feb. 2d, 1878, 1^h 17^m 15^s : find the Moon's R.A.

R.A. 1^h, 21^h 11^m 45^s·3
2^h, 21 13 41 '3
Var. 1^h, 1 56 '0
Time, 17 15
+ 0 33 '3
2'5104

R.A. 1^h, 21 11 45 '3
RED. R.A. 21 12 18 '6

Ex. 2. Green. Date, April 28th, 1878, 16^h 56^m 45^s : find the Moon's R.A.

R.A. 16^h, 23^h 58^m 54^s·6
17^h, 0 0 40 '4
Var. 1^h, 1 45 '8
Time, 56 45
1 40
2'0331

R.A. 16^h, 23 58 54 '6
RED. R.A. 0 0 34 '6

The greatest change in 1^h is 2^m 55^s, the smallest is 1^m 45^s ; hence to have the result true to 1^s, the Greenwich Date must be true to 20^s.

[9.] *Right Ascension of Venus.*

592. With the Green. Date and daily variation of R.A. deduce the prop. part by Table 21 ; this is to be *added* to the R.A. at the preceding noon when *increasing*, and *subtracted* when *decreasing*.

Ex. 1. Green. Date, Sept. 11th, 1903, 11^h 47^m : find Venus' R.A.

R.A. Sept. 11th, 11^h 37^m 18^s·8
Sept. 12th, 11 35 13 '3
Daily Var. 2 5 '5

11^h 30^m, var. 2^m 0^s 0 57 '5
5 '5 2 '4
17^m, 2 5 '5 1 '4

1 1 '3
R.A. Sept. 11th, 11 37 18 '8
RED. R.A. 11 36 17 '5

Ex. 2. Green. Date, May 5th, 1903, 22^h 47^m : find Venus' R.A.

R.A. May 5^h, 5^h 17^m 49^s·3
May 6th, 5 22 58 '6
Daily Var. 5 9 '3

22^h 30^m, var. 5^m 4 41 '2
9 '3 8 '4
17^m, 5 9 '3 3 '6

4 53 '2
R.A. May 5th, 5 17 49 '3
RED. R.A. 5 22 42 '5

The greatest daily change of R.A. is 6^m.

[10.] *Declination of Venus.*

593. Find the proportional part, and apply it to the declin. at the preceding noon, as directed in No. 580. As the process, whether Approximate or Accurate, is the same as that for the sun, no example is necessary.

The greatest daily change of declination is $35'$.

[11.] *Right Ascension and Declination of Mars.*

594. Proceed as for Venus. The greatest daily change of R.A. is 4^m ; that of declination, $25'$.

[12.] *Right Ascension and Declination of Jupiter.*

595. Proceed as for Venus. The greatest daily change of R.A. is 1^m ; that of declination, $4'$.

[13.] *Right Ascension and Declination of Saturn.*

596. Proceed as for Venus. The greatest daily change of R.A. is $40''$; that of declination, $2'$.

2. *Reduction by Logarithms.*

597. (1.) The proportional part may be found by the Proportional Logarithms, Table 74, thus:—For 24-hourly variations take the constant log. 9.1249; for 12-hourly variations take 8.8239; for 3-hourly variations, no constant; and for hourly variations, 9.5229.

Then to the constant add the prop. log. of the Green. Date, (reading hours and min. as min. and sec. when the var. corresponds to more than 3^h), and the prop. log. of the variation as given for 24^h , 12^h , 3^h , or 1^h ; the sum is the prop. log. of the proportional part required.

Ex. 1. (Daily Variation.) Green. Time
 $11^h 30^m$, Daily Var. $14' 42''$.

	const. log.	9.1249
Gr. Time $11^h 30^m$	p. log.	1.1946
Var. $14' 42''$	p. log.	1.0880
PROP. PART $7' 2'' 6$	p. log.	1.4075

Ex. 2. (Twelve-hourly Var.) Green.
Time $4^h 11^m$, Var. $16'' 6$.

	const. log.	8.8239
Gr. Time $4^h 11^m$	p. log.	1.6337
Var. $16'' 6$	p. log.	2.8133
PROP. PART $5'' 8$	p. log.	3.2709

Ex. 3. (Three-hourly Var.) Green. Time
 $7^h 18^m 12^s$, change in 3 hours $1^o 31' 41''$; find the Prop. Part for $1^h 18^m 12^s$.

Gr. Time $1^h 18^m 12^s$	p. log.	3621
Var. $1^o 31' 41''$	p. log.	2930
PROP. PART $0^o 39' 49''$	p. log.	6551

Ex. 4. (Hourly Var.) Green. Time
 $10^h 56^m 10^s$, Hourly Var. $8' 47'' 2$.

	const. log.	9.5229
Gr. Time $56^m 10^s$	p. log.	5058
Var. $8' 47'' 2$	p. log.	1.3114
PROP. PART $8' 13'' 5$	p. log.	1.3401

(2.) The proportional part for 24^h is obtained conveniently from Table 21 A,* thus:—

* In common practice at sea the prop. part may be taken out at sight from Table 21: when extreme precision is required the logarithms to four places only are not sufficient. For ex., at sea, for the Time $7^h 10^m$, and Daily Variation $22' 27'' 5$, we enter the table with $22' 30''$, and take out at once (No. 50) the quantity about $\frac{1}{2}$ between $6' 33'' 7$ at $7^h 0^m$, and $7' 1'' 9$ at $7^h 30^m$, that is, $6' 40''$, or $6' 7$. Now this mental interpolation is performed in very considerably less time than it takes to write down the quantities, while the small inaccuracy to which it is liable, amounting here to $6' 42'' 4 - 6' 40''$, or $2'' 4$ only, would be wholly inappreciable in practice at sea. The logarithms in Table 21 A give in this case the result true to $0'' 1$; but if the prop. part were above $8'$ the logs. could no longer be depended

Take out from this Table the log. of the Greenwich Time, and add to it the log. of the Daily Variation; the sum is the log. of the prop. part required.

Ex. 1. (The Sun's Declination.) Green.
Date, May 13th, 11^h 30^m.

Gr. Time	11 ^h 30 ^m	log.	3195
Daily Var.	14' 42"	log.	2129
PROP. PART	7' 2".6	log.	5324

Ex. 2. (The Sun's Right Ascension.)
Green. Date, June 6th, 9^h 19^m.

Gr. Time	9 ^h 19 ^m	log.	4109
Daily Var.	4 ^m 7".5	log.	7643
PROP. PART	1 ^m 36"	log.	1'1757

Ex. 3. (The Equation of Time.) Green.
Date, June 25th, 6^h 11^m.

Gr. Time	6 ^h 11 ^m	log.	5890
Daily Var.	12"	log.	3010
PROP. PART	3"	log.	8900

Ex. 4. (Right Ascension of Venus.)
Green. M.T. 19^h 13^m, Daily Var. 4^m 54^s.

Gr. Time	19 ^h 13 ^m		0965
Daily Var.	4 ^m 54 ^s		6900
PROP. PART	3 ^m 55 ^s		7864

3. Correction for Second Differences.

598. The quantities in the Nautical Almanac do not in general change uniformly, that is, by equal portions in equal times, but the differences of any series of quantities taken in order exhibit differences among themselves, or *second differences*, as in the case of alts., p. 200. Hence the proportional part found by the preceding rules is not always the *actual change* in the interval, but may require a correction, which is called the *equation of second differences*.

The greatest error which can arise in any case from neglecting this correction, that is, the greatest value of the equation itself, is $\frac{1}{2}$ of the whole 2d diff.; this takes place when the interval for which the proportional part is required is *half* the interval for which the quantities are set down in the table.

For example, suppose the second diff. of the sun's decl. to be 26" in 24^h; the greatest error of neglecting the equation will be 1-8th of 26", and will take place when the Green. Date is 12^h, or midnight.

599. To find the Equation of Second Differences. Take the two quantities in the table next on each side of the given one, and set them down in order. Add together the 1st and 4th, and the 2d and 3d; write against the sum of the 2d and 3d, whether it be the *greater* or the *lesser* of the two sums.

Half the diff. of these two sums is the 2d diff.

Under the Tabular Interval, and with the Green. Date as intermediate time, enter Table 25 and take out the multiplier, by which multiply the 2d diff.; this is the Equation of 2d differences. If the 2d sum is marked the *greater*, *add* the equation to the prop. part deduced by one of the preceding rules; if the *lesser*, *subtract* the equation.

upon as shewing the true tenth, not only because the last figure ceases to change by lat. 7^h 58^m, but because the last figure of any logarithm is itself but an approximation.

Although logarithms afford material service in multiplication or division of many figures, yet in short and easy reductions they are attended, as is well known to experienced arithmeticians, with considerable loss of time, and should accordingly be resorted to only when they unequivocally effect a saving of time and labour.

It is also important to observe that the facility of mental interpolation constantly improves by exercise, and that the habit sharpens the perception of arithmetical proportions.

By Logarithms. To the prop. log. of the 2d diff. add the ar. co. log. of the multiplier; the sum is the prop. log. of the equation required.

Ex. Greenwich Date, June 17th, 1878, 13^h 11^m M.T.: find the Sun's Declination. The two declinations preceding are those of the 16th and 17th; the two following are those of the 18th and 19th.

June 16th,	23° 22' 3 ^s 5
17th,	23 23 57 3
18th,	23 25 26 3
19th,	23 26 30 6
	<u>46 48 34 11</u>
	46 40 23 6 (<i>greater</i>)
	<u>2) 49 5</u>
2d Diff.	24 75

In Table 25, Tabular Interval 24^h and 13^h 11^m give .124.

This multiplied by 24.75 gives 3^s 07, the EQUATION of 2d DIFFS.; which being added to prop. part as found by No. 580, gives DECLIN. required.

By Logs.

24.75	p. log. 2.6400
Log. 9.0925	ar. co. 0.9075
	p. log. 3.5475

600. This correction is of the most importance when the quantity attains its *maximum*, that is, arrives at its greatest amount between two times given in the Nautical Almanac. This circumstance is known thus:—When the sum of the vars. in 1 hour opposite the Green. day and the following one is equal to the diff. of the vars. in 1 hour opposite the Greenwich day and the preceding one; for ex. on Dec. 20th, 21st, and 22d, the vars. in 1 hour of the sun are 1^m 70, 0^m 52, and 0^m 66 respectively, hence the declin. is maximum at some time between the noons of the 21st and 22d.

III. CONVERSION OF TIMES.

1. Intervals.

[1.] To convert an Interval of Mean Time into an Interval of Sidereal Time.

601. *Approximately*.—Increase the Interval by 1^m for every 6 hours, or by 10^s for each hour, or by 1^s for every 6^m.

602. *Accurately*.—Add to the Interval the *Acceleration* (Table 23), corresponding to the hours, minutes, and seconds.

Ex. 1. (Approximately.) Convert 7^h 12^m 6^s of M.T. into S.T.

	7 ^h 12 ^m 6 ^s
70 ^s and 2 ^s	+ 1 12
INTERV. IN SID. T.	7 13 18

Ex. 2. (Accurately.) The same ex.

	7 ^h 12 ^m 6 ^s
7 ^h 1 ^m 59 ^s 99	
12 ^m 1 ^s 97	+ 1 10 98
6 ^s 03	
INTERV. IN SID. T.	7 13 16 98

[2.] To convert an Interval of Sidereal Time into an Interval of Mean Time.

603. *Approximately*.—Diminish the Interval by 1^m for every 6 hours, or by 10^s for each hour, or by 1^s for every 6^m.

604. *Accurately*.—Subtract from the Interval the *Retardation** (Table 24), corresponding to the hours, minutes, and seconds.

* Or from corresponding tables in Naut. Almanac.

Ex. 1. (Approximately.)	Convert	Ex. 2. (Accurately.)	The same ex.
$7^h 13^m 17^s$ of S.T. into M.T.		$7^h 13^m 17^s$	
70^s and 2^s	$7^h 13^m 17^s$	$7^h 13^m 8^s \cdot 81$	
INTERV. IN M.T.	$\begin{array}{r} -1 \ 12 \\ \hline 7 \ 12 \ 5 \end{array}$	$\begin{array}{r} 13^m \ 2 \ 15 \\ 17^s \ 05 \\ \hline \end{array}$	$\begin{array}{r} -1 \ 10 \ 99 \\ \hline 7 \ 12 \ 6 \ 01 \end{array}$

The above precepts relate to *Intervals* of time; the following are employed in the conversion of *absolute time* of one kind into that of another.

2. Absolute Times.

[1.] To convert Apparent Time into Mean Time.

605. Reduce the Equation of Time, taken from page I. of the Nautical Almanac, or from Table 62 by No. 583, or 584, and apply it to the given App. Time as directed in the said page I. or in Table 62.

If the Eq. of T. when subtractive exceeds the A.T., add 24^h to the A.T. and date the time on the day before.

Ex. 1. March 2d, 1902, at $11^h 56^m 43^s$ A.M., A.T., long. 148° W.: find M.T.	Ex. 2. Nov. 10, 1902, $0^h 13^m 40^s$ P.M., A.T., long. 36° E.: required M.T.
The Green. Date is $2^d 9^h 49^m$.	Green. Date, $9^d 21^h 50^m$.
Eq. T. 2d, $12^m 27^s \cdot 8$	Eq. T. 9th, $-16^m 7^s \cdot 6$
3d, $12 \ 15 \cdot 6$	10th, $-15 \ 2 \cdot 7$
Daily Var. $12 \cdot 2$	Daily Var. $4 \cdot 9$
$9^h 49^m$, var. $12^s \cdot 2$	$21^h 50^m$, var. $4^s \cdot 9$
2d, $12 \ 27 \cdot 8$	9th, $16 \ 7 \cdot 6$
Red. Eq. T. $+12 \ 22 \cdot 7$	$-16 \ 2 \cdot 6$
App. T. $23 \ 56 \ 43$	App. T. $0 \ 13 \ 40 \cdot 0$
MEAN TIME, 2d $0 \ 9 \ 5 \cdot 7$	MEAN TIME, 9th $23 \ 57 \ 37 \cdot 4$

[2.] To convert Mean Time into Apparent Time.

606. Find the Green. Date; reduce to it the Eq. of T. from page II. of the Nautical Almanac, or from Table 62, and apply it to the given M.T. as directed in the said page II., or the *contrary way* to that directed in Table 62.

If the Eq. of T. when subtractive exceeds the M.T., add 24^h to the M.T. and date the time on the day before.

Ex. 1. Aug. 31st, 1902 long. 18° W., $20^h 58^m 51^s$ M.T.: find A.T.	Ex. 2. Feb. 17th, 1902, long. 120° E., $0^h 5^m 18^s$ M.T.: find A.T.
Green. Date, M.T., $31^d 22^h 11^m$.	Green. Date, M.T., $16^d 16^h 5^m$.
R. d. Eq. T. $-0^m 11^s \cdot 1$	R. d. Eq. T. $-14^m 17^s$
M.T. 31st, $20 \ 58 \ 51 \cdot 0$	M.T. $0 \ 5 \ 18$
App. TIME 31st $20 \ 58 \ 39 \cdot 9$	App. TIME, 16th $23 \ 51 \ 1$

[3.] To convert Sidereal Time into Mean Time.

That is, having given the Right Ascension of the Meridian, to find Mean Time.

607. In W. long. *add* the Acceleration for the long. to the Sid. T. at mean noon; in E. long. *subtract* it.

From the given Sid. Time (increased if necessary by 24^h) sub-

tract this reduced Sid. T. at the preceding noon; the remainder is the approximate M. T.; subtract from this time the Retardation corresponding (Table 24).

Ex. 1. Jan. 1st. 1878, long. $9^h 50^m 40^s$ E., at $21^h 9^m 23^s$ Sid. T.: find M.T.

Sid. T. M. Noon,	$18^h 44^m 0^s.7$	Given Sid. T.	$21^h 9^m 23^s.0$
Accel. $9^h 1^m 28^s.7$	} $- 1 37^o$	Red. Sid. T. M. Noon,	$18 42 23.7$
$50^m 8^s.2$		Approx. M.T.	$2 26 59.3$
$40^s .1$		Ret. $2^h 19^m 7^s$	} $- 24.2$
Sid. T. M. Noon,	$18 42 23.7$	$2^m 4^s.3$	
		$59^s 0^s.2$	
		MEAN TIME,	$2 26 35.1$

Ex. 2. March 22d, 1878, long. $7^h 22^m 35^s$ W., at $11^h 5^m 27^s.2$ Sid. T.: find M.T.

The RED. SID. T. is $0^h 0^m 37^s.9$; whence the approx. M.T. is $11^h 4^m 49^s.3$, and the Ret. to this is $1^m 48^s.9$ sub. leaves MEAN TIME $11^h 3^m 0^s.4$.

[4.] *To convert Mean Time into Sidereal Time.*

That is, having given the Mean Time, to find the R.A. of the Meridian.

608. In W. long. *add* the Acceleration for the long. to the Sid. T. at the preceding mean noon; in E. long. *subtract* it.

To this reduced Sid. T. at mean noon add the given M. T. and the Acceleration for the said M.T.; the result (rejecting 24^h if it exceed 24^h) is the Sid. T. required.

Ex. 1. June 19th, 1878, long. $10^h 39^m 6^s$ W., at $3^h 37^m 46^s.6$ M.T.: find Sid. T.	Ex. 2. Nov. 26th, 1878, long. $8^h 52^m 15^s$ E., at $14^h 55^m 7^s.8$ M.T.: find S.T.
Sid. T. at M. Noon, 29th, $6^h 29^m 44^s.3$	Sid. T. M. Noon, 26th, $16^h 21^m 7^s.6$
Accel. for long. $10^h 39^m 6^s$ $+ 1 45^o$	Accel. for $8^h 52^m 15^s$ $- 1 27.4$
Red. S.T. M. Noon, $6 31 29.3$	Red. S.T. at M. Noon, $16 19 40.2$
M.T. $3 37 46.6$	M.T. $14 55 7.8$
Accel. $3^h 29^m 6^s$ } $+ 35.8$	Accel. $14^h 2^m 18^s.0$ } $+ 2 27.0$
$37^m 6^s.1$	$55^m 9^s.0$
$47^s .1$	$7^s.8$
Sid. TIME, $10 9 51.7$	Sid TIME, $7 17 15.0$

IV. HOUR-ANGLES.

1. *To find the Hour-angle, Mean Time being given.*

[1.] *Hour-angle of the Sun.*

609. Find the Green. Date; Reduce to it the Eq. of T., and apply it to the M.T. as directed page II. of the Nautical Almanac, or the contrary way to that directed in Table 62; the result is A.T.

If A.T. is less than 12^h , it is the Sun's Hour-angle, reckoning from the meridian westwards; if A.T. exceed 12^h , subtract it from 24^h : the remainder is the Hour-angle, reckoning from the meridian eastwards

Ex. 1. May 19th, 1878, long. $57^{\circ} 4' W.$, at $3^h 7^m 46^s$ M.T.: find the Sun's Hour-angle.

The Green. Date is $19^d 6^h 56^m 2^s$.	
Eq. T. 19th, Page II.	$+ 3^m 45^s.3$
20th,	$+ 3^m 42^s.5$
	$2^s.8$
$6^h 56^m$, var. $2^s.8$	$- 2^s.8$
	$3^m 45^s.3$
Red. Eq. T.	$+ 3^m 44^s.5$
M.T.	$3^m 7^s 46^s.0$
Hour-angle,	$3^h 11^m 30^s.5$

Ex. 2. July 2d, 1878, long. $62^{\circ} 1' E.$, at $20^h 26^m 53^s$ M.T.: find the Sun's Hour-angle.

The Green. Date is $2^d 16^h 18^m 49^s$.	
Eq. T. 2d, Page II.	$3^m 43^s.9$
3d,	$3^m 55^s.1$
Daily Var.	$11^s.2$
$16^h 19^m$, var. $11^s.2$	$+ 7^s.7$
	$3^m 43^s.9$
Sub. from M.T.	$3^m 51^s.6$
M.T.	$20^h 26^m 53^s.0$
	$20^h 23^m 1^s.4 W.$
Hour-angle,	$3^h 36^m 58^s.6 E.$

610. When the Sun's Hour-angle is required from midnight, if A.T. is less than 12^h , subtract it from 12^h ; the remainder is the Hour-angle, reckoned westwards. If A.T. exceed 12^h , subtract 12^h from it; the remainder is the Hour-angle, reckoned eastwards.

[2.] *Hour-angle of a Star.*

611. (1.) Find the Green. Date, to which reduce the Sid. T. at mean noon.

(2.) To the M.T. add this reduced Sid. T., and from the sum (increased if necessary by 24^h) subtract the star's R.A.; the result is the Hour-angle W.

If the Hour-angle exceed 12^h , subtract it from 24^h ; the remainder is the Hour-angle E.

Ex. 1. July 21st, 1878, long. $32^{\circ} 10' W.$, at $9^h 45^m 21^s$ M.T.: required the Hour-angle of Arcturus.

Green. Date, $21^d 11^h 54^m 1^s$.	
Sid. T. Mean Noon, 21st,	$7^h 56^m 28^s.5$
Accel. 11^h ,	$1^m 48^s.4$
54 ^m ,	$8^s.9$
Red. Sid. T.	$7^h 58^m 25^s.8$
M. T.	$9^h 45^m 21^s.0$
	$17^h 43^m 46^s.8$
* R.A.	$14^h 10^m 8^s.4$
Hour-angle,	$3^h 33^m 38^s.4$

Ex. 2. Sept. 1st, 1878, long. $169^{\circ} 57' E.$ at $8^h 57^m 39^s$ M.T.: find the Hour-angle of Altair.

Green. Date, Aug. $31^d 21^h 37^m 51^s$.	
Sid. T. at M. Noon, 31st,	$10^h 38^m 7^s.3$
Accel. 21^h ,	$3^m 27^s.0$
37 ^m ,	$6^s.1$
51 ^s ,	$1^s.1$
Red. Sid. T.	$10^h 41^m 40^s.5$
M. T.	$8^h 57^m 39^s.0$
	$19^h 39^m 19^s.5$
* R.A.	$- 19^h 44^m 53^s.5$
	$23^h 54^m 26^s.0 W.$
Hour-angle,	$0^h 5^m 34^s.0 E.$

Ex. 3. Oct. 1st, 1878, long. $92^{\circ} 48' E.$, at $5^h 58^m 19^s$ M.T.: required the Hour-angle of Markab.

Hour-angle, $4^h 20^m 7^s.8 E.$

Ex. 4. Dec. 25th, 1878, long. $86^{\circ} 45' W.$, at $5^h 7^m 35^s$ M.T.: find Rigel's Hour-angle.

Hour-angle, $5^h 43^m 55^s. E.$

Ex. 5. March 22d, 1878, long. $110^{\circ} 39' W.$, at $11^h 3^m 37^s$ M.T.: find the Hour-angle of Antares.

Hour-angle, $5^h 15^m 53^s.9 E.$

[3.] *Hour-angle of a Planet or the Moon.*

612. (1.) Find the Green. Date, and reduce thereto the Sid. T. at mean noon, and the R.A. of the body.

(2.) Add this reduced Sid. T. to the M.T., and proceed as for a star.

Ex. 1. Oct. 15th, 1878, long. $41^{\circ} 44' W.$,
at $6^h 56^m 54^s$ P.M. M.T.: find the Moon's
Hour-angle.

Green. Date, Oct. 15 ^d 9 ^h 43 ^m 50 ^s .			
Sid. T. Mean Noon, 15th,	13 ^h 35 ^m 32 ^s 2		
Accel. 9 ^h	1 28 7		
43 ^m	7 1		
50 ^s	.1		
Red. Sid. T.	13 37 8.1		
C's R.A. 9 ^h	4 40 ^m 20 ^s 5		
10 ^h	4 42 37.5	9 5229	
	2 17	1 8967	
	43 50	0 6135	
	1 39 9	2 0331	
C's R.A. 9 ^h	4 40 20.5		
Red. R.A.	4 42 0.4		
Red. Sid. T.	13 ^h 37 ^m 8 ^s 1		
M.T.	6 56 54		
	20 34 2.1		
C's R.A.	-4 42 0.4		
	15 52 1.7 W.		
Hour-angle,	8 7 58.3 E.		

Ex. 2. Feb. 11th, 1878, long. $87^{\circ} 6' W.$,
at $4^h 46^m 48^s$ A.M. M.T.: find the Hour-
angle of Mars.

Green. Date, Feb. 10 ^d 22 ^h 35 ^m 12 ^s .			
Sid. T. Mean Noon, 10th	21 ^h 21 ^m 43 ^s 0		
Accel. 22 ^h	3 36 8		
35 ^m	5 8		
Red. Sid. T.	21 25 25.6		
Mars' R.A. 10th	2 ^h 15 ^m 57 ^s 0		
11th, 2	18 22 2		
Daily Var.	2 25 2		
22 ^h 35 ^m var. 2 ^h 25 ^m gives	2 17 1		
R.A. 10th	2 15 57.0		
Red. R.A.	2 18 14.7		
Red. Sid. T.	21 ^h 25 ^m 25 ^s 6		
M.T.	4 46 48.0		
	26 12 13.6		
Mars' R.A.	-2 18 14.1		
	23 53 59.5 W.		
Hour-angle,	0 6 0.5 E.		

2. To find the Hour-angle, the Altitude being given.

613. *By Inspection.* See Explan. of Table 5.

614. *By Computation.* Add together the alt., lat., and pol. dist., take half the sum, and from it subtract the alt.

Add together the log. sec. of the lat., the log. cosec. of the pol. dist., the log. cos. of the half sum, and the log. sine of the remainder; the sum (rejecting tens) is the log. sine square of the Hour-angle.*

Note.—When the Hour-angle is less than 2^h , four places of the logarithms give it to the nearest second of time.

Ex. 1. Alt. $37^{\circ} 51'$, lat. $51^{\circ} 10' N.$, pol. dist. $70^{\circ} 33'$, or decl. $19^{\circ} 27' N.$: find the Hour-angle. See Ex. 1, of No. 615.

Alt.	37° 51'		
Lat.	51 10	sec.	0.20269
Pol. dist.	70 33	cosec.	0.02552
Sum	159 34		
Half	79 47	cos.	9.24888
Rem.	41 56	sin.	9.82495
Hour-angle	3 ^h 32 ^m 47 ^s	sin. sq.	9.30204

Ex. 2. Alt. $21^{\circ} 19' 5''$, lat. $51^{\circ} 9' 26'' N.$, decl. $11^{\circ} 14' 44'' S.$: find the Hour-angle.

Alt.	21° 19' 5''	Pts. for'	
Lat.	51 9 26	sec.	0.202536, + 78
P. dist.	101 14 44	cosec.	0.008414, + 6
	173 43 15		
	86 51 37	cos.	8.758820, - 277
	65 32 32	sin.	9.959167, + 2
			8.908937
			- 201
		* sin. sq.	8.908736
	2 ^h 12 ^m 19 ^s		707
			3 29
Hour-angle	2 12 19.3		

Ex. 3. Lat. $30^{\circ} 11' 24'' N.$ Decl. $14^{\circ} 2' 46'' N.$ Alt. $61^{\circ} 9' 17''$. Hour-angle $1^h 43^m 52^s$.

When both the lat. and decl. are 0, the zenith distance in time is the measure of the Hour-angle.

At sea it is near enough to take the alt., lat., and pol. dist., to the nearest minute; but if the sum is *odd* and greater than 170° , take the cos. and sin. to $30''$, because the neglect of this may make a sensible error in the Hour-angle.

* Log. sine square, Table 69, is the same as the log. haversine of Inman's Tables.

[1.] *Errors of the Hour-Angle.*

615. The following rules give, very nearly, the effect of 1' error in the alt., lat., and pol. dist., and therefore for any small number of min. or sec. in the like proportion:—

(1.) Error of hour-angle, or time, due to 1' error of alt.* Add together the parts for 30'' of the cos. and sine: the sum, divided by the parts for 1° (Tab. 69), gives the error required.

When the alt. is too *small*, the hour-angle is too *great*; when the alt. is too *great*, the hour-angle is too *small*.

(2.) Error of hour-angle, or time, due to 1' error of lat.† Multiply the parts for 30'' of the sec. by 2, and add the parts for the sine; under the sum put the parts for 30'' of the cos., and take the diff.; divide this diff. by the parts for 1°.

When the lat. and true bearing are of the *same* names, the errors of the hour-angle and lat. are of the *same* kind; when of *contrary* names, of *contrary* kinds.

Ex. In N. Lat., if the sun is to the N. of E. or W., and the Lat. employed is too *great*, the computed hour-angle will be too *great*; if the sun is to the S., in the same case, too *small*.

(3.) Error of time, or hour-angle, due to 1' error of pol. dist. Multiply the parts for 30'' of the cosec. by 2, and add the parts for 30'' of the cos.; under the sum put the parts for 30'' of the sine; take the diff., and divide it by the parts for 1°.

When the parts for 30'' of the sine are *less* than the sum over them, the error of the hour-angle is of the *contrary* kind to that of the pol. dist.; when *greater*, of the *same* kind.

Ex. See Ex. 1, of No. 614.

Parts for 30".	Error 1' of Alt.	Error 1' of Lat.	Error 1' of Pol. Dist.
51° 10' sec. 78	Cos. 354	Sec. 78	Cosec. 22
70 33 cosec. 22	Sin. 71	× 2	× 2
79 47 cos. 354	(Sum) 425	156	44
41 56 sin. 71	ERROR OF TIME	Sin. 71	Cos. 354
Parts for	425	(Sum) 227	(Sum) 398
1° table 69 } 64	= 64 = 7°	Cos. 354	Sin. 71
p. 830 }		(Diff.) 127	< Diff.) 327
		ERROR OF TIME	ERROR OF TIME
		127	327
		= 64 = 2°	= 64 = 5°

The error of the hour-angle may, possibly, be made up of the *sum* of these three errors, but in most cases they will partially compensate.

* To find, approximately, the small interval of time corresponding to a small change of alt. by means of the Azimuth:—Add together the log. sine of the change of alt., the log. cosec. of the azim., and the log. sec. of the lat.: the sum (rejecting tens) is the log. sine of the interval required.

To find the same, by means of the Hour-angle:—Add together the log. sine of the change of alt., the log. sec. of the lat. and declin., the log. cos. of the alt., and the log. cosec. of the hour-angle: the sum is the log. sine, as above.

One of these processes may, on some occasions, be convenient.

† To find this error by means of the Azimuth:—Add together the log. cot. of the azim., the log. sec. of the alt., and the log. sine of the error of lat.: the sum is the log. sine of the error required.

3. To find the Hour-angle, the Azimuth being given.

616. Add together the log. sine of the azimuth, the log. cos. of the lat., and the log. sec. of the decl.; the sum (rejecting tens) is the log. sine of the angle A.*

Under A put the azimuth, reckoned from the elevated pole, and take half the sum.

Take half the sum of the pol. dist. and colat., and half the diff.

Add together the log. tan. of the half sum of A and the azim., the log. cos. of the half sum of the p. dist. and colat., and the log. sec. of the half diff.; the sum (rejecting tens) is the log. cot. of an arc.

When each half sum is less, or greater, than 90° , twice this arc is the Hour-angle required; but if one only of the half sums exceed 90° , twice the suppl. of the arc is the Hour-angle.

Ex. Lat. $51^\circ 30' N.$, decl. $20^\circ 2' N.$, azim. N. $110^\circ 21' W.$: find the Hour-angle.			
Az. $110^\circ 21'$	sin. 9.97201	P. Dist. $69^\circ 58'$	
Lat. $51^\circ 30'$	cos. 9.79415	Colat. $38^\circ 30'$	
Decl. $20^\circ 2'$	sec. 0.02711		
A $38^\circ 25'$	sin. 9.79327	Sum $108^\circ 28'$	half $54^\circ 14'$
Az. $110^\circ 21'$		Diff. $31^\circ 28'$	do. $15^\circ 44'$
Sum $148^\circ 46'$, half $74^\circ 23'$			$1^\circ 38' 52''$
			2
		Hour-angle, $3^\circ 17' 44''$	

4. To find the Hour-angle, the Altitude and Azimuth being given.

617. Add together the log. sine of the azim., the log. cos. of the alt., and the log. sec. of the decl.; the sum (rejecting tens) is the log. sine of the Hour-angle.

Ex. Alt. $40^\circ 25'$, azim. $69^\circ 39'$, decl. $20^\circ 2'$: required the Hour-angle.

Az. $69^\circ 39'$	sin. 9.97201
Alt. $40^\circ 25'$	cos. 9.88158
Decl. $20^\circ 2'$	sec. 0.02711
Hour-angle, $3^\circ 17' 48''$	sin. 9.88070

b. To find the Hour-angle on the Prime Vertical.

618. *By Inspection.* See Table 29.

619. *By Computation.* Add together the log. cot. of the lat. and the log. tan. of the decl.; the sum (rejecting tens) is the log. cos. of the Hour-angle.

Ex. Lat. $31^\circ 28'$, Decl. $14^\circ 11'$ of the same name: find the Hour-angle of a celestial body on the prime vertical.

Lat. $31^\circ 28'$	cot. 0.21325
Decl. $14^\circ 11'$	tan. 9.40266
Hour-angle, $4^\circ 22' 26''$	cos. 9.61591

6. To find the Hour-angle at Rising or Setting.

620. *By Inspection.* When the decl. is less than 24° , take out of

* This angle A is the angle at the body contained between its pol. dist. and sen. dist., or the angle P A Z, fig. p. 162.

Table 26 the *time of setting*; this is the Hour-angle required. It is called also the Semidiurnal arc.

When the decl. exceeds 24° , see No. 621, or Explan. of Table 5.

621. *By Computation.* Add together the log. tangents of the lat. and decl.; the sum (rejecting tens) is the log. cos. of the Hour-angle at rising or setting, or its supplement.

When the lat. and declin. are of the *same* name, take the *supplement*; when of *contrary* names the Hour-angle is that taken out.

Ex. 1. Lat. $48^{\circ} 42'$ N. decl. $20^{\circ} 11'$ N.:
find the Hour-angle at rising or setting.

Lat. $48^{\circ} 42'$	tan.	$0^{\circ} 0562$
Decl. $20^{\circ} 11'$	tan.	$9^{\circ} 5654$
<hr/>		
$4^h 21^m 4^s$	cos.	$9^{\circ} 6216$
<hr/>		
Hour-ANGLE, $7^h 38^m 56^s$		

Ex. 2. Lat. $31^{\circ} 10'$ N. decl. $11^{\circ} 14'$ S.:
find the Hour-angle at rising or setting.

Lat. $31^{\circ} 10'$	tan.	$9^{\circ} 7816$
Decl. $11^{\circ} 14'$	tan.	$9^{\circ} 2980$
<hr/>		
Hour-ANGLE, $5^h 32^m 24^s$ cos. $9^{\circ} 0796$		

7. To find the Hour-angle near the Meridian, by the observed Change of Altitude.

622. The alts. must be on the same side of the meridian.

Correct the diff. of alts. and the interval by adding the correction in the following table:—

TIME.				ARC.							
12 ^m	0 ^s	43 ^m	15 ^s	1° 0'	0'	0"	6° 15'	0' 44"	10° 45'	3' 51"	
13	1	44	16	30	0	1	30	0 50	11 0	4 7	
20	1	45	18	2 0	0	2	45	0 56	15	4 25	
23	2	46	19	30	0	3	7 0	1 3	30	4 43	
25	3	47	20	45	0	4	15	1 10	45	5 2	
26	3	48	21	3 0	0	5	30	1 17	12 0	5 21	
28	4	49	23	15	0	6	45	1 25	15	5 42	
30	5	50	24	30	0	8	8 0	1 34	30	6 4	
32	6	51	26	45	0	10	15	1 44	45	6 27	
33	7	52	27	4 0	0	12	30	1 53	13 0	6 51	
34	7	53	29	15	0	14	45	2 3	15	7 15	
35	8	54	31	30	0	17	9 0	2 14	30	7 41	
36	9	55	32	45	0	20	15	2 26	45	8 8	
37	10	56	34	5 0	0	23	30	2 39	14 0	8 36	
38	11	57	36	15	0	27	45	2 52	15	9 4	
40	12	58	38	30	0	31	10 0	3 16	30	9 34	
41	13	59	40	45	0	35	15	3 20	45	10 5	
42	14	60	42	6 0	0	39	30	3 34	15 0	10 37	

Add together the log. sin. of the diff. alts. (thus corrected), the log. cosec. of the interval (corrected), the log. sec. of the declin., the log. cos. of the mean of the two alts., and the log. sec. of the lat.: the sum (rejecting tens) is the log. sine of the hour-angle at the middle of the interval, nearly.

To find the hour-angle for the alt. *nearest* the meridian, *subtract* half the interval from this hour-angle. To find the hour-angle for the alt. *furthest* from the meridian, *add* half the interval to the hour-angle found.

Note.—If the alts. are not measured, the merid. alt., deduced from the lat. by acc., figures No. 452, may be employed, recollecting that this alt. is always somewhat *too great*, except when below the pole, when it is too small.

Ex. 1. Lat. $51^{\circ} 30' N.$, decl. $22^{\circ} 20' N.$, obtained tr. alts. $60^{\circ} 27' 52''$ and $60^{\circ} 34' 35''$, or diff. alts. $6' 43''$ at an interval of 4^m : find the Hour-angle at the time of the alt. nearest the meridian.

D. Alt. $6' 43''$ (no corr.)	sin.	7.2909
Int. 4^m (do)	cosec.	1.7581
Decl. $22^{\circ} 20'$	s. c.	0.0339
Mean Alt. $60 31$	cos.	9.6921
Lat. $51 30$	sec.	0.2058
Mid. Int. $0^h 21^m 58^s$	sin.	3.9808
$\frac{1}{2}$ Int. -2		
Hour-Angle $19 58$		

Ex. 2. Lat $40^{\circ} N.$, decl. $20^{\circ} N.$, obtained tr. alts. $69^{\circ} 58'$ and $67^{\circ} 0'$, or diff. alt. $2^{\circ} 58'$, with interv. of $47^m 39^s$: find the Hour-angle at the time of the alt. furthest from the meridian.

D. Alt. $2^{\circ} 58' 0''$	Int.	$47^m 39^s$
Corr. $+5$	Corr.	$+21$
$2 58 5$		$48 0$
D. Alt. $2^{\circ} 58' 5''$	sin.	8.7142
Int. $48^m 0^s$	cosec.	0.6821
Decl. $20^{\circ} 0'$	sec.	0.0270
Mean Alt. $68 29$	cos.	9.5644
Lat. $40 0$	sec.	0.1157
Mid. T. $29^m 10^s$	sin.	9.1034
$\frac{1}{2}$ Int. $+23 49$		
Hour-Angle $52 59$	(only 2° too small.)	

The degree of dependence is chiefly to be estimated from the effect produced by a small change in the diff. alts.

For finding by an easy operation the apparent local time from an observed altitude, Davis's "Chronometer" Tables (J. D. Potter, London, 10s. 6d.) will be found of service; they also make clear the effect and direction of any small error in the observer's latitude.

V. TIMES OF CERTAIN PHENOMENA.

1. Time of Passing the Meridian.

[1.] Meridian Passage of the Sun.

623. The *Apparent Time* of the sun's meridian passage is $0^h 0^m 0^s$ except below the pole, when it is $12^h 0^m 0^s$.

624. To find the *Mean Time* of the meridian passage:—

Take the Eq. of T. from page I. of the Nautical Almanac, or from Table 62; reduce it for the long. as the Green. Date. Then, if the reduced Eq. of T. is *additive* to A.T., it is the time P.M. of the sun's meridian passage. If the Eq. of T. be *subtractive* from A.T., *subtract* it from 12^h : the remainder is the M.T. of passage.

Ex. 1. March 31st, 1902, long. $140^{\circ} W.$: find Mean Time of Sun's meridian passage.

Eq. T. 31st,	$+4^m 28.3$
32d,	$+4 10.1$
Daily Var.	18.2

Long. $9^h 20^m$, var. 18.2	-7.0
	$4 28.3$

Red. Eq. T. add to A.T. $4 21.3$

M.T. or M. Pass. $12^h 4^m 21.3$.

Ex. 2. Dec. 1st, 1902, long. $93^{\circ} E.$: find Mean Time of Sun's meridian passage.

Green. Date, Nov, 30 ^d	$17^h 48^m$
Eq. T. 30th,	$-11^m 29.1$
31st,	$-11 7.3$

Daily Var.	21.8
$17^h 48^m$, var. 21.8	-16.4

Red. Eq. T. $-11 12.7$

M.T. or Pass. $11^h 48^m 47.3$.

[2.] Meridian Passage of a Star.

625. To find the *Apparent Time* of a star's meridian passage:—*At Sea*.—See Table 27, and Explanation.

Or, from the R.A. of the star (adding 24^h if necessary) subtract the R.A. of the sun at noon, Nautical Almanac, page I., or deduced from Sidereal Time in Table 61 (*see* Note, page 211); the remainder is the A.T. required.

Ex. 1. Oct. 17, 1902: find A.T. of the Mer. Pass. of Sirius.

By Table 27.

Oct. 1st,	$18^h 14^m$
For 17 days	$\underline{59}$
Mer. Pass.	$\underline{17 15} \text{ P.M.}$
Or 18th,	$5 13 \text{ A.M.}$

By Sun's R.A.

R.A. Sirius	$6^h 41^m$
Oct. 17th. \odot 's R.A.	$\underline{13 26}$
Mer. Pass.	$\underline{17 15} \text{ P.M.}$
Or 18th,	$5 13 \text{ A.M.}$

Ex. 2. Find the A.T. of the Mer. Pass. of α Urs. Maj., above and below the Pole, on Feb. 11th, 1902.

Ans. $1^h 19^m \text{ A.M.}$; $1^h 17^m \text{ P.M.}$

Ex. 3. Find A.T. of Mer. Pass. of Capella on July 20th, 1902.

Ans. $9^h 11^m \text{ A.M.}$; $9^h 9^m \text{ P.M.}$

626. To find the *Mean Time* of a star's meridian passage:—

Accurately.—From the R.A. of the star (increased, if necessary, by 24^h) subtract the Sid. T. at mean noon on the day: the remainder is the approx. M.T. of transit.

Subtract from this the Retardation, Table 24.

In W. Long. *subtract* from this result the Acceleration for the Long. In E. Long. *add* the Acceleration.

The result is the M.T. of meridian passage.

Ex. 1. Jan. 1st, 1902, long. $1^{\circ} 25' \text{ W.}$: find M.T. of Mer. Pass. of Aldebaran.

R.A. Aldebaran	$4^h 30^m 17.8$
Sid. T. Mean Noon	$\underline{-18 40 48.5}$
	$9 49 29.3$
Ret. $9^h 1^m 28.7$	
$49^m 8.0$	$\underline{-1 36.8}$
$29^{\circ} .1$	
$1^{\circ} 25' \text{ W., or } 5^m 40^s$	$\underline{-9}$
M.T. Mer. Pass.	$9 47 51.6$

Ex. 2. May 22d, 1902, long. $131^{\circ} 11' \text{ E.}$: find M.T. of Mer. Pass. of Spica.

R.A. Spica	$13^h 20^m 4.6$
Sid. T. Mean Noon	$\underline{3 56 42.6}$
	$9 23 22.0$
Ret. $9^h 23^m 22^s$	$\underline{-1 32.6}$
	$9 21 49.4$
Long. $8^h 44^m 44^s$	$\underline{+1 26.2}$
M.T. of Pass.	$9 23 15.6$

Ex. 3. Aug. 8th, 1902, long. $90^{\circ} 15' \text{ E.}$: find M.T. of Mer. Pass. of Altair.

Ans. $10^h 41^m 3.4$.

Ex. 4. Feb. 1st, 1902, long. $172^{\circ} 34' \text{ W.}$: find M.T. of Mer. Pass. of Regulus.

Ans. $13^h 16^m 5.0$.

Ex. 5. Oct. 1st, 1902, long. $90^{\circ} 48' \text{ E.}$: find M.T. Mer. Pass. of Markab.

Ans. $10^h 22^m 6.1$.

[3.] Meridian Passage of the Moon.

627. This is required only approximately.

In W. Long. take from the Naut. Almanac the diff. between the Mer. Pass. of the proposed day and the next (given in *mean time* to 0^m 1). In E. Long. take the diff. between that for the proposed day and the day before. The diff. is the daily variation.

Take from Table 28 the correction corresponding to the daily variation and longitude. In W. Long. add this corr. to the time of

mer. pass. on the given day; in E. Long. subtract it; the result is the time required.

When one mer. pass. has 23^h , and the next 0^h , 24^h must be added to the latter in finding the Daily Variation.

Ex. 1. Find Mer. Pass. of C Jan. 16th, 1878, long. 46° W.

Mer. Pass. 16th,	$10^h 9^m 1$
17th,	$11 11 6$
Daily Var.	$1 2 5$
46° W. var. $62^m 5$	$+ 7 6$
	$10 9 1$
MER. PASS.	$10 16 7$
Jan. 16th, at $10^h 16^m 7$ P.M.	

Ex. 2. July 24th, 1878, long. 130° E.; find the Mer. Pass. of the Moon.

Mer. Pass.	$23^h 19^m 1^s$
	$22 18 14 1$
Daily Var.	$47 7$
130° E. var. $47^m 7$	$- 16 8$
	$23 19 1 8$
MER. PASS.	$23 18 45 0$
July 24th, at $6^h 45^m$ A.M.	

628. As the lunar day, or the interval between the moon's mer. pass. and her return to the same meridian again, exceeds 24 hours or a mean solar day, an entire day passes at certain intervals without a lunar transit. For ex. :—

The moon passes the meridian on the 3d, at $23^h 50^m$, or 10^m before the noon concluding the 3d. The lunar day being, at least, 40^m longer than the mean solar day, the moon will not have reached the merid. by about 30^m at next noon, or that concluding the 4th; she accordingly passes the merid. about $0^h 30^m$ on the 5th, having skipped the 4th altogether

There may thus be no mer. pass. on the day proposed.*

Ex. 1. March 3rd, 1878, long. 21° W.; find the Moon's Mer. Pass.

Mer. Pass.	$2^d 23^h 44^m 1$
	$3 * *$
	$4 0 23 5$
Daily Var.	$39 4$
Long. 21° W. var. $39^m 4$	$+ 2 0$
	$2 23 44 1$
MER. PASS.	$2 23 46 1$
March 3rd at $11^h 46^m 1$ A.M.	

Ex. 2. October 26th, 1878, long. 38° E.; find the Moon's Mer. Pass.

Mer. Pass.	$26^d 0^h 7^m 7$
	$25 * *$
	$24 23 10 2$
Daily Var.	$57 5$
Long. 38° E. var. $57^m 5$	$5 7$
	$26 0 7 7$
MER. PASS.	$26 0 2 0$
October 26th, at $0^h 2^m$ P.M.	

In W. Long., when the sum of the corr. and mer. pass. exceeds 24^h , subtract 24^h , and reckon the time on the next day. In E. long., when the corr. exceeds the time of mer. pass., add 24^h to the latter, and reckon the time on the day before.

Ex. 1. Suppose Ex. 1 above, the Long. to be 170° W.

Long. 170° W. var. $39^m 4$	$+ 18^m 0$
	$2^d 23 44 1$
MER. PASS.	$3 0 2 1$
March 3rd, at $0^h 2^m 1$ P.M.	

Ex. 2. Suppose Ex. 2 above, the long to be 90° E.

Long. 90° E. var. $57^m 5$	$- 13^m 7$
	$26^d 0^h 7 7$
MER. PASS.	$25 23 54$
October 26th, at $11^h 54^m$ A.M.	

* This occurs about the time of conjunction with the sun, and the day skipped is marked \odot in the Nautical Almanac. In like manner a day is skipped at the lower transit (under the pole) at opposition.

[4.] *Meridian Passage of a Planet.*

629. The meridian passages of the planets, like those of the moon, are given in the Nautical Almanac to 0^m.1 of mean time.

A planet, of which the R.A. increases faster than that of the sun, skips a day at conjunction, as observed in No. 628 of the moon. On the other hand, when the R.A. diminishes, or the motion of the planet among the stars is reversed, two transits occur within the limits of the mean solar day.

As the greatest daily variation of meridian passage of Venus amounts to 6^m only, the mer. passages of the planets may be taken at once from the Nautical Almanac for all practical purposes.

2. *Time of Passage of the Prime Vertical.*[1.] *Of the Sun.*

630. *Approximately.* Find the Hour-angle by Table 29: this is the App. Time, approximately, of the afternoon passage; the supplement to 12^h is the Approx. Appar. Time of the forenoon passage.

Ex. 1. Jan. 20th, 1878, lat. 39° S.: find the times of the Sun's Passage of the Prime Vertical.

Jan. 20th, Sun's Decl. 20° 5' S., Table 29, lat. 39° and decl. 20°, give Hour-angle 4^h 13^m. The A.T. of the W. transit is 4^h 13^m P.M., that of the E. is 12^h - 4^h 13^m, or 7^h 47^m A.M.

Ex. 2. June 20th, 1878, lat. 55° N.: find the A.M. and P.M. transits of the Prime Vertical.

Lat. 55° decl. 23° 27' N., or 23½°, Hour-angle 4^h 52^m, which is P.M. transit: the other passage is at 7^h 8^m A.M.

631. *Accurately.* Having found the Approx. App. Time as above (No. 630), apply to it the long. in time; this gives the Green. Date in App. Time.

To this reduce the sun's declination, and compute the hour-angle by No. 619.

Ex. 1. Aug. 29th, 1878, required the App. Time of Passage P.M. at Tenby, in lat. 51° 40' 20" N., long. 4° 41' W.

Lat. 51½° decl. 9½° } Table 29 gives } 4° 41' W. } Green. Date, 29th, } Decl. 29th, 9° 19' 33" N. } 30th, 8° 58' 6" N. }	5 ^h 30 ^m + 19 5 49 9 19 33.8 N. 8 58 6.1 N.
	21 27.7 0485 5 49 6155 5 12 6640 9 19 33.8
Red. Decl	9 14 21.8 N.

	Parts for'
51° 40' 20" cot.	9.898010 - 86
9 14 22 tan.	9.211018 + 295
	9.109028
	+ 209
	Cos. 9.109237
	PASS. P. VERTICAL, 5 ^h 30 ^m 27"

Ex. 2. May 13th, 1878, find the Time of Passage A.M. at South Shields, lat. 55° 0' 50" N., long. 1° 25' W.

Green. Date, May 12^d 10^h 0^m
Red. Declin. 18° 22' 16" N.
APP. TIME PASS. 6^h 53^m 45^s A.M.

[2.] *Of a Star.*

632. Find the A.T. of meridian passage. When the time of the east transit is required, subtract the Hour-angle (Table 29) from

this A.T. (increased if necessary by 24^h); for the time of *west.* transit, add the Hour-angle.

Ex. 1. Find the Times of Eastern and Western Transits of Prime Vertical of Aldbaran at So. Shields, on Jan. 1st, 1878.

App. Time Mer. Pass. Tab. 27 $9^h 41^m$
Decl. 16° lat. 55° $- 5 14$

APP. TIME OF E. TRANSIT, 4 27 P.M.

$9^h 41^m$
 $5 14$
 $14 55$

W. TRANSIT OF 2D, 2 55 A.M.

Ex. 2. July 11th, 1878, lat. $51^\circ 30'$ N.: find Times of E. and W. Transits of Prime Vertical of α Lyræ.

Ans. APP. T. OF PASS. E. $7^h 50^m$ P.M.; W. $2^h 30^m$ A.M.

Ex. 3. Dec. 4th, 1878, lat. $40^\circ 10'$ S.: find Times of E. and W. Transits of Prime Vertical of Antares.

Ans. APP. T. OF PASS. E. $8^h 1^m$ A.M.; W. $3^h 17^m$ P.M.

Ex. 4. Aug. 17th, 1878, lat. $56^\circ 3'$ N.: find Time of E. Transit of Prime Vertical of Altair.

Ans. APP. T. OF PASS. E. $4^h 22^m$ P.M.

[3.] Of the Moon.

633. *Approximately.* Proceed as for a star, using M.T. for A.T., because the time of her mer. pass. is given in M.T.

634. *More Accurately.* Find the approximate time as for a star; find the Green. Date, and reduce to it the declination. Find the Hour-angle by No. 619. This Hour-angle, with the correct time of mer. passage, gives the time more nearly. Correct the declination and repeat the computation. For extreme precision, a correction would be required for the oblateness of the earth.

[4.] Of a Planet.

635. Find the M.T. of the Meridian Passage of the planet, in the Nautical Almanac, and apply the Hour-angle as directed for a star; the result is in M.T.

Ex. 1. Jan. 19th, 1878, lat. $54^\circ 33'$ S.: find the time of W. Transit of Prime Vertical of Venus.

M.T. Mer. Pass. 19th } $2^h 39^m$
page 274 N.A.

Lat 54° S., Decl. 6° S. $+ 5 42$

M.T. OF PASS. 8 21 P.M.

Ex. 2. Aug. 9th, 1878, lat. $49^\circ 56'$ S.: find the Time of E. Transit of Prime Vertical of Jupiter.

M.T. Mer. Pass. 9th } $10^h 57^m$
page 254 N.A.

Lat. 50° S., Decl. 21° S. $- 4 10$

M.T. OF PASS. 0 47 P.M.

3 Times of Rising and Setting.

These are required approximately only.

[1.] Of the Sun.

636. See Table 26, and Explanation.

[2.] Of a Star, the Moon, or a Planet.

637. Find the A.T. (or M.T., according as required) of the meridian passage, No. 625, &c. Find the Hour-angle at rising or setting, No. 620.

To find the time of *rising*, subtract this Hour-angle from the time of mer. passage (increased if necessary by 24^h); to find the Time of *setting*, add them together, rejecting 24^h if the sum exceed 24^h .

Ex. Jan. 1st, 1878, lat. 50° N. : find A.T. of rising and setting of Aldebaran.

A.T. Mer. Pass., Table 27 $9^h 41^m$
 55° N., Decl. 16° N. $-7 \frac{37}{100}$
 A.T. OF RISING $2 \ 4 \text{ P.M.}$

A.T. Mer. Pass. $9^h 41^m$
 $7 \frac{37}{100}$
 A.T. OF SETTING $17 \ 18$
 Or at $5^h 18^m$ A.M. on 2d.

638. To find the change in the time of apparent rising or setting due to the horizontal refraction and the height of the spectator, No. 446 (1) and (2).

By Computation. Add together the log. secants of the latitude and declination, the log. cosec. of the hour-angle at rising or setting, and the log. sine of $34' + \text{depr.}$ for the height of the eye, Table 8; the sum is the log. sine of the portion of time required, nearly.

Ex. 1. Find the difference of times of Sunset to an eye at the level of the sea, and on the summit of the Peak of Teneriffe, on May 4th.

Hour-angle at setting (No. 621), $6^h 35^m 52^s$.

Lat. $28^{\circ} 16'$ sec. $0^{\circ} 0551$

Decl. $16 \ 10$ sec. $0^{\circ} 0175$

H.-Ang. $6^h 36^m$ cosec. $0^{\circ} 0054$

$34' + 117' = 2^{\circ} 31'$ sin. $8^{\circ} 6426$

TIME REQ. $12^m 3^s$ sin. $8^{\circ} 7206$

Ex. 2. Lat. $28^{\circ} 16' \text{ N.}$, declin. $16^{\circ} 10' \text{ N.}$: required the difference in the times of Sunset to the eye at the level of the sea, and elevated 16 feet above it.

Hour-angle at level of the sea, $6^h 35^m 52^s$.

Lat. sec. $0^{\circ} 0551$

Decl. sec. $0^{\circ} 0175$

Hour-angle cosec. $0^{\circ} 0054$

$34' + 4'$ sin. $8^{\circ} 0435$

TIME REQ. $3^m 2^s$ sin. $8^{\circ} 1215$

This process is very nearly correct in low latitudes, but in high latitudes, where the body, instead of rapidly passing the horizon, partly skims along it, the result, when the dip is large, is too small.

Thus, for the above depression, $117'$, in lat. 50° (and declination above), the time comes out $17^m 23^s$; it should be $17^m 38^s$; and in lat. 60° , the result, $24^m 17^s$, should be $25^m 4^s$.

639. More accurately, find the Hour-angle of the given celestial body when below the horizon $34' + \text{depression}$ due to the observer's height, by No. 642; this is effected by using $34' + \text{depr.}$, instead of 18° . The Diff. between this Hour-angle and that found by No. 621 is the portion of time required.*

640. Since the moon's parallax exceeds the refraction, Nos. 433 and 436, she always appears below her true place, and therefore rises later, and sets earlier, than a more distant body of the same declination. Accordingly, in the preceding rule we must use, instead of $34'$, the diff. between the hor. par. and $34'$, and the difference instead of the sum of the latter and the Depression. If the depression is the greater, the rising is accelerated, otherwise retarded. For the hor. par. $61'$, these effects neutralise each other at the height of 650 feet; for $53'$, at 320 feet; that is, to the eye placed at these heights the moon in these cases rises and sets nearly at her true time.

* In strictness, however, some correction (subtractive) is due to the refraction itself when the body is seen at a considerable depression.

4. Times of the Beginning and End of Twilight.

641. *By Inspection.* See Explanation of Table 5.

642. *By Computation.* Add together 18° , the lat., and the pol. dist., take half the sum, and from it subtract 18° , or the upper term.

Add together the log. sec. of the lat., the log. cosec. of the pol. dist., the log. sine of the half sum, and the log. cos. of the remainder; the sum (rejecting tens) is the log. sine square of the sun's hour-angle when 18° below the horizon.

This Hour-angle is the App. time of the *end* of twilight, P.M.; and the *supplement* to 12^h is the App. time of the *beginning*, A.M.

NOTE.—The declination at noon, and 4, or even 3, places in the logs. are enough for this purpose.

Ex. 1. April 22d, 1878, lat. $51^\circ 46' N.$:
find the Beginning and End of Twilight.

Const.	$18^\circ 0'$		
Lat.	$51^\circ 46'$	sec.	$0^\circ 20' 84''$
P.D.	$77^\circ 45'$	cosec.	$0^\circ 01' 00''$
	<u>147 31</u>		
	$73^\circ 45'$	sine	$9^\circ 9' 823$
	$55^\circ 45'$	cosine	$9^\circ 7' 504$
END	$9^h 28^m$	sine sq.	$9^\circ 9' 511$
BEG.	$2^h 32$		

Ex. 2. Dec. 21st, 1878, lat. $55^\circ 1' N.$:
find the Beginning and End of Twilight.

Const.	$18^\circ 0'$		
Lat.	$55^\circ 1'$	sec.	$0^\circ 24' 16''$
P.D.	$113^\circ 27'$	cosec.	$0^\circ 03' 74''$
	<u>186 28</u>		
	$93^\circ 14'$	sine	$9^\circ 9' 993$
	$75^\circ 14'$	cosine	$9^\circ 4' 063$
END	$5^h 52^m$	sine sq.	$9^\circ 6' 846$
BEG.	$6^h 8$		

Ex. 3. March 3d, 1878, lat. $60^\circ 47' S.$ Twilight begins $2^h 8^m$ A.M., ends $9^h 52^m$ P.M.

Ex. 4. Jan. 2d, 1878, lat. $70^\circ 1' N.$, Twilight begins, $6^h 42^m$ A.M., ends $5^h 18^m$ P.M., the sun not appearing above the horizon.

643. The *duration* of twilight, or the interval between the beginning of twilight and the sun's rising, or between sunset and darkness, is found by taking the differences of these times. Thus, in Ex. 1, it is $9^h 28^m - 7^h 3^m$ (setting, Table 26), or $4^h 57^m$ (rising) $- 2^h 32^m$, which is $2^h 25^m$. In Ex. 2, it is $5^h 52^m - 3^h 27^m$, or $2^h 25^m$.

The shortest duration is at the equator, when the sun moves through 18° in $1^h 12^m$; at the poles it continues several months.

When the lat. (of the same name with the decl.) exceeds the compl. of $18^\circ + \text{decl.}$, the sun is less than 18° below the horizon at midnight, or twilight lasts all night, as for ex. with lat. $58^\circ N.$, decl. $21^\circ N.$

VI. ALTITUDES.

1. Correction of the Observed Altitudes.

644. The corrections necessary to reduce an altitude observed from the sea-horizon with a sextant or circle to the *true* altitude, consists of the Index Correction, the Dip, the Correction of Altitude (or the joint effect of refraction and parallax, No. 438,) and, in certain cases, the Semidiameter.

When one of the instruments, No. 522 or 523 is used, the Dip is omitted; the constant correction should be applied the first thing.

645. The *apparent* alt. is deduced from the *observed* alt. by applying all the above corrections except refraction and parallax.

646. When the altitude is less than 10° , the mean refraction in Table 31 may be in error more than $1'$, and should be corrected by Tables 32 and 33 if a barometer and thermometer are at hand. For precision, this is necessary in all cases.

[1.] To Correct the Sun's Altitude.

647. *At Sea.* Apply the Ind. Corr.; subtract the dip corresponding to the height of the eye, Table 30; subtract the refraction for this alt., Table 31, to the nearest minute.

When the *lower* limb is observed, *add* $16'$ to this reduced alt.; when the *upper* limb is observed, *subtract* $16'$; the result is the true or corrected alt. of the sun's centre.

Ex. 1. Obs. alt. of \odot $28^\circ 54'$, ind. corr. $+3'$, height of the eye 16 feet: required True Alt. of the centre.

Obs. Alt.	$28^\circ 54'$
Ind. Corr.	$+ 3$
	<hr/>
	$28\ 57$
Dip	$- 4$
	<hr/>
	$28\ 53$
Refr. (for 29°)	$- 2$
	<hr/>
	$28\ 51$
Semid. (<i>low. l.</i>)	$+ 16$
	<hr/>
TRUE ALT.	$29\ 7$

Ex. 2. Obs. alt. of \odot $42^\circ 11'$, ind. corr. $-17'$, height of the eye 30 feet: required True Alt. of the centre.

Obs. Alt.	$42^\circ 11'$
Ind. Corr.	$- 17$
	<hr/>
	$41\ 54$
Dip	$- 5$
	<hr/>
	$41\ 49$
Refr. (for 42°)	$- 1$
	<hr/>
	$41\ 48$
Semid. (<i>upper l.</i>)	$- 16$
	<hr/>
TRUE ALT.	$41\ 32$

Ex. 3. Obs. alt. \odot $10^\circ 4'$, ind. corr. $+2'$, height of eye 18 feet: required the True Alt. of Sun's centre. TRUE ALT. $10^\circ 13$

Ex. 4. Obs. alt. \odot $42^\circ 11'$, ind. corr. $-17'$, height of eye 30 feet: required the True Alt. of the centre. TRUE ALT. $41^\circ 32'$.

648. In the open sea, where an error of $2'$ or $3'$ of lat., and a corresponding error of long., are of no great consequence, the corr. of alt. for the sun (when the *lower* limb is observed), may be taken from Table 38, in which it is given to the nearest minute.

Ex. 1. (Ex. 1 above.)

Obs. Alt. \odot	$28^\circ 54$
Ind. Corr.	$+ 3$
	<hr/>
	$28\ 57$
Ht. 16 f., Alt. 29° Corr.	$+ 11$
	<hr/>
TRUE ALT.	$29\ 8$

Ex. 2. (Ex. 3 above.)

Obs. Alt. \odot	$10^\circ 4$
Ind. Corr.	$+ 2$
	<hr/>
	$10\ 6$
Ht. 18 f., Alt. 10° , Corr.	$+ 7$
	<hr/>
TRUE ALT.	$10\ 13$

If the upper limb has been observed, proceed as above, and deduct $32'$.

Ex. Obs. Alt. \odot $88^\circ 40'$, Ht. of Eye 30 f., Ind. Corr. -5 , TRUE ALT. $88^\circ 14'$.

649. *Accurately.* Apply the ind. corr. and (at sea) the dip; correct the refr. by Tables 32, 33; take the semid. and parallax from the Nautical Almanac; and subtract the parallax in alt., Table 34.

Minute accuracy in alt. at sea can rarely be worth the trouble

restowed upon it, from the uncertain state of the sea-horizon. The examples, No. 651, will serve, supplying the dip.

650. When the altitude of either limb of the sun is observed, and the altitude of the other limb (which will appear the same in the instrument) is observed from the opposite point of the horizon (No. 535), take half the diff. of these angles and *add* to it the correction of alt.; the sum is the true zen. dist.

Ex. 1. Obs. Alt. ☉ S. $63^{\circ} 49' 20''$,
☉ N. $115^{\circ} 46' 20''$: required the true Zenith Distance.

☉ N.	$115^{\circ} 46' 20''$
S.	$63 \ 49 \ 20$
	$2) 51 \ 57 \ 0$
App. Zen. Dist.	$25 \ 58 \ 30$
Refr.	$+ 29$
TRUE Z. Dist.	$25 \ 58 \ 59 \text{ N.}$

Ex. 2. Obs. Alt. ☉ N. $81^{\circ} 59' 0''$,
☉ S. $97^{\circ} 40' 30''$: required the true Zenith Distance.

☉ S.	$97^{\circ} 40' 30''$
N.	$81 \ 59 \ 0$
	$2) 15 \ 41 \ 30$
App. Zen. Dist.	$7 \ 50 \ 45$
Refr.	$+ 8$
TRUE Z. Dist.	$7 \ 50 \ 53 \text{ S.}$

651. *On Shore.* When the alt. is observed from the quicksilver, apply the ind. corr. at once; halve the result, and proceed as in No. 649, omitting the dip.

Ex. 1. Jan. 1st, 1878, alt. ☉ in the quicksilver $17^{\circ} 24' 0''$, ind. corr. $- 4' 50''$, bar. 30.6 inch, therm. 44° : find the True Alt.

	Obs. Alt. ☉	$17^{\circ} 24' 0''$
	Ind. Corr.	$- 4 \ 50$
		$2) 17 \ 19 \ 10$
M. Refr.	$6' \ 6''$	$8 \ 39 \ 35$
Therm.	$+ 5$	
Bar.	$+ 7$	
	$6 \ 18$	
Par.	$- 9$	
Corr. of Alt.	$6 \ 9$	$- 6 \ 9$
		$8 \ 33 \ 26$
		Semid. $+ 16 \ 18$
		TRUE ALT. $8 \ 49 \ 44$

Ex. 2. July 1st, 1878, alt. ☉ $60^{\circ} 11' 40''$, ind. corr. $+ 2' 35''$, bar. 29.2 , therm. 76° , find the True Alt.

	Obs. Alt. ☉	$60^{\circ} 11' 40''$
	Ind. Corr.	$+ 2 \ 35$
		$2) 60 \ 14 \ 15$
M. Refr.	$1' \ 41''$	$30 \ 7 \ 7$
Therm.	$- 5$	
Bar.	$- 3$	
	$1 \ 33$	
Par.	$- 7$	
Corr. of Alt.	$1 \ 26$	$- 1 \ 26$
		$29 \ 49 \ 55$
		Semid. $- 15 \ 46$
		TRUE ALT. $29 \ 49 \ 55$

Ex. 3. May 3d, 1878, obs. alt. ☉ in the quicksilver $116^{\circ} 14' 0''$, ind. corr. $+ 2' 0''$, bar. 29.2 , therm. 58° : required the True Altitude. TRUE ALT. $58^{\circ} 23' 23''$.

Ex. 4. July 9th, 1878, obs. alt. ☉ in the quicksilver $120^{\circ} 17' 50''$, ind. corr. $+ 54''$, bar. 29.8 , therm. 62° : required the True Altitude. TRUE ALT. $60^{\circ} 24' 39''$.

[2.] To Correct a Star or a Planet's Altitude.

652. *At Sea.* Apply the index corr.; subtract the dip and refraction.

Ex. 1. Obs. alt. of a star $10^{\circ} 28'$, ind. corr. $+ 2'$, height of eye 16 feet: required the True Alt.

	$10^{\circ} 28'$
	$+ 2$
	$10 \ 30$
Dip 4 and Refr. 5'	$- 9$
TRUE ALT.	$10 \ 21$

Ex. 2. Obs. alt. of a star $46^{\circ} 12'$, ind. corr. $- 3'$, height of eye 16 feet: required the True Alt.

	$46^{\circ} 12'$
	$- 3$
	$46 \ 9$
Sub. 3', 4', and 1'	$- 8$
TRUE ALT.	$46 \ 4$

Or, having corrected for index error, subtract the corr. in Table 38.

Ex. 3. Obs. alt. of the planet Venus $30^{\circ} 14'$, ind. corr. $+ 3'$, height of eye 12 feet: required the True Alt.

Obs. Alt.	$30^{\circ} 14'$
Ind. Corr. $+ 3'$	$- 2$
Table 38, $- 5'$	
TRUE ALT.	$30^{\circ} 12'$

Ex. 4. Obs. alt. of the planet Mars $78^{\circ} 57'$, ind. corr. $+ 7'$, height of eye 30 feet: required the True Alt.

Obs. Alt.	$78^{\circ} 57'$
Ind. Corr. $+ 7'$	$+ 2$
Table 38, $- 5'$	
TRUE ALT.	$78^{\circ} 59'$

653. *Accurately.* Proceed as for the sun, No. 649, omitting semidiameter.

A star's corr. of alt. is the refraction alone, No. 438, p. 147.

For a planet, find the hor. par. in the Nautical Almanac; find the par. in alt. corresponding, in Table 45, and deduct it from the refraction.

Ex. 1. Obs. Alt. of Sirius in the quicksilver $37^{\circ} 9' 35''$, ind. corr. $- 7' 30''$, bar. 30.2 , therm. 42° : required the True Alt.

* Obs. Alt.	$37^{\circ} 9' 35''$
Ind. Corr.	$- 7' 30''$
2) $37^{\circ} 2' 5''$	
	$18^{\circ} 31' 2''$
M. Refr. $2' 53''$	$- 2^{\circ} 57'$
Therm. $+ 3$	
Bar. $+ 1$	
Corr. $- 2^{\circ} 57'$	
TRUE ALT.	$18^{\circ} 28' 5''$

Ex. 2. Obs. alt. of α Polaris in the mercury $102^{\circ} 38' 30''$, ind. corr. $+ 1' 30''$, therm. 62° , bar. 30 inch.

* Obs. Alt.	$102^{\circ} 38' 30''$
Ind. Corr.	$+ 1' 30''$
2) $102^{\circ} 40' 0''$	
	$51^{\circ} 20' 0''$
M. Refr. $0' 46'' \cdot 8$	$- 0^{\circ} 46'$
Therm. $- 1^{\circ} 2'$	
Corr. $0^{\circ} 45' \cdot 6$	
TRUE ALT.	$51^{\circ} 19' 14''$

Ex. 3. Dec. 21st, 1878, obs. alt. Venus in the quicksilver $116^{\circ} 48' 40''$, ind. corr. $+ 1' 40''$, bar. 29.8, therm. 62° : required the True Alt.

Venus' H.P., p. 277, N.A. $5' \cdot 2$	
Obs. Alt.	$116^{\circ} 48' 40''$
Ind. Corr.	$+ 1' 40''$
2) $116^{\circ} 15' 20''$	
	$58^{\circ} 25' 10''$
M. Refr. $0' 35'' \cdot 9$	$- 0^{\circ} 32'$
Therm. $- 0' 9''$	
Bar. $- 0' 2''$	
Par. $0^{\circ} 34' 8''$	
Corr. of Alt. $0^{\circ} 32' 2''$	
TRUE ALT.	$58^{\circ} 24' 38''$

Ex. 4. Feb. 6th, 1878, obs. alt. Mars in the quicksilver, $41^{\circ} 49' 30''$, ind. corr. $+ 1' 20''$, bar. 29.2, therm. 58° : required the True Alt.

Mars' H.P., p. 278, N.A. $5' \cdot 5$	
Obs. Alt.	$41^{\circ} 49' 30''$
Ind. Corr.	$+ 1' 20''$
2) $41^{\circ} 50' 50''$	
	$20^{\circ} 55' 25''$
M. Refr. $2' 31'' \cdot 8$	$- 2^{\circ} 20'$
Therm. $- 3$	
Bar. $- 4$	
Par. $2^{\circ} 24' \cdot 8$	
Corr. of Alt. $2^{\circ} 19' \cdot 7$	
TRUE ALT.	$20^{\circ} 53' 5''$

[3.] To Correct the Moon's Altitude.

654. *At Sea.* Find the Green. Date roughly, and take out of the Nautical Almanac the hor. par. and semid. to the nearest noon or midnight.

Apply the ind. corr. to the alt., subtract the dip; when the *lower* limb is observed, *add* the semid.; when the *upper* limb is observed, *subtract* it; the result is the *app. alt.* of the centre.

With the A. alt. and hor. par. find, in Table 39, the moon's corr. of alt., which *add*. The result is the true or corrected alt. of the moon's centre, approximately.

Ex. 1.* May 13th, 1878, long. 51° W., at $3^h 42^m$ P.M., obs. alt., $\Downarrow 37^{\circ} 10'$, ind. corr. + $3'$, height of eye 14 feet: required the True Alt.

The Gr. Date is 13th, $12^h 10^m$, H.P. at midnight $60'$, semid. $16'$.

Ind. Corr.	+ $3'$	\Downarrow	$37^{\circ} 10'$
Dip	- 4		+ 15
Semid.	+ 16		
			<hr/>
			$37^{\circ} 25'$, H.P. $60'$
			$\quad \quad \quad + 46$
			<hr/>
			TRUE ALT. $38^{\circ} 11'$

Ex. 2. Sept. 18th, 1878, long. 160° E., at 2^h A.M., obs. alt. $\Downarrow 61^{\circ} 20'$, height of eye 16 feet, ind. corr. - $3'$: find the True Alt.

The Gr. Date 17th, $3^h 20^m$, H.P. at noon, $55'$, semid. $15'$.

Ind. Corr.	- $3'$	\Downarrow	$61^{\circ} 20'$
Dip	- 4		- 28
Semid.	- 15		
			<hr/>
			$60^{\circ} 58'$
			$\quad \quad \quad + 26$
			<hr/>
			TRUE ALT. $61^{\circ} 24'$

Ex. 3. Jan. 3d, 1878, long. 159° E., at $9^h 10^m$ P.M. $\Downarrow 85^{\circ} 42'$, height of eye 20 feet, ind. corr. + $3'$ TRUE ALT. $86^{\circ} 1'$.

Ex. 4. July 5th, 1878, long. 172° W., at 3^h A.M. $\int 14^{\circ} 28'$, ind. corr. $0'$, height of eye 18 feet. TRUE ALT. $15^{\circ} 1'$.

655. *Accurately.* (1.) Reduce the hor. par. to the Gr. Date, and find the semid. Table 40. Reduce the par. by Table 41, and augment the semid. Table 42.

(2.) Take out the refraction for the limb observed, correct it for barom. and therm.; subtract this corrected refraction from the alt. and apply the augmented semidiameter.

(3.) To the log. sec. of the alt. thus reduced add the prop. log. of the reduced hor. parallax; the sum is the prop. log. of the parallax in alt. This par. added to the reduced alt. gives the true alt. of the centre.

As, however, the degree of precision obtained by these precepts will rarely be required, we shall, in the following example, employ Table 39.

Ex. 1. July 30th, 1878. lat. 42° S., long. $42^{\circ} 13'$ W., at $5^h 24^m 38^s$ M.T. obs. alt. $\Downarrow 36^{\circ} 39' 50''$, ind. corr. + $2' 17''$, height of eye 22 feet; therm. 72° , bar. 29.1 : required the True Alt.

The Gr. Date, 30th, $8^h 13^m 30^s$	
H.P. 30th, Noon	$59^{\circ} 55' 6''$
30th, Midn.	$60^{\circ} 6' 2''$
12-hourly Var.	$+ 10' 6''$
$8^h 14^m$, var. $10'' 6''$	$+ 7' 2''$
	<hr/>
	$59^{\circ} 55' 6''$
Equat. H.P.	$60^{\circ} 6' 8''$
Red. for Lat.	$- 5' 2''$
Red. H.P.	$59^{\circ} 5' 6''$
Semid. corresp. to $59^{\circ} 58'$	$16' 21''$
Augment.	$10''$
Aug. Semid.	$16' 31''$

Obs. Alt.	$36^{\circ} 39' 50''$
Ind. Corr. + $2' 17''$	$\left. \begin{array}{l} \\ \end{array} \right\} - 2' 13''$
Dip. - $4' 30''$	
	<hr/>
Aug. Semid.	$36^{\circ} 37' 37''$
	$+ 16' 31''$
	<hr/>
	$36^{\circ} 54' 8''$
$36^{\circ} 50'$ and $59'$	$45' 56''$
4	- 2
58"	$+ 47''$
	<hr/>
	$46' 41''$
Therm. 72° , sub. $3''$	$\left. \begin{array}{l} \\ \end{array} \right\} + 5''$
Bar. 29.1 sub. $2''$	
	<hr/>
	$46' 46'' + 46' 46''$
	<hr/>
	TRUE ALT. $37^{\circ} 40' 54''$

656. When the moon is referred to the opposite point of the horizon, No. 535, half the diff. of the alt. and its supplement is the zenith distance of the illuminated limb, to which the augmented

* The examples being given merely in illustration of the rules, no regard has been paid to the visibility of the moon at the time and place specified.

semid. is to be applied the contrary way to that directed for the alt. In certain cases both limbs can thus be observed, No. 540, and the semidiameter avoided.

2. To Reduce the True to the Apparent Altitude.

[1.] *For the Sun, a Star, or a Planet.*

657. Take out the refraction to the true alt. as if for the app. alt., correcting it, when necessary, for the barom. and therm.; *subtract* the parallax in alt., add the remainder to the true alt., and *subtract* the correction in Table 43.

[2.] *For the Moon.*

658. Find her corr. of alt. for the true alt., as if for the app. alt., and apply the corr., Table 44.

Ex.	☉'s Hor. Par. 59', True Alt.	48° 41' 12"
	48° 41', and 59', - 38' 6"	
	Corr. Table 44, - 28 }	- 38 34
	APP. ALT.	48 2 38

659. To reduce the app. alt. to the observed alt. for a particular instrument and given height of the eye, apply the ind. corr. the *opposite* way, and *add* the dip.

3. Reduction of Two Altitudes to an Intermediate Point of Time.

660. Two altitudes observed at periods of time not distant, afford, by simple p. oportion, the altitude at an intermediate time.

(1.) Find the interval between the time of the 1st alt. and the time proposed, and call it the partial interval.

(2.) To the prop. log. of the partial interval add the ar. co. prop. log. of the whole interval, and the prop. log. of the diff. of alts.; the sum is the prop. log. of the change of alt. in the partial interval.

(3.) When the 1st alt. is the *lesser*, *add* this change; when it is the *greater*, *subtract* the change.

Ex. 1. At 10^h 18^m 4^s by watch, obs. an alt. 54° 56'; at 10^h 29^m 11^s obs. a second alt. 55° 12'; required the Alt. at 10^h 23^m 6^s.

Alt. 54° 56'	time 10 ^h 18 ^m 4 ^s	} 5 ^m 2 ^s	pr. log. 1.553
	10 23 6		
	10 29 11		ar. co. p. log. 8.791
Diff. 55 12			pr. log. 1.051
16			pr. log. 1.395
Change of Alt. 7'			
54 56			
ALT. req. 55 3			

Ex. 2. At 12^h 57^m 24^s by watch, obs. an alt. 39° 2'; and at 1^h 8^m 18^s obs. a second alt. 36° 42'; required the Alt. at 1^h 1^m 29^s. Change of Alt. - 0° 53', and ALT. req. 38° 9'.

Ex. 3. At 1^h 58^m 36^s by watch, obs. an alt. 47° 33', and at 1^h 5^m 47^s obs. a second alt. 47° 52'; required the Alt. at 1^h 1^m 29^s. Change of Alt. + 8', and ALT. req. 47° 41'.

The altitude thus deduced differs from the true alt. by a proportional part of the 2d diff. of alt. upon the interval, No. 558. The

method serves very well when the azimuth is large, or the object 60° or more from the meridian, or less if the interval be small; but in cases near the meridian the result will be sensibly in error, unless the interval is very small. The error arising from the neglect of the 2d diff. will be less as the intermediate time is nearer to the beginning or end of the interval.

4. *Reduction of an Altitude to another Place of Observation.*

661. The run of the ship in the interval between the taking of the two altitudes which constitute certain observations, renders it necessary to reduce one to the place of the other.

When the ship approaches the sun directly she raises him 1 for each mile of distance made good. When the sun bears obliquely (as for ex. 3 points) from the course made good, if we consider the angle between this last course and the sun's bearing (or 3 points) as a course, the space by which the ship approaches the sun is the D. Lat. corresponding to her Dist. made good.*

When the sun's bearing is at right angles to the course made good, the ship neither approaches nor recedes from him; when the bearing is abaft this line, she drops the sun.

When it is required to reduce an alt. observed at 1 o'clock (for ex.) to what it would have been if observed at the place where the ship is at 2 o'clock, the ship having approached the sun, we have merely to add to the alt. observed at 1 o'clock the portion of space or arc by which the ship would have raised the sun in 1^h, if he had preserved his bearing at 1 o'clock unaltered. Hence the following rules.

To reduce the 1st alt. to the second place of observation.

(1.) Take the diff. between the bearing of the body at the first observation and the ship's course, as a Course, and the dist. run as a Distance; the D. Lat. corresponding is the reduction for run.

(2.) When this course is *less* than 90° or 8 points, *add* the red. to the first alt.; when the said course exceeds 90° or 8 points, *subtract* the red.; the result is the alt. reduced to what it would have been if observed at the second place of the spectator.

If the ship does not preserve the same course, the course made good must be employed.

As it is *difference* only of bearing or azimuth that enters into this question, the variation (supposed the same at both observations) is not considered; but if the ship's course changes, the deviation should be attended to.

Ex. 1. Observed the sun's alt., the sun bearing S.E. by E. $\frac{1}{4}$ E., the course E. by N. $\frac{1}{4}$ N. (by compass). Sailed for 1^h 15^m at the rate of $7\frac{1}{2}$ knots: required the Reduction of the Alt. for Run.

From S.E. by E. $\frac{1}{4}$ E. to E. is $2\frac{1}{2}$ pts.; from E. to E. by N. $\frac{1}{4}$ N. is $1\frac{1}{2}$ pts. The course $4\frac{1}{2}$ points, and dist. 9.4, give D. Lat. $6'3$ the Reduction to be added to the Alt.

* As the distance is described upon a spherical surface, in strictness a correction is necessary; also the dist. made good on the spiral rhumb should be reduced to that on a great circle; but these refinements are generally inconsistent with the rude data of the question.

Ex. 2. Sun South, alt. $55^{\circ} 30' 5''$, course E. by N., rate 6.8 knots, interval 12^m: reduce the Alt. for the Run.

The suppl. of 9 pts., or 7 pts., and dist. 1.4, give D. Lat. $0^{\circ} 27'$, or $0^{\circ} 3'$, which *subtracted* from $55^{\circ} 30' 5''$, gives $55^{\circ} 30' 2''$, the ALT. required.

Ex. 3. Obs. sun's alt., sun bearing N.E. $\frac{1}{2}$ E., course N.W. $\frac{1}{2}$ N., sailed for 36^m 10^s at the rate of 10.2 knots: required the Reduction for Run. The REDUCTION is $0^{\circ} 0'$.

Ex. 4. Obs. a star's alt. $37^{\circ} 18' 40''$, bearing S.E. by E. $\frac{1}{2}$ E., course N.W. by W. $\frac{1}{2}$ W., rate 5.8 knots, interval 2^h 24^m: reduce the Alt. for Run.

The REDUCTION is $13' 9''$ to *sub.*; the ALT. $37^{\circ} 4' 8''$.

When the course at the 1st observation is *directly towards* the sun, the dist. run in the interval is the correction, and is to be *added* to the 1st alt.; when *directly from* the sun, to be *subtracted*.

Ex. Obs. sun's alt. $29^{\circ} 7' 30''$, bearing E.S.E., course E.S.E., rate 5.4 knots, interval 3^h 6^m: reduce the Alt. for Run.

The REDUCTION is $16' 7''$ to *add*; the ALT. $29^{\circ} 24' 2''$.

662. To reduce the 2d alt. to the first place of observation.

Take the bearing at the last observation; find the reduction of the alt. as above, and apply it to the 2d alt. the contrary way to that directed in (2) above.

Ex. 1. Observed the sun's alt., sailed S.S.W. for 48^m at the rate of $3\frac{1}{2}$ knots, when the 2d alt. was taken, the sun bearing W.S.W.: required the Correction of the Alt. for Run.

From S.S.W. to W.S.W. is 4 pts. The course 4 pts., and Dist. 2.8, give the D. Lat. $2^{\circ} 0'$ to be *subtracted* from the 2d Alt.

Ex. 2. Course N.W. by N., observed the sun's alt. After sailing for 1^h 36^m at 8.2 knots, observed the 2d alt. $39^{\circ} 44'$, the sun bearing E.S.E.

From N.W. by N. to E.S.E. is 13 pts.; then the course 3 pts., and Dist. 13.1, give D. Lat. $10^{\circ} 9'$, which *added* to $39^{\circ} 44'$ gives $39^{\circ} 54' 9''$, the Alt. reduced.

When the course at the 2d observation is *directly towards* the sun, the dist. run is the correction, and is to be *subtracted* from the second alt.; when *directly from* the sun, it is to be *added*.

5. To find the Altitude.

[1.] On the Meridian.

663. For the sun, the moon, or a planet, find the time of Mer. Pass., No. 623, &c., and reduce the declin., No. 579, &c. Find the colat. When the lat. and decl. are of the same name take the sum of the colat. and decl.; when of different names, their diff.; the result is the mer. alt. If the sum exceeds 90° take its complement.

Below the Pole. Find the pol. dist., and subtract it from the latitude.

[2.] On the Prime Vertical.

664. *By Inspection.* See Table 29, and Explan. of Table 5.

665. *By Computation.* (1.) Find the approx. time of Passage, No. 630; to this reduce the declin., in the case of the sun, moon, or a planet

(2.) Add together the log. sine of the declin., and the log. cosec. of the lat.; the sum is the log. sine of the true alt. required.

Ex. 1. Ju'y 12th, 1872, lat. $51^{\circ} 48' N.$, long. $4^{\circ} 56' W.$: find the Sun's Alt. on the Prime Vertical, W.

Table 29, Lat. 52° , Decl. 22° , } Hour-angle, or App. Time)	$4^h 46^m$
Long. $4^{\circ} 56' W.$	$+ 20$
Green. Date 12th,	$\frac{5}{6}$
⊙ Decl. 12th,	$21^{\circ} 58' N.$
13th,	$21^{\circ} 50' N.$
Daily Var.	$\frac{8}{8}$

Daily Var. $8'$ and $5'$ gives $2'$, whence

Red. Decl. is $21^{\circ} 56'$	
Decl. $21^{\circ} 56'$	sine $9^{\circ} 57272$
Lat. $51^{\circ} 48'$	cosec. $0^{\circ} 10166$
ALT. $28^{\circ} 23'$	sine $9^{\circ} 67698$

Ex. 2. Lat. $50^{\circ} 48' N.$: find the Alt. of α Lyrae on the Prime Vert. $W.$

Decl. $38^{\circ} 40'$	sine	$9^{\circ} 79573$
Lat. $50^{\circ} 48'$	cosec	$0^{\circ} 11073$
ALT. $53^{\circ} 44'$	sine	$9^{\circ} 90646$

Ex. 3. Lat. $46^{\circ} 14' N.$: find the Alt. of Capella on the Prime Vertical.

Decl. $45^{\circ} 52'$	sine	$9^{\circ} 85596$
Lat. $46^{\circ} 14'$	cosec.	$0^{\circ} 14136$
ALT. $83^{\circ} 38'$	sine	$9^{\circ} 99738$

[3.] To find the Altitude, the Hour-angle being given.

666. *By Inspection.* See Explan. of Table 5.

667. *By Computation.* Having (in the case of the sun, moon, or planet) found the Gr. Date and the declination.

Take the suppl. of the hour-angle to 12^h ; add together the pol. dist. and colat.

Add together the log. sine square of the suppl. of the hour-angle, and the log. sines of the pol. dist. and colat.; the sum (rejecting tens) is the log. sine square of an auxiliary arc x

Write x under the sum of the pol. dist. and colat. and take the sum and diff., and half the sum and half the diff.

Add together the log. sines of the last two terms; the sum (rejecting tens) is the log. sine square of the zen. dist.

Ex. 1. Lat. $22^{\circ} 15' N.$, decl. $2^{\circ} 49' S.$, hour-angle $2^h 14^m 36^s$: required the Alt. (working to the nearest minute).

Hour-angle	$2^h 14^m 36^s$	
Suppl.	$9^h 45^m 24^s$	sin. sq. $9^{\circ} 96200$
P. Dist.	$92^{\circ} 49'$	sine $9^{\circ} 99947$
Colat.	$67^{\circ} 45'$	sine $9^{\circ} 96639$
Sum	$160^{\circ} 34'$	
Arc x	$133^{\circ} 57'$	sin. sq. $9^{\circ} 92786$
Sum	$294^{\circ} 31'$	
Diff.	$26^{\circ} 37'$	
$\frac{1}{2}$ S.	$147^{\circ} 15'$	sine $9^{\circ} 73318$
$\frac{1}{2}$ D.	$13^{\circ} 18'$	sine $9^{\circ} 36182$
Zen. Dist. $41^{\circ} 19'$		sin. sq. $9^{\circ} 09500$
ALT. $48^{\circ} 41'$		

Ex. 2. Lat. $35^{\circ} 15' N.$, decl. $20^{\circ} 0' N.$, hour-angle $4^h 53^m 19^s$. ALT. $24^{\circ} 41'$.

Ex. 3. Lat. $19^{\circ} 20' S.$, decl. $19^{\circ} 20' S.$, hour-angle $1^h 18^m 10^s$. ALT. $71^{\circ} 35'$.

When the lat. is 0, we may use either N. or S. pol. dist. When the declin. is 0, the pol. dist. is 90° . When both lat. and declin. are 0, the z. d. is the hour-angle converted into arc.

Ex. 1. Lat. 0, decl. $23^{\circ} 27' N.$, hour-angle $4^h 30^m 14^s$. ALT. $20^{\circ} 30'$.

Ex. 2. Lat. $30^{\circ} 0' N.$, decl. 0, hour-angle $3^h 38^m 30^s$. ALT. $30^{\circ} 5'$.

[4.] To find the Altitude, the Azimuth being given.

668. Add together the log. sine of the azim., the log. cosine of the lat., and the log. sec. of the decl.; the sum (rejecting tens) is the log. sine of an angle Λ (see note to No. 616), p. 222.

Under Λ put the azim. reckoned from the elevated pole; take half the sum and half the diff.

Take half the sum of the pol. dist. and colat.

Add together the log. tan. of this half sum, the log. cos. of the half sum of the azim. and Λ , and the log. sec. of their half diff.; the sum (rejecting tens) is the log. tan. of half the zen. dist.

Ex. Lat. $51^{\circ} 30' N.$, decl. $20^{\circ} 2' N.$, azimuth S. $69^{\circ} 39' W.$, that is N. $110^{\circ} 21' W.$; required the Alt.

Az. $69^{\circ} 39'$	sin.	9.97201	Colat.	$38^{\circ} 30'$	
Lat. $51^{\circ} 30'$	cos.	9.79415	P. Dist.	$69^{\circ} 58'$	
Decl. $20^{\circ} 2'$	sec.	0.02711	Su n	$108^{\circ} 28'$	$\frac{1}{2}$ S. $54^{\circ} 14'$
$\Lambda = 38^{\circ} 25'$	sin.	9.79327			$74^{\circ} 23'$
Az. $110^{\circ} 21'$					$35^{\circ} 58'$
Sum $148^{\circ} 46'$	$\frac{1}{2}$ S. $74^{\circ} 23'$				
Diff. $71^{\circ} 56'$	$\frac{1}{2}$ D. $35^{\circ} 58'$				
					$24^{\circ} 47'$
					$\frac{1}{2}$
					Zen. Dist. $49^{\circ} 34'$
					ALT. $40^{\circ} 26'$

For other Examples reverse those in No. 674.

6 To find the Change of Altitude in a Small Interval of Time.

[1.] The Hour-angle and Altitude being given.

669. (1.) When the body is to the E. of the meridian, *subtract* half the interval from the hour-angle; when to the W. of the meridian, *add* half the interval: call the result the reduced hour-angle.

(2.) Add together the log. cosines of the lat. and decl., the log. sine of the red. hour-angle, the log. sec. of the alt. and the log. sine of the interval; the sum (rejecting tens) is the log. sine of the change of alt.*

(3.) When the body is to the E. of the meridian, *add* this change to the alt.; when to the W., *subtract* it: the result is the alt. required.

Ex. 1. Lat. $51^{\circ} 30'$, decl. $22^{\circ} 20'$, true alt. $44^{\circ} 47' 36''$, hour-angle $3^h 0^m 0^s$ to the E. of the meridian: required the Alt. 10^m afterwards.

Hour-angle $3^h 0^m 0^s$ E.	lat. cos.	9.7942
Half-int. $5^m 0^s$	decl. cos.	9.9661
Red.H.ang. $2^m 55^s 0''$	sine	9.8398
$44^{\circ} 47' 36''$	sec.	0.1490
	int. sin.	8.6397
CHANGE $1^m 24^s 1''$	sin.	8.3888
ALT. $46^{\circ} 11' 37''$		

The true alt. is $46^{\circ} 12' 48''$, or the process is here $1' 11''$ in defect.

Ex. 2. Lat. $51^{\circ} 30'$, decl. $22^{\circ} 20'$, true alt. $44^{\circ} 47' 36''$, hour-angle $3^h 0^m 0^s$ to the W.: find the Alt. 20^m afterwards.

$3^h 0^m 0^s$ W.	lat. cos.	9.7942
$+ 10^m 0^s$	decl. cos.	9.9661
$3^h 10^m 0^s$	sine	9.8676
$44^{\circ} 47' 36''$	sec.	0.1490
	int. sine	8.9403
$2^m 59^s 20''$	sin.	8.7172
ALT. $41^{\circ} 48' 16''$		

The true alt. is $41^{\circ} 52' 24''$, or the error is $4' 8''$ in consequence of the length of the interval.

* The prop. logs. may be used for the sines of the small arc and the interval, provided that the arithmetical complements of all the other quantities be employed, and the const. 8.8239 added. The proper logarithm for the purpose is the log. of the small arc or the interval in seconds of arc ("). The inaccuracy attending the use of the sine, instead of its arc, in these computations is insensible, as the sine of $1''$ falls short of its arc by only $0''.2$, the sine of $2''$ by $1''.5$, and that of $3''$ by $2''.9$, or $0''.19$ of time.

The method is more accurate as the object is more nearly E. or W.

The proper alt. to employ in this computation is the middle alt. between those at the beginning and end of the interval; for greater accuracy, therefore, the work should be repeated with a new alt. thus deduced.

[2.] *The Azimuth being given.*

670. *By Inspection.* Multiply the change of alt. in 1^m of time, Table 46, by the interval, both being in min. and decimals.

Ex. Lat. 52°, azim. 72°: find the change in Alt. in 3^m 12^s.

The change of alt. in 1^m is about 8'·7, which multiplied by 3·2 gives 28', the CHANGE required.

671. *By Computation.* Add together the log. sine of the azimuth (reckoned either from N. or S.), the log. cos. of the lat., and the log. sine of the interval of time; the sum (rejecting tens) is the log. sine of the change of altitude.

It is more correct to use the azimuth corresponding to the middle of the interval of time.*

Ex. Lat. 51° 49', azimuth of Arcturus 72°: find the change of Alt. in 3^m 12^s, and also in 2^m 51^s.

Az. 72°	sine 9·9782			9·9782
Lat. 51 49'	cos. 9·7911			9·7911
Int. 3 ^m 12 ^s	sine 8·1450			8·0946
CHANGE req. 28' 13"	sine 7·9143		Int. 2 ^m 51 ^s	7·8639
			CHANGE req. 25' 8"	

672. All bodies on the same or opposite azimuths change their altitudes at the same rate, whatever be their declinations.

VII. AZIMUTHS.

1. *To find the Azimuth, the Altitude being given.*

673. *By Inspection.* See Explanation of Table 5.

674. *By Computation.* Add together the pol. dist., the lat., and the alt., take half the sum,† and take the diff. between this half sum and the pol. dist.

Add together the log. sec. of the lat., the log. sec. of the alt., the log. cosines of the half sum and remainder; the sum (rejecting tens) is the log. sine square of the azimuth,‡ to be reckoned from the S. in N. lat., and from the N. in S. lat.

* The above rules, Nos. 669, &c., relate to the change of the *true* altitude. To compare the change of alt. as shewn by an instrument with the true difference, in a given interval of time, a small correction would, in general, be necessary, on account of the change of refraction, and in the case of the moon, for the change also in her parallax in altitude.

† The learner will observe that in this formula the pol. dist., lat., and alt., occur in the reverse order of that in No. 614, in which last their initials form the word *slp*. The 2d and 3d terms take secants; the last two, cosines.

‡ The angle obtained is the *supplement* of the angle P Z A in fig. 1, p. 162

Ex. 1. Lat. $51^{\circ} 30' N.$, alt. $40^{\circ} 25'$ to the W., decl. $20^{\circ} 2' N.$: required the Azimuth.

Pol. Dist.	$69^{\circ} 58'$	
Lat.	$51^{\circ} 30'$	sec. $0^{\circ} 20585$
Alt.	$40^{\circ} 25'$	sec. $0^{\circ} 11842$
	<u>$161^{\circ} 53'$</u>	
	$80^{\circ} 56\frac{1}{2}'$	cos. $9^{\circ} 19711$
	$10^{\circ} 58\frac{1}{2}'$	cos. $9^{\circ} 79198$

AZIMUTH, S. $69^{\circ} 39' W.$ sin. sq. $9^{\circ} 51336$

Ex. 2. Lat. $40^{\circ} 8' S.$ Decl. $11^{\circ} 0' N.$, alt. $38^{\circ} 11'$ to the Eastward: required the Azim.

P Dist.	$101^{\circ} 0'$	
Lat.	$40^{\circ} 8'$	sec. $0^{\circ} 1106$
Alt.	$38^{\circ} 11'$	sec. $0^{\circ} 1046$
	<u>$179^{\circ} 19'$</u>	
	$89^{\circ} 39\frac{1}{2}'$	cos. $7^{\circ} 7755$
	$11^{\circ} 20\frac{1}{2}'$	cos. $9^{\circ} 9914$

AZIMUTH, N. $11^{\circ} 19' E.$ sin. sq. $7^{\circ} 9881$

When the lat. is 0, if the declin. is N. the azimuth is to be reckoned from the south; if it is S. from the north.

When the declin. is 0, the azimuth is reckoned from the N. in S. lat., and from the S. in N. lat.

Ex. 1. Lat. 0° , decl. $23^{\circ} 27' S.$, alt. $41^{\circ} 2' W.$ AZIM. N. $121^{\circ} 50' W.$, or S. $58^{\circ} 10' W.$

Ex. 2. Lat. $11^{\circ} 12' N.$, decl. 0° , alt. $54^{\circ} 30'$, to the East. AZIM. S. $73^{\circ} 53' E.$

When both the lat. and decl. are 0, the object moves on the prime vertical.

2. To find the Azimuth, the Hour-angle being given.

675. (1.) Take half the sum of the pol. dist. and colat., and half the difference.

(2.) Add together the log. cot. of half the hour-angle, the log. sec. of the half sum, and log. cos. of the half diff.: the sum (rejecting tens) is the log. tan. of half the sum of the azimuth and another angle A.

When the half sum of the pol. dist. and colat. exceeds 90° , take the suppl. of the resulting arc for the half sum required.

To the log. cot. already employed add the log. cosec. of the half sum, and the log. sine of the half diff.; the sum (rejecting tens) is the log. tan. of half the diff. of the same two angles.

(3.) The sum of the resulting half sum and half diff. is the greater of the said two angles; the difference is the lesser.

When the pol. dist. exceeds the colat. the greater of the two angles is the azimuth required; when the pol. dist. is less than the colat., the lesser of the angles is the azimuth required

Ex. 1. Lat. $10^{\circ} 20' N.$, decl. $22^{\circ} 14' S.$, hour-angle $1^h 44^m 17^s$: required the Azimuth.

H. Angle	$1^h 44^m 17^s$		
Half	<u>$0^h 52^m 8^s$</u>	cot. $0^{\circ} 63548$	cot. $3^{\circ} 63548$
P Dist.	$112^{\circ} 14'$		
Colat.	<u>$79^{\circ} 40'$</u>		
Sum	$191^{\circ} 54'$		
Diff.	<u>$32^{\circ} 34'$</u>		
$\frac{1}{2}$ S.	$95^{\circ} 57'$	sec. $0^{\circ} 98439$	cosec. $0^{\circ} 00235$
$\frac{1}{2}$ D.	$16^{\circ} 17'$	cos. $0^{\circ} 98222$	sin. $9^{\circ} 44776$
	$88^{\circ} 34'$	tan. $1^{\circ} 60209$	$50^{\circ} 37'$ tan. $0^{\circ} 08559$
	<u>$91^{\circ} 26'$</u> (suppl.)		
	<u>$50^{\circ} 37'$</u>		

Sum N. $142^{\circ} 3' W.$ AZIMUTH (p. dist. exceeds col.)

Diff. $40^{\circ} 49'$ the other Angle, or A.

Ex. 2. Lat. $47^{\circ} 11' S.$, decl. $11^{\circ} 18' S.$, hour-angle $5^h 11^m 20^s$: the Azimuth $91^{\circ} 6'$, the other angle, or A, $43^{\circ} 52'$.

Ex. 3. Lat. $13^{\circ} 52' N.$, decl. $46^{\circ} 8' N.$, hour-angle $1^h 21^m 11^s$ E. of Mer.

AZIM. $33^{\circ} 49\frac{1}{2}' W.$

3. To find the Azimuth, the Hour-angle and Altitude being given.

676. Add together the log. sine of the pol. dist. (or log. cos. of the declin.), the log. sine of the hour-angle, and the log. sec. of the alt.; the sum rejecting tens is the log. sine of the azimuth.

Ex. 1. Hour-angle $1^h 19^m 19^s$, alt. $58^\circ 40'$, pol. dist. $104^\circ 24'$: required the Azimuth.

Pol. Dist. sin.	9.9861
Hour-angle sine	9.5305
Alt. sec.	0.2840
AZIM. $39^\circ 11'$ sin.	9.8006

Ex. 2. Hour-angle $0^h 46^m 39^s$, alt. $63^\circ 0'$, decl. $14^\circ 24'$ (N. or S.): required the Azimuth.

Decl. cos.	9.9861
Hour-angle sin.	9.3057
Alt. sec.	0.3430
AZIM. $25^\circ 33'$ sin.	9.6348

This method cannot shew whether the body is to the N. or S. of the prime vertical; for this purpose see No. 673, &c.

4. To find the Azimuth, not far from the Meridian, by the observed change of Altitude in a small Interval of Time.

677. *By Inspection.* Divide the given change of alt. by the interval, in min. and decimals; the quotient is the change of alt. in 1^m .

With this change and the lat. enter Table 46, and take out the azimuth, which corresponds approximately to the middle of the interval.

Ex. Lat. 35° ; the change of alt. in $20^m 12^s$ is $59'$: find the Azimuth.

59 divided by 20.2 gives 2.9 , the change of alt. in 1^m , which gives the AZIM. about 14° .

678. *By Computation.* Add together the log. sine of the change of alt., the log. cosec. of the interval, and the log. sec. of the lat.; the sum is the log. sine of the azimuth about the middle of the interval.

Ex. 1. Lat. $51^\circ 26'$; in $5^m 20^s$ observed $22'$ change of alt.: required the Azimuth.

D. Alt. $22'$	sine	7.8061
Int. $5^m 20^s$	cosec.	1.6332
Lat. $51^\circ 26'$	sec.	0.2052
AZIM. $26^\circ 10'$	sine	9.6445

At about 3^m after the 1st observation.

Ex. 2. Lat. $34^\circ 40'$; in $20^m 12^s$ observed $59' 6''$ change of alt.: required the Azimuth.

D. Alt. $59' 6''$	sine	8.2353
Int. $20^m 12^s$	cosec.	1.0554
Lat. $34^\circ 40'$	sec.	0.0849
AZIM. $13^\circ 44'$	sine	9.3756

At about 10^m after the 1st observation.

679. This method will sometimes be useful, as for determining the variation, but it must be employed with caution; the interval should not be very small, the body should not be far from the meridian, and both alts. must of course be observed on the same side.

The degree of dependance is easily estimated by changing the diff. of alts. by the amount of probable error, as about $1'$ or $2'$: Thus, $1'$ error of diff. alts. produces in Ex. 1 an error of $1^\circ\frac{1}{4}$, while in Ex. 2 it produces an error of only $14'$. *

* The work of finding the Azimuth is much lessened by the use of suitable tables. Burdwood and Davis's Azimuth tables and Star Azimuth tables extend from the equator to 60° latitude, and are published in a convenient form by J. D. Potter, 145 Minories, London, E. Such tables are indispensable for the navigation of iron ships. See also Lecky's "Wrinkles," for stars.

CHAPTER V.

FINDING THE LATITUDE.

- I. BY THE MERIDIAN ALTITUDE. II. BY THE REDUCTION TO THE MERIDIAN. III. BY DOUBLE ALTITUDE OF THE SAME BODY. IV. BY DOUBLE ALTITUDE OF DIFFERENT BODIES. V. BY THE ALTITUDE OF THE POLE STAR.*

680. The pole remains always in the same absolute fixed position from whatever point of the earth's surface it is viewed; its altitude at any particular place is, therefore, always the same. The position of the equator, which is 90° from the pole, is also always the same at the same place, and is determined by reference to the celestial bodies, whose declinations are measured from it. The latitude of the place may, therefore, be determined directly by observation, and independently of the latitude of any other place.

When the body observed is on the meridian (at which time its altitude ceases to change) the time is not noted; but if it is not on the meridian, either the absolute time must be given, or a second altitude must be obtained after a measured interval.

I. BY THE MERIDIAN ALTITUDE.

681. The simplest, and in general the most satisfactory, method of determining the latitude, is by observation of the altitude of a celestial body when on the meridian of the place.†

* The several methods of latitude which are given in this work under the heads enumerated above, and which may be considered as distinct methods, of which the solution depends on circumstances as elsewhere described, amount to eight. The seaman, who will remember the adage, "lead, latitude, and look-out," scarcely needs to be reminded that the latitude is often the only element necessary,—that headlands on vast tracts of coast are approached, and numerous passages or channels taken, by reference to latitude alone,—and that the time, and therefore the longitude itself, depends on the latitude. In these days, also, when such great and continued velocity is attained, in steam-vessels, increased facilities are demanded for determining the place of the ship from time to time; the seaman accordingly should be furnished with a method of finding the latitude (provided it be convenient and satisfactory) adapted to every occasion that may present itself by day and by night.

† The manner of deducing the latitude from the mer. alt. and declin. is fully described in No. 452.

1 *Meridian Altitude of the Sun.*

682. *The Observation.* When the sun is near the meridian, continue to observe the altitude till it is found to decrease; the *greatest* alt. reached is the mer. alt.*

In latitudes above $66\frac{1}{4}$ the sun, being above the horizon the whole 24 hours during part of the summer months, may often be observed below the pole at midnight; in this case the *smallest* altitude is the mer. alt.†

When accuracy is required, note the barom. and therm.

683. *The Computation. At Sea.* (1.) Take the sun's decl. from the Nautical Almanac, page I., or Table 60, for the noon of the day, and reduce it by Table 19 for the longitude by account.

(2.) Correct the alt. for index error, dip, semidiameter, and refraction, No. 647; subtract it from 90° , the remainder is the zenith distance.

(3.) When the observer is to the N. of the sun, call the zen. dist. *north*; when he is to the S. of the sun, call it *south*.

When the zen. dist. and decl. are of the *same* name, take their *sum*; when of *contrary* names, take their *difference*: the result is the lat.

When the decl. and zen. dist. are of the *same* name, the lat. is also of *that* name; when the decl. and zen. dist. are of *different* names, the lat. takes the name of the *greater*.‡

Ex. 1. May 3d, 1902, long. 38° W.,
obs. Mer. Alt. \odot $56^\circ 10'$ to the southward,
ind. corr. $+2'$, height of eye 20 feet: re-
quired the Latitude.

Decl. 3d, Table 60,	$15^\circ 29'$ N.
Corr. for 38° W.	$+2$
Red. Declin.	$15\ 31$ N.
Obs. Alt. \odot	$56^\circ 10$
Ind. Corr. $+2'$	-2
Dip -4	
App. Alt. \odot	$56\ 8$
Refr. $-1'$	
Semid. $+16$	$+15$
True Alt.	$56\ 23$
Zen. Dist.	$33\ 37$
LATITUDE	$33\ 37$ N. $49\ 8$ N.

Ex. 2. July 4th, 1902, long. 101° E.;
obs. Mer. Alt. \odot $81^\circ 59'$ bearing north,
ind. corr. 0, height of eye, 16 feet: required
the Latitude.

Decl. 4th,	$22^\circ 57'$ N.
Corr. for 101° E.	$+1$
Red. Declin.	$22\ 58$ N.
Obs. Alt.	$81^\circ 59$
Table 38,	$+12$
True Alt.	$82\ 11$
Zen. Dist.	$7\ 49$
LATITUDE	$7\ 49$ S. $15\ 9$ N.

* At sea it is usual to keep advancing the index till the sun has *dipped*, but it is better to take separate altitudes.

† Since the sun, moon, and planets, change their declinations, the mer. alt. is not always the *maximum* or *minimum* altitude. Near the equator the difference, which is as the tangent of the latitude nearly, is very minute. In lat. 60° the sun's alt. will be maximum, in the extreme case, at half a min. from the meridian, and the altitudes will differ only $0''.4$; in the same latitude these quantities will be, for the moon, $7'$ and $2'$ respectively. As $0''.4$ is inappreciable by ordinary instruments, and as the moon can be employed for approximation only, it is not necessary to tabulate this correction.

‡ A ship, on board which the declination had been applied the wrong way, made the Orkney Islands, in coming from the westward, instead of the Channel. A few years ago a ship bound homewards from Australia round C. Horn got too far to the southward; a similar

When the declin. is 0, the zen. dist. is the latitude; and when the zen. dist. is 0, the declin. is the latitude.

Ex. 3. March 21st, 1902, long. 15° W.; obs. mer. alt. \odot $48^{\circ} 16'$ bearing N., index error $-5'$, eye 16 feet: find the Latitude.

Decl. 21st	$0^{\circ} 1' S.$
Corr. for long. 15° W.	-1
Red. Decl.	$0^{\circ} 0'$
Obs. Alt. \odot	$48^{\circ} 16'$
Index $-5'$	
Semi. -16	
Dip -4	
Ref. -1	
True Alt.	$47^{\circ} 50'$
Zen. Dist.	$42^{\circ} 10' S.$
Decl.	$0^{\circ} 0'$
LATITUDE	$42^{\circ} 10' S.$

Ex. 4. July 13th, 1902, long. 49° W.; obs. mer. alt. \odot $89^{\circ} 44'$ N., index error $+4'$, eye 18 feet: find the Latitude.

Decl. 13th	$21^{\circ} 56' N.$
Corr. for long. 49° W.	-1
Red. Decl.	$21^{\circ} 55' N.$
Obs. Alt. \odot	$89^{\circ} 44'$
Index $+4'$	
Table 38 $+12$	$+16$
True Alt.	$90^{\circ} 0'$
Zen. Dist.	$0^{\circ} 0'$
Decl.	$21^{\circ} 55' N.$
LATITUDE	$21^{\circ} 55' N.$

Ex. 5. March 21st, 1902, long. 60° E., obs. mer. alt. \odot $56^{\circ} 26'$ N., index error $+2'$, eye 20 feet: required the Latitude. Red. decl. $0^{\circ} 5' S.$ True alt. $33^{\circ} 21'$.

LAT. $33^{\circ} 26' S.$

Ex. 6. Aug. 5th, 1902, long. 47° W., obs. mer. alt. \odot $72^{\circ} 47'$ N., index error $+2'$, eye 16 feet. Red. decl. $17^{\circ} 8' N.$ True alt. $73^{\circ} 1'$.

LAT. $0^{\circ} 9' N.$

Ex. 7. March 20th, 1902, long. 90° W., obs. mer. alt. \odot $89^{\circ} 48'$ S., index error $-1'$, eye 12 feet. Red. decl. $0^{\circ} 19' S.$ True alt. 90° .

LAT. $0^{\circ} 19' S.$

Ex. 8. Jan. 1st, 1902, long. 138° W., obs. mer. alt. \odot $89^{\circ} 55'$ S., index error $+2'$, eye 12 feet. Red. decl. $23^{\circ} 3' S.$ True alt. $90^{\circ} 10'$.

LAT. $23^{\circ} 13' S.$

Ex. 9. June 20th, 1902, long. 172° W., obs. mer. alt. \odot $52^{\circ} 18'$ S., index error $-2'$, eye 60 feet (the top). Red. decl. $23^{\circ} 27' N.$ True alt. $52^{\circ} 23'$.

LAT. $61^{\circ} 4' N.$

Ex. 10. Feb. 18th, 1902, long. 71° E., obs. alt. \odot 's centre (by bisecting the cloudy disc, No. 539), $48^{\circ} 22'$ S., eye 18 feet. Decl. $11^{\circ} 55' S.$ True alt. $48^{\circ} 17'$.

LAT. $29^{\circ} 48' N.$

Ex. 11. Dec. 20th, 1902, long. 160° E., obs. mer. alt. \odot $28^{\circ} 18'$ S., above the sea horizon $2\frac{1}{2}$ miles distant, eye 20 feet. Red. decl. $23^{\circ} 25' S.$ True alt. $28^{\circ} 26'$.

LAT. $38^{\circ} 9' N.$

684. When the sun is observed below the pole (at midnight), instead of subtracting the true alt. from 90° , add 90° to it; the lat. will be of the same name as the declin.

Ex. 1. June 5th, 1902, long. 29° E. at 12^h P.M., obs. mer. alt. \odot below the pole $3^{\circ} 38' N.$, ind. corr. $+2'$, height of eye 20 feet: required the Latitude.

Red. Declin. No. 579 (2), $22^{\circ} 31' N.$	
Obs. Alt. \odot	$3^{\circ} 38'$
Ind. Corr. $+2'$	
Dip. -4	
	$3^{\circ} 36'$
Refr. $-13'$	
Semid. $+16$	$+3$
True Alt.	$3^{\circ} 39'$
Supp. Zen. Dist.	$93^{\circ} 39'$
Decl.	$22^{\circ} 31' N.$
LATITUDE	$71^{\circ} 8' N.$

Ex. 2. Nov. 13th, 1902, long. 98° W. at 12^h P.M., obs. mer. alt. \odot below the pole $5^{\circ} 37' S.$, ind. corr. $-2'$, height of eye 30 feet.

Declin. Noon	$17^{\circ} 48' S.$
Corr. for 12 ^h add $8'$	
98° W. add 4	12
Red. Declin.	$18^{\circ} 0' S.$
Obs. Alt.	$5^{\circ} 37'$
Ind. Corr. $-2'$	
Table 38 $+2$	0
True Alt.	$5^{\circ} 37'$
Supp. Zen. Dist.	$95^{\circ} 37'$
Decl.	$18^{\circ} 0' S.$
LATITUDE	$77^{\circ} 37' S.$

blunder was discovered to have been made, but the existence of an error in the latitude was suspected only from the circumstance of the ship being becalmed with ice.

In crossing the meridian of 180° , when the long. changes from W. to E., or from E. to W., care must be taken to change the application of the corr. of the declin. accordingly. The neglect of this precaution has been a fertile source of mistakes.

685. *Accurately.* Reduce the declin. to the nearest second for the long., correct the refraction for the barom. and therm. and add the sun's parallax.

As the sun passes the meridian at 0^h 0^m 0^s App. Time, the Greenwich Date may be deduced in App. Time by means of the long. in time, No. 576 (3). Or it may be taken at once from the chronometer, in which case it will be in Mean Time, as is supposed in Ex. 1, following.

Ex. 1. March 20th, 1878, long. 1° 25' W., obs. mer. alt. ☉ in the mercury 69° 8' 10" bearing S., time by chron. 20^d 0^h 13^m 12^s, index error + 1' 10", bar. 29.5 inches, therm. 40°.

☉'s Decl. 20th	0° 5' 38".7 S.
21st	0 18 2.4 N.
Daily Var.	23 41.1
13 ^m 12 ^s , var. 23' 41"	-12 6
	0 5 38.7 S.
Red. Decl.	0 5 26.1 S.
Obs. Alt.	69° 8' 10"
	+ 1 10
	2)69 9 20
	34 34 40
Ref. -1' 25"	}
Ther. + 2	
Bar. - 1	
	- 1 24
	34 33 16
Semid.	+ 16 5
Par.	+ 7
True Alt.	34 49 28
Zen. Dist.	55 10 32 N.
Decl.	0 5 26 S.
LAT.	55 5 6 N.

Ex. 2. June 20, 1878, long. 26° 5' E., at midnight, obs. mer. alt. ☉ in the quicksilver 26° 26' 20", index 0', bar. 29.8 inches, therm. 34°.

Green. Date, A.T. June	20 ^d 10 ^h 15 ^m 40 ^s
Reduced Decl.	23° 27' 16" N.
Obs. Alt.	26° 26' 20"
	13 13 10
Ref. -4' 4"	}
Ther. + 8	
Bar. - 1	
	- 3 57
	13 9 13
Semidiam.	+ 15 46
Par.	+ 8
True Alt.	13 25 7
Supp. Zen. Dist.	103 25 7
Decl.	23 27 16 N.
LAT.	79 57 51 N.

Ex. 3. July 27th, 1878, long. 2° W., obs. mer. alt. ☉ in the quicksilver 116° 2' 30", zenith N. ind. corr. + 2' 15", bar. 30.0 inch., therm. 60°: required the Latitude.

Green. Date (A.T.), 27^d 0^h 8^m; Red. Decl. 19° 12' 17" N.; True Alt. 57° 46' 4" S. LAT. 51° 26' 13" N.

686. When the altitude of either limb of the sun is observed, and the alt. of the other limb (which will appear the *same* in the instrument) is observed from the opposite point of the horizon (No. 535), take half the diff. of these angles and *add* to it the correction of alt.; the sum is the true zen. dist.

Ex. 1. Aug. 5th, 1878, long. 25° W.	
Obs. Alt. ☉ N.	115° 46'.3
S.	63 49.3
Diff.	51 57
	25 58.5 N.
Corr. of Alt.	+ .4
Zen. Dist.	25 58.9 N.
Red. Decl.	16 56.3 N.
LAT.	42 55.2 N.

Ex. 2. Oct. 20th, 1878, long. 1° W.	
Obs. alt. ☉ N.	105° 5'
S.	74 32.2
Diff.	30 32.8
	15 16.4 N.
Corr. of Alt.	+ .2
Zen. Dist.	15 16.6 N.
Red. Decl.	10 23.9 S.
LAT.	4 52.7 N.

Thus it appears that this observation, which is the most efficient in practice, is also the shortest in computation.

Ex. 3. July 15th, 1878, alt. ☉ N. 93° 58', S. 85° 38', long. 71° W. LAT. 25° 39'.7 N.

Ex. 4. July 4th, 1878, alt. ☉ N. 81° 59', S. 97° 40', long. 83° E. LAT. 15° 3'.7 N.

2. Meridian Altitude of a Star or a Planet.*

687. *The Observation* is the same as for the sun, but it is still more necessary to take separate altitudes of a star in order to avoid straining the eye to perceive its small rise or fall when near the meridian. See No. 542.

688. *The Computation. At Sea.* (1.) Take the decl. either from the Nautical Almanac, or, in the case of a star, from Table 63.

(2.) Correct the alt. for index-error, dip, and refraction, No. 652. Find the zenith dist. and proceed as for the sun.

Ex. 1. May 15th, 1878, obs. mer. alt. of Spica $33^{\circ} 17' S.$ index error $+1' 20''$, eye 50 feet.

Obs. Alt.	$33^{\circ} 17' S.$
Index err.	$+1'$
Dip	-5
Ref.	-1
True Alt.	$33^{\circ} 12' S.$
Zen. Dist.	$56^{\circ} 48' N.$
Star's Decl.	$10^{\circ} 32' S.$
LAT.	$46^{\circ} 16' N.$

Ex. 2. April 6th, 1878, P.M. long. $126^{\circ} W.$, obs. alt. of Mars $49^{\circ} 20' N.$, index corr. $+3'$, eye 16 feet.

In N.A. page 244, the M.T. of mer. pass. of Mars is Aug. 9th 3^h 36^m. The Green. Date is Aug. 9th 12^h 0^m, and the Red. Decl. is $23^{\circ} 39' N.$

Obs. Alt.	$49^{\circ} 20' N.$
Index Corr.	$+3'$
Dip	-4
Ref.	-1
True Alt.	$49^{\circ} 18'$
Zen. Dist.	$40^{\circ} 42' S.$
Red. Decl.	$23^{\circ} 39' N.$
LAT.	$17^{\circ} 3' S.$

Ex. 3. Dec. 21st, 1878, obs. mer. alt. Aldebaran $50^{\circ} 27' N.$; height of eye 20 feet; required the Latitude. LAT. $23^{\circ} 22' S.$

Ex. 4. Jan. 1st, 1878, obs. mer. alt. Sirius $81^{\circ} 13' S.$, ind. corr. $-4'$, height of eye 18 feet; required the Latitude. LAT. $7^{\circ} 38' S.$

Ex. 5. Feb. 18th, 1878, obs. mer. alt. Canopus $37^{\circ} 25' S.$, ind. corr. $+2'$, height of eye 16 feet; required the Latitude. LAT. $0^{\circ} 0'$

Ex. 6. Feb. 1st, 1878, obs. mer. alt. Arcturus $80^{\circ} 12' N.$, ind. corr. $+4'$, height of eye 18 feet; required the Latitude. LAT. $10^{\circ} 1' S.$

Ex. 7. Feb. 18th, 1878, obs. mer. alt. α Lyræ, below the pole, $12^{\circ} 30'$, ind. corr. $+2'$, height of eye 18 feet; required the Latitude. LAT. $63^{\circ} 44' N.$

Ex. 8. Oct. 6th, 1878, long. $87^{\circ} W.$, obs. mer. alt. Mars $57^{\circ} 45' S.$, index corr. $-2'$, height of eye 18 feet. LAT. $30^{\circ} 15' N.$

Ex. 9. July 6th, 1878, long. $178^{\circ} E.$, obs. mer. alt. Jupiter $57^{\circ} 50' S.$, index corr. $+3'$, height of eye 20 feet. LAT. $13^{\circ} 2' N.$

Ex. 10. Jan. 6th, 1878, long. $169^{\circ} W.$, obs. mer. alt. Venus $69^{\circ} 54' S.$, index corr. $-1'$, height of eye 15 feet. LAT. $9^{\circ} 15' N.$

689. *Accurately.* Take the decl. from the Nautical Almanac. For a planet find the Gr. Date, and reduce its hor. par. and decl. Correct the refraction for the thermometer and barometer.

690. Stars which never set at the place may be observed both above and below the pole. In this case the latitude is half the sum of the altitudes corrected for refraction.

691. If two stars are observed on the meridian, on different sides of the zenith, and at equal altitudes, the result is independent of the refraction, unless it changes in the interval of the observations. If the altitudes are not equal, the result involves only the difference of the refractions proper to each.

* Venus may often be observed by daylight, even in high latitudes.

3. Meridian Altitude of the Moon.

692. *The Observation.* The same as for the sun. See No. 540.

693. *The Computation.* At Sea. (1.) Find the Green. Date by means of the time at ship; or, if this time is uncertain several minutes, find the M.T. of the moon's mer. pass., No. 627, &c. Reduce thereto the moon's decl., No. 589, her hor. par., and take the corresponding semid. from Table 40, all to the nearest minute.

(2.) Correct the observed alt., No. 654, and proceed as for the sun, No. 683 (3).

Ex. 1. Nov. 3d, 1878, long $150^{\circ} 15' E.$,
at $7^h 7^m$ P.M. mean time at ship, obs. alt. \Downarrow
 $45^{\circ} 13' S.$, height of eye 16 feet.

M.T.S. Nov.	$3^d \ 7^h \ 7^m$
Long. in time	$-10 \ 1 \ E.$

M.T.G. Nov.	$2 \ 21 \ 6$
-------------	--------------

\Downarrow 's Decl. at 21^h	$14^{\circ} 47' \ 45'' S.$
6^m , var. $119''$	$-1 \ 11$

Red. Decl.	$14 \ 46 \ 34 \ S.$
------------	---------------------

Hor. Par.	$54' \ 50''$
Semid.	$14 \ 58$

Obs. Alt. \Downarrow	$45^{\circ} 13$
------------------------	-----------------

Dip -4	$\}$ $+11$
----------	------------

Semid. $+15$	$\}$
--------------	------

$45^{\circ} 20'$, and H.P. $55'$	$+38$
-----------------------------------	-------

True Alt.	$46 \ 2$
-----------	----------

Zen. Dist.	$43 \ 58 \ N.$
------------	----------------

Decl.	$14 \ 47 \ S.$
-------	----------------

LAT.	$29 \ 11 \ N.$
------	----------------

Ex. 2. May 20th, 1878, A.M. long. $114^{\circ} W.$, obs. mer. alt. \Downarrow $48^{\circ} 48' S.$, height of eye 18 feet.

Moon's Mer. Pass.	$19^d \ 15^h \ 12^m$
Corr. for Long.	$+16$

M.T. Mer. Pass. at ship	$19 \ 15 \ 28$
-------------------------	----------------

Long. in time	$7 \ 36$
---------------	----------

M.T.G. May	$19 \ 23 \ 4$
------------	---------------

\Downarrow 's Decl. at 23^h	$24^{\circ} 34' \ 22'' S.$
---------------------------------	----------------------------

4^m , var. $69''$	-8
---------------------	------

Red. Decl.	$24 \ 34 \ 14 \ S.$
------------	---------------------

Hor. Par.	$56' \ 33''$
-----------	--------------

Semid	$15 \ 26$
-------	-----------

Obs. alt. \Downarrow	$48^{\circ} 48$
------------------------	-----------------

Dip $-4'$	$\}$ -20
-----------	------------

Semid. -16	$\}$
--------------	------

$48^{\circ} 30'$ and H.P. $57'$	$+37$
---------------------------------	-------

True Alt.	$49 \ 5$
-----------	----------

Zen. Dist.	$40 \ 55 \ N.$
------------	----------------

Decl.	$24 \ 34 \ S.$
-------	----------------

LAT.	$16 \ 21 \ N.$
------	----------------

Ex. 3. Dec. 21st, 1878, A.M. long. $149^{\circ} W.$, obs. mer. alt. \Downarrow $84^{\circ} 9' N.$ index corr. $+2'$, height of eye 14 feet.

LAT. $31^{\circ} 14' S.$

Ex. 4. Aug. 10th, 1878, P.M. long. $134^{\circ} E.$, obs. mer. alt. \Downarrow $59^{\circ} 44' N.$ index corr. $-1'$, height of eye 18 feet.

LAT. $53^{\circ} 48' S.$

It will in general be loss of time to work nearer than to minutes, because the moon's declination cannot be found to seconds unless the Greenwich time is known with precision.*

694. When both the upper and lower limbs are well defined, the suppl. of the alt. can be observed, and the precept No. 683 applied. When only one limb can be observed, the semi-diameter must be applied.

695. *Degrees of Dependence.* The error of the resulting lat. is obviously the sum or difference of the errors of alt. and decl. The lat. by the sun at sea may be depended upon within $2'$ or less, that by the moon not so nearly, and the lat. by a single star in a dark night perhaps not within $3'$ or $4'$.

* Also as the moon at certain times changes her declination very rapidly, or $17'$ an hour, her mer. alt. may differ considerably from the maximum alt.; and an interval of several minutes may occur between these two altitudes. See note †, p 244.

Errors of observation or of the instrument may be removed by employing celestial bodies of nearly equal altitudes N. and S. of the zenith.* (See No. 999.)

It may in general be considered that the lat. by mer. alt. is not decisively determined unless alts. on both sides of the zenith have been employed.

II. BY THE REDUCTION TO THE MERIDIAN.

696. When the sky is cloudy, or the weather variable, the sun or any other celestial body, though obscured when exactly on the meridian, frequently appears, for short intervals of time, both before and after the meridian passage.†

When the body is near the meridian, the change of alt. in a small portion of time is very small; and though the altitude near the meridian changes at a different rate in different latitudes, yet the *change of altitude* in a given small interval is not sensibly affected by a change of several miles in the latitude, and therefore it may be computed with tolerable accuracy, even when the lat. by account (which is used in the computation) is considerably in error. If, accordingly, at the time of observing an alt. near the meridian, we know the hour-angle, we may find very nearly, by computation, the difference of alt. by which to reduce the observed alt. to the mer. alt., and which is thence called the *Reduction to the Meridian*.

This method is, in point of simplicity, but little inferior to the meridian altitude, to which it is next in importance; and it particularly demands the attention of seamen, because, when the latitude by observation is left, as it too generally is, to the casualty of obtaining the merid. alt., it is frequently lost for the day.

697. The term "near the meridian" implies a meridian distance limited according to the lat., the decl., and also the degree of precision with which the time is known. The Limits are given in Table 47 See also Explan. of the Table.

698. Since the lat. by acc. is employed in computing the Reduction, it may be necessary, when this lat. has been found to be much in error, to repeat the work.

* Though the lat. by a single star may not be very correct, yet the error will in general be much less than that of the D.R. The altitude of a star also affords a certain check against the mistake of applying the sun's declination the wrong way; and it may be remarked, that a single observation of the kind would have prevented all the delay, wear and tear, and danger incurred in the cases mentioned in the note p. 244, from the ships being so far out of their proper latitudes.

† Capt. Sir Richard Grant remarks that in H.M.S. Cornwallis, alts. of the sun and stars were rarely to be obtained while within the limits of the Gulf Stream, but they had a momentary glimpse of the sun near noon once in two or three days.—Nautical Magazine, 1838, p. 437.

1. *Reduction to the Meridian at Sea.*[1.] *By the Sun.*

699. *The Observation.* When the sun is within the limits in Table 47, observe two or three altitudes,* quickly, noting the times.

When the alts. are not observed very close together, either a separate result should be obtained from each alt. with its corresponding time, or the case should be solved by No. 727.

700. *The Computation.* (1.) Take the mean of the alts. and the mean of the times.

(2.) Find the sun's hour-angle, or the time from noon, thus:

1. When the App. Time has been lately *determined by observation*. If the ship has since made *westing*, *subtract* the diff. long. made good from the A.T. found; if she has made *easting*, *add* the diff. long. to the A.T.: the result is the A.T. required.

2. When the A.T. has *not* been lately determined by observation. Find A.T. by the chron. and the long. by acc., thus: To the G. M. T. (found by applying to the chron. the gain or loss up to the time) reduce the Eq. of T. and apply it to the G. M. T., as directed page II. of the Nautical Almanac, or the *contrary* way to that directed in Table 62: the result is A.T. at Greenwich. In W. long. *subtract* the long. in time from this Gr. T. (increased, if necessary, by 24^h); in E. long., *add* it: the result (rejecting 24^h if it exceed 24^h) is A.T. *at ship*.

When the A.T. of observation is P.M., it is the hour-angle required; when it is A.M., subtract it from 24^h : the rem. is the hour-angle.

If A.T. is near 12^h , subtract it from 12^h ; if it exceed 12^h , reject 12^h : the rem. is the hour-angle from midnight.

Find the sun's decl., No. 579.

(3.) Correct the alt., No. 647.

(4.) Add together the logarithm from Table 70 and the log. sine square of the hour-angle: the sum is the log. sine of the Reduction.

(5.) *Add* the reduction to the true alt., unless the observation is near midnight, when *subtract* it: the result is the mer. alt. at the place where the alt. was observed; and the resulting lat. is the lat. of the ship at the time of observation (not at noon).

Having the mer. alt., proceed by No. 683 (3).

Ex. 1. Aug. 5th, 1826. H.M.S. Leven, lat. by acc. 47° N.; long. by acc. 25° W. at $11^m 48^s$ before noon; obtained true alt. \odot $63^\circ 54'$ to the southward: required the lat. The reduced decl. was $17^\circ 4' N.$

Lat. 47° , decl. 17° (same name)	0.416
$11^m 48^s$ sine sq.	6.821
Red. $0^\circ 6'$ sin.	7.237
$63 \quad 54$	
Mer. alt. $64 \quad 0$	

Mer. alt.	$64^\circ 0'$
Zen. dist.	$26 \quad 0 \quad N.$
Red. decl.	$17 \quad 4 \quad N.$
LAT.	$43 \quad 4 \quad N.$
Repeating the work gives $43^\circ 3'$	

* As more than one altitude would, for greater security, always be obtained when possible, we shall, to avoid repetition, consider the term "altitude" in the subsequent rules and examples, as implying the mean of two or more altitudes corresponding to the mean of the times.

Ex. 2. Lat. $55^{\circ} 6' N.$, \odot 's decl. $20^{\circ} 4' S.$, at $0^h 54^m 12^s P.M.$, sun's true alt. $14^{\circ} 1' S.$ required the Latitude.

The Red. is $0^{\circ} 54'$, mer. alt. $14^{\circ} 55'$, and the LATITUDE $55^{\circ} 1' N.$

Ex. 3. Feb. 23d, 1878, lat. by acc. $40^{\circ} 5' S.$, long. $132^{\circ} E.$, at $11^h 45^m 20^s A.M.$, obs. alt. $\odot 59^{\circ} 40' N.$, index corr. $-2'$, eye 20 feet: find the Latitude.

Red. decl. $9^{\circ} 54' S.$, true alt. $59^{\circ} 49'$, Red. $11'$, LAT. $39^{\circ} 54' S.$

Ex. 4. Dec. 12th, 1878, lat. by acc. $0^{\circ} 0'.$, long. $162^{\circ} W.$, at $0^h 11^m 52^s P.M.$, obs. alt. $\odot 66^{\circ} 34' S.$, index corr. $-5'$, eye 16 feet: required the Latitude.

Red. decl. $23^{\circ} 7' S.$, true alt. $66^{\circ} 41'$, Red. $11'$, LAT. $0^{\circ} 1' N.$

Ex. 5. June 21st, 1878, lat. by acc. $42^{\circ} 18' S.$, long. $53^{\circ} E.$, obs. alt. $\odot 23^{\circ} 41' N.$, index corr. $-1'$, eye 14 feet; time by watch $0^h 50^m 53^s P.M.$, fast on A.T. $14^m 28^s$, diff. long made since $20^{\circ} E.$: find the Latitude.

Red. decl. $23^{\circ} 27' N.$, true alt. $23^{\circ} 50'$, Red. $35'$, LAT. $42^{\circ} 8' S.$

701. When the number of minutes of arc, in the Reduction, exceeds the number of minutes of time from the meridian, it is proper to refer to Table 48, to ascertain if it be necessary to employ the *Second Reduction*.

Ex. 1. (The preceding.) The number of min. in the Reduction, or 6, being less than the number of min. of time, or 11, it is not necessary to refer to the Table.

To Compute the 2d Red. Double the log. sine of the Red.; add to it the log. tan. of the mer. alt. found, and the constant 9.6990: the sum (rejecting tens) is the log. sine of the 2d Red.

This is to be *subtracted* from the 1st Red. (above the Pole), that is applied to the alt. the *contrary way* to that of the 1st Red.

Ex. 2. May 5th, 1878, lat. acc. $5^{\circ} 3' N.$, long. $71^{\circ} 10' E.$; time by watch $5^h 3^m 7^s P.M.$, fast on app. time at ship $4^h 47^m 27^s$: obs. alt. $\odot 77^{\circ} 59' N.$; height of eye 16 feet.

Time by Watch	$5^h 3^m 7^s$	Lat. 5° , Decl. $16\frac{1}{2}^{\circ}$ (same name)	0.992
Fast	$-4 47 27$	$0^h 15^m 40^s$	sin sq. 7.067
A.T.S.	$5 0 15 40$		sin. 8.059
Long. in Time	$-4 44 40$	True Alt.	$78 11$
A.T.G.	$4 19 31 0$		6.118
Decl. $16^{\circ} 1' N.$	Obs. Alt. $77^{\circ} 59'$		$78 50$
Corr. $+14$	Table 38 $+12$		tang. 0.705
Red. Decl. $16 15 N.$	True Alt. $78 11$		const. 9.699
			sin. 6.522
		Mer. Alt.	$78 49$
		Zen. Dist.	$11 11 S.$
		Decl.	$16 15 N.$
		LAT.	$5 4 N.$

Ex. 3. Jan. 6th 1878, A.M., lat. acc. $1^{\circ} 10' N.$, long. $58^{\circ} E.$, at $8^h 4^m 53^s$ by watch, $3^h 36^m 28^s$ slow on A.T., long. made since $23' W.$; obs. alt. $\odot 65^{\circ} 13' S.$, height of eye 16 feet: required the Latitude.

Red. decl. $22^{\circ} 30' S.$, Red. $31'$, 2d Red. $0'$, LAT. $1^{\circ} 34' N$

Ex. 4. Sept. 15th, 1878, lat. acc. $4^{\circ} 58' S.$, long. $110^{\circ} W.$, at $0^h 11^m 19^s P.M.$ A.T. obs. alt. $\odot 81^{\circ} 33' N.$, index error $-2'$, eye 16 feet: find the Latitude.

Red. decl. $2^{\circ} 52' N.$, Red. $30'$, 2d Red. $1'$, LAT. $4^{\circ} 6' S$

702. If a second altitude, some time after the first, do not confirm the lat., the time is probably in error. In such cases the mean latitude is *not* to be taken as the true latitude, because that result which is nearest to the meridian is the best.

If the time only is in error, it will be easy to find, by trial, that time from noon which will make the two results agree; and thus this observation may serve to correct, approximately, the error of the watch. When the interval, however, between the alts. amounts to 6^m or 8^m, the case should be solved as a *Short Double Altitude*, No. 720.

[2.] *By a Star, a Planet, or the Moon.*

703. Compute the hour-angle: this must be done by means of the time at ship, by No. 611 or 612. But in general it will be better to observe the alt. of a star nearly E. or W., and to deduce its hour-angle, as directed in No. 737.

In other respects proceed as above directed. When the decl. exceeds 24°, the log., Table 70, must be computed.

704. *Degree of Dependence.* The error of the result is composed of that of the mer. alt., No. 695, together with that of the computed Red., which latter, when well within the limits of Table 47, will rarely be worth notice.

2. Circummeridional Altitudes.

705. On shore, when the time is accurately known, or even at sea under favourable circumstances, the result of several altitudes may be obtained by a computation which is the same in principle as the preceding, and is of much greater value than that of any single observation on or near the meridian.

[1.] *By the Sun.*

706. *The Observation.* When the sun is within the limits in Table 47, observe altitudes as fast as convenient, noting accurately the times by watch, of which the error on Apparent Time must be known or found as soon as possible afterwards.

When precision is required, note the barometer and thermometer.

707. *The Computation.* (1.) Find the Green. Date for noon at the place, in app. time, and reduce the decl. If the error of the watch is given on M.T., reduce also the Eq. of Time.

(2.) By means of the error of the watch obtain A.T. at each altitude. To these App. Times take out the Reduction in seconds from Table 49. Take the mean of the Reductions.

(3.) Find the mean of the alts., and correct it, No. 649 or 650. If the meridian alt. is not observed nearly, deduce it, No. 663, &c.

(4.) Add together the log. of the mean Reduction, the log. cos. of the lat. by acc., the log. cos. of the decl., and log. sec. of the mer. alt.: the sum is the log. of the Reduction.

(5.) At noon, add the Reduction to the mean alt.; at midnight, subtract it: the result is the mer. alt.

Ex. 1. July 9th, 1836, lat. by acc. $51^{\circ} 49' N.$; long. $0^h 3^m W.$; obs. alts. of the sun's lower limb, near noon, by a sextant.

Times, by Watch.	Double Alt. (C)
$11^h 58^m 21^s$	$120^{\circ} 28' 0''$
0 0 47	120 30 30
0 3 40	120 32 37
0 25 46	120 7 0
0 30 39	119 51 40

At $11^h 55^m 1^s$ by watch
the watch was $2^m 10^s 9$ fast
on M.T., and at $0^h 44^m 51^s$
it was $2^m 8^s 7$ fast.

Ind. corr. + $54''$, barom. 29.8 inches, therm. 66° .

The observation being at noon in long. $0^h 3^m W.$, the Gr. Date is July 9th, $0^h 3^m$, app. time.

The reduced Eq. of T. is $4^m 49^s 4$, subtr. from M.T.; red. decl. $22^{\circ} 21' 11'' N.$

Error on App. T.	App. Times	Reductions	
T. by W. $11^h 55^m 1^s$	$11^h 51^m 21^s$	$146'' 9$	
Fast $2 11$	$11 53 47$	$75 9$	
M. T. $11 52 50$	$11 56 40$	$21 8$	
Eq. of T. $- 4 49$	0 18 46.....	$691 1$	
App. T. $11 48 1$	0 23 39.....	$1097 2$	
T. by watch $11 55 1$		$5) 2032 9$	
W. fast on A.T. $7 0$		$406 6$	$\log \dots \dots \dots 2.6099$
	60° Refr. $33''$		Lat. cos. 9.7911
	Par. -4		Decl. cos. 9.9661
	Mean Corr. 29		M. Alt. sec. 0.3079
Sum of Alts. $601^{\circ} 29' 47''$	Th. 61° , Alt. 60° , $-0'' 9$ } Bar. 29.8 , -0.2 } -1		$472'' 4 \log. \dots \dots \dots 2.6743$
$120 17 57$	True Corr. 28		$472'' = 0^{\circ} 7' 52''$
$+ 54$	$60 25 10$		$60 24 42$
$2) 120 18 51$	True Alt. $60 24 42$		Mer. Alt. $60 32 34$
$60 9 25$			Zen. Dist. $29 27 26 N.$
$+ 15 45$			Declin. $22 21 11 N.$
Mean Alt. $60 25 10$			LAT. $51 48 37 N.$
Approx. Mer. Alt. $60 32$			

708. To compute the 2d Reduction.

Take from Table 50 the 2d Reductions (these will be sensible in the larger hour-angles only), and divide the sum by the whole number of altitudes.

To twice the sum of the three logs. used before (namely, lat., decl., and alt.) add the log. of the mean of the 2d Reductions; the sum is the log. of the 2d Red. required.

Ex. (Ex. 1 preceding.)	$23^m 39^s$	2d R. $2'' 9$	3 logs. 0.0651
	$18 46$	$1 1$	2
		$5) 10$	0.1302
		$0.8 \log.$	9.9031
		2d Red. $1'' 08$	$\log. 0.0333$

Subtracting $1'' 1$ from $7' 52'' 4$ gives the lat. omitting decimals, $51^{\circ} 48' 38''$.

709. When the declin. changes considerably, take the difference between the sums of the Eastern and Western hour-angles, in decimals of an hour; multiply it by the hourly diff. of declin., and divide by the number of altitudes.

When the sun is *approaching* the elevated pole, if the E. sum is the *greater*, add this quotient to the Red.; if the *lesser*, subtract it. When the sun is *receding* from the elevated pole, the *contrary*.

Ex. 2. May 7th, 1847, lat. by acc. $55^{\circ} 1' N.$, long. $0^h 6^m W.$, obs. alt. of sun's alternate limbs in the quicksilver, near noon, with the circle; bar. 29.6 inch, therm. 52° .

Times by W.

11^h 38^m 24^s
 11 43 3
 11 46 38
 11 50 13
 11 52 33
 11 54 27
 11 57 15
 11 59 21
 0 6 5
 0 7 19
 0 9 37
 0 11 53
 0 14 5
 0 17 17
 0 21 27
 0 25 33

During the observation the angle was carried twice quite round the limb, and the final angle registered was

Increased by $211^{\circ} 59' 30''$ which gives
 Total Angle } $1440 \quad 0 \quad 0$
 Measure } $1651 \quad 59 \quad 30$

The error of watch at noon, as determined by equal alts, was $2^m 3^s 0$ fast on A. T.

The obs. being made at noon in long. $0^h 6^m$, the Green. Date is May 7th, $0^h 6^m$ in App. Time.

Sun's Decl. at Green. Date, $16^{\circ} 43' 1'' N.$

To find Approx. Mer. Alt.

Decl. $16^{\circ} 43'$
 90
 $106 \quad 43$
 Lat. $-55 \quad 1$
 Mer. Alt. $51 \quad 42$

Sum of Alts. 16) $1651^{\circ} 59' 30''$
 $2) 103 \quad 14 \quad 58$
 Obs. Alt. $51 \quad 37 \quad 29$
 True Alt. $51 \quad 36 \quad 49$

App. Times Reductions 2d Red.
 11^h 36^m 21^s ... 1097.2 2.9
 11 41 0 ... 708.3 1.2
 0 23 30 ... 1083.3 2.8
 Sum 5817.4 16) 9.6

To find the Effect of a Change of Declin.

The Sum of the E. H.-ang. is $97^m 30^s$

Do. Western do. $94 \quad 53$

Diff. of E. and W. H.-ang. $\Delta \quad 37$

Or 05^h

Hourly Diff. $41' 32$

16) $2^{\circ} 0660$

13

Do. + 16 $363.6 \log. 2.5606 \quad 0.6 \log. 9.7781$

Lat. $55^{\circ} 1' \cos. 9.7584$

Decl. $16 \quad 43 \cos. 9.9812 \quad 9.9474$

Mer. Alt. $51 \quad 42 \sec. 0.2078 \quad 2$

$322.2 \log. 2.5080 \quad 9.8948 \quad 9.8948$

$322'' = 5' 22'' \quad 2d \text{ Red. } 0.5 \log. 9.6729$

Alt. $51 \quad 36 \quad 49$

Mer. Alt. $51 \quad 42 \quad 11$, and LAT. $55^{\circ} 0' 50''$

Effect of Change, Decl. is $0'' 13$ only.

710. The rate of the watch must be allowed for in deducing each hour-angle. In the case of the sun the rate should be found upon A. T., but it is of course near enough for this purpose to employ M. T.

711. An error in the absolute time affects all the hour-angles alike, but it produces the greatest errors in the greater Reductions. The higher the altitude, the greater is the precision required in the time.

When the time is inaccurate the Reductions on one side of the meridian will be too great, and on the other too small; if, therefore, the altitudes P.M. be taken so as to correspond nearly with those A.M. the errors of the Reductions will very nearly compensate.

This distribution of the altitudes, by equalising the number of the hour-angles A.M. and P.M. has also the advantage of neutralising the effect of a change of declination. It is proper, moreover, to multiply the observations near the meridian, in order to weaken, by subdivision, the small errors to which the outer reductions may be liable

712. The effect of *irradiation*, or the increase of the sun's apparent diameter caused by the extreme brightness, and which may amount to $5''$ or $6''$ (Dr. Robinson on Irradiation, "Mem Roy. Ast. Soc." vol. iv.), is removed by observing both limbs.

[2.] *By a Star or a Planet.*

713 *The Observation* is the same as for the sun, No. 706.

714. *The Computation.* (1.) Having the error of the watch on M. T., find the Greenwich Date. Reduce thereto the Sidereal Time at mean noon, and also the R.A. and decl.; and for a planet, the hor. par.

(2.) Find the hour-angle at each alt. and proceed as for the sun.

When the watch shews Sid. Time, the hour-angles are obtained at once.

715. The stars near the poles, and especially the pole-star, are the best adapted to this observation; because, from the slowness of the motion in altitude, an error of time produces but little error in the Reduction.

716. Errors of altitude, of whatever kind, are removed by employing two bodies on opposite sides of the zenith, and at equal altitudes. A single result, even though obtained with the circle, and without the roof, cannot accordingly be considered definitive when extreme precision is required.

717. Therefore, in the northern hemisphere the best south stars to pair with Polaris are those whose meridian altitudes are about the same as the latitude of the place.

Similarly, in taking Lunars, stars lying at about equal distances, east and west of the moon, should be chosen. *See* No. 861.

III. BY DOUBLE ALTITUDE OF THE SAME BODY.

718. Two altitudes, of the same or different celestial bodies, with the interval of time between them, constitute an observation which is called a Double Altitude.* The interval may extend from a few minutes to several hours. *See Sumner's Method*, No. 1009.

719. When a double altitude of the same body is taken, the precepts below will be convenient in directing the method of solution proper for the case.

Also, when a first altitude has been obtained, the observer will find, on referring to the numbers indicated, under the heads *Observation* and *Limits*, instructions how to complete the observation in the manner adapted to the circumstances.

Selection of the Method of Solution.

When *both alts.* are not far from the meridian, on the same side, No. 729; on different sides, No. 731; in a doubtful case, No. 728.

When *one alt.* is near the meridian, No. 737.

When *neither alt.* is near the meridian. If the lat. by acc. is not greatly in error, No. 746. If it is greatly in error, or if it is proposed to do without it, No. 757.

* This is the old-established term; it is, however, defective, inasmuch as the word *double* means *twice the same*. Since the process involves two altitudes used in combination with one another, the term which would naturally suggest itself is *Combined Altitudes*; we should then have, accordingly, combined altitudes of the same or different bodies, and of long or short intervals. This term, therefore, which is accurate as respects definition, would be clear and descriptive in use. All changes in nomenclature, in this subject, however, must be made with caution.

1. *Short Double Altitude.*

720. When the time is not known with some degree of precision, the Reduction to the meridian cannot be computed. In such cases recourse must be had to two altitudes separated by a short interval, and not very distant from the meridian.

721. The change of altitude in a small interval of time (No. 696) depends chiefly on the hour-angle or meridian distance, and is nearly the same for a considerable difference of latitude. Although altitudes at sea are always more or less uncertain, yet *difference* of alt. may often be obtained with much precision. If, therefore, the difference of alt. in a small interval of time be measured by an instrument, the hour-angle corresponding may be found by computation. The Reduction to the meridian being then computed for this hour-angle, the latitude is obtained by the method in the last section.

722. The error of the watch is immaterial, but its *rate* should be known nearly enough for measuring the interval without much error.

723. When the altitudes are observed at different places, it is necessary to allow for the ship's run in the interval.

724. Since the lat. by acc. is necessary in computing the Reduction, the work should be repeated when this lat. is found to be very erroneous.

725. *Limits.* When both alts. are taken on the *same* side of the merid., if the outer alt. fall near the limits in Table 47, the Interval should exceed one-fourth of the time of that alt. from noon, and should not be less than 5^m. The observation may be comprised within double the mer. dist. implied in Table 48.

When the alts. are taken on *different* sides, the Interval may vary from 5^m to twice the limit in Table 47.

[1.] *By the Sun.*

726. *The Observation.* Observe an alt.* and note the time. Note the sun's bearing for the purpose of allowing for run. After the proper interval, No. 725, observe the second alt. and bearing, noting the time.

727. *The Computation.*† (1.) Subtract the first of the two times from the second (increased if necessary by 12^h); the rem. is the In-

* Two only, or at most three, altitudes taken in quick succession would be employed in observations with a short interval.

† The first work in which a method occurs of finding the latitude by two altitudes observed near the meridian (but restricted to the *same side*) with an interval of a few minutes, is the "Cours d'Observations Nautiques," by Ducom. The advantage which Admiral W. Owen acquainted me that he had derived from the practice of this method led me to give an account of it in the "United Service Journal," vol. x., together with a rule for adapting it to longer intervals. Soon after the account appeared, Commander Graves, commanding H. M. surveying-vessel *Mastiff*, was enabled, as he informed me, by this observation, to run direct for Malta before the coming on of a *grecale*, or N.E. gale, to which another of Her Majesty's ships was exposed.

Interval. Reduce the decln. for the time of the alt. nearest the mer., No. 579; or to the middle of the interval (that is, to noon) when the alts. are equal.

(2.) Correct the altitudes, No 648 or 649. Also correct the Interval by watch for the rate, if this is very large.

When the sun is rising or falling at both observations, proceed by Case I., No. 729; when rising at one observation, and falling at the other, proceed by Case II., No. 731.

728. When sufficient time is not afforded to perceive the rising or falling of the sun, and when it is not known otherwise whether the altitudes are taken on the same or on different sides of the meridian, proceed thus:

Consider the interval* as a time from noon; and compute the Reduction to it; then,

If the Reduction is *less* than the diff. of alts., the observations are on the *same* side; if the Reduction is the *greater*, they are on *different* sides.

Hence, if the Reduction is *equal* to the diff. of alts., one of the alts. is the meridian altitude.

No great precision is to be expected, as the rules are only approximate. In a doubtful case use either.

729. Case I. The observations on the *same* side of the meridian.

(1.) When the alts. are both A.M. reduce the 1st to the place of the 2d, No. 661; when they are both P.M. reduce the 2d to the place of the 1st, No. 662.† Find the diff. of the alts. and their mean. Correct the diff. alts. and the interval by the Table, p. 223.

(2.) Add together the log. sine of the diff. of alts., the log. cosec. of the interval, the log. sec. of the lat., the log. sec. of the decl., and the log. cos. of the mean alt.: the sum (rejecting tens) is the log. sine of the hour-angle, approximately, at the middle time between the two observations.

(3.) From this time subtract half the interval: the remainder is the time from noon of the altitude nearest the meridian.

(4.) To this time compute the Reduction, which apply to the alt. nearest the meridian, and proceed by No. 700 (5): the result is the latitude at the time and place where the alt. nearest the meridian was observed.‡

* It is proper to remark here, that the *interval* between two observations of the sun should, in strictness, be measured in *apparent time*, instead of mean time, which is shewn by the watch. To correct the interval on this account, find the change of the Eq. of T. for the interval. When the Eq. is *additive*, if it is *increasing*, *subtract* the change; if *decreasing*, *add* it; and the contrary when the Eq. is *subtractive*. In the short double alt., however, this correction is insensible, and in long intervals the result is of so inferior a kind that the trifling accuracy gained by this process can rarely be worth the trouble bestowed upon it.

† This reduction is of particular consequence in this observation, because the accuracy of the result depends on that of the difference of altitudes.

‡ This observation, which affords the latitude, the app. time near enough for common purposes, and thence an approximate long. by chronometer, with the azimuth (No. 678), and consequently the variation of the compass, will, it is presumed, be found one of the most useful observations that can be made at sea, especially in high latitudes.

Ex. 1 Oct. 9th, 1878, A.M., lat. acc. $34^{\circ} 55' N.$, long. $61^{\circ} W.$, had following obs. height of eye 16 feet, ind. corr. $+3'$.

T. by Watch	$11^{\text{h}} 12^{\text{m}} 52^{\text{s}}$	Alt. \odot	$46^{\circ} 47' 50''$		$48^{\circ} 11' 0''$
Ditto	$11 \quad 43 \quad 4$	Ind. corr.	$+3$	Alt. \odot	$47 \quad 1 \quad 50$
Interval	$30 \quad 12$	Table 38	$+11$		$95 \quad 12 \quad 50$
Half Int.	$15 \quad 6$		$47 \quad 1 \quad 50$	$+11$	Mean Alt. $47 \quad 36 \quad 25$
		Greater Alt.	$48 \quad 11$		Diff. Alt. $1 \quad 9 \quad 10$
Decl. noon	$6^{\circ} 19' 8''$				
Corr. $61^{\circ} W.$	$+4$				
Red. Decl.	$6 \quad 23 \quad S.$				

D. Alts.	$1^{\circ} 9' 10''$	sine	8.3036
Int.	$30^{\text{m}} 12^{\text{s}}$	cosec.	0.8814
Lat.	$34^{\circ} 55'$	sec.	0.0862
Decl.	$6 \quad 23$	sec.	0.0027
Alt. mean	$47 \quad 36$	cos.	9.8289
Mid. T.	$29^{\text{m}} 8''$	sine	9.1028
$\frac{1}{2}$ Int.	$15 \quad 6$		
T. fr. noon	$14 \quad 2$ (of the greater alt.)		

Lat. 35° , decl. $6\frac{1}{2}^{\circ}$, Table 70	0.391
$14^{\text{m}} 2^{\text{s}}$ sin. sq.	6.972
$8'$ sin.	7.363
Greater Alt	$48 \quad 11$
Mer. Alt.	$48 \quad 19$
	$41 \quad 41 \quad N.$
Red. Decl.	$6 \quad 23 \quad S.$
LAT.	$35 \quad 18 \quad N.$

(The Red. for the interval $30^{\text{m}} 12^{\text{s}}$ is $37'$, which being less than $69'$, shows the observations to be on the same side of the meridian, if this were doubtful. No. 728.)

The 2d Red. is not worth notice. Repeating the work gives $35^{\circ} 18' N.$

Ex. 2. Aug. 4th, 1878. lat. acc. $41^{\circ} 54' N.$, long. $39^{\circ} W.$, obtained true alt. \odot $63^{\circ} 57' 53''$ after $11^{\text{m}} 12^{\text{s}}$ true alt. $64^{\circ} 32' 5$ (allowing for run). Red. decl. $17^{\circ} 12' N.$; mean alt. $64^{\circ} 15'$; diff. alts. $35' c.$

$35' 0''$	sin.	8.0078
$11^{\text{m}} 12^{\text{s}}$	cosec.	1.3111
$41^{\circ} 54'$	sec.	0.1282
$17 \quad 12$	sec.	0.0199
$64 \quad 15$	cos.	9.6379
Mid. T. $29^{\text{m}} 16''$	sin.	9.1049
$\frac{1}{2}$ Int. $-5 \quad 36$		
$23 \quad 40$		

Lat. $42^{\circ} N.$, decl. $17^{\circ} N.$	0.527
$23^{\text{m}} 40^{\text{s}}$ sin. sq.	7.425
$0^{\circ} 31'$ sin.	7.952
$64 \quad 33$	
$65 \quad 4$	

Whence LAT. $42^{\circ} 8' N.$

The 2d Red. is not worth notice.

(The Red. for $11^{\text{m}} 12^{\text{s}}$ is $6' 9$, which is less than $35' c.$ See No. 728.)

Ex. 3. Aug. 11th, 1826, A.M., lat. by acc. $47^{\circ} N.$, long. $13^{\circ} W.$, obtained true alt. \odot $55^{\circ} 41' 9''$, bearing S., course E. by N. 7 knots; after $12^{\text{m}} 14^{\text{s}}$ obtained true alt. \odot $56^{\circ} 37' 9''$ 1st alt. corrected for run, $55^{\circ} 41' 6''$, mean alt. $56^{\circ} 11'$, diff. alts. $56' 3$, reduced decl. $15^{\circ} 23' N$ Corrections, p. 205, 0.

The mid. time from noon is $1^{\text{h}} 0^{\text{m}} 14^{\text{s}}$. Reduction $2^{\circ} 0'$, mer. alt. $58^{\circ} 34\frac{1}{2}'$. LAT. $46^{\circ} 48\frac{1}{2}' N.$

The 2d Red. by Table 48, alt. 58° , is $1'$ for Red. $1^{\circ} S.$, and therefore for Red. $1^{\circ} 54'$ it exceeds $1'$.

730. Degree of Dependence. The smaller the hour-angle, the less is the effect of error in the D. alts. As the interval may, from its smallness, be assumed to be correctly measured, the value of the result depends chiefly on the difference of alts., and may be estimated by finding the effect of an error of $1'$ in the diff. of alts., which is easily done. Divide the middle time by the diff. of alts., both in minutes: the quotient is the number of minutes of error in the time from noon, caused by $1'$ error in the diff. of alts.: the case now becomes that of an error in the Reduction itself, No. 704.*

Ex. In Ex. 3, above, 60^{m} divided by $56'$ gives $1^{\text{m}} 1$, which is the error in the time from noon, supposing $56'$ to be $1'$ in error. Now, by inspecting Table 47, lat. 47° and decl. 15° , (same name) give 27^{m} as the limit, or time from noon at which 1^{m} error of time causes 2

* When the lat. is found to have been very erroneous, repetition is very easily effected, as the sec. lat. is the only log. in 729 (2) that changes.

error in the reduction: hence 1^m error at 1^h from noon will cause about 5' error in the Reduction, and therefore in the latitude.

This example is not an eligible one, since 12^m is only 1-5th of 1^h, instead of being not less than 1-4th. See No. 725.

731. Case II. Observations on *different* sides of the meridian.

(1.) Reduce the alts. to the place of the alt. nearest the meridian, No. 661 or 662. Find the diff. of alts.; correct it and the half interval, when necessary, by the Table, p. 223.

(2.) To the arith. comp. of the log. in Tab. 70 add the log. sine of the diff. of alts. and the log. cosec. of half the interval: the sum is the log. sine of half the diff. of the times from noon corresponding to the two altitudes.

(3.) Subtract this half diff. from the half interval: the remainder is the time from noon (or merid. dist.) of the alt. nearest the meridian.

(4.) Compute the Reduction to this time, and apply it to the alt. nearest the meridian, and proceed as directed, No. 700. The result is the latitude at the time and place where the alt. nearest the meridian was observed.

Ex. 1. April 3d, 1838, lat. by acc. $46^{\circ} 2' N.$, long. $17^{\circ} W.$, the true alts. of the sun to the southward, reduced to last place of observation as below. Red. decl. $5^{\circ} 23' N.$

Times by Watch	$2^h 35^m 54^s$
Interval	$34^m 58^s$
Lat. 46° , decl. 5° , ar. co. log.	9.676
Diff. alts. $13' 23''$	sin. 7.590
Half int. $17^m 29^s$	cosec. 1.118
Half diff. $-5^m 33^s$	sin. 8.384
T. fr. noon	$11^m 56^s$ (of greater alt.)

true alt. $49^{\circ} 10' 30'' A.M.$, or rising.
 $49^{\circ} 23' 53'' P.M.$, or falling.

diff. alt. $13^m 23^s$

Lat. 46° , decl. 5° , log. 0.324

$11^m 56^s$ sin. sq. 6.831

Red. $0^{\circ} 5'$ sin. 7.155

Gr. alt. $49^{\circ} 24'$

Mer. alt. $49^{\circ} 29'$

which given the LAT. $45^{\circ} 54' N.$

Ex. 2. H.M.S. Leven, Aug. 10th, 1826, lat. by acc. $46^{\circ} N.$, long. $15^{\circ} W.$, obtained true alt. $\odot 59^{\circ} 57' 2''$; after $28^m 42^s$ true alt. $59^{\circ} 20' 5''$, the ship having little or no way. Reduced decl. at 1st alt. $15^{\circ} 40' N.$

46° and 16° , ar. co. log.	9.573
Diff. alts. $36' 42''$	sin. 8.028
Half int. $14^m 21^s$	cosec. 1.204
Half diff. $14^m 39^s$	sin. 8.805

This small excess of the computed $\frac{1}{2}$ diff.

over the $\frac{1}{2}$ interval (which should be the greater) is due to the error of the method itself, which becomes apparent in a long interval, and it shews that the alt. $59^{\circ} 57' 2''$ is very nearly the mer. alt. This gives the LAT. $45^{\circ} 43' N.$

Ex. 3. Dec. 23d, 1825, lat. by acc. $8^{\circ} S.$, observed true alts. $\odot 74^{\circ} 26' A.M.$ and $74^{\circ} 16' P.M.$, with the interval $36^m 37^s$. Reduced decl. $23^{\circ} 27' S.$

Ar. co. log.	9.168
10° sin.	7.464
$18^m 18^s$ cosec.	1.098
$-1^m 14^s$ sin.	7.730
$17^m 4^s$	

$17^m 4^s$	0.832
Red. $0^{\circ} 32'$	sin. 7.142
-1^m	(Table 48.)
$74^m 26^s$	
$75^m 57^s$	

The Lat. is $8^{\circ} 24' S.$ This Ex. is far without the limits, Table 47.

Ex. 4. Aug. 9th, 1826, lat. by acc. $45^{\circ} N.$, long. $15^{\circ} W.$, A.M., obtained true alt. $\odot 60^{\circ} 29' 5''$. After $52^m 27^s$ obtained true alt. $60^{\circ} 30'$. The 1st alt. reduced for 1' northing made good in the interval is $60^{\circ} 28' 5''$.

The diff. alts. $1' 5''$ and a half interval $26^m 16^s$ give half diff. 19^s ; the Red. is $31'$, and mer. alt. $61^{\circ} 1'$, which, with reduced decl. $15^{\circ} 57' N.$, give LAT. $44^{\circ} 56' N.$

732. When the alts. are equal, the half interval is the time from noon.

733. *Degree of Dependence.* It would not be easy to give a concise rule for this in long intervals. The rule No. 730 applies very nearly in short and moderate intervals, using, instead of the "middle time," the time from noon of the alt. nearest the meridian.

[2.] *Short Double Altitude of a Star.*

734. Increase the interval by 1^s for every 6^m . Take the decl. from the Nautical Almanac, or Table 63. In other respects proceed as for the sun.

[3.] *Short Double Altitude of a Planet.*

735. Find the Greenwich Date for the middle of the interval, and reduce the decl. Find the daily variation of R.A., and deduce by Table 21 the change of R.A. for the interval. When the R.A. is *increasing*, *subtract* this change from the interval; when *decreasing*, *add* it. Increase the interval by the acceleration upon it. In other respects proceed as for the sun.

As the R.A. and decl. of a planet sometimes change very slowly; much of the above labour is not always necessary: particular rules for all such cases would, however, be superfluous.

[4.] *By the Moon.*

736. Find the Greenwich Date as nearly as possible at each observation, and compute the R.A. *Subtract* from the interval the change of R.A., and add to it the acceleration. Reduce the decl. to the middle of the interval, as also the hor. par. and semid. In other respects proceed as for the sun.

As a proper allowance for a considerable change of declination would complicate the rule, the moon can be employed satisfactorily in this observation only in cases of very short intervals, and when her declination changes slowly.

2. *Double Altitude, one Altitude being near the Meridian.*

737. When one of two altitudes is taken near the meridian, and the other when the body has a large azimuth, the *outer* hour-angle (or that corresponding to the altitude furthest from the meridian) may be computed nearly (No. 614), since it will not be much affected by an error in the latitude by account.* The difference of the hour-angles being afforded by the measured interval of time, the other, or *inner* hour-angle, is found; and the Reduction being computed thereto, the mer. alt. is deduced. See Nos. 722 and 723.

738. *Limits.* The inner alt. must be within the limits in Table 47, and the outer angle should be as nearly E. or W. as possible.

When the outer bearing is not near E. or W., the outer hour-

* The *latitude by account*, in cases in which the ship's change of place is considerable, refers of course, to the place to which the alts. are reduced.

angle may be sensibly affected by the error of the lat. by acc.; and if the inner hour-angle be not very small, the work may require to be repeated.

[1.] *By the Sun.*

739. *The Observation.* Observe the sun's alt., noting the time and the bearing. After a sufficient interval (No. 738) observe the second altitude. See note to No. 726.

740. *The Computation.* (1.) Reduce the decl. at both observations, either by Table 19, No. 579, or by the Green. Date, No. 580, and find the outer pol. dist.

(2.) Correct the interval for the rate of the watch when large.

Correct the altitudes.

When both observations are A.M., reduce the 1st alt. to the 2d place of observation, No. 661. When both observations are P.M., reduce the 2d alt. to the place of the 1st, No. 662. When one observation is A.M., and the other P.M., reduce the alts. to the place of the alt. nearest the meridian.

(3.) With the outer alt., the lat. by acc., and the outer pol. dist., compute the hour-angle, No. 614.

(4.) Take the diff. between this hour-angle and the interval: this is the *inner* hour-angle.

(5.) With this hour-angle compute the Reduction to the meridian and apply it (No. 700 (4) and (5)), to the alt. nearest the merid. The decl. which is to be applied to the mer. zen. dist. is that reduced to the time of the alt. nearest the meridian.

Ex. 1. July 23d, 1878, lat. by acc. $54^{\circ} 57' N.$, long. $1^{\circ} 25' W.$, at about $7^h 0^m$ A.M.; obs. alt. $\odot 24^{\circ} 30'$, bearing E. by S. by compass; $4^h 30^m 12^s$ afterwards obs. alt. $\odot 54^{\circ} 26'$, source S.S.E., rate 4.5 knots; ind. corr. + 2', eye 18 feet: required the Lat. at 2d obs.

From S.S.E. to E. by S., or 5 pts., and dist. in interval $20^{\circ} 3'$ give corr. of alt. + 11.

Decl. 23^d at noon	$20^{\circ} 4' N.$	Alt.	$24^{\circ} 53'$	
Long. $1^{\circ} - 0'$		Lat.	$54^{\circ} 57'$	sec. $0^{\circ} 24086$
$5^h 0^m + 3$	+ 3	P. Dist.	$69^{\circ} 53'$	corec. $0^{\circ} 02734$
1st Red. Decl.	$20^{\circ} 7'$		$74^{\circ} 51'$	cos. $9^{\circ} 41728$
Int. $4^h 30^m$	- 2		$49^{\circ} 58'$	sine $9^{\circ} 88404$
2d Red. Decl.	$20^{\circ} 5'$	Hour-an.	$5^h 0^m 14^s$	sin sq. $9^{\circ} 56946$
Obs. Alt. $24^{\circ} 30'$		Interval	$4^h 30^m 12^s$	
Ind. corr. + 2'	+ 12	Inn. H.-an.	$30^{\circ} 2'$	sin. sq. $7^{\circ} 6; 2$
Tab. 38 + 10	+ 11	Lat. 55° Decl. 20°	(same name)	$0^{\circ} 274$
	$24^{\circ} 42'$	Red.	+ 28'	sin. $7^{\circ} 906$
2d Alt.	$54^{\circ} 39'$		$54^{\circ} 39'$	
Corr. for 18 ft	+ 11	Mer. Alt.	$55^{\circ} 7'$	
1st Alt.	$24^{\circ} 53'$	Zen. Dist.	$34^{\circ} 53' N.$	
(The Alt. nearest Mer. is here the 2d.)		Decl.	$20^{\circ} 5' N.$	
		LAT.	$54^{\circ} 58' N.$	

Ex. 2. April 3d, 1878, lat. by acc. $46^{\circ} 7' N.$, long. $14^{\circ} W.$ at about $2^h 10^m$ A.M. obs. alt. $\odot 26^{\circ} 10'$, sun S.E.; $3^h 26^m 35^s$ afterwards (corrected for rate) obs. alt. $\odot 49^{\circ} 8'$ to the southward; course W.; rate 6.8 knots; index $-3'$; eye 16 feet: find Lat. at 2d obs.

From W. to S.E. is 12 pts.; 4 pts. and dist. 23.1 give corr. of 1st alt. $- 16'$. The lat

red decl. $5^{\circ} 20' N.$; the 2d, $5^{\circ} 23' N.$; the 1st alt. (corr. for run), $26^{\circ} 1'$; 2d alt. $49^{\circ} 16'$.

Alt. $26^{\circ} 1'$, lat. $46^{\circ} 7'$, and P. dist. $84^{\circ} 40'$, give hour-angle $3^h 49^m 41^s$, hence inn. hour-angle $23^m 6^s$ and Red. $+ 18'$, LAT. $45^{\circ} 49' N.$

Ex. 3. Dec. 30th, 1825, lat. by acc. $8^{\circ} S.$, long. $6^{\circ} W.$, at about $4^h 8^m 16^s$ by watch, the mean of 3 alts. $\odot 49^{\circ} 9' 4''$, bearing S. $44^{\circ} E.$ magnetic, course W.N.W. 6 knots; at $6^h 18^m 52^s$ mean of 2 alts. $\odot 73^{\circ} 39'$, the watch losing $4^s 5$ an hour on the chron., and the chron. gaining $6^m 6$ a-day; height of eye, 16 feet; ind. corr. $+ 1'$; reduced decl. $23^{\circ} 11' S.$

In the interval, $2^h \frac{1}{2}$, the chron. gained about 1-10th of $6^m 6$ or $0^m 7$, and the watch lost $10^m 1$ on the chron.; the measured interval must therefore be increased by $9^m 4$, and becomes $2^h 10^m 45^s$.

From W.N.W. to S. $44^{\circ} E.$ is 156° ; course 24° and dist. 13 miles give D. Lat. $11' 9$, to be subtracted from the 1st alt.

Alt. $49^{\circ} 10'$, lat. $8^{\circ} 1'$, and pol. dist. $66^{\circ} 49'$, give outer hour-angle $2^h 38^m 16^s$; the diff. of this and $2^h 10^m 45^s$, or $27^m 31^s$, is the inner hour-angle, which, with alt. $73^{\circ} 52'$, reduction $1^m 27^s$, and 2d reduction $4'$, give LAT. $8^{\circ} 26' S.$

[2.] *Double Altitude of a Star, one Alt. near the Meridian.*

741. Increase the interval by 10^s for each hour. Take the decl. from the Nautical Almanac, or from Table 63. In other respects proceed as for the sun.

[3.] *Double Altitude of a Planet, one Alt. near the Meridian.*

742. Find the Green. Date at each observation, and reduce to it the R.A. and decl. Apply the change of R.A. to the interval, as directed No. 735, and add to the interval the acceleration upon it. Proceed as for the sun.

[4.] *Double Altitude of the Moon, one Alt. near the Meridian.*

743. Proceed by No. 736 as far as adding the acceleration. Reduce the decl. to each Gr. Date, and the hor. par. and semid. to that nearest the meridian. Proceed as for the sun.

744. The moon may be advantageously employed for this purpose when the Greenwich Time can be nearly ascertained, and in all cases when near her maximum declination, because her polar distance may then be very nearly computed.

745. *Degree of Dependence.* The error of the inner hour-angle is the same as that of the outer one, which, when the body is near E. or W., will be very small, even when the lat. by acc. is considerably in error.

3. *Double Altitude, neither Altitude being near the Meridian.*

746. When neither altitude is near the meridian, the computation is different from those hitherto given, of which the object is to find the meridian altitude.

We shall give, 1st, an *approximate* method, the object of which is to find the *correction of the lat. by acc.*; and, 2d, the *rigorous* method, the object of which is to find the *latitude itself* directly, both in Ivory's form (suited to the case in which the decl. is the same at both observations) and in a general form.

747. The principle of the approximate method will easily be

understood. Suppose the time* to be computed at each observation, then, if the interval between these computed times agrees with that actually shewn by a good watch, the latitude by acc. (which is an element of the calculation of the time) is obviously correct, but if on the other hand, the computed interval does not agree with the interval by the watch, the disagreement indicates an error in the latitude by acc.,† the *amount* of which is to be computed.

748. When the correction of the lat. by acc. exceeds 10' or 15', it may, generally, be advisable to repeat the computation; but when it is less than 4' or 5' it may be considered rather as confirming the lat. by acc. within this limit, than as correcting it by so small a quantity.

See, also, Nos. 722 and 723, which apply to this observation.

749. *Limits.* An observation that is usually a substitute for a better, which the state of the weather has prevented, or seems likely to prevent, from being obtained, must be taken when it offers itself; but when there is a choice of observations, the limits are as follows:—

(1.) When the observations are on the *same* side of the meridian, the difference of bearing at the two observations should exceed the lesser true bearing.

(2.) When on *different* sides of the meridian, the *supplement* of the diff. of bearing should exceed the lesser true bearing.

The diff. of bearing should, when possible, be 90°.

750. The simplest case in computation. This will of course be selected when the weather allows a choice of observations.

In N. lat. both altitudes are to be taken to the southward of E. or W. (or the prime vertical); in S. lat. both are to be taken to the northward of E. or W.

When the lat. and decl. are of *contrary* names, the simple case is the only one that offers itself, and therefore applies to the sun during the six months which include the winter. When the lat. and decl. are of the *same* name, the hour-angle at each observation is to be *less* than the hour-angle in Table 29, or the altitude is to be *greater* than the alt. in that Table.

[1.] *Double Altitude of the Sun.*

751. *The Observation.* Take the alt. (see note to No. 726), noting the time, and the true bearing. After the proper change of bearing take the other altitude, noting the time.

As waiting for the proper change of bearing may risk the loss of the 2d alt. it will be prudent to provide an altitude earlier to serve in case of accident.

* As the hour-angles only are here concerned, the consideration of Time, as found by observation, will present no difficulty to a learner.

† Admiral Sir Edward Owen informed me, that when in the North Sea he made constant use of the method of finding the lat. by the discrepancy of the computed times, as he found it much more convenient in practice, in cases where it was necessary to profit by every opportunity of observation, than any solution of the Double Altitude as a question of latitude only. In Lynn's Tables the same problem is worked by trial and error. In Capt. Owen's journals the observation, solved upon the same principle as that here adopted, constantly occurs.

Note at each observation whether the sun is to the northward or to the southward of E. and W.

An example will shew how to select the simple case.

Ex. 1. Oct. 3d, lat. 25° N. The lat. is N. and declin. south, and it is the simple case.

Ex. 2. Sept. 1st, lat. 40° N. The decl. is 8° N.; hence (Table 29) the 1st alt. must be taken after $6^h 39^m$ A.M. (which is the suppl. to 12^h of the hour-angle $5^h 21^m$), and the 2d before $5^h 21^m$ P.M. (A.T.); or each alt. of the centre must exceed $12^{\circ} 5'$.

752. The Computation. The approximate method.*

If the difference of azimuth is not considerable this method should not be employed. In low lats. it will accordingly be less serviceable than in high latitudes. The proper limits for the solution will be seen on inspecting Table 71; cases outside the limits should be rejected, and those bordering on them employed with caution, especially if the error of the latitude by account is large.

(1.) Find the Green. Date at the first observation. Reduce the declin. to each time of observation. For the sun, it is immaterial whether app. time or mean time be used. In general at sea app. time will be preferable, because when the observation confirms the lat. by acc. the apparent time at ship is determined. Find the polar distances (No. 443).

(2.) If the rate of the watch is large, correct the interval for it. Correct the alts. and reduce the 1st alt. to the 2d place of observation.† No 661.

(3.) With the alt., lat. by acc., and pol. dist., compute the hour-angle at each observation, No. 614.

(4.) When the observations are on the *same* side of the meridian, take the *difference* of the hour-angles; when on *opposite* sides, their *sum*. If this diff. or sum agrees with the interval by watch within $10'$, or even $20'$, provided the difference of azimuth is considerable, the lat. is confirmed, and the time is also obtained, nearly enough in the open sea. If they do not agree, proceed thus:—

(5.) In N lat. if the body at both observations is to the *southward* of E. or W., it is the simple case (No. 750); if the body is to the *northward* of E. or W., mark such hour-angle V.

In S. lat., if the body at both observations is to the *northward* of

* This method, besides affording the time when the lat. by acc. is not very erroneous, employs the azimuths, which in practice is a considerable advantage, since the azimuth is the means of determining the degree of dependance of the lat. by double altitude.

† As some misunderstanding has prevailed upon the necessity of correcting the *interval of time* for the *change of longitude* of the ship, the following illustration, which was given in answer to the question, in the Nautical Magazine, 1840, is here inserted:—

Suppose at a place A, at 10 A.M., the sun's alt. is observed $13^{\circ} 18'$, and $3^h 40^m$ afterwards a 2d alt. is observed. These two alts. with the interval $3^h 40^m$ afford the latitude of A.

Again, suppose at a place B an observer had obtained the alt. at 10 A.M., or exactly at the same instant the observer at A took his 1st alt., and $3^h 40^m$ afterwards he obtains his 2d alt. $14^{\circ} 15'$. These two alts. with the interval $3^h 40^m$ afford the lat. of B. Now suppose a ship had left A at 10 A.M., having obtained the 1st alt. $13^{\circ} 18'$, and at the end of $3^h 40^m$ she arrives at B, where she obtains her 2d alt. $14^{\circ} 15'$; then she has the given interval $3^h 40^m$ with the 2d alt. $14^{\circ} 15'$; and it is clear that by reducing the 1st alt. observed at A, or $13^{\circ} 18'$, to what it would have been if observed at B (that is, in other words, correcting the 1st alt. for the mere *change of place*), she has precisely the elements for determining the lat. of B, which is required.

Thus, when the interval is measured by a watch, no correction for longitude appears.

E. or W., it is the simple case; if the body is to the *southward* of E. or W., mark such hour-angle V.

If the bearing has not been observed, or if it is doubtful, look in Table 29; then, if the computed hour-angle *exceeds* the hour-angle in the Table, mark it V; if the comp. hour-angle is the *lesser*, use no mark. If both hour-angles are less than in Table 29, it is the simple case.

(6.) For the Correction of the Lat. Compute the azimuths at each observation, No. 676.

(7.) When the observations are on the *same* side, both of the meridian and prime vertical, enter Table 71, Part I. with the azimuths. When the observations are on *different* sides, either of the meridian or prime vertical, enter Part II.

To the log. from Table 71 add the log. sec. of the lat. by acc., and the prop. log. of the error of the interval; the sum (rejecting tens) is the prop. log. of the correction of the lat. by acc.

(8.) In the simple case (No. 750), apply the correction to the lat. by acc. according to the following directions:—

Observations on the <i>same</i> side of the Meridian		Observations on <i>different</i> sides of the Meridian	
The Computed Interval being		The Computed Interval being	
the greater	the lesser	the greater	the lesser
<i>sub.</i>	<i>add</i>	<i>add</i>	<i>sub.</i>

In the case in which *one* or *both* hour-angles are marked V (No. (5) above), apply the correction according to the directions in the next Table.

	Observations on the <i>same</i> side of the Meridian				Observations on <i>different</i> sides of the Meridian			
	The Computed Interval being the <i>greater</i>		the <i>lesser</i>		The Computed Interval being the <i>greater</i>		the <i>lesser</i>	
Both observations on the <i>same</i> side of the Prime Vertical, and <i>both</i> marked V.	The <i>greater</i> Hour \angle being with the		The <i>greater</i> Hour \angle being with the					
	<i>greater</i> Azim.	<i>lesser</i> Azim.	<i>greater</i> Azim.	<i>lesser</i> Azim.				
	<i>add</i>	<i>sub.</i>	<i>sub.</i>	<i>add</i>	<i>sub.</i>		<i>add</i>	
Observations on <i>different</i> sides of the Prime Vertical, or <i>one</i> marked V.	The Hour \angle V being with the		The Hour \angle V being with the		The Hour \angle V being with the		The Hour \angle V being with the	
	<i>greater</i> Azim.	<i>lesser</i> Azim.	<i>greater</i> Azim.	<i>lesser</i> Azim.	<i>greater</i> Azim.	<i>lesser</i> Azim.	<i>greater</i> Azim.	<i>lesser</i> Azim.
	<i>sub.</i>	<i>add</i>	<i>add</i>	<i>sub.</i>	<i>add</i>	<i>sub.</i>	<i>sub.</i>	<i>add</i>

Note. This second Table, which contains the remaining fourteen out of eighteen cases, may appear complicated in its general aspect. It is, however, easy of reference when the case is proposed. For ex. :—

1. Suppose the observations to be on *different* sides of the meridian ; of this point, with a long interval, there can never be a doubt. Again,

2. Let them be on *different* sides of the prime vertical, of which there can rarely be any doubt.

3. Let the computed interval be the *greater*.

Then the precept *add* or *sub.* depends on the condition that the hour-angle marked V is with the *greater* or with the *lesser* azimuth.

Ex. 1. (Observ. *same* side both of Mer. and Pr. Vert.) May 20th, 1878, lat. by acc. $40^{\circ} 12' N.$, long. $62^{\circ} W.$, at about $8^h 0^m 0^s A.M.$, obs. alt. $\odot 35^{\circ} 32'$, bearing E. by S.; at $11^h 8^m 32^s A.M.$, obs. alt. $\odot 66^{\circ} 58'$; index $-3'$, eye 16 feet: course during interval S.E. $\frac{1}{2}$ E.; rate 4 knots: required the Lat. at 2d observation.

From S.E. $\frac{1}{2}$ E. to E. by S., or $2\frac{1}{2}$ pts. and dist. 12.4 , corr. of 1st Alt. $+11'$.

Decl. noon, 20th,	$20^{\circ} 1' N.$	Alt. \odot	$35^{\circ} 32'$	Alt. \odot	$66^{\circ} 58'$
$4^h -2'$		Ind.	$-3'$	$-3'$	
$62^{\circ} W. +2$	0	Table 38	$+11$	$+12$	$+9$
1st Red. Decl.	$20^{\circ} 1$		$35^{\circ} 40$	2d True Alt.	$67^{\circ} 7$
$3^h 9^m$	$+2$	Corr. run	$+11$		
2d Red. Decl.	$20^{\circ} 3$	1st True Alt.	$35^{\circ} 51$		

1st Hour-angle.			
Alt.	$35^{\circ} 51'$		
Lat.	$40^{\circ} 12$	sec.	0.11702
P. Dist.	$69^{\circ} 59$	cosec.	0.02706
	$146^{\circ} 2$		
	$73^{\circ} 1$	cos.	9.46552
	$37^{\circ} 10$	sin.	9.78113
1st H.-angle $3^h 57^m 49^s$	sin. sq.	9.39073	

2d Hour-angle.			
Alt.	$67^{\circ} 7'$		
Lat.	$40^{\circ} 12$	sec.	0.11702
P. Dist.	$69^{\circ} 57$	cosec.	0.02715
	$177^{\circ} 16$		
	$88^{\circ} 38$	cos.	8.37756
	$21^{\circ} 31$	sin.	9.56440
2d H.-angle $0^h 50^m 43^s$	sin. sq.	8.03607	
1st ditto	$3^h 57^m 49$		
Comput. Int.	$3^h 7^m 6$	(the <i>lesser</i>)	
Interval	$3^h 8^m 32$		
Error	$1^m 26$		

1st Azimuth.			
$3^h 57^m 48^s$	sine	9.9351	
Decl. $20^{\circ} 1$	cos.	9.9729	
Alt. $35^{\circ} 51$	sec.	0.0912	
Azim. 87°	sin.	9.9992	

2d Azimuth.			
$0^h 50^m 43^s$	sine	9.3414	
Decl. $20^{\circ} 3$	cos.	9.9728	
Alt. $67^{\circ} 7$	sec.	0.4100	
Azim. 32°	sin.	9.7242	

Correction of the Latitude.

Table 71, Part I., 32° and 87°	9.014
Lat. sec. (above)	0.117
$2^m 26^s$ pro. log.	2.097
Corr. of Lat. $11'$	Pro. log. 1.230

The lat. being N., and both observations to the southward, it is the simple case; the obs. being on the same side of the merid. and the computed interval the *lesser*, $11'$ is to be added to $40^{\circ} 12'$, which gives Lat. $40^{\circ} 23' N.$

Ex. 2. (*Different* sides of Mer.) Oct. 16th, 1878, lat. by acc. $41^{\circ} 22' S.$, long. $150^{\circ} E.$, at about $10^h 45^m A.M.$ obs. alt. $\odot 53^{\circ} 2' 20''$, bearing by compass S.E. by S.; time by chron. $6^h 29^m 19^s$; at $10^h 39^m 6^s$ by same chron. obs. alt. $\odot 41^{\circ} 1' 10''$, ind. corr. $-3' 20''$, height of eye 14 feet; chron. *gaining* 12.2 daily. Course S.E. by S.; rate 6 knots.

The course being exactly towards the sun, the run in 4^h gives 24 to be added to 1st alt. The pol. dists. $81^{\circ} 14'$ and $81^{\circ} 10'$; 1st alt. $53^{\circ} 35'$; 2d, $41^{\circ} 9'$.

Alt.	53° 35'		
Lat.	41 22	sec.	0°12465
P. Dist.	81 14	cosec.	0°00508
	<u>176 11</u>		
	88 5	cos.	8°52434
	34 30	sine	9°75313
1st H.-angle	1 ^h 13 ^m 34 ^s	sin. sq.	8°40720

1st Azimuth.

1 ^h 13 ^m 34 ^s	sine	9°499
Decl. 8° 46'	cos.	9°995
Alt. 53 35	sec.	0°226
Azim. 31°	sin.	9°720

Alt.	41° 9'		
Lat.	41 22	sec.	0°12465
P. Dist.	81 10	cosec.	0°00518
	<u>163 41</u>		
	81 50	cos.	9°15245
	40 41	sine	9°8141
3d H.-angle	2 ^h 45 ^m 33 ^s	sin. sq.	9°0964

1st do.	1 13 34
Interval	<u>3 59 7 (the lesser)</u>
	<u>3 59 47</u>
	0 0 40

2d Azimuth.

2 ^h 45 ^m 34 ^s	sine	9°820
Decl. 8° 50'	cos.	9°995
Alt. 41 9	sec.	0°123
Azim. 60°	sin.	9°938

Correction of the Latitude.

Table 71, Part II., 31° and 60°	9 174
Lat. sec. (above)	0°125
0 ^m 40 ^s pro. log.	<u>2°431</u>
3' pro. log.	1°730

The obs. on *different* sides of meridian and the computed interval the *lesser*, 3' has to be subtracted from 41° 22', which gives Lat. 41° 19' S.

Ex. 3. (*different* sides of the pr. vert.) Feb. 19th, 1878, lat. by acc. 52° 55' S., long. 11° E., at 1^h 40^m P.M. obs. alt. ☉ 43° 53', bearing S.W. by S.; at 5^h 39^m 5^s P.M. obs. alt. ☉ 11° 55'. Course in int. N.E. by N., 3.5 knots an hour; height of eye 16 feet: required the LATITUDE at 2d observation.

1st Alt. (run allowed for) 43° 50', 2d Alt. 12° 3'; 1st Pol. Dist. 78° 48', 2d Pol. Dist. 78° 51'; 1st Hour-angle 1^h 38^m 46^s, Az. 35°; 2d Hour angle 5^h 38^m 57^s, V. Az. 87°; corr. of lat. 7' to be subtracted, because the obs. are on the same side of mer., the computed int. *greater*, obs. on *different* sides of pr. vert., and the hour-angle V with greater azimuth. LAT. 52° 48' S.

[2.] Double Altitude of a Star.

753. This is the same as for the sun, except that the interval by watch must be *increased* by 10^s an hour.

[3.] Double Altitude of a Planet.

754. Find the Green. Date at each obs., and reduce thereto the R.A. and decl. Apply the change of R.A. to the interval, as directed No. 735, and add to the interval the Acceleration upon it. In other respects proceed as for the sun.

[4.] Double Altitude of the Moon.

755. Find the Green. Date at each observation, and reduce the R.A. and decl. *Subtract* the change of R.A. from the interval, and add to the interval the Acceleration upon it. In other respects proceed as for the sun.

756. For the *Degree of Dependence*, see No. 771.

4. Ivory's Solution, for the same Body.

757. Though this method applies, strictly, to a body which does not change its declination, yet it answers well enough, in common

practice, with the sun, by employing a mean between the pol. dista. proper to each observation. The same is true of the moon when near her greatest declination, N. or S., since at that period she changes her decl. about $1'$ only in 6 hours.

(1.) With the sun, the moon, or a planet, find the Greenwich Date for the middle time between the observations, and reduce the decl. thereto.

Find the pol. dist. by means of the lat. by acc., N. or S.

Correct the altitudes, and reduce them to the 2d place of observation.

Find the polar angle. For the sun, this is the interval in app. time; or mean time, as shewn by the watch, is near enough. For a star, see No. 734. For a planet, see No. 735. For the moon, see No. 736. Take half the interval, and find half the sum and half the difference of the altitudes.

Note.—When the interval is rather small, more care is required in the work, which may then be carried to quarter minutes in Table 68, at sight.

(2.) For Arc 1. To the log. sine of the half interval add the log. cos. of the decl.: the sum is the log. sine of arc 1.

(3.) For Arc 2. Take the ar. comp. of the log. sine found, and add to it the log. cos. of the half sum of the alts., and the log. sine of their half diff.: the sum is the log. sine of arc 2.

(4.) For Arc 3. To the log. sine of the decl. add the log. sec. of arc 1: the sum is the log. cos. of arc 3.

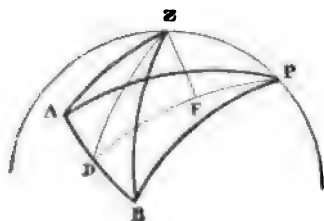
When the lat. and decl. are of contrary names, or the pol. dist. exceeds 90° , take the suppl. of this arc.

(5.) For Arc 4. Add together the log. sec. of arc 1, the log. sine of the half sum of the alts., the log. cos. of their half diff., and the log. sec. of arc 2: the sum is the log. cos. of arc 4.

(6.) For Arc 5. This is the diff. or sum of arcs 3 and 4.* When the observations are on *different* sides of the meridian; if the pol. dist. is *greater* than the colat. take the *diff.*; if *less*, the *sum*.

When the observations are on the *same* side of the merid., when the pol. dist. *exceeds* the colat., take the *diff.* When the pol. dist. is *equal* to or *less* than the colat., take out the log. sine of the lat. by acc.; then add together the log. sines of the decl. and mean of the

* This step is so near the end of the operation, that the computer may content himself with trying whether the sum or diff. gives the result in lat. nearest to the lat. by acc., as in all eligible cases the two results will differ greatly.



A and B are the places of the body at the two observations; PA, PB the polar distances; ZA, ZB the zen. dists.; APB the polar angle or interval. PD is drawn perp. to AB, and dividing APB into two equal parts; ZF is perp. to PD.

Then, Arc 1 is AD; Arc 2 is ZF; Arc 3 is PD. As PD is usually greater than AD, from which it is determined, if a small error occurs in AD, PD will be in error still more. Arc 4 is DF; Arc 5 is PF. PF here is PD - DF; but when the pol. dist. is much less than PZ, F may fall beyond D on PD produced, and then PF

= PD + DF. The colat. PZ is then found from PF and ZF.

alts. (already employed). If this last sum is *less* than the *sig.* of the lat., take the *diff.*; if *greater*, the *sum*. One place in the logs. is enough, since, if the distinction is not strongly marked, the case should be rejected.

(7.) For the Latitude. To the log. sec. of arc 5 add the log sec of arc 2; the sum is the log. cosec. of the latitude.

Note.—To save reopening Table 68 at the same place, logs. taken out at the same opening, or repeated, are marked with the same letters.

Ex. 1. (Obs. *same* side.) Lat. by acc. 10° S., long. 7° E.; true alts. of the sun, $58^{\circ} 40'$, and $63^{\circ} 0'$ reduced to the same place; interval, $32^m 54^s$: required the Latitude.

Red. of Decl. in the Form, Ex. 1, p. 261.

Red. Decl. 14° 24' N.
Pol. Dist. 104 24

Correction of Alts. in the Form, Ex. 1,
p. 266, then,

1st Alt.	58° 40		
2d	63 0		
Sum	121 40	Half Sum	60° 50
Diff.	4 20	Half Diff.	2 10

Int.	<u>32° 54'</u>				
Half	16 27	sin.	8° 85605		
Decl.	14° 24'	cos.	<u>9° 98614</u> (a)	sin.	9° 39566 (a)
Arc 1	3 59	sin.	<u>8° 84219</u> (b)	sec.	0° 00105 (b)
			(Suppl.) 75° 34'	cos.	<u>9° 39671</u>
			Arc 3 104 26		

Half Sum	60° 50'	cos.	9°68784 (e)	sin.	9°94112 (c)	...	sec. Arc 1 (rep.)	0°00105 (b)
Half Diff.	2 10	sin.	8°57757 (d)	cos.	9°99909 (a)	...		
Arc 2	15 22	sin.	9°42322 (e)						sec. Arc 2	0°01581 (e)
					Arc 4	24 53	cos.	9°95767		
					Arc 5	79 33	sec.	0°74142		

Criterion for Sum or Diff. of Arcs 3 and 4.

Pol. Dist. exceeds colat.-diff.

LAT. 10° 4'

Arc 2, sec. (rep.) $0^{\circ}01581$ (e),
cosec. $0^{\circ}75723$

Ex. 2. (*same side mer.*) Lat by acc. $43^{\circ} 10' N.$; alts. of Capella, reduced to the same place, $22^{\circ} 58'$ and $56^{\circ} 14'$; interval by chronometer, $3^h 34^m 17^s$; required the Lat.

Interval red. $3^h 34^m 53^s$; decl. $45^\circ 50' N.$; arc 3, $40^\circ 55'$. Criterion, sin. lat. 9.8 ; sum of sines of decl. and mean alt. 9.6 ; take the diff. of arcs 3 and 4. LAT. $43^\circ 29' N.$

Ex. 3. (obs. *different sides*.) Lat. by acc. 10° N.; alts. of Castor, $63^{\circ} 16'$ and $46^{\circ} 12'$; interval by a watch, $3^h 55^m 25^s$; decl. $32^{\circ} 14'$ N.: required the Lat.

Arc 1, $24^{\circ} 33\frac{1}{2}'$; Arc 2, $11^{\circ} 54'$; Arc 3, $54^{\circ} 5\frac{1}{2}'$; Arc 5, $78^{\circ} 58'$. LAT. $10^{\circ} 47\frac{1}{2}'$ N.

758. (1.) When the alts. are equal, this method is peculiarly convenient.

Compute arcs 1 and 3, as above. Arc 2 is 0.

For Arc 4. Add together the log. sine of the alt. and the log. sec. of arc 1: the sum is the log. cos. of arc 4.

When the pol. dist. exceeds the colat., the diff. of arcs 3 and 4 is the colat.; otherwise their sum.

Ex. Equal alts. $46^{\circ} 51'$; pol. dist. $66^{\circ} 33'$; interval, $4^h 37^m 50^s$. LAT. by acc. 60° .

Arc 1, $31^{\circ} 30\frac{1}{2}'$; Arc 3, $62^{\circ} 10\frac{1}{2}'$; Arc 4, $31^{\circ} 9\frac{1}{2}'$. LAT. $58^{\circ} 59'$.

(2.) When the declin. is 0, the half int. is arc 1, and arc 3 is 90° .

Ex. Lat. by acc. 60° N., decl. 0, int. $2^{\text{h}} 0^{\text{m}} 0^{\text{s}}$; true alts. $28^{\circ} 53'$ and $20^{\circ} 42'$. Arc 1 is $15^{\circ} 0'$; Arc 2, $14^{\circ} 29\frac{1}{2}'$; Arc 5, $26^{\circ} 34'$. LAT. $59^{\circ} 59\frac{1}{2}'$ N.

Note.—If the time also is required from the observation, with the outer alt., lat. found, and pol. dist. (red. to time of outer alt.), find the hour-angle, No. 614, and see No. 780 (4), p. 279. The sum of log. sec. lat. and log. sin. arc 2 is log. sin. mid. time between the obs.

IV BY DOUBLE ALTITUDE OF *DIFFERENT* BODIES.

759. The forms of solution described in Nos. 737 and 747 for the cases of two altitudes of the same celestial body apply to the altitudes of different bodies, the difference of their right ascensions supplying in part, or entirely, the place of the measured interval.

Since the value of this observation, like the former, depends upon the difference of azimuth, the two bodies may often be so selected as to afford the best possible result under the circumstances, while in the case of a single body the necessary conditions are not, generally, matter of choice. Hence this method may be practised with equal convenience in all latitudes.

This observation is particularly convenient in the case of two stars, because, as the right ascensions of the stars change very slowly no reference to the absolute time is necessary.

760. When the two observations can be obtained at nearly the same time, this method has the advantage of being independent of the rate of the watch, and also of the errors of the ship's run; but when an interval elapses between the observations, allowance must be made both for the rate and the run.

1. *One of the Altitudes (of Two Bodies) being near the Meridian.*

761. *Limits.* These are the same as those given in No. 745. It must be remarked, that the rules for the limits apply to the bearings at the time the bodies are actually observed, whether there be an interval or not. For ex., if the sun be observed S.S.E., and the moon E. by S., the case is a good one; but if the observation of the moon were delayed till she bore S.E., the case would not be good.

762. *The Observation.* Take the alt. of the outer body, which should be observed as nearly E. or W. as possible. Then observe the alt. of the inner one; lastly, that of the outer one again, noting the times of each alt.

763. *The Computation.* (1.) For the sun, moon, or a planet. Find the Green. Date, and reduce thereto the R.A. and declination; and for the moon, her hor. par. and semid.

For a star. Take the R.A. and decl. from the *Nautical Almanac*, or from Table 63.

Call the diff. of R.A., or its suppl., *the polar angle*.

(2.) Reduce the alts. to the same instant, and correct them.

(3.) With the outer alt. and pol. dist. find the outer hour-angle, and proceed as in No. 740 (4), to the end.

Ex. 1. March 6th, 1878, at about 5^h 55^m P.M. M.T.; lat. acc. 40° 15' S. long. 38° 52' W., obs. alt. Saturn 11° 50'; also (reduced to the same instant) obs. alt. Aldebaran near meridian 33° 17'; ind. corr. + 1', height of eye 18 feet: required the Latitude.

The Gr. Date is 6^h 8^m 30^s.

Saturn's Red. R.A.	23 ^h 34 ^m 24 ^s
Aldebaran's R.A. + 24 ^h	28 28 56
Polar angle	4 54 32
The true Alt. of Sat. 11° 41', lat. 40° 15', pol. dist. 85° 6' give Saturn's hour- angle	5 15 19
Aldebaran's hour-angle	20 47
Saturn's Decl. 4° 54' S. pol. dist.	85° 6'
Aldebaran's decl. 16° 16' N.	

Aldebaran's obs. alt. 33° 17', true alt. 33° 13'	
Lat. 40°, Decl. 16° (contrary names)	} 0° 250
20° 47°	
sin. sq.	7° 313
sin	7° 563
Mer. Alt.	33 12
Zen. Dist.	56 35 S.
Decl.	16 16 N
Lat.	40 19 S.

Ex. 2. Feb. 2d, 1878, lat. by acc. 54° 53' N.; obs. alt. Regulus 15° 54', and the alt. of Aldebaran (reduced to the same instant) 51° 17'; ind. corr. -3'; height of eye 20 feet: required the Latitude.

R.A. Regulus, 10^h 1^m 55^s, decl. 12° 34' N.; R.A. Aldebaran, 4^h 28^m 57^s, decl. 16° 16' N. Regulus' true alt. 15° 43'; Aldebaran's ditto, 51° 19'; hour-angle of Regulus, 5^h 21^m 54^s, hour-angle of Aldebaran, 11^h 4^m; Red. + 4'. LAT. 55° 3' N.

764. When the change of alt. of one of the bodies is not given by the observation, its altitude cannot be reduced to the same instant as the other by No. 660; to compute it (No. 671), the azimuth is required, which, if not observed with some precision, must be computed. But this reference to the altitude may be avoided, thus:—

Add the interval of time, increased by 1^s for every 6^m, to the R.A. of the body first observed, and subtract the R.A. of the body last observed; the rem. is the polar angle.

If the sum exceed 24^h, reject 24^h.

Ex. 1st, June 24th, 1878, lat. by acc. 40° N., long. 149° 52' W.; time by chron. 24^h 0^m 1^s, obs. alt. of α Andromedæ 41° 53', and 2^m 15^s afterwards obs. alt. of Jupiter 30° 29' to the southward; height of eye 16 feet.

Red. R.A. of Jupiter 20^h 33^m 17^s, Red. decl. 19° 22' S., true alt. 41° 48'.

R.A. of α Andromedæ	0 ^h 2 ^m 8 ^s
	2 15
	0 4 23
Jupiter's R.A.	20 33 17
Polar Angle	3 31 6

The hour-angle of α Andromedæ computed from alt. 41° 48', lat. 40°, and p. l. dist. 61° 35', is 3^h 50^m 33^s.

The difference between the polar angle and the hour-angle of α Andromedæ leaves Jupiter's hour-angle 19^m 27^s, which gives Red. + 10', mer. alt. 30° 33', and Lat. 40° 5' N.

Ex. 2. Jan. 3d, 1878, lat. by acc. 54° 50' N., obs. alt. Regulus 17° 21', and 3^m 40^s afterwards obs. alt. Rigel 26° 46' S.; ind. corr. -5'; height of eye 16 feet: required the Latitude.

R.A. Regulus, 10^h 1^m 54^s, decl. 12° 34' N.; R.A. Rigel 5^h 8^m 42^s, decl. 8° 21' S.; polar angle 4^h 56^m 52^s; true alt. Regulus, 17° 9', hour-angle Regulus 5^h 11^m 57^s; hour-angle Rigel 15^m 5^s; Red. to this + 5'. Lat. 54° 59' N.

765. When the body nearest the meridian is observed below the pole, add the hour-angle of the other to the polar angle: the suppl. to 12^h of this sum is the inner hour-angle, to which compute the Reduction.

Ex. March 21st, 1831, off Cape Horn, lat. by acc. 56° 50' S., long. 65° W., at night, obs. true alt. α Pavonis 24° 38', not long past the mer. below the pole; and after 3^m 25^s obs. alt. γ Crucis 64° 47'; both stars rising, and both to the S. of E.

α Pavo R.A.	$20^h 12^m 17^s$
irt.	$+ 3 \ 23$
	$20 \ 15 \ 40$
γ Crux R.A.	$- 12 \ 21 \ 50$
Polar Angle	$7 \ 53 \ 50$

The hour-angle of γ Crux, computed from alt. $64^\circ 47'$, lat. $56^\circ 50'$, and pol. dist. $33^\circ 50'$, is $3^h 6^m 18^s$.

This hour-angle, added to the polar angle, gives hour-angle of α Pavo $11^h 0^m 3^s$, or $59^m 52^s$ below the pole. The Red. to this is $38'$, and the mer. alt. $24^\circ 0'$ gives Lat. $56^\circ 44' S.$ (Decl. of α Pavo, $57^\circ 16' S.$)

2. Neither of the Altitudes (of Two Bodies) being near the Meridian.

766. *Limits.* These are the same as for No. 749.

767. *The Observation.* Take an alt. of the outer body, then of the inner one, and, lastly, of the outer one, noting the times. At each observation note whether the body is to the northward or southward of E. or W. (true).

768. *The Computation.* The approximate method.

(1.) Take out the right ascens. of the bodies from the Nautical Almanac, reducing them, if necessary, to the Green. Date. Take the diff. of R.A., or its suppl. to 12^h , for the polar angle.

If the 2d alt. of the first body be lost, proceed by No. 763. The result is the polar angle.

(2.) Correct the altitudes.

(3.) Compute the hour-angle of each body.

When the bodies are on the *same* side of the meridian, take the *diff.* of the hour-angles; when on *opposite* sides, their *sum*, for the computed polar angle.

If this sum, or diff., agree tolerably well with the polar angle, the lat. by acc. is near enough; if not, proceed as in No. 752 (5) to find the corr. of lat.

Ex. 1. Feb. 25th, 1830. H.M.S. Eden, lat. by acc. $11^\circ 45' S.$, long. $19^\circ W.$, took alts. of Canopus and Sirius as following, both stars to the E. of the mer., and both to the southward of the E. point.

Canopus.		Sirius.		Canopus.	
$5^h 43^m 11^s$	$46^\circ 58' 4''$	$5^h 48^m 0^s$	$71^\circ 47' 4''$	$5^h 51^m 4^s$	$47^\circ 27' 4''$
$5 \ 45 \ 25$	$47 \ 7 \ 2$	$5 \ 50 \ 0$	$72 \ 14 \ 6$	$5 \ 54 \ 0$	$47 \ 33 \ 4$
Means $5 \ 44 \ 18$	$47 \ 2 \ 8$	$5 \ 49 \ 0$	$72 \ 1 \ 0$	$5 \ 52 \ 32$	$47 \ 30 \ 4$
Sirius R.A.	$6^h 37^m 40^s$	Decl.	$16^\circ 29' 7'' S.$	Pol. Dist.	$73^\circ 30' 3''$
Canopus	$6 \ 20 \ 11$		$52 \ 36 \ 5 S.$		$37 \ 23 \ 5$
Polar Angle	$17 \ 29$				

Reducing the alt. of Canopus to the time $5^h 49^m$ gives alt. required, $47^\circ 18' 4''$. The true alt. of Canopus, $47^\circ 13' 6''$, and of Sirius, $71^\circ 56' 7''$.

Hour-angle of Canopus $1^h 2^m 57^s$

Hour-angle	$1^h 2^m 57^s$	sin.	9.433
Pol. Dist.	$37^\circ 23'$	sin.	9.783
Alt.	$47 \ 14$	sec.	0.168
Azim.	14°	sin.	9.384

Hour-angle of Sirius	$1^h 11^m 52^s$
Ditto Canopus	$1 \ 2 \ 57$
Diff. or comput. Pol. Angle	$8 \ 55$
Pol. Angle	$17 \ 29$
Error	$8 \ 34$

Hour-angle	$1^h 11^m 52^s$	sin.	9.489
Pol. Dist.	$73^\circ 30'$	sin.	9.982
Alt.	$71 \ 56$	sec.	0.509
Azim.	78°	sin.	9.980

Table 71, Part I., 14° and 73°	9.398
Lat. sec.	0.009
$8^m 34^s$ pr. log.	1.322
Corr. of lat. $34'$ pr. log.	0.723

The obs. are on the same side of the merid. and of the pr. vert. ; both hour-angles are to be marked V ; the comput. int. the *lesser* ; the greater hour-angle is with the greater azimuth ; $34'$ is to be *subtracted* from $11^{\circ} 45'$, which gives the Lat. $11^{\circ} 11' S$.

Ex. 2. (The Ex. No. 765.) The computed hour-angle of α Pavo is $11^h 5^m$; the diff. of which, and $3^h 6^m 18^s$, is $7^h 58^m 42^s$, the computed polar angle, which is *greater* than $7^h 53^m 50^s$. The error is $4^m 52^s$.

The azim. of α Pavo is 8° , that of γ Crux $71\frac{1}{2}^{\circ}$; the corr. of lat. by Table 71, Part I., is $6'$, which, since in this case the *greater* hour-angle $11^h 5^m$ is with the *lesser* azimuth, is to be *subtracted* from $56^{\circ} 50'$, and gives LAT. $56^{\circ} 44' S$, as by the other solution.

Ex. 3. Dec. 1st, 1878, lat. by acc. $41^{\circ} 28' N$. ; obs. alt. of Markab, $59^{\circ} 2'$, and that of Altair, reduced to the same instant, $23^{\circ} 38'$; both bodies to the S. and E. ; ind. corr. $-2'$; height of eye 16 feet : required the Latitude.

R.A. Markab, $22^h 58^m 45^s$, decl. $14^{\circ} 33' N$. ; R.A. Altair, $19^h 44^m 52^s$, decl. $8^{\circ} 33' N$. ; true alt. of Markab, $58^{\circ} 55'$; that of Altair, $23^{\circ} 30'$; polar angle, $3^h 13^m 52^s$; Markab's hour-angle, $1^h 11^m 44^s$; Altair's hour-angle, $4^h 24^m 26^s$. Then $4^h 24^m .6^s - 1^h 11^m 44^s = 3^h 12^m 42^s$. Azimuth of Markab, 35° ; azimuth of Altair, 80° . Corr. of lat. 11' to be added to $41^{\circ} 28'$. LATITUDE, $41^{\circ} 39' N$.

Ex. 4. May 1st, 1878, lat. by acc. $29^{\circ} 48' S$; obs. alt. of Altair, $26^{\circ} 24'$, and the obs. alt. of Arcturus, reduced to the same instant, $32^{\circ} 23'$; the bodies on different sides of the meridian, and to the north ; ind. corr. $+2'$; height of eye 14 feet : required the Latitude.

R.A. of Altair, $19^h 44^m 52^s$, decl. $8^{\circ} 33' N$. ; R.A. of Arcturus, $14^h 10^m 9^s$, decl. $15^{\circ} 49' N$. ; polar angle, $5^h 34^m 42^s$; true alt. of Altair, $26^{\circ} 20'$; do. of Arcturus, $32^{\circ} 20'$; hour-angle of Altair, $3^h 31^m 43^s$; Arcturus' hour-angle, $2^h 2^m 3^s$; error, $0^m 56^s$; azimuths, 62° and 34° ; corr. of lat. $6'$ to *sub.* from $29^{\circ} 48'$. LATITUDE, $29^{\circ} 42' S$.

769. The error of the correction of lat. is directly proportional to the error of the interval : hence, when the moon is employed, her R.A. should be computed for the actual time at Greenwich, as given by the chronometer, or found from observation of a lunar distance rather than by means of the erroneous long. by account.

Ex. April 7th, 1831, lat. by acc. $34^{\circ} 40' S$, long. $42^{\circ} W$. ; true alt. $\triangleright 38^{\circ} 27'$ to the N.W. At the same time, true alt. $\odot 47^{\circ} 44'$ to the N.E.-d ; Gr. M.T. by lunar observation, $2^h 14^m 13^s$: required the Latitude.

\odot R.A. $1^h 2^m 41^s$, pol. dist. $96^{\circ} 42'$; \triangleright R.A. $20^h 52^m 28^s$, pol. dist. $74^{\circ} 10'$; \odot 's hour-angle $0^h 36^m 45^s E$. ; \triangleright ditto, $3^h 35^m 27^s W$. ; \odot 's az. 14° ; \triangleright ditto, 81° ; suppl. of diff. of R.A. $4^h 10^m 13^s$. The error of the computed polar angle is $1^m 59^s$, corr. of lat. $+6'$, and LAT. $34^{\circ} 46' S$.

This Ex. may be worked by No. 763 (3), thus : the \triangleright 's hour-angle, $3^h 35^m 27^s$, subtracted from $4^h 10^m 13^s$, gives the \odot 's hour-angle $34^m 46^s$. The Reduction to this is $49'$, and LAT. $34^{\circ} 45' S$.

3. The General Solution, for the same, or different Bodies *

770. (1.) Find the polar angle. This, for the sun, is properly an interval of A.T. ; but mean time is near enough. For a star, see No. 753. For the moon or a planet, see Nos. 754, 755.

* Though this method is general, yet it is not well adapted to cases of short intervals (No. 727) ; because, in such cases, a small arithmetical inaccuracy in the process may produce a considerable error in the resulting latitude, as the reader may easily convince himself by working examples. This is the chief ground on which an approximate and indirect method is often superior, in practice, to the rigorous method.

In the figure in the note, p. 268, omitting the lines P D, Z D, and Z F, arc A is A B ; θ and B are the places of the same body at different times, or of different bodies ; angle B

For different bodies, it is the diff. of their R.A.

Find the polar distances at each observation; in assigning these, one pole must necessarily be assumed as the elevated pole, whether the lat. be approximately known or not. Correct the altitudes, and reduce them to the second place of observation, and find the zenith distances.

(2.) For the Arc A. Take the suppl. of the polar angle; and add the pol. dists. together. Add together the log. sine square of the suppl. and the log. sines of the pol. dists.; the sum (rejecting tens) is the log. sine square of an arc x .

Put x under the sum of the pol. dists.; take the sum and diff. and half the sum and half the diff. Add together the log. sines of the last two terms: the sum (rejecting tens) is the log. sine square of an arc A.

(3.) For the angle B. Add together the arc A and the two polar dists.; take half the sum, and from it subtract the arc A and the outer pol. dist., noting the two remainders. If the half sum is the lesser, subtract it from the other quantity.

Add together the log. cosec. of A, the log. cosec. of the outer pol. dist., and the log. sines of the remainders: the sum (rejecting tens) is the log. sine square of the angle B.

(4.) For the angle C. Add together the arc A and the two zenith dists., and from half the sum subtract A and the outer zen. dist.; note the two remainders. If the half sum is the lesser, subtract it from the other quantity.

Add together the log. cosec. of A, the log. cosec. of the outer zen. dist., and the log. sines of the two remainders: the sum (rejecting tens) is the log. sine square of the angle C.

(5.) For the angle D. This is the sum, or diff., of B and C, according to the following directions:—

In the case of the same body.

Observations on the <i>same</i> side of the Meridian			Observations on <i>different</i> sides of the Meridian		
Pol. Dist. <i>greater</i> than Colat.	Pol. Dist. <i>less</i> than Colat. <i>greater</i> Alt. with <i>lesser</i> Azim.	<i>greater</i> Alt. with <i>greater</i> Azim.	Pol. Dist. <i>greater</i> than Colat.	Pol. Dist. <i>less</i> than Colat. Interval <i>less</i> than 12 ^h	Interval <i>greater</i> than 12 ^h
<i>diff.</i>	<i>sum</i>	<i>diff.</i>	<i>diff.</i>	<i>sum</i>	<i>diff.</i>

Note.—The difference of bearing in the interval must be *less* than 180°.

is PBA; angle C is ZBA; angle D is PBZ, which is PBA—ZBA. When PZ is larger and PA smaller, PBZ may be PBA+ZBA. Then the two sides PB, BZ, with the included angle PBZ, give PZ.

In the case of two stars, A and B are very nearly constant, and have accordingly been computed for certain pairs of stars, and inserted in tables, by which the computation is materially shortened.—*Tables for facilitating the Computation of Double Altitudes*, by LIEUT. SHADWELL, R.N. 1836.

6.) For the Latitude. Take the supplement of D to 180° . Take the sum of the outer polar and zenith distances.

Add together the log. sine square of the suppl. of D and the log. sines of the outer pol. and zen. dists.: the sum (rejecting tens) is the log. sine square of an auxiliary arc y .

Put this arc under the sum of the zen. and pol. dists.; take the sum and diff., and half sum and half diff.

Add together the log. sines of the last two terms: the sum (rejecting tens) is the log. sine square of the colatitude, reckoned from the same pole as the pol. dists.

Ex. 1. Interval, $32^\circ 54'$; the 1st and outer alt., corrected and reduced to the 2d place, is $48^\circ 39' 42''$; the 2d alt. $62^\circ 59' 36''$; outer pol. dist. $104^\circ 24' 30''$; the other, $104^\circ 24' 14''$.

For the Arc A.

Interval	$32^\circ 54'$	
Suppl.	$11\ 27\ 6$	sin. sq. 9.997761
Pol. Dist.	$104^\circ 24' 30''$	sin. 9.986121
Pol. Dist.	$104\ 24\ 12$	sin. 9.986130
Sum	$208\ 48\ 42$	
Auxly. arc x	$150\ 3\ 42$	sin. sq. 9.970012
Sum	$358\ 52\ 24$	
Diff.	$58\ 45\ 0$	
Half Sum	$179\ 26\ 12$	sin. 7.992640
Half Diff.	$29\ 22\ 30$	sin. 9.690660
Arc A	$7^\circ 57' 52''$	sin. sq. 7.623300

For the Angle B.

Arc A	$7^\circ 57' 52''$	cosec. 0.858367
Outer p. d.	$104\ 24\ 30$	cosec. 0.013879
Inner p. d.	$104\ 24\ 12$	
	$216\ 46\ 34$	
	$108\ 23\ 17$	
	$100\ 25\ 25$	sin. 9.992773
	$3\ 58\ 47$	sin. 8.841384
Angle B	$90^\circ 59' 20''$	sin. sq. 9.706403

For the Angle C.

Arc A	$7^\circ 57' 52''$	cosec. 0.858367
Outer z. d.	$31\ 20\ 18$	cosec. 0.283921
Inner z. d.	$27\ 0\ 24$	
	$66\ 18\ 34$	
	$33\ 9\ 17$	
	$25\ 11\ 25$	sin. 9.629028
	$1\ 48\ 59$	sin. 8.501014
Angle C	$51^\circ 16' 31''$	sin. sq. 9.272310

The observations are on the same side of the meridian, and the pol. dist. greater than the solst.: hence D is the diff. of B and C, and is therefore $39^\circ 42' 49''$.*

For the Latitude.

Arc D	$39^\circ 42' 49''$	
Suppl.	$140\ 17\ 11$	sin. sq. 9.946759
Outer Pol. Dist.	$104\ 24\ 30$	sin. 9.986121
Outer Zen. Dist.	$31\ 20\ 18$	sin. 9.716079
	$135\ 44\ 48$	
Auxly. Arc y	$83\ 45\ 20$	sin. sq. 9.648950
	$219\ 37\ 8$	
	$51\ 59\ 28$	
	$109\ 45\ 4$	sin. 9.973668
	$25\ 59\ 44$	sin. 9.641773
	$79^\circ 55' 24''$	sin. sq. 9.615441
LATITUDE	$10\ 4\ 36\ S.$	

* A general rule for assigning the sum or the diff. of B and C, in the case of *diff. alt.*

This process is less troublesome than it appears. The 1st and 4th steps are of the same form, as are, also, the 2d and 3d.*

Ex. 2. Lat. by acc. 12° S.; true alt. of Sirius, $71^{\circ} 56' 42''$, pol. dist. $73^{\circ} 30' 18''$; true alt. of Canopus, $47^{\circ} 13' 36''$, pol. dist. $37^{\circ} 23' 30''$; diff. of R.A. $17^{\text{m}} 29^{\text{s}}$. Both stars to the eastward, and Sirius the outer one or easternmost.

The arc x is $99^{\circ} 22' 15''$; A is $36^{\circ} 16' 45''$; angle B, $4^{\circ} 30' 10''$; angle C, $100^{\circ} 10' 33''$; the angle D, the sum of B and C, is $104^{\circ} 40' 43''$. The arc y is $38^{\circ} 54' 38''$, and the LAT. $11^{\circ} 13' 27''$ S.

771. *Degree of Dependence.* The lat. by double altitude is affected by the errors of altitudes, pol. dists., and interval, or polar angle. The effect is the same, whether by the approximate or rigorous process.

(1.) To find the error of lat. caused by 1' error in one of the alts. To the log. 3.431 add the log. sine of the azimuth at that alt. and the log. from Table 71: the sum (rejecting tens) is the prop. log. of the error required, nearly.

Ex. Suppose in Ex. 1, No. 768, the alt. of Canopus is 3' in error.

Canopus az. 14°	sin.	$3' 43$	The ERROR OF LAT. is therefore about $3' 24''$.
14° and 72° , Tab. 71		$9' 38$	
		$9' 39$	
$1' 8''$		$2' 20$	

(2.) The error of pol. dist. will be worth notice only in the case of the moon, in consequence of her rapid change of declination, and the uncertainty of the Green. Date.

Find the error of each hour-angle in which the moon's pol. dist. is involved by No. 615 (3). This gives the error of the computed interval; and the error of the correction of lat. is the same part of the corr. itself, that the error of the computed interval is of that interval.

(3.) The error of the rate of the watch will rarely be sensible.

bodies, would require the hour-angles to be known; but the observer who is well acquainted with the positions of the circles, as shewn in the figures, p. 162, will perceive at the time of observation how the angle D is composed.

* When the lat. is found, the hour-angle and azimuth may be computed thus:—

For the hour-angle. To the log. sine of D add the log. sine of the outer zen. dist. (already taken out) and the log. sec. of the lat.: the sum is the log. sine of the hour-angle corresponding, or of its suppl. Circumstances will usually decide; but, in a doubtful case, take the sum of the log. sines of the decl. and lat.: if this is less than the log. cos. of the zen. dist., the hour-angle is found; if greater, take the supplement.

For the azimuth. To the log. sine of D add the log. sine of the outer pol. dist. (already taken out) and the log. sec. of the lat.: the sum is the log. sine of the azim. or its suppl. If this is doubtful, when the sum of the log. sine of the lat. and cos. of the zen. dist. is less than the log. sine of the decl., the azim. is found; if greater, take the suppl. Reckon the azimuth from the N. in N. lat., and S. in S. lat.

V. BY THE ALTITUDE OF THE POLE STAR.

772. *The Observation.* Observe the alt. of the pole star, noting the time. On shore, note also the thermometer and barometer.

773. *The Computation. At Sea.* (1.) The error of the Watch on A.T. being known, take the R.A. of the sun from the Nautical Almanac, or Table 61, and add the A.T. of observation to it: the result is the R.A. of the meridian.

(2.) Correct the alt. for index-error, dip, and refraction.

(3.) Enter Table 51 with the R.A. of the mer. and the alt.; take out the correction, and apply it as there directed: the result is the latitude, north.

Ex. 1. July 5th, 1897, at 11^h 2^m P.M.
app. time, obs. alt. of the pole star, 51° 20';
ind. corr. + 2'; height of eye 16 feet: re-
quired the Latitude.

App. Time	11 ^h 2 ^m
R.A. ☉	6 58
R.A. Mer.	18 0
* Obs. Alt.	51° 20'
Ind. Corr. + 2' }	
Table 38 - 5 }	- 3
	51 17
18 ^h 0 ^m , Alt. 50°	+ 27
LAT.	51 44 N.

Ex. 2. March 11th, 1890, at 3^h 30^m A.M.
app. time, obs. alt. of the pole star, 53° 51';
ind. corr. - 3'; height of eye 12 feet: re-
quired the Latitude.

App. Time	15 ^h 30 ^m
R.A. ☉	23 26
	38 56
	- 24
R.A. Mer.	14 56
* Obs. Alt.	53° 51'
Ind. Corr. - 3' }	
Table 38 - 4 }	- 7
	53 44
15 ^h 0 ^m , alt. 50°	+ 1 9
LAT.	54 53 N.

774. *Accurately.* (1.) Find the Greenwich Date; reduce to it the Sid. T. at mean noon; take out the star's R.A. and decl. from the Nautical Almanac, and find the pol. dist.

Find the star's hour-angle.

(2.) Correct the altitude, accurately.

(3.) For the 1st Correction. To the log. sec. of the hour-angle add the prop. log. of the pol. dist.: the sum (rejecting tens) is the prop. log. of the 1st Correction.

For the 2d Correction. To the log. cosec. of the hour-angle add the prop. log. of the pol. dist.; double the sum; add to this the const. 1.5821 and the log. cot. of the altitude: the sum (rejecting tens) is the prop. log. of the 2d Correction.

(4.) When the hour-angle is *greater* than 6^h and *less* than 18^h, *add* the 1st Corr. to the altitude; when the hour-angle is *less* than 6^h or *greater* than 18^h, *subtract* it.

Add the 2d Correction in all cases

Ex. July 24th, 1890, long. $0^h 6^m W.$; at $10^h 24^m 12^s.8$ obs. alt. of Polaris in the quicksilver, $109^{\circ} 36' 40''$; ind. corr. $-1' 30''$, therm. 62° , bar. 30.0 inches: required the Latitude.

Gr. Date, 24th, $10^h 30^m 13^s$	
Sid. T. mean noon, 24th $8^h 8^m 18^s.2$	
10^h $1^m 38^s.6$	
30^m $4^s.9$	+ 1 43.5
13^s 0	
Red. Sid. Time	$8^h 10^m 1^s.7$
M.T.	$10^h 24^m 12^s.8$
R.A. Mer.	$18^h 34^m 14^s.5$
* R.A.	$-1^h 14^m 2^s.1$
Hour-angle	$17^h 20^m 12^s.4$
Or	$5^h 20^m 12^s.4$
1st Corr.	2d Corr.
$5^h 20^m 12^s$ Sec. 0.7625 cosec. 0.0066	
P.D. $1^{\circ} 16' 56''$ P.L. 0.3092 P.L. 0.3692	
1st Corr. $13' 17''$ P.L. 1.1317	0.3758
	2
	0.7516
	Const. $1^s.5821$
	$54^{\circ} 47'$ cut. $9^s.8487$
2d Corr. $1' 11''$ P.L. $2^s.1824$	

* R.A.	$1^h 14^m 2^s.1$
Decl.	$88^{\circ} 39' 31''$
Alt.	$109^{\circ} 36' 40''$
Ind. Corr.	$-1^s.30$
	$2)109^{\circ} 35' 10''$
	$54^{\circ} 47' 35''$
Ref. $41''$	}
Ther. 1	
	-40
True Alt.	$54^{\circ} 46' 55''$
1st Corr.	$13' 17''$
2d Corr.	$1' 11''$
Lat.	$55^{\circ} 1' 23'' N.$

775. *Degree of Dependence.* The error is very nearly the same as that of the alt., as a small error of time produces but little effect.

N.B.—The Nautical Almanac method for obtaining Latitude from Pole Star is strongly recommended. Every year tables are calculated expressly for this purpose. Where accuracy is required, as in observations for latitude made on shore, these yearly tables should always be used.

CHAPTER VI.

FINDING THE TIME.

I. BY A SINGLE ALTITUDE. II. BY DIFFERENCE OF ALTITUDE NEAR THE MERIDIAN. III. BY EQUAL ALTITUDES. IV. RATING THE CHRONOMETER.

776. In consequence of the perpetual revolution of the celestial bodies, the hour-angle of any one of them affords the measure of time, No. 471, &c. By whatever method, therefore, the hour-angle may be determined, the time may be deduced. At sea, where the only fixed object to which the ever-changing positions of the celestial bodies can be referred is the horizon, altitude is the only means of determining the time.

I. BY A SINGLE ALTITUDE.

777. The sun's hour-angle being apparent time, when his alt. is observed, the time is at once determined. In the case of any other

celestial body which does not pass the meridian with the sun, it is necessary to allow for the difference of their hour-angles, or of their right ascensions (No. 471), at the instant of observation, by referring both bodies to the first point of Aries (from which R.A. is reckoned), as will be described.

1. *Altitude above the Horizon.*

778. Limits. The body should be nearly E. or W., because, when on the prime vertical, errors, both of the latitude of the observer, and of the altitude observed, produce the least effect on the hour-angle.

In general, however, the body may be observed at any time, while moving at the rate of not less than 6' of alt. in 1^m of time; because in this case an error of 1' in the alt. will cause not more than 10^s error of time, and the same error of lat. will in the same case cause a still smaller error of time. The *smallest* azimuth, reckoned either from N. or S., which the body can have under this last condition, is seen in Table 46, in the column of 6'.

On the other hand, the alt. should not be observed when small, as, for ex., under 10° or 15°, on account of the uncertainty of refraction, especially in very hot or very cold weather.

779. In lat. 60° 24' and upwards, 1' error of alt. must always cause more than 10^s error of time; the body should therefore be observed as nearly E. and W. as possible.

In the tropics, on the other hand, the time may often be more correctly determined, when the body is less than an hour from the meridian, than at several hours from it in high latitudes.

At sea, the uncertainty of the sea-horizon may sometimes be removed by observing to opposite points. Errors of alt. proper to the instrument, or to the eye, are obviated by observing the alt., of the same measure, on opposite sides of the meridian.

[1.] *To find Apparent Time, and thence Mean Time, by the Altitude of the Sun.*

780. The Observation. Observe a set of altitudes, (Number 557) at the proper limits, noting the times. See also No. 535.

For accuracy, note the thermometer and barometer.

781. The Computation. (1.) Having found the time corresponding to the altitude, find the Green. Date by the chronometer No. 575, which will be mean time; or by the time roughly estimated and the long. by acc., No. 576, which will generally be App. Time. Reduce to this the sun's declination, No. 580, or, for common purposes at sea, this may be done by No. 579. Find the sun's polar distance, No. 443.

When mean time is required, reduce the Equation of Time. No. 583 or 584.

(2.) Correct the alt. at sea by No. 647, or, if greater accuracy is required, by No. 649.

(3.) Compute the sun's hour-angle, No. 614.

(4.) When the sun is to the W. (or P.M.), this hour-angle is

Apparent Time; when he is to the E. (or A.M.), subtract the hour-angle from 24^h : the remainder is A.T. reckoned on the *day before*.

(5) For Mean Time. Apply the reduced equation of time as directed in p. I. of the Nautical Almanac, or in Table 62, to the App. Time: the result is Mean Time.

The difference between the time of observation, as shewn by the watch, and either of these times, is the error of the watch on that time.

Ex. 1.* Jan. 12th, 1902, at sea, at about $9^h 30^m$ A.M. app. time; lat. $35^\circ 35' N.$; long. $14^\circ W.$; height of eye, 30 feet; ind. corr. $+4' 30''$; obs. alt. of sun as below: required app. and mean time, and the error of the watch on each time, at the instant of observation.

Note.—The differences of the alts. and the times are taken to test their accuracy by means of their agreement with each other, No. 556.

Times by W.	$9^h 30^m 28^s$	Diff.	Alt.	$22^\circ 18' 20''$	Diff.
	31 3	$0^m 35^s$		23	$4' 40''$
	31 34	31		26 50	3 50
	32 7	33		30 40	3 50
	32 34	27		34	3 20
	<u>157 46</u>			<u>132 50</u>	
Time	9 31 33		Alt.	22 26 34	
Jan.	$11^d 21^h 30^m$		O's. Alt. ☉	$22^\circ 26' 34''$	
Long. $14^\circ W.$	<u>+ 56</u>		Index error	+ 4 30	
G.A.T. Jan.	11 22 26		Table 38	+ 8 0	
Decl. 11^d	$21^\circ 54' 19'' S.$		True Alt.	22 39 4	
Corr.	<u>- 8 52</u>		A.T. at Ship	$21^h 32^m 45^s$	
Red. Decl.	21 45 27 S.		Watch	21 31 33	
	<u>90</u>		Watch slow for A.T.	<u>1 12</u>	
Pol. Dist.	111 45 27		A.T. at Ship	21 32 45	
Eq. Time 11^d	$7^m 51^s$		Eq. Time	+ 8 13	
Corr.	<u>+ 22</u>		M. Time	21 40 58	
Real. Eq. Time	8 13		Watch	21 31 33	
Alt.	$22^\circ 39'$		Slow for M.T.	<u>9 25</u>	
Lat.	35 55	sec. 0.09158	Chronometer Time		
P.D.	111 45	cosec. 0.03207	of Observation	$10^h 39^m 49^s$	
	<u>170 19</u>		Chr. fast on G.M.T.	<u>- 2 31</u>	
	85 9	cos. 8.92710	G.M.T. of Obs.	10 37 18	
	62 30	sine 9.94793	Ship M.T. of Obs.	<u>9 40 58</u>	
Hour-angle $2^h 27^m 15^s$	sin. sq. 8.99868			<u>56 20</u>	
A.T.	21 32 45		Long. See No. 827	$14^\circ 5' 0'' W.$	

Ex. 2. March 12th, at about $4^h 15^m$ P.M. mean time, lat. $50^\circ 48' N.$, long. $65^\circ 58' E.$; obs. alt. ☉ $14^\circ 50' 10''$; corresponding time by W. $4^h 13^m 54^s$; ind. corr. $-2' 20''$; height of eye, 18 feet: required A.T. and M.T. and the error of the watch on each

G.M.T. March $11^d 23^h 51^m$, pol. dist. $93^\circ 15'$, true alt. $14^\circ 55'$, Eq. T. $+9^m 55^s$; hour-angle P.M. or A.T. $4^h 5^m 54^s$; watch fast on A.T. 8^m ; M.T. $4^h 15^m 49^s$, watch slow on M.T. $1^m 55^s$.

* In this example some of the quantities are noted to seconds for the sake of a form; but at sea the nearest minute (to which the hour-angle is here worked) is generally enough, unless the observation itself is remarkably good.

Ex. 3. Oct. 20^h 1878, at sea, at 4^h 40^m P.M. app. time; lat. 41° 18' S., long. 21° W.; height of eye 16 feet; ind. corr. - 2'; at 4^h 28^m 56^s by watch, obs. alt. \odot 23° 7': required A.T. and M.T. and the Error of the Watch on each.

G.A.T. Oct. 20^h 6^h 4^m, pol. dist. 79° 31', true alt. 23° 15', Eq. T. - 15^m 11^s; A.T. 4^h 32^m 42^s; Watch *slow* on A.T. 3^m 46^s; M.F. 4^h 17^m 31^s; Watch *fast* on M.T. 11^m 25^s.

[2.] *To find Mean Time, and thence Apparent Time, by the Altitude of a Star.*

782. *The Observation* is the same as for the sun, Nos. 541, 542.

783. *The Computation.* (1) Having found the means of the times and the altitudes, take from the Nautical Almanac, or Table 63, the star's R.A. and declin., and also from the Nautical Almanac, or Table 61, the sidereal time at mean noon for the given day.

(2) Correct the altitude, No. 652 or 653.

(3) Compute the star's hour-angle, No. 614.

(4) When the star is to the W. of the meridian, *add* the hour-angle to the star's R.A.; when to the E., *subtract* the star's hour-angle from its R.A. (increased if necessary by 24^h); the result is the R.A. of the meridian.

From the latter (increased if necessary by 24^h) subtract the sidereal time at mean noon; the rem. is the approximate M.T.

From this last subtract the Retardation upon it, Table 24.

Take out the Acceleration for the long.; in W. long *subtract* the Accel. from the result, in E. long. *add* it; the result, if less than 12^h, is Mean Time; if greater than 12^h, reckon the time on the preceding day.

(5.) For App. Time. By the M.T. obtained, and the long. by acc., or by the chronometer, find the Gr. Date; reduce the equation of time and apply it as directed in p. II. of the Nautical Almanac, or the contrary way to that directed in Table 62.

Ex. 1. Jan. 1st, 1902, P.M., lat. 50° 46' N., long. 61° 37' W., at 7^h 56^m 18^s by watch, obs. alt of Procyon 15° 40' to the S. and E., eye 20 feet, ind. err. 0': required the Mean and App. Times, and the Error of the Watch.

Procyon's R.A. 7^h 34^m 10^s; Decl. 5° 28' N.; Sid. T. mean noon, 18^h 40^m 48^s.

Obs. Alt.	15° 40'	Alt.	15° 32'		Hour-angle	- 4 ^h 48 ^m 12 ^s
Ind. Corr. 0' }	- 8	Lat.	50 46	sec. 0.19895	* R.A.	7 34 10
Table 38 - 8 }		P.D.	84 32	cosec. 0.00198	R.A. Mer. (+ 24 ^h)	2 45 58
True Alt.	15 32		150 50		Sid. T. M. Noon -	18 40 48
			75 25	cos. 9.40103	Approx. M.T.	8 5 10
Chr. at Time } h m s			59 53	sine 9.93702	Ret.	- 1 19
of Obs. }	12 11 30			sin. sq. 9.53898		8 3 51
Chr. fast on Gr.	- 2 15	4 ^h 48 ^m 12 ^s			Accel. 61° 37' W.	- 40
Gr. M.T.	12 9 15				M.T.	8 3 11
Ship M.T.	8 3 11				Time by Watch	7 56 18
Long. in Time	4 6 4				Watch <i>slow</i> on M.T.	6 53
Long.	61° 31' 0" W.					

The Red. Eq. T. is 3^m 34^s, which *subtracted* from M.T. gives A.T. 7^h 59^m 37^s, and the watch *slow* on A.T. 3^m 19^s.

Ex. 2. April 27th, 1902, A.M., lat. $29^{\circ} 47' 45''$ S., long. $31^{\circ} 7' \text{ E.}$ at $2^{\text{h}} 19^{\text{m}} 41^{\text{s}}$ by watch, obtained true alt. of Altair $25^{\circ} 14' 20''$ to the E. and N.: required the M.T. of observation.

Altair's R.A. $19^{\text{h}} 46^{\text{m}} 2^{\text{s}}$, Decl. $8^{\circ} 36' 35'' \text{ N.}$, Sid. T. M. Noon $2^{\text{h}} 18^{\text{m}} 9^{\text{s}}$.

Alt.	$25^{\circ} 14' 20''$		Hour-angle	$-3^{\text{h}} 37^{\text{m}} 8^{\text{s}}$
Lat.	$29 47 45$	sec. 0.061561	* R.A.	$19 46 2$
P.D.	$98 36 35$	cosec. 0.004920	R.A. Mer.	$16 8 54$
	$153 38 40$		Sid. T. M. Noon	$-2 18 9$
	$76 49 20$	cos. 9.357794	Approx. M.T.	$13 50 45$
	$51 35 0$	sin. 9.894046	Ret.	$-2 16$
$3^{\text{h}} 37^{\text{m}} 8^{\text{s}}$		sin. sq. 9.318321		$13 48 29$
			Accel. long. $31^{\circ} 7' \text{ E.}$	$+0 20$
			MEAN TIME	$13 48 49$

[3.] To find Mean Time, and thence Apparent Time, by the Altitude of the Moon or a Planet.

784. The Observation is the same as for the sun. See, also, Nos. 540, 541, 542.

785. The Computation. (1.) Having found the means of the times and of the altitudes, find the Gr. Date as nearly as possible by the chron., No. 575, or by the estimated M.T. and long. by acc., No. 576. Reduce the moon's R.A., No 591, and decl., No. 589, and thence her pol. dist.; also her horiz. parall., No. 586 or 587, and semid., Table 39.

(2.) Deduce the app. alt., No. 654. Take out the correction of alt., Table 39. Correct the altitude.

(3.) Compute the hour-angle, and proceed as for a star, 783 (4).

Ex. 1. July 21st, 1878, A.M., lat. $39^{\circ} 57' \text{ N.}$, long. $8^{\circ} 53' \text{ E.}$; M.T. at Green. by chron. $20^{\text{h}} 11^{\text{m}} 48^{\text{s}}$, obs. alt. $\underline{24^{\circ} 10'}$ E. of mer.; eye 16 feet.

☉'s R.A.	$0^{\text{h}} 33^{\text{m}} 19^{\text{s}}$	Obs. Alt.	$24^{\circ} 10'$
Corr.	$1 26$	Dip.	$-4'$
Red. R.A.	$0 34 45$	Semid.	$+15'$
☉'s Red. H.P.	$54' 13''$		$24 21$
☉'s Aug. Semid.	$14 53$	Corr. Par.	$+47$
☉'s Decl.	$8^{\circ} 26' 35'' \text{ N.}$	True Alt.	$25 8$
	$1 2$		
Red. Decl.	$8 27 37 \text{ N.}$	☉'s R.A. (+24 ^h)	$0^{\text{h}} 34^{\text{m}} 45^{\text{s}}$
	90	Hour-angle	$-4 16 45$
Pol. Dist.	$81 32 23$	R.A. of mer.	$20 18 0$
Alt.	$25^{\circ} 8'$	Sid. T. M. Noon	$7 52 32$
Lat.	$39 57$	Approx. M.T. at ship	$12 25 28$
Pol Dist.	$81 32$	Ret.	$-3 2$
	$146 37$		$12 22 26$
	$73 18\frac{1}{2}$	Accel. for $8^{\circ} 53' \text{ E.}$	$+6$
	$48 10\frac{1}{2}$	M.T. at Ship	$12 23 32$
$4^{\text{h}} 16^{\text{m}} 45^{\text{s}}$			
	sec. 0.11543		
	cosec. 0.00476		
	cos. 9.45822		
	sin. 9.87226		
	sin. sq. 9.45067		

Ex. 2. Feb. 22d, 1878, at about $9^{\text{h}} 30^{\text{m}} \text{ P.M.}$, lat. $42^{\circ} 40' \text{ N.}$, long. 140° W. , obs. alt. Mars $23^{\circ} 43' \text{ W.}$ of mer., time by watch $9^{\text{h}} 24^{\text{m}} 27^{\text{s}} \text{ P.M.}$, eye 18 feet: find M.T. and Error of Watch.

G. T. Feb. 22^d 18^h 50^m, Mar's Red. R.A. $2^{\text{h}} 47^{\text{m}} 33^{\text{s}}$, Red. Decl. $1^{\circ} 10' \text{ N.}$, True Alt $48^{\circ} 37'$.

Alt. $23^{\circ} 37'$			Hour-angle	$4^h 53^m 39^s$ W.
Lat. $42^{\circ} 40'$	sec. $0^{\circ} 13353$		Mars' R.A.	$2^h 47^m 33^s$
1 st D. $72^{\circ} 50'$	cosec. $0^{\circ} 01979$		R. A. of Mer.	$7^h 41^m 12^s$
$139^{\circ} 7'$			Sid. T.M. Noon	$22^h 9^m 2^s$
$69^{\circ} 33\frac{1}{2}'$	cos. $9^{\circ} 54314$		Approx. M.T.	$9^h 32^m 10^s$
$45^{\circ} 56\frac{1}{2}'$	sin. $5^{\circ} 85651$		Ret.	$-1^m 34^s$
$4^h 53^m 30^s$	sin sq. $9^{\circ} 55297$			$9^h 30^m 36^s$
	\odot		Accel. 140° W.	$-1^m 32^s$
			M.T.	$9^h 29^m 4^s$

Whence the watch is $4^m 37^s$ slow on M. T.

786. When the true G.M.T. is given by a chronometer, the moon's R.A. and declination may be correctly found. When the moon is at her greatest declination, N. or S., a small error in the Gr. Date will but slightly affect her pol. dist. An error of 1^m in the Gr. Date causes about 2^s error in the moon's reduced R.A.

787. If the errors of the watch, as found by observation of two bodies on different sides of the meridian, but on the same side of the prime vertical, by the same observer with the same instrument, be not identical, that error is nearest to the true error of the watch which accompanies the greater or outer azimuth. If the azimuths are equal, the mean of the errors is the true error.

788. *Degree of Dependence.* The alt. and the lat. being in general, at sea, more or less uncertain, and the pol. dist. of the sun and moon being reducible with precision in certain cases only, the time is in general liable to three causes of error. See No. 615.

When it is proposed to test the observation, the parts to $30''$ for the sec., &c., will be taken out with those quantities.

2. By the Altitude 0, or the Body on the Horizon.

789. In low latitudes the entire orb of the sun is, during certain seasons, frequently seen at rising and setting; and in the variable climates of high latitudes it is occasionally visible, though more usually clouded at those times. When the instant at which either limb touches the horizon can be distinctly noted, the time may be determined approximately; and though the degree of approximation be rude as compared with some other methods, yet the result may often be valuable, especially after one or more days without observation. It is also a recommendation to this method, as a resource when others fail, that it is independent of every instrument except a watch or other means of measuring time.*

(1.) Find the time of sunrise or sunset in Table 26. Apply to this the long. in time, as directed, No. 576: the result is the Green. Date. Reduce the declination, and find the pol. dist.

(2.) To the horizontal refraction, $33'$, add the depression, Table 8, and from the sum subtract the semid. when the lower limb is ob-

* Mr. Fisher acquaints me that he has employed this observation on a few occasions, but circumstances were not convenient for comparing the results with those of other observations.

served, or *add* it when the *upper* limb is observed: the result is the angular depression of the sun's centre below the horizon at the instant of observation.

(3.) Compute the hour-angle of the sun below the horizon by No. 642, using, instead of 18° , the sun's depression.*

(4.) At sunset this hour-angle is app. time; at sunrise take the suppl. to 12 hours.

Ex. 1. May 12th, 1878, lat. $51^\circ 20'$ N., long. 26° W., observed the sun's lower limb at setting touch the horizon at $7^h 40^m 56^s$ by watch; eye 16 feet: required App. Time.

☉ Decl. 18° . Table 26 gives	Hor. Refr.	33'	Depr.	$0^\circ 21'$		
App. Time Sunset $7^h 35^m$.	Depr.	4	Lat.	51 20	sec.	0°20427
Long. 26° W.		37	P.D.	71 44	cosec.	0°02246
G.A.T. 12th	Semid.	-16		123 25		
	Depr. Centre	21		61 42	sin.	9°04472
Decl. 12th				61 21	cos.	9°68075
Corr.					sin. sq.	9°85220
Red. Decl.						
	A.T.	$7^h 40^m 7^s$				
	Watch	$7^h 40^m 56^s$				
						0 49 Watch fast.

Ex. 2. Oct. 14th, 1878, lat. $18^\circ 39'$ N., long. $62^\circ 30'$ E., the sun's upper limb at rising appeared on the horizon at $5^h 46^m 11^s$ by watch; eye 20 feet: required App. Time.

Gr. Date, Oct. 13^d 14^h 0^m, red. decl. $8^\circ 3'$ S.; depr. of sun's centre $54'$; Hour-angle $5^h 52^m 54^s$; App. Time $6^h 7^m 6^s$ A.M.; watch $20^m 55^s$ slow on A.T.

790. *Degree of Dependence.* This we have at present no certain data for determining, more especially when the observation is taken from a considerable elevation, as from a hill.

The terrestrial refraction does not, it should seem, affect the instant of the apparent passage of a celestial body over the visible horizon, since the rays of light from the horizon and those from the body are similarly affected; and hence the uncertainty of the result is probably due entirely to that of the astronomical refraction at the time and place. It may be proper, accordingly, to admit an error of $2'$, at least, in the refraction; and the effect on the result is then found by merely adding together the parts for $30''$ of the cosine and sine, dividing the sum by the parts for $1''$ of the sine square, and doubling the result.

Ex. In Ex. 1, above, the parts are 34 and 116; the sum, divided by 20, gives $7\frac{1}{2}''$, which, doubled, is $15''$, the effect due to $2'$ error in the refr. In Ex. 2 this is $8''$.

* In the tropics the method No. 638 may be substituted, using log. sine depr. \odot cent.

As an aid to the working of a sun chronometer, Davis's "Chronometer" Tables will be found very useful; they contain hour angles calculated exactly for degrees of Latitude, Altitude, and Declination, with means of making allowance for the minutes which must be taken into account. J. D. Potter, 145 Minorics, London, E., price 10s. 6d.

II. BY DIFFERENCE OF ALTITUDE NEAR THE MERIDIAN.

791. When the sun is too near the meridian for a satisfactory observation of a single altitude, the time may be determined approximately, and sometimes nearly, by means of the observed difference of alt. in a measured interval.

The method has been already introduced in the Short Double Altitude, p. 256, and it was on the ground that the same observation might be usefully employed for Time also, that the small corrections from p. 223, which are scarcely appreciable in the resulting latitude, were applied. It is also worth while, in finding the time by this method, to correct for change of declination.

The method (as already shewn in Case II., p. 259) is available with alts. taken on both sides of the meridian; but, as this case would be comparatively rare, the rules have been arranged for observations on the *same* side of the meridian only.*

792. *Limits.* The observations should both be within an hour from noon. The interval should constitute a large portion of the mid. time from noon; but it should not, generally, amount to the whole time from noon.

The Observation is that in No. 726.

793. *The Computation.* (1.) Reduce the declin., by the long., to noon at the place, which will be near enough.

(2.) Find the interval, and correct the second of the times by watch for the rate in the interval, when considerable. Correct the alts., and reduce the 1st to the place of the 2d; find their mean and their difference. Correct the diff. of alts., and also the interval by the quantity in the Table, p. 223.†

(3.) Compute the hour-angle at the middle of the interval, No. 729 (2), and add half the interval. When the observation is P.M. this is App. T., and being compared with the second time by watch, shews the error of the watch. When the observation is A.M., take the suppl. of this time to 12^h.

Note. If the rising or falling of the sun has not been distinctly noticed, or it is uncertain whether the alts. are on the same or different sides of the meridian, ascertain the fact by the precept, No. 728.

* For the like reason, namely, not to increase unnecessarily the number of precepts, the observation below the pole is not treated; this presents no difficulty.

† This is the quantity which, added to the sine, makes it equal to the arc, and by means of it we employ the table of sines equally well for arcs.

Ex. 1. May 14th, 1878, about 11^h A.M., lat. 48° 4' N., long. 21° 11' W., at 11^h 28^m 20^s by watch, obs. alt. ☉ 58° 9'; at 11^h 52^m 50^s by watch, obs. alt. ☉ 59° 39'; ind. corr. -1' 20"; height of eye, 16 feet; rate, 5½ knots; ☉ a-head at 1st obs.: required the Error of the Watch.

Times by } 11 ^h 28 ^m 20 ^s	Alt. ☉ 58° 9' 0"	Alt. ☉ 59° 39' 0"	Alts. 58° 21' 11"
Watch } 11 52 50	Ind. Corr. -1 20	-1 20	59 49 1
Interv. 24 30	Dip -4 0	-4 0	118 10 12
Corr. 24 33	58 3 40	59 33 40	Mean 59 5 6
☉ Decl. 14th 18° 40' N.	Corr. Alt. -32	-30	Diff. 1 27 50
21° W. +1	Semid. 58 3 8	59 33 10	Corr. +1
Red. Decl. 18 41 N.	+15 51	+15 51	1 27 51
	Run 58 18 59	2d Alt. 59 49 1	
	1st Alt. 58 21 11		
Diff. Alts. 1° 27' 51"	sine 8.4074	Hour-angle 0 ^h 44 ^m 44 ^s	
Interv. 24 ^m 33 ^s	cosec. 0.9710	Comp. Mid. T. 11 15 16	
Lat. 48° 4'	sec. 0.1750	Half Int. +12 15	
Decl. 18 41	sec. 0.0235	T. of 2d Obs. computed 11 27 31	
Mean Alt. 59 5	cos. 9.7108	Do. by Watch 11 52 50	
Hour-angle 0 ^h 44 ^m 44 ^s	sine 9.2877	Watch fast 25 19	

Ex. 2. Lat. 10° 41' S., red. decl. 20° 56' N., alts. ☉ 58° 2' and 57° 17', interval 12^m 14^s Computed App. Time of 2d Observation, 0^h 39^m 0^s.

794. *Correction for Change of Declination.* When the sun is on the meridian, his motion in declination (which then takes place on the meridian) is perp. to the horizon, and consequently affects the alt. by exactly the same quantity. When, on the other hand, that part of the sun's celestial meridian or declin. circle, on which he is, is parallel to the horizon, his change of declin. does not affect the alt. at all. Hence the corresponding change of alt. is always between 0 and the whole amount of change of declination.

The 2d alt. differs therefore by the whole, or a part, of the change of declin. in the interval, from what it would have been had the decl. remained constant. When the motion in declin. tends to increase the alt. the 2d alt. is too great; otherwise too small. There is, however, no necessity, in this method, for a very nice process of correction, for when the mer. alt. is small, and the sun not far from the meridian, the motion in declin. corresponds very nearly to that of alt., and the entire change may be applied; and when, on the other hand, the mer. alt. is great, the motion in alt. is so rapid, that a few seconds, in the estimation, are of no consequence in practice, or the whole quantity may even be neglected.

Ex. 1. May 3rd, 1878, lat. 26° 14' N., long. 161° W., at 10^h 31^m 18^s by watch, obtained true alt. ☉ 71° 49', and at 11^h 7^m 21^s true alt. 77° 46': find the Error of the Watch.

The Hour-angle is 46^m 18^s, Mid. T. 11^h 13^m 42^s, and Watch slow 24^m 22^s.

Ex. 2. Nov. 4th, 1878, P.M., lat. 63° 46' N., long. 54° W., at 2^h 14^m 56^s by watch, obs. alt. ☉ 10° 18' 1", and at 2^h 36^m 27^s obs. alt. ☉ 10° 2' 29". Ind. corr. +2', height of eye 16 feet, the ship having no way.

The diff. alts. 15' 40", and Int. 21^m 32^s (corr. by 1"), give Mid. T. 25^m 46^s. The change of decl. 17', added to 2d alt. gives diff. alts. 15' 23", and corrected Mid. T. 25^m 18^s.

795. *Degree of Dependence.* As the interval may be measured

with precision, and as the lat., declin., and alt., are required approximately only, the value of the result depends almost entirely on the diff. alts.

(1.) The error of the mid. time due to a given error in the diff. alt. is found by taking away the sine employed, and adding that of the diff. alts. vitiated by a proposed error. The result is more trustworthy as the diff. alts. is greater.

In Ex. 1, No. 793, lat. $48^{\circ} 4' N.$, an error of $30''$ in the diff. of alts. causes 15° error of time; the obs. alts. would be better nearer noon.

In Ex. 1, No. 794, $30''$ error of diff. alts. causes 4° error of time.

In Ex. 2, No. 793, $30''$ error of diff. alts. causes 22° error of time.

In Ex. 2, No. 794, lat. $63^{\circ} 46'$, $30''$ error of diff. alts. causes 48° . The case is unfavourable from the smallness of the motion in alt.

(2.) The chief merit of the method is its insensibility to an error in the latitude, which, under the same circumstances, renders the observation of a Single Alt. useless. The effect of a proposed error is found by changing the sec. lat. before employed for the sec. of the lat. proposed.

In the following examples the effect of an error of lat. in the result by Single Alt. also is noted for comparison of the two methods.

In Ex. 1, No. 794, lat. $26^{\circ} 14'$, $10'$ error of lat. (that is, using $26^{\circ} 24'$) causes only 4° error of time. The effect of this error on the time by the single alt. $71^{\circ} 49'$ would be 28° .

In Ex. 2, No. 793, $10'$ error of lat. causes 1° error of time. The error of time by the single alt. $57^{\circ} 17'$ would be $2^{\text{m}} 9^{\text{s}}$.

Since a single alt. very near the meridian cannot be employed for finding the time, and since the latitude at sea is usually uncertain some miles, unless it has been determined very recently, the above method is adapted to finding the time at ship during that portion of the day when the single altitude is not practicable.

III. BY EQUAL ALTITUDES.

796. Since the altitude of a body which does not change its declination varies exactly at the same rate while rising on the E. side of the meridian as while falling on the W. side, the same altitude occurs at the same hour-angle on each side of the meridian, and the middle point of time between the instants of two equal altitudes is the instant at which the body passes the meridian. Hence the time and, consequently, the error of the watch, may be found by observation of equal altitudes.

In the case of the sun, the middle point of time, or the mean of the observed times of equal altitudes A.M. and P.M., is apparent noon. In the case of a star, or other celestial body, the mean of the observed times corresponds to the R.A. of the star when on the meridian, that is, to the sidereal time, which may be converted into A.T. or M.T.

797. Since the sun changes his declination sensibly in large intervals of time, two equal alts. A.M. and P.M. do not in general correspond to equal hour-angles, and it becomes necessary to apply to the mean of the observed times a correction, which is called the *Equation of Equal Altitudes*.

The object of the computation is to find what time the watch shewed when the body was on the meridian; the rate, therefore, does not affect the result, unless it is irregular, in which case the mean of the A.M. and P.M. times is not the time shewn by the watch when the interval is half expired.

In like manner, the variation of the sun's motion in R.A. (which is the variation of the equation of time) produces no effect, provided it be uniform. The irregularity of this variation is inconsiderable

1. *Equal Altitudes at Sea.*

798. When the course made good during the interval of the observation of two equal altitudes is true E. or W., the ship changes her longitude only by the portion of time which she gains or loses on the sun in the interval; this change introduces no correction, and the only question is the time by watch when the interval is half expired. But when the ship changes her latitude, the same altitude no longer corresponds to the same time from noon, and a correction becomes necessary.*

799. This method, though but approximate, has some advantages: it is independent of the terrestrial refraction, provided this remains unchanged in the interval employed; and the correction for change of lat., when necessary, requires the lat. and alt. to be but roughly known. In the tropics the interval may in general be very small, on account of the rapid change of altitude, and the correction for change of latitude in such cases may sometimes be omitted. In high latitudes, on the contrary, the ship's change of latitude considerably alters the time from noon at which the 2d alt. (which should be equal to the 1st) is taken: hence, in such cases, the method is less useful.

Note.—As the equation of equal alts. is generally a small quantity as compared with the correction due to change of place, we shall not here consider it. If, however, it is required to introduce it, proceed afterwards to No. 806.

800. *The Observation.* Observe the sun's alt. before noon, noting the time. Note the instant of the same alt. of the same limb P.M. For greater accuracy, several equal alts. should be obtained.

When the motion in alt. is quick, both limbs may be observed.

801. *The Computation.* (1.) Take the mean of the A.M. and P.M. times by watch; this, when the ship does not change her lat., is the mean time by watch of apparent noon. Then the Equation of Time applied as to *Mean Time*, will give the time of mean noon at ship as shown by the watch. Applying to this the error of the watch on Greenwich will give Greenwich time at the mean noon of the ship, which is the longitude in time.

* N.B.—The altitude should not be less than 70° , or the time from noon more than 10^m.

(2.) Correction for change of latitude. With half the interval as an hour-angle compute the azimuth, No. 676.

To the log. sine of half the D. Lat. made good, add the log. sec. of the lat., and the log. cotan. of the azim.: the sum, rejecting tens, is the log. sine of the correction, *in time*.

When the ship has *approached* the sun in the interval, *subtract* this time from the above mean; when she has *receded* from the sun *add* it: the result is the time by watch at apparent noon.

Ex. 1. June 8th, 1826, lat. by acc. 6° N., at $2^h 43^m 1^s$ by watch (A.M.) and at $3^h 0^m 3^s$ (P.M.) obs. alt. $\odot 84^{\circ} 30'$ to the northward; course, N.N.W. true, rate, $3\frac{1}{2}$ knots. The interval, 17^m , gives Dist. run 1.1 mile and D. Lat. 1.

Alt. (true)	$84^{\circ} 46'$	sec.	1.040	D. Lat.	$30''$	sin.	6.163
Decl.	$22^{\circ} 50'$	cos.	9.965	Lat.	6°	sec.	0.002
Half-Int.	$8^m 31^s$	sin.	8.570	Az.	22°	cot.	0.394
Azim.	22°	sin.	9.575	Corr.	$-0^h 0^m 5^s$	sin.	6.559
				<u>2 51 32</u>			

T. by Watch of App. Noon $2 51 27$ or Watch *fast*.

Here the sun is to the northward, and the course is to the northward, or the ship has *approached* the sun.

Ex. 2. June 22d, 1828, at sea, lat. 4° S., course S.W. true, rate $7\frac{1}{2}$ knots, obs. alts of the sun to the northward; ship receding from the sun.

Alt. \odot	$59^{\circ} 44'$	Times	$12^h 29^m 57^s$ A.M.	$2^h 8^m 39^s$ P.M.
	50		30 53	7 37
	55		31 45	6 45
		Means	<u>12 30 52</u>	<u>2 7 40</u> int. $1^h 37^m$
				<u>0 30 52</u>

Approx. T. by Watch of noon $1 19 16$ or Watch *fast*.

The Dist. run in $1^h 37^m$ is 12m.; D. Lat. made good, $8' 5''$.

Alt.	60°	sec.	0.301	D. Lat.	$4' 15''$	sin.	7.092
Decl.	$23\frac{1}{2}$	cos.	9.962	Lat.	4°	sec.	0.001
Half Int.	$48^m 30^s$	sin.	9.322	Azim.	$22\frac{1}{2}^{\circ}$	cot.	0.383
Azim.	$22\frac{1}{2}^{\circ}$	sin.	9.585	Corr.	$+0^h 0^m 41^s$	sin.	7.476
				<u>1 19 16</u>			

T. by Watch of App. Noon $1 19 57$
or error of the watch, *fast*.

802. *Degree of Dependence.* (1.) The error of time due to an error of $1'$ in one of the alts. is half that due to $1'$ change of alt., No. 788 (1.)

(2.) To find the error due to an error of $1'$ in the D. Lat. made good, divide the correction obtained by the D. Lat. For ex., $1'$ error in Ex. 2 causes 5^s error in the correction.

2. Equal Altitudes on Shore.

803. The method of equal altitudes is susceptible of considerable accuracy, but it can be completely put in practice on shore only, as the sea-horizon is always subject to uncertainty.

[1.] *The Sun, Morning and Evening.*

805. *The Observation.* In the A.M., when the sun is within the limits (No. 778), set the index of the sextant at the altitude, nearly; clamp the index, and observe the instant of the alts. of both limbs, noting the times. Do the same in the afternoon, when the limbs will follow in reverse order.

The value of the method consists in the same altitude being repeated, without regard to the precise measure of it. But as the second or corresponding altitude is often lost by a cloud hiding the object, the usual practice is to set the index to certain whole divisions, as $10'$, $20'$, &c., and to observe the altitudes. The moving of the index destroys, indeed, the integrity of the method, since the second altitude is no longer identical with the first, but is merely inferred to be equal to it from the reading. The errors, however are greatly diminished by taking numerous altitudes: or a number of instruments may be employed, set to different altitudes.

806. *The Computation.* (1.) Reckon the time P.M. as 12^h , 13^h , &c., instead of 0^h , 1^h , &c. Add together the A.M. and P.M. times of observation; take the mean of these sums, and divide it by 2. Take the difference between the 1st and 3d times (as set down in the example below) to the nearest minute, and call it the interval.

(2.) Find the Greenwich Date for apparent noon at the place; reduce the sun's decl. (p. I. of the Naut. Alm.) to the nearest minute only, marking it as of the *same* or *contrary* name to the latitude, and as *increasing* or *decreasing*. Reduce the equation of time, p. I. Naut. Alm.

(3.) Take the sum of the changes of the sun's declination for the 24^h before and the 24^h after the Gr. Date; call this the double change.*

(4.) Compute the equation of equal altitudes thus:—

Part I. From Table 72 take out the logarithms A and B. To log. A add the log. cot. of the latitude and the prop. log. of the double change: the sum, rejecting tens, is the prop. log. of Part I.

Part II. To log. B add the log. cot. of the decl. and the prop. log. of the double change: the sum, rejecting tens, is the prop. log. of Part II.

(5.) Apply these parts, which form the equation, to the approximate noon by watch, by the following directions.

	Part I.		Part II.	
	Lat. and Declin.		Interval	
	of the <i>same</i> name.	of <i>contrary</i> names.	<i>less</i> than 12 hours.	<i>greater</i> than 12 hours.
Declination increasing	<i>sub.</i>	<i>add</i>	<i>add</i>	<i>sub.</i>
Declination decreasing	<i>add</i>	<i>sub.</i>	<i>sub.</i>	<i>add</i>

The result is the time shewn by the watch at the instant the sun was on the meridian, or apparent noon by the watch, and therefore shews the error of the watch on A.T.

To obtain the error on M.T. To apparent noon, $0^h 0^m 0^s$, or

* As the decl. in Table 60 is given only to the nearest minute, the daily change, as taken from this table, may be a minute in error. This will not cause an error of 1^s in the equation of equal alts.; but, for precision, the Nautical Almanac is necessary.

12^h 0^m 0^s, apply the reduced Equation of T. as directed p. I. of the Naut. Alin., or Table 62: the result is the *mean time* of the sun's meridian passage (as in No. 624). By comparing with this the time of apparent noon by the watch, its error on mean time is found.

Three places in the logarithms give the equation to 0^h 1^s.

Ex. 1. Feb. 15th, 1830, at Ascension, lat. 7° 57' S., long. 14½° W., the following observations of the sun's limbs were taken in the quicksilver, the sextant being clamped at 81°.

A.M.	P.M.	Suma deducting 24.	Red. Decl. 12° 44' S.
10 ^h 45 ^m 40 ^s	17 ^h 29 ^m 19 ^s	4 ^h 14 ^m 59 ^s	Eq. of T. 13 ^m 50 ^s 5 <i>additive</i> .
10 47 54	17 27 8.5	4 15 2.5	
	Sum	8 30 1.5	
		4 15 0.7	Two-daily change, 39' 12",
	Approx. Noon by Watch	2 7 30.3	<i>decreasing</i> .
From 10 ^h 46 ^m		Log. B	2.412
to 17 27		Decl. cot.	0.646
Int. 6 41	log. A		0.661
	Lat. cot.		Part II. 2°.1
	39' 18" p. l. 0.661		3.719
Part I. 2°.0	pr. log.		Int. less than 12 ^h ; decl. <i>decreasing</i> , sub-
Lat. and decl. <i>same name</i> ; decl. <i>decreasing</i> , add.	3.734		tract.
		Approx. Noon	2 ^h 7 ^m 30 ^s 3
		- 2.1	Eq. of Eq. Alts. - 0.1
		+ 2.0	
		App. Noon by Watch	2 7 30.2
		Eq. of T. <i>additive</i> , or	
		Mean Noon, No. 624	13 50.5
		Watch fast on M.T.	1 53 39.7

Ex. 2. July 24th, 1878, lat. 55° 1' N., long. 0^h 6^m W., obtained following observations of sun's limbs in the quicksilver, the sextant being clamped at 49°.

A.M.	P.M.	Suma deducting 24.	☉'s Red. Decl.
7 ^h 6 ^m 51 ^s	17 ^h 12 ^m 39 ^s 5 ...	0 ^h 19 ^m 30 ^s 5	19° 52' N. <i>decr.</i>
7 10 27.5	17 8 57 ...	0 19 24.5	Two-daily change
	Sum	55.0	25' 17"
		0 19 27.5	Eq. of T.
		0 9 43.7	6 ^m 14 ^s 1 <i>addit.</i>

Int. 10^h 2^m; Part I., 15°.6, lat. and decl. *same name*; decl. *decreasing*, add. Part II., 15°.0 int. less than 12^h; decl. *decreasing*, subtract; app. noon by watch, 0^h 9^m 58^s 3; Eq. of T. *additive*, or M.T. of Mer. Pass. 0^h 6^m 14^s 1. Watch fast on M.T. 0^h 3^m 44^s 2.

[2.] The Sun, Evening and Morning.

807. Instead of observing A.M. and P.M. on the same day, it is often convenient to observe on the afternoon of one day and the morning of the next.

The Computation. (1.) Take the mean of the times as directed; No. 806; this is the approximate time by watch of apparent midnight. Find the interval as in No. 806.

(3.) Find the Green. Date in app. time for midnight at the place

* It is often convenient, when all possible accuracy is required, to employ the logarithms of numbers. In this case, take the arith. complements of the logs. A and B, employ the tangents of the lat. and decl., and the log. of the two-daily change in seconds.

Ex. (the above.)

Log. A	2.2183	ar. co. 7.7817	Log. B	2.4121	ar. co. 7.5879
Lat.		tan. 9.1450	Decl.		tan. 9.3541
39' 18" = 2358"		log. 3.3725			3.3725
Part I. 15°.99		log. 0.2992	Part II. 2°.06		log. 0.3145

Reduce the sun's decl. and the Eq. of Time.

(3.) Find the double change, as before directed.

(4.) Compute the equation of equal altitudes, apply the 1st part the contrary way to (5): the result is the time by watch of apparent midnight.

Ex. Feb. 22d, 1830, P.M., and Feb. 23d, A.M., lat. $7^{\circ} 57' S.$, long. $14\frac{1}{2}^{\circ} W.$, obtained observations of equal altitudes.

P.M.	A.M.	Sums (-12h).	
5 ^h 18 ^m 32 ^s	10 ^h 59 ^m 47 ^s	4 ^h 18 ^m 19 ^s	Decl. $12^{\circ} 44' S.$, <i>decreasing</i> .
5 19 36	10 58 41	4 18 17	Eq. of T. $13^m 46^s 4.$, <i>additive</i> .
5 20 40.5	10 57 36	4 18 16.5	
		52.5	Double change, $43' 8''$
		4 18 17.5	
Approx. Midnight by Watch		2 9 8.7	

Part I.

	5 ^h 19 ^m	
	10 7.8	
Int.	5 39	log. A 2.235
		Lat. cot. 0.855
		43' 8'' 0.614
-4.2		3.704

Part II.

Log. B	2.307
Decl. cot.	0.646
	0.614
2.5	3.627

The int. is greater than 12^h , that used for log. A being its suppl. The Eq. of eq. alt. is $+0^s 3$; the watch fast on M.T. $1^h 55^m 22^s 6.$

[3.] *Equal Altitudes of a Star.*

808. This observation determines the absolute time with much precision and convenience, as there is no equation of equal altitudes.

809. *The Computation.* (1.) The mean of the times shewn by the watch is the time by watch corresponding to the sidereal time, or R.A. of the merid., which, in this case, is the same as the R.A. of the star.

(2.) Find M.T. by No. 607, and thence the error of the watch.

810. *Correction for Change of Refraction.* As the method of equal altitudes is capable of much precision, and as the rate deduced may be much affected by small errors in the absolute time, it is worth while to make the proper correction for every cause of inaccuracy. A shift of wind or a fall of rain, in the interval, may be accompanied by a change of refraction, which, especially when the altitude is low, may produce a sensible effect. To allow for this,

(1.) Find the correction of the refraction at both observations for the barom. and therm., Tables 32, 33; then, when the corrections differ,

(2.) To the prop. log. of their diff. add the prop. log. of the time the sun takes to move through his diameter (which, if not shewn by the observation, may be found by note *, p. 221), and the ar. comp. of the prop. log. of the semi-diameter; the sum is the prop. log. of a portion of time, *half* of which is to be applied to the time of noon, or midnight, thus:—

1st obs. A.M., or to the eastward, when the east. refr. is the *greater*, *add*; when the *lesser*, *subtract*.

1st obs. P.M., or to the westward, when the east. refr. is the *greater*, *subtract*; when the *lesser*, *add*.

Ex. May 21st, 1850, Fort Villagagnon, Rio de Janeiro, lat. $22^{\circ} 55' S.$, long. $43^{\circ} W.$.
 obtained equal alta. 57° in the quicksilver, A.M. and P.M.; the refr. at the eastern observation
 $12''$ less than at the west.

Reduced decl. $20^{\circ} 50' N.$ (of const. ~~any~~ name to lat. and increasing), double change $24' 36''$
 Eq. of T. $3^m 44^s 7$, subtr. from A. T

A.M.	P.M.
$7^h 21^m 54^s$	$13^h 25^m 6^s$
$7 \ 23 \ 23$	$13 \ 23 \ 36$
$7 \ 24 \ 56$	$13 \ 22 \ 4$
$3 \ 2$	

Suma
$20^h 47^m 0^s$
$20 \ 46 \ 59$
$20 \ 47 \ 0$
$140 \ 59$
$20 \ 46 \ 59 \cdot 7$
$10 \ 23 \ 29 \cdot 8$

The int. 6^h from
 $7^h 22^m$ to $13^h 22^m$
 gives the two parts
 $+ 3^h 7$ and $+ 2^h 2$, or
 the equation of eq.
 alts. $+ 5^h 9$.

Correction for unequal refraction.

$12''$	prop. log.	$2 \cdot 95$
$3^m 2^s$	do.	$1 \cdot 77$
$15' 49''$	Ar. co. do.	$8 \cdot 94$
$2^h 3$	prop. log.	$3 \cdot 66$
Corr. $-1^h 1$		

Approx. Noon by Watch	$10^h 23^m 29^s \cdot 6$
Eq. Equal Alts.	$+ 5^h 9$
	$10 \ 23 \ 35 \cdot 7$
Corr. for Refract.	$- 1 \cdot 1$
App. Noon by Watch	$10 \ 23 \ 34 \cdot 6$
Eq. of T. $+ 12^h$	$12 \ 3 \ 44 \cdot 7$
Watch slow on A. T.	$1 \ 36 \ 25 \cdot 4$
Watch slow on M.T.	$1 \ 32 \ 40 \cdot 7$

811. *Degree of Dependance.* The error of the equation of equal altitudes caused by an error in the double change of decl. is a matter of simple proportion. The effects of small errors in the lat. and decl. are insensible, therefore neither the lat. of the place nor the declin. is required to great precision. But variations in the refraction, not to be removed by corrections, will always leave the result in some degree doubtful. On this account, the method, even under the most favourable circumstances, can rarely be considered as affording extreme precision.

IV. RATING THE CHRONOMETER.

812. The RATE of a chronometer is the difference of its error from day to day. It is called *gaining* when the watch goes too *fast*, and *losing* when it goes too *slow*.

813. When the chronometer is *fast*, either on G. M. T. or on the time at place, if the error is *increasing*, the rate is *gaining*; if *decreasing*, the rate is *losing*. When the chron. is *slow*, if the error is *increasing*, it is *losing*; if *decreasing*, it is *gaining*.

The amount of the daily rate (supposed uniform) is found by dividing the change of the error by the number of days in the interval between the observations.

Ex. May 27th, at 9^h A.M. chron. slow	$2^h 7^m 18^s$
June 3d, at 5^h P.M. slow	$2 \ 6 \ 51$
Diff. of Error in $7^d 8^h$	$0 \ 0 \ 27$

Then 27^s , divided by $7 \cdot 33$ days, gives $3^s 7$ DAILY RATE, *gaining*.

814. When the error is found to have changed from fast to slow, or from slow to fast, the rate is the sum of the errors divided by the number of days elapsed.

Ex. 1. June 28th, at 3 P.M., the chron. was $0^m 7^s \cdot 0$ fast; on July 5th it was $0^m 16^s \cdot 1$ slow: required the Daily Rate. The sum $23^s \cdot 1$, divided by 7 (days), gives $3^s 3$, *losing*.

Ex. 2. On the 14th, the chron. was $0^m 17^s$ slow; on the 31st, it was $0^m 12^s$ fast: required the Rate. The sum $0^m 29^s$, divided by 17, gives $1^s.7$, *gaining*.

815. As the chronometer rarely goes for any length of time without some irregularity, the rate should be deduced afresh at every opportunity. This is done, 1st, by finding the *absolute error on the time* at place, by observation, after intervals of a few days; 2dly. by direct comparison of the *interval of time* shewn by the chronometer with that measured by a clock of known rate, or with the motion of a star. Also, as longitude is measured by time, No. 479, the absolute longitudes of places, when correctly laid down, and their differences of long. may be employed in a corresponding manner.

All observations for the purpose of rating a chronometer should be made, if possible, on shore, on account of the uncertainty of the sea-horizon, because a small error in the absolute time may produce a great error in the daily rate deduced. Also, the observations should be made by the same person with the same instrument, and under the same circumstances, as nearly as possible.

1. *By Comparison with the Absolute Time, or Longitude*

[1.] *By the Time.*

816. The best observation (out of the observatory) for the purpose, is equal altitudes carried on for several days. The next in value is the same alt. repeated several days successively, in the same part of the day; for the times determined by A.M. and P.M. sights on the same day do not, it appears, agree exactly either at sea or on shore.*

As the rate cannot be depended upon for a considerable length of time, it is necessary to take frequent opportunities of obtaining alts. on shore by the artificial horizon. It is proper, therefore, to remark, that by a little care, and by not mixing A.M. and P.M. sights, the rate may be determined nearly as well as by equal altitudes.

817. At sea, the lunar observation, No. 836, or, under very favourable circumstances, the moon's altitude, No. 864, affords the absolute error of the chronometer on G. M. T., and may discover, accordingly, if any considerable change in the rate has taken place; but it would be highly injudicious to attempt to establish a rate from observations so discordant as these usually are.

818. An excellent method has been afforded of late years, of determining the error and rate of the chronometer by the establishment of time-balls at some observatories. These, with the G. M. T. at the instant the ball is dropped, are given in Table 13. The time-ball obviates the necessity of observations for rate.

819. When the ship leaves any place, and after an interval not much exceeding a fortnight returns to it again, the error of the

* The late Captain Hewett informed me, that being obliged to keep account of the daily rates of his chronometers, by means of altitudes observed from the sea-horizon, while surveying the North Sea, in H.M.S. *Fairy*, the constant discrepancies between the A.M. and P.M. sights rendered it necessary to employ the A.M. sights alone.

chronometer accumulated in her absence is found directly by comparing the time shewn by the chronometer with the times obtained by observation both at her departure and at her return. The error thus found affords the actual *sea-rate*, and the method, when it can be practised, is far more efficient than that of deducing harbour-rates.

Ex. By an observation taken immediately before the ship's departure from a port the chron. was found slow $3^h 27^m 14^s$. By an observation taken at her return, or 11·3 days afterwards, the error was $3^h 27^m 44^s\cdot5$, or $30^s\cdot5$ more. Hence the RATE during her absence has been, on the average, $2^m\cdot7$ losing.

[2.] *By the Longitude.*

820. When, on making a well-determined point of land, the long. by chron. does not agree with the actual position of the ship, and when, accordingly, the chronometer must have been going at a different rate from what was supposed, it will be convenient to refer to the following Table.

	Sailing E.	Sailing W.
The land not made so soon as expected.	The Chronometer has	
	gained less, or lost more,	gained more, or lost less,
The land made unexpectedly.	gained more, or lost less,	gained less, or lost more,
	than allowed for.	

Ex. A ship from India to the Cape of Good Hope makes the land unexpectedly. The ship is sailing W., the land made too soon; the chron. has therefore gained less or lost more than allowed for.

But it must be borne in mind that chronometers do not preserve the same rates, generally speaking, for a long time together; and, therefore, after a considerable interval, as upwards of a fortnight, this method shews only the gain or loss *on the whole*, not whether the chronometers are gaining or losing now.

2. *By Comparison of Intervals, of Time, or Longitude.*

[1.] *By a Clock.*

821. The chronometer being compared at different times with a clock of which the rate is known (as in No. 564), the difference of the errors for the intervals is obtained, and thence the rate is deduced. The mode of comparison is already described, p. 203.

[2.] *By a Star.*

822. Since every star returns to the same point of the heavens $3^m 55^s\cdot91$ of mean time earlier every mean solar day, the return of the same star to the same altitude, or to the wire of a fixed telescope, day after day, determines the rate very correctly. The alt. should

be considerable, in order to avoid errors of refraction, and the telescope, for the same reason, should be nearly in the meridian.

To find the rate, multiply $3^m 55^s.91$ by the number of days elapsed, and subtract the product from the first time noted; the remainder is the time the chronometer would shew if it went uniformly, and the difference between this and the time it shews is the difference of the error for the interval, which gives the daily rate.

Ex. At an observation of a star on May 1st, the chron. shewed $7^h 51^m 11^s$; after four days it shewed $7^h 35^m 44^s.6$: required the Daily Rate.

$$\begin{array}{r} \text{First time noted} \quad 7^h 51^m 11^s \\ 3^m 55^s.91 \times 4 \quad \underline{- 15 \ 43^s.6} \\ 7 \ 35 \ 27^s.4 \\ 7 \ 35 \ 44^s.6 \end{array}$$

Gaining in four days $17^s.2$ hence the DAILY RATE is $4^s.3$, *gaining*.

The disappearance of a star behind any elevated object answers the same purpose.

[3.] By Difference of Longitude.

823. When the error of the chronometer upon the time at any known place A is compared with the error on the time at another known place B, the difference between these two errors is the diff. long., in time, between the places. Hence if the difference of the errors does not agree with the Diff. Long. found from Table 10, or in Table of Secondary Meridians, p. 392, the discrepancy arises from a wrong rate having been employed in the interval between the observations for time, and the true rate may be found by trial, as in the following example:—

Ex. At Falmouth, Feb. 3d, at $3^h 20^m 18^s$ M.T. by observation, the chron. shewed $4^h 31^m 47^s$, or was $1^h 11^m 29^s$ fast. At Funchal, on the 12th, at $5^h 30^m 27^s$ M.T., or $9^h 1$ days afterwards, the chron. shewed $7^h 29^m 34^s$. The supposed rate, $2^s.3$ *gaining*. The D. Long. in Table 10 A is $47^m 28^s$. Required the true rate.

Obs. at Falm., T. by chron.	$4^h 31^m 47^s$	Obs. at Funchal, T. by chron.	$7^h 29^m 34^s$
M.T. by obs.	$3 \ 20 \ 18$	$2^s.3 \times 9^d$ d. <i>gain</i>	$- 21$
1st error, fast	$1 \ 11 \ 29$		$7 \ 29 \ 13$
		M.T. by obs.	$5 \ 30 \ 27$
		2d error, fast	$1 \ 58 \ 46$
		1st error, ditto	$1 \ 11 \ 29$
		Difference, or <i>chron. D. Long.</i>	$47 \ 17$

This diff. should be $47^m 28^s$, or is too small by 11^s . By inspecting the process, it is evident that the quantity 21^s (which, from the nature of the case, is supposed to be in error) is too large by 11^s . The RATE, therefore, is 10^s divided by 9^d , or $1^s.1$ *gaining*.

When one error is fast and the other slow, make them both fast or both slow, by adding or subtracting any number of hours.

3. Keeping Account of the Chronometer.

824. In keeping account of the chronometer, the error on G.M.T. is entered in a book as fast or slow, with the date, and the rate is applied to this according as it is gaining or losing, day by day.

If, after a time, the long. or G.M.T. be obtained independently, the error on G.M.T. is found; if this does not agree with the rate

allowed, a new rate must be assigned from consideration of the circumstances.

825. As it is impossible, without an independent reference, to determine whether a chronometer, A, is gaining upon another, B, or B is losing while A goes as before, no direct rules of certain application can be given for reducing the rates of chronometers by mere comparison. Since, however, it may be presumed, in general, that in a number of watches the true time will be that shewn by the majority, regard being had to the quality of each, it is proper to keep an account, in which an approved watch being taken as the standard, the rest are severally compared with it every day.

It is convenient to distinguish the chronometers by letters, as A, B, C, &c., and to write the difference between A and B thus, A—B; that between A and C thus, A—C, over each column.

Advantage should be taken of favourable opportunities of landing at well-determined places (*see* Table of Longitudes accepted for Secondary Meridians, p. 392) for good observations of time, because the diff. long. between the places will at once discover any considerable change in the rate, afford means of correcting it, and be a means of obtaining the *sea-rates* of the chronometers.

CHAPTER VII.

FINDING THE LONGITUDE.

- I. BY THE CHRONOMETER. II. BY THE LUNAR OBSERVATION.
III. BY THE ALTITUDE OF THE MOON. IV. BY AN OCCULTATION.
V. BY ECLIPSES OF JUPITER'S SATELLITES.

826. The apparent motions of the celestial bodies parallel to the equator, produced by the revolution of the earth round its axis, being perpetual, no fixed point or circle can be obtained from which the longitude of the observer, which is measured, like right ascension, on the equator, may be determined. Longitude, accordingly, can be ascertained only with reference to the meridian of some other place; and, as it is measured by time (No. 193), it is determined by comparison of the time at place with the time at some other place.

I. BY THE CHRONOMETER.

1. *Determination of the Absolute Longitude.*

827. The most convenient method of finding the longitude is by comparison of the time at place with the time at Greenwich, as shewn by a chronometer.

The mean time at place being found (Chapter VI.), take the difference between this time and the time by chronometer, brought up to the time of observation by applying the error with the rate.

When the time at Greenwich is the *least*, the long. is E.; when the *greatest*, it is W.

Ex. 1. The M.T. at place is $3^h 48^m 2^s$; the G.M.T. is $4^h 15^m 11^s$: hence the Long. of the place is $0^h 27^m 9^s$, or $6^\circ 47' 15''$ W.

Ex. 2. The M.T. at place is $7^h 14^m 22^s$; the G.M.T. is $2^h 6^m 57^s$: hence the Long. is $5^h 7^m 25^s$, or $76^\circ 51' 15''$ E.

828. *Degree of Dependence.* The time at place, as deduced from observation, and the time shewn by chron., being both liable to error, the error of the resulting longitude is made up of the sum or difference of these two errors.

829. When the rate of the chronometer has changed, and the long. is required at a time past, the error of the chronometer at the time proposed must be deduced from the two rates by consideration of the circumstances, as no rule can apply to all cases.

2. Determination of Difference of Longitude.

830. The ordinary method is to find the absolute longitudes of both places by comparison of the Greenwich mean time, as above described, and then to take the difference between them.

Ex. M.T., at a place A, is $3^h 11^m 43^s$, when the G.M.T. is $7^h 7^m 18^s$: hence the long. of A is $3^h 55^m 35^s$ W. Again, some days afterwards the M.T., at a place B, is $2^h 19^m 45^s$, when the G.M.T. is $6^h 26^m 34^s$: the long. of B is $4^h 6^m 49^s$ W.

The DIFF. LONG. between the places is, therefore, $11^m 14^s$, and B is west of A.

831. But it is more concise, in a question relating to a *difference* only, to proceed without regard to the absolute longitude of either place, by considering merely the error of the chron. on the time at each of the two places, as in the following example:—

Ex. 1. At $3^h 11^m 43^s$ M.T., by obs. at a place A, the chronometer shewed $5^h 11^m 19^s$, or was $1^h 59^m 36^s$ fast on the time at A. Again, some days afterwards, at $2^h 19^m 45^s$ M.T., at a place B, the chron. (after applying the rate) shewed $4^h 30^m 35^s$, or was $2^h 10^m 50^s$ fast on the time at B.

Now it is evident that if A and B were in the same long., the chron., supposing the rate truly determined, would have the same error at each place; and hence the difference of the errors, $1^h 59^m 36^s$ and $2^h 10^m 50^s$, or $11^m 14^s$, is the DIFF. LONG.

Since the chron. is *faster* at B than at A, the time at B is *behind* that at A, or B is west of A.

The proceeding, reduced to a rule, is as follows:—

Find, by observation, the error of the chron. on the time at place. Having moved to another place, take an observation for time; correct the time shewn by the chron. by applying the rate for the time elapsed since the former observation, and find the error: the difference of the two errors is the diff. long.

When the chron. is *fast* at both places, the place at which the error is the greatest is *west* of the other.

When the chron. is *slow* at both places, the place at which the error is the greatest is *east* of the other.

When the chron. is fast at one place and slow at the other (as may occur when the error is less than the diff. long.), add 5 or 6

hours to each of the times by chron. in order to render both the errors of the same kind.

Ex. 2. At A, M.T. $5^h 36^m 10^s$, chron. $6^h 36^m 20^s$, error $1^h 0^m 10^s$ fast
 At B, M.T. $3^h 28^m 30^s$, chron. $4^h 9^m 20^s$, error $0^h 40^m 50^s$
 A west of B, Diff. Long. $0^h 19^m 20^s$

832. Since the whole value of a chronometric determination depends upon the rate of the chronometer, and since the rate is liable to change, the result is better as the time occupied in the run is less. This, however, does not, in strictness, apply to intervals less than 24 hours; for the works go through an entire revolution in 24 hours, and the *rate*, which is determined for an entire day, may be unequally distributed over different parts of the 24 hours. For extreme precision, the rate should be known for given intervals on the dial-plate.

833. When the ship returns without loss of time from a place to that from which she set out, the opportunity will in general be very favourable for determining the difference of longitude.

834. While a chronometer continues to gain or to lose, the difference of longitude shewn by it between two places will be differently affected, according as it is measured eastwards or westwards: hence, if the differences do not agree, the true diff. long. will be between them.

When the chron. *gains* on its rate, the computed long. is to the *west* of the true long.; when the chron. *loses* on its rate, the computed long. is to the *east*.

If the rate is steady, the true diff. long. will be correctly found by dividing the error according to the number of the days in the two passages.

3. Communication of Chronometric Differences.

835. Individuals possessing one or more good chronometers frequently have opportunities of furnishing, verifying, or correcting meridian distances. It is proper, therefore, here to enumerate the considerations which influence the value of the results, more especially as many such determinations are communicated to authority from time to time, which, however, not being accompanied with the details necessary for an estimation of their value, remain unemployed.

(1.) It is absolutely necessary to specify or to describe the *exact spot of observation* at each place.

(2.) The *number of days* employed in the run, or in the interval between the observations for time, or both, if these differ much, together with the *number of chronometers*, should be expressed; also, the times and manner of rating, and the character of the rate, as steady or unsteady, should be briefly noticed.

(3.) The *maker's name* and the *number* of the chronometer should be specified, because the character of a watch affects the value of a determination in which it is employed.

(4.) When there are several chronometers, the result given by each should be exhibited. The general *arithmetical mean* should be given, and, besides this, an *estimated mean*, obtained by giving more or less weight to the several results, according to the performance of each chronometer, and of which the observer alone can be a judge. The two final results should be expressed in *time*, and also in *arc*, for the more ready comparison of positions on the chart.

(5.) The *extreme difference* of the greatest and least results by the different chronometers employed should be stated, as this shews whether the chronometers went well together or not; for, though their going together does not prove that all or any of them are right, their not going together proves that some of them are wrong.

(6.) All observations for the longitudes of places are supposed to be made by means of the quicksilver, unless the contrary is expressed. When the altitudes are taken from the sea-horizon, the result should, therefore, be distinguished by the word (*sea*).

(7.) It will be useful to state the temperature of the chronometer-room, and to remark whether it has remained constant or been subject to variation. Also, the general direction of the ship's head should be noted.

(8.) Lastly, every result should be given without any regard as to *whether it agrees or not with received determinations*. Many received positions are very erroneous, and the only means by which they can be decisively rectified are the comparisons of independent and impartial evidence.

In the following example, D. L. is the abbreviation of Diff. Long.; ch. is that of chronometers; d. that of days; and the extreme difference is denoted by the number of seconds enclosed in brackets, implying limit or boundary.*

Ex. May, 1838, Capt. A., of H.M.S. —, sailed from Barbadoes to Port Royal, Jamaica, the points of observation being Engineers' Wharf and Fort Charles. He carried five chronometers, viz., No. 152, Molyneux; No. 192, Breguet; No. 702, Arnold and Dent; No. 650, Parkinson and Frodaham; and No. 490, M'Cabe. The passage occupied seven days. The extreme difference of the results was 7 seconds of time. The arithmetical mean was $1^h 8^m 49^s$; the estimated mean, $1^h 8^m 52^s$. The temperature of the chronometer-room ranged from 78° to 80° ; the ship's head chiefly west.

These particulars, abbreviated, stand thus:—

Capt. A., May 1838, D. L. Barbados (Eng. Wharf) to Port Royal (Fort Charles), 5 ch.			
			7 d. [7 ^s]
			Arith. Mean, $1^h 8^m 49^s = 17^\circ 12' 15''$
			Estim. Mean, $1^h 8^m 52^s = 17^\circ 13' 0''$
M.	No. 152	$1^h 8^m 46^s$	
B.	No. 192	$1^h 8^m 52^s$	
A. and D.	No. 702	$1^h 8^m 53^s$	Temp. 78° to 80° [2 ^o]
P. and F.	No. 650	$1^h 8^m 45^s$	Head west.
M'C.	No. 490	$1^h 8^m 49^s$	

* This plan was proposed in the Naut. Mag., 1839, p. 402, to which the reader is referred for other details of the subject.

II. THE LUNAR OBSERVATION.

Clearing the Distance, Nos. 842, 844, 845—Lunar Obs. by the Sun, No. 847—Lunar Obs. by a Star or a Planet, No. 849—Special Corrections, No. 851—Degree of Dependence, No. 858—Calculation of Altitudes, No. 863.

836. The angular distance of the moon from any celestial body being in perpetual change, each of the several degrees of magnitude through which it passes corresponds to a certain instant of time. Accordingly, the distance of the moon from the sun and certain other bodies, at the end of every three hours, being given in the Nautical Almanac, the observation of this distance affords the means of determining the time at Greenwich, and thence the longitude of the observer.

This observation, on account of its great importance at sea, has been distinguished by the name of the *Lunar Observation*.

837. If the distance between the moon and the other body were the same to the spectator, whether he were at the surface or the centre of the earth, there would evidently be nothing more to do than to measure the distance by an instrument, to find from the Nautical Almanac the Greenwich time corresponding, and to compare this time with the time at place. But the refraction of the sun, a star, or a planet, being greater than its parallax in altitude, causes one of these bodies to appear *above* its true place; while, on the contrary, the moon's parallax in alt. being greater than her refraction, causes her to appear *below* her true place.

Z is the zenith, S and \mathfrak{D} the true places of the sun (or star) and moon, S' and \mathfrak{D}' their apparent places. Then S \mathfrak{D} is the true distance, and S' \mathfrak{D}' the apparent distance.



Fig. 1.

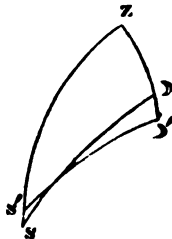


Fig. 2.

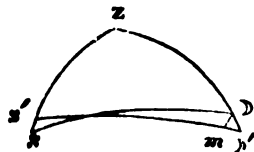


Fig. 3.

SS' is the sun's corr. of alt., $\mathfrak{D}\mathfrak{D}'$ the moon's corr. of alt. In fig. 1, where the \mathfrak{D} 's alt. is the lesser, the app. dist. exceeds the true, for \mathfrak{D}' is farther from S than \mathfrak{D} is, and S' is also farther from \mathfrak{D} than S is. In fig. 2, the app. dist. is the lesser. In fig. 3, both angles at S and \mathfrak{D} are acute, as is the case when the alts. are nearly equal, and always when the distance exceeds 85° .

As $\Delta P'$ is always less than $56'$, the arc Δm , fig. 3, of a circle, having its centre at S , is nearly a right line, and Δm (which, from the apparent place of the moon, is here the excess of the app. dist. above the true) is equal to $\Delta P' \cos.$ of the angle at P' . The like term (or 1st correction of the app. dist.) for the sun is $SS' \cos. S$, or $SS' \cos. S'$ nearly. This is the principle of the approximate methods.*

Hence the *apparent* distance between the moon and the other body differs from the *true* distance, except in the particular case in which the two opposite effects happen exactly to compensate. This last circumstance may sometimes occur during the time that two bodies within distance are above the horizon, but not being discoverable from the observation it is productive of no simplification.

The process of reducing the apparent to the true distance, or removing the effects of parallax and refraction, is called *Clearing the Distance*.

838. It is evident from the above that the difference between the true and apparent distances depends almost entirely on the corrections of altitude (No. 438); and, consequently, is affected by every variation, however minute, of those corrections. Also, since the most rapid change of distance is about $1^{\circ} 48'$ in three hours, the effect of $1'$ error of dist. is $25'$ of long., or the effect of $15''$ error of distance is $6'$ of long., in the most favourable case. Hence it may become of great importance to the accuracy of the result, in many cases, that the heights of the barometer and thermometer should be noted at the time of observation.

839. The lunar observation, which is the only independent method of finding the longitude generally available at sea, is also, from not being confined like some others to a particular instant, of service on shore. A single observation, however, is not capable of affording a decisive result; great practice is necessary for measuring the distance successfully; and the application of so many small corrections as are necessary when accuracy is required is, even with extraordinary care and some skill, scarcely compatible with extreme precision.

840. *Limits.* The distance must fall between the greatest and

* The approximate process will be easily intelligible by attending to the following considerations.

The moon must always be *raised*, and the sun or star *lowered*, to attain their true places. Now, when the moon is the lower of the two bodies, it is evident that raising her will diminish the apparent distance; that is, her correction of distance must be *subtractive*. Again, when she is the higher body it is generally *additive*. When the sun or star is the lower body, *lowering* it will increase the app. dist.; its corr. of dist. is therefore *additive*, but *subtractive* in general when the uppermost body.

The angle at the *lower* body, $Z \Delta S'$, or $Z S' \Delta'$, is *always acute*, the corresponding angle at the other body will generally be obtuse when the altitudes are very unequal, and the dist. not great.

The *correction of dist.* in Method I. is the D. Lat. corresponding to this angle as a course, and the corr. of alt. as Dist. The sum or diff. of the Dep. and N is the cosine of the angle in question to the radius 100. When the dist. is less than 90° and the Dep. greater than N , the angle is acute, but obtuse when the Dep. is the lesser. Thus, in Ex. 1 the angle at the moon is $55^{\circ} \frac{1}{4}$; that at the star, 76° .

When the moon's alt. amounts to nearly 80° , or when the distance is so small as $20'$, M and N vary irregularly, and Method I. does not serve well.

least distances in the Nautical Almanac. The alts. should not be less than 5° or 6° ; and, when the barometer and thermometer are not at hand, not less than 12° or 15° , especially in very hot or very cold weather.

As the chief part of the computation consists of *clearing the distance*, it will be more convenient for reference to consider this portion of the work separately.

1. *Clearing the Distance.*

[1.] *Approximate Methods.*

841. In these methods the object is to find the *correction* of the apparent distance due to the corrections of altitude of each body. The first, or that by *inspection*, is performed by means of the Spherical Traverse Table; and the second, by *logarithms*,* is a useful and convenient process, without the embarrassment of various cases, and requiring only four places of figures.

The approximate methods are, in general, not susceptible of much precision when the distance is less than 20° .

842. Method I. *By Inspection.* (1.) For the Moon's Correction of Distance. With the moon's app. alt. and the compl. of the app. dist. to 90° , take out M and N.

With the sun's or star's† alt. as Course, and M as Dist. find the Dep., which place under N.

When the distance is *less* than 90° , take the *difference* of this Dep. and N, marking the Dep. according as it is greater or less than N.

When the distance is *greater* than 90° , take the *sum* of the Dep and N.

With the Dist. 100, and the said *diff.* or *sum* as D. Lat., find the Course.‡ With this course and the moon's corr. of alt. as Dist., find the D. Lat.; this is the moon's correction of distance.

For the Moon's 2d Corr. Enter Table 56 with the app. dist. and the moon's corr. of alt., and take out the seconds. Enter again with the corr. of dist. and take out the seconds. The diff. of these two quantities is the 2d corr., which apply as directed in the Table.

(2.) For the Sun's or Star's Correction of Distance. With the sun's or star's app. alt. and the co-dist., take out M and N.

With the moon's alt. as Course and M as Dist. find the Dep., which place under N, marking it as greater or less than N when the dist. is less than 90° .

Take the *diff.* or *sum* as before directed.

With the Dist. 100 and this *diff.* or *sum* as D. Lat. find the Course. With this course and the sun's or star's corr. of alt. as Dist. find the D. Lat.; this is the corr. of distance required.§

* This is a slight variation of the method commonly known among seamen as Norie's 4th method, and attributed to Mendoza Rios.

† In the case of a planet, substitute the word planet for star in the several rules.

‡ If this sum or diff. exceed 100, a mistake has been made.

§ The correction of distance may be found more correctly by multiplying the diff. or sum

Note. In finding the moon's corr. work to the nearest *half degree*; and when the sun's or star's alt. is less than 20° , take out the Dep. to the nearest *third or quarter* of a degree. In the sun's or star's corr. work to the nearest *whole degree*.

Apply the corrections to the app. dist. as follows; the result is the true distance.

Distance <i>less</i> than 90°				Distance <i>greater</i> than 90°			
) Corr. of Dist.		⊙ or * Corr. of Dist.) Corr. of Dist.		⊙ or * Corr. of Dist.	
When the Dep. is <i>less</i> than N		When the Dep. is <i>greater</i> than N					
<i>add</i>	<i>sub.</i>	<i>sub.</i>	<i>add</i>	<i>sub.</i>		<i>add</i>	
) 2d Correct. of Dist. <i>add</i>) 2d Correct. of Dist. <i>sub.</i>			

Ex. 1. (Dist. *less* than 90° .) App. alt. $\odot 47^\circ 31'$; A. alt. $\triangleright 36^\circ 52'$; app. dist. $48^\circ 20' 29''$. \odot corr. of alt. $47''$; \triangleright corr. of alt. $45' 35''$. (Co-dist. 414° .)

\triangleright 's Corrections.

$\triangleright 37^\circ$ and 414° , M 167, N 66.6
 $\odot 474'$ and 167, Dep. 123.1 (gr.)
 (diff.) 56.5

Dist. 100 and D. Lat. 56.5 give the Course $55\frac{1}{2}^\circ$; at which,

Dist. $45'$ gives D. Lat. 25.5 $25' 30''$
 $35''$ 20
 25.50

(which *sub.*, since 123.1 exceeds 66.6 .)

\triangleright 2d corr. $16''$
 5 $+ 11''$

\odot 's Correction.

$\odot 47^\circ$ and 41° , M 194.3 , N 93.2
 $\triangleright 37^\circ$ and 194 , Dep. 116.8 (gr.)
 (diff.) 23.6

Dist. 100 and D. Lat. 23.6 give the Course 76° ; at which,

Dist. $47''$ gives D. Lat. $11''$
 (which *add*, since 116.8 exceeds 93.2 .)

\odot corr. $+0^\circ 0' 11''$
 \triangleright 2 corrs. -25.39
 $-0.25.28$

A. dist. $48.20.29$
 True Dist. $47.55.1$

Ex. 2. (Dist. *greater* than 90° .) App. alt. $\odot 13^\circ 10'$; app. alt. $\triangleright 36^\circ 6'$; app. dist. $120^\circ 29' 53''$. Hor. par. $59' 42''$; \triangleright corr. of alt. $46' 58''$; \odot corr. of alt. $3' 56''$. (Co-dist. 304° .)

\triangleright 's Corrections.

$\triangleright 36^\circ$ and 304° , M 143.4 , N 42.8
 $\odot 134'$ and 143.4 , Dep. 32.9
 (sum) 75.7

100 and D. Lat. 75.7 give Course 41° .

$46'$ gives 34.7 $34' 42''$
 $58''$ 44

\triangleright 2d corr. 120° and $47', 11''$ } $-5''$
 $35, 6$

\odot 's Correction.

$\odot 13^\circ$ and 30° , M 118.5 , N 13.3
 $\triangleright 36^\circ$ and 118 , Dep. 69.4
 (sum) 82.7

100 and D. Lat. 82.7 , Course 34° .

$3'$ gives 2.5 , $0^\circ 2' 30''$
 $56''$ 46

$+0.3.16$
 $-0.35.31$

$-0.32.15$
 $120.29.53$

True Dist. $119.57.38$

(of the Dep. and N) by the correction of alt., pointing off two more decimals than the product contains. The seconds may either be taken separately, or as decimals of a minute.

This process, worked however roughly, affords a check against a mistake in using the Traverse Table.

Ex. 1 of No. 842.

Diff. 56.5
 \triangleright corr. of alt. $45' 35''$ 45.6
 Prod. 2576.40
 Pointing off two dec. 25.76 or $25' 46''$

Diff. 23.6
 \odot corr. of alt. $47''$ 47
 Prod. 1109.2
 Pointing off two dec. 11.09 or $11'$

) 27° and 17½°, M 117.4 N 15.6
 @ 72° and 117, Dep. 111.3
 95.7

$$\begin{array}{r} 46' \\ 30'' \\ \hline 44 \quad 0'' \\ \underline{-44 \quad 29''} \end{array}$$

© 72° and 17°, M 358.4, N 94.1
) 27° and 338, Dep. 153.0
 58.9

16', @ DIST.	+0° 0' 9"
	-0 44 28
	-0 44 19
	72 18 32
TRUE DIST.	71 34 13

$$\begin{array}{r} 46' \\ 54'' \\ \hline 34' \quad 42'' \\ \quad 41'' \\ \hline -35 \quad 23 \end{array}$$
$$\begin{array}{r} 4' \\ 9'' \\ \hline 3' 18'' \\ \hline 7 \\ + 3 \ 25 \\ \hline \end{array}$$

TRUE DIST. $119^{\circ} 57' 50''$

(52°) 29' 36" 114' 4" 12' 1" 49 61' 1"

 13 4" + 4" 0

 -29 49

$$\begin{array}{r} 113.7 \quad 11.6 \\ \underline{50.0} \\ 61.6 \end{array}$$

(52°)
$$\begin{array}{r} +0^{\circ} \quad 1' \quad 9'' \\ \underline{-0 \quad 29 \quad 45} \\ -0 \quad 28 \quad 36 \\ \hline 104 \quad 37 \quad 49 \end{array}$$

TRUE DIST. 104 9 13 (3' too small)

$$\begin{array}{r} 352.7 \\ 54'' \\ \hline 185.3 \\ 262.3 \\ \hline 77.0 \end{array}$$
$$\begin{array}{r} 180.3 \\ 74.9 \\ \hline 169.1 \\ 94.2 \end{array}$$
$$\begin{array}{r} 175^{\circ} 1' \\ 71^{\circ} 1' \\ \hline 153^{\circ} 1' \\ 82^{\circ} 0' \end{array}$$

$$17^{\circ} \left. \begin{array}{l} \\ 5 \end{array} \right\} + 12^{\circ}$$

296.9	186.8
	170.4
	16.4
-0° 0' 4"	
-0 35 33	
-0 35 37	
43 44 50	
TRUE DIST. 43 9 13 (17" too small).	

X

exhibit a sufficient variety of cases, that the method is accurate enough for navigation in the open sea.

844. Method II. *By Logarithms*.—Set down in order the sun's or star's app. alt., the moon's app. alt., and the app. dist.; take half the sum, and subtract from it the first term in order (sun's or star's alt.); call the rem. the 1st rem.; subtract the second term in order (the moon's alt.), and call this rem. the 2d rem.

For the 1st Corr. To the log. cos. of the moon's app. alt. add the log. sine of the app. dist., the const. 9.6990, the log. sec. of the half sum, the log. cosec. of the 1st rem., and the prop. log. of the moon's corr. of alt.: the sum (rejecting tens) is the prop. log. of the 1st correction.

For the 2d Corr. Take the difference between the moon's corr. of alt. and the 1st corr. Enter Table 56 with the app. dist. and the moon's corr. of alt., and take out the seconds. Enter again with the above difference, take out the corresponding seconds, and subtract them from those taken out before: the rem. is the 2d corr. Apply this corr. as directed in the table.

For the 3d Corr. To the log. cos. of the sun's (or star's) app. alt. add the log. sine of the app. dist., the const. 9.6990, the log. sec. of the half sum, the log. cosec. of the 2d rem., and the prop. log. of the sun's (or star's) corr. of alt.: the sum (rejecting tens) is the prop. log. of the 3d correction.

(As the 2d, 3d, and 4th logs. are common to the two corrections, it will be convenient to take the sum of these three logs.)

Subtract from the app. dist. the moon's corr. of alt. and the 3d corr.; add the 1st corr., the sun's (or star's) corr. of alt., and apply the moon's 2d corr. as directed in Table 56: the result is the true distance.

Ex. 1. App. alt. \odot $47^{\circ} 31'$; app. alt. \triangleright $36^{\circ} 52'$; app. dist. $48^{\circ} 20' 29''$. Sun's corr. of alt. $47''$; moon's corr. of alt. $45' 35''$.

\odot Alt.	$47^{\circ} 31'$	cos.	9.8296	A. Dist.	$48^{\circ} 20' 29''$
\triangleright Alt.	$36^{\circ} 52'$	cos.	9.9031	\triangleright Corr. Alt.	$- 45' 35''$
Dist.	$48^{\circ} 20'$	sin.	9.8733	3d Corr.	$- 37''$
	$\frac{132}{2}$ $\frac{43}{2}$		9.6990		$47' 34' 17''$
Half S.	$66^{\circ} 21'$	sec.	0.3967	1st Corr.	$+ 19' 45''$
1st Rem.	$18^{\circ} 50'$	cosec.	0.4910	\odot Corr. Alt.	$+ 47''$
2d Rem.	$29^{\circ} 29'$			\triangleright 2d Corr.	$+ 10''$
	$45' 35''$	pr. log.	0.5965		True Dist. $47' 54' 59''$
1st Corr.	$19^{\circ} 45'$	pr. log.	0.9596	3d Corr. $37''$	
Diff.*	26				
	A. Dist. 48° , and \triangleright Corr. Alt. $46'$, Tab. 56,		$\frac{16''}{26}$		
			2d Corr. $+ 10''$		

Ex. 2. App. alt. \odot $32^{\circ} 36'$, app. alt. \triangleright $65^{\circ} 22'$, app. dist. $81^{\circ} 15' 51''$; \odot 's corr. of alt. $1' 22''$, \triangleright 's corr. of alt. $22' 27''$: required True Distance.

1st Corr. $37''$, 2nd Corr. 0, 3d Corr. 0, True Dist. $80^{\circ} 55' 23''$.

Ex. 3. App. alt. \star $50^{\circ} 44'$, app. alt. \triangleright $27^{\circ} 50'$, app. dist. $93^{\circ} 9' 6''$, \triangleright 's corr. of alt. $50' 25''$, \star corr. of alt. $47''$.

1st Corr. $4' 45''$, 2d Corr. 0, 3d Corr. $9''$, True Dist. $92^{\circ} 24' 4''$.

* This diff. is the moon's corr. of dist. by the method No. 842. The sun's or star's corr. of dist. is found in like manner, thus: $47'' - 37'' = 10''$ (agreeing within $1''$).

[2.] *The Rigorous Method.*

845. In this method we find, by calculation, the true distance directly from the apparent distance and apparent altitudes.

(1.) Take both the app. alts. to the nearest even or odd minute, take their sum, and call the supplement of it the *1st supplement*.

Subtract from this suppl. the moon's corr. of alt., and add to it the sun's or star's corr. of alt.; call the result the *2d supplement*.

(2.) Take out the Logarithmic Difference, Table 73.

Take the app. dist. to the nearest even minute. Mark the seconds, if taken in *excess*, to be *subtracted*, or if *omitted*, to be *added* afterwards. To this add the 1st suppl., take the half sum, and from the half sum subtract the app. dist.

Add the log. sines of this half sum and remainder to the log. diff.; the sum (rejecting tens) is the log. sine square of an auxiliary arc x .

(3.) Under x put the 2d suppl., take the sum and the diff., and half the sum and half the diff.

Add together the log. sines of the last two terms; the sum is the log. sine square of an arc, which becomes the true distance on applying the reserved seconds.

Ex. 1. A. alt. \odot $47^{\circ} 31'$; app. alt. \triangleright $36^{\circ} 52'$; app. dist. $48^{\circ} 20' 29''$.

Sun's corr. of alt. $47''$; moon's H. P. $58' 35''$; moon's corr. of alt. $45' 35''$

\odot Alt. $47^{\circ} 32' 0''$	
\triangleright do. $36^{\circ} 52' 0''$	
$84 \ 24 \ 0$	1st Sup. $95^{\circ} 36' 0''$
	$45' 35'' + 47'' = -44 \ 48$
	2d Sup. $94 \ 51 \ 12$
$\triangleright 36^{\circ} 50'$, H. P. $58'$,	$9^{\circ} 995792$
2,	-5
	$35'' = -45$
$\odot 47^{\circ}$,	-14
	-64
	Log. Diff. $9^{\circ} 995728$

A. Dist. $48^{\circ} 20' (29'' \text{ omitted})$	
1st Sup. $95 \ 36$	
Sum $143 \ 56$	
Half S. $71 \ 58$	sine $9^{\circ} 978124$
Rem. $23 \ 38$	sin. $9^{\circ} 603017$
$\# 75^{\circ} 48' 48''$	sin. sq. $9^{\circ} 576869$

$\# 75^{\circ} 48' 48''$	
2d Sup. $94 \ 51 \ 12$	
Sum $170 \ 40 \ 0$	
Diff. $19 \ 2 \ 24$	
Half S. $85 \ 20 \ 0$	sine $9^{\circ} 998558$
Half D. $9 \ 31 \ 12$	sine $9^{\circ} 218363$
	pts. for 149
$47 \ 54 \ 32$	sin. sq. $9^{\circ} 217970$
$add \ 29$	
Ta. Dist. $47 \ 55 \ 1$	

846. It is useful to bear in mind, as a check against a gross mistake in clearing the dist., that the true and apparent distances cannot differ by more than the *sum* of the corrections of altitude. Again, when the moon's alt. is *equal* to, or *less* than, that of the other body, the true distance is *less* than the app. dist.; but the contrary does not always hold when the moon's alt. is the *greater*.

2. *Lunar Observation by the Sun.*

847. *The Observation.* (1.) The alts. of the sun and moon are required at the instant at which the distance is observed; when, therefore, the observer has assistants provided with proper watches, they will obtain the alts. during the time that he is observing the distance. See Nos. 560 and 561.

When the observer is alone, he will first observe the alt. of the body farthest from the meridian, then that of the other body, and then the distance; concluding with the alts. in the reverse order.* As precision is not necessary in the alts., one observation of the alt. will generally be enough at each time.

The time by watch is, of course, to be noted at each contact.

(2.) To observe the distance. Set the index nearly to the distance in the Nautical Almanac, at the nearest estimated Greenwich time; put down one or more shades to screen the central mirror, direct the sight to the moon, and, holding the plane of the instrument in the line joining the two bodies, vibrate it slowly round the line of sight as an axis till the sun's image is seen. Make a contact roughly, clamp the index, put in the telescope (previously adjusted to distinct vision by the moon), and complete the contact. See note 5, p. 182.

The relative brightness of the object and image is most conveniently adjusted by altering the distance of the telescope from the plane of the sextant by means of the screw for the purpose, as this motion causes a greater or lesser quantity of light to proceed to the eye from the silvered or brightest part of the mirror.

Observe at least 3 or 5 distances, or, with the circle, 3 or 5 pairs.

When, at sea, the ship has much motion, the observer fixes himself firmly in a corner, or lies on his back on the deck, in order to remove, as much as possible, the sense of bodily effort and inconvenience which disturbs the eye and the attention.

(3.) For precision observe the moon's true bearing; if she is near the zenith, observe that of the star instead.

848. *The Computation*. — (1.) Having reduced the alts. to the time of the mean of the distances, No. 660, find the Gr. Date. At sea, the Gr. Date is required only to the nearest hour; but if the moon's alt. is not observed, it must be found with precision. Reduce the hor. par., and thence the semid., from Table 40. Augment the semid., Table 42. For precision, correct the hor. par. by Table 41.

(2.) Find the App. Alts. of the centres by applying the ind. corr., dip, and semid.

Correct the observed distance for ind. error, and add the semi-diameters of the bodies: the result is the *apparent distance*.

(3.) Find the Sun's Corr. of Alt. by subtracting the par. in alt. from the refraction. Find the Moon's Cor. of Alt. by Table 39. Correct for the therm. and barom. whenever these instruments are accessible. Tables 32, 33.

(4.) Find the true distance by No. 842, 844; or, for precision, No. 845, and apply the corrections, Nos. 852 and 853.

(5.) For the G.M.T. Find, in the Nautical Almanac, the two distances between which the true distance falls. Take out the first of these, and set it down under the true dist., and write against it

* The reason of this order, as a general rule in such cases, is, that the outer body preserves uniformity in its change of alt. for a longer time than the other, and consequently its alt. may be reduced, by simple proportion, to an intermediate time, with less error than the alt. of the other body. See No. 558.

its prop. log given in the Nautical Almanac; note also the time (that is, the three hours) corresponding.

Take the difference between the two distances thus set down, and from its prop. log. subtract the prop. log. taken from the Nautical Almanac; the remainder is the prop. log. of a portion of time to be added to the time from the Nautical Almanac. The result is the G.M.T. of the true distance.

For precision, see No. 856.

The G.M.T. being found, the long. is determined.

Ex. 1. H M S. Eden, April 7th, 1831, lat. by acc. $34^{\circ} 30'$ S., long. 42° W., watch slow on the chron. $8^h 16^m 31^s$; chron. slow of G.M.T. $4^h 54^m 33^s$; height of eye, 16 feet; ind. corr. $-7' 36''$; had the following observations: required the error of the chronometer.

Times by Watch.	Alt. ☾	Alt. ☉	Distance.
12 ^h 57 ^m 24 ^s	39° 2'		
12 58 36		47° 33'	
1 1 29			66° 0' 8" (the mean of three sights.)
1 5 47		47 52	
1 8 18	36 42		
Reduction of the Altitudes to the time 1 ^h 1 ^m 29 ^s .			
☾ 39° 2',	12 ^h 57 ^m 24 ^s ,	4 ^m 5 ^s	1.644
	1 1 29		
36 42,	1 8 18,	10 54	8.782
2 20			0.109
			0.535
	-52'		
	39 2		
Moon's Alt.	38 10		
Sun's Alt. 47 41			
Reduced Obs.—Time, 1 ^h 1 ^m 29 ^s ; Alt. ☾ 38° 10'; Alt. ☉ 47° 41'; Obs. Dist. 66° 0' 8".			
Time by Watch	1 ^h 1 ^m		
Watch slow of Chron.	8 16		
Time of Obs. by Chron.	9 17		
Chron. slow	4 55		
	14 12		
	Gr. Date,* 7th	2 12	
Obs. ☾	38° 10'	Obs. ☉	47° 41'
Ind. Corr. — 8'		Ind. Corr. — 8'	
Dip — 4		Dip — 4	
Sem. — 16		Semid. + 16	
	-28		+4
☾ App. Alt.	37 42	☉ App. Alt.	47 45
☾ App. Alt. 37° 40', H. P. 56', 43' 5"		☉ App. Alt. 48°, Refr.	53"
2 pts. — 2"		Par. in Alt.	-6
38 + 30		☉ Corr. of Alt.	47
☾ Corr. of Alt.	43 33		
Clearing the Distance (No. 842), to the End.			
☾ Alt. 37½°, and Co-dist. 23½°		☉ Alt. 47° and 23°, M 159° 3', N 45° 5'	
M 137° 5', N 33° 4'		37° and 159	Dep. 95.7 (gr.)
☉ 47½° and 137° 5'		☉ Corr.	+0° 0 24
Dep. 101.4 (gr.)		☾ 2 Corrs.	-0 29 32
(Diff.) 68.0			-0 29 8
☾ 1st Corr.	-29' 37"	A. Dist.	66 24 6
☾ 2d Corr. 44', 8" } Corr. + 5"		True Dist.	65 54 58
30, 3 }		Do. at 0 ^h	67 0 8
			1 5 10
			2 ^h 11 ^m 35 ^s
		T. of Pr. Dist.	0
		G.M.T.	2 11 35
			p. log. 3054
			p. log. 4412
			p. log. 1361

* In working by an approximate method, an expert computer will infer the Gr. Date at once, and perform many other parts of the computation with little or no writing.

The watch being slow of the chron. $8^h 16^m 31^s$, the time of the obs. by the chron. is $1^h 1^m 29^s + 8^h 16^m 31^s$, or $9^h 18^m 0^s$; the chron. is therefore $7^h 6^m 26^s$ fast, or $4^h 53^m 35^s$ slow of the G.M.T. Now, by Table 58, an error of 1 in the dist. causes, in this case, an error of $2^m 8^s$ in the G.M.T.; hence the result may be considered as confirming the error of the chron. nearly enough.*

Ex. 2. Sept. 28th, 1878, at $3^h 11^m 40^s$ P.M., M.T. at ship; in lat. $48^\circ 50'$ N., long. $146^\circ 55'$ W.; obtained the mean of 7 distances between sun and moon $34^\circ 48' 16''$, obs. alt. $\odot 22^\circ 37'$, obs. alt. $\text{J} 18^\circ 7'$; height of eye 16 feet.

Gr. Date, Sept. $28^d 12^h 59^m 20^s$		App. Dist.	$35^\circ 20' 54''$
\odot 's Red. H.P.	$60' 35''$	\odot 's App. Alt.	$22 49$
Aug. Semid.	$16 37$	\odot 's App. Alt.	$18 20$
\odot 's alt. $22^\circ 49'$	Ref. $2' 18''$	$18^\circ 20'$ H.P. 60	$54' 4$
	Par. -8		$+ 33$
\odot 's corr. of alt.	$2 10$	\odot 's Corr. of Alt.	$54 37$

Clearing the Distance by No. 844.

\odot App. Alt. $22^\circ 49'$cos. 9'9646	App. Dist.	$35^\circ 20' 54''$
\odot App. Alt. $18 20$ cos. 9'9774	\odot Cor. Alt. $54' 37''$	} - 56 47
App. Dist. $35 21$ sin. 9'7624	3d Corr. $2 10$	
$76 30$ 9'6990		$34 24 7$
Half Sum $38 15$ sec. $0'1050$		1st Corr. $+ 41 34$
1st Rem. $15 26$ cosec. $0'5749$		\odot 's Corr. Alt. $+ 2 10$
2d Rem. $19 55$	cosec. $0'4677$	2d Corr. $+ 36$
Corr. Alt. $54' 37''$ P.L. $0'5179$	$2' 10''$ P.L. $1'9195$	True Dist. $35 8 27$
1st Corr. $41 34$ P.L. $0'6366$	3 Cor. $2 10$ P.L. $1'9182$	At 12^h $34 34 33$ P.L. $24 17$
Diff. $13 3$		$0 33 54$ P.L. $72 51$
		$0^h 59^m 8^s$ P.L. $48 34$
		12
Dist. $35^\circ 55'$ Corr. $38''$		M.T.G. $28^d 12 59 8$
13		M.T.S. $28^d 3 11 40$
2d Corr. $+ 36$		Long. $9 47 28$
		$= 146^\circ 52' W.$

Ex. 3. Sept. 1st, 1878, at $4^h 40^m 4^s$ P.M., M.T. at ship; lat. $3^\circ 2'$ N., long. $1^\circ 5' W.$, obs. alt. $\odot 20^\circ 0'$, obs. alt. $\text{J} 62^\circ 30'$, obs. dist. $61^\circ 26' 26''$; height of eye 18 feet.

Gr. Date, Sept. $1^d 4^h 44^m 24^s$		App. Dist.	$61^\circ 58' 51''$
\odot 's Red. H.P.	$59' 38''$	\odot 's App. Alt.	$20 12$
Aug. Semid.	$16 31$	\odot 's App. Alt.	$62 42$
\odot 's Alt. $20^\circ 12'$	Ref. $2' 37'$	$62^\circ 40'$ H.P. 59'	$26 36''$
	Par. -8	2	-2
\odot 's Corr. of Alt.	$2 29$	$38''$	$+ 16$
		\odot 's Corr. of Alt.	$26 52$

* The Nautical Almanac, before 1834, was computed for apparent time; the above result is therefore Greenwich app. time. This does not, however, in any way affect the value of a mere example.

Clearing the Distance by No. 844.

☉ App. Alt. 20° 12cos. 9° 9' 24"	App. Dist.	61° 58' 51"
☽ App. Alt. 62 42	cos. 9° 66' 15"	☽ Corr. Alt. 26° 52'	- 27 10
App. Dist. 61 59	sin. 9° 94' 59"	3d Corr. 0 18	J
144 53	9° 69' 90"		61 31 41
Half Sum 72 26½	sec. 0° 52' 04"	1st Corr.	+ 31 39
1st Rem. 52 14½	cosec. 0° 102' 0"	☉'s Corr. Alt.	+ 2 29
2d Rem. 9 44½	cosec. 0° 77' 16"	2d Corr.	+ 0 4
Corr. Alt. 26° 52'	P. L. 0° 82' 61"	True Dist.	62 5 53
1st Corr. 31 39	P. L. 0° 75' 49"	At 3 ^h	61 7 38 P. L. 2541
Diff. 4 47	3d Corr. 0° 18' P. L. 2° 76' 95"		0 58 15 P. L. 4900
			1 ^h 44 ^m 33 ^s P. L. 2359
			3
Dist. 62° 27	Corr. 4"	M. T. G. 1 ^d	4 44 33
	5	M. T. S. 1 ^d	4 40 4
	2d Corr. + 4	Long.	4 29
			= 1° 7' 15" W.

Ex. 4. Sept. 30th, 1878, at 4^h 24^m 46^s P.M., M.T. at ship, lat. 17° 9' S, long. acc. 102° 40' W.; obs. alt. ☉ 16° 12'; obs. alt. ☽ 73° 14'; obs. dist. 60° 22' 59"; height of eye 16 feet.

G.M.T. Sept. 30^d 11^h 35^m 26^s, corr. H.P. 58' 59", aug semid. 16' 21". ☉'s app. alt. 16° 24', ☽'s app. alt. 73° 26', app. dist. 60° 55' 21"; ☉'s corr. of alt. 3' 8", ☽'s corr. of alt. 16' 32", true dist. 61° 10' 36". Long. 102° 47' 30" W.

3. Lunar Observation by a Star or a Planet.

849. *The Observation.*—Take the alts. as directed, No. 847. In taking the distance, direct the view to the star, make the contact nearly between the star and the illuminated edge of the moon, whether it be the nearest or farthest limb; clamp the index, put in the telescope previously adjusted to distinct vision by the star, and complete the contact by bisecting or splitting the star upon the moon's limb.*

When the moon is bright, it is necessary to use a shade.

The setting of the index, No. 847 (2), is a more important step in observing with the star than with the sun, for the amount of distance is often the only security for employing the right star.

For precision, note the azimuth as directed No. 847 (3).

850. *The Computation.* (1.) Proceed by No. 848 (1). For a planet, take out the hor. par. from the Nautical Almanac, and reduce it.

(2.) Find the app. alts. as in No. 848 (2).

For the app. dist., correct the observed dist. for ind. error. When the *nearest* limb is observed, *add* the moon's semid.; when the *farthest*, *subtract* it.

* It has been recommended to observe the star open of the moon's edge, leaving a dark space of about 40". But this dark space will appear differently in different telescopes; and, moreover, it is better to be in the practice of observing accurately than loosely.

The inaccuracy which arises in bisecting a planet when it is not, as we should say of the moon, at the full, is but small; since, even in the case of Venus, the only planet which ever appears as a crescent when observed with the moon, it can scarcely exceed 6" or 8". It has been proposed to correct for this by a special computation.

(3.) Find the star's corr. of alt., which is the refraction. For a planet, apply the par. in alt. from Table 45. For the moon, take her corr. out of Table 39. For precision, correct for the height of the barom. and therm.

(4.) Find the true distance, and proceed as in No. 848 (4), to the end.

Ex. July 16th, 1826, near midnight, lat. by acc. $27^{\circ} 5' N.$, at $2^h 34^m 13^s$ by the chron., obs. alt. $\searrow 35^{\circ} 12'$; obs. alt. Fomalhaut, $12^{\circ} 51'$; obs. dist. farthest limb, $70^{\circ} 1' 10''$. Ind. corr. $-20''$; height of eye, 16 feet: required the error of the chron. supposed fast on G.M.T. $1^h 6^m 25^s$.

Time by chron.	$2^h 34^m$	H.P. 16th, midnight	$59' 42''$
Chron. fast.	$1 \quad 6$	17th, noon	$59 \quad 35$
G.D. 6th, past midnt.	$1 \quad 28$	Var. in 12^h	7
		Red. H.P.	$59 \quad 41$
		Corresp Sem. $16' 16''$; Aug. do. $16' 27''$.	
Obs. Alt. \searrow	$35^{\circ} 12'$	Obs. Alt. *	$12^{\circ} 51'$
Dip $-4'$		Dip	-4
Sem. $+16'$	$+12$	* A. Alt.	$12 \quad 47$
A. Alt.	$35 \quad 24$	Obs. Dist.	$70^{\circ} 1' 10''$
		Ind. Corr.	-20
$35^{\circ} 20'$, and H.P. $59'$,	$46' 47''$	D Sem.	$-16 \quad 27$
$4, -2'$	$+31$	A. Dist.	$69 \quad 44 \quad 23$
$41', +33'$		* Alt.	$12^{\circ} 47'$
Corr. of Alt.	$47 \quad 18$	* Corr. of Alt.	$4 \quad 12''$

Clearing the Distance (by No. 842) to the End.

$\searrow 35\frac{1}{2}^{\circ}$ and 20° , M $130^{\circ} 7'$ N. $26^{\circ} 0'$	* 13° and 20° , M $109^{\circ} 2'$ N. $8^{\circ} 4'$
* 13° and 131° Dep. $29^{\circ} 5'$ (gr.)	$\searrow 35^{\circ}$ and 109° Dep. $62^{\circ} 5'$ (gr.)
$3' 5$	* Corr. $+0^{\circ} 2' 12''$ 54.1
\searrow 1st Corr. $-1 \quad 36''$	\searrow 2 Corrs. $-0 \quad 1 \quad 30$
\searrow 2d Corr. $\{ 47', 6'' \} +6$	$+0 \quad 0 \quad 42$
	A. Dist. $69 \quad 44 \quad 23$
	True Dist. $69 \quad 45 \quad 5$
	Dist. at Mid. $70 \quad 31 \quad 15$ p. log. $.2747$
	$46 \quad 10$ p. log. $.5909$
	G.M.T. $1^h 26^m 55^s$ p. log. $.3162$
	T. by Chron. $2 \quad 34 \quad 13$
	Error, fast $1 \quad 7 \quad 18$

Ex. 2. Sept. 7th, 1838, P.M., lat. $3^{\circ} 2' N.$, long. $4^h 0^m W.$, at $12^h 57^m 8^s$ by watch, obs. five distances of the moon's nearest limb from Aldebaran, $27^{\circ} 47' 12''$. App. alt. * $26^{\circ} 32'$; app. alt. $\searrow 53^{\circ} 34'$; watch slow $9^m 17^s$ of M.T.; ind. corr. $-1' 10''$; required the longitude.

\searrow red. H.P. $59' 48''$; true dist., by No. 845, $28^{\circ} 37' 17''$; dist. at XV^h, $29^{\circ} 47' 47''$.
LONG. $59^{\circ} 56' W.$

Ex. 3. Sept. 2d, 1840, P.M., lat. $3^{\circ} 2' N.$, long. $60^{\circ} 0' W.$, at $8^h 48^m 39^s$ by watch, obtained the mean of 5 distances between Saturn and the moon's nearest limb, $89^{\circ} 42' 55''$; ind. corr. $-1' 25''$; watch slow of M.T. $7^m 33^s$; app. alt. $\searrow 53^{\circ} 3'$; app. alt. Sat. $23^{\circ} 34'$.

\searrow red. H.P. $60' 44''$; true dist., by No. 845, $89^{\circ} 56' 11''$; dist. at III^h, $89^{\circ} 1' 31''$.
LONG. $60^{\circ} 1' W.$

Ex. 4. July 14th, 1878, at $2^h 10^m 0^s$ A.M., M.T. at ship, lat. $22^{\circ} 0' S.$, long. acc. $149^{\circ} 30' E.$, obs. alt. Antares $19^{\circ} 33'$, obs. alt. $\searrow 51^{\circ} 48'$, obs. dist. near limb $74 \quad 32' 49''$, height of eye 24 feet.

G.M.T. July 13^d 4^h 12^m, corr. H.P. 56' 41". aug. semid. 15' 29", * app. alt. 19° 28',
 ½ app. alt. 51° 59' app. dist. 79° 38' 18", * corr. 2' 44", ½'s corr. 34' 9", true dist.
 79° 29' 41". LONG. 149° 33' E.

Ex. 5. June 19th, 1878, at 4^h 30^m A.M.; M.T. at ship, lat. 20° 10' N., long. acc. 75° W.,
 obs. alt. Venus 23° 14', obs. alt. ☽ 52° 54'; obs. dist. near limb 86° 45' 44", height of eye
 16 feet.

J.M.T. June 18^d 21^h 30^m, corr. H.P. 55' 7", aug. semid. 15' 14", Venus' app. alt. 23° 10',
 ½'s app. alt. 53° 5'; app. dist. 87° 0' 58", Venus' corr. 2' 9", ☽'s corr. 32' 23", true dist.
 86° 43' 48". LONG. 75° 6' 15" W

4. *Special Corrections.*

851. When precision is required, it is necessary, besides removing from the distance the general effects of refraction and parallax, to apply certain corrections.

[1.] *Correction for the Elliptical Figure of the Disc.*

852. Since the refraction of each point of the disc of the sun or moon is greater as the alt. of such point is less, and since the change of refraction is proportional to small changes of alt., the upper and lower halves of the circular disc take more or less the figures of ellipses, the lower half being more flattened than the upper half. The distance, therefore, between the centre and the limb, as it would actually be observed, is less than the horizontal semidiameter of the Tables. The elliptical figure of the sun, due to this cause, is often conspicuous at rising and setting. The correction in Table 53 is to be subtracted from the semidiameter.*

[2.] *Correction for the Spheroidal Figure of the Earth.*

853. The true distance found from the data, as above, is deduced on the supposition that the earth is a sphere, instead of a spheroid. The true distance found is, in fact, that corresponding to a sphere of smaller dimensions than those circumscribed by the equator,† and to an horizon differently placed with respect to the equator, or to another latitude than that of the spectator.

Since, however, the mere change of the place of the spectator would cause no alteration in the apparent angular distance of two stars, the change of distance arises solely from the variation of the apparent place of the moon, produced by the changing of the observer's astronomical latitude for the geocentric latitude. The change of place of the moon is thus in general the resultant of a change both of her altitude and her azimuth.

This correction is 0 at the equator and poles, and is greatest in lat. 45°. As it cannot much exceed $\frac{1}{6}$ of the reduction of latitude, it may in practice be omitted, but the effect rarely disappears altogether.

* We have not applied this correction, because at low altitudes, the only case in which it is sensible, the observation is not to be depended upon within such small quantities.

† The correction on this account has already been made in the reduction of the moon's equatorial parallax.

854. To correct the distance.

Enter Table 55 with the lat. and the alt. 90° , and take out the number.

For Part I. Enter Table 5 with the complements of the moon's azimuth and of the angle at the moon (found by No. 842 or 844),* and take out M. Divide the number by M.

For Part II. Enter Table 5 with the moon's azimuth and the angle at the moon, and take out M. Divide the number by M.

The quotients are in seconds, and are to be applied to the distance as follows.

Note.—The observer is supposed to face the moon, and the azimuth is reckoned from the S. in N. lat., and from the N. in S. lat.

Part I.					Part II.		
☾ to the Eastward	In N. Lat.		In S. Lat.		Angle at the ☾ less than 90°	Azimuth of the ☾	
	Sun or Star		Sun or Star			less than 90°	greater than 90°
	to the right	to the left	to the right	to the left			
	sub.	add	add	sub.		sub.	add
☾ to the Westward	add	sub.	sub.	add	Angle greater than 90°	add	sub.

Ex. Lat. 48° N.; moon's alt. 30° ; star's alt. 61° ; dist. 54° ; moon's azim. S. 72° E.; and the star to the right.

The angle at the moon is 34° .

The number in Table 55 is 1100.

Co-az. 18° , Co-ang. 56° , M 1880

$\frac{1100}{188} = 6''$, subtractive.

As. 72° , Ang. 34° , M 390

$\frac{1100}{390} = 3''$, subtractive.

Hence the CORRECTION is $-9''$.

855. When the moon is near the zenith, or when her alt. exceeds 80° , with the lat. and the compl. of the star's azimuth as an altitude, take out the seconds from Table 57, and divide them by 100; the quotient is the correction required in seconds.

When the star's azim. (reckoned as above) is less than 99° , subtract the corr., otherwise add it.

* Since the angle at one or both bodies, which is given by the method No. 842, is necessary in making the corrections, No. 852, 853, and since that method affords both an approximation by which the long. by acc., if greatly in error may be corrected, and at the same time a check against any important error in the rigorous process itself, it will be advisable to employ it on all occasions.

The angle at the body may be found from No. 844, when that method is employed, thus:—Take the sum of the logs., rejecting the const. 9.6990 and the prop. log.; the ar. co log. of this sum is the log. sine square of the angle required.

Ex. No. 844.

Sum of four logs.

0.6641

Sum of logs.

0.4075

ANGLE at \odot $55^\circ 30'$ sin. sq. 9.3359

ANGLE at \odot $77^\circ 12'$ sin. sq. 9.5925

[3.] *Correction for the Inequality of the Moon's Motion.*

856. Since the moon does not generally change her distance from the sun or a star at the same rate, both at the beginning and end of 3 hours, it is often proper to apply a correction to the Gr. M. T. found, which, in the extreme case, may be in error 50' of long.

When the distance exceeds 26°, this correction will not exceed 15' of long.; when the distance is near 90°, it will not exceed 2'. In general, it is smallest in the case in which the sun or star is in a direction perpendicular to the line of cusps or horns.

857. Take the diff. between the prop. logs. in the Nautical Almanac against the two distances between which the given true dist. falls. With this diff., and the portion of time found in No. 848 (5), enter Table 57, and take out the seconds. When the prop. logs. in the Nautical Almanac are *increasing*, *subtract* these seconds; when *decreasing*, *add* them; the result is the M. T. at Greenwich, corrected.

Ex. 1. Dist. in Naut. Alm., preceding given dist.,

	22° 58' 21"	prop. log. 3079
following do.	24 56 56	do. 3054 (<i>decreasing</i>)
		Diff. 25

Diff. 25 under Int. 13^m, (*add*)

0 ^h	0 ^m	2 ^s
0	26	9
0	26	11

CORRECTED G. M. T.

Ex. 2. In Ex. 2, No. 850, dist. 29° 47' 47" has the prop. log. 2527; the next in order has 2531; the diff. 54 gives 14^s to be *subtracted*; and the long. corrected, 59° 52' W.

858. *Degree of Dependence.* The true distance is affected by errors of observation, and by errors of computation. An error in the distance, of whatever kind, produces, on the average, about 30 times its amount in the longitude; thus, 10" error of distance produce about 300" or 5' error of longitude.

The observed distance is liable to the ordinary errors of angular distance, the chief of which are, perhaps, most usually that due to defect of parallelism of the telescope, and that arising from making the contact above or below the centre of the field. Irradiation is also included in the errors of observation.

859. The error of the computed result arises from two sources; the errors in the elements of the observation, and those of the method of solution.

(1.) Under the first of these heads are comprised the errors in the horiz. par. in reducing it to the Gr. Date, and for the figure of the earth, the error of the tabular semidiameter;* and that of refraction in low altitudes.

(2.) The effects of errors of a few minutes in the altitude are insensible. Hence an ill-defined horizon is no great detriment to a

* The Greenwich observations shew that the semidiameter of the moon, as given in Besselhardt's tables, is 3" too small.— See "Green. Obs." 1837.

good observation; and hence, also, in computing the altitudes, precision is not essential. This last remark is worth attention, since the calculation of altitudes is a heavy addition to the work of a lunar. On the same account it will not be necessary to consider the change of place during the observation, unless the second alt. of either body be lost.

(3.) The importance of correcting for the barometer and thermometer has been noticed, No. 838. The atmospherical correction is of most consequence at low altitudes, and when the bodies are in or near a vertical plane.

(4.) The smaller corrections, namely, reduction of equatorial parallax, corrections for elliptical disc, for the figure of the earth, and for unequal motion, cannot all be applied the same way in any observation; compensation will accordingly take place to a considerable extent even when these corrections are omitted altogether. It will, however, be advisable to apply the latter correction, No. 856, when large.

860. The error of the method of solution, No. 842, may be estimated for distances exceeding 50° at not more than $20''$, in general, or $10'$ of long.

Method II., No. 844, will, in the same cases, be more accurate.

861. The effects of errors in general, and especially constant errors of observation, are removed in a considerable degree by observing *equal distances* on *opposite sides* of the moon, since the errors of the resulting longitudes will be of opposite kinds. The true long. will not, however, be the *mean* of the two erroneous longitudes, unless the moon changes her distance from both bodies at the same rate.

When the two longitudes in such a case differ widely, add the prop. log. of their difference in time to the prop. log. of the *greater* motion in 3 hours (which is the *smaller* of the prop. logs. in the Nautical Almanac), and the ar. co. prop. log. of the sum of the two 3-hourly motions; the sum is the prop. log. of a portion of the time to be applied to the long. obtained by the star whose prop. log. is employed.

Since the true long. must fall between the two given results, it will be known at once whether to add or subtract.

When the sum exceeds 3° , read the degr. and min. as min. and sec.

Ex. The long. by Regulus, in a certain case of a lunar, is $2^h 37^m 15^s$; by Antares, $2^h 40^m 58^s$; the distances being nearly equal on opposite sides, and observed by the same observer with the same instrument. The 3-hourly motion of Regulus is $1^\circ 45' 31''$, that of Antares $1^\circ 30' 29''$: required the True Long.

Long. Reg.	$2^h 37^m 15^s$	3-hour. mot.	$1^\circ 45' 31''$	p. l.	$(1' 45'')$	$2^o 101$
Ant.	$2^h 40^m 58^s$	do.	$1^\circ 30' 29''$			
			$3^\circ 16' 0''$	ar. co.	$(3' 16'')$	$8^o 2588$
				p. l.		$1^o 6851$
	$\therefore 43 \dots$		$0^h 2^m 0^s$	p. l.		$1^o 9540$
			$2^\circ 37' 15''$			
			$2^\circ 39' 15''$			

Long. req. $2^\circ 39' 15''$ ($9''$ more than the mean).

862. After the result has been obtained with the utmost care, there remains the error of the lunar tables, which appears to be about 0.5 of R.A., or 4' of long. This can be removed only by careful examination of observations of the moon, made near the same time in a fixed observatory. In general, the result will have more value as the moon's horizontal parallax is greater, because her motion is then more rapid; on the contrary, the result is of less value as the horiz. par. is less. Since the changes of the moon's R.A., at their maximum and minimum, are nearly in the ratio of 5 to 3 and since the change of R.A. is in a considerable degree, though not in exact proportion, greater as her distance from the earth is less, it is evident that the place of the moon at the time of observation materially affects the value of the result.*

5. Computation of the Altitudes.

863. When the altitudes are not observed they must be calculated. M. T. is supposed to be given.

(1.) Reduce to the Gr. Date the sid. time at mean noon, also the R. A. and decl. of each body, unless one of them is the sun, in which case reduce the equat. of time instead of his R. A.

(2.) Find the hour-angles, Nos. 609 to 612, and compute the alt. of each body, No. 667. See No. 859 (2).

For the *apparent* altitudes. Take out the corrections of altitude to the true alts., found as if for app. alts., to the nearest minute, and apply these corrections the *contrary way* to that directed in the rules, Nos. 644, &c.†

Ex. Sept 11th, 1838, A.M., at Fort St. Joaquim, lat. $3^{\circ} 2' N.$, long. $4^h 0^m W.$, at $9^h 49^m 40^s$ by watch, obtained the mean of five distances of the sun and moon, $82^{\circ} 16' 51''$. Ind. corr. — $55''$; watch fast of M. T. $3^m 2^s$; therm. 85° ; barom. 29.7 inch.

T. by watch	$9^h 49^m 40^s$	D H. P. 11th, noon	$56' 56''$
Watch fast	$- 3 \quad 2$		$56 \quad 32$
	<hr/>		<hr/>
	$9 \quad 46 \quad 38$		$0 \quad 24$
M. T.	$21 \quad 46 \quad 38$		<hr/>
Long W.	$4 \quad 0 \quad 0$		$0 \quad 3$
Gr. Date, 10th,	$25 \quad 46 \quad 38$		<hr/>
or 11th,	$1 \quad 46 \quad 38$	Red. H. P.	$56 \quad 56$
		Semid.	$56 \quad 53$
			<hr/>
			$15 \quad 30$

* In combining the results of different observations for the purpose of deducing the longitude of a place, regard would be had to this and other circumstances in giving a different weight to each several result. The final determination of positions, however, by means of observations made at different times and under different circumstances, concerns the hydrographer or geographer rather than the seaman or traveller, and is not a subject for this volume.

† As the altitudes in a lunar are not required with precision, Tables 43 and 44, which are necessary to remove the inaccuracy of using the true alts. as arguments, will rarely be employed.

It will be prudent to verify the result by the method of inspection (see Expl. of Table 5), in order to avoid entailing any material error on the whole of the subsequent computation.

Elements for computing the Altitudes.*

Sid. T. noon	11 ^h 20 ^m 14 ^s	M. T.	21 ^h 46 ^m 38 ^s	R. A. 11th, 1 ^h ,	5 ^h 41 ^m 14 ^s
1 ^h , 10 ^s }			+ 3 24	2,	5 43 42
46 ^m 1, 7 }	17		21 50 2 W.		2 18
Red. S. T.	11 20 31	☉ H.-ang.	2 9 58		9 5229
M. T.	21 46 38	☉ Decl.	4° 38' 38" N.	2 ^m 28 ^s	1 8612
	33 7 9		4 15 45 N.	46 38	0 5866
Eq. of T. 11th,	3 ^m 23 ^s		22 53	0 ^h 1 ^m 55 ^s	8 9727
12th,	3 44		1 40	5 41 14	
	21	Red. Decl.	4 38 38	Red. R. A.	5 43 9
Rel. Eq T.	3 24	P. Dist.	4 36 58 N.		33 7 9
			85 23	☉ H.-A.	3 24 0
				☉ Decl.	28° 36' 48" N.
				D. 13"	1
				☉ Decl.	28 38
				P. Dist.	61 22

Computation of the Altitudes.

☉ H.-A.	2 ^m 9 ^m 58 ^s		☉ H.-A. 3 ^h 24 ^m 0 ^s	
Suppl.	9 50 2	sin. sq. 9 96461	Suppl.	8 36 0
P. D.	85° 23'	sine 9 99859	P. D.	61° 22'
Col.	86 58	sine 9 99939	Col.	86 58
	172 21			148 20
Arc π	146 36	sin. sq. 9 96259	Arc π	115 21
	318 57			263 41
	25 45			32 59
	159 28	sine 9 54500		131 50
	12 53	sine 9 34824		16 29
	32° 29'	sin. sq. 8 89324		54° 45'
☉ Tr. Alt.	57 31		☉ Tr. Alt.	35 15
Corr. Alt.	+ 1		Corr. Alt.	- 46
☉ A. Alt.	57 32		☉ A. Alt.	34 29
				82° 16' 51
				- 55
				82 15 56
				+ 15 55
				+ 15 50
				+ 9
				A. Dist. 82 47 50
☉ 57° 32',	37"		☉ 34° 20', H. P. 56',	44' 50"
	- 5		9	- 4"
85°, - 2"	32		53" + 43	+ 39
2, 0	- 2			45 29
☉ Corr. of Alt.	30		85°, - 5"	+ 6
			- 1	
			☉ Corr. of Alt.	45 35

Proceeding to clear the distance by No. 845, the log. diff. is 9 996092, and the true dist. 82° 4' 51". The next dist. preceding is 82° 58' 33", at noon; and the G. M. T. 1^h 47^m 0^s, or Long. 60° 5' 30" W.†

* To adapt this form for computing the altitudes to the case of a planet, put the planet's hor. par. in the place of the equat. of time; and in the next column the planet's R. A.

† This observation, and those in Examples 2 and 3 of No. 850, were taken, with several others, by Sir Robert Schomburgk, to whom I am indebted for them.

III. BY THE MOON'S ALTITUDE.

864. Since Mean Time is determined by the hour-angle and R.A. of a celestial body, the R.A. may be determined from the M.T. and the hour-angle, the latter being computed from the observed altitude. Now the moon's R.A. being given in the Nautical Almanac for certain points of time, the time at Greenwich corresponding to any given R.A. of the moon may be at once found.

The moon's altitude has accordingly been often thus employed in determining the longitude; but the method requires much caution, because an error of altitude produces, in the hour-angle computed from it, a quantity greater than itself, except in the single case in which the observer is on the equator and the body on the prime vertical, when these errors are equal. Accordingly, since an error in the moon's hour-angle appears in its full amount in her deduced R.A., and since the R.A. changes at the rate of about 2^m only in an hour, the longitude required is vitiated to the extent of not much less than thirty times the error of altitude in the most favourable cases.

It is evident, therefore, since the place of the sea-horizon is often doubtful from $1'$ to $3'$, that the result of a simple lunar altitude must be in general greatly inferior to that of a lunar distance, in which a good observer rarely makes an error exceeding half a minute. But as many persons, who are not sufficiently expert in the lunar observation to obtain on all occasions a satisfactory longitude, are nevertheless capable of observing altitudes with precision, and, moreover, as the stars, when the air is not very clear, are often too faint for the lunar observation, the former method may, on some occasions, prove of service, provided that proper steps are taken to diminish the effects of the errors of latitude and altitude.

Since on the equator, when the body is E. or W., an error of $1'$ in alt. produces an error of $4'$ in the hour-angle, and an error of $8'$ in lat. 60° (or in the ratio of the secant of the latitude to 1), the method serves better in low than in high latitudes.

If the resulting longitude differs much from the long. by account, the computation should of course be repeated.

865. *Limits.* The azimuth is the same as that laid down for determining the time by a single altitude, No. 778. The alt. should in general not be less than 6° or 8° ; and when the barometer and thermometer are not at hand, not less than 25° or 30° , especially in very cold or very hot weather.

866. *The Observation.* Observe the moon's alt., noting the time.

If the mean time is not accurately known, obtain observations for it.

At sea, the uncertainty of the apparent dip may be removed by referring the moon's altitude to the opposite point of the horizon, as well as to that under her (No. 535).

But it will be preferable to observe the *difference* of alt. of the moon and some star on nearly the same bearing, and to apply it to the star's alt. found by computation; for the time may sometimes be more nearly known than the lat., and the alt. of a star computed more nearly than it can be observed.

For Ex. Suppose, in lat. 40° , the γ bearing E.S.E. (true), that the place of the sea horizon is $1' 30''$ in error, and the time in error 5^s . Then the error of the γ 's computed hour-angle (and therefore of her R.A.) will be 9^s (No. 671), and the resulting error of long. about $4^m 30^s$, or $1^\circ 4'$ (Nos. 858, 864). Now the error of the computed alt. of a star E. or W. due to an error of 5^s will here be $56''$ (No. 671); hence the error of the long., as determined by the moon's alt. referred to this star, will be diminished in the proportion of $1' 30''$ to $56''$, that is, from $64'$ to $40'$.

867. *The Computation.* (1.) Find the Gr. Date, and reduce to it the Sid. T. at mean noon, the moon's decl., and thence her pol. dist., her hor. par., and semidiameter; correct the hor. par. by Table 41.

(2.) Add the M.T. to the red. Sid. T.; the sum (rejecting 24^h if it exceed 24^h) is the R.A. of the meridian.

(3.) Correct the alt.*

(4.) Compute the moon's hour-angle, No. 614.

(5.) When the moon is to the E. of the meridian, *add* her hour-angle to the R.A. of the mer. If the sum exceed 24^h , reject 24^h . When to the W., *subtract* the hour-angle from the R.A. of the mer., increased, if necessary, by 24^h : the result is the moon's R.A.

(6.) For the G. M. Time. Set down in order this R.A., that preceding it, and that following it (from the Nautical Almanac); take the diff. between the 1st and 2d, and between the 2d and 3d, adding 24^h , if necessary, to effect the subtraction.

To the constant 0.4771 add the prop. log. of the first of the diffs. and the ar. co. prop. log. of the 2d; the sum is the prop. log. of a portion of time to be *added* to the hour at Green. of the middle one of the three right ascensions: the sum is the G. M. T.

Ex. 1.† Jan. 5th, 1839, lat. $4^\circ 54' 0''$ S., long. by acc. $33^\circ 13' W.$, at $20^h 56^m 40^s.8$ M.T., obs. alt. γ $30^\circ 6' 20''$ to the W.; ind. corr. $-35''$; height of eye, 12 feet; therm. 82° , barom. 30.0 inches: required the longitude.

M. T.	$20^h 56^m 41^s$	γ Decl. 5th, at $23^h, 0^\circ 16' 39''$ S.	H. P. 5th, Mid.	$54^\circ 25' 2''$
$33^\circ 13' W.$	$+ 2 \ 12 \ 52$	Diff. for $1c^m, 142''$	6th, Noon	$54 \ 18 \ 0$
Gr. D.	$23 \ 9 \ 33$	$0^\circ 16 \ 39''$	Var. in 12^h	$7 \ 2$
Sid. T. 5th,	$18 \ 57 \ 34.8$	$140'', 9^m, 2' 6''$	$7^m 2$ and $11\frac{1}{2}^h$,	$0 \ 6 \ 8$
23^h	$3 \ 46.7$	$33'' \ 7.7$		$54 \ 25 \ 2$
9^m	1.5	$2 \ 9\frac{1}{2}^m \ 1.9$	Equat. H. P.	$54 \ 18 \ 4$
33^s	$.1$	Red. Decl. $0 \ 18 \ 55$ S.	Corr. Table 41	0
Red. S. T.	$19 \ 1 \ 23.1$	Pol. Dist. $89 \ 41 \ 5$	Corr. Semid.	$14 \ 48$
M. T.	$20 \ 56 \ 40.8$		Augm.	7
R. A. Mer.	$15 \ 58 \ 39$		Aug. Sem.	$14 \ 55$

* It cannot be worth while to follow the 2d and 3d precepts of No. 655, unless the observation is in every respect such as to afford extreme precision in the result.

† These examples are selected from observations made by Mr. J. C. Rowring on board *rd. M. S. Stag*, with which I have been favoured by Mr. Pentland, her Majesty's late consul-general at Bolivia.

Obs. Alt. \bar{Y}	30° 6' 20"
Ind. Corr. --0' 35"	
Dip. -3 20	<u>-3 55</u>
	30 2 25
	<u>-14 55</u>
App. Alt.	29 47 30
29° 40' and 54'	45' 14"
7 sub. $\frac{3}{3}$	
13 add 16	<u>+13</u>
	45 27
Th. 82° add 6	
Ear. 30 0	6
	<u>+45 33</u>
True Alt.	30 33 3

Alt.	30° 33' 3"
Lat.	4 54 0
P. Dist.	89 41 5
	<u>125 8 8</u>
	62 34 4
	<u>32 1 1</u>
Hour-ang. 3 ^h 57 ^m 25 ^s ·2	sin. 9'663417
	<u>sin. 9'724415</u>
	sin. sq. 9'389429
	<u>15 58 3 9</u>
R. A. 12 0 38 7	0°4771
At 23 ^h , 12 0 23 9	0°14'·8 2'8632
0, 12 2 8 3	1 44 4 7'9853
	<u>0^h 8^m 30^s·3</u>
	23
G. M. T.	23 8 30 3
M. T.	20 56 40 8
LONG.	2 11 49 5 or 32° 57' W.

An error of 1° of R. A. would produce here 34° or 8½' error of long., as the R. A. changes very slowly. An error of 1' of alt. would cause 4° of R. A. and 34' of long., and an error of 1' of lat. only 0°·1 of R. A. The moon's azim. is 87°.

Ex. 2. Jan. 23d, 1839, lat. 20° 57' 10" N., long. by acc. 42° 39' W., at 3^h 32^m 10^s M. T. obs. alt. \bar{Y} 42° 25' 28" to the E. Ind. corr. +1' 17"; height of eye, 12 feet; required the Longitude.

Gr. Date, 23d	6 ^h 22 ^m 46 ^s	Red. Decl.	21° 42' 15" N.	Equat. H. P.	58' 42"·1
Red. S. T.	20 9 35 7	Pol. Dist.	68 17 45	Red. do.	58 40 8
R. A. Mer.	23 41 45 7			Corresp. Sem.	16 0
				Aug. Sem.	16 11

Corr. of Alt.	42' 26"
True Alt.	42 50 10

Hour-angle	3 ^h 23 ^m 27 ^s ·0
R. A.	3 5 12 7
Do. at 6 ^h	3 4 20 2
	<u>3 6 41 8</u>
G. M. T.	6 ^h 22 ^m 15 ^s
LONG.	2 50 5 or 42° 31' W

An error of 1° of R. A. produces here 25°, or 6' error of long.; an error of 1' of alt. produces 4°·3 error of R. A., or 27' of long.; and an error of 1' of lat. causes 0°·9 of R. A., or 5' of long.

868. When two or three observations are taken on the same side of the meridian and prime vertical, the true long. is not the mean of the results, but is nearer to that which is furthest from the meridian.

When two observations are taken on opposite sides of the meridian and on the same side of the prime vertical, the right ascensions resulting will be affected in different ways by the same errors of altitude and latitude, and the true long. will be between the two results.

869. *Degree of Dependence.* This is determined by the effects produced on the hour-angle by given errors in the alt., lat., and pol. dist., No. 615. It is evident, from the remarks above, that unless considerable care, and some skill, are devoted to diminishing, according to the circumstances of the case, the effects of errors of latitude and altitude, it cannot be prudent, notwithstanding the occasional success of observations of this kind, to depend upon the result as nearer than ½ of a degree.

On shore, when the lat. and time are accurately known the result may, with proper attention, be more satisfactory.

No. 862 applies to this observation.

IV. BY AN OCCULTATION.

870. The moon in her perpetual revolution round the earth necessarily passes over every star or other body in her path at certain periods. The disappearance of a star or planet, called the *immersion*, and the reappearance from behind the body of the moon, called the *emersion*, being instantaneous, the phenomenon affords the means of determining the longitude at all places where it is visible.

At the instant of occultation the apparent R.A. of the moon's limb is the same as the R.A. of the star; the effect of the parallax of the moon being removed by computation, the true R.A. is deduced, and the G.M.T. thence found.

871. This observation affords, in favourable cases, the most decisive results, because it is both instantaneous and altogether independent of instrumental adjustments. On board ship the motion prevents the telescope, which is almost always necessary, from being kept steadily directed to the moon, and in consequence the method has been very rarely practised at sea. The precise instant of the phenomenon is, however, not necessary in all cases; it is enough that the observer is certain that at one instant he sees the star, and that at another he does not see it; because the whole resulting error in the time of observation in this case, and therefore in the longitude itself, cannot exceed the time elapsed between two sights of the moon.

872. The M.T. at Greenwich, at which the moon and the star to be occulted are in conjunction in R.A., is set down in the Nautical Almanac, as also the parallels between which the phenomenon is visible.

As it would require a distinct calculation to learn beforehand approximately the time at which the phenomenon will take place, the observer may content himself with finding, from the long. by acc., the time at place of the conjunction; he must then, at an early opportunity, single out the star, and watch the progress of the moon towards it. In general, when the star is to the *eastward* of the observer at the time of conjunction, the phenomenon occurs *before* that time; when to the *westward*, it occurs afterwards.

1. *Occultation of a Star.*

873. *The Observation.* Note the instant of immersion or emersion as nearly as possible.

874. *The Computation.* (1.) Find the Green. Date, and reduce to it the Sid. Time at mean noon, the moon's declination, hor. par., and semid.; reduce the hor. par. by Table 41.

(2.) Find the geocentric latitude by subtracting from the lat. the reduction of lat., Table 52. From the time at place find the star's hour-angle, No. 611.

(3.) For arc A. To the prop. log. of the reduced hor. par. add the log. cosec. of the geocentric lat. and the log. sec. of the star's decl.: the sum is the prop. log. of arc A.

For arc B. To the prop. log. of the red. hor. par. add the log. sec. of the geoc. lat., the log. cosec. of the star's decl., and the log. sec. of the hour-angle: the sum is the prop. log. of arc B.

For arc C. Add together the prop. log. of the red. hor. par., the log. sec. of the geoc. lat., and the log. cosec. of the hour-angle; double the sum, add to it the const. 1.582, and the log. cot. of the star's decl.: the sum is the prop. log. of arc C.

(4.) When the lat. and decl. are of the *same* name, *add* A to the star's decl.; when of *contrary* names, *subtract* it.

When the star's hour-angle is *less* than 6^h, *subtract* B from the star's decl.; when *greater* than 6^h, *add* it

Subtract C from A.

Call the result the prepared declination.

(5.) For Part I. of the μ 's Parallax in R. A. Take the diff. between the moon's decl. and the prepared decl.; under this diff. put the semid.: take the diff. and sum. Add together the log. cos. of the prepared decl., the const. 1.1761, half the prop. logs. of the diff. and sum: the sum is the prop. log. of Part I.

For Part II. Add together the log. cos. of the prepared decl., the const. 1.1761, and the sum of the 3 logs. used in arc C: the sum is the prop. log. of Part II.

When the moon is on or near the meridian, this Part disappears.

(6.) Apply Parts I. and II. to the star's R. A., thus:—

Part I. In an *immersion*, *subtract*; in an *emersion*, *add*.

Part II. When the μ is to the E. of the Mer., *subtract*; when W., *add*. The result is the moon's R. A.

(7.) Find the G.M.T., as directed, No. 867 (6.)

Ex. Dec. 9th, 1823, lat. 9° 40' S., long. by acc. 29° 51' W., at 7^h 19^m 57^s M.T., observed the immersion of α Aquarii,* W. of the meridian: required the longitude.

Gr. Date, 9 th	9 ^h 19 ^m 23 ^s	* Decl.	5° 7' 43".6 S.	Red. Eq. H. P.	54° 38' 07"
Red. S.T. at m. n.	17 11 13.7) Red. Decl.	5 16 12.6	Red. H. P.	54 38 04
M.T.	7 19 57			Semid.	14 53 4
	24 31 10.7			Lat.	9° 40'
Star's R.A.	22 28 39			(Tab. 52) Cor.	— 3 41
Hour-angle	2 2 31.7				9 36 19
Arc A.		Arc B:		Arc C.	
H.P. 54° 38' p. log.	0.5178	0.5178	0.5178
Geoc. Lat. cosec.	0.7777	sec.	0.0061	0.0061
* Decl. sec.	0.0017	cosec.	1.0487	Hour-angle cosec.	0.2928
P. log.	1.2972	Hour-angle sec.	0.0653		0.8167
A, + 9' 4".8		P. log.	1.6379	0.8167 \times 2 =	1.6334
B & C, — 4 8".8		B, — 4' 8".5		Const.	1.5820
+ 4 56".0		(Hour-angle less than 6 ^h		* Decl. cot.	1.0469
(Decl. S. lat. S. add.)		subtract.)		C, — 0".3 p. log.	4.2623

* This occultation, kindly furnished me by the Hon. Capt. F. De Ros, R.N., is given as having been observed by him, at sea, in H.M. frigate *Creole*.

Part I.				Part II			
* Decl.	5° 7' 43".6			Cos. of Prep. Decl.		9°9982	
Prep. Decl.	5 12 39 .6	cos.	9°9982	Const.		1°1761	
> Decl.	5 16 22 .6	const.	1°1761	Sum of 3 logs. Arc C.		0°8167	
	3 43			Pt. II.	+ 1° 50' 2	p. log.	1°9910
Semid.	14 53 .4			Pt. I.	— 0 57 .9		
Diff.	11 10 .4	½ pro. log.	0°6035		+ 52 .3		
Sum.	18 36 .4	½ pro. log.	0°4928	* R.A.	22 28 39		
	— 0 57 .9	pro. log.	2°2706	> R.A.	22 29 31 .3		4772
(Subtract, being immer.)				At 9 ^h	22 28 55 .7	0' 35".6	2 4820
				At 10 ^h	22 30 45 .1	1 49 .4	8°0060
					0 19 30 .3	p. log.	9657
					9		
				G.M.T.	9 19 30 .3		
				Ship M.T.	7 19 57		
				Long. in time	1 59 33 .3	or 29° 53' 19" W.	

Ex. 2. Jan. 7th, 1836, Bedford, lat. 52° 8' 28" N., long. acc. 1° W., at 10^h 45^m 53^s 2 M.T. observed the immersion of ι Leonis, E. of the meridian: required the Longitude.

Gr. Date 10^h 47^m, Red. S.T. 19^h 6^m 8^s 5, star's R.A. 10^h 23^m 26^s 4, decl. 14° 58' 38" 8 N., > red. decl. 15° 49' 40" N., H.P. 55' 54" 9, Semid. 15' 16" 1, geocen. lat. 51° 57' 19".

Arc A. 42° 33', E. 3° 21" 5, C. 2° 3'. Prep. decl. 15° 37' 48" 0. Part I. 39° 9, Pt. II. 2° 12' 6. > R.A. 10^h 20^m 33^s 9. At 10^h, 10^h 18^m 55^s 5; at 11^h, 10^h 20^m 58^s 5. G.M.T. 10^h 48^m 0^s. By corr. of Part I. 10^h 47^m 45^s.

2. Occultation of a Planet.

875. *The Observation.* The planet having sensible semidiameter, the phenomenon does not take place instantaneously. Note the instant of final disappearance, or the instant of reappearance.

876. *The Computation.* Subtract the planet's horiz. parallax from the reduced horiz. parallax of the moon. Also subtract its semidiameter from the moon's semidiameter. In other respects proceed as for a star.

877. *Degree of Dependence.* A small error of Gr. Date will not sensibly affect the moon's parallax or semidiameter, and the declination is the only element liable to sensible error; Part I., therefore, is alone affected.

To find the error in the long. in time, caused by 1^m error of Gr. Date. Find the change of decl. in 1^m, add it to the diff. of declin., and recompute Part I.: the diff. between the result and Part I., as computed before, is the diff. or error of R.A. The error of long. in time will be, on the average, 30 times greater.*

If the star pass very near the moon's upper or lower limb, the observation is not good.

The inequality of the moon's surface, and an imperfect estimation of the figure of the earth, may cause small inaccuracies.

The cases least liable to error on the several accounts enumerated are those which occur when the moon is near the meridian, and in which the central zone of the moon passes over the star. The emersion from the dark limb is the case most distinctly marked.

No. 862 applies to this observation.

* Hence, to obtain the long. in time true to 1° or 15", the parallax in R.A. must be true to 0° 003. This remark shews the difficulty of obtaining extreme precision from any single observation.

V. BY ECLIPSES OF JUPITER'S SATELLITES.

878. The eclipse or disappearance of a satellite in the shadow of the planet, called the *Immersion*, or the reappearance after eclipse, called *Emersion*, being a phenomenon which takes place at the same absolute point of time wherever the spectator may be placed, affords a ready method of finding the longitude.

The diagrams of the positions of the planet and its satellites, as seen in N. lat., and other necessary information, are given in the *Nautical Almanac*. The figures must be reversed in S. lat. It will be convenient for the observer to bear in mind, that when Jupiter comes to the meridian before midnight, the whole eclipse (both immersion and emersion) takes place on the E. side of the planet; when after midnight, on the W. side. In an inverting telescope this will appear to be reversed.

879. *The Observation.* The telescope should have a magnifying power of not less than 40, and the observer should be ready some minutes before the time of observation, estimated by applying the long. by acc. to the time in the *Nautical Almanac*.

The sun should not be less than 8° below the horizon, nor Jupiter less than 8° above it, for the phenomenon to be distinctly visible.

880. *The Computation.* The difference between the M. T. at place, found by observation, and that at Greenwich, is the long.

Ex. Oct. 6th, 1822, near Igloodik, lat. $69^{\circ} 21'$ N., immersion of the 1st satellite, $10^h 29^m 33$, M. T. The M. T. at Gr., in the *Nautical Almanac*, is $15^h 56^m 0^s$; the diff., $5^h 26^m 27^s$, long. W.

881. *Degree of Dependence.* This method, though easy and convenient, is not very accurate; the eclipse is not instantaneous; and the clearness of the air, and the power employed, affect considerably the time of the phenomenon. Observers have been found to differ 40^s or 50^s in the same eclipse.

The observation may be considered complete only when the immersion and emersion of the same satellite are observed on the same evening, and as nearly as possible under the same circumstances. Thus, if the satellite disappear a little sooner than if the air had been clearer, it will emerge a little later from the same cause, and the mean of the two results may be near the truth.

The first satellite is preferable to the others on account of the greater rapidity of its motion.

CHAPTER VIII.

FINDING THE VARIATION OF THE COMPASS.

I. BY THE AMPLITUDE. II. BY THE AZIMUTH. III. BY ASTRONOMICAL BEARINGS. IV. BY TERRESTRIAL BEARINGS.

882. THE Variation is found by comparing the bearing of the sun or other celestial body, as shewn by the compass, with the true bearing as found by calculation. See No. 907.

883. When the time is known, the body may be observed, in the simplest cases, at its passage of the meridian, at which time it bears due N. or S., or at its passage of the prime vertical, when it bears due E. or W. In other cases, the true azimuth may be found by calculation.

When the time is not given the azimuth may be determined by observation of the altitude. When the altitude is nothing, or the body is on the horizon, as at rising or setting, it is usual to refer the bearing to the prime vertical, the angular distance from which (or the complement of the azimuth) is called the *amplitude*. The azimuth may also sometimes be determined from the observed difference of altitude in a measured interval of time.

The following rules are arranged more particularly for observations of the sun; but, after the explanations and precepts already given, no difficulty will occur in adapting them, when necessary, to observations of other celestial bodies.

I. BY THE AMPLITUDE.

884. This method, which is particularly convenient, is available twice a-day in fine weather, and at all seasons of the year.

885. *The Observation.** At sunrise, when the upper limb appears on the horizon, observe its bearing, and continue to take bearings of the centre, bisecting the sun's disc by keeping the up-

* The usual instructions for taking an amplitude direct the sun to be observed when his lower limb is half way between the centre and the horizon, at which time he is really on the horizon, No. 433. But as it is not easy to seize the bearing at the required instant, and still less so to observe several bearings equally distributed on both sides of the proper position, which is essential to a correct result, the sun is commonly observed a whole diameter too low. The observation as recommended above is more convenient in practice, and the error arising from not observing the sun at the instant to which the true amplitude corresponds (No. 446 (1)), is removed by the correction.

right wire on the upper limb, until the lower limb appears. Read off each bearing. At sunset, when the lower limb touches the horizon, proceed in like manner, until the upper limb disappears. See No. 221.

The mean of the readings, reckoning from the E. or W. point, is the *observed amplitude*.

886. *The Computation, by Inspection* (1.) Enter Table 59 with the Lat. and Declin., take out the amplitude, and mark it of the same name as the Declin.

(2.) Take from Table 59 A the correction. If this does not amount to nearly 1° , it may in general be omitted.

At *Rising*. In N. lat. apply the corr. to the *right* of the observed amplitude. In S. lat. apply it to the *left*.

At *Setting*. In N. lat. apply the corr. to the *left* of the observed amplitude. In S. lat. apply it to the *right*.

(3.) When the observed and true amplitudes are both N. or both S., their *difference* is the Variation. If one is N. and the other S., their *sum* is the Variation.

Then, the observer being in the centre of the compass, when the *observed* amplitude is to the *left* of the true, the Variation is East; when to the *right*, it is West.

Ex. 1. June 10th, lat. 17° N., long. 25° W., observed sun's amplitude at setting, W. 40° N.: required the Variation.

Lat. 17° , Decl. 23° , Amp. W. 24° N.
Obs. W. 40° N.
VAR. 16° W.

Ex. 2. June 10th, lat. $36^\circ 40'$ S., long. 17° W., obtained sun's amplitude at setting, W. $12^\circ 3'$ N.: required the Variation.

Lat. $36^\circ 7'$, Decl. $23^\circ 0'$, Amp. W. $29^\circ 2'$ N.
37° and 23° , Corr. $0^\circ 7'$ } W. $13^\circ 0'$ N.
Obs. Amp. W. $12^\circ 3'$ N. }
VAR. $16^\circ 2'$ E.

Ex. 3. May 28th, lat. 47° N., long. 18° W., observed the sun's amplitude at rising, E. 10° N.

Lat. 47° , Decl. $21\frac{1}{2}^\circ$, Amp. E. $32^\circ 5'$ N.
50° and 22° , Corr. $0^\circ 9'$ } E. $9^\circ 1'$ N.
Obs. Amp. E. $10^\circ 0'$ N. }
VAR. $23^\circ 4'$ W.

Ex. 4. Sept. 25th, lat. 7° N., long. 151° E., observed the sun's amplitude at rising, E. 4° N.: required the Variation.

Lat. 7° , Decl. 1° , Amp. E. 1° S.
Obs. Amp. E. 4° N.
VAR. 5° E.

The Corr. here is 0.

The correction in Table 59 A is the same for a star or a planet as for the sun, and is applied in the same way. When the moon is employed, the correction, which, in the case of the sun or a star, involves the sum of the dip and horizontal refraction, is the excess of her horizontal parallax over this sum. As the moon's hor. par. is 1° , and the refraction $\frac{1}{4}^\circ$, in round numbers, this excess is about $\frac{3}{4}^\circ$, which is nearly the quantity employed in Table 59 A. This correction, therefore, serves for the moon, but it must be applied the *contrary* way to that directed for the sun.

887. *The Computation, Accurately.*

(1.) Find the Greenwich Date and reduce the declination to it.

(2.) To the log. sec. of the lat. add the log. sine of the declin.: the sum is the log. sine of the amplitude. Apply the correction as above.

888. *Degree of Dependence.* In low latitudes the amplitude is susceptible of much precision; in high latitudes refraction renders the result less certain. The relative temperature of the sea and the air produces no effect on the observed amplitude.

II. BY THE AZIMUTH.

1. *By Azimuth on the Meridian.*

890. *The Observation.* When the sun approaches the meridian observe the azimuth, and continue observing till the same time after noon. The mean of the readings is the observed azimuth.

When the sun is observed to the southward, if the observed bearing is to the E. of S., the variation is E.; if to the W., it is W. When he is observed to the North, the contrary in each case.

2. *By Azimuth from the Short Double Altitude.*

891. The true azimuth is obtained from the observation of the short double altitude, p. 256, without regard to the apparent time.

Case I. Observations on the *same* side of the meridian, No. 729.

892. *The Observation.* Observe the sun's azimuth during the interval between observing the alts., so as to obtain it at the middle of the interval. See No. 221.

893. *The Computation.* Having corrected the alts. and taken their difference, No. 729 (1), add together the log. sine of the diff. of alts., the log. cosec. of the interval,* and the log. sec. of the lat.: the sum is the log. sine of the azimuth at the middle time from noon, nearly.

Ex. (Ex. 1, p. 256.) Lat. $34^{\circ} 40'$ S., diff. of alts. $59' 1''$, interval $20^m 12^s$.

D. Alt.	$0^{\circ} 59' 1''$	sin.	8.2153
Int.	$20^m 12^s$	cosec.	1.0554
Lat.	$34^{\circ} 40'$	sec.	0.0849
AZIMUTH $13^{\circ} \frac{1}{2}$		sin.	9.3756

This azimuth compared with that observed would afford the variation.

* When it is intended to find the Variation by this method at the same time as the Latitude, it will be convenient to take the sum of these three logs. first. The five logs. employed in No. 729 will thus afford two distinct results.

894. *Degrees of Dependence.* By adding to the result the diff. for 30' in the sine of the D. alt., the effect on the azimuth of $\frac{1}{2}$ in the diff. alts. is seen, and the effect of an error, or small variation of the D. alts. estimated. See also No. 679.

Case II. Observations on *different* sides of the meridian, No. 731.

895. *The Observation.* Observe the sun's azimuth when at the alt. nearest noon. See No. 221.

896. *The Computation.* Having found the time from noon of the greater alt., to the log. sine of this time add the log. cos. of the declin., and the log. sec. of the greater alt.; the sum is the log. sine of the azimuth at the time of observing the greater alt.

Ex. (Ex. 1, p. 259.) Time from noon, 11^m 59', decl. $5\frac{1}{2}^{\circ}$, greater alt. $49^{\circ} 41'$.

T. from noon	11 ^m 59'	sin. 8.718
Decl.	$5\frac{1}{2}^{\circ}$	cos. 9.998
Great alt.	$49^{\circ} 41'$	sec. 0.189
AZIMUTH	$4\frac{1}{2}^{\circ}$	sin. 8.905

3. By Azimuth from Equal Altitudes.

897. The true azimuth may be obtained directly from the observation of equal altitudes at sea, for time, No. 798. The azimuth, being computed as directed in No. 801, and compared with that observed at one or both of the times of equal altitudes, determines the variation. The altitude is required with more precision than for finding the time by the method, No. 798.

This method is, however, not always eligible, because in low latitudes, where the observation of equal altitudes is favourable for the determination of time, the altitudes near noon are great, and therefore unfavourable for the observation of the azimuth. See No. 889.

4. By Azimuth on the Prime Vertical.

898. *The Observation.* Having found by Table 29 either the app. time or the altitude at the instant of the passage of the prime vertical, begin to observe a little before that time, and continue observing till the same time afterwards.

The mean of the readings, when it is not accurately E. or W., is the variation.

A.M. If the sun bear to the northward of E., the variation is E.; if to the southward, it is W.

P.M. If the sun bear to the northward of W., the variation is W.; if to the southward, it is E.

899. As a celestial body, when on the prime vertical, changes its azimuth more slowly than at any other time, an error in the apparent time will be of little consequence, and the method will be found one of the most convenient in practice in high latitudes during the six months that include the summer.

5. *By Azimuth deduced from an Altitude.*

900. *The Observation.* Take bearings of the sun's centre, noting the time of each reading. Take an alt. as soon as convenient before and after the bearings, noting the times.

901. *The Computation.* (1.) Having found the mean of the azimuths and of the corresponding times, reduce the alts. to the mean of the times, No. 660, reduce the decl., correct the alt., and find the azimuth, No. 678 or 674.

Ex. Feb. 19th, 1828, P.M., Paia Bay, Naples, lat. $40^{\circ} 50' N.$, long. $14^{\circ} 3' E.$, Mr. Fisher observed the mean of seven azimuths of the sun by Kater's compass, N. $223^{\circ} 24' E.$ (or S. $43^{\circ} 24' W.$) Sun's true alt. $33^{\circ} 34'$; sun's reduced decl. $11^{\circ} 14' S.$

By Expl. Tab. 5.				Dist. 100 and D. Lat. $88^{\circ} 5'$ give	
lat. 41° , alt. $33\frac{1}{2}^{\circ}$ M	158.9	N 57.5		course or Az. S.	$28^{\circ} W.$
Decl. $11\frac{1}{4}^{\circ}$, dist. 159		Dep. $31^{\circ} 0'$ (lesser)		Ditto observed	$43\frac{1}{2}$
	Sum	88.5			Var. $15\frac{1}{2} W.$

6. *By Azimuth deduced from the Time.*

902. The observation is already described in No. 900.

(1.) Find the Green. Date, to which reduce the declination and the elements employed in finding the hour-angle.

(2.) Compute the azimuth, No. 675.*

Ex. 1. June 23rd, 1829, P.M. at Constantinople, lat. $41^{\circ} 1' N.$, long. $28^{\circ} 59' E.$; the mean of seven times by chron. $4^h 43^m 15^s$, and of seven azimuths of the sun, observed by Mr. Fisher with Kater's compass, between $286^{\circ} 30'$ and 288° , was N. $287^{\circ} 16' E.$, or N. $72^{\circ} 44' W.$

Reduced pol. dist. $66^{\circ} 33'$.

Time	$4^h 43^m 15^s$				
Chron. fast on A.T.	$3 \quad 32$				
Sun's Hour-angle	$4 \quad 39 \quad 43$	half $2^h 19^m 51^s$	cot. $0^{\circ} 15531$		$0^{\circ} 15531$
Pol. Dist.	$66^{\circ} 33'$				
Colat.	$48 \quad 59$				
	$114 \quad 92$	half $57^{\circ} 46'$	sec. $0^{\circ} 27297$	cosed.	$0^{\circ} 07269$
	$17 \quad 34$	$8 \quad 47$	cos. $9^{\circ} 99488$	sin.	$9^{\circ} 18383$
		$69^{\circ} 19'$	tan. $0^{\circ} 42316$	$14^{\circ} 28'$ tan.	$9^{\circ} 41183$
		$14 \quad 28$			
Azimuth	N $83 \quad 47$ W.				
Do. observed	N $72 \quad 44$ W.				
Var.	$11 \quad 3$ W.				

Ex. 2. Dec. 27th, 1831, Lisbon, lat. $38^{\circ} 42' N.$, long. $9^{\circ} 8' W.$, Mr. Fisher observed the mean of ten azimuths of the sun by Kater's compass (between 165° and $166^{\circ} 50'$) to be N. $166^{\circ} 7' E.$ The mean of the times by chron. (between $10^h 7^m 30^s$ and $10^h 15^m 45^s$) was $10^h 11^m 47^s$. Chron. fast on A.T. $42^m 18^s$; red. pol. dist. $113^{\circ} 22'$.

Computed Az. N. $143^{\circ} 44' E.$; Var. $22^{\circ} 23' W.$

* The work of finding the Azimuth is much lessened by the use of suitable tables. Burdwood and Davis's Azimuth tables and Star Azimuth tables extend from the equator to 60° latitude, and are published in a convenient form by J. D. Potter, 146 Minories, London, E. Such tables are indispensable for the navigation of iron ships. See also Lecky's "Wrinkles," for stars.

III. BY ASTRONOMICAL BEARINGS.

903. The true bearing of a point of land, or other terrestrial object, may be determined by means of the *difference of bearing* between it and the sun, or other celestial body; the true bearing of the latter being deduced by observation, or computed from the time.

The difference of bearing may be obtained directly by observing with the compass the bearings of both the sun and the object; or by the sextant, when the sun is on the horizon. But as the observation of two bearings at the same instant cannot always be conveniently made, the angular distance between the sun and the object is measured by a sextant or circle, and the bearing of the object alone observed. The difference of bearing is then deduced, by calculation, from the observed angular distance and the altitudes of the sun and the object.

The true azimuth of the object being thus obtained, the variation is deduced.

904. *The Observation.* Observe the sun's alt., then the angles between the object and the nearest and farthest limbs; lastly, observe the sun's alt., noting the times of each contact. Take the alt. of the object, at the point from which the sun's distance is measured.

When the variation is required at the same time, the bearing of the object must be obtained as nearly as possible at the time of the observation of the angular distance.

905. *The Computation.* (1.) Find the means of the times and angular distances, and reduce the sun's alt. to the mean of the times. Find the Green. Date, and reduce the sun's decl.; find his pol. dist., correct the obs. ang. dist., and the alt. of the object for index-error, when necessary.

Note For common purposes, when the observer is not much elevated and the alt. of the object does not exceed a few minutes, the sun's decl. may be corrected at sight, the dip, refraction, paral'ax, and the alt. of the object neglected, and the precepts (2) and (4) omitted.

(2.) Find the app. alt. of the sun's centre (by applying the ind.-corr. dip, and semid.), and thence the true alt. by subtracting the refr. or corr. of alt.

(3.) Find the sun's true azimuth. When the sun is not near the meridian, this is found by No. 674. When he is near the meridian it is better found from the time, No. 675. The lat. will be required more correctly as the sun is nearer the meridian, and less so as he is farther from it.

(4.) For the corr. of ang. dist. arising from the point observed not being exactly on the true horizon. Take the diff. between the obs. alt. of the object and the apparent dip, Table 80.

To the log. sine of the remainder add the log. sine of the sun's app. alt. and the log. cosec. of the ang. dist.: the sum is the log. sine of the correction of the ang. dist.

When the dip is *less* than the alt. of the object, *add* the corr. to the ang. dist.; when the dip is the *greater* of the two, *subtract* it.

(5.) For the diff. of azimuth. To the log. cos. of the corrected ang. dist. add the log. sec. of the sun's app. alt.; the sum is the log. cos. of the diff. of azim. between the sun and the object.

When the ang. dist. exceeds 90° , take the supplement of the arc found as the diff. of azim.

(6.) For the Variation. Apply the diff. of azim. to the sun's azim., according to the case, which will be best understood by drawing a figure: the result is the true azim. or bearing of the object.

The true bearing compared with that observed shews the variation.

Ex. Dec. 4th, 1819, at $7^h 30^m$ A.M., in Pernambuco Road, lat. $8^\circ 4' S.$, long. $34^\circ 52' W.$ M. Givry took the following alts. and angular dist., height of the eye 16 feet, ind.-corr. 0.— (*Mém. sur l'Emploi, &c.*)

Time by W. $7^h 25^m 40^s$	Alt. \odot $23^\circ 16'$	Ang. Dist. Circle. $190^\circ 30' 30''$	Object. S. $31^\circ 40' W.$
Mean $7^h 26^m 10^s$	$23^\circ 23'$	$190^\circ 30' 30''$	Alt. 0 10
	$23^\circ 19' 5''$	$95^\circ 15' 15''$	Corr. 0.
(1.)		(2.)	
Green. Date, 3d, $21^h 47^m$	Red. Decl. $22^\circ 10' 47'' S.$	Obs. Alt. $23^\circ 19' 8''$	
	Pol. Dist. 67 49	$-4'$	
		$+16.2$	$+12.2$
		App. Alt. $23^\circ 32' 0''$	
		-2	
		True Alt. $23^\circ 30'$	

(3.) Sun's Azimuth.

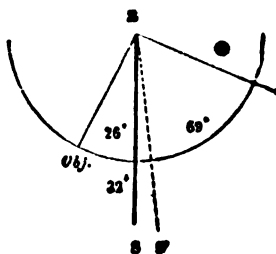
Pol. Dist. $67^\circ 49'$	
Lat. 8 4	sec. 0.00432
Alt. $23^\circ 30'$	sec. 0.03760
$99^\circ 23'$	
$49^\circ 41'$	cos. 9.81091
$18^\circ 8'$	cos. 9.97788
$110^\circ 45'$	sin. sq. 9.83071
or S. $69^\circ 15' E.$	

(4.) Corr. of Ang. Dist.

(Alt.) $10' - (\text{dip}) 4' = 6'$	sine 7.242
\odot Alt. $23^\circ 30'$	sine 9.601
Dist. 95 15	cosec. 0.002
$+ 8$	sine 6.845
Corr. Ang. Dist. 95 17	

(5 & 6.) Computation of Diff. of Azim.

Ang. Dist. $95^\circ 17'$	cos. 8.9642
\odot Alt. 23 30	sec. 0.0376
Suppl. $84^\circ 14'$	cos. 9.0018
	$95^\circ 46'$
\odot Az. S $69^\circ 15' E.$	
Obj. Az. S $26^\circ 31' W.$	
Observed S $31^\circ 40' W.$	
VAR. $5^\circ 11' W.$	



IV. BY TERRESTRIAL BEARINGS.

906. The true bearing or azimuth of a mountain, at a considerable distance, is determined from its geographical position and that of the observer. As the true azimuth and the course on the great circle are the same thing, the problem is that in No. 339 (1), p. 133. But as mountains are rarely seen much beyond a hundred miles, it is near enough to proceed thus:—

Find the D. Lat. and D. Long. between the places in minutes of arc. Turn the D. Long. into Dep., No. 318 or 319. Find the Course, No. 280 (1). This is the approximate azimuth.

With the mid. lat. as a course, and the D. Long. as dist., find the Dep.; this is a number of minutes, one-half of which is to be subtracted from the approx. azim.; the remainder is the true azimuth, very nearly.

Ex. Lat. $60^{\circ} 6' N.$, long. $142^{\circ} 50' W.$, find the true azim. of Mt. St. Elias in lat. $60^{\circ} 18'$, long. $140^{\circ} 52'$.

D. Lat. 12 and D. Long. 118 give Dep. $58' 6''$, and Course $78^{\circ} 26'$. Then 60° and 118 give Dep. $108' 2''$; and $51'$ subtracted from $78^{\circ} 26'$ gives the Azim. N. $77^{\circ} 35' E.$

In low latitudes, and in all cases when the object is near N. or S., the correction may be neglected. (For more precision, see No. 395, p. 161.)

907. The term Variation, as defined in No. 882, and used in this chapter, is the difference between the true bearing of any object and its bearing by a compass. From what has been said in Chapter II., this quantity must differ from the correct variation by the instrumental error of the compass, by the local effects of the land, and, further, on board ship, by the deviation.

There may be instrumental errors in a compass, which cannot be detected unless the correct magnetic bearing of some object is known. For this reason it is desirable, when there is any reason to suspect the accuracy of the standard compass, that advantage should be taken of being in a port where the exact variation is known, to examine the compass according to the process described in No. 224. Errors in observed bearing, arising from the sight-vane not being vertical, or from the reflector being out of place, may be avoided by using low azimuth's amplitudes, or nearly horizontal bearings of terrestrial objects. Errors arising from the centre of the card not being in the same vertical plane as the line of sight, may be avoided by taking bearings of several objects distributed round the horizon. The true bearing of one object may be determined by process III. or IV., the others by horizontal angles therefrom.

The effects of such local disturbances as are mentioned in No. 222 may generally be eliminated, either on land or at sea, by observing in several positions, with the view of getting on oppo-

site sides of the disturbing cause, and taking the mean of the results as the correct variation.

When an observation is made at sea with a compass which is instrumentally correct, and is free from local disturbance of the land or ground, the difference between a true bearing and a compass bearing, commonly called the *Total Error*, enables the navigator to shape a correct true course. This is in general all that is actually required for navigation. But such an observation would not determine the variation, unless the deviation is exactly known. A good value of the deviation may be obtained by interpolation, if the ship has been swung a short time previously, and again a short time after. Allowing the same on the total error will give the variation.

When the compass is well placed, the mean of the total errors on two opposite cardinal points is a good value of the variation. A still better value may be obtained by taking the mean of the total errors on the four cardinal points.

To obtain an accurate compass bearing, it is necessary that the ship's head should be steadied as directed in No. 248. When a ship's head is moving to port or starboard, the compass card is obviously liable to be dragged round in the same direction as the head is moving, by the friction on the pivot. On the other hand, in iron ships it has been found, that when the head is moving to the right, the compass-needle stands a little to the left of its due position, and *vice versa*. The last mentioned effect of the ship's motion in azimuth is especially noticeable when the ship's head is near the north or south points. It is due, possibly, to the transient magnetism not instantly adapting itself to the position of the ship, as she moves round in azimuth. An exact bearing can be obtained by taking the mean of two, taken with the ship's head moving in opposite directions; also an accurate deviation-table may be quickly obtained by turning a ship round to port and to starboard under steam, making use of the sun's azimuth, and taking the mean on the four cardinal points as the variation, where it is not otherwise known.

Reduction of the True Course to the Course by Compass.

908. When the true course to be steered is determined, it must be reduced to the course by compass. The variation of the compass is to be applied (No. 221); the result is the *correct magnetic course*. See p. 159.

When the total error (No. 907) of the compass is known, it is to be applied to the true course, otherwise the deviation (No. 227) must be applied to the *correct magnetic course*; the result is the *course by compass*.

CHAPTER IX.

THE TIDES.

I. PHENOMENA OF THE TIDES. II. RULES FOR FINDING THE TIME OF HIGH WATER. III. TIDE-OBSERVATIONS.

IN this chapter we shall attempt merely a general enumeration of the principal phenomena of the tides, with such other matters as are of direct practical importance.*

I. PHENOMENA OF THE TIDES.

909. The connexion observed in all ages, and, with particular exceptions, in all places, between the succession of high waters and the moon's meridian passage, has established the belief that the moon is the cause of the tides. The principle of gravitation,† on which the motions of the earth and the celestial bodies are calculated, and their figures explained, has confirmed, and at the same time corrected, this belief, by shewing that sensible effects must be produced not only by the moon, but also by the sun, though, from her greater nearness, the moon has by far the greater influence; and the general result would, naturally, until the observations were analysed, be attributed exclusively to her.

910. The attraction of the moon acting most strongly on those parts of the ocean which are nearest to her, that is, over which she is vertical, tends to draw these parts towards her, while their place is supplied by the water at the sides of the globe. And since the central parts are likewise more affected in the same action than the surface at the opposite or farthest side, the figure of the earth becomes elongated in the direction of a line drawn towards the moon; that is, the water is accumulated at the point exactly under

* The reader may refer, for additional information, to various papers, by Sir John Lubbock and the Rev. Dr. Whewell, in the *Philosophical Transactions*, &c., 1833, particularly to "An Essay towards a Map of Cotidal Lines," followed by other dissertations by Dr. Whewell; and to "The Tides," by Professor George Howard Darwin (John Murray, Albemarle Street).

† This principle is that there subsists amongst all particles of matter a mutual attraction whose intensity is inversely as the square of the distance.

the moon, and at another point distant from the former 180° in latitude and longitude. The moon, in her progress to the westward, causes thus, at each meridian in succession, a high water, not by drawing after her the water first raised, but by raising continually that under her at the time.

The opposite high water, or, as it is called, the *inferior* tide, would, if the moon's action was uninterrupted, follow the other, or *superior* tide, after the interval of half a lunar day, or $12^h 24^m$ on the average.

Again, the sun, acting in the same manner, though with less force than the moon (in consequence of his distance more than counterbalancing his greater magnitude), produces two tides, which would follow each other, if uninterrupted, after an interval of half a solar day, or 12 hours.

911. But, instead of four separate tides produced by the independent actions of both bodies on the mass of waters in their original form, the effect produced is the same as if, after one of the bodies, as the moon for example, has given a form to the waters, the sun alters that form, the two separate actions thus producing a joint result. Hence the place at which it is high water is that at which the *sum* of the heights of the tides produced by the two bodies is greater than any where else.

912. When the sun and moon are on the meridian together, their actions concur, and the tide is higher than at any other time. The same holds when they are in opposition. These highest tides are called *spring-tides*, and occur after new and full moon. Again, when the sun and moon are 90° apart, their actions tend to neutralise each other; and the *neap-tides*, which occur after the first and third quarters of the moon, are the smallest of all. (See No. 919.)

913. Since the sun and moon act with greater force as they are nearer, the effect of each body in raising the tide is greater as its parallax is greater (No. 436). The highest spring-tides would occur, therefore, in January, about the time of the month when the moon's hor. par. is greatest. But the effect of both bodies is greater, generally speaking, as their alts. are greater, since when vertical the effect is greatest. This period, therefore, depends on circumstances.

914. If the actions of the sun and moon were, as we have hitherto supposed, uninterrupted by obstacles or forces of any other kinds, the tides would be regular, and their calculation certain. But from the unequal depth of the ocean, and the barriers presented by continents which stand across the natural progress of the tides, their motion is interrupted, and the *tide-wave* (as the accumulation of waters is called), abandoned by the forces which originated it, becomes subjected to the mechanical action proper to waves in general.

915. It is necessary to distinguish between the motion of a wave and that of a current. A wave is not an absolute transfer of the body of moving water in the direction of the motion of the waves, but is a motion perpendicular to the surface, or up and down. The

motion of waves is represented in the fluttering of a flag and the shaking of a sail. It is easy to see that this kind of motion is compatible with immense velocity, without any appreciable current in the water itself; thus the tide-wave appears to pass from the Cape of Good Hope to Cape Blanco in twelve hours.

916. The motion of waves is quicker as the water is deeper. Also, the largest waves are the swiftest; a fact illustrated by the superior velocity of a heavy sea over that of the rippling of a pool. When the water shoals, the wave is retarded and becomes steeper on the advancing side, as is seen in the approach of waves to a shelving shore, and in the bores of rivers. The velocity of waves is also considered to be greater as their length (or distance from hollow to hollow) is greater; thus the tide-wave, though inferior in height to the waves of an agitated sea, yet travels with prodigiously greater velocity. Waves of different size and velocity merge into one another, as is known to those who have endeavoured to follow with the eye the waves of the sea. Lastly, when the waves meet with obstacles, such as sand-banks or reefs, the directions of their motions, as well as their figures, are changed. Several of the anomalies which the tides present are attributed to these and like circumstances.*

917. The current which accompanies the tide, and changes its direction with the ebb and flow, is the effect of the alteration of the level of the water during the passage of the tide-wave. Also, when a body of water in a channel has been set in motion, the motion does not immediately cease with the cause that produced it. Hence the *tide-current* does not necessarily, and in all cases, change with the tide; and thus, under certain circumstances, the current of the ebb continues to run for some hours after the flood-tide has made.

It is considered probable that many of the anomalies in recorded times of tide have arisen from thus confounding the time of high or low water with the time of slack water.

Admiral Beechey, who bestowed much attention upon the complicated movements of the tides on our Western coasts, states that though each point of the coast in the Irish Channel has its proper time of high water, yet the turn of the stream takes place simultaneously to all, namely, about the time of high water at Morecombe Bay. This time is nearly that of Liverpool; accordingly, in order to know whether the stream is setting into the Irish Channel or out of it, it is necessary merely to find whether the tide is rising or falling at this place. Thus while the tide-wave, in coming in, is making it high water at the different places succeeding each other in its progress, the *stream* is, nevertheless, running out.†

* Among the most curious of these effects are those called *interferences*, whereby two distinct sets of waves may, in their combination, produce apparent rest. See *Phil. Trans.* 1832, p. 154. On this principle are explained, also, tides which occur at irregular intervals.

† A Report on Observations made on the Tides in the Irish Sea, &c., by Capt. F. W. Beechey, R.N., *Phil. Trans.* 1848; see also *Naut. Mag.* 1849, p. 70.

918. The *height* of the tide is the difference between the level of high water and that of low water.*

The height of the tide in the open ocean is supposed to be very small; and the great heights observed on some shores are evidently due to the shoaling of the water and the narrowing of the channel.

The tides are insensible or very small in inland seas; as also in high latitudes, except from local causes.†

919. It is found, in general, that the tide is not due to the moon's transit immediately preceding, but to a transit which has occurred some time before. The time thus elapsed between the transit at which the tide originated and the appearance of the tide itself is called the *retard*, or *age of the tide*.

Thus the tide on the western coasts of Spain and France is a day and a half old; that at London is two days and a half old.

It appears certain that the age of the tide on the W. coast of Ireland is 2 days (p. 38), and on the S. W. coast $1^d 20^h$ (p. 110).‡

It would appear further that changes in the parallax and declinations of the sun and moon produce their several effects on the time and height of the tide after particular intervals.

It is thus constantly necessary to discriminate between a tide which may happen after any particular transit and the tide which really *corresponds* to that transit; thus, for example, if the moon passes the meridian at 4 P.M. to-day, and the high water occurs at 7 P.M., this tide will not in general be that which *corresponds* to the transit 3 hours before, but may have had its origin several transits back. The transit to which the tide really corresponds is found by examining the observations of the several preceding tides, the highest of which, being due to the united actions of the sun and moon, is known to correspond to the moon's transit at 12 o'clock, noon or midnight.

920. The *mean level* of the sea is the middle between the levels of high water and low water.

Though the heights of high water and those of low water may vary considerably, yet the mean level seems confined to very narrow limits. Thus, at Singapore, where the heights of two consecutive low waters differ sometimes six feet, the mean level varies only a few inches.—*Phil. Trans.* 1837.

Hence it follows that heights measured above the sea should be referred to the mean level as the standard or zero, instead of that of either low or high water.

It is not, however, to be supposed that the middle point between any two consecutive tides is the mean level. This will be the case

* The term *range* would be preferable to *height*, as it implies a distance between boundaries, as, for ex., the range of the barometer. The "height of the tide" is continually, in common discourse, used for the height of the water.

† Sir John Ross found a rise and fall of 8 feet in lat. 74° N.

‡ On the Law of the Tides of the Coasts of Ireland, by G. B. Airy, Esq., Astronomer Royal, *Phil. Trans.* 1845. This paper refers to a most extensive and complete series of observations made in 1842 under Gen. Colby, director of the Trigonometrical Survey chiefly for the purpose of referring the elevations observed to the level of the sea.

only when two tides in succession attain the same high-water level and the same low-water level, as at springs.

921. By the *Establishment of the Port* or *Tide-hour* has been commonly understood the apparent time of the first high water that takes place in the afternoon of the day of full or change. This Dr. Whewell has called the *Vulgar Establishment*.

922. The interval between the moon's transit and the high water next following is called a *lunitidal interval*.

The lunitidal interval varies from day to day during the fortnight between full and change.

923. The *correct establishment* is the lunitidal interval corresponding to the day on which the moon passes the meridian exactly at noon (with the sun) or at midnight. This is found by taking the mean of all the times of H. W. for a fortnight. The *Vulgar Estab.* may thus be an hour, or considerably more, in error when used as representing the H. W. on *any* day of the fortnight.

The tide caused by the united actions of the sun and moon, when each of these bodies is in one of the positions most favourable for raising the water, is identified by its superior height. And it is thus found (as observed in No. 919) that the interval by which the tide follows the moon on the day when the full or change occurs at 12 o'clock, or the lunitidal interval *corresponding* to that particular transit, is not the interval actually observed *on* that day.

The establishment of the port, and also the height of the tide, appear to be subject to change.

924. The difference between the lunitidal interval at each transit of the moon and the correct establishment is called (by Sir J. Lubbock), from the period of its recurrence, the *semi-menstrual inequality*.

This inequality is found to be different for different places; hence the time of high water at any place cannot, generally, be accurately deduced from that at any other place by merely applying the difference of time between the two establishments.

925. The tide is subject, in like manner, to a semi-menstrual inequality in the height. This inequality being, like that in the time, different for different places, the height of a tide at any one place cannot always be correctly inferred from the given height at any other.

926. It has been found that the morning and afternoon tides do not rise to the same height; the difference is called the *Diurnal Inequality*.

This irregularity is the consequence of the sun and moon not being always on the equator. Thus, suppose the moon in 20° N. declin.: then the summit of the superior tide is in 20° N. lat., and of the inferior tide in 20° S. lat., each alternate tide having thus its greatest elevation in the other hemisphere. The diurnal inequality is subject to steady rules, and may be predicted.

927. The maximum of the diurnal inequality *corresponds* to the moon's greatest declination, though it may not appear till after the

time of the greatest declination. In like manner, it disappears with the moon's declination, but not till some time after she has crossed the equator. For example, the age, as it may be termed, of this inequality is, at Liverpool, six days; at Singapore, a day and a half. A diurnal inequality appears in the times, as well as in the heights, of the morning and afternoon tides.

928. The *Diurnal Inequality* is a feature in tidal phenomena, which, being particularly small in British waters, has not received the attention it merits from the English sailor, for in the Indian seas,* and indeed in most other parts of the globe, this diurnal inequality is a regular change, considerable in amount, and almost universal in prevalence.

In consequence of the diurnal inequality, it sometimes happens that the day tides are higher than the night tides, or the reverse, for many weeks together. And hence it has sometimes been stated at such places, that the day tides are always the highest, or the reverse. But this is not the case. The rule of the diurnal inequality depending on the declination of the moon and sun, if the day tides are the highest at one time of the year, they are the lowest at another.

The diurnal inequality sometimes affects the time of high water as much as two hours, that of low water about forty minutes; at the same time a variation of twelve inches may be observed in the height of high water, and of thirty-six inches in that of low water. Such effects are far too great to be neglected, either in the prediction of tides or the reduction of soundings.

929. Strong winds affect the time and height of the tide, but chiefly the former, especially in rivers and narrow seas.†

The pressure of the atmosphere also affects the height of the tide, the water being in general higher as the barometer is lower.‡

930. Though high and low water may succeed each other regularly as to time, yet the water does not always rise and fall at the same rate. Thus, for ex., the water in some places falls faster during the first of the tide than afterwards.

Irregularities both in the duration of the tide and in the rate at which the water rises or falls, are, however, most conspicuous in rivers.§ At Limerick and New Ross, the fall of the water occupies a longer time than the rise; at most other stations the rise appears to occupy a little longer time than the fall. This last, however, appears less certain.—*Phil. Trans.*, 1845, "Law of Tides."

* See Tide Tables for the Indian Ports, by Captain S. G. Burrard, R.E., and Mr. E. Roberts, F.R.A.S., F.S.S., published yearly by the authority of the Secretary of State for India.

† Adm. Beechey acquainted me that he considered strong winds do not raise the water more than 2 feet, even in the Bristol Channel, where the range is above 40 feet.

‡ It has been established that a rise in the barometer of an inch is accompanied by a fall in the height of the water of 12 or 14 inches. This opposite motion of the water and the mercury due to the atmospheric pressure was established by Mr. Daussy in discussing the tide-observations made at Brest.

§ At Limerick, after low water, the water sometimes rises as much in ten minutes as it had previously dropped in two hours. Such irregularities cause considerable difficulty in ascertaining the true state of the case.

II RULES FOR FINDING THE TIME OF HIGH WATER.

931. The first of the two following rules, which is the old method of finding the time of high water by the moon's age, affords merely a rough estimate, as it may be in error nearly two hours. The second, which involves the semi-menstrual inequality, will be found a tolerable approximation on our own coasts, being generally within 15^m or 20^m ; but as each place has a different semi-menstrual inequality, the degree of accuracy which it may possess as applied to other parts of the world than those for which the table is constructed, cannot be pronounced.

Complete rules for computing the time and the height of the tide involve, also, corrections for parallax and declination, and require special tables for each port.*

932. Rule I. for a *rough estimate*. (1.) For the moon's age. To the epact of the year, Table 14, add the epact of the month, and the day of the month. The result, if less than $29^d 13^h$, is the moon's age at noon; if it exceed $29^d 13^h$, subtract $29^d 13^h$.

In leap-years, in January and February, deduct 1 day.

(2.) For the moon's meridian passage.† Multiply her age, to the nearest day, by 8, and point off one decimal: the result is the time of the merid. passage nearly.‡

(3.) For the time of high water. To the time of merid. pass. add the establishment of the port (or tide-hour).

(4.) If the sum be less than 12 hours, it is the time of high water P.M.; if it exceed 12 hours, it is the time of high water next morning; and, to obtain the time for P.M. on the present day, subtract $12^h 24^m$.

If the sum exceed 24 hours, it is the apparent time of high water P.M. the next day; for the time P.M. on the proposed day, subtract $24^h 48^m$.

Note.—This rule supposes that the tide always follows the moon by the same interval; but this interval, generally speaking, is different for each day of the fortnight. See No. 923.

* Such tables are given in the Tides published annually by the Hydrographic Office. The errors of the predicted times do not appear to exceed five or ten minutes, except in gales of wind, when the time of high water may be altered upwards of half an hour.

† This is often called *southing*; but as in south latitude the moon passes the meridian to the northward, this term is not adapted to general use.

‡ The moon's age thus found may be more than a day in error, but her merid. pass. will generally be less than an hour in error.

Ex. 1. Find the time of high water at Falmouth, Oct. 3d, 1891.

Epoch 1891	20 ^d 9 ^h
Do. Oct.	7 5
Days	3
	<u>30 14</u>
	-29 13
	1
	8
J's Mer. Pass.	08 = 0 ^h 48 ^m
Tide-hour	+4 57
TIME OF H.W.	5 45 P.M.

Ex. 2. Required the time of high water at Shields, March 31st, 1891.

Epoch 1891	20 ^d 9 ^h
Do. March	29 11
Days	31
	<u>80 20</u>
	-59 2
	21 18
	8
	<u>168 = 16^h 48^m</u>
Tide-hour	+3 21
	20 09
	<u>12 24</u>
TIME OF H.W.	7 45 P.M.

Ex. 3. Find the time of high water at Liverpool, March 10th, 1891.

Tide-hour 11^h 23^m

TIME OF H.W. 11^h 23^m P.M.

Ex. 4. March 30th, 1891, find the time of high water at Portsmouth.

Tide-hour 11^h 41^m

TIME OF H.W. 2^h 53^m P.M.

Ex. 5. June 2d, 1891, find the time of high water at Liverpool.

Tide-hour 11^h 23^m

TIME OF H.W. 7^h 15^m P.M.

933. Rule II. (1.) Take from the Nautical Almanac the M.T. of the moon's meridian passage, and correct it for the longitude by Table 28.

(2.) Take from Table 15 the semi-menstrual inequality corresponding to this time, and apply it to the reduced time of mer. pass. as directed in the table. To this result add the tide-hour, and the sum is the time of high water.

(3.) When this time exceeds 12 hours, it is the time of high water past midnight,—that is, A.M. the next day.

When, therefore, the P.M. tide preceding is required, it is necessary to employ the *inferior* transit of the moon.

Ex. 1. Aug. 6 h, 1891, find the time of high water at Shields. Long. 1° 25' W.; tide-hour 3^h 21^m.

J's tr. 6th	1 ^h 33 ^m	Inf. tr. 6th	1 ^h 5 ^m A.M.
Corr. for long.	0 0	Sem. ineq.	- 14
Sem. ineq.	-0 21		<u>51</u>
	1 12	Tide-hour	3 21
Tide-hour	3 21	TIME OF H.W.	4 12 A.M.
TIME OF H.W. 6th	4 33 P.M.		

Ex. 2. Aug. 29th, 1891, find the time of H.W. at Portsmouth.

Tide-hour 11^h 41^m. HIGH WATER 29th, 7^h 10^m A.M. and 7^h 54^m P.M. on 29th.

Ex. 3. March 11th, 1891, find the time of high water at Cherbourg.

Tide-hour 8^h 0^m. HIGH WATER 11th, 8^h 32^m A.M., 8^h 53^m P.M.

(4.) When the time of the moon's transit on the given day exceeds 12 hours, the transit occurs A.M. on the *next* day (civil

time). It is evident, therefore, that to obtain the times of high water on the same day, we must, in such cases, employ the transit of the preceding day.

Subtract 12^h from the time of transit, to enter the table of the semi-menstrual inequality.

To find the other tide, we must employ the inferior transit as already directed.

Ex. 4. April 8th, 1891, find the times of high water at Shields.

Trans. April 7th	$23^h 49^m$	For the A.M. tide preceding.	
Corr. for long.	0	Inferior trans. April 7th	$11^h 21^m$
Sem. ineq.	+ 2	Sem. ineq.	+ 8
Tide-hour	+ 3 21	Tide-hour	+ 3 21
TIME OF H.W. April 7th	$\frac{27}{3} 12$ P.M.	TIME OF H.W. April 7th	$\frac{14}{2} 50$ P.M.
or April 8th	3 12 P.M.	or April 8th	2 50 A.M.

Ex. 5. July 20th, 1891, find the times of high water at Tynemouth bar.
Tide-hour $3^h 20^m$. HIGH WATER July 20th, $2^h 4^m$ A.M., and $2^h 28^m$ P.M.

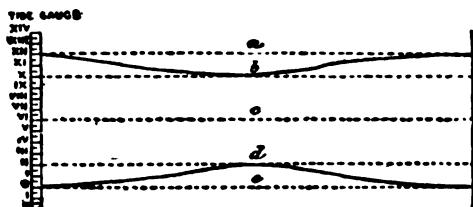
934. When the range of tide is considerable, and the depth not great, and it is required to identify the place of the ship by the soundings, or when about to enter a harbour in a vessel whose draught of water is nearly equal to the depth, it is necessary to find the height of the tide as exactly as circumstances permit. If the place is one of those of which particulars are given in the tide-tables published by the Hydrographic Office, the depth is found by the rules there given.* When such tables are not at hand, it may be found approximately by Table 16.

935. It is proper to remark that the age of the tide is necessary to the computation of its height. Thus, suppose it is H.W. at $2^h 30^m$ P.M. on Monday, the day of change. Now, if this H.W. is the tide *really corresponding* to the transit of the sun and moon together (No. 919), it will also be that which gives the spring range; the next range, therefore, will be less, and each range in succession will go on decreasing to the neap-tide. But if the age of the tide, in the supposed case, is 2 days, that is, if the highest tide does not follow till 2 days later, or till Wednesday afternoon, then the range on Monday will not be so high as on Wednesday; that is, the range, instead of *decreasing* continually to the neap-tide, will go on *increasing* for the next 2 days; after which it will begin to decrease until the neap-tide, which will take place 2 days after the 1st quarter, and not on the day of the 1st quarter.

* The soundings marked on the Admiralty Charts show the depth at Low Water ordinary springs; hence a correction has to be applied to the soundings obtained to compare it with these shown upon the chart to know the depth over a bar or in a harbour. See Table on p. 344.

TIDES.

The following Diagram is intended to explain the terms Spring Rise, Neap Rise, and Neap Range, as made use of in this work.



- a = Mean level of High Water Ordinary Springs.
 b = " " " " Neaps.
 c = Half Tide or Mean Level of the sea both at Springs and Neaps.
 d = Mean Level of Low Water Ordinary Neaps.
 e = " " " " Springs.

Example.

Spring Rise (or Mean Spring Range) = e to a = 12 ft.
 Neap Rise = e to b = 10 ft.
 Neap Range = d to b = 8 ft.

For ordinary purposes the following Table, for Reducing Soundings to the Mean Low Water Spring Tides, will be found sufficiently correct, except where the Tides are affected by a large diurnal inequality.

AT SPRING TIDES.

At the 1st hour, before and after high water, deduct	$\frac{1}{2}$	} Of the rise at springs.
" 2nd " " " " "	$\frac{3}{4}$	
" 3rd " " " " "	$\frac{1}{2}$	
" 4th " " " " "	$\frac{1}{3}$	
" 5th " " " " "	$\frac{1}{4}$	
" 6th " " " " "	0	

AT NEAPS.

At the 1st hour, before and after high water, deduct	$\frac{1}{2}$	} Of the rise at springs
" 2nd " " " " "	$\frac{3}{4}$	
" 3rd " " " " "	$\frac{1}{2}$	
" 4th " " " " "	$\frac{1}{3}$	
" 5th " " " " "	$\frac{1}{4}$	
" 6th " " " " "	0	

Trinity High-Water Mark, as established by Act of Parliament in 1800, is cut upon a large stone on the lower outer wing wall of the Hermitage entrance of the London Docks. Trinity high-water mark is 12·53 feet above the Datum used by the Ordnance Survey, i.e. Mean Level of the sea at Liverpool; therefore by obtaining from the Ordnance map the level of any Bench mark and applying 12·53 feet to it, the level of the Trinity high-water mark is found.

The Trinity high-water mark will be found cut upon the Tower Wharf, and also upon the front of the Fishmongers' Hall Wharf, next above London Bridge.

III. TIDE-OBSERVATIONS.

§38. It is evident, from what has been said (Nos. 919, 922), that the establishment cannot be truly deduced from the notice of a solitary high water; and that observations, continued, at least through a semi-lunation, are necessary for even a tolerable approximation. But the true establishment cannot be successfully determined from a series of observations involving the semi-menstrual inequality, the various effects of changing declinations and parallaxes, with temporary and local circumstances, except by persons not only thoroughly versed in arithmetical operations on an extensive scale, but well exercised in the particular intricacies of these laborious calculations. We have, therefore, confined ourselves here to merely indicating the details which should accompany tide-observations.

(1.) The exact *spot of observation* must be specified.

(2.) The *instant* of both *high water* and *low water* should be stated, with the *height*, or difference of the two levels, in feet and inches. As the water hangs for some time towards the turn of the tide, and as the tide-current may be independent, it is necessary to note the instant at which the water passes a fixed mark, both in rising and falling; the means of these times are the instants of high and low water respectively. The marks should be fixed in some place to which the water passes slowly, because the waves, however small, continually washing over the marks, render it difficult to detect a small rise or fall of the water.

The observations of both low and high waters of the 24^h are necessary for determining the Diurnal Inequality; but as the time of this inequality is of less importance than the height, it will often be enough, in respect to this particular point, to note the height alone.

About mean water (or half tide) the surface rises or falls with greater velocity than at any other time, and accordingly the instant at which the water passes a fixed mark or a given horizontal line may be observed with greater precision than at any other time. Hence it has been recommended to notice the instant of passing one or two such marks, instead of the times of high and low water.—“On the Law of the Rise and Fall of the Sea’s Surface during each Tide.”—*Phil. Trans.*, Part II. for 1840.

It has been proposed to place the marks at half-tide, but this does not answer, especially where the diurnal inequality is consider-

able.* The intervals should be short on either side, of high and low water, because the tides do not rise and fall with equal velocity.

(3.) The times of *slack water* should be noted.

(4.) The direction, and, in general terms, the force of the *wind*, should be stated, as, also, the height of the barometer.

As the effects of winds and atmospherical changes are not confined to the particular hours during which such causes are in action, it will be proper, when only a short series of observations can be obtained, to add further a brief notice of the state of the weather for some time previous.

Observations continued for a fortnight afford a first approximation to the Tide-hour; and when carried on for some months, this, with some other principal elements, may be obtained with considerable accuracy.

937. The custom has prevailed of noting the establishment as the *hour of the day*; but it obviously should, as recommended by Dr. Whewell (*Phil. Trans.* 1833, p. 229), be considered merely as an *interval*. Since the correct establishment is measured from twelve o'clock, it may, indeed, appear to be indifferent whether we call it an absolute time or an interval; but the *absolute time* of the tide is in all cases referred to the instant of the moon's transit, and it is absurd to talk of adding two absolute times together; as, for example, adding three o'clock of the day to five o'clock of the day. Also, by considering the establishment as an interval only, we avoid confounding mean and apparent times.

938. The soundings on the charts are the depths at "low water;" but this term may imply indifferently the mean low water of the whole year, or of the equinoctial spring-tides, of which the average is not always identical, or of those low waters only which were observed during the operations of survey. Since these may differ considerably from each other, the computed depth may be in error by the same difference. It might appear less equivocal if the lowest of all the low waters were understood; but this, though a natural phenomenon, and, so far, preferable to an imaginary standard, as an average, is still defective, since it is affected by winds. It would appear, therefore, as Capt. Beechey proposes,† that the standard low water should be identified as so many feet and inches below the mean level, which appears to be the only element nearly constant.

The mean level may, it appears, be found approximately by observations of four consecutive tides, which include the diurnal inequality.

* Adm. Bayfield (to whom I am indebted for some important remarks and corrections here and elsewhere in the former editions) informs me that in the St. Lawrence the alternate ebbs do not fall to the half-tide mark at all when the diurnal inequality is considerable. Also Adm. Beechey acquainted me, as the result of numerous observations, that at Plymouth the half-interval of time between the passages over the half-tide marks requires $\frac{1}{4}$ of the whole int. to be added to it for the correct time of high water, in consequence of the unequal rise and fall.

† "A Report of Observations," &c

NAVIGATING THE SHIP

I. SHAPING THE COURSE. II. PLACE OF THE SHIP. III. DETERMINING THE CURRENT. IV. STORMS. V. MAKING THE LAND.

939. In the preceding part of this volume each point of the subject has been treated separately. The present section, which will conclude the PRACTICE, and to which the former chapters may be considered subservient, contains matters of general reference in conducting the navigation of the ship.

I. SHAPING THE COURSE.

940. As soon as the ship is clear of the land, and circumstances permit, her head is put upon the course to be steered, the log hove, and the departure taken.

When the course is to be shaped for a distant port, recourse is had, in defect of personal experience, to the Sailing Directions,* in order to learn what point to steer for, so as to profit by particular winds or currents, or to avoid dangers. The bearing of such point is then worked for by parallel, middle latitude, or Mercator's sailing, according to the case; or, a ruler being laid on the chart over the place of departure, and the point in question shews the course, No. 381.

941. When the wind is foul, reference will be made to No. 299; but, in the case of a prevailing foul wind, the proper line of proceeding will be indicated in the Sailing Directions.

A steam-vessel will generally preserve her course without regard to the wind, except in long passages.

* The Sailing Directions contain descriptions of ports and anchorages, with accounts of the winds, currents, and tides, for various coasts and seas. Besides these and other particulars, necessary for navigation alone, works of this kind contain well-selected passages from voyages and travels, by which the reader may obtain clear ideas of the physical aspect of the shores, climate, and natural phenomena of most parts of the world, and derive considerable information respecting the manners and customs of the inhabitants, the productions, and articles of merchandise.

1. *Shaping the Course in a Current.*

942. When the whole or any part of the voyage lies through a current, having everywhere the same direction and velocity, it is proper to shape that course which shall keep the port on the same bearing (No. 294), because the ship will thus cross the current in the shortest possible time. But if the current be different in different parts of the voyage, this rule does not hold good. This point cannot be pursued further in this volume.

When the current, setting the ship away from her port, is so strong, or the wind so light, that the ship cannot preserve the bearing of the port unaltered, she will be kept so that the course made good shall not be more than eight points from the bearing of the port; because, though she cannot thus near the port till circumstances change, yet she will not increase her distance from it, as would result from shaping any other course.

The application of all such rules must, accordingly, depend upon the circumstances of the case.

943. When the ship, having a foul wind, is in a current of which the direction and rate are known, she should be kept as much as possible on that tack on which the current tends most to drift her to windward, or is least unfavourable in drifting her to leeward.

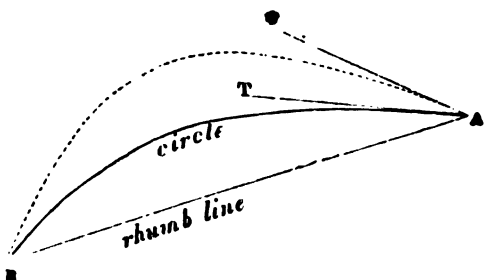
For example. Suppose the course to be steered is S.W., the wind S.S.W., the current S.S.E., 2 knots. Then, on the larboard tack, lying west, and going, suppose, 6 knots, she will make good S. 70° W. 5½ miles, No. 292. On the starb. tack, lying S.E. and going 6 knots, she will make good S. 39° E., 8 knots. The distance made good in the direction of the port when her head is S.E. is 0·8 miles per hour, No. 285; when lying west, this quantity is 5 miles.

In this case the current tends to drift the ship to windward on both tacks; but the larboard tack is the most favourable.

2. *Shaping the Course on a Great Circle.*

944. When the ship sails on the arc of a great circle, the distance traversed in passing between any two points in her track is (as observed in Nos. 336, &c.) less than if she had sailed on a rhumb-line. A distinction of greater importance between these two tracks is, however, that every point of the great circle lies in a higher latitude than any point, having the same longitude, on the rhumb-line. Thus, if two ships sail from St. Helena to C. Horn, the one upon the great circle, and the other on the rhumb-line, altering their longitude by the same quantity, the ship on the circle will be 440 miles to the southward of the other, when the two vessels are most widely separated; that is, when the vessel on the circle is at the point of maximum separation latitude (No. 345). Now the difference of distance is only 76 miles in 3740 (No. 337, Ex. 1); whereas the difference of 440 miles in latitude may place the vessels in different winds.

945. A course taken anywhere between the great circle and the rhumb-line will always be attended with at least some saving of distance.



Thus, any course between A B and A T (the tangent of the circle at A, and shewing its direction at that point) gives a distance less than A B. Again, since the circle is the minimum distance between A and B, on the surface of the globe, we may take a series of tracks between A and B on the other or *polar* side of the circle, increasing in length as they lie further from it, till we come to the dotted line which represents a curve *equal in length* to the rhumb. Hence a ship sailing anywhere between A B and A U (the tang. which shews the direction of the dotted curve at A),—that is, through a space nearly *twice* as great as that between the rhumb and the circle,—will still have less distance to describe than that on the rhumb-line. On this principle a partially foul wind may often be turned into a fair one.

Thus, in the voyage alluded to above, the vessel on the circle, instead of passing 440 miles to the southward of the track on the rhumb-line, may pass at nearly this distance to the southward of the great circle, or between 800 and 900 miles to the southward of the rhumb-line; and yet, after all, she may make good a distance less than that on the rhumb-line, while the great difference of latitude may enable her to avail herself, for part of the voyage at least, of winds proper to regions far removed from those crossed by the rhumb-line.

946. When it is proposed to sail on a great circle the course is shaped with reference to the present place of the ship; and, therefore, when she is found to have got off the original line laid down, the course should, strictly speaking, be shaped anew. But, in practice, this will rarely be necessary, since moderate deviations from the course will not sensibly alter the bearing of a distant port, that is, the same course will serve as before.

947. In great circle sailing with a foul wind the ship will be put upon that tack in which she lays nearest the circle. The rule for windward sailing, which directs that she should be put on that tack in which she looks best up for her port (No. 299), is, therefore, strictly applicable. Indeed, it is only on laying down the great circle, which alone shews the real direction of the port, that it can be decided whether the wind is foul or not for a distant port.

If the rhumb-line differs more than two points from the circle, it is evident that, by shaping the course on the rhumb-line and then laying the ship on the wrong tack, she will head more than eight points away from the true direction of the port, while on the other

tack she would lie within less than 4 points of the course. Thus a seaman not acquainted with the principles of great-circle sailing may cause his ship to recede from her port instead of nearing it.

948. If the wind, when contrary, is in the direction of the great circle, one tack is as good as the other, and the selection must depend on the current, probable change of wind, or other circumstances. The ship should not, however, deviate from the circle so far as to have to shape a new course, for if she has much deviated from that line which was the shortest possible, she must have altered her position for the worse.

950. In navigating the ship on a great circle, in high lats., the course should be shaped anew at each 60 or 80 miles of distance.

The place of the ship is necessarily brought up by middle latitude or Mercator's sailing.

A modification of great-circle sailing has received the name of Composite Sailing. It presents itself whenever the great-circle track, by passing too close to the Pole, becomes dangerous or impracticable on account of the ice which pervades those high latitudes. When this occurs, some one parallel of latitude is fixed upon for the maximum; then the shortest route, under these circumstances, will consist of a portion of that parallel and of parts of the two great circles which touch it and which pass—one through the ship and the other through the destination. This combination of great-circle sailing and parallel sailing offers, therefore, no difficulty. See Davis's *Star Azimuth Tables*, p. 136.

Log, Course, and Dead Reckoning. See Nos. 956 to 969.

951. Dead reckoning has not always met with the attention it deserves. Dead reckoning is a fine art, dependent first upon a well determined position to start with; secondly a knowledge of the correct Variation and Deviation, or total error of the compass steered by; and thirdly on good steering and logging, to carry it on. Remember the remark of John Davis, the navigator, written in 1607, "*the stredge* may be so disorderly handled as that thereby the Pylote may be abused.*" Dead reckoning is also dependent on a correct knowledge of probable currents and tidal streams, on the winds that have been and are blowing.

952. *Good Dead Reckoning* can be attained by practice. See note (Rennel's) on p. 353, 359. Let the position by dead reckoning be considered a serious matter, to be carefully compared with the position obtained by observation. If there is a difference between the positions, let that difference be accounted for, and if it exceeds that probably caused by weather, or by known tides or currents, let it be considered that the distance has been wrongly estimated, or the errors applied to the compass courses incorrect, or the ship badly steered. (*The stredge disorderly handled.*) Let more care be taken the next day, and so on until a confidence is engendered in the dead reckoning that may be useful in closing the land in thick weather.

* "Stredge" may stand for stretch, a term for a ship's course.

II. PLACE OF THE SHIP.

I. *By Dead Reckoning.* See Nos. 951, 952.[1.] *Keeping the Dead Reckoning.*

954. *Latitude D. R.* The latitude by D. R. is deduced by applying the difference of lat. made good by the ship to the lat. by observation of the preceding noon.

When the latitude was not observed at noon, but at some other time it is proper to note the lat. D. R. as "brought up;" because the lat. by D. R., when employed for comparison with the observation, is of course considered as referred to the beginning of the day, unless the contrary is expressed.

When, however, there is no observation, the lat. by D. R. must be referred to the lat. D. R. at the preceding noon.

955. *Longitude D. R.* The longitude by D. R. is deduced by applying the difference of longitude made good to the long. D. R. of the preceding noon.

The long. by D. R. is usually carried on till a new departure is obtained, because the observations for longitude are not so decisive as those for latitude; for the chronometer may alter its rate, and the moon's distance from a star, or her R.A., may be much affected by a small error of observation. Hence, when the longitude by a single observation differs much from the account, it is not always considered safe to adopt it until it has been confirmed by another observation.* When, however, such confirmation is obtained, or two distances, observed at the same time on opposite sides of the moon, give results not differing much from each other,† the resulting

* In vol. i. of the East India Directory, Horsburgh gives an example of the danger of trusting to a single chronometer for a length of time, or to a single lunar, in the case of the Taunton Castle, which got aground in the Straits of Mozambique in 1791. A lunar 5 days before had agreed with the chron., but a lunar 12 hours before differed from it 1°. It was naturally considered that the former lunar confirmed the chron., and that the later observation was erroneous; the contrary, however, turned out to be the case.

† Horsburgh states that he has found the mean of two lunars, observed on opposite sides of the moon, nearly a degree in error. So strange a result would seem, however, to throw doubt on one of the observations.

The Rev. G. Fisher, in the Appendix to Captain Parry's second voyage, p. 282, states that the mean of 2500 lunars observed in December differed 14' from the mean of 2500 observed in March following; and that the mean of the observations made in the same summer differed 10' from those last, or 24' from the first. Capt. King, in his survey of Australia, notices a discrepancy of a similar kind, to the amount of 12', at the Goulburn Islands.

longitude should be taken as a departure from which to carry on the D. R.

Although it is recommended not to alter the long. by D. R. on slight grounds, yet it can answer no useful purpose to persevere in carrying it on after observations have proved it to be wrong.

[2.] *Errors of the Dead Reckoning.*

956. These are the errors of the course and distance, with their effects upon the lat. and long. by account.

An error of half a point in the course is equivalent to an error of $\frac{1}{10}$ in the dist. run, very nearly.

957. *Error of the Course.* The ship, besides moving in a path more or less serpentine from the action of the waves, and from imperfect steerage, is driven bodily by the wind, and often by currents and tides; hence the general direction of the ship's head is a very imperfect index of her course by compass. Again, the course by compass is affected by the variation and by the deviation; the latter, as already remarked, varies in different ships, and in different positions of the same ship.

960. *Error of the Distance.* The rate of sailing varies, from time to time, with the strength and direction of the wind, the quantity of sail set, the trim of the sails, the running of the sea, and, in a slight degree, on the skill of the helmsman. Hence, since the log can be hove at intervals only, while the compass is constantly inspected, the distance run, unlike the course steered, is left in a great degree to estimation.

While a vessel is steaming, her rate is, of course, less liable to change.*

961. The allowance to be made for the *heave of the sea* is doubtful. As regards the motion of the waves alone, it would appear that no such action takes place, and any effect of the kind must be referred to the progressive motion which the water at the surface acquires from the action of the wind, and which affects both the vessel and the log. The existence of a surface-current accompanying a strong wind is established by the falling over or breaking of the tops of the waves, which subsides accordingly with the wind, and disappears long before the swell goes down.

962. In steam-vessels the log is found to give too much distance. This is accounted for thus:—The water at the surface being continually urged astern by the paddle-wheels, preserves its motion for some time after the vessel is past; the log, therefore, unless thrown perfectly clear of this current, is carried in the direction opposite to that of the vessel. On this account it is proper to heave the log from the paddle-boxes.

* By practice seamen learn to estimate the rate of sailing within half a knot, and the number of revolutions in a given time of the engines of a ship under steam furnish a means of determining her speed very closely.

963. In consequence of the fore and after bodies of vessels in general being dissimilar, the resistance of the water to the rolling and pitching produces unequal actions on the bottom, from which results a slow motion of the vessel herself in the direction of her length. The nature and quantity of this motion is determined by the form of the bottom. Most vessels forge ahead, but some astern.*

964. *Error of the Latitude D. R.* This is composed of the errors of the course and distance.

If the lat. by D. R. does not agree with the observation, it is customary, when the course since the observation is nearly N. or S., to attribute the error to the distance; because, in this case, any small variation or error in the course will not affect the D. Lat. Again, when the course is nearly E. or W., such error is attributed to the course; because, in this case, a small error in the course will affect the D. Lat., while a small error in the Dist. will not.

These suppositions, though plausible, are not always true, and therefore are not to be implicitly adopted.

965. An error in the latitude is the same number of nautical miles in all parts of the world.

966. *Error of the Longitude D. R.* This error, when the long. is carried on by parallel or by mid. lat. sailing, is proportional nearly to the error of the Dep. When the long. is carried on by Mercator's sailing, the error is due to an erroneous course and distance, and also, in most cases, to using latitudes by observation inconsistent with the given course.

967. An error of a given number of minutes of longitude (') is the same number of sea-miles† when the ship is near the equator; but in higher latitudes the same number of min. of long. is equal to a smaller number of sea-miles. Hence precision in the longitude is of less consequence to the safety of the ship in high than in low latitudes.

For the same reason the long. by D. R. will in general be kept more correctly in low than in high latitudes.

968. As regards the probable *amount* of the errors of the ship's place in latitude and longitude, it may be supposed that the error of the course will rarely amount to a point, and that the distance will not be in error more than $\frac{1}{10}$ of itself.‡ Such estimations, however, must depend entirely on circumstances.

The error, on the whole, will be that due to the sum or the difference of these errors; more frequently, however, to their differ-

* Capt. W. Ramsay informs me that the *Black Joke*, a very fast vessel which he commanded on the coast of Africa, always forged astern in a calm.

† Seamen are in the habit of calling minutes of longitude *miles*; but a mile is a measure of invariable length, while a min. of long. is different in different latitudes; the practice, therefore, should not be followed.

‡ Rennell ("Investigation of the Currents of the Atlantic," p. 70—London, 1832) quotes Flinders's opinion that the reckoning may be kept within 5 miles of distance, and half a point in the course.

ence, since experience establishes that, when several observations are taken together, their errors tend to compensate each other.

969. Under the head "D. R." is included the determination of the ship's place by bearing and distance of the land. When a point of land bears N. or S., the diff. lat. of the point and the ship is the distance; and consequently the error of the lat. is exactly equal to that of the distance, while a point or two of error in the bearing produces but small error in the lat.

On the other hand, if the place bears E. or W., the ship's lat. is that of the point itself, and an error in the bearing produces in the lat. an error proportional to her distance.

This applies to longitude by reading, in the above, long. for lat., and interchanging N. and S. with E. and W.

[3.] *Variation of the Time at Sea.*

970. When the ship sails to the eastward, she meets the sun, and therefore anticipates the hour of the day by a portion of time equal to the diff. long. she makes good. In sailing to the westward, the contrary takes place. Hence in sailing eastward the apparent day is always less than 24 hours, and in sailing westward greater than 24 hours, by the diff. long. made good, in time.

Thus a ship, in sailing round the world to the eastward, gains a day in her reckoning of time: for each day in which her head is to the eastward is less than the common day of 24 hours by the diff. long. made good; and this goes on till the diff. long. has accumulated to 360° , or 24 hours. Hence, on completing the voyage (but without any relation to the time of performing it), the ship, by constantly gaining on the next day, is found to have completely anticipated it; so that, instead of finding it Wednesday, for instance, among the natives, it appears by her journal to be Thursday.

In sailing round the world westwards, the ship in like manner loses a day. In these cases the voyage is performed in days of a different length from the average of 24 hours, and the whole period is made up of a different number of days.*

971. This alteration of the date in the journals of ships crossing the Pacific is often attended with considerable embarrassment to the reader, especially if he does not bear in mind the direction of the ship's route. In order to provide against this ambiguity, the navigator should insert the Greenwich Date at full length, in every case in which a reference to the absolute time may be required.

972. The variation of time, or the irregularity in the length of the day, falls on the hour or half-hour preceding noon, the last glass

* Sir James Ross remarks that in crossing the meridian of 180° eastwards they made two Thursdays, and two Nov. 25ths, by which means their reckoning would correspond to that of Australia and England on their arrival.

A short rule to estimate day and hour of arrival for steamships crossing the Pacific is: Going West: Add one day to assumed time of length of passage, and subtract the Diff. Long. in time between the two ports. Going East: Subtract one day from assumed time of passage, and add the Diff. Long. in time.

or two not being turned. When there is no observation for some days, the time is thus liable to be considerably in error.

This uncertainty in the absolute time causes no difficulty in bringing up observations to noon, or to any other time, nor in connecting observations made A.M. with others made P.M., because the courses and distances marked on the log-board are those corresponding to the actual intervals elapsed.

973. It is evident, since the time at ship always has reference to the diff. long. made good subsequent to the observation for time, that the account of the time is more correctly kept in low than in high latitudes. (See No. 967.)

[2.] *Place of the Ship by Observation.*

974. Besides the latitude and longitude of the ship by observation, we shall consider, under the above head, those observations from which the elements necessary in the calculation of her place at any time are obtained: as observations for Time, and for the Variation of the Compass.

[1.] *Latitude by Observation.*

975. In variable climates it is often advisable to take, early in the forenoon, an altitude of the sun, to be followed by another after the proper change of azimuth, No. 749, for a double altitude, in case the meridian alt. is not obtained.

If the second alt. is observed within the limits of Table 47, the operation is simpler, and the result more satisfactory. If it is near the meridian, and the time is not very much in error, the second alt. alone determines the latitude by the reduction to the meridian, p. 249.

In either of these cases the first alt. affords the apparent time, when the lat. has been ascertained.

976. (1.) The lat. will of course be obtained, when possible, by the meridian altitude of the sun. The short double altitude A.M. has the advantage of providing against the loss of this observation,* and it enables the navigator to determine the place of the ship before 12 o'clock.

The altitude of the moon on or near the meridian (Nos. 702, 703) may often be obtained during bright sunshine. Also, the moon's alt., combined with that of the sun, affords the lat. by double alt., No. 759, &c.

The planet Venus may often be observed during the day.†

* The only observation disturbed by the ship's change of place (No. 548) is the mer. alt. Suppose, for ex., the ship is approaching the sun 12 knots, she raises him at the rate of 12" in 1°. Hence he continues to rise till he is so far past the merid. as to have begun, by his motion in altitude, to fall at this rate. In high lats. where the motion in alt. is slow, the interval will be considerable; in lat. 60 he would appear to dip about 5 min. P.M., and in the same case, with the ship receding from him, he would dip about 5 min. A.M. To compute this time, see No. 622.

† Horsburgh states that he has observed the meridian alt. of Venus, at the Cape of

When the planet is not bright enough to be distinctly visible to the naked eye, it may generally be found, when near the meridian, thus :—Compute the merid. alt., No. 663 ; add to it the dip and refraction ; set this angle on the sextant, put in the inverting telescope, screwing it close down to the plane of the instrument : then, directing the sight to the N. or S. point of the horizon, the planet should be seen in the silvered part of the glass.*

977. The lat. is found at night by observations of stars on or near the meridian, No. 687. The lat. by a star at night not only is useful in preventing the accumulation of error in the D. R., but also serves as a check on the lat. by the sun (note *, p. 249).

The observation of stars at night is, however, a very different observation from other altitudes by day, and, to ensure success, the observer should make it a matter of special practice.

It is, however, during the twilight that stars and planets may be most advantageously observed at sea, as the horizon at that time is strongly marked, and, when not sufficiently so, may be rendered distinctly visible by the inverting telescope. In favourable cases such lat. may be depended upon with as much confidence as that of the sun. In north latitudes above 20° or 30° , the pole-star may always be observed when the sky is clear.

[2.] *Time by Observation.*

978. The Time is generally found by a single altitude (p. 278), early in the forenoon, when the error of the ship's lat. produces no sensible error of time. It should also be found late in the afternoon. In certain cases it may be found by equal alts., No. 798, the result of which is apparent noon ; and also approximately by the short double altitude (p. 285), and at sunrise and sunset (p. 283).

The time may likewise be deduced from one of the altitudes of a common double altitude (p. 276) ; but the latitude resulting from this observation not being very correct in general, and more especially when the reduction of the alts. to the same place of observation is large, the time deduced would not always be satisfactory.

979. When the sun and moon are both visible, and one of them is near the meridian, the lat. may be found, and also the time, which (Nos. 696, 757) thus has the advantage of being free from the errors of the reckoning. In like manner the alt. of a planet might be taken with that of the sun at the same instant, or some time afterwards (No. 764).

980. When the time is found at night by alts. of stars or of the moon (Nos. 782, 784), since the sea-horizon is often unfavourable for observation at that time, the result should be considered as of

Good Hope, during bright sunshine. Capt. Basil Hall, to whom I am indebted for several valuable suggestions, acquainted me that, on a voyage to Malta in H.M.S. *Indus*, in August 1841, he observed the mer. alt. of Venus every day for a fortnight. Capt. Wickham also tells me that he has found the lat. by Venus, in the tropics, at 3^h in the afternoon.

* Capt. Hall informed me that he had often found the lat. in this way, both by Venus and Jupiter, when the planets were altogether invisible to the naked eye.

inferior value; or stars should be observed on both sides of the meridian, in order to diminish the effects of errors from this cause.

The remarks on the observations of planets or stars by twilight for lat. (in No. 977) apply to observations for time. Stars may often be obtained nearly on the prime vertical, and on opposite sides of the meridian (No. 787); and the alt. for time should always, if possible, be accompanied with another for lat., in order to avoid all reference to the reckoning.

981. An approximation to the apparent time may be conveniently obtained, during part of the six months that include the summer, by setting the index of the sextant to the apparent alt. of the sun's lower limb deduced from the true alt. of the centre, at the time of passing the prime vertical, Table 29; the hour-angle at which the limb attains this alt. is then taken out from the adjacent column.

982. Since the change of alt. of any celestial body is greatest at the equator and nothing at the pole, the time deduced by means of altitudes is more correctly determined in low than in high latitudes. (See Nos. 778, 779.)

983. Advantage should be taken of favourable opportunities of landing at well-determined places for good observations of time, because the diff. long. between the places will at once discover any considerable change in the rate of the chronometer, and afford the means of correcting it. Comparatively few places indeed are as yet laid down with sufficient accuracy for the general practice of this simple and decisive method; but, in proportion as the longitudes approach to precision, the differences of longitude will be employed by seamen as the means of obtaining, directly, the *sea-rates* of their chronometers, instead of waiting to obtain harbour-rates.*

984. *Error of the Time at Sea.* The time at sea, as found by a single altitude, can rarely be depended upon to less than 10" (Nos. 778, 779). If, therefore, the ship's reckoning were correctly kept, her diff. long. applied to the time, as found by observation on a former occasion, would give the time at ship within about 10" of the truth. But as the D. R. is always more or less in error, and as the error may be considered generally to increase with the time elapsed, the error of the time at ship may be considered as 10" *plus* the error of the diff. long. accumulated since the observation.

[3.] *Longitude by Observation.*

985. The longitude by chronometer may be ascertained whenever the time is obtained. The long. by chron. is thus the most efficient check on the long. by account from time to time; but after a lapse of time it may be greatly in error, as the rate is liable to change. See No. 531.

* This important remark is due to Col. Sabine, "Account of Experiments," p. 401.

When there is no chronometer on board, the longitude by D. R. can be corrected only on making the land, or by a lunar observation, or sometimes by speaking another vessel.

986. When a satisfactory longitude is obtained by independent means, as by observation of the moon, it should be adopted as a new departure taken at the instant of observation, instead of carrying it back to the preceding noon or any other time; because this last process, which is attended with no advantage, impairs the value of the observation by mixing with it the errors of the run.

987. Since the object of the lunar observation is to find the mean time at Greenwich at the instant of observation, the simplest and most direct application of the method is to find at once the error of the chronometer on G. M. T.; because this process is not embarrassed by consideration either of the time at place, or of the change of long. in the interval between the lunar observation and the observation for time. This is the practice of the most experienced navigators.

988. When there is no chronometer on board, the longitude itself must be found for the instant of the mean of the observed distances. For this purpose the time at place is necessary. If, therefore, either of the altitudes observed for the lunar is favourable for determining the hour-angle corresponding, the time may be obtained from it, and being compared with the G. M. T. found by the lunar, the long. is determined, No. 827.

If neither of the altitudes is fit for the purpose, the time must be found as soon as possible afterwards. In this case, add the interval elapsed to the G. M. T. deduced by the lunar: the sum is the G. M. T. of the observation for time. This time, compared with M. T. at place, gives the longitude.

Ex. At $3^h 11^m 26^s$ by watch, obtained a lunar, which gave G. M. T. $2^h 14^m 32^s$. At $3^h 56^m 18^s$ by watch, obtained an observation for time. Find G. M. T. at this second observation.

T. by watch, of lunar	$3^h 11^m 26^s$	G. M. T. of lunar	$2^h 14^m 32^s$
Ditto of obs. for time	$3 56 18$		$44 52$
Interval	$44 52$	G. M. T. at 2d obs.	$2 59 24$

989. In the Arctic regions, in summer, the presence of the sun at night prevents the stars from being seen; also frequent fogs obscure the moon. Hence the lunar observation is much less available there than in other climates, and the chronometer in consequence more valuable.*

990. The number of observations, either for latitude or longitude, which it may be proper to take for determining the ship's place, obviously depends on the distance of the land and on the state of the weather. For example, in making a passage with a trade-wind, a much less degree of attention will be necessary than in unsettled weather, when the D. R. cannot be kept with equal correctness,

* "An Account of the Arctic Regions," &c., by W. Scoresby, jun. 2 vols. Edinburgh, '820.

or than when the ship is in the neighbourhood of the land or a danger.*

It is always advisable, when any observation is taken, to obtain, either at the same time or as soon as possible afterwards, another of such a kind that the same error may produce different effects on the result; whereby the two results being in error opposite ways, their mean will be preferable to either separately. The kind of observation proper for this purpose, in any case, has been generally noticed in the *Degree of Dependence*. See No. 999.

When the observation consists of one or more alts., the errors of observation may often be removed at sea by observing also the supplement of the alt. It is, however, proper to remark, that when the supplement is observed by an ordinary sextant or circle, it is, in consequence of its greater magnitude, much more affected by the error of parallelism (Table 54), when this is considerable, than the alt. itself.

[4.] *Observations for the Variation.*

991. The total error of the standard compass should be constantly observed and recorded, not only for the purpose of secure navigation, but with the view of determining the variation, and so helping to maintain, for the benefit of all seamen, a correct chart of its value.

993. The amplitudes of bright stars and planets may often be well observed, especially about twilight, when the horizon is strongly defined. The observation is most convenient at setting, because a star may be followed to the place of its final disappearance below the horizon; but it is not always easy to identify a star at rising.

With care the error of the course due to the compass alone should not exceed a degree: less accuracy is hardly compatible with good navigation in fast steam-ships.

[5.] *Combination of Results.*

997. As all observations are liable to errors, and as given errors of observation produce different effects according to the case, the results of different observations do not generally agree.

In some cases the same errors of observation will cause all the results obtained under the same circumstances to be in error the same way, instances of which occur in Nos. 702, 868. In other cases, the effects of errors will tend to compensate.

998. In general, when the particular errors with which the observation is affected are not known, the *mean* of the several results is employed, or the sum of the results divided by the number of observations.

* Rennell remarks that the facilities afforded in these days for finding longitude may tend to diminish the *necessary attention to the reckoning*, on the ground that the next day's observations will set all right. P. 70.

Since one of two results may be nearly or exactly true, and since it will rarely happen that one is precisely as much too great as the other is too small, the mean of two results will generally be merely less in error than the worst.

999. In taking the result of observations affected by the same *constant error*, care must be taken not to mix those of opposite kinds, as N. and S., or E. and W., but to take the mean of the two different results. For Ex.: Suppose the lat. is $1^{\circ}28'$ by each of two stars N. of the zenith, and the instrument has a constant error of $1'$, then the lat. by one star S. will be $1^{\circ}26'$, and the true lat., $1^{\circ}27'$, is the mean of $1^{\circ}28'$ and $1^{\circ}26'$. But the mean of the *three* results, taken promiscuously, or one-third of $1^{\circ}28'$, $1^{\circ}28'$, and $1^{\circ}26'$, is $1^{\circ}27'20''$, which is not right.

The same would be true, however great the number of observations on one side, or however small on the other; and hence it is always proper to make this separation, which is also a means of detecting a constant error. For instance, if the moon's semidiameter in the Naut. Alm. is erroneous, the result of lunar observations of one limb will differ from that of observations of the other limb and the mean of the two results, not of the whole indiscriminately, will afford the true longitude.

1000. When the error of observation is given, the *amount* of the error of the result may be computed. Examples of this have already been given in most of the rules for the *Degree of Dependence*. Again, the effect of a constant though unknown error of observation may sometimes be removed, as in No. 861, where the same error in each distance produces more or less error in long., exactly in proportion as the moon's motion in respect to each star is less or greater.

1001. When some of the several results of different observations are known from circumstances to be better than others, it is proper to give to the superior results a greater weight or influence in the general determination. This is effected by writing them down oftener than the others, and dividing the sum by the number of results thus augmented. For example, suppose a diff. long. by a chronometer A is $1^h 11^m 18^s$, and by another, B, it is $1^h 11^m 23^s$; and suppose the result of A is estimated from its superior performance, or other circumstances, as half as good again as that of B, that is, of superior value in the ratio of 3 to 2; then, writing down 18^s three times, and 23^s twice, and dividing by the sum of 3 and 2, or 5, gives 20^s , or the estimated result, $1^h 11^m 20^s$.

The preference of any one result to another under the same or different circumstances, or the degree in which one may be supposed superior to another, must be left to that judgment or tact which is the result of experience and constant attention to a particular subject, as it is obviously impossible to lay down rules of certain application for such questions.

1002. Though it usually happens that the mean of several observations is near the truth, yet, as this is not certain, we must not

hastily assume that the mean of even a very considerable number is a definite determination.*

It is proper to bear in mind that the chronometers, when they agree, are either all right or all wrong; but that when they disagree, some of them must be wrong.† See No. 531.

1003. We shall here remark, also, that every determination whatever is liable to the suspicion of having been influenced by the premature adoption of an approximate mean. For ex.: an observer collects 6 or 8 observations; 2 or 3 of these differ widely from the rest, and they are rejected forthwith. Succeeding observations are compared with the mean, and admitted or rejected accordingly. Now these outlying observations may happen to be as good as the others, if not better; but by this partial suppression of evidence the question is prejudged, and the increasing number of observations only tends to fix the erroneous determination more firmly.

3. *Laying off the Ship's Place on the Chart*

[1.] *Position in Latitude and Longitude.*

1004. As the account of the ship's place is closed at noon, the ship is pricked off at that time; also at 8 P.M., when the course is shaped for the night.

The ship's place is laid down by observations, when these can be obtained; in other cases it depends upon the D. R., or frequently upon both.

1005. It is the practice of some seamen, besides taking the ship's place by obs., to mark also her place, as brought up by D. R., from her former position by observation; a line joining these two points stands thus as a leg apart from the ship's track. When the ship stands nearly on the same course, and carries the same wind for some time, this method has the advantage of exhibiting any constant effect produced by a current, or by local deviation, or arising from not making a proper allowance for lee-way.

1006. Since the determination of latitude is absolute and independent (No. 680), the lat. of the ship should be marked whenever a satisfactory observation is obtained.

1007. The longitude, when determined by chron., should be marked on the chart for the time at which the observation is taken, because thus it is unmixed with the errors of the run.

It may be prudent, when there is but one chronometer on board, and when observations of the moon are not practised, to assign a

* Capt. Fitzroy's chronometric measures, the results of 20 or 25 chronometers, amounted, when added together, to $24^{\circ} 0' 36''$, or $36''$ more than the entire circumference. This seemed to be considered, at the time, as a somewhat curious circumstance; but it is evident that some excess or defect was to be looked for, since nothing but accidental compensation of errors could produce, out of a number of discordant elements, the precise quantity $24^{\circ} 0' 0''$.

† Adm. Beechey acquainted me that on one occasion all his chronometers agreed within $1'$, being nearly $30'$ in error, and that the single chronometer of the *Starling*, the tender, was right. As the large majority was considered conclusive, the error was near leading to serious consequences.

second track to the long. by D. R. alone, in intervals of making the land.

1008. As a tolerably good watch alters its rate but little from day to day, the ship's track, as laid down by chronometer, represents truly the relative positions of the ship at different times, and therefore exhibits nearly the true *figure* of her track for a few days together; while its absolute position in *long.* may, at the same time, be erroneous, if the error on G. M. T. is not well known.

On the other hand, since the longitude by lunar, though of undoubted value, is not susceptible of much numerical precision; the difference of two longitudes by lunar, separated by an interval of time, will not, in general, agree with the diff. long. as measured by a chronometer. Hence the track of a ship, as laid down by lunars, would exhibit violent irregularities of figure, while its absolute position in longitude would not be very far from the mean of all the lunar determinations.

Accordingly, when the long. by chronometer is proved by lunar observations to be much in error, and it is required to correct the position of the ship's track, it will be proper to take a mean position among the several positions by lunar, and the lat. at the last lunar. This point being assumed as a departure, the track for the time previous may be adjusted.

*Sumner's Method.**

[2.] *Position on a Line of Bearing.*

1009. When the lat. by acc. is uncertain, the resulting long. by chron. is uncertain in a corresponding degree; but this long., far from being valueless, is capable of an important application, especially when the ship is near the land.

Suppose a second lat. by acc. near the first, as, for ex., 10' greater, a second long. by chron. will be found corresponding; in like manner we may suppose a third lat., with its corresponding long., and so on. Now these positions are those points in different latitudes at which the *same alt.* is observed, and constitute the curve or *circle of equal altitude*, since the observer, moving over the globe so as to keep the sun always at the same alt., would move on a circle, the pole of which is that point where the sun is vertical.

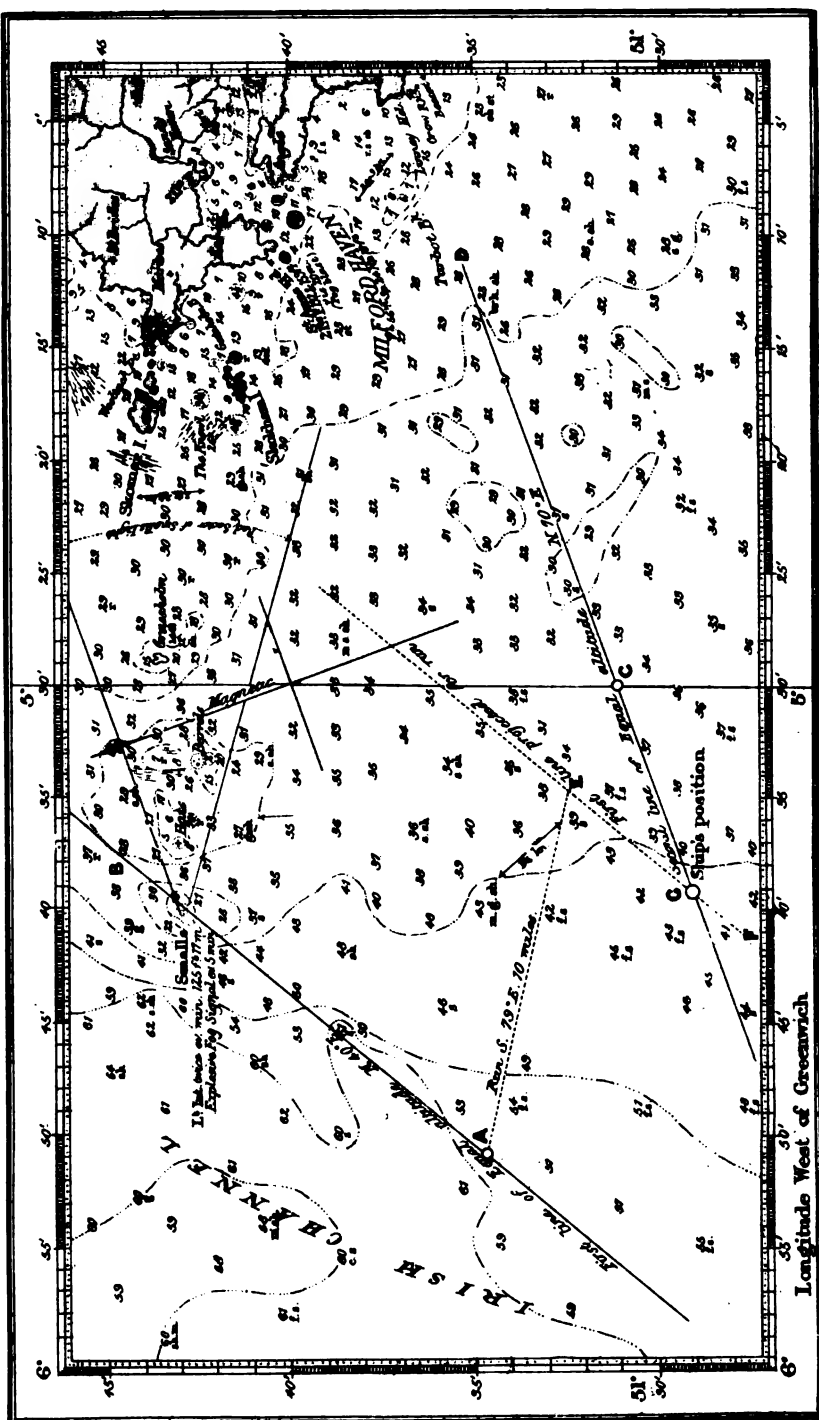
The small portion of this curve passing through two positions near together would appear, on the chart, a straight line; and thus, if this line (being produced) passes through a point of land or other object, the *bearing* of such object is known, though the ship's *place* on the line of its direction is not known.

1010. The process of finding the line of equal alt. consists thus in

* "A New and Accurate Method of finding a Ship's Position at Sea," by Capt. Thos. H. Sumner. Boston, 1843.

In 1843, Commander Sullivan, R.N., not having heard of this work, found the line of equal alt. on entering the River Plate, and identifying the ship's place on it, in 12 fathoms, by means of the chart, shaped his course up the river. The idea may thus have suggested itself to others; but the credit of having reduced it to a method, and made it public, belongs to Capt. Sumner.

DIAGRAM
To illustrate Sumner's method for finding the position of a ship at sea.



ALL BEARINGS ARE TRUE

Longitude West of Greenwich

assuming two lats. by acc., finding the long. by chron. corresponding to each, laying off these two positions on the chart, and joining them by a straight line. But since the sun's bearing is 8 points or 90° from the direction of the line of equal alt., this line may be expeditiously obtained from one obs. only, by drawing a line through the assumed position of the ship at right angles to the sun's azimuth at time of obs., as found by Chap. VII. p. 240; or from the Azm. Tables of Burdwood or Davis.*

From a second obs. of the same or different bodies taken at a suitable difference of bearing, another line of equal alt. is similarly obtained. The intersection of these two lines gives the position of the ship supposing the ship not to have changed her position in the interval.

1011. When the ship changes her place the *true* course and distance made good must be laid off from the first assumed position. Through the point thus found a line must be drawn parallel to the first line of equal alt. Where this line cuts the second line of equal alt. will be the ship's position at the second obs.

The difference of bearings of the sun or bodies used at the two observations should not be less than 25° , or the lines of equal alt. will cut too acutely.

Example, see Diagram.

In the Irish Channel, August 18th, 1890, at $9^h 36^m$ A.M., in lat. by acc. $51^\circ 35' N.$ the long. by obs. was $5^\circ 51' W.$, and the sun's true bearing being $N. 130^\circ E.$, the direction of the line of equal alt. A B, drawn through position A, was $N. 40^\circ E.$

At $11^h 8^m$ A.M., in lat. by acc. $51^\circ 31' N.$, the long. by obs. was $5^\circ 30' W.$, and the sun's true bearing being $N. 160^\circ E.$, the direction of the line of equal alt. G C D, drawn through position C, was $N. 70^\circ E.$

The run of the ship in the interval (A E) was $S. 79^\circ E.$ *true*, distance 10 m.

Through E the line E F is drawn parallel to A B; this line cuts the line C D in G. G is the position of the ship at the second obs. in lat. $51^\circ 29' N.$, long. $5^\circ 39' 30'' W.$

1012. As the ship must be somewhere on the line of equal alt. drawn upon the chart, if this line falls upon a well-sounded chart, her position may be approximately known from the depth of water obtained at the time of obs. Thus on the line A B a depth of over 50 fms. would shew the ship to be at a safe distance from the Smalls. Similarly on the line C D a depth of 40 fms. shews her to be about 23 m. from Linney Head. The line of equal alt. at the first obs. should therefore be drawn as soon as the observations are taken and worked.

When the coast trends parallel to the line of equal alt., the distance of the ship from the shore is ascertained, though her absolute position is uncertain.

1013. The lat. assumed should be as nearly correct as can be obtained by D. R.; this is important when the alt. is high. In low latitudes, when one obs. falls within the limits of the problem for finding the lat. by Reduction to the Meridian (see Table 47), this method should be used in preference to "Sumner's."

* The line of equal alt. may be found by the change in hour angle and consequent change in long. due to a change of one mile in lat. found by No. 615.

1014. As the sun rises and sets to half the globe, the circle of equal altitude at rising and setting is the entire circumference. On the other hand, when he is in the zenith, this circle is reduced to a mere point, or, for opposite points of the sun's disc, covers 32 sea-miles. When the alt. is $89^{\circ} 50'$, the radius of this circle is $10'$, or its extent is 20 miles; when the alt. is 50° , the radius is $40'$, or the extent $80'$. Thus when the sun is low this circle is large, the small portion of it comprised between two assumed lats. very nearly a straight line, and the sun's azim. the same from both ends; but when he is high the circle is small, a small portion of it may be much curved, and the direction of the two extremities very different; that is, the bearing of the land, and the sun's azimuth, may be sensibly different from different parts of the same portion. An error in the assumed lat. has therefore most effect when the alt. is high, and least when it is low, which last is consequently always the preferable case.

As the change from or towards the object of 1 mile in the observer's place changes its alt. $1'$, the effect of an error of alt. is shewn by moving the line parallel to itself through the same amount.

An error in the chronometer places the line of equal alt. too far E. or too far W., bodily, but does not alter its *direction*.

III. DETERMINING THE CURRENT.

1015. The direction and rate of the current are found from the change of place of the ship, or from experiment.

In No. 297 examples are given of finding the current by the comparison of the place of the ship by D. R. with that by observation, and also by reference to the land. In consequence, however, of the unavoidable errors of the reckoning, such determinations must be far from conclusive; and there is no doubt that currents are often assumed to account for discrepancies between the D. R. and observation.* The only decisive method is, evidently, to determine astronomically the place of a floating body, or substance, not exposed to the action of the wind, at intervals of time.

1016. As currents are considered to prevail for a very small portion of the depth of the ocean, it has been recommended to sink a weight to a considerable depth to serve as an anchor for a boat, from which the current at the surface is determined by the compass and the log. This method, however, can obviously discover only the difference between the current at the surface, and that at the depth to which the weight is lowered.

* From good or carefully kept D. R. a reliable Current in 24 hours may, however, be often obtained.

IV. MAKING THE LAND.

1029. When confidence cannot be placed in the correctness of the longitude, it is proper, if circumstances permit, to make the latitude of the port, and then to run on the parallel for it.

1030. On approaching the land it will be prudent to charge the ship's place with some inaccuracy; and the best reckoning can never supersede the necessity of a vigilant look-out.

1031. When the land is made, the ship's place should at once be laid off by the reckoning; for the reckoning may be good, and if so, the ship's position, as laid down, will be correct, or nearly so.

And, again, it is not uncommon, on making the land, especially in defective light, or on a new bearing, and consequently under an unaccustomed aspect, to mistake one point for another, or to make a considerable error in estimating the distance. Now the position laid down is that by which the ship's course is shaped on the chart, and if it depends on an erroneous bearing or distance, it may lead her too near the shore or a danger. The effect of moonlight is generally to make land appear more distant than it really is.

1032. Navigation among coral reefs is facilitated by the clearness of the sea-water. On the reefs on the east coast of Australia, a depth of 5 fathoms was seen from the mast-head, at the distance of half a mile; in 7 fathoms a patchy bottom was well made out from the boat's gunwale; but in 10 fathoms the bottom was scarcely distinguishable from the dark blue of the open sea.

1033. In navigating among coral reefs it is recommended, as essential to safety, that the day should be clear, the sun behind the ship, the water low, and, when the shoals are not clearly distinguished, that the ship should anchor if possible. When the sun draws ahead, coral patches become less distinct; and hence caution is necessary, when making for coral reefs with the sun ahead of the ship.

It is also remarked that the look-out, when placed half-way up the rigging on these occasions, sees better than from the mast-head, where the eye is dazzled by the glare.*

When approaching to round a point of land or shoal, and for that purpose bringing it on what appears a safe angle on the bow, care must be taken that the danger is brought aft—that is, that its angle on the bow is increased as the ship goes on. This is

* When looking out for a light at night, the fact is often forgotten that from aloft the range of vision is much increased. By noting a star immediately over the light a very correct bearing may be afterwards obtained from the standard compass. The intrinsic power of a light should always be considered when expecting to make it in thick weather. A weak light is easily obscured by haze, and no dependence can be placed on its being seen.

especially necessary with a tide or current on the off-bow. From want of due caution in this respect, a ship having only low speed may get into a position with reference to a danger from which it may be difficult to extricate her. The custom of handling ships from forward makes this caution the more necessary.

From No. 369 it will be seen that the seaman can certainly know when a vessel is outside any projecting or outlying shoal by an angle between two fixed marks on the adjacent land. Thus if A and B (fig. ex. 1) are two marks on the land, and the circle OBA passes through those marks and outside any off-lying danger, then, when the angle subtended by the two marks is less than the angle AOB (in this case 46°) the ship cannot be within the circle OBA. The angle AOB has been called the danger-angle.

Such angles may be most accurately measured with a sextant; but the angle between any two bearings taken with a compass, if the ship's head is kept in the same direction while they are taken, is also correct, the bearings being equally affected by variation and deviation. But if such bearings are plotted as cross-bearings, and either the estimated variation or deviation is erroneous, the position of the ship so obtained would also be erroneous.

When ships were navigated chiefly under sail, seamen were much less disposed to approach the land than now. The certain command of course and speed given by steam has led to closing the land, in order to save distance or for other purposes, in a way which would formerly have been considered unsafe. This practice has not been unattended with loss, from the fact that general charts are made from surveys which were not intended for such close navigation. Harbours and their immediate approaches are generally very closely sounded, but to survey every sea-coast in such detail would occupy very much more time than is generally available. The mere fact that vessels have frequently passed close to the land in certain positions without accident, is far from being such reliable evidence of the non-existence of danger as the close sounding of an accurate survey.*

1034. The supply of *water* is a matter of so great consequence as to justify a slight deviation from formal strictness of design in allusion to it. Most of the places at which water is procured are denoted in Table 10 by the letter w, but there are some general suggestions on the subject which may be highly important on occasions, and which it is, therefore, worth while to collect here for reference, more especially as the various works through which they are scattered cannot be generally accessible to seamen.

(1.) The water carried by rivers into the sea is often found at a considerable distance beyond the mouth. For, a cubic foot of fresh

* Further, though ships now better preserve any given course, and the distance run is estimated more accurately than formerly, there are in modern iron ships elements of uncertainty about dead reckoning which still make it perilous to close the land, unless there are means of knowing *with certainty* when the ship is in dangerous proximity thereto.

water weighs 1000 oz. avoirdupois, while a foot of salt water weighs 1028 oz.; the fresh water is thus lighter than salt in the ratio of 100 to 103, or by 1 part in 34 parts; and hence, when running into salt water, diffuses itself over the surface, where it remains till mixed by the agitating effect of the wind or other causes. Numerous instances are recorded of fresh water being thus found at considerable distances from the shore. Dampier, whose interesting voyages contain sagacious remarks on almost every circumstance that deserves the attention of seamen, relates that, being about 2 miles outside a small river, near Achen, in Sumatra, they "found the water of a muddy grey colour, and on tasting it found it fresh;" and he adds that in such cases "we must dip but a little way down, for sometimes if the bucket goes but a foot deep it takes up salt water with the fresh." A similar circumstance happened to the crew of the *Alceste's* barge, when conveying Lord Amherst to Batavia, after the wreck of the ship, on his return from his embassy to China in 1817. Ships have watered two miles outside one of the mouths of the Mississippi, the end of the suction-hose being carefully kept just below the surface. On the like occasions it has been observed that the water has been fresh on one side of the ship and salt on the other, the difference (which of course is only superficial) being due, no doubt, to the protection afforded by the ship on one side against the effect of the wind to mix the waters.

(2.) When rain falls on sand contiguous to the sea, the sand protects it from agitation, and it may remain a considerable time unmixed with the salt water. Accordingly, water is often found, especially after a shower, by digging in sand, taking care to remove it slowly; and advantage may no doubt be occasionally taken of the vicinity of a sandy shore or island to recruit water.

The troops being greatly distressed for want of water in Egypt, Sir Sidney Smith pointed out, that wherever date-trees grow, water was to be found; and a hole having been dug by his directions near some trees of this kind, and a cask sunk in it, a supply was obtained.

Adm. W. H. Smyth (in his *Memoir descriptive of the Resources &c. of Sicily and its Islands*, London, 1824, p. 112) states that on both sides of the Channel (the Faro of Messina), pure, though rather hard, fresh water, is procured, by digging a hole in the sand, within two or three feet of the margin of the sea; this supply is obtained by the filtering of the *fiumare* (torrents), the beds of which, though apparently dry, are never utterly so. The shores here alluded to are wide and flat, and consist of sand and gravel.

In the sailing directions for the North Atlantic, it is stated that water is always procurable near the Is. de Los, by digging near the root of a cocoa-nut tree. Adm. Beechey describes water as found by digging in the coral rock and recommends selecting the higher spots, distant from the sea. Lieut. Ruxton (*Naut. Mag.* 1846, p. 12) states that water is procurable, notwithstanding discouraging appearances, at a trifling depth in the sand, on the S.W. coast of Africa, to the northward of Walvisch Bay. Extensive

tracts of coast, in different parts of the world, are, however, described as absolutely without water.

(3.) Water is often found by following the track of animals, which, whether wild or domesticated, form paths to watering places. It was by following a path made by goats at Ascension, that Dampier discovered the spring which bears his name. Capt. Fitz Roy states that water was found on Charles and James Islands in the Galapagos by following the track of the terrapin.

(4.) Boats' crews or survivors of a shipwreck may find it useful to know that rain-water and dew collect round the stems of plants which shoot leaves upwards. Dampier (*Voyages to the Bay of Campeachy*, p. 56) remarks that it is often obtained from wild pines. 'These take root and grow upright from trees. The leaves hold a pint and a half or a quart. We stick our knives into the leaves, just above the root, and that lets out the water, which we catch in our hats, as I have done many times to my great relief.'

The cocoanut-tree, the fruit of which is found plentifully, but not everywhere, in the tropics, and chiefly near the sea,* and whose singular and beautiful form, reaching to the height of between 40 and 110 feet, renders it a conspicuous object as a mark, is denoted in Table 10, on account of its value to seamen, by a special symbol. The natives near Cape Grenville, Australia, carry with them, when travelling inland where they are not likely to find water, the juicy roots of a shrub (*Naut. Mag.* 1847, p. 178). Captain Stokes remarks that a pint of water has been collected by a sponge from leaves in the morning, even on the S. coast of Australia, where the dews are not so heavy as on the N.W. coast (*Discoveries in Australia, &c.*, in *H.M.S. Beagle*, 1837-43," vol. ii. p. 12).

(5.) Ice islands are frequently composed of pure fresh-water ice, which is found in pools on the surface,† or running down the sides; and watering in this manner is a general practice of ships in icy seas. It is often, however, difficult to land on ice; and in such circumstances Admiral Bellingshausen cannonaded an ice island, and sent the boats for the fragments splintered off.

A peculiar danger is incurred by landing, for the purpose of cutting away a portion, upon ice which, from the advanced period of the summer, or the warmth of the air or sea, tends towards dissolution. A blow of an axe may split the whole mass, and the two portions, in turning over to acquire a new position for floating, may engulf the boat and the persons employed. (Scoresby, *Journal of a Voyage to the Northern Whale Fishery in the Baffin*, in 1822, p. 300.) A mass of ice is likewise often liable to turn over, to float in a new position, in consequence of having undergone a change of form by thawing irregularly.

The pools of water on the ice are often brackish in the autumn,

* This has long been remarked. Dampier records that the finest he had ever seen grew on Trieste, a small island off Sumatra, overflowed at spring-tides.

† In about 62° S. the U.S. Expl. Exped. found on an iceberg a pond of excellent water, an acre in extent, and 3 feet deep, covered with a scum of ice 10 inches thick.

when the ice becomes porous, and the salt water is drawn up by capillary attraction (*Narrative of an Attempt to Reach the North Pole in Boats*, by Capt. W. E. Parry, 1827).

Though excellent water is often obtained from ice, it appears by no means certain that this is always the case. Mr. Rae, who left Fort Churchill in July 1846, to explore the coast from "Dease and Simpson's furthest," to Fury and Hecla Straits, states "that they had much difficulty in finding water that was drinkable" (*Naut. Mag.* 1847, p. 620). Baron Wrangel (*Le Nord de la Sibérie, Voyage, &c.*, 1822, &c.), mentions that the salt left by evaporation on the surface of the ice, is mixed with the snow that falls upon it, and eaten as salt with food, though bitter and aperient. He found the green transparent ice brackish, the blue, fresh.*

1. *Indications of Land.*

1035. The neighbourhood of land is often indicated by the presence of birds, and its position inferred from the direction in which they take their flight at sunset. Birds, however, are often found attending floating masses of seaweed, which they follow for the sake of fish, and which is found at all distances from land.

The sudden appearance of birds flying round the ships at night aroused the attention of the officer of the watch, and was thus the means of saving D'Entrecasteaux's squadron from great danger near New Caledonia (*M. D'Urville's Voyage in the Astrolabe*, 1826; Paris, 1833, vol. iv.)

Adm. Beechey remarks that birds fly near reefs and islands in the Low Archipelago, and calls the attention of seamen to this circumstance.

1036. It has generally been supposed that the appearance of particular birds denotes the land to be near. Cook remarks (1st Voy. vol. i. p. 53), that "they had been so often deceived that they ceased to look upon aquatic birds as sure signs of the vicinity of land." He observes (1st Voy. vol. ii. p. 37), that shags and some other birds seldom fly out of sight of land, and adds that he believes gannets, boobies, men-of-war birds, seldom go far out to sea. Sir E. Belcher, however, met constantly with the gannet, frigate-bird, tropic bird, and booby, at considerable distances from the land, in the N. Pacific (*Narrative of a Voyage round the World in H.M.S. Sulphur*, 1840). Cook considered divers a sign of land (1st Voy. vol. i. p. 47). Admiral Bellingshausen makes a similar remark† (*Voyage of the Mirny and Vostok*, vol. i. p. 215).

* It is a mistake to suppose that merely filtering the water removes all noxious matters, as the process merely arrests, mechanically, solid particles. The Chinese purify water which has become offensive, by mixing half an ounce of alum to one ton, and leaving it for some time. Sir E. Home tried this with complete success in H.M.S. *North Star* (*Naut. Mag.* 1846, p. 625). This use of alum has long been known; powdered charcoal, and stirring clay in the water, have also been used.

† The stormy petrel (*Mother Carey's chicken of sailors*) is supposed to foretell wind; Bellingshausen remarks, on the contrary, that this bird made its appearance (at least near 4° N. and 20° W) before continued calms. Vol. i. p. 89.

Adm. Beechey remarks that black and white tern fly 40 miles from uninhabited islands, but desert altogether those that are inhabited.

1037. Dr. Scoresby observes that in the Arctic regions birds desert closing spaces in the ice, and repair to others which are opening.

1038. As a current of water, interrupted by the rising of a shoal or coast from the bottom of the sea, is carried upwards by the pressure from behind, and as the water below is, in warm and temperate climates, considerably colder than that on the surface, a fall in the temperature of the surface-water has often been found on approaching a shoal or the land, and the thermometer has accordingly been confidently recommended as a guide in coming into soundings. But it is evident that this effect must depend upon the relative coldness of the water above and below, and also upon the depth and other circumstances of the current, and it has been found that the indication is neither so constant, nor so marked, as to be depended upon. Capt. Foster, and more recently Capt. Fitz Roy found no such change on the Abrolhos. Sir E. Belcher (*Voy. in H.M.S. Sulphur, 1840-1, vol. ii. p. 292*) found no perceptible change on entering soundings off the Cape of Good Hope, or in the N. Pacific.

M. Du Petit Thouars (*Voyage autour du Monde sur la Frégate La Vénus, 1836-9, vol. iii. p. 419*) paid particular attention to this indication, and remarks that the observations generally shew a lowering of the thermometer on approaching land, but they disprove that the water on a bank is *always* colder.*

1039. The temperature of the sea has been observed to change several degrees, in intervals of time varying from a few hours to a day and a half previous to a change of wind, the water becoming gradually warmer when the wind was about to blow from a warm quarter, and colder in the contrary case. In squally weather the temperature has fluctuated.†

1040. The temperature of both the sea and the air is, however, so much influenced by the vicinity of ice in considerable mass, that the indications of the thermometer in such circumstances are highly important, more especially as fog, arising from the condensation of aqueous vapour by the cold, frequently occurs at the same time.

When the vessel is to leeward of the ice the air is greatly cooled; and, on the other hand, when the ice is to leeward and not far distant, the water through which it has drifted will be found colder than elsewhere.

1041. Amongst the signs of a near approach to land, on some occasions, are breakers. The depth of water at which they appear seems, however, very uncertain; and it is sometimes difficult to

* In the Gulf-stream, and on the banks of Newfoundland, the thermometer is said to be regular in its changes. (*Purdy's Sailing Directions for the N. Atlantic.*)

† Adm. Beechey records having made observations of this kind in the North Pacific, off C. Horn, and near Spitzbergen. (*Beechey's Voyage to the Pacific, 8vo. vol. i. p. 325; Appendix, p. 390.*)

distinguish between breakers and topping seas. The late Commander Mudge observed that a heavy swell often breaks in 9 or 10 fathoms, and always in 4 or 6; he adds that the swell is often heavier in a calm than in blowing weather. The sea is reported to break on the bar of the River Senegal in 8 fathoms.*

Mr. Thomas, master of H.M.S. Investigator, says that in the gale of August 1833, at the Shetlands, the sea broke over all rocks having less than 8 fathoms on them (Naut. Mag. 1835, p. 309).

1042. The only certain indication, in the absence of external signs, is the depth of water, when soundings can be obtained. Hence *sounding is an indispensable precaution*; and *neglecting to sound* has, in courts of inquiry and courts-martial, always been deemed *inexcusable*. See pp. 343, 344.

2. Illusory Appearances.

1043. While it is necessary to be on the alert for the discovery of danger, it is scarcely less so to be prepared against false alarms. For ex.: in a moonlight night, when blowing fresh, it is easy to fancy breakers and shoals, especially when on the look-out for them. Effects of light and shade have so much resembled breakers as to raise alarm; and sunbeams in the horizon, seen through rain, have been taken for rollers.—(Voyage of H.M.S. Sulphur.)

1044. Clouds and fog-banks often resemble land so much as to deceive an experienced eye. Sir Jas. C. Ross observes, that the vapour-line near the margin of ice in the polar regions is always taken for land by novices.

1045. Many reported islands or shoals, of which the accounts given have been apparently circumstantial, have, doubtless, been trees, fish, alive or dead, or ice islands. Phipps (Voyage to the North Pole in the Racehorse and Carcase, 1773, p. 57) took a small piece of ice covered with gravel for an island. Weddell (A Voyage towards the South Pole, 1822) records that it was only on passing 300 yards from an ice island that they ascertained it was not solid land, but ice covered with black earth. He also mentions having taken the swollen carcase of a dead whale for a rock,—a mistake of frequent occurrence. Sir Jas. Ross met with an iceberg which had turned over unperceived, and presented a new surface covered with earth and stones, so like an island, that nothing but landing on it convinced them to the contrary (vol. i. p. 195). Lieut. Wilkes records that a supposed rock turned out on examination to be a large tree covered with weeds and surrounded by fish (U.S. Expl. Exped.).

1046. Whales have probably, as Horsburgh remarks, been taken for rocks. These fish float at the surface for a long time together, and, being covered with barnacles, grass, or seaweed, exhibit an

* The sea is stated to have broken in 40 fathoms on the coast of Syria, in the gale of Dec. 1840 (Naut. Mag. 1841, p. 233).

appearance so like that of a rock that it is often difficult to believe the contrary.*

1047. The sound of breakers or surf has often been found to be caused by a shoal of fish. Kerguelen (*Relation d'un Voyage dans la Mer du Nord*, 1767-8, Paris, 1770, p. 121) saw a large shoal of small red fish that had the appearance of a sandbank, of the extent of two leagues, on which the sea was breaking, and the illusion was rendered the more complete by the great numbers of birds that accompanied it. Capt. Fitz Roy observes, that a shoal of fish seen under the water may have given rise to a report of a bank, which it much resembles. Weddell records having been alarmed in a fog by a cry of breakers, for which a noise produced by fish was taken. Most seamen's experience will supply similar instances.†

It has been remarked that it is very difficult at a distance to distinguish straggling ice and breakers from each other.

1048. A sound like that of guns is produced by the splitting of large masses of ice. Cook records an instance (*1st Voyage*, p. 47), and it is familiar to those who have been in the polar regions.

1049. The surface of the sea, in some parts of the world, is occasionally found streaked, for leagues together, by a matter which produces the "discoloured" aspect of shoal water, and which sailors suppose to be the spawn of fish. Water having this appearance is not approached without anxiety by those who are unaccustomed to it; and in those seas especially where coral reefs rise perpendicularly from very great depths, an increase of vigilance is demanded on such occasions.‡

1050. In these days, when the ocean is traversed by innumerable ships, appearances which were strange or alarming to the first navigators have become familiar; and the dangers which the enterprising men who first ventured upon an unknown sea were naturally disposed to multiply have disappeared from our charts. But in earlier times, when the solitary vessel had either no chart at all, or one put together from imperfect or incongruous materials, the feeble state of navigation justified the excess of caution in reporting as a danger every suspicious appearance.

Accounts, therefore, of new land or dangers, which are published from time to time, are not to be received without extreme caution, unless they state some circumstance which is decisive.

* Sir F. Beaufort tells me, that in approaching the River Plate, in command of H.M.S. *Woolwich*, a whale was reported as a rock, and believed to be so by every one on board. But knowing that no rock existed in the situation, he steered direct for it, and when about 30 yards distant it dived. In H.M.S. *Tyne*, in the South Pacific, we bore up for what seemed to be the wreck of a ship floating, with her quarter raised out of the sea, but which, on approaching it, turned out to be a whale.

† To these or other circumstances, which have given rise to reports of shoals, may perhaps be added the shocks which have been experienced by ships striking against whales or other large fish.

‡ In the *Alceste*, while among imperfectly known parts of the Eastern Seas, we frequently passed through water thus tinged with some colouring matter. Mr. Darwin (*Voyages of the Adventure and Beagle*, vol. iii.) considers the effect to be produced by animalculæ.

3. *Dangers.*

1051. When the ship, going free, is found to be running into danger, the proper tack to haul to the wind upon is, generally speaking, that on which she will most rapidly increase her distance from it, because thus time will be gained.

1052. In high latitudes ice islands are often met with towards the close of the summer, or earlier. The presence of ice at night is often indicated by a peculiar effect of light, and in fog by a kind of blackness in the atmosphere (Scoresby's *Arctic Regions*, p. 255).

On falling in with ice the ship is recommended to pass to windward of it. It is observed that the smaller portions drift more quickly than larger ones, and that pieces of a round figure drift nearly before the wind, while angular pieces move irregularly.

Ice islands have been met with to the southward of the parallel of 50° N., in the Atlantic, and in the Southern Ocean in 36° S. The Captain of the *s.s. Forfarshire* reports that, in Jan. 1891 icebergs were met with in the following localities:—From lat. 51° 30' S. to 49° 50' S., and long. 46° 0' W., sixty-three icebergs, half a mile to 3 miles long, and 200 to 300 feet high, were seen. Also an ice island, estimated to be over 30 miles in length and 300 to 400 feet high, was passed at the distance of about 5 miles.

From reports received there is reason to believe that icebergs may often be found in the positions given, and mariners are warned to give the localities a wide berth. See Admiralty Ice Chart, No. 1241; also Wind and Current Charts.

A remarkable diminution in the strength of the wind is experienced when to leeward of ice, even of very small extent. This is noticed by Sir E. Parry and by other navigators.

1053. There is also another source of danger, which appears to have increased of late years, and one less easily guarded against, in vessels which have been abandoned by their crews, in some cases unnecessarily, and which, having become more or less waterlogged, remain drifting about.

1054. To these may be added *rollers*, which term is applied to a very heavy swell rising on particular coasts, without any known cause, generally very quickly, and subsiding very soon, and which constitutes a formidable danger. H.M.S. *Julia* was wrecked in a calm at Tristan d'Acunha in a few minutes. More recently very severe loss was experienced at St. Helena. Rollers are noticed as a great danger on the coast of Guiana, where they break in 5 or 6 fathoms (Commander Darley in *Naut. Mag.* 1844, p. 649). The U. S. Expl. Expd. anchored off St. Francisco Nov. 1, 1841, the *Vincennes* being in 7 fathoms, and 3 miles off shore. About 10 P.M. the rollers got up and broke with the continued roar of a surf. At midnight a sea broke heavily on board the *Vincennes*, a ship of 780 tons, displaced the booms and boats, and killed a man. The other ships, in deeper water, felt no inconvenience.*

* Though great danger is incurred from breakers in shoal water, yet there are coasts on which the gradual shelving of the bottom dissipates the swell by degrees without causing a

4. *Determination of Position or Danger.*

1055. *Out of Sight of Land.*—When a rock, a shoal, or an island, is unexpectedly met with at sea, its bearing and estimated distance are to be noted, with the time by chronometer. As the true position can be determined by astronomical observation alone, the following directions are inserted for reference, the calculations being deferred to a convenient time.

(1.) When the *sun* is visible. Observe his altitude, noting the time by chronometer (see the note, No. 726). This gives the lat., Nos. 681, 696, or 718, or the time, No. 776, or 791, and thence the long. by chronometer.

(2.) When the *sun and moon* are visible. Observe both alts. with all possible care, and the lunar distance; the lat. is hence found, Nos. 681 or 692, 696 or 703, or 759, &c., and thence the time, and the long. by chron. or by lunar.

(3.) When the *moon* is visible. See Nos. 692, 703. In favourable cases the alt. gives the long., No. 864.

(4.) When the *moon and stars* are visible. Obtain the lunar distance, and both alts. with care. See, also, Nos. 864 and 866.

(5.) When the *stars* alone are visible. Observe altitudes near the meridian, and on opposite sides of the zenith, for lat.; and near the prime vertical for time and long. by chron.

Of the dangers to which navigation is exposed none is more formidable than a reef or a shoal in the open sea; not only from the almost certain fate of the ship and her crew that have the misfortune to strike upon it, but also from the anxiety with which the navigation of all vessels, within even a long distance, must be conducted, on account of the uncertainty to which their own reckonings are ever open. No commander of a vessel, therefore, who might meet unexpectedly with any such danger, could be excused, except by urgent circumstances, from taking the necessary steps both for ascertaining its true position, and for giving a description as complete as a prudent regard to his own safety allowed.

1056. *In Sight of Land.* The position of a rock or a shoal may be determined by cross-bearings (No. 366) when the variation and deviation are known. It may be determined more accurately by taking the bearings of three objects, and using the angle between the bearings (No. 368). The sextant may be used, in preference to the compass, for convenience and accuracy; the face should be held horizontal, and the angles measured between points vertically under the objects, or determined by plumb-lines conceived to pass through the objects. No. 368.

[1.] *Report of New Discovery, or Correction of Position.*

1057. In transmitting an account of a new discovery, or the correction of a position, the first consideration is the lat. or long., or

dangerous break. On the coast of Barbary, in H.M.S. Adventure, under the command of Capt. W. H. Smyth, we frequently, when the wind was dead on shore, ran to leeward out of the sea, till we found a convenient depth of water for anchoring.

the situation with respect to some other place. Attention should therefore be directed to the instructions at No. 835. It will, indeed, be evident on a moment's reflection, that the long. described merely, as is too often the case, as "long. by chron." without reference to some fixed point, is utterly valueless. Again, when such fixed point is mentioned, it is no less necessary to note the long. adopted: for ex.: "Long. by chron. from Callao," is little better than no allusion to place at all, as Callao appears in the tables in different longgs. from $77^{\circ} 10.5'$ to $77^{\circ} 15.7'$.

When the determination depends on a lunar, notice should be taken, 1. of the skill of the observer; 2. of the instrument; and especially whether distances on opposite sides of the moon are observed; also, 3. of the probable error of the time.

1058. After the position the point next in importance is the *extent*, and general direction, if this can be assigned. Then follows height or depth, with notice of the appearance; and then anchorage, landing, supplies, and natives. The seaman will find these matters of detail passed in review, in the same constant order, in the symbolised descriptions in Table 10; and he may render much service by taking the opportunity of recording these particulars on passing any of the numerous places of which we have no very exact accounts.*

It will often be important to notice both the extent and appearance of islands, which have not been visited for a long time. Krusenstern, in alluding to the growth of many islands by submarine formations, which are continually extending themselves, as established by Fleurieu, Flinders, and Beechey, remarks that Capt. Carteret discovered a small flat island so nearly at the level of the sea, as scarcely to deserve the name of an island, which he called *Osnaburgh*. It was on this island that the *Matilda* was wrecked in 1792, as is proved by the agreement of her observations with those of Adm. Beechey, who found here the wreck of a ship. Thus the "small island" had, in 1827, an extent of 14 miles (*Mém. Hydr.* 1835, p. 94).

Again, in warm climates, reefs at the level of the sea are covered by degrees with a low vegetation, which, in due time, is succeeded by trees. Many places, therefore, now known merely as reefs, or not noticed at all, will probably become hereafter conspicuous islands.

1059. Whenever a position is noted, the bearings of headlands and islands should be observed as accurately as possible. The neglect of this is seriously felt in the arrangement of positions.†

Seamen may also supply very important elements for correcting

* If, in sending home such accounts, the writer uses symbols, he must be very careful to draw them in their perfect form, lest one may be taken for another. The great saving of time and space which they effect claims the necessary attention in writing them legibly.

† In the third and later editions of this work a discrepancy was admitted in the positions of Tanna, Annatom, and Erronan, from the want of bearings, though the places are in sight of each other. Capt. Denham, of H.M.S. *Torch*, removed the difficulty.

the charts by observing with care the bearing of two points of land when seen in a line, or *on with each other*, or of a summit seen over a point. Such bearings are called *transit bearings*.

1060. Views should accompany all hydrographic notices, when there is any one on board who can draw. On these should be marked one or more bearings (selecting, first, that of the nearest point), and the angles measured by a sextant between remarkable points or other objects; also the angular elevations of summits, as these last serve for the determination of heights.

It is also important, where the range is considerable, to note the time of tide, because the rise or fall of several feet in the water may cause a material change in the appearance of the shore, and has also the effect of altering the apparent dimensions of an island with shelving shores. Again, when the spectator is on shore, the place of the visible horizon varies with the height of the tide, being nearer to him and higher, when the water is higher (or when he is less elevated above it), and further off and lower, as the water falls (or as he increases his relative height). The consequence of this is, that an island beyond the visible horizon appears to the spectator on shore to be of different lengths at different times of the tide.

A small pamphlet entitled "Notes bearing on the Navigation of H.M. Ships," lately issued by the Admiralty, will be found to contain much practical and useful information.

EXPLANATION OF THE TABLES.

IN this division of the work the use and application, and, in some degree, the construction, of the Tables, are described.

Rules are given for computing the terms in the Tables. These rules will be found useful for the purpose of verification; for the computation of an intermediate term instead of the ordinary interpolation; and also when the computer may require, for a particular object, to employ a table on a more extensive scale than would be convenient for the general purposes of the collection.

NAVIGATION *

THE SAILINGS.

These tables are used chiefly in the methods, Chapter III.

TABLE 1.

This is called the TRAVERSE TABLE from its use in Traverse Sailing.

1. *Direct Application.*

Table 1 contains the Diff. Lat. and Dep. for the Course at every degree, and for each mile of distance to 600 miles, with the time corresponding to each degree.

When the Course is given in points, it should be turned into degrees (No. 216). If it is less than 4 points or 45° , the table is to be entered at the top; but from the bottom when it exceeds 4 points or 45° .

Ex. 1. Course $2\frac{1}{2}$ pts., Dist. 74 miles; find the D. Lat. and Dep.

In Table 1, at $28^\circ = 2\frac{1}{2}$ points, and against 74 in the Dist. column, are D. Lat. 65.3 , and Dep. 34.7 .

Ex. 2. Course 68° , Dist. 241 miles; find the D. Lat. and Dep.

In Table 1, over 68° at the bottom, and against 241, are D. Lat. 90.3 , and Dep. 223.5 .

* The general division of the subject into Navigation and Nautical Astronomy naturally suggests the like division among the Tables. But, besides this, the computer cannot, in general, make proper use of the Astronomical Tables unless acquainted beforehand with his position on the globe. The Tables, therefore, relating to this last point, that is, those which are concerned in finding the position of the ship with reference to the place left, necessarily precede the others. The Table of Positions, which is usually found at the end of a collection of tables, is, according to this disposition, placed among those relating to Departures, since in actual navigation it is referred to only with reference to the place of the ship.

The author is indebted to many individuals whose opinions are entitled to every consideration for suggestions relative to the arrangement or order. It will, however, be obvious that no arrangement can be devised which shall be equally convenient for all persons at all times; and, perhaps, no plan is open to fewer objections of weight than one in which regard is paid both to the classification of subjects and to the successive stages of the computations.

In like manner, in taking out the Course corresponding to a given D. Lat. and Dep., when the D. Lat. is greater than the Dep., take the Course from the top; when less, from the bottom.

(1.) To take out the D. Lat. or Dep. to a fraction of a degree.

Ex. To find the Dep. to $11^{\circ}\frac{1}{4}$ and Dist. 100.

The Dep. to 11° is 19.1, that to 12° is 20.8; $\frac{1}{4}$ of the difference 1.7, or .4, added to 19.1 gives 19.5, the Dep. required.

In finding the D. Lat. this prop. part is subtractive.

(2.) To find the D. Lat. or Dep. for a fractional Dist., as, for example, for 59.3; find it for 59, and then for 3 (dividing the last by 10).

(3.) When the given Dist. exceeds 600 miles, divide it by 10, and multiply the D. Lat. and Dep. found by 10. So, likewise, when the given D. Lat. or Dep. exceeds the limits of the Table, divide it by 10, and multiply the resulting Dist. by 10.

Ex. 1. Course 31° , Dist. 1872 miles. The Course 31° , and Dist. 187, give D. Lat. 160.3, and Dep. 96.3; hence the required D. Lat. and Dep. are 1603 and 963 nearly.

Ex. 2. D. Lat. 660, and Dep. 165, to find the Course and Dist. D. Lat. 66, and Dep. 16.5, give Course 14° , and Dist. 68; the required Dist. is, therefore, 680 nearly.

This is near enough in general. For greater accuracy, in Example 1, take out the D. Lat. or Dep. for 600, and for the excess above 600.

2. Trigonometrical Quantities.

If the angle ACB, fig., No. 162, be considered the Course, and AC the Distance, then AB becomes the Dep. and CB the D. Lat.

Hence, by No. 162, the Dep. corresponding to the Dist. 100 is the *sine* for the radius 100.

The D. Lat. to the Dist. 100 is the *cosine* for the radius 100.

In like manner, the Dep. to the D. Lat. 100 is the *tangent* for the radius 100.

The Dist. to the D. Lat. 100 is the *secant* to the radius 100.

Thus also the D. Lat. to the Dep. 100 is the *cotangent*; and the Dist. to the Dep. 100 is the *cosecant* to the same radius 100.

The trigonometrical quantities (which are calculated for radius 1) are deduced from the numbers thus found in the Traverse Table by marking off two decimals.

Ex. 1. Find the Sine of 27° . At the arc 27° , the Dist. 100 gives the Dep. 45.4. The SINE is, therefore, .454, the log. of which is 9.657 (Nos. 58 (2) and 59, p. 19). This is the log. given in Table 68.

Ex. 2. Find the Cosine of 56° . At 56° , the D. Lat. to the Dist. 100 is 55.9, the COSINE is .559, the log. of which is 9.747.

Ex. 3. Find the Tangent of 38° . At 38° , the D. Lat. 100 corresponds to Dep. 78.2, the TANGENT is .782, the log. of which is 9.893.

Ex. 4. Find the Secant of 42° . At 42° , the D. Lat. 100 corresponds to the Dist. 134.6, the SECANT is 1.346, the log. of which is 0.129, or in Table 68, 10.129 (No. 166, Note).

Ex. 5. Find the Cotangent of 54° . At 54° , the Dep. 100 corresponds to D. Lat. 72.7 the COTANG. is .727, the log. of which is 9.861.

Ex. 6. Find the Cosec. of 18° . At 18° , the Dep. 100 corresponds to Dist. 323.4, the COSEC. is 3.234, the log. of which is 0.510.

[1.] Solution of Right-Angled Triangles.

These tables are useful in solving approximately cases of right-angled triangles, as also in roughly verifying the results of questions of the kind when obtained by logarithms.

Ex. p. 48. Angle A 50° , CA 28 feet, find AB and BC.

At 50° , the Dist. 28 gives the D. Lat. 18, which is AB, and the Dep. $21'4$, or CB.

Ex. p. 49, Case II. Angle A 30° , BC 171; find AB and AC.

Course 30° and Dep. $85'5$ give Dist. 171, or BC 342, and D. Lat. $148'1$, or AC $296'2$.

Ex. p. 49, Case III. AB 220'3, AC 101'9; find the Angle B and BC.

Dist. 220 and Dep. $103'3$ are the nearest, and give 28° for the Angle B, and the D. Lat. or BC 194.

8. Proportional Quantities.

Mr. A. C. Johnson, R.N., in his valuable pamphlet on "Finding Latitude and Longitude in Cloudy Weather,"* has shown how Table I. may be used to correct the Longitude for error in Latitude.

With the complement of the object's bearing at sights as a course, and error in Latitude as a Diff. Lat., take out Dep. This converted into Diff. Long. will be the correction required.

East: When the true latitude is South of the approximate, and azimuth of object between N. and E., or between S. and W.

Or when the true latitude is North of the approximate, and azimuth of object between S. and E., or between N. and W.

West: When the true latitude is South of the approximate, and azimuth of object between S. and E., or between N. and W.

Or when the true latitude is North of the approximate, and azimuth of object between N. and E., or between S. and W.

Ex. In Lat. 45° S., sun bearing S. 55° W., ship by observation was in long. $3^\circ45'$ W., but the error in lat. was found to be 18 m. South.

Complement of Azimuth 35° . Then Course 35° and Diff. Lat. 18' give Dep. $12'6$. Dep. $12'6$ and Lat. 45° give Diff. Long. 18'. True lat. South of approximate, and azimuth between S. and E., and correction is E.

Long. from Observation	$3^\circ45'$ W.
Correction	$18'$ E.
True Long	$3^\circ27'$ W.

* Published by J. D. Potter, Agent for Admiralty Charts, 145 Minories.

[To face p. 378.

(1.) To turn *statute miles* into *nautical* or *geographical miles*.

1 statute mile = 0.8684 geogr. 1 geogr. mile = 1.1515 statute miles.
At 61° , the Dist. and Dep. correspond to *statute* and *geogr.* miles.

(2.) To turn *feet per second* into *nautical miles per hour*.

At 36° , the Dist. and Dep. correspond to *feet* and *miles*; thus the rate of 19 feet per second is 11 miles an hour, nearly.

The measures and soundings on foreign charts are reduced, in like manner, to our own scales.

(1.) To turn *Danish Favne* into *English Fathoms*.

1 fav. = 1·0292 fath. 1 fath. = 0·9716 fav.

At 76°, the Dist. and Dep. correspond to *fathoms* and *favne*; thus, 100 favne are 103 fath. nearly.(2.) To turn *Danish Feet* into *English Feet*.1 Dan. foot (*foð*) = 1·0270 Eng. feet. 1 Eng. foot = 0·9737 Dan. ft.At 77°, the Dist. and Dep. correspond to *English* and *Danish feet*; thus, 200 Danish feet are 205 English feet nearly.(3.) To turn *Dutch (Amsterdam) Feet* into *English Feet*.

1 Amst. foot = 0·9287 Eng. ft. 1 Eng. foot = 1·077 Amst. ft.

At 68°, the Dist. and Dep. correspond to *Dutch* and *English feet*. Thus, 300 Dutch feet are 278·2 English feet nearly.(4.) To turn *Dutch Palms* into *English Feet*.

1 palm = 0·3283 ft. 1 foot = 3·046 palms.

At 19°, Dist. and Dep. correspond to *palms* and *feet*. Thus, 100 palms are 32·6, or more nearly, 32·8 feet.(5.) To turn *French Brasses* into *English Fathoms*.

1 brass = 0·888 fath. 1 fath. = 1·126 brass.

At 62°, the Dist. and Dep. correspond to *brasses* and *fathoms*. Add 1 in 180. Thus 200 brasses are 176·6, or more nearly 177·6 fathoms.(6.) To turn *French Metres* into *English Yards*.*

1 metre = 1·0936 yard. 1 yard = 0·9144 metre.

At 66°, the Dist. and Dep. correspond to *yards* and *metres*. Thus, 300 yards are 274·1 metres nearly.(7.) To turn *French Feet (Pieds)* into *English Feet*.

1 pied = 1·0658 ft. 1 foot = 0·9383 pied.

At 70°, the Dist. and Dep. correspond to *pieds* and *feet*. Thus, 200 *pieds* are 213 feet nearly.(8.) To turn *French Toises* into *English Fathoms*.

1 toise = 1·0658 fath. 1 fath. = 0·9383 toise.

At 70°, the Dist. and Dep. correspond to *toises* and *fathoms*. Thus, 200 toises are 213 fathoms nearly.(9.) For the *Prussian Foot (Fuss)*, see *Danish*.(10.) To turn *Russian Arsheens* into *English Feet*.

1 arsh. = 2·3343 ft. 1 foot = 0·4284 arsh.

At 25°, the Dist. and Dep. correspond to *feet* and *arsheens*. Deduct 1 in 60. Thus 86 arsheens are 203 feet, or more nearly 200 feet.(11.) To turn *Russian Sashes (Sazhens)* into *English Fathoms*.

1 sazhen = 1·1671 fath. 1 fath. = 0·8568 sazhen.

At 59°, the Dist. and Dep. correspond to *fathoms* and *sashes*. Thus, 300 fathoms are 257·1 sashens. Thus, the arsh. = 28 in.; the sazhen = 7 f., and the verst (12) = 500 sashens.

* The following French measures occur frequently:—

1 Myriametre	= 10,000 metres.	Metre	= 39·37079 Eng. in
1 Kilometre	= 1000	Decimetre	= 1·10th met. = 3·937079
1 Hectometre	= 100	Centimetre	= 1·100th met. = 0·393708
1 Decametre	= 10	Millimetre	= 1·1000th met. = 0·039371

To turn *Russian Versts* into *Nautical Miles*.

1 verst = 0.5759 mile. 1 mile = 1.7364 verst.

At 35°, the Dist. and Dep. correspond to *versts* and *miles*. Add 1 in 260. Thus, 300 versts are 172.1, or more nearly (adding .6) 172.7 miles.

(13.) To turn *Spanish Brazas* into *English Fathoms*.

1 braza = 0.915 fath. 1 fath. = 1.092 bras.

At 66°, the Dist. and Dep. correspond to *brasas* and *fathoms*. Thus, 200 brasas are 183 fathoms nearly.

(14.) To turn *Spanish Varas* into *Yards*

1 vara = 0.9142 yard. 1 yard = 1.0964 var.

At 66°, the Dist. and Dep. correspond to *varas* and *yards*. Thus, 300 varas are 274.3 yards.

(15.) To turn *Swedish Feet* into *English Feet*.1 Swed. foot (*fed*) = 0.9739 Eng. foot. 1 Eng. foot = 1.0268 Swed. foot.

At 77°, the Dist. and Dep. correspond to *Swedish* and *English feet*. Thus, 300 Swedish feet are 292.3 English feet.

To compute a Term. For the D. Lat. To the log. of the Dist. add the log cos. of the Course; the sum is the log. of the D. Lat

For the Dep. To the log. of the Dist. add the log. sine of the Course; the sum is the log. of the Dep.

TABLE 3. DEPARTURE AND CORRESPONDING DIFFERENCE OF LONGITUDE

This Table shews the number of minutes of Longitude in any number of nautical miles from 1 to 10, measured E. and W., in lats. under 70°.

Ex. 1. Lat. 49°, Dep. 27m.; find the D. Long.			Ex. 2. Lat. 31° 30', Dep. 8.7m.; find the D. Long.		
49°	20 (2 × 10)	30.48	31°½	8	9.38
	7	10.67		0.7	0.82
	D. Long.	41.15		D. Long.	10.20

In general, interpolation for any fraction of a degree may be effected nearly enough at sight, as in Ex. 2; but when accuracy is required, find the D. Long. for the two whole degrees, including the fractional lat., take the diff. of the two results, and with it enter the col. headed D to 1°, take out the parts and *add* them.

The Table may often be useful in parallel and mid. lat. sailing; though, to be properly adapted to this purpose, it should be greatly extended. Its chief utility lies in the reduction or comparison of longitudes in plans not graduated.

To compute a term. To the log. of the Dep. add the log. sec of the Lat.; the sum (rejecting 10) is the log. of the D. Long.

TABLE 4 DIFFERENCE OF LONGITUDE AND CORRESPONDING DEPARTURE

This Table shews the number of nautical miles in any number of minutes of longitude from 1 to 10, in lats under 70°

Ex. 1. Lat. 64° , D. Long. $272'$; find the Dep.				Ex. 2. Lat. $22^{\circ}\frac{1}{2}$, D. Long. $4^{\circ}6'$; find the Dep.			
64° ,	200	88.0	$22^{\circ}, 4$	$3^{\circ}71$	3 71
	70	30.7	23,	$3^{\circ}68$	
	2	0.9			D. to $1^{\circ}0'03$, for $30'$...	— .02
Dep.			<u>119.6</u>				<u>3.69</u>
				$22\frac{1}{2} 0.6$		<u>4.25</u>
						Dep.	4.25

The remarks on Table 3 apply to Table 4, except that the parts for the fraction of a degree arc to be *subtracted*.

To compute a term. To the log. of the D. Long. add the log cos of the Lat.; the sum (rejecting 10) is the log. of the Dep

TABLE 5. SPHERICAL TRAVERSE TABLE

This Table is named from its being used with the common or plane Traverse Table, in cases which involve Spherical Trigonometry.

The Table is entered with the *lesser* of two given arcs or angles at the top, and the other at the side; thus, to take out M and N for 64° and 15° , enter with 15° at the top and 64° at the side, then M is found 236.2, and N 54.9 *

Interpolation for a fraction of a degree is easy, because M and N always increase. In general, it is enough to take M or N at sight, as directed No. 19; thus, for ex., to find M for $59^{\circ}47'$ and $66^{\circ}18'$, that is, for $59\frac{1}{2}$ and $66\frac{1}{2}$, we may take 496.

For greater precision, take the differences between each two terms concerned, and proceed to proportion separately for each.

The Table solves by inspection, approximately only, but very expeditiously, several problems. This method, besides being near enough for many practical purposes, will often be useful as a check against mistakes in longer methods.

(1.) To find the Hour-angle from the alt. No. 618.

With the lat. and decl. find M and N. With the alt. as Course, and M as Dist. find the Dep.

When the lat. and decl. are of *contrary* names, take the *sum* of the Dep. and N. The course answering to this sum as D. Lat. and Dist. 100 is the Hour-angle required.

When the lat. and decl. are of the *same* name, take the *diff.* of the Dep. and N. When the Dep. *exceeds* N, the course answering to this Diff. as D. Lat. and Dist. 100 is the Hour-angle; but when the Dep. is *less* than N, the supplement of the said course is the Hour-angle.

Ex. 1. Lat. $15^{\circ}32'$ N., decl. $8^{\circ}35'$ S., alt. $15^{\circ}26'$: required the Hour-angle.				Ex. 2. Lat. $51^{\circ}10'$ S., decl. $19^{\circ}27'$ N. alt. $11^{\circ}51'$: required the Hour-angle.			
$15^{\circ}\frac{1}{2}$ and $8^{\circ}\frac{1}{2}$,	M	104.9,	N 4.1	$19^{\circ}\frac{1}{2}$ and 51° ,	M	168.6,	N 44.7
$15^{\circ}\frac{1}{2}$ (alt.) and 105,		Dep.	28.0	$11^{\circ}\frac{1}{2}$ and 169,		Dep.	34.4
	(sum)		32.1		(sum)		79.1
Hour-angle, $4^{\text{h}}44^{\text{m}}$.				Hour-angle, $2^{\text{h}}31^{\text{m}}$.			

* It will be perceived, on inspecting the examples, that after M and N are taken out to the given arcs, the arithmetical process is very similar in all the problems; very little practice will, therefore, render the several uses of the Table familiar. As the process of computation consists in the addition or subtraction of two numbers only, thus taken out by inspection, it will be difficult, if not impossible, to find general solutions more concise. As M is always greater than N, they can never be confounded together.

It is because the Dep. always *increases* with the course, that it is used in preference to the D. Lat. in the solutions by this Table, the rules being adapted accordingly

Ex. 3. Lat. $56^{\circ} 50' S.$, decl. $56^{\circ} 10' S.$,
alt. $64^{\circ} 47'$; required the Hour-angle.

57° and 56° , M 328.3 , N 228.3
 65° and 328 , Dep. 297.3
(diff.) 69.0

Hour-angle, $3^h 5^m$ (since the Dep. exceeds N).

Ex 4. Lat. $47^{\circ} 3' N.$, decl. $22^{\circ} 37' N.$
alt. $8^{\circ} 20'$; required the Hour-angle.

47° and $22^{\circ} \frac{1}{2}$, M 158.7 , N 44.4
 $8^{\circ} \frac{1}{2}$ and 159 , Dep. 23.0
(diff.) 21.4

Course, $5^h 11^m$; or Hour-angle, $6^h 49^m$
(since the Dep. is less than N).

When the lat. or the decl. is 0, N is 0, and the Dep. is to be taken as the D. Lat. to 100; the Course corresponding is the Hour-angle required.

Ex. 5. Lat. 0° , decl. $14^{\circ} N.$ or $S.$, alt.
 27° ; required the Hour-angle.

0 and 14° , M 103.1
 27° and 103 , Dep. 46.8
Hour-angle, $4^h 8^m$.

Ex. 6. Lat. $38^{\circ} N.$ or $S.$, decl. 0° , alt.
 27° ; required the Hour-angle.

0° and 38° , M 126.9
 27° and 127 , Dep. 57.7
Hour-angle, $3^h 40^m$.

(2.) To find the Hour-angle on the Prime Vertical, No. 618.

With the decl. and colat. find N; with 100 as Dist. and N as D. Lat. find the Course.

Ex. Lat. 31° , decl. 14° . 14° and 59° give N. 41.5 ; 100 Dist. and 41.5 D. Lat. give Hour-angle $4^h 22^m$.

(3.) To find the Hour-angle at rising and setting, No. 620.

With the lat. and decl. take out N. With the Dist. 100 and N as D. Lat. find the Course.

When the lat. and decl. are of *contrary* names, this is the Hour-angle required; when of the *same* name, take the *suppl.* to 12 hours.

Ex. 1. Lat. $51^{\circ} N.$, decl. $27^{\circ} N.$: find
the Hour-angle at rising or setting.

27° and 51° give N 62.9

Dist. 100 and D. Lat. 62.9 give Course
 $3^h 24^m$, and the Hour-angle required $8^h 36^m$.

Ex. 2. Lat. $31^{\circ} N.$, decl. $40^{\circ} S.$: find
the Hour-angle at rising or setting.

31° and 40° give N 50.4

100 and 50.4 give 4^h , the Hour-angle
required.

(4.) To find the effect of Refraction, &c. on the above, No. 638.

With the lat. and decl. take out M. With M as Dep. and the Hour-angle at rising or setting as Course, take out the Dist. Multiply this Dist. by the sum of $34'$ and the depression to the height, Table 8; the product divided by 1500 is the portion of time required in min. and decimals.

Ex. 1, No. 638. Lat. 28° and Decl. 16° give M 117.8 . Then Lat. $28^{\circ} N.$ and Decl. $16^{\circ} N.$ give Hour-angle at setting, $6^h 35^m$. The suppl. of this, as it exceeds 6^h , or $5^h 25^m$ as Course, and Dep. 117.8 , give Dist. 119 .

Dist. 119 mult. by $34 + 117$, or 151 , is 17969 ; which, \div by 1500 , gives $11^m.9$.

(5.) To find the Time of Twilight, No. 641.

With the lat. and the sun's decl. find M and N. With the Course 18° and the Dist. M find the departure.

When the lat. and decl. are of *same* name, *add* this dep. to N; the Course corresponding to the sum as D. Lat. and Dist. 100 is the A. T. of the beginning of twilight, A.M.

When the lat. and decl. are of *contrary* names, take the diff. between the above Dep. and N; the Course corresponding to this diff. as D. Lat. and Dist. 100 is the time twilight *begins*, A.M., when the Dep. is *greater* than N; and the time it *ends*, P.M., when the Dep. is *less* than N.

Each of these times is the supplement of the other to 12^h .

Ex. Lat. 30° N., sun's decl. 20° N.: required Beginning and End of Twilight.

20° and 30° give M 122.9 and N 21. Course 18° and Dist. 123 give Dep. 38 (greater), same name) sum 59. Dist. 100 and D. Lat. 59 give Course $3^h 56^m$, the time it Begins A.M.; hence it Ends at $8^h 24^m$ P.M.

(6.) To find the altitude on the Prime Vertical, No. 664.

With 0 and the colat. find M. With the decl. as Course and M as Dist. find the Dep. With Dist. 100 and this Dep. find the Course.

Ex. Lat. 52° , Decl. 22° . 0 and 38° give M 126.9, 22° and Dist. 127 give Dep. 47.6. Dist. 100 and 47.6 give Course or ALT. $28^{\circ} \frac{1}{2}$.

Ex. 3, No. 665 (worked to the nearest degree), gives Dep. 100, equal to the Dist. which means that the Alt. is 90° , or it is an extreme case.

(7.) To find the Altitude, the Hour-angle being given, No. 666.

With the lat. and decl. take out M and N. With the compl. of the hour-angle to 6^h as a Course, and Dist. 100, find the Dep.

When the lat. and decl. are of *contrary* names, take the *diff.* of this Dep. and N. When the lat. and decl. are of the *same* name; if the hour-angle is *less* than 6^h , take the *sum* of the Dep. and N; if *greater* than 6^h , take the *diff.*

With this sum, or diff., as Dep. and M as Dist. find the Course, which is the alt. required.

Ex. 1. Lat. $15^{\circ} 32' N.$, decl. $8^{\circ} 35' S.$, Hour-angle, $4^h 45^m$: required the Alt.

$8^{\circ} \frac{1}{2}$ and $15^{\circ} \frac{1}{2}$, M 104.9, N 4.1
 $1^h 15^m$ and Dist. 100 Dep. 32.2
 (cont. name), *diff.* 28.1

Dist. 105 and Dep. 28.1 give Co. $15^{\circ} \frac{1}{2}$ the ALT.

Ex. 2. Lat. $47^{\circ} 3' N.$, decl. $22^{\circ} 37' N.$, Hour-angle, $6^h 50^m$.

$22^{\circ} \frac{1}{2}$ and 47° , M 158.7, N 44.4
 $0^h 50^m$ and 100 Dep. 21.6
 (*diff.*) 22.8

159 and Dep. 22.8 give ALT. 8° .

Ex. 3. Lat. $56^{\circ} 50' N.$, decl. $56^{\circ} 10' N.$, Hour-angle, $3^h 5^m$.

56° and 57° , M 328.3, N 228.3
 $2^h 55^m$ and 100. Dep. 69.0
 (sum) 297.3

164.1 and 148.6 give ALT. 65° .

Ex. 4. Lat. $22^{\circ} S.$, decl. $3^{\circ} N.$, Hour-angle, $2^h 15^m$.

3° and 12° , M 108.0, N 2.1
 $3^h 45^m$ Dep. 82.9
 (*diff.*) 80.8

ALT. 49° .

When the lat. or decl. is 0, N is 0, and the Dep. taken as Dep., with M as Dist. gives the course. When both lat. and decl. are 0, the alt. is the compl. of the hour-angle in arc.

(8.) To find the Azimuth, the Altitude being given, No. 673.

With the lat. and alt. take out M and N. With the decl. as course, and M as Dist., find the Dep.

When the lat. and decl. are of *contrary* names, take the *sum* of this Dep. and N; when of the *same* name, their *difference*.

With the dist. 100, and this sum or diff. as D. Lat., find the course, which is the azimuth required.

When the lat. and decl. are of *contrary* names, this azimuth is to be reckoned from the S. in N. lat. and from the N. in S. lat. When they are of the *same* name,—when the Dep. is *less* than N, reckon the azimuth from the S. in N. lat., and from the N. in S. lat.; when the dep. is *greater* than N, reckon the azimuth from the elevated pole, or from the N. in N. lat.

The azimuth is reckoned E. or W. as the celestial body is to the E. or W. of the merid. at the time proposed.

Ex. 1. Lat. 10° S., alt. $58^{\circ} 40'$ to E-d.,
decl. $14^{\circ} 24'$ N. (*contrary names*).

10° and $58^{\circ} \frac{2}{3}$ M 195.8 N 29.0

$14^{\circ} \frac{1}{2}$ and 196 Dep. 49.0

(sum) 78.0

100 and D. Lat. 78.0 give $39^{\circ} \frac{1}{4}$, the
As.M. req., which (in S. lat.) is N. $39^{\circ} \frac{1}{4}$ E.

Ex. 2. Lat. $51^{\circ} 30'$ N., alt. of Arcturus
 $40^{\circ} 25'$ to W-d., decl. $20^{\circ} 2'$ N. (*same name*).

$51^{\circ} \frac{1}{2}$ and $40^{\circ} \frac{1}{2}$ M 211.2 N 107.3

20° and 211 Dep. 72.2

(diff.) 35.1

100 and D. Lat. 35.1 give $69^{\circ} \frac{1}{4}$, or As.M.
req., S. $69^{\circ} \frac{1}{4}$ W., as the Dep. is the *lesser*

When the Lat. is 0, N is 0, and the Dep. itself becomes the D. Lat., which, with Dist. 100, gives the Course.

When the Declin. is 0, the Dep. is 0, and N becomes the D. Lat., which, with Dist. 100, gives the Course.

Ex. 3. Lat. 0, declin. 21° N., alt. 61° .

Lat. 0 and 61 M 206.3 N 0

21 and 206.3 Dep. 73.8

100 and D. Lat. 73.8 give $42^{\circ} \frac{1}{2}$, the
AZIMUTH.

Ex. 4. Lat. 48° S., decl. 0, alt. 34° .

48° and 34° M 180.3 N 74.9

0 and 180.3 Dep. 0

100 and 74.9 give Course $41^{\circ} \frac{1}{2}$, the
AZIMUTH.

To compute *M* and *N*.* For *M*, add together the log. secants of the given arcs, add 2 to the index, and reject the tens; the sum is the log. of *M*. For *N*, add together the log. tangents, and proceed as for *M*.

Ex. Find *M* and *N* for $15^{\circ} 40'$ and $69^{\circ} 11'$.

$15^{\circ} 40'$ log. sec. 0.01644

$69^{\circ} 11'$ log. sec. 0.44931

M 292.2 log. 2.46575

log. tan. 9.44787

log. tan. 0.41999

N 73.8 log. 1.86786

TABLE 6. MERIDIONAL PARTS.

These are the number of minutes corresponding to each degree and minute of lat. on Mercator's chart. For ex., the mer. parts to lat. $39^{\circ} 12'$ are 2560.†

The mer. parts are given to each minute of latitude as far as 78° .

To compute a Term. Add 45° to half the latitude, and take out the log. tan. of this sum (rejecting 10), take away the decimal mark.

The process may now be completed *arithmetically*, thus:—Complete this number to 7 figures by annexing ciphers, or, if the index is 11, to 8 figures, and multiply by 0.00079157.

But it is more convenient to use logs. Consider the log. tan. thus prepared, as a natural number, and take out its logarithm. When the lat. is less than $13^{\circ} 6'$ prefix the index 5, when between $13^{\circ} 6'$ and $78^{\circ} 34' 44''$ prefix 6, and when above this last, 7. Add the const. log. 6.898489; the sum is the log. of the mer. parts.

* By the plane Traverse Table. With the greater arc as a course, and D. Lat. 100, take out the Dist. and Dep. With the other arc as course, and the said Dist. as D. Lat., take out the Dist.; this is *M*. With the said Dep. as D. Lat. take out the Dep.; this is *N*.

When the D. Lat. 100 is not found exactly, take out the Dist. and Dep. for the next less, and add the Dist. due to the defect from 100.

Ex. Find *M* and *N* to 20° and 42° . The Course 42° and D. Lat. 100 give Dist. 134.6, and Dep. 90.0. Then 20° and D. Lat. 134.6, give the Dist. or *M* 143.2, and the D. Lat. 90 gives Dep. or *N* 32.8

All the methods by Inspection may thus be effected by the plane Traverse Table.

† The nearest unit is, of course, enough in navigation. In the construction of charts two decimals may be necessary, and recourse may be had to Dr. Inman's, or Mendoza River's Tables.

<p>Ex. 1. Find the Mer. Pts. for the Lat. $3^{\circ} 19'$ $2) 3^{\circ} 19'$ $\begin{array}{r} 1\ 39\frac{1}{2} \\ 45 \end{array}$ } $46^{\circ} 39\frac{1}{2}$ log. tan. $10^{\circ} 025154$ Arithmetically. Annexing 2 ciphers gives 2515400, which multiply by $0^{\circ} 00079157 =$ $199^{\circ} 112$. By loga. 2515 .log. 400538 $\begin{array}{r} 4 \\ 70 \end{array}$ Index 5, $\begin{array}{r} 5400608 \\ 6898489 \end{array}$ Const. $6^{\circ} 898489$ MER. PTS. $199^{\circ} 11$ log. $2^{\circ} 299097$</p>	<p>Ex. 2. Find the Mer. Parts for Lat. $58^{\circ} 50'$ $2) 58^{\circ} 50'$ $\begin{array}{r} 29\ 25 \\ 45 \end{array}$ } $74^{\circ} 25$ log. tan. $10^{\circ} 554565$ 5545 log. 743902 $\begin{array}{r} 6 \\ 5 \end{array}$ $\begin{array}{r} 47 \\ 4 \end{array}$ Index 6, Const. $6^{\circ} 743953$ $6^{\circ} 898489$ MER. PTS. $4389^{\circ} 77$ log. $3^{\circ} 642442$</p> <p>Ex. 3. Find the Mer. Parts for the Lat $78^{\circ} 36'$. The log. tan. is $11^{\circ} 000812$, the index prefixed 7, Mer. Parts $7922^{\circ} 13$.</p>
--	---

The 6th figure in using tables to 6 places, will often be in error nearly 1; hence the mer. parts may be in error nearly .01, or 1-100th of a mile, or nearly 60 ft.

NOTE.—If the Spheroidal Mer. Pts. are required, enter the Traverse table with the lat. as a Course and 21.4 as a Dist.: the Dep. will be the reduction required. Ex. lat. 51° has Mer. Pts. 3569: Course 51° and Dist. 21.4 has Dep. 17: then $3569 - 17 = 3552$, Spheroidal Mer. Pts. for 51° .

DEPARTURES.

These Tables are used in the methods, chap. iv. p. 137.

TABLE 7. FOR FINDING THE DISTANCE OF AN OBJECT BY TWO BEARINGS AND THE DISTANCE RUN BETWEEN THEM.

The use of this Table is described in No. 350.

To compute a Term. To the log. sine of the difference between the course and the 1st bearing, add the log. cosec. of the diff. between the difference of the course and the 1st bearing and that of the course and the 2d bearing; the sum (rejecting tens) is the log. of the term.

TABLE 8. TRUE DEPRESSION OF THE SEA-HORIZON.

This Table contains the Depression to each minute as far as 240, with its square, and the corresponding height in feet.

The Depression is the Distance of the visible horizon, No. 205.

The Table may be also useful for reference, as containing the squares and square roots of several numbers.

To compute a Term. Multiply the square root of the height in feet by 1.063. Or, for greater precision, to the const. log. $6^{\circ} 49034$, add half the log. of the height in feet; the sum is the log. tangent (or log. sine nearly enough) of the depression.*

Approximately, the dist. visible in miles is the square root of the height in feet, an accidental relation easy to remember.

* As the lower latitudes are more frequented by shipping than the higher, 40° has been assumed as the average latitude. Also, as the curvature of the earth is different on the prime vertical and on the meridian, the circle of curvature, crossing the meridian at 45° of azimuth, has been employed. The depression is accordingly computed to the radius 20,909.577 feet which gives the length of the average nautical mile 6082 feet. nearly. See Table 64A.

Ex. Find the True Depression for the height 107 feet.

By Table 8 the square root of 107 is seen to be 10½, or 10·3 nearly.

Then $10·3 \times 1·063 = 10·9$ the Tr. DEPR.

Square root of	$\frac{2}{20909577}$	= Const.	6·4903
Log. of 107,	2·0294,		1·0147
Tr. DEPR.	11' 0"	sin.	7·5050

TABLE 9. NUMBER OF FEET SUBTENDING AN ANGLE OF 1'.

This Table gives, by simple proportion, the number of feet subtending an angle of any number of minutes and seconds within 3° or 4°, for any distance in nautical miles. It is very convenient for finding approximately the distance in miles of an object of given dimensions, as also the dimensions of an object seen under a given angle at a given distance.

The simplest way of using the Table is to find from the question the number of feet subtending 1'.

Ex. 1. The angular height of a mast-head, 138 feet high above the water-line of the vessel, and no horizon intervening, is 9': required the Distance of the Vessel.

$138 \div 9$ gives 15·3 feet, which subtends 1' at nearly 9 miles, the Dist. required.

Ex. 2. The distance between two vertical lights is 60 feet, and the angle it subtends is 4': required the Distance of the Light-house.

$60 \div 4$ gives 15 feet for 1', and Dist. required 8½ miles.

Ex. 3. The length of a vessel from the stern to the jib-boom end is 198 feet, and she subtends (when seen exactly, or nearly, broadside on), 27': required her Distance.

$198 \div 27$ gives 7·3 feet to 1', and Dist. required 4 miles.

Ex. 4. A cliff distant 5½ miles subtends a vertical angle of 39' (above the water or surf line): required its Height.

At 5½ miles 972 feet subtend 1', and 39×972 , 379 feet, the HEIGHT required.

The number of feet in the Table corresponds nearly to the number of miles increased by ¾ of itself; thus, 8 miles gives 14 feet.

To compute a Term. To the log of the dist. in feet add 30103 (the log. of 2) and the log. tan. of half the angle proposed (here 1'): the sum is the log. of the term required.

TABLE 10. MARITIME POSITIONS.

Order of Places. The places follow each other in their order along the coasts, except where it is convenient to pass to an island or shoal adjoining, after which the coast is again continued.

The Alphabetical Index at p. 540 removes the difficulty which would otherwise be experienced in searching for a particular place under any arrangement whatever of islands irregularly placed in the ocean.

Names in the Side Columns. The names of countries and seas inserted at the side of each column are intended merely to assist the forming of a general idea of the contents of the page, and are not to be considered as accurately defining geographical or political divisions.

Mountains. Mountains visible from the sea are inserted, as convenient for taking departures, and for the examination of the compass. The heights

of summits (to the tops of trees) are given in feet; when the height is considerable, and not accurately known, the distance in *leagues*, at which it is visible, is given instead of the height. The height may on many occasions be the means of identifying the land.* When the height precedes the point of which the position is given, it applies to the summit of the island or cape.

Lights. The descriptions of lighthouses are in most cases given. In the case of two lights, the height, and also the position, relate to the highest. See also pp. 402, 403.

Heights. All the heights taken from the latest Admiralty charts are reckoned from *high water*, in order to throw the error due to a difference in the height of the tide on the safe side. For ex., a light 120 feet above high water, seen at a certain (angular) altitude, places the ship 2 miles off. Now, at any other time of tide, the height exceeds 120 feet, and, in order to view it under the same angle, the ship must be more than 2 miles off; that is, the ship is really further off than is supposed, which is as it should be.

Secondary Meridians. These are the places in small capitals. See p. 392.

Latitudes and Longitudes. The Latitudes of ports are given to the nearest tenth of 1'; that is, to 6". The error due to this manner of notation cannot exceed 3", which is a quantity not worth dispute, except in fixed observatories.

The Longitudes of ports are given to those tenths only of 1' which correspond to the nearest *second of time*. These are .25, .5, and .75; the .05 being dropped, .2 stands for 1^s (or 15"), .5 for 2^s (or 30"), and .7 for 3^s (or 45"); that is, the seconds of time are, in round numbers, *half* the number of tenths: thus, 27.2 is read 27' 15", or 1^m 48^s and 1^s, or 1^m 49^s. The 2 and 7 used thus are distinguished by a dot below. By this slight change in the notation, we are enabled to employ at once the diff. long as deduced by the Traverse Table in minutes of arcs and tenths, while we preserve the utmost precision that can ever be required in practice.†

As 1' of long is 4^s of time, the error of neglecting the seconds in the longitude cannot exceed 2^s.

The omission of the tenths in the longitude, when those of the latitude are given, implies that such longitude is not well determined. The *tenths* of 1' noted in several longitudes do not, however, always imply precisely this degree of accuracy in the position, but serve to indicate stations to which the longitudes of places, not very distant, may conveniently be referred.

The positions of headlands, which are generally passed at the distance of some leagues, are given to the nearest minute only, in order to relieve the

* It does not consist with the design of this volume to give rules for determining the height of the land from the observation of its altitude with a sextant. But when the distance of the ship from the land is known, it will always be easy, by observing the altitude and *assuming* a height, to find whether the assumed height agrees or not with the known distance, by means of the rules in chap. iv. p. 139, and thus by a trial or two the true height will be obtained nearly. As the height of the land is a very important element in navigation and maritime geography, seamen may render essential service by taking advantage of favourable opportunities of determining heights in this way.

† Admiral W. F. W. Owen has employed this method of notation in his Table of latitudes and longitudes, as more convenient, in actual navigation, than that of seconds

computation from useless details. When the position falls on a half min. it is marked $\frac{1}{2}$ a min. to *seaward*, to throw the error on the safe side.

The position relates to the last-mentioned point (not in parentheses).

Groups of Islands. All groups of islands, and all single islands, rocks or shoals, recorded, are inserted. In many groups all the islands are noticed; where this is not necessary, those marking the limits are given.

Sulmarine Volcanoes. Between the lats. 7° N. 1° S., and long. 16° and 24° W., several ships have met with ashes or experienced shocks. Krusenstern, on May 9th, 1806, saw, in $2^{\circ} 43'$ S., $20^{\circ} 33'$ W., a column of smoke, which shot up at intervals. There is little doubt, therefore, that the region is volcanic; and though Capt. Wickham, in H.M.S. *Beagle*, found no bottom at 190 fathoms in $1^{\circ} 55'$ S., 23° W., it is not unlikely that a shoal may at some time appear, and on this account the attention of seamen is directed to this region in column (41).

It may be remarked here, that land suddenly thrown up has quickly sunk again.

Orthography. In the names of places, of which the native alphabet does not correspond to ours, or where the language is unwritten, the reader must expect some trifling inconsistencies, owing partly to our own irregular orthography. We have followed chiefly the Hydrographic Office, which employs the Italian vowels, with some modification. Thus, *a* as in *father*, *ai* as *i* (English) in *shine*; *au* as *ow* (English) in *cow* (Dutch *ow*); *e* as *a* (English) in *face*; *u* (or *ou* in some cases) as *oo* (English) in *fool*, or *u* in *sure* (French *ou*, Dutch *oe*). For ex., *Apia*, pronounced Ah-pee-a; *Mitiéro*, pronounced Mee-tee-air-o; *Manua*, pronounced Man-oo-a, not Manyúa. Cook's "Whytootackie" is spelt *Aitutaki*, as by the missionaries, who, wherever they have instructed the Pacific islanders in writing, have wisely given them the Italian vowels. Some names we preserve in forms already known to our seamen, as Nareenda, Toofoca (pronounced *Narinda*, *Toufona*), &c., as also Otaheite (*Tahiti*), in which the *o* is not, however, absolutely, erroneous.

We have sometimes marked the pronunciation by an accent, as Battantá, Galápagos, Tongatábon, &c.

It must, however, always be borne in mind that each different people calls the same place by different names; this accounts for the discrepancies in names given to numerous islands.

Notation and Details. Everything in parentheses is additional information (to be explained under the Symbols), but which does not relate to the position.

Ex. Col. (30) C. Xyli (pk. 1040 f., N $1^{\circ} 5'$) . . . denotes that there is a pk., &c., but the position is of C. Xyli.

Col. (55) Ras Gurdim \perp (rk S.E. 3m.) denotes there is a rock, &c., but the position is of Ras Gurdim.

Col. (81) Pt. Sipang, a $\overline{\text{rk}}$ (rks. 5m.) . . . denotes a rk. (awash) off Pt. S—, and rks. also 5m. out, but the position is that of the rock close off.

The seaman must draw no conclusions from the *absence* of details; he is not, for example, to infer that a place is safe merely because it is not marked dangerous.

Uses of the Table. This Table has, in navigation, two applications: 1st. It furnishes points of departure in leaving and in making the land, under which head are included, also, islands made in passages, and dangers to be

avoided in shaping the course; 2nd. It gives the positions of ports and anchorages for the more complete regulation of the chronometer. Places, therefore, not belonging to one or the other of these two classes are unnecessary, because, in such circumstances, generally, the ship is either in pilot-water, or is navigated by the chart alone.

Lights, however, are inserted in greater number, because a ship in a fog may pass an outer light unseen, and learn her position from an inner one.

1. *Arrangement of the Positions.*

It is proper here to describe the principles on which this Table has been constructed, and to which allusion was made in the preface to the first edition.

It will be admitted, as remarked (pref. p. viii), that the *relative* positions of places are of much greater consequence in navigation than their *absolute* positions. For no astronomical observations taken at sea can be implicitly depended upon within at least one minute, and the chronometer, in consequence of not preserving exactly the same rate, ceases, after some days, to afford the true longitude of the ship. Since, therefore, the absolute longitude of the ship herself cannot be determined with certainty, the knowledge of the precise longitude of any position, as a rock, or a shoal, which she may be near, is but of little service. But, on the other hand, a tolerably good account of the ship's change of place, in short intervals of time, is afforded by a chronometer even of inferior quality, and hence it becomes of paramount importance that the places which the navigator employs as points of departure should be rightly placed *with respect to each other*, whether they are in their true positions or not.

Previously to Cook's voyages, which may be considered as the commencement of modern hydrography, the only method (besides the rude and imperfect determination of the ship's run) of obtaining the longitude of every new land made, was the lunar observation. But as that method, from its inaccuracy, fails altogether in exhibiting truly relative positions (No. 1008), chronometers were employed in combining together the results of observations taken at different places, of which numerous instances are recorded by Horsburgh in his East India Directory. Since, however, the observations made at two places are not in general equally good, this method of combining observations with chronometric differences has the disadvantage of impairing the better determination of the two, and in consequence throws a difficulty over the connexion of either of them with a third place better known. Succeeding navigators, proceeding in the same way, have obtained other results of observation, and other chronometric differences; and, in consequence, the hydrographer who has not the means afforded him of instituting a critical examination of the several positions, or of their connexion with each other, is driven to the necessity of taking a mean between each new result and those adopted from former navigators, and thus the whole mass of positions is kept in a state of perpetual fluctuation, from which it is impossible that universal precision can ever be obtained.

In marine surveys, again, different meridians have been assumed, and different longitudes of the same meridian. In some cases the long. of the meridian assumed has not been given; in others, the meridian itself has not been specified at all.

If, however, instead of thus throwing open the discussion of every place at each new voyage of discovery or surveying expedition, and unsettling all that had previously been done, without any assurance that the new series of positions would not in its turn be unsettled again, navigators and hydrographers would agree to *consider*, for the time being only, certain important stations, as already established in longitude, whether really so or not, with the view of referring all the subordinate positions to them, the indistinctness which now hangs over absolute and relative position would be forthwith cleared up. The question would be narrowed into the determination of *chronometric differences* alone, until favourable opportunity occurred for the definitive determination of a fundamental position. Accurate chronometric measures would be no longer lost to the world by being merged in the uncertain results of a few astronomical observations; and the labours of each navigator would always maintain their proper value, instead of being set aside, as they must inevitably be, on the appearance of a new survey, in which the data are exhibited in a distinct form. The works of different navigators, and of the navigators of different countries, could be brought into immediate comparison, a task which is at present often difficult and unsatisfactory, if not impossible. The labours of the hydrographer would be materially simplified; and as the points to which inquiry should next be directed would, by this system, be distinctly brought into view, the whole subject would advance steadily to its ultimate perfection.

The following instances may be cited in illustration:—The long. of Rio de Janeiro (Fort Villagagnon) had been by some stated to be $43^{\circ} 15'$, by others $43^{\circ} 9'$, while both parties adopted $56^{\circ} 13'$ as the long. of Monte Video (Rat Island). Now the true D. Long. of these places is $52^{\text{m}} 18^{\text{s}}$, probably within 1° or 2° , certainly within 4° ; but the diff. of $43^{\circ} 15'$ and $56^{\circ} 13'$ is $51^{\text{m}} 52^{\text{s}}$, or an error is admitted on one side of 26° in a run of about 10 days. Had attention been earlier directed to differences of longitude as measured from fundamental points, such inconsistencies would speedily have disappeared.

Accordingly, it was proposed (Naut. Mag. 1839, On the longitudes of the principal maritime points of the globe) to adopt certain points under the name of *Secondary Meridians*, this general term being used to distinguish them from the *prime* meridians, as Greenwich, Paris, &c., from which the longitudes in the tables or on the charts must be reckoned. The longitudes (from Greenwich) accepted for the *Secondary Meridians*, on which Table 10, and the Admiralty Charts now (1898) depend, have been amended from Telegraphic determinations to 1887.* The points selected are so far distant from each other that the errors of their relative positions could not be easily discoverable by the ship's chronometers; and they must themselves depend on astronomical observations, of which it is important to remark, the number necessary for an unimpeachable determination appears to be very great. The *Secondary Meridians*, with the districts for which they are intended generally to serve, and their adopted longitudes, from *Greenwich*, are as follows:—

* The number of *Secondary Meridians* in the last edition was 25; considerable corrections and additions have now been made.

TABLE OF LONGITUDES ACCEPTED FOR SECONDARY MERIDIANS.

SHORES OF ATLANTIC OCEAN, AND NEIGHBOURING SEAS.

Copenhagen (<i>Observatory</i>)	-	12	34	48	E.	=	0	50	19.2	Kattegat, Coasts of Norway; Sweden.
St. Petersburg (<i>Pulkowa Observatory</i>)	-	30	19	40	E.	=	2	01	18.7	Baltic, White, and Black Seas.
Paris (<i>Observatory</i>)	-	2	20	15	E.	=	0	09	21.0	Coasts of France. West coast of Italy; Algeria.
Lisbon (<i>Dome of Royal Observatory</i>)*	-	9	11	10	W.	=	0	36	44.7	Coasts of Spain and Portugal.
Cadiz (<i>San Fernando Observatory</i>)	-	6	12	24	W.	=	0	24	49.6	
Pola Observatory	-	13	50	45	E.	=	0	55	23.0	Adriatic.
Malta (<i>Spencer's Monument</i>) †	-	14	30	40	E.	=	0	58	02.7	West coasts of Italy, Greece, Sicily; North coast of Africa.
Gibraltar (<i>Dockyard Flagstaff</i>) ⊕	-	5	21	27	W.	=	0	21	25.8	
Alexandria (<i>Lighthouse</i>)	-	29	51	40	E.	=	1	59	26.7	Egypt and Syria.
Smyrna (<i>Mill on Daragaz point</i>)	-	27	09	42	E.	=	1	48	38.8	Grecian Archipelago.
Constantinople (<i>St. Sophia</i>)	-	28	58	59	E.	=	1	55	55.9	Black Sea.
Madeira, Funchal (<i>British Consul's House</i>)*	-	16	54	30	W.	=	1	07	38.0	Azores, Madeira, Canary and Cape de Verde islands; West coast of Africa to Fernando Po.
Madeira (<i>Fort St. Jago</i>)*	-	16	53	53	W.	=	1	07	35.6	
Madeira (<i>Pontinha</i>) ‡	-	16	55	01	W.	=	1	07	40.1	
Porto Grande, Cape Verde Islands (<i>Flagstaff in front of Brazilian Submarine Telegraph Co.'s Office</i>)*	-	24	59	22	W.	=	1	39	57.5	
Newfoundland, St. John's (<i>Chain Rock Battery</i>)	-	52	40	47	W.	=	3	30	43.1	Newfoundland and Labrador.
Halifax, Nova Scotia (<i>Naval Yard Observatory</i>) §	-	63	35	21	W.	=	4	14	21.4	British North America and Canada.
Boston, United States (<i>Cambridge Observatory</i>)	-	71	7	39	W.	=	4	44	30.6	United States; North America.
Key (Cay) West, U.S. Naval Storehouse (<i>Observing Spot</i>)	-	81	48	24	W.	=	5	27	13.6	
Key (Cay) West (<i>Lighthouse</i>)	-	81	48	04	W.	=	5	27	12.3	

* U.S. Telegraphic determination in 1878-9 from Greenwich. Published by U.S. Government, 1880.

† Telegraphic determination, 1875, from Berlin, by Professor Auwers and Dr. Gill

⊕ Telegraphic determination from Malta by H.M.S. *Sylvia*, 1886.

‡ Depending on being 1' 8" west of Fort St. Jago by chart.

§ Telegraphic determination in 1851 and 1872 from Washington, and from Greenwich.

|| U.S. Telegraphic determinations in 1875-6 from Washington. Published by U.S. Government, 1877, No. 65.

EXPLANATION OF THE TABLES.

293

	h. m. s.			
Vera Cruz (<i>San Juan de Ulloa Lighthouse</i>)*	96	07	57 W. =	6 24 31·8
Havana (<i>Morro Lighthouse</i>)†	82	21	30 W. =	5 29 26·0
Santiago de Cuba (<i>Blanca Battery. South angle</i>)†	75	50	30 W. =	5 03 22·0
Port Royal, Jamaica (<i>Fort Charles</i>)†	76	50	38 W. =	5 07 22·5
Aspinwall (<i>Aspinwall Light-house</i>)†	79	54	45 W. =	5 19 39·0
San Juan de Puerto Rico (<i>Morro Lighthouse</i>)†	66	07	28 W. =	4 24 29·9
Virgin Islands, St. Croix (<i>Lang's Observatory, centre of Transit Pier</i>)†	64	41	17 W. =	4 18 45·2
St. John, Antigua (<i>North tower of Cathedral</i>)†	61	50	28 W. =	4 07 21·9
St. Pierre, Martinique (<i>St. Murthe Battery</i>)†	61	11	12 W. =	4 04 44·8
Bridgetown, Barbados (<i>Flagstaff of Rickett's Battery</i>)†	59	37	18 W. =	3 58 29·2
Port Spain, Trinidad (<i>Flagstaff of Water Battery</i>)†	61	30	38 W. =	4 06 02·6
St. Thomas (<i>Fort Christian</i>)†	64	55	52 W. =	4 19 43·5
Para (<i>Portico of Custom House</i>)†	48	30	01 W. =	3 14 00·0
Pernambuco (<i>Lighthouse near Fort Pico</i>)†	34	51	56 W. =	2 19 27·8
Bahia (<i>San Antonio Lighthouse</i>)†	38	32	05 W. =	2 34 08·4
Rio de Janeiro (<i>Fort Villagagnon</i>)†	43	09	29 W. =	2 52 38·0
Monte Video (<i>Rat Island</i>)†	56	14	00 W. =	3 44 56·0
Monte Video (<i>S.E. tower of the Cathedral</i>)†	56	12	15 W. =	3 44 49·0
Buenos Aires (<i>Cupola of Custom House</i>)†	58	22	14 W. =	3 53 29·0

West India.

East coast of South America; Brazil.

INDIAN OCEAN AND RED SEA.

Cape of Good Hope (<i>Government Observatory</i>)§	18	28	40 E. =	1 13 54·7	South Africa, Madagascar, Seychelles.
Zanzibar (<i>British Consulate</i>)	39	11	08 E. =	2 36 44·5	Adjacent African Coast.
Aden (<i>Submarine Telegraph Office</i>)¶	44	58	57 E. =	2 59 55·8	Gulf of Aden.
Aden (<i>Local Telegraph Office</i>)	44	59	07 E. =	2 59 56·5	
Aden (<i>Observation spot. Ras Mârbut</i>)	44	58	31 E. =	2 59 54·1	
Suez (<i>Port Ibrahim</i>)**	32	33	30 E. =	2 10 14·0	Red Sea.
Mauritius (<i>Martello tower, Fort George</i>)††	57	29	00 E. =	3 49 56·0	Madagascar — African Coast.
Bombay (<i>Observatory</i>)¶	72	48	58 E. =	4 51 15·9	Persian Gulf, West Coast of India & adjacent sea.

* U.S. Telegraphic determinations, 1883-4, from Washington. Published by U.S. Government in 1885, No. 76.

† U.S. Telegraphic determinations in 1875-6 from Washington. Published by U.S. Government, 1877, No. 65.

‡ U.S. Telegraphic determinations in 1878-9 from Greenwich. Published by U.S. Government, 1880.

§ Telegraphic determinations in 1881, by Dr. Gill from Aden.

|| Telegraphic determination, 1881, by Dr. Gill from the Cape of Good Hope.

¶ Telegraphic determination, India Trigonometrical Survey, 1878.

** Transit of Venus expedition, 1874.

†† Transit of Venus expedition, 1874 (meridian distance from Rodriguez).

Madras (<i>Observatory</i>)*	-	-	-	8° 14' 51" E.	=	5 20 59.4	Bay of Bengal.
Andaman Islands. Port Blair							
(<i>Observatory, Chatham Ind.</i>)	92	43	00	E.	=	6 10 52.0	Andaman Islands.

JAVA, CHINA, AND JAPAN SEAS.

Batavia (<i>Observatory</i>)†	-	-	-	106 48 37 E.	=	7 07 14.5	W. Coast Sumatra, Java Eastern Archipelago.
Banjuwangi (<i>Fort Utrecht</i>)‡	-	-	-	114 22 55 E.	=	7 37 31.7	Adjacent islands.
Singapore§ (<i>Green's transit pier in rear of Muster Attendant's Office</i>)	103	51	15	E.	=	6 55 25.0	Malacca Strait, South part of China Sea, Palawan.
Cape St. James (<i>Lighthouse</i>)	-	-	-	107 04 55 E.	=	7 08 19.6	Coast of Cochin China.
Manila (<i>Cathedral</i>)	-	-	-	120 58 06 E.	=	8 03 52.4	Philippine Islands.
Hong Kong (<i>Cathedral</i>)	-	-	-	114 09 31 E.	=	7 36 38.1	Coasts of China.
Hong Kong (<i>Observatory Kau-lung</i>)	114	10	25	E.	=	7 36 41.7	
Hong Kong (<i>Palos Pier</i>)	-	-	-	114 09 43 E.	=	7 36 38.8	
Amoy (<i>Kulangsu Signal Staff</i>)	118	04	03	E.	=	7 52 16.2	
Shanghai (<i>British Consulate Flag-staff</i>)	121	28	55	E.	=	8 05 55.7	Yellow Sea and Korea.
Vladivostok (<i>Scharnhorst's Station</i>)	131	52	44	E.	=	8 47 31.0	Russian Tartary.
Nagasaki (<i>Minage Point</i>)	-	-	-	129 51 13 E.	=	8 39 24.9	Japan.
Yokohama (<i>Flagstaff English Victualling Depot</i>)	139	39	13	E.	=	9 18 36.9	

AUSTRALIA, TASMANIA, AND NEW ZEALAND.

Sydney (<i>Observatory</i>)¶	-	-	-	151 12 23 E.	=	10 04 49.5	Australia and adjacent islands.
Sydney (<i>Fort Macquarie</i>)**	-	-	-	151 13 00 E.	=	10 04 52.0	
Moreton Bay (<i>Cape Moreton Lighthouse</i>)††	153	28	00	E.	=	10 13 52.0	Queensland.
Townsville (<i>Flagstaff Pilot Hill</i>)⊕	146	49	54	E.	=	9 47 19.6	
Cooktown (<i>Boatshed at inner end of Jetty, Pilot Station</i>)⊕	145	15	12	E.	=	9 41 00.8	
Cape York (<i>Sextant Rock</i>)	-	-	-	142 32 48 E.	=	9 30 09.2	Torres Strait and New Guinea.
Samarai (<i>Dinner I. China Strait Observation spot</i>)⊕	150	39	47	E.	=	10 02 39.1	
Port Essington (<i>Site of old Government House</i>)	132	09	18	E.	=	8 48 37.2	North-west Coast of Australia.
Port Darwin (<i>Transit pier, east extreme of cable House</i>)¶	130	50	37	E.	=	8 43 22.5	
Swan River (<i>Scott's Jetty</i>)††	-	-	-	115 44 30 E.	=	7 42 58.0	West Australia.
Adelaide (<i>Snapper point</i>)††	-	-	-	138 30 50 E.	=	9 14 03.4	South Australia.
Port Phillip (<i>Melbourne Observ.</i>)††	144	58	32	E.	=	9 39 54.1	Victoria.

* Telegraphic determination, India Trigonometrical Survey, 1878.

† Telegraphic determination from Singapore by Professor Oudemans in 1871, adopting U.S. determination of Singapore, 1881-2.

‡ Telegraph determination through Singapore and Port Darwin (in connection with Greenwich), in 1883. Communicated by Mr. Ellery, Government Astronomer at Melbourne, in letter dated January 8, 1885.

§ From Green's transit pier the old Observation spot in Fullerton battery, Singapore, bears S. 5° 37' W. (true) distant 169 feet.

|| U.S. Telegraphic determination, 1881-2. Published by U.S. Gov., 1883, No. 65b.

¶ Telegraph determination through Singapore and Port Darwin (in connection with Greenwich), in 1883.

** Depending on Fort Macquarie being 47" E. of Sydney Observatory on chart.

†† Depending on Fort Macquarie, Sydney, being in 151° 13' 00" E.

⊕ Telegraphic determination from Sydney by H.M. ships *Dart* and *Lark*, 1886.

+ Meridian distance from Townsville, H.M.S. *Dart*, 1886.

††† Telegraph determination through Singapore and Port Darwin (in connection with Greenwich), in 1883.

Tasmania. Hobart (<i>Site of Fort Mulgrave</i>)*	147 20 35 E. = 9 49 22.3	Tasmania.
New Zealand. Wellington (<i>Pitsea point</i>)	174 47 02 E. = 11 39 08.1	New Zealand.
New Zealand. Mt. Cook (<i>Observatory</i>)†	174 46 38 E. = 11 39 06.5	

PACIFIC OCEAN.

Levuka, Ovalau (<i>Site of old School-house</i>)	178 51 00 E. = 11 55 24.0	Fiji Islands, South-west Pacific Ocean.
Tahiti (<i>Point Venus extreme</i>)	149 29 00 W. = 9 57 56.0	South-east Pacific Ocean.
Honolulu (<i>King's Cottage</i>)†	157 51 53 W. = 10 31 27.5	North Pacific Ocean.
Esquimalt harbour (<i>Duntze Head, site of Observatory</i>)	123 26 45 W. = 8 13 47.0	Vancouver Island and British Columbia.
San Francisco (<i>Fort Point Light-house, south side of entrance</i>)‡	122 28 38 W. = 8 09 54.5	California.
San Salvador, La Libertad (<i>Pier head</i>)§	89 19 22 W. = 5 57 17.5	Mexico and Ecuador.
Panama (<i>Cathedral, South tower</i>)	79 32 12 W. = 5 18 08.8	
Panama (<i>North-east bastion</i>)	79 32 03 W. = 5 18 08.2	West Coast of South America.
Paita (<i>Cathedral tower</i>)§	81 07 17 W. = 5 24 29.1	
Lima (<i>South tower of Cathedral</i>)§	77 00 02 W. = 5 08 10.6	
Callao (<i>San Lorenzo Lighthouse</i>)§	77 15 44 W. = 5 09 02.9	
Arica (<i>Church spire, Igleuiu Matrix</i>)§	70 20 00 W. = 4 41 20.0	Magellan Strait.
Valparaiso (<i>Capota of Exchange</i>)§	71 38 36 W. = 4 46 34.4	
Magellan Strait, Sandy point (<i>Bout-house</i>)¶	70 54 03 W. = 4 43 36.2	
Magellan Strait, Port Famine (<i>Fitz Roy's Obs. spot</i>)**	70 56 37 W. = 4 43 46.5	

Meridians adopted in the construction of Foreign Charts.

Russia, Sweden, Denmark, Norway, Holland, Austria, and the United States of America adopt the Meridian of Greenwich.

France adopts the Meridian of Paris, assumed to be in Long. $2^{\circ} 20' 15'' = 0^{\circ} 09' 21.0''$ E. of Greenwich.

Spain adopts the Meridian of San Fernando, Cadiz, assumed to be in Long. $6^{\circ} 12' 24'' = 0^{\circ} 24' 49.6''$ W. of Greenwich, or $05^{\circ} 22'$ E. of Old Observatory.

Portugal adopts the Meridian of the Observatory, assumed to be in Long. $9^{\circ} 11' 10'' = 0^{\circ} 36' 44.7''$ W. of Greenwich.††

The Pulkowa Observatory of St. Petersburg (sometimes referred to in Russian Charts) is assumed to be in Long. $30^{\circ} 19' 40'' = 2^{\circ} 1' 18.7''$ E. of Greenwich.

The Royal Observatory of Naples (sometimes referred to in Italian Charts) is assumed to be in Long. $14^{\circ} 15' 7''.3 = 0^{\circ} 57' 00.5''$ E. of Greenwich.

* Transit of Venus expedition of 1874.

† Telegraphic determination from Sydney, 1883.

‡ U.S. Telegraphic determination in 1870 from Washington.

§ U.S. Telegraphic determinations, 1883-4, from Washington. Published by U.S. Government in 1885, No. 76.

|| U.S. Telegraphic determinations in 1875-6 from Washington. Published by U.S. Government, 1877, No. 65.

¶ From Professor Auwers (German Transit of Venus expedition), 1882. By meridian distances measured in H.M.S. *Nassau*, 1866-69, from Rio de Janeiro (Fort Villegagnon being considered in $43^{\circ} 09' 29''$ W.), the longitude of Sandy Point is $70^{\circ} 54' 06''$ W. By meridian distance measured in H.M.S. *Sylvia*, 1882, from Monte Video (Rat Island being considered in $56^{\circ} 14' 00''$ W.), the longitude of Sandy Point is $70^{\circ} 54' 08''$ W.

** Depending upon Sandy Point, being in $70^{\circ} 54' 03''$ W.

†† The longitude of Lisbon castle deduced from the U.S. telegraphic longitude of the Lisbon Royal Observatory (in $9^{\circ} 11' 10''$ W.) is $9^{\circ} 07' 55''$ W.

[1.] *Symbols denoting the Values of the Determinations.*

The symbols \bigcirc \ominus \odot \otimes attached to certain places, indicate the degree of precision with which their positions are supposed to be known.

The circle represents the horizon of the place; the line thus — a parallel of latitude; and the line thus | a meridian. Accordingly, the meaning of the symbols, generally, is as follows:—

1. \bigcirc implies *undetermined* either in lat. or long.
2. \ominus implies determined in *latitude* only, or the longitude wanting
3. \odot implies determined in *longitude*, or the latitude wanting.
4. \otimes implies determined both in latitude and longitude.

A dot under the \bigcirc implies *aggravated uncertainty*.

As very few places are *determined* in the strict sense of the word, while, on the other hand, no known place can be said to be absolutely *undetermined*, the sense attached to these two words must be defined by the purposes which the symbols are intended to serve in hydrography or in the navigation of a ship.

The different *degrees* of determination are indicated by the *position* of the symbol.

1. The symbol \bigcirc denotes a doubt of not less than 2' of lat., or somewhat more of long. It is used when the authorities differ from each other, or themselves: thus Capt. W. F. W. Owen places Cape Nun in $28^{\circ} 41' N.$, and Lient. Arlett in $28^{\circ} 46'$, the long. not being well known.

This symbol placed after the name in the *side column* denotes that the district generally is imperfectly known, as parts of the Eastern Archipelago.

2. The symbol \ominus indicates the latitude well enough determined for ordinary purposes, but the longitude defective. It occurs frequently.

3. The symbol \odot occurs rarely.

4. The symbol \otimes after the name of a *point*, implies a tolerably precise determination.

It would have been prefixed to Pulo Aor, col. 67, but this island is 2 m. from E. to W., and the precise point of observation is not specified.

When placed *after* the name in the *side column*, it implies trigonometrical survey, subject to future, though probably small, correction; as, for ex., parts of our own coasts, the coast of Holland, Iceland, Greece, Italy, India, Corsica, R. St. Lawrence, Massachusetts, Rhode I., &c.

When placed *before* the name in the *side column*, it denotes final determination. The coasts so distinguished are part of our own, and it should have been attached to France.

This final characteristic cannot obviously be applied until the secondary meridian is fixed.*

When no symbol is attached either to the district or to the points of

* The attention of seamen is particularly called to the considerations in the text. By having distinctions established, in the Table, between correct and uncertain positions, the navigator will have his circumspection awakened on approaching land of doubtful situation; and on leaving it again he will be enabled to avoid errors or perplexity in his reckoning consequent on adopting an erroneous point of departure.

It is also hoped that a further important end will be answered by the use of the symbols, and that intelligent individuals, thus made aware of the deficiencies or errors of the charts and tables, will, for the benefit of navigation and hydrography, avail themselves of opportunities to determine or verify doubtful positions.

the coast, it is implied that we are not in possession of such additional evidence as might serve to form a definite opinion on the accuracy of the several points.

The Secondary Meridians take no symbol, since, though not all finally determined, they are assumed as the leading points of the arrangement.

2. *Description-Symbols.*

The importance of abbreviations and symbols in saving time in writing is so generally felt that most persons who write much, habitually employ certain signs, intelligible to themselves, to save the tedious repetition of the same letters and syllables.

Suitable and expressive symbols are, however, not merely a convenience to the writer, but afford, in general, the advantages of distinctness, explicitness, and economy of time to the reader, together with another of still greater consequence, namely, certainty. This last assertion will not, perhaps, be so generally assented to as the former, but the truth of it is easily established. For example, a seaman in any particular part of the world opens a book to learn where he may find a good anchorage. His eye naturally looks for the word "anchorage" or "anchor," as it would for a sign or symbol. Having found the word, he is then obliged to read the entire sentence which contains it, in order thoroughly to comprehend the meaning; since, without a clear understanding of all that is said about anchorage, it is not safe to act. Now this sentence, though it relates, as we suppose, in some way to anchorage, may not contain at all the information that he requires; it may, for example, allude to some ship having partially or unsuccessfully searched for an anchorage, or it may merely intimate that no good anchorage has been found between some place in the neighbourhood and another more distant. Moreover, it is often difficult, from the arrangement of the matter, to know the precise point the account refers to, without reading back. If, on the contrary, the reader's eye catches the symbol ⚓, or this symbol so modified as to express with clearness "no anchorage," or "good anchorage," or "bad anchorage," or "anchorage at times only," or "confined to a small space," his work is done at once; he seizes in an instant the information that is given, and his mind is altogether unembarrassed by circumstances of narration, or the consideration of suppositions, inferences, and conditions, which often tend to obscure language in full development.

There are numerous other matters which, on like grounds, demand conspicuous indication: such as the dimensions of islands and shoals the leading particulars of dangers; the character and appearance of land, for the purpose of distinguishing one point from another; the class of vessels to which a harbour is adapted; channels; landing-places; as also notice of water, refreshments, and fuel, &c.

But, besides the mere notice or indication, it is often no less necessary to denote *quality*, or character, as good or bad; thus the seaman should know whether the inhabitants of a place he may visit are likely to assist his wants or to massacre his crew; that is, whether the character of the people is friendly or hostile.

The consideration of *quantity* has a powerful influence on the indications of language. One place has some trees upon it; another is well wooded; another densely wooded. It is entirely by increase of quantity that we pass from *trees* to *wood*, and from *wood* to *forest*. In like manner,

It is no less the abundance than the superior quality of the water, refreshments, &c., that determine the selection of the place at which to obtain supplies.

The following cases exemplify the great conciseness of expression and clearness of symbols which may be considered as appropriate.

☐¹⁰ A harbour for smaller sized vessels (i.e. of which the depth is not always so much as 3 fathoms) having 18 feet water at high water, and 6 feet at low water, spring tides.

The symbols represent twenty words, in the space of two or three letters, besides indicating the rise of the tide, which is found by subtracting the lower depth from the upper.

☐¹¹ A harbour (as above), having 18 feet at high water, and dry at low water.

These symbols represent eighteen words.

w' Water, in abundance, and of good quality.

⌒ 4m. Lying North-north-east and South-south-west, and extending 4 miles.

The last symbols represent twelve words; and the compass symbol exhibits to the eye, without reference to the names of the points, the two opposite quarters of the compass in which the line of direction is contained.

The reader must be distinctly informed that the symbols do not, in any way, interfere with the usual purposes of this Table, and therefore he may, if he please, disregard them altogether. He will, however, never do wrong in taking any known sign in its usual sense, as those symbols and abbreviations which have come into general use are here adopted as the groundwork of the system. The seaman who may find some little difficulty in learning to read these signs at first, may wish that the information they contain was printed at greater length. But there is no room for this, as the Tables are already too bulky; and it is only through the remarkable condensation afforded by the symbols that such information can be given at all. But when he has once taken the trouble to learn the system, which he will find very easy, he will, on the contrary, be induced to prefer the short and concise, positive, and unmistakable symbol to the tedious, indiscriminative, and not seldom obscure process of language written at length.

There is no doubt that proper symbols would be of great advantage to seamen in consulting books and tables relating to Maritime Geography, and also Charts; and we shall now enter on the system of which the first steps occurred to me while preparing the second edition of this work in 1841.

[1.] *General Rules for the Employment of the Symbols.*

1. An abbreviation, or an appropriate symbol, is assigned to each point of information; as lt. light; ⚓ anchorage; w water.*

2. A zero, or cipher, below, and to the right, denotes *no*, or *none*; as w₀ *no water*, ⚓₀ *no anchorage*.

Note.—This zero is of as much consequence as the symbol itself, and is the only secondary or subordinate sign that is so. It may, at first sight, seem awkward to write the symbol, and then to destroy it, as it were, by the zero; but it is the necessary process of thought: when we wish to say “no water,” we necessarily direct the mind to *water* as the subject, and then add that there is *none* of it. To leave out the symbol altogether would not express the *privation* of the *thing*, but merely that we had nothing to say upon it.

* In employing these signs it is essential that capitals and small letters should not be confounded.

3. A symbol inverted has its meaning reversed : thus the boathook, *hook*, inverted, as *hook*, would denote *embarking*.

4. A hollow letter implies *temporary* or *occasional*, in opposition to the solid letter implying *permanent*; thus *F* (after *lt.*) denotes a *permanent* fixed *lt.*; *F* an *occasional* fixed *lt.*

5. The symbol repeated denotes the same thing at *different places*, or not everywhere; as *⚓ ⚓*, anchorages, in *certain places*.

6. A symbol followed by the same with the zero sign denotes *at times*; as *ww.*, water *at times* (literally, water and no water).

Note.—This is, in general, equivalent to the hollow letter above; but all symbols cannot conveniently be printed in the hollow form.

[2.] Component Signs.

These are used only in combination with others.

1. The line — denotes the *surface of the sea*; everything above this is, accordingly, conceived as above the level of the sea, and below it, below that level: as *rk.* a *rk.* always *above* the surface; *rk.* a *rk.* always *below* the surface, i.e. *sunken*.

A symbol between two such lines, that is, between *two levels*, denotes *awash*, as *rk.* Such is, for example, the *Vrach*, off *Alderney*, which shows only at low spring-tides.

2. A line thus | denotes *vertical*.

3. The cross +, with a number denoting the point in the proper quarter, constitutes the *Compass Symbol*; thus *⚓* denotes *ENE*.

The cross with the *N. pt.* turned a little to the *right* would denote *magnetic*, as affected by *Easterly Variation*; turned to the *left*, as affected by *Westerly Variation*.

4. A square, or oblong, implies *enclosure*, whether partial or total; as *⚓*, an anchorage enclosed, represents *harbour*.

5. Brackets [1] imply *within limits*; as [*⚓*] anchorage confined to a narrow or limited space; [2] a shoal patch, with 2fms. on it, that is, 2fms. confined to a small space; [*⚓*] trees confined to a small space, a clump.

When a letter denoting dimension (as *c*, *f*, *m*), with or without a number, and inserted in brackets, follows the word *Id.*, or a term describing a danger, it indicates *extent*; thus [*lm*], “within the limits of 1 mile,” that is, *extending* 1 mile. [*c*] A cable’s length, or so, in extent. [*3c*] Three cables in extent.

[3.] Subsidiary Signs.

These are the dots under, the apostrophes over, and the accents or letters to the right of, the symbol.

Note.—The subordinate signs follow, and never precede, the symbol.

They denote, 1st, *Quantity*; and 2nd, *Variety*.

I. The *quantity-signs* are the dots and apostrophes.

(1.) The *dot* (below) denotes *plenty*, abundance; as *⚓* plenty of water. The dot has this acceptation in the weather symbols, p. 156. Two dots denote a greater abundance, and three dots express the highest degree for which language has a term: thus *⚓* a tree or trees; one dot would denote many trees; *⚓* wood (well wooded), and three dots would denote forest, or densely covered.

(2.) The *apostrophe* (above) implies *scarcity*; as *⚓* water not plentiful.

This sign is adopted from its use in contractions, as in such words as

can't; whence it becomes associated with the idea of diminution. It is placed above in order still further to contrast with the plenty-sign or dot, and to prevent the possibility of confounding one with the other, even in the case of almost total obliteration. Two apostrophes would denote great scarcity, and three, the almost entire absence of the thing indicated.

II. The *variety-signs* are the letters, accents, or any other symbols as convenient, to the right of the symbol, and above or below it.

(1.) The most general of these is the accent, which denotes some variety of the thing symbolised: thus N, S, E, W, denoting the true points of the compass, N', S', E', W', denote the *magnetic* points of the compass.*

(2.) In things having quality, that is, which may be good or bad, the accent is placed *above* to denote *superior*, or good quality, as opposed to *inferior*, or *bad* quality, denoted by the accent *below*; as w' good water, w, bad ditto; ‡ good anchorage, ‡, bad ditto.

Two accents would denote the next, and three the highest, degree for which language has a term: as w'' water very good, w''' ditto excellent; ‡,, anchorage very bad, ‡,,, the worst possible, or where a ship should anchor only in great distress.

(3.) The letters used for these secondary distinctions must obviously take their signification from the thing symbolised, and likewise their position above or below: as w^a river water, good; or w_a ditto, bad. P_a people *run* (from ships), who are, generally, the worst characters.

As the subsidiary signs are independent of each other, any number of them may be employed at convenience: as †' water scarce, but good; †, water scarce and bad; ‡,, water by digging, in plenty, but very bad.

The notation is thus comprised in a primary or class *symbol*, a *quantity-sign*, and a *variety-sign*.

The vacant spaces following the names of places being, by this plan, turned to account, much important information is inserted without increasing the size of the volume.† It is also proper to observe that, as the signs represent ideas or things, and not words (with a few exceptions), the system is independent of any particular language.

The abbreviations and symbols used in the Table are, for reference, alphabetically arranged in the following

* A special notation for this purpose is much required. In Purdy's "Sailing Directions," both the magnetic and the true bearing are given in order, as "the bearing and distance of the Capes Teulada and Malfatan are E. $\frac{1}{2}$ S. [E. $\frac{1}{2}$ N.] 8 miles."

Here E. $\frac{1}{2}$ N. refers to the *true* compass; but this can only be known by referring to the notice at the beginning of the book, unless the reader is aware that the variation at the place is westerly. The italic letters are already required for those passages in which, from the importance of the remark, the whole sentence is italicised; but the notation E' $\frac{1}{2}$ S' presents every advantage which a notation should possess: it is perspicuous, unequivocal, concise in the extreme, and elegant.

We must be careful to accent *all* the letters: thus N' E', not N E'; for this last combining true N. and magnetic E., presents no idea which occurs in practice.

A second accent denotes, further, local deviation, as N'' E'', which shews, at once, that there are two corrections necessary to reduce it to true NE. This notation would remove much of the difficulty which often arises in endeavouring to combine bearings taken under different circumstances.

This notation need not, from the nature of the case, appear in ships' logs.

† It is no part of our design to enter all information which can be conveyed in symbols. A few leading points have been inserted where it seemed advisable; the reader must refer for other details to the Sailing Directions, or to voyages. The symbols, however, will answer the further purpose of affording the means of making extracts, or of taking notes, of certain particulars, in a very small space, and in a very short time.

GENERAL VIEW.

- ⦿ (Anchor) Anchorage for large vessels.
 ⦿ good do. ⦿, bad do. ⦿, no do.
 ⦿ do. for smaller vessels.

⦿ good do. T, bad do.

- ⦿ Harbour for large vessels, or having always 3 fathoms water.

- ⦿ Harbour for smaller vessels, or having at times less than 3 fathoms.

The depth at H.W. and L.W. springs is denoted by the figures annexed above and below.

Ex. 1. ⦿²⁰₁₂, 20ft. at H.W. and 12ft. at low.

Ex. 2. ⦿¹⁵₀, 16ft. at H.W. and dry at low water.

When the depth at high water, of a harbour which dries at low water, is not known, it is expressed (for the present) by the letter n, implying some number not given; ex. Stonehaven, ⦿ⁿ₀.

Note.—In cases in which these details are not well known vacancies are left, which will be filled up on a future occasion.

- ⦿ Ball.

⦿¹, Time ball dropped at 1 P.M.

bk. Bank.

B. Bay.

bl. Bell.

bl. blue.

bl. black.

~ Birds. As birds frequent some places in preference to others, they may afford a means of identification.

⦿ (Boathook).—See Landing.

T Bold to.—See Component Signs, 1, 2.

[] Brackets.—See Component Signs, 5.

⦿ Break, or breakers.

⦿₀ do. at times.

⦿ Brushwood (a tree without a trunk).

b Burn (or fuel).

⦿ (fuel enclosed), a coal dépôt; coaling station for steam-vessels.

On some of the shores of the Polar Sea, and elsewhere, b denotes *drift-wood*. In some places *peat*, as at New I. Falklands. Where trees or brushwood occur, the symbol b is omitted, as, though many woods do not burn when green, fuel may be picked up in such places.—See Table 11

C. Cape.

Cath. Cathedral.

c. Cable's length.

! (Note of admiration, surprise), denotes Caution, or calls attention, as Current!

⦿ Channel, or passage, passages.

⦿ Several channels; ⦿₁, chan. with 35fms.; ⦿₀ no channel.

At a river the symbol relates to the entrance.

Chap. Chapel.

Ch. Church.

⦿ Coal depot.

⦿ Cocoa-nut tree, or trees; [⦿] a clump of cocoa-nut trees; 2 [⦿] two clumps do., and so on.

Compass symbol.—See Compon. Signs, 3. crl. coral.

⦿ Danger, dangerous; ⦿⦿ dangerous in different places.

⦿ (no danger) safe.

d Days.

Depth of water, denoted by the no. under the mark —, as 3 four fms.; 3 f, 3 feet.

The depth is that at low water. The depth relates to the bar, where there is one.

Distance is expressed in leagues, or miles; as C. Lookout, rka. 1 l., implies rka. 1 league from the Cape; ⦿ 2m., dangerous 2 miles out; ⦿₀ ½m., no danger, may be approached within ½ a mile, ⦿₀ ¼c., safe at ¼ a cable distance; ⦿ - 2 l. a danger NE. 2 leagues.

Dk. yd. Dockyard.

Dry, or above water.—See Comp. Signs, 1.

E East. E' magnetic E.

Entrance.—See Channel.

extr. Extreme, extremity.

F after a light, denotes that the flame has a fixed, not a changing appearance.—See lt.

F denotes a lt. (flame) of a fixed character, but only shewn occasionally.—See General Rules, No. 4, p. 399.

Fl. after a lt. denotes flashes.—See lt.

fl. Flag.

fl. st. Flag-staff.

Hd. Head.

A High.

ho. house.

hum. hummock.

I. Island.

The compass-symbol after an island shews the direction, or *lay*, of the longest diameter, and is followed by the length of this diameter in leagues, miles, or cables.

Ex. 1. $\frac{3}{4}$ 3m. denotes NNW. and SSE. (true), and extending 3 miles.

Ex. 2. EW $6\frac{1}{2}$ m. denotes lying E. and W. (true), extent $6\frac{1}{2}$ miles.

Note.—These bearings are all TRUE.

The bearing, though given to 2 points only, is near enough for the purposes required, as it can be in error only 1 pt. The distance is noted with more or less precision, according to the case, and is not always to be taken as an exact measure.

When the extent is very small, the bearing or direction is omitted; as Rockal, [2c.], or 2 cables in extent.

I after a light, denotes intermitting.—See lt.

Is. Islands. The compass-symbol and distance following shew the extent and general direction of the group, as described above in Id.

The number after Is. denotes the number in the group, as Wallis Is. 9.

l Landing (a boathook, the hook to the ground); l. no landing; ll, landing at times; l' good do.; l, bad.

L Leagues. When a number of leagues follows next to the name, it denotes the number of leagues the place is visible—as Tiger L. 17 l., denotes visible 17 leagues. When the L. stands next after a compass indication, it implies of course a distance measured in the given direction; as Is. $\frac{3}{4}$ 5 l., islands NW 5 leagues.

/ low.

lt. light. The capital letter next after the light denotes the *character of the flame*, as F fixed, I intermittent, R revolving, Fl. flashing or varied by occasional flashes, or rapid change in the intensity.

The number of feet (which stands the last among the particulars of the light) denotes the *height* of the lantern or flame above high water. Where this is not known, the range in miles is inserted.

When a lt. stands on a *summit*, the abbreviation *sum.* is inserted; when, therefore, *sum.* does not appear, the lt., however high, is usually not on the summit.

ts. The compass indication and no. of feet next after 2 lts., denote their

bearing and dist. asunder—the spectator looking at them from the sea; thus, the Lizard Is., lying N 72° E and S 72° W, are seen in one, from a ship to the westward, or towards the ocean, in the direction N 72° E.

Note.—These bearings are all TRUE, and they are intended to afford a means of determining the state of the compass when the ship is in a line with the 2 lts. in one.

m. miles.

After a shoal or danger, denotes the distance; as rf. 3m., a reef 3 miles distant.

mid. middle.

Mk. or mk. mark.

mo. mouth.

Mt. mount.

N North. N' magnetic N.

† Palm-tree.

() Parentheses, contains extra or additional information.—See p. 389.

Passage.—See Channel.

Patch.—See Compon. Signs, &

Penins. Peninsula.

P People—or peopled.

P. Uninhabited.

P' People of favourable character.

P,—of unfavourable do.

pk. Peak.

Pt. Point, being part of a name, as Hartland Pt.

pt. point.

R River. After a lt. denotes *revolving*.

r red.

rf. Reef.

rf, rf. always dry; rf, rf. always covered; rf, rf. awash.

r Refreshments, that is, vegetables, fruit, and meat.

As fish is often procurable where there are neither vegetation nor inhabitants, it is expressed by the separate symbol F, denoting r under the water.

— Rising gradually. — Rising in the middle, as I. Fuerte.

rk. Rock.

rk, dry; rk, sunken; rk, awash.

The number under a line, a 2, denotes the depth in fms. over a sunken rk.

rks. Rocks; a compass indication, with a number of miles or cables, denotes the extent, as described under Island.

rky. rocky.

S South. S' magnetic S.

— Saddle-shaped, as Huafo I., a valley.— See Sloping. Rising.

sd. Sand, or sandy.

This quality is noticed occasionally, as sand often affords water, it is used in cleaning, and turtles lay their eggs in sand.

sp. wh. white.

* Seamen are generally content with the mere fact of revolution or intermission, and do not trouble themselves to measure the interval. This, therefore, is an occasion on which it is very useful to be able to count seconds, for all persons do not carry seconds watches, and it is not always possible for the same person to hold the watch to a lamp and to see the light at the same instant.

The lighthouse, or building, being useful as a guide by day, many lighthouses are accordingly painted in order to answer this second purpose.

All the distances given in the Admiralty Light Lists and on the charts for the visibility of lights are calculated for a height of an observer's eye of 15 feet. The table of distances visible due to height, at end of each Light List, affords a means of ascertaining how much more or less the light is visible should the height of the bridge be more or less. The glare of a powerful light is often seen far beyond the limit of visibility of the actual rays of the light, but this must not be confounded with the true range. Again, refraction may often cause a light to be seen farther than under ordinary circumstances.*

The power of a light can be estimated by remarking its order, as given in the Light Lists, and in some cases by noting how much its visibility in clear weather falls short of the range due to the height at which it is placed. Thus, a light standing 200 feet above the sea, and only recorded as visible at 10 miles in clear weather, is manifestly of little brilliancy, as its height would permit it to be seen over 20 m. if of any power.

The Admiralty Light Lists, corrected yearly, should always be consulted as to the details of a light, as the description in the Sailing Directions may be obsolete, in consequence of changes made since publication.

4. *Compass-names of Points of Land.*

Navigators and hydrographers have not hitherto adopted any constant rule in the application of *compass-names* to the projecting angles of land. Thus, Krusenstern says (Mém. Hydr. ii. p. 283), "The north point of Owhyhee, which Vancouver calls the west point," &c. This extreme diversity of expression establishes the necessity of a systematic employment of such terms.

The north point of an island may be considered, 1. as that point which is to the northward of the middle or *body* of the island; or, 2. as the northernmost or *extreme* north point. In a circular island both terms agree, but in irregular forms they are ambiguous; thus Krusenstern calls the S. extreme of Atooi, "the S.E. pt.," probably from its position S.E.-d of the body of the island.

It will, perhaps, be admitted, that, in a purely practical subject, such a

* It is not unlikely that a light may be found sufficiently powerful, by the addition of a proper reflector, to illuminate the clouds, and, in a fainter degree, the atmosphere itself, over a lighthouse. The pale light in which a distant town appears enveloped at night; the distinctness of the forms of the clouds over a large city, illuminated by its ordinary lamps; and the vivid glare diffused over the heavens by a fire, show that the atmosphere renders the reflected light visible at a considerable distance. It is merely a question of intensity. If a sunbeam were admitted through a hole in the earth in a dark night, it would appear in the atmosphere as a column of astonishing splendour. As the light suggested would have a conical or shaft-like appearance, and would exhibit no flame, its proper designation would be a *shaft-light*. The shaft might, by the disposition of the reflector, be vertical, or inclined seawards or landwards, or be kept in motion, and the effect would be a great relief to the already exhausted resources for varying the appearance of lights.

This idea of Raper's is now carried out, and the illumination of the clouds by the new Electric Flashing Light at Ushant has been seen from a distance of 70 miles.

mode of expression should be selected as is best adapted to *application*, provided no error be thereby involved. But, in this question, both efficacy in practice and precision of language concur in directing the use of terms according to their *absolute significations*. Thus, if we call a southerly point of Atooi the "S.E. pt.," we leave it doubtful whether there is land to the southward or not; and, therefore, a ship could not, without reference to the chart, venture to run; but if we call the south point by the proper term, this doubt is not suggested, since the word "south" declares that no other part of the coast projects so far to the southward.

Accordingly, in this work, the compass-names N., S., E., or W., denote the extreme projecting point in that direction, without regard to the figure of the rest of the coast.

A point which is an extreme both in latitude and longitude, as, for ex., the S.E. projecting Cape of Samar (Philippines) we call what it is, namely, the South *and* East extreme, and so of the S. and W., N. and E., N. and W. points.

[1.] *Ambiguous Terms.*

Another case in which serious ambiguity may arise from the want of critical rules in such matters, and which may with propriety be noticed here, occurs in such phrases as "the Lizard lights in one clear the Manacles to the eastward." This is intended to imply that the ship passes to the eastward of the *rocks*; but, by omitting all mention of the ship, the bearing might be supposed to relate to the rocks, as would be the case if another verb were put for "cleared," as "saw the M. to the eastward," in which cases the ship is clearly to the westward. If the sentence ran "clear the ship to the eastward," no obscurity could exist, yet "clear the M. to the eastward," also puts the ship to the eastward. There must be something very defective in an expression which keeps the same meaning when reversed.

It would be well to adopt the rule that the bearing specified should relate to the thing mentioned, and not to anything else absent or understood; thus, in the above phrase, the term "eastward" should be held to relate to the rocks, and not to the ship, just as in "clear the ship to the eastward," it relates to the ship, and not to the rocks.

It might be dangerous to force a reform too suddenly in technical expressions, however vicious; but, on the other hand, no expression can maintain its ground when proved to be wrong. In the meantime it will be proper to use a fuller form of phrase, such as "clear the M., leaving them to the westward." In the course of time, "leaving them" would be dropped, and we should have the expression in its correct form, the bearing relating to the thing mentioned.

Some ambiguity necessarily attaches to the word "pass," because it is both active and neuter; thus, "passing an island to the westward," does not altogether declare whether the ship passes to the westward or leaves the island to the westward.

It is often, in like manner, a matter of doubt whether bearings given in the description of a light relate to the light itself or to the spectator: thus, "a light obscured from N. to E." may mean either "invisible from the N.E. quarter" (that is, when bearing S.W.-d), or "invisible to a spectator in the S.W. quarter" (or bearing N.E.)

This ambiguity is removed by the same rule, which supposes the spectator always in the centre of the compass, and, therefore, that the bearing specified relates to the point mentioned. The above phrase should, therefore, be held to mean the light invisible when bearing between N and E.

TABLE 11. PLACES AT WHICH DOCKS, WET OR DRY, OR SLIPS, MAY BE FOUND, REPAIRS MADE, COALS OBTAINED, &c.

This Table has been corrected from the most recent information. For fuller details see the Admiralty Dock Book for 1890.

TABLE 12. NAVIGABLE DISTANCES.

This Table, in former editions, afforded the means of estimating approximately the length in days of passages from port to port, but steam having made the table obsolete, it has been replaced by one showing the Navigable Mercatorial Distances in Nautical Miles between the Principal Ports of the World, arranged geographically. The sailor, knowing the speed at which his vessel can be driven in fair weather and foul, also the probable force and direction of the winds and currents he is liable to meet during the voyage, will be able by Table 12 to quickly make a fair estimate of the time of arrival at the port or ports to which he may be bound.*

There is some difficulty in giving at sight the distances between ports lying in different oceans. An attempt has been made to connect the first-class ports by inserting auxiliary tables where the distances between London, Liverpool, &c., and the Chinese and Australian ports are directly given. In other cases a little addition will be necessary. Care has been taken to give prominence to the great corners or turning-points of the world, as Gibraltar, Aden, Galle, Cape Leeuwin, Pernambuco, Cape Verde, &c.

The Mediterranean tables are connected with the principal ports in both hemispheres by tables from Gibraltar and Port Said.

Required the distance between Vera Cruz and Brisbane by Cape of Good Hope; by Cape Horn; and by Suez Canal; also between Genoa and San Francisco; and Famagousta and Zanzibar.

Vera Cruz to Pernambuco . . .	4,205	Vera Cruz to Pernambuco . . .	4,205
Pernambuco to Cape of Good Hope . . .	3,346	Cape Horn to „ . . .	3,289
Cape of Good Hope to Brisbane . . .	6,680	Brisbane to Cape Horn . . .	5,995
	<u>14,231</u>		<u>13,489</u>
Vera Cruz to Gibraltar . . .	5,044	Genoa to Gibraltar . . .	852
Gibraltar to Port Said . . .	1,920	Gibraltar to San Francisco . . .	12,569
Port Said to Brisbane . . .	8,698		<u>13,421</u>
	<u>15,662</u>		
Genoa to Port Said . . .	1,428	Famagousta to Port Said . . .	250
Port Said to Hong Kong . . .	6,465	Port Said and Zanzibar . . .	3,108
Hong Kong to San Francisco . . .	6,444		<u>3,358</u>
	<u>14,337</u>		

* It must be remembered that ships in sailing or steaming round the world, *gain a day* in their reckoning, going *East*; and *lose a day* going *West*. This alteration of date may be attended with some embarrassment if care is not taken to insure accuracy, by referring the days and hours of departure and arrival to Greenwich time by means of the Greenwich Date: See No. 481 and "Variation of Time at Sea," p. 354.

A short rule to estimate day and hour of arrival for steamships crossing the Pacific Ocean is: Going *West*: Add one day to assumed time of length of passage, and subtract the Diff. Long. *in time* between the two ports. Going *East*: Subtract one day from assumed time of passage, and add the Diff. Long. *in time*.

TABLE 13. TIME SIGNALS.

This Table shews, for all parts of the world, where the Time Signals are made from which the error of the chronometers on Greenwich Mean Time can be obtained, and by which, if the length of stay permits, they can also be rated. For more detailed information see List of Time Signals, published yearly by the Admiralty.

TABLE 14. EPOCHS OF YEARS AND MONTHS.

The Table contains the Epochs for certain years, and for the first day of each month.

The Epoch for the year is the moon's age on January 1st. The Epoch for the month is her age on the first day of the month, supposing her to change on January 1st at noon.

As a mean lunation is $29^d 12^h 44^m$, the moon describes, in 365 days, twelve complete lunations, and $10^d 15^h$ of the thirteenth; hence, on each 1st of January her age is $10^d 15^h$, on the average, more than on the preceding 1st of January, and $11^d 15^h$ if the preceding year was leap year.

TABLE 15. SEMI-MENSTRUAL INEQUALITY.

The Table contains the Semi-menstrual Inequality for the places enumerated. Its use is shewn in the examples, p. 342. The Table was constructed by combining together the several semi-menstrual inequalities of the places specified, together with a few observations at St. Helena, to which place, also, the Table therefore may be applied.*

TABLE 16. RISE AND FALL OF THE TIDE.

The Table shews approximately the space through which the surface of water rises or falls at given intervals from high or low water. It is entered with the said interval at the top, and the range for the day at the side.

Ex. 1. It is high water at a dock-sill at $11^h 20^m$ A.M., and the water is 31 ft. deep, the range is 24 ft.: find the depth at $12^h 15^m$. From $11^h 20^m$ to $12^h 15^m$ is 55^m (or 1^h); then under 1^h , against 24 ft., is 1.6, which is the fall of tide in 1^h , and being subtracted from 31 ft., leaves 29.4, the depth required.

Ex. 2. It is low water at $4^h 50^m$ P.M., and the depth is 2 ft. At a place where the range is 17 ft. find the depth at $8^h 30^m$. $3^h 40^m$ and 17 give 11.4, which, added to 2, gives 13.4, the depth required.

If the range for the day is not known, a rough estimate may be formed from the spring and neap ranges.

The Table may serve for reducing, approximately, the soundings taken at any particular time of the tide to the low-water depth. Thus, the depth 10 feet is obtained at $1^h 50^m$ after low water: the range between this low water and the succeeding high water is 11 feet; then $1^h 50^m$ and 11 give

* I am indebted for this useful table to the late Mr. Dessiou, of the Hydrog. Office, master in Her Majesty's navy, who was employed at the Admiralty in reducing the greater part of the tide observations made at our ports for many years; a task which Dr. Whewell considers, in the amount of labour and in the judgment displayed in the mode of proceeding, as not inferior to any discussion of large masses of astronomical or other observations by modern calculators, and of which some idea may be formed from the circumstance that London alone furnished 13,000 observations.

0·8, which, deducted from 10 feet, leaves 9·2 feet, the reduced low-water depth. The results are only approximate. It has been remarked, at least at some places, that the rise and fall do not correspond, and that the water falls more rapidly at first.* Care must be taken in using this Table where there is a large Diurnal Inequality (see Nos. 926-928).

To compute a Term. With the time from high or low water as a course, and the Range as dist., find the diff. lat., and subtract it from the range; the remainder is the rise or fall.

NAUTICAL ASTRONOMY.

REDUCTION OF THE ELEMENTS IN THE "NAUTICAL ALMANAC."

THESE Tables are used in the rules from p. 205 to p. 228.

TABLES 17 AND 18. ARC AND TIME.

These Tables contain the corresponding divisions of Time and Arc. Their use has been exemplified in Nos. 570 and 572.

TABLE 19. CORRECTION OF THE SUN'S DECLINATION AT NOON AT SEA, FOR LONGITUDE AND TIME.

This Table contains the correction for the sun's declination at noon, as taken out of the Naut. Alm. or Table 60, for reducing it to any other long. than that of Greenwich, or to any other hour of the day than noon. The correction is the variation of the declination, and, as it depends chiefly on the declin. itself, the declin. is employed as the argument instead of the day of the month.

The Table is entered with the declin. at the top, and the Long., or the time, at the side. See examples, No. 579.

TABLE 20. CORRECTION OF THE EQUATION OF TIME AT NOON, AT SEA, FOR LONGITUDE AND FOR TIME.

The Table is entered with the daily variation at the top, and the longitude, or the time, at the side; the correction, in the body of the Table, is in seconds of time. See the examples, No. 583.

TABLE 21. FOR REDUCING DAILY AND 12-HOURLY VARIATIONS.†

This Table shews the proportional part for each half-hour of the 24^h, or each 15^m of the 12^h, corresponding to any daily or 12-hourly variation from 1' to 30', or 1" to 30".

* With such irregularity will also be taken that called *tide and half tide*, in some places where the fall of the water is checked about half ebb, and a temporary rise takes place, as in the superior height of the night tides in the river Columbia, observed by Sir K. Belcher.

† For the design of this very convenient table I am indebted to Capt. W. Ramsay, R.N.

When the variation exceeds 30, take the parts for 30 and for the excess above 30.

Consider minutes of time above 0^m or 30^m as hours, and write the min. of the proport. part as seconds, and the seconds as thirds.

Examples are given in No. 580, and many others.

For extreme precision, the even columns (2', 4', &c.) only must be used, because the odd columns are often $0''\cdot05$ in defect, as are all those for $30''$.

The Table serves for reducing the R.A. and Decl. of the sun and planets, the Equation of Time, the Moon's Horizontal Parallax, and Semi-diameter; and also for various other purposes, as proportioning for the rate of a watch, the drift of a current, &c.

TABLE 21 A. LOGARITHMS FOR REDUCING DAILY VARIATIONS.

This Table contains logarithms for reducing 24-hourly variations. Its use is described in No. 597 (2).

To compute a Term. From the const. $3\cdot15836$ (the log. of 1440, the number of min. in 24^h , or of seconds in 24^m) subtract the log. of the given time or arc; read hours or degrees as min., and min. as seconds.

$$\begin{array}{rcl} \text{Ex. 1. Find the Log. for } 11^h 28^m. & & \\ \text{Const. } 3\cdot1584 & & \\ 11^h 28^m = 688^s \text{ log. } 2\cdot8376 & & \\ \text{Log. req. } 0\cdot3208 & & \end{array}$$

$$\begin{array}{rcl} \text{Ex. 2. Find the Log. for } 21' 27'' & & \\ \text{Const. } 3\cdot1584 & & \\ 21' 27'' = 1287'' \text{ log. } 3\cdot1096 & & \\ \text{Log. req. } 0\cdot0488 & & \end{array}$$

TABLE 22. FOR REDUCING THE MOON'S DECLINATION.

The Table is entered with the difference for 10^m (from the Naut. Alm.) at the top, and the minutes of the Greenwich Date at the side.

Ex. Green. Date, $11^h 27^m$, Diff. for 10^m , $136''$.

$$\begin{array}{rcl} 27^m \text{ and } 130'' & & 5' 51' \\ 6 & & 16\cdot2 \\ \text{Proportional Part} & & 6 \quad 7\cdot2 \end{array}$$

The parts may be taken out to the seconds of the Greenwich Date by reading minutes as seconds, and seconds as thirds.

TABLE 23. ACCELERATION.

This is the change of the sun's mean Right Ascension in a mean solar day. It is employed in reducing the Sidereal Time at mean noon to the Green. Date, and in converting Mean Time into Sidereal Time.

The Acceleration is itself a portion of Sidereal Time.

TABLE 24. RETARDATION.

This is the change of the sun's mean Right Ascension in a sidereal day. It is employed in converting Sidereal Time into Mean Time.

The Retardation is itself a portion of Mean Time.

For examples of the use of these two Tables, see Nos. 585, 602, &c.

TABLE 25. FOR FINDING THE EQUATION OF SECOND DIFFERENCES.

The use of this Table is described in No. 599. The column headed 1^h (which may be read 1° or $1'$) is adapted to all tables in which the intervals are sexagesimally divided.

To compute a term. Multiply half the difference between the Tabular Interval and the proposed Interval by the latter, and divide the product by the square of the Tabular Interval.

Ex. Tabular Interval 12^h , Proposed Interval $5^h 40^m$, or $5^h 7$

Tab. Int.	12^h
Proposed	$5^h 7$
	$\frac{6^h 3}{6^h 3}$
Half Diff.	$3^h 1$

then $\frac{3^h 1 \times 5^h 7}{144} = 0.1227$, the multiplier.

TIMES OF CERTAIN PHENOMENA.

These Tables are employed in the methods, p. 205, &c.

TABLE 26. APPARENT TIME OF THE SUN'S RISING AND SETTING.*

The Table is entered with the Latitude at the side, and the Sun's Declination, at the *top*, when these are of the *same* name; but at the *bottom* when of *contrary* names. Thus, in lat. 31° N., the sun, when in 4° S. decl., rises at $6^h 10^m$ A.M., and sets at $5^h 50^m$ P.M.

This is the *Civil Time* of the rising or setting of the sun's *centre*, to the eye at the level of the sea, and without the atmosphere. For greater exactness see No. 638.

To compute a Term. See Nos. 620, 621.

TABLE 27. APPROXIMATE APPARENT TIMES OF THE MERIDIAN PASSAGES OF THE PRINCIPAL FIXED STARS.

TABLE 27 A. CORRECTION OF THE TIMES IN TABLE 27.

The times are given in Table 27 for the 1st of each month, and the meridian of Greenwich. To find the time of passage for any other day, *subtract* the portion of time corresponding to the day of the month in Table 27 A from the time in Table 27. For an ex. see No. 625.

The Table is adapted to 1902, but will be within 2^m for many years.

TABLE 28. CORRECTION OF THE MOON'S MERIDIAN PASSAGE.

The Table is entered with the Daily Variation at the top, and the Longitude at the side.

The Daily Variation in W. long. is the difference between the time of the moon's transit on the given day and the next; in E. long. it is the difference between the moon's transit on the given day and the day before.

In W. long. *add* the correction to the time of meridian passage on the given day; in E. long. *subtract* it.

* This is the apparent (not mean) time of the true (not the *visible*) rising or setting.

Ex. 1. May 9th, 1870, long. 51° W.:
required the time of the Moon's Mer. Pass.

Mer. Pass. N.A. 9th	$7^h 17^m$
10th	$8 \quad 9$
Daily Var.	$\underline{52}$
Corr. for 51° W.	$\underline{7}$
	$\underline{7 \quad 17}$
TIME req.	$7 \quad 24 \text{ P.M.}$

Ex. 2. July 25th, 1870, long. 132° E.:
required the time of the Moon's Mer. Pass.

24th	$21^h 29^m$
23d	$\underline{20 \quad 39}$
Daily Var.	$\underline{50}$
Corr. for 132° E	$\underline{-18}$
	$\underline{21 \quad 29}$
	$\underline{21 \quad 11}$
TIME req.	$9 \quad 11 \text{ A.M.}$

TABLE 29. HOUR-ANGLE AND ALTITUDE OF A BODY UPON THE PRIME VERTICAL.

The Table is entered with the Declination at the top, and the Latitude (of the *same* name) at the side.

Ex. Lat. 50° and \odot 's Declin. 10° , give his Hour-Angle $5^h 26^m$, and Alt. $13^{\circ} 2'$, or $13^{\circ} 12'$.

The alt. which, partly for space and partly for distinction, is noted to the nearest $0^{\circ} 1'$, or $6'$, will not be in error on this account more than $3'$. Thus the alt. $13^{\circ} 1'$, which is properly $13^{\circ} 6'$, may be between $13^{\circ} 3'$ and $13^{\circ} 9'$; but $13^{\circ} 2'$ is $13^{\circ} 0'$, and $13^{\circ} 10'$ is $13^{\circ} 2'$. Hence, taking $13^{\circ} 1'$ as $13^{\circ} 6'$ cannot entail an error exceeding $3'$. The error will generally be less.

This alt. being the *true* alt., the sun or a star will pass the prime vertical at an alt. *greater* than the alt. given, by the diff. between the true and obs. alts.; the moon, on the contrary, at a *lesser* alt., by this amount.

As no star of which the declin. is greater than the lat. passes the prime vertical, such cases do not appear in the table.

The Table shews at once, roughly, the effect of an error of 1° of lat. in determining the time by a single altitude in the most favourable case.

Ex. Lat. 45° N., Decl. 3° N., the times are the same for 3° or 4° of latitude; that is, a gross error of lat. is of no consequence in computing the time of passage. But if the body have 23° of declin. an error of 1° of lat. will cause an error of 3^m or 4^m in that time.

By reversing the lat. and declin., the hour-angle and altitude become those of a body at its greatest elongation, or azimuth, from the pole.

To compute the Hour-angle, see No. 619. To compute the Alt., see No. 665.

ALTITUDES.

These Tables are used in the rules, p. 280, &c.

TABLE 30. APPARENT DIP OF THE SEA-HORIZON.

This is the angular depression of the sea-horizon below the true level, in ordinary states of the atmosphere, and when the sea and air are of equal temperature.

The apparent dip is the true depression (Table 8), diminished by about $\frac{1}{4}$ of itself. As this correction varies with the state of the air near the horizon, altitudes taken at sea, especially low altitudes, are not to be depended on where great accuracy is required. See No. 208.

TABLE 31. MEAN ASTRONOMICAL REFRACTION.

The Refraction is given for the barometer at 30 inches, and Fahrenheit's thermometer at 50°, according to Ivory.* The diff. to 10' of alt. is inserted.

Ex. 1. The refraction at 20° is 2' 39'.

Ex. 2. The refr. to the alt. 38° 35' is 1' 13''·3, deducting ·2, or 1' 13''·1.

The tenths of seconds are omitted at altitudes below 35°, on account of the uncertainty at low altitudes.

To find the Refraction approximately. With the alt. as course and dep. 58, find the D. Lat.; this is the refraction in seconds. For the refr. is proportionally to the tang. of the zen. dist., and is 58''·2 at zen. dist. 45°

Ex. Alt. 10°, as course, and Dep. 58, give 329'', or 5' 29'', the refr. required.

TABLE 32. CORRECTION OF THE MEAN REFRACTION FOR THE HEIGHT OF THE THERMOMETER.†

The Table is entered with the Alt. at the top, and the degree of Fahrenheit's therm. at the side. When the therm. is *below* 50°, the correction is *added* to the mean refr.; when *above* 50°, it is *subtracted*.

Ex. Alt. 17° 10', therm. 72°; the corr. is 8'', which, subtracted from the mean refr., 5' 7'', gives the true refraction 2' 59''.

To find the Correction, nearly. Multiply the mean refraction in seconds by 2, and by the difference between the height of the therm. and 50°, and divide the product by 1000.

Ex. Alt. 5°, therm. 38'. The mean refr. 9' 54'', or 594'', mult. by 2 and by 12, is 14256, and this divided by 1000 gives 14''.

TABLE 33. CORRECTION OF THE MEAN REFRACTION FOR THE HEIGHT OF THE BAROMETER.

The Correction is given to each tenth of an inch. The Table is entered like Table 32. When the barom. is *above* 30 inches, the correction is to be *added*; when *below*, *subtracted*.

Ex. Alt. 17° 10', barom. 29·2 in.; the corr. is 5'', and true refr. 3' 2'.

To find the Correction. Multiply the mean refr. in seconds by the difference between the height of the barom. and 30 inches, and divide the product by 30.

Ex. (Above.) 3' 7'', or 187'', mult. by ·8, and divid. by 30, gives 5''.

* The refractions now used by astronomers are those according to Bessel. Ivory's exceeds these by 0·9'' at alt. 45°, by 2'' at alt. 20°, and 5'' at alt. 10°. The difference of the tables is scarcely worth a more extended notice.

† This correction involves the term $\frac{d^2\delta}{d\tau^2}(\tau-50^\circ)$. The term $\frac{d^3\delta}{d\tau^3}(p-30)$ is omitted as insensible.—*Phil. Trans.* 1823, p. 476.

TABLE 34. THE SUN'S PARALLAX IN ALTITUDE AND SEMIDIAMETER.

These are given for convenience on some occasions, but not for extreme precision.

To compute the Sun's Parallax in Altitude. Take the hor. par. in the Naut. Alm. as dist., and find the D. Lat. to the app. alt. as course.

TABLE 35. DIP OF A SHORE-HORIZON.

The Table shows the Apparent Dip to be used instead of the dip in Table 30, when the distant sea-horizon cannot be seen, and the altitude is observed from the water-line on the beach. The distance of this line may either be estimated nearly, as it is always less than the true dip due to the height of the eye (Table 8), or it may be found by the method No. 350.

To compute a Term. Take the diff. between the depr. to the eye (Table 8) and the dist. of the beach-line, and divide by twice this last; add the quotient to the app. dip in Table 30.

TABLE 36.*

This Table contains the scales of the Centigrade and Réaumur thermometers, corresponding (approximately) with that of Fahrenheit.

The zero of the two former, or the freezing point of water, being 32° of Fahr., and their boiling points 100° and 80° respectively, while that of Fahr. is 212° ; the following rules are derived for the conversion of the scales.

To convert the Centigrade into Fahrenheit. Multiply the degrees of the Centigrade by 9, and divide the product by 5. When the Centigrade degrees are above 0, add 32° to the quotient; when *below* 0 (or marked —), subtract it from 32° .

To convert Réaumur into Fahrenheit. Multiply the degrees by 9, and divide the product by 4. Apply the quotient as directed above.

Ex. Centig. — 11.7 , find Fahr. $11.7 \times 9 = 105.3$, this $\div 5 = 21.1$, which *subtracted* from 32° gives 10.9 .

To extend the Table. For the Centigrade add 0.555 , &c., and for Réaumur 0.444 , &c., for each 1° of Fahr.

TABLE 37.

This Table contains the English measures corresponding to the *Mètre*, *Kilomètre*, *Décimètre*, and *Millimètre*.† See p. 380. Thus 30 centim. are 11.81 inches; 3 kilom. are 1.618 nautical miles.

The barometer scale, in English inches, and millimètres (approximately), is annexed.

To reduce the French to the English barometer scale. Divide the millimètres by 25.4, the quotient is the number of English inches required.

* As numerous valuable works relating to Navigation are published by the French, and as other Continental nations frequently employ the language of that country in hydrographic documents, Tables 36 and 37 are added, for the ready reduction of such French measures as most frequently occur.

† The quantities are taken from the *Annuaire*, for 1846. The mètre is the 10-millionth part of the quadrant of a meridian.

When the French scale is given in inches and lines (or 12ths of an inch), multiply the inches by 1.065, the product is English inches.

To extend the barometer scale, add 2.54 millimètres for each 0.1 of an inch.

TABLE 38. CORRECTIONS OF ALTITUDE OF THE SUN AND STARS.

The Table contains the gross corr. of alt., or the corrections enumerated in No. 644, exclusive of index error, to the nearest tenth of a minute, using Bessel's Mean Refractions.

For examples, see No. 648.

TABLE 39. THE MOON'S CORRECTION OF ALTITUDE.

The Table contains the Correction to each minute of horizontal parallax and every 10' of alt.; for the barom. 30 inches, and Fahrenheit's therm. 50°.

Ex. The corr. to app. alt. 15° 30' and hor. par. 56', is 50' 31".

For seconds of parallax. Look among the columns on the right side of the page, and against the alt., and take out the seconds, which *add* to the correction.

For minutes of altitude. Take the seconds from the extreme right of the page, and apply them as there directed.

Ex. Moon's App. Alt. 35° 37', Hor. Par. 57' 32"; find the Correction of Altitude.

35° 30' and 57'	45' 3"
32", parts 26 }	
7 parts, -4 }	22
CORRECT. req.	45 25

To correct for the Barom. and Therm. Take the corrections from Tables 32 and 33, but apply them to the correction of alt. the *contrary way* to that directed. Ex., No. 655.

To compute a Term. Correct the app. alt. (of the centre) for refraction To the log. sec. of this alt. add the prop. log. of the horizontal parallax; the sum is the prop. log. of the parallax in alt. From this subtract the refraction; the rem. is the correction of alt.

The Table does not give the correction with precision at low alts.*

TABLE 40. CORRESPONDING HORIZONTAL PARALLAX AND SENIDIAMETER OF THE MOON.

As these two elements are generally required together, the Table renders it necessary to reduce the parallax alone to the Greenwich Date.

TABLE 41. DIMINUTION OF THE MOON'S HORIZONTAL PARALLAX FOR THE SPHEROIDAL FIGURE OF THE EARTH.

The Table is entered with the Horizontal Parallax at the top and the Latitude at the side; the seconds corresponding are to be *subtracted* from the equatorial hor. par.

The compression employed is $\frac{1}{800}$.

* In all these tables of refraction the eye is supposed at the level of the sea; when the observer is at very great elevations, low altitudes cannot be corrected with precision by the tables in common use. The refraction is in such cases too great.

TABLE 42. AUGMENTATION OF THE MOON'S SEMIDIAMETER.

The Table is entered with the Moon's Semidiameter at the top and her Altitude at the side; the seconds corresponding are the excess by which her apparent semidiameter at her actual altitude exceeds that at which it would appear if seen from the centre of the earth. See Nos. 439 and 440.

TABLES 43 AND 44. FOR CONVERTING TRUE INTO APPARENT ALTITUDES.

These contain the further correction necessary in reducing a true to an apparent altitude, after *adding* the refraction and *subtracting* the parallax. See Nos. 657 and 658.

TABLE 45. PARALLAX OF THE PLANETS IN ALTITUDE.

The Table is entered with the Planet's Horizontal Parallax at the top, and its Altitude at the side; and the corresponding seconds taken out.

To compute a Term. Enter the Traverse Table with the alt. as course and the hor. par. as dist., and take out the D. Lat.

TABLE 46. AZIMUTH CORRESPONDING TO THE CHANGE OF ALTITUDE IN 1^m OF TIME.

The Table shews the Change of Altitude in 1^m of Time at any Azimuth in Latitudes below 66°. The azimuth is reckoned either from N. or S.

Ex. In lat. 50°, at the azim. 40°, reckoned either from N. or S., the change of alt. in 1^m is 6' and some seconds.

The Table shews also, roughly, the true bearing when the change of alt. in 1^m is given. See also No. 677.

The column of 6' limits the azimuth for finding the time, No. 778.

LATITUDE.

THESE tables are employed in the rules in Chap. V., p. 243.

TABLE 47. LIMITS OF THE REDUCTION TO THE MERIDIAN AT SEA.

This Table shews how long before or after noon the sun's altitude may be observed, so that the Reduction shall not be *in error* more than 2' when the time is 1^m in error. The Table, therefore, shews the Limits of this method for common practice at sea.

If the time be in error, or doubtful, 2^m, 3^m, &c., the Reduction will, at the limits, be in error, or doubtful, 4', 6', &c. In like manner, if the error of time be less than 1^m, that of the Reduction will be less than 2', in the same proportion.

If the time is doubtful 2^m, 3^m, &c., and we require that the error of the Reduction shall not exceed 2', we must take for the limit $\frac{1}{2}$, $\frac{1}{3}$, &c., that set down; thus, if in lat. 48° N., decl. 10° N., the time be doubtful 3^m, we must take the alt. within $\frac{1}{3}$ of 28^m, and that is, 9^m from noon.

When the time from noon, of observation, exceeds the limits set down, the error of the Reduction (caused by 1^m error in the time) will exceed 2' in the same proportion; thus, in the above case, if the alt. be observed 56° from noon, the error of 1^m in the time will cause 4' error in the Reduction.

The time in the Table is that hour-angle, nearly, at which the number of minutes (of time) is equal to the number of minutes (of arc) in the Reduction.

To find this Hour-Angle. To the constant 0.4771, add the log. from Table 70; the sum is the prop. log. of the hour-angle required, in time.*

TABLE 48. VALUE OF THE REDUCTION AT WHICH THE SECOND REDUCTION AMOUNTS TO 1'.

The Table contains, against each Mer. Alt. under 85°, that value of the Reduction at which the 2d Reduction amounts to 1'; and therefore shews whether it is necessary or not to compute the latter.

Ex. Suppose the mer. alt. 68° and the (first) Red. computed to be 47', then the error of omitting the 2d Red. cannot amount to 1'; but if the 1st Red. were 54', the omission of the 2d Red. would cause an error of more than 1'.

One eighth of the quantity in this Table is that (1st) Reduction at which the 2d Red. amounts to 1".

Thus, in Ex. No. 707, p. 252, the mer. alt. is 60°, the value of the 1st Red. in the Table is 1° 3', 1-8th of which is 8'; hence, if the Red. exceed 8', the 2d Red. will exceed 1".

To compute a Term. To the constant 6.7648 (the sin. of 2'), add the log. cot. of the mer. alt.; half the sum (preserving 10 in the index) is the log. sine of the reduction required.

Ex.	Const.	6.7648
Mer. alt. 60° 50' cot.		9.7467
		2)16.5115
		8.2557

RED required 1° 2' log. sin.

To find the time from noon, or the hour-angle, to which this (1st) Reduction corresponds: from the log. sine of the Red. subtract the log. in Table 70, the remainder is the log. sine square of the time or hour-angle required.

Ex. 1. Lat. 60° N., decl. 14° N. (mer. alt. 44°), Red. 1° 24'; 8.388 - 0.130 = 8.258, the sin. sq. of 1° 1' 53", the hour-angle required.

Ex. 2. Lat. 29° N., decl. 17° S. (mer. alt. 44°), Red. 1° 24', gives 0° 47' 3".

These precepts concerning the Reductions are, of course, merely approximations near enough in practice.

TABLES 49 AND 50. FOR COMPUTING THE REDUCTION TO THE MERIDIAN IN SECONDS. See No. 707.

The seconds forming part of the 1st Reduction (Table 49) are taken out to the min. and sec. of the hour-angle. When the sun is observed in the forenoon, the Table is entered with the time from midnight, for convenience.

* Mr. Towson has constructed convenient tables for reducing an alt. observed near the merid. to the mer. alt., which are published by the Hydrographic Office (J. D. Potter, agent).

The seconds for the 2d Reduction (Table 50) are taken out for the hour-angle to the nearest 10^s.

To compute a Term in Table 49. To the const. 5.615455, add the log. sine square of the hour-angle; the sum is the log. of the number of seconds.

To compute a Term in Table 50. To the const. 5.6155 add twice the log. sine sq. of the hour-angle; the sum is the log. of the 2d Red.

Ex. Find the Reduction, and also the 2d Red., in seconds, for the hour-angle 28^m 4^s

	Const.		Const.
H. Ang. 28 ^m 4 ^s	sin. sq. 5.61545		sin. sq. $\times 2$ 5.615
	7.57341		5.147
REDUCT. 1544 ^m .8 log.	3.18886	2d RED. 5 ^m .8	log. 0.762

TABLE 51. CORRECTION OF THE ALTITUDE OF THE POLE-STAR AT SEA.

The Table is entered with the Altitude of the star at the top, and the Right Ascension of the Meridian at the side. The quantity taken out is to be applied to the star's true alt. as directed, ex. No. 773.

The last column contains the variation in ten years, which is always *subtractive* from the correction in the Table.

As the observation at sea is imperfect, the correction has been computed to whole minutes only.

The quantity is the D. Lat. answering to the star's hour-angle as course and 77^s as dist. (the star's pol. dist. in 1890), together with a second correction computed in No. 774.*

TABLE 52. REDUCTION OF THE LATITUDE.

This is the difference between the latitude as actually found by any astronomical observation and what it would be if the earth were a sphere, which last is called the *geocentric* latitude.

To reduce the lat. by observation to the geocentric latitude, *subtract* the reduction of latitude.

This quantity, which is also called the *angle of the vertical*, is 0 at the equator and at the pole, and is greatest in lat. 45°.

The compression assumed is $\frac{1}{308}$; that is, the polar radius is supposed to be shorter than the equatorial radius by $\frac{1}{308}$ of the latter.

LONGITUDE.

These Tables are employed in the methods, Chapter VII. p. 297

TABLE 53. CORRECTION OF THE LUNAR DISTANCE FOR THE CONTRACTION OF THE VERTICAL SEMIDIAMETER.

The Table is entered with the Alt. at the top and the Angle contained between a plumb-line through the body, and the line joining the other body.† See No. 852.

* The Nautical Almanac method strongly recommended.

† The argument in this table, in the usual form, is the angle which the semidiameter in the direction of the other body makes with the *horizon*; but it is difficult to imagine the horizon where it is not, whereas the plumb-line is an absolute standard everywhere.

TABLE 54. ERROR OF OBSERVATION ARISING FROM AN ERROR IN THE PARALLELISM OF THE LINE OF SIGHT.

The Table shews the Error on any observed angle less than 120° , arising from the line of sight not being parallel to the plane of the sextant or circle. See No. 495 (3).

As the observer will not, knowingly, allow this adjustment to remain defective, or observe elsewhere than in the centre of the field when the adjustment is perfect, the Table serves rather to shew the consequence of such errors than for the purpose of applying a specific correction.

To compute a Term. To twice the log. sine of the error in the parallelism of the telescope, add the log. tan. of half the angle measured; the sum is the log. sine of the required error in the observed angle.

Ex. Error of parallelism $12'$, angle measured 97° : required the Error of the Angle.

$12'$ log. sin. 7.5429	$\times 2$ 5.0858
97° half, $48^\circ 30'$	tan. 0.0532
Error req. $2''.8$	sine 5.1390

TABLE 55. FOR CORRECTING THE LUNAR DISTANCE FOR THE SPHEROIDAL FIGURE OF THE EARTH.

The Table is entered with the Latitude and the Moon's Altitude. The numbers are noted to the nearest 10. See No. 853.

To compute a Term. To the log sine of the red. of lat. add the log. sine of the mean horizontal parallax (in Table 40= $57'$), and the log. sine of the alt.; the sum is the log. sine of a small arc, which multiply by 100.

TABLE 56. FOR COMPUTING THE MOON'S SECOND CORRECTION OF DISTANCE.

Enter the Table with the App. Dist. at the top or bottom, and the Moon's Corr. of Alt. at the side, and take out the seconds.

In the same column take out the seconds standing against the corr. of dist. (No. 842 or 844) at the side. The difference between the two numbers thus taken out is the 2d corr. required.*

When the Dist. is less than 90° , add; when greater, subtract.

Ex. App. dist. 48° ; \odot 's corr. of alt. $46'$; corr. of dist. $26'$: find the Second Corr.

48° and $46'$	$17''$
26	6
SECOND CORR.	$\frac{11}{11}$ to be added.

To compute a Term, approximately (1.) To square an arc in minutes. Find the square of the number of min.; divide it by 60: the quotient is the number of seconds in the square required, roughly. For greater accuracy, increase the quotient by $\frac{1}{30}$ of itself.

(2.) With the app. dist. as Course, and the said square as Dep. find the D. Lat.; half this is the term required.

* This 2d corr. may be dispensed with altogether by repeating the work, No. 844, p. 306 using the mean of each true and app. alt. and the mean of the app. and first found dist. The result, with care, will agree very nearly with the rigorous process.

kv. Corr. (of alt. or of dist.) 55', app. dist. 31°.

55 squared (by Table 8)	3025, divided by 60	50°·4
	add 1-20th	<u>2·5</u>
	Required SQUARE of 55'	53

Dep. 53 and Course 31° give D. Lat. 88; the term is 44".

TABLE 57. CORRECTION OF THE GREENWICH MEAN TIME FOR THE SECOND DIFFERENCE OF THE LUNAR DISTANCE.

This Table is entered at the top with the Approximate Interval, and at the side, with the Diff. of the Prop. Logs. standing against the two distances in the Nautical Almanac, which include the given true distance.

For an example, see No. 857.

To compute a Term, approximately. Multiply together the approx. interval in hours and tenths, its compl. to 3^h, the diff. of the prop. logs. above (attending to the decimal point), and 1400.

Ex. Approx. interval, 1^h 10^m, diff. prop. logs. 64;
then $1·2 \times 1·8 \times 0·0064 \times 1400 = 19$, the required term.

TABLE 58. THE ERROR OF THE SHIP'S PLACE AND OF THE LONGITUDE IN TIME, CORRESPONDING TO AN ERROR OF 1' IN THE LUNAR DISTANCE.

The Table is entered with the Latitude at the top, and the Prop. Log. against the lunar dist. in the Nautical Almanac at the side.

Ex. Lat. 50°, prop. log. 2800; an error of 1' in the lunar dist. will cause an error of 19 miles in the ship's place, in Departure, and 2^m 0^s ERROR OF LONG. IN TIME.

Since it is the actual distance of the ship from the shore that we are concerned with at sea, rather than the nominal diff. of long., this Table will afford a useful check on the supposed place of the ship in making the land by a lunar observation.

The error of long. in time is also the error of the G. M. Time, as determined by a lunar observation.

To compute a Term. Divide 2700 by the 3-hourly change in minutes; the quotient is the error in min. of long. in arc at the equator. For any particular latitude see No. 307.

TABLES FOR DETERMINING THE VARIATION OF THE COMPASS.

These Tables are employed in Chapter VIII. p. 326.

TABLE 59. AMPLITUDES.

The Table shews the True Amplitude of the sun (or of any other celestial body, having the same declination), at rising or setting. It is entered with the Decl. at the top and the Lat. at the side.

To find the Amplitude by the Traverse Tables. With 0 and the lat.

find M. With M as Dist., and the Decl. as Course, find the Dep. With 100 as Dist. and this Dep. find the Course.

By Computation. To the log. sec. of the lat. add the log. sine of the Declin.; the sum is the log. sine of the amplitude.

Ex. Lat. 17° , Decl. 23° : find the Amplitude.

Lat.	$17^{\circ} 0'$	sec.	0.0194
Decl.	$23^{\circ} 0'$	sine	9.5919
AMPLITUDE,	$24^{\circ} 7'$	sin.	9.6113

TABLE 59 A. CORRECTION OF THE OBSERVED AMPLITUDE.

The Table shows the Change produced on the Amplitude by the joint effect of the refraction at the horizon (assumed at $33'$), and the height of the eye, supposed 16 feet. An example is given in No. 886.

To find the correction for any other height of the eye. To $33'$ add the Dip, multiply the sum by the correction in the Table, and divide by 37; the quotient is the correction required.

Ex. Lat. 55° , decl. 23° , height of the eye 100 feet; 33 and 10 are 43, which, multiplied by 1.4 and then divided by 37, gives $1^{\circ} 6'$, the correction required.

TABLES TO SUPPLY THE PLACE OF THE NAUTICAL ALMANAC.

These Tables, which afford for several years approximate values of the quantities contained in them, are useful on various occasions, and may serve for the ordinary purposes of navigation. But when much accuracy is required, and whenever the moon is employed, recourse must be had to the Nautical Almanac.

TABLE 60. DECLINATION OF THE SUN.

The Table contains the Declination for each day of the years 1901, 1902, 1903, and 1904, to the nearest minute.

TABLE 60 A. CORRECTION OF THE SUN'S DECLINATION IN TABLE 60 FOR THE YEARS FOLLOWING 1901, &c.

The Table contains the Corrections by which the declination for any day on one of the four years enumerated may be converted into that for the same day on any following year, till 1928.

When the declination is *increasing*, add the correction; when *decreasing*, subtract it.

Ex. 1. Feb. 3rd, 1914, find the Sun's declination.

1914 answers to 1902.
1902, Feb. 3rd, $16^{\circ} 42' S.$ (decr.)
Corr. $1' 6'$, or -2
DECLIN. req. $16^{\circ} 40' S.$

Ex. 2. Sept. 27th, 1920, find the Sun's declination.

1920 answers to 1904.
1904, Sept. 27th, $1^{\circ} 34' S.$ (incr.)
Corr. $2' 8''$ $+3$
DECLIN. req. $1^{\circ} 37' S.$

If the correction when subtractive exceed the declination itself, take the less from the greater, and consider the remainder as the declination required, and of the *contrary* name to that given.

The correction is additive when the declination is increasing, and subtractive when decreasing, thus changing from one to the other at the equinoxes and solstices.

To compute this Correction for reducing approximately the declination of the sun for any year, by means of the declination for any four successive years, the following rule is given by Mackay, in his Complete Navigator.

Note the number of *fours* necessary to reduce the proposed year to one of the years in the table.

Take the difference of the declination (for the year thus found), to the given and following days. Multiply this difference by the number of fours, and divide by 83: the quotient is the correction required, in minutes.

Ex. (1. above.) 1890 reduced by fours gives 1878, the number of fours being 3.

The daily diff. of the decl. on the 3d and 4th is 18, which multiplied by 3 is 54, this divided by 83 gives about 1' 6", the CORR. required to be *subtracted*.

Since, at the equinoxes the correction changes suddenly from additive to subtractive, or from *sub.* to *add.*, and since applying it wrongly would cause an error of double the amount of the correction, it is advisable, in case of doubt, to find the declin. for some days before the equinox, and to subtract from it the daily variation, which at this season varies uniformly for several days.

TABLE 61. SIDEREAL TIME AND RIGHT ASCENSION OF THE SUN.

The Table contains the Sidereal Time for the years 1901, 1902, 1903, and 1904, to the nearest tenth of a minute.

N.B.—The Sun's Right Ascension to the nearest tenth of a minute may be found by applying the Equation of Time in Table 62 to the Sidereal Time as there directed. See p. 209, and Note, p. 211.

TABLE 62. THE EQUATION OF TIME.

The Table contains the Equation of Time for apparent noon for 1901, 1902, 1903, and 1904, to the nearest second. The Equation for each year will serve very well for common purposes for the 4th or 8th year afterwards. The error will be greatest from the latter end of May to the middle of July, when it may amount to 2^s or 3^s in a period of 4 years, or about 7^s in four or five such periods. Towards the beginning or end of the year the error will not much exceed 2^s or 3^s, even for a considerable number of years.

TABLE 63. MEAN PLACES OF THE PRINCIPAL FIXED STARS.

The Table contains the mean places of sixty-six stars, for the 1st of January, 1900. The mean places may be reduced for any antecedent or subsequent year by applying, as directed in the Table, the annual variation in R.A., and in declination, multiplied by the number of years exceeding 1900.

To find the place for any year prior to 1900, the variation must be applied the contrary way to that directed.

The right ascension and declination of every star change during the year. The change of right ascension is, for most of the stars in the Table, between 4" and 6"; that of declination between 15" and 40". Among the stars which change their right ascension least are Spica, and α Cygni, the

change being between 3° and 5° . The stars Capella, α Pavonis, and α Triang. Austr., change their right ascension about 6° , 7° , and 9° , respectively, during the year. These stars are therefore less favourable than others for finding the latitude by double altitude, or the time. The star α' Crucis changes its declination $\frac{1}{2}$ of $1'$ from one part of the year to another. The variation of the right ascension of Polaris amounts to more than 2^m ; that of declination to nearly $1'$. In this Table $+$ signifies *add*, and $-$ *subtract*.

As the variations of right ascension occupy several months, their effects would not be sensible in rating a chronometer by the method, No. 821.

As the stars are given in this Table for the purpose of finding the latitude or time in different parts of the world at any hour of the night, they are selected nearly equally from all parts of the heavens, and the list does not necessarily include all stars above, or exclude all stars below, any particular magnitude,

The figures 1, 2, 3, indicate the first (or largest), second, and third magnitudes. The figures 1, 2, denote a magnitude between the 1st and 2d; and the figures 2, 3, a magnitude intermediate between the 2d and 3d.*

LOGARITHMS

These Tables are used in those parts of the several computations which are effected by logarithms. The more general tables stand first, and the others follow nearly in the order already observed.

TABLE 64. LOGARITHMS OF NUMBERS.

The Table contains the logs. of numbers from 1 to 9999, to six places, with differences and proportional parts.

The diff. D. is the mean of the diffs. between each log. and the succeeding one in the same line; and is near enough for most cases.

1. *Direct process*; to find the logarithm of a given number.

1. To find the logarithm to any number consisting of two or three figures. Look for the number at the side, and take out the log. against it. Thus, the log. of 717 is 855519.†

2. To find the logarithm of a number consisting of four figures. Look for the three first figures at the side, and the fourth at the top; thus, the log. of 7176 is 855882.

3. To find the logarithm of a number consisting of more than four figures. Find the log. of the first four figures; find the diff. D. in the lower part of the Table, in column D, and against it, under the 5th figure (or 6th, if required), are the parts, which add.

Not.—Observe to set down the parts correctly, carrying those for the 6th figure one place to the right of the parts above them, as a mistake frequently occurs here.

* Sir John Herschel having, soon after the appearance of this work, favoured me with a communication respecting the magnitudes or relative brilliancy of the stars, to which that distinguished astronomer has paid particular attention, I have altered the numbers marked against several of the stars in the first edition.

† This, however, is only part of the complete logarithm, as adapted to the purposes of computation by logarithms, and requires the *index*. See Nos. 57 and 58.

Ex. 1. (<i>Five</i> figs.) Find the log. of 26574. 2657 log. 424392 D. 164 Against 1). 164, under 4 66 Log. req. 424458	Ex. 2. (<i>Six</i> figs.) Find the log. of 265748. 2657 log. 424392 D. 164 4 (parts 66) 66 8 (parts 131 ÷ 10) 13 Log. req. 424471
--	---

II. *Inverse Process*; to find the number corresponding to a given log.

1. When the natural number is not required to consist of more than four figures, it is taken out at once.

Ex. Given the log. 645820, required the natural number.

The nearest log. in the Table is 645815; the figures at the side are 442, annexing to which that at the top, or 4, gives 4424, the number required.

The placing of the decimal point is directed in No. 59.

2. When the Number is to consist of *five* figures. Take out the next less log. to the one given, and note down the four figures of the corresponding number. Note the diff. D.

Subtract this next less log. from the given one, and look for the remainder among the parts standing against D, in the lower part of the Table; note the figure at the top under which the remainder is found, and add it to the four taken out.

3. When the Number is to consist of *six* figures, the more direct and accurate method is to take the diff. between the given log. and the next less in the Table, annex 2 ciphers, and divide by the diff. between the next less and the next greater; the quotient is the number of figures to be annexed to the natural number, answering to the *next less* log.

The placing of the decimal point is directed in No. 59.

Ex. 1. (<i>Five</i> figs.) Find the No. to the log. 424471. Given 424471 Next less (2657) 424392 D. 164 Rem. 79 5th fig. 4, next less 66 Num. req. 26574	Ex. 2. (<i>Six</i> figs.) Find the No. to the log. 424471. Given log. 424471 Next less (2657) 424392 79 Next greater 424555 163 Then 7900 ÷ by 163, gives 48, and the numb. req. is 265748.
---	--

TABLE 64A.

Spheroidal Tables; showing the length in feet of a degree, minute, and second of lat. and long.; the corresponding number of statute miles in every even degree of lat.; and number of nautical miles contained in a degree of long. under each even degree of lat.

TABLE 65. NATURAL SINES, COSINES, &c.

These quantities are convenient for working problems such as that given in No. 254.

TABLE 66. LOG. SINES OF SMALL ARCS TO EACH SECOND.

The Table contains the log. sines from 0 to 1° 30' (or log. cosines from 88° 30' to 90°), to each second. Five places are given as far as 1° and six beyond. The Table is applicable to log. tangents, thus: to find the log. tan. add the log. sec. to the log. sine; to find the arc to a given log. tan., find it as for a sine, subtract from the given log. the log. sec., and consider the rem. as a sine

For 10ths of seconds proceed by proportion, or, in very small arcs, as directed for proportional logarithms. The last method is true in the 5th place for arcs under 5'.

TABLE 67 LOG. SINES OF SMALL ARCS TO TEN SECONDS.

The Table contains the log. sines from $1^{\circ} 30'$ to $4^{\circ} 30'$ (or the log. cosines from $85^{\circ} 30'$ to $88^{\circ} 30'$), to each $10''$, with parts for single seconds.

The parts are true for each $2'$ and $7'$ in the units' place of the arc, and very nearly for others, as the parts under $32'$ serve from $1^{\circ} 30'$ to $1^{\circ} 35'$, and those under $37'$, from $1^{\circ} 35'$ to $1^{\circ} 39'$. The error of using one column for the next will rarely amount to half a second.

The parts for the log. cos. are to be taken as for the sine of the compl. of the arc; thus, the parts for cos. of $87^{\circ} 42'$, being those for sine of $2^{\circ} 17'$ are found under $17'$.

Direct Process. Find the sine or cos. for the next less $10''$, *add* the parts for the sine, *subtract* those for the cosine.

Ex. 1. The log. sine of $2^{\circ} 22' 37''$ is 8.617417 for $2^{\circ} 22' 30''$, *adding* the parts under $12'$ for $7''$, or 356 , which gives 8.617773 . The log. cos. of $87^{\circ} 46' 14''$ is 8.590181 for $87^{\circ} 46' 10''$, *deducting* 218 (the parts for $4''$ under $12'$), or 8.589963 .

Inverse Process. For the sine look for the next less; for the cosine look for the next greater; note the deg., min., and $10''$.

Take the diff. between the sine or cos. taken out and the given one; look for it in the col. of parts; take out the corresponding seconds and add them.

Ex. 1. Find the arc to the log. sine 8.508462 .				Ex. 2. Find the arc to the log. cosine 8.758561 .			
Arc	$1^{\circ} 50' 50''$	Given	8.508462	Arc	$86^{\circ} 42' 40''$	Given	8.758561
		Next less	8.508321			Next gr.	8.758688
		Pts. at $32'$	141			Pts. at $17'$	127
Arc req.	$1^{\circ} 50' 52''$			Arc req.	$86^{\circ} 42' 43''$		

For extreme precision proceed by proportion.

The Table is used for tangents by the rules in expl. Table 66.

TABLE 68. LOGARITHMIC SINES, COSINES, TANGENTS, COTANGENTS, SECANTS, AND COSECANTS.

The Table contains the terms to half-minutes, and to six places.

The second column and the last but one contain a time scale, corresponding to the upper and lower degree; thus $73^{\circ} 33' 30''$ corresponds to $4^h 54^m 14^s$. This scale is very convenient for converting arc and time, but it is introduced to suit those rules in which the time itself is an argument.

The parts for each second are given, beyond 9° ; from 4° to 9° , to each $10''$; but under 4° the variation is too rapid for their insertion, and recourse will be had for precision to Tables 66 and 67.* The parts are true for the *middle* term of the argument; thus, the parts from $20^{\circ} 30'$ to $20^{\circ} 45'$, are true for $20^{\circ} 37\frac{1}{2}'$, and approximate for the rest, but the inaccuracy in the extreme case corresponds only to $\frac{1}{3}$ of $1''$.

It is, of course, the more correct way to take the parts with reference to the *nearest* term, and to apply them accordingly; thus, to find the sine of $9^{\circ} 40' 28''$, find it for $9^{\circ} 40' 30''$, and *subtract* the parts for $2''$.

* The diff. D., in the early portion (inserted merely for uniformity), is not that of two consecutive terms, but corresponds to *half* the tabular interval on *both* sides of a term. This is done to avoid breaking the continuity of the horizontal lines, which must occur when actual diffs. are exhibited, and is teasing to the eye.

For greater accuracy proceed by proportion.

Direct Process. When the given angle is less than 45° , its log. sine, &c. are taken from the top; when greater than 45° , from the bottom; thus, the log. sine of $28^\circ 17'$ is 9.675624; the log. sine of $84^\circ 3'$ is 9.997654. In like manner, the log. sine 9.452060 corresponds to the arc $16^\circ 27'$, the cotangent 9.47714 to the arc $73^\circ 18'$.

The log. sine of an angle is the log. cosine of the complement of the angle to 90° , whether in excess or defect; so, likewise, the log. cosine is the log. sine of the complement; and the like holds of the tangent and cotangent, secant and cosecant.

When the given angle exceeds 90° , find the log. sine, tangent, or secant, for the supplement to 180° . But it is generally easier to find the log. co-sine, co-tangent, and co-secant, for the excess above 90° .

Ex. 1. The log. sine of $127^\circ 50'$ is the log. sine of $52^\circ 10'$, or the log. cos. of $37^\circ 50'$, which is 9.897516.

Ex. 2. The log. cos. of $163^\circ 49'$ is the log. cos. of $16^\circ 11'$, or the log. sine of $73^\circ 49'$, which is 9.982441.

Ex. 3. The log. cosec. of $97^\circ 4'$ is the log. cosec. of $82^\circ 56'$, or the log. sec. of $7^\circ 4'$, which is 0.003312.

In like manner to find the log. co-sine, co-tangent, or co-secant, of an arc above 90° , take out the log. sine, tangent, or secant, of the excess above 90° .

To find the log. sine, &c. of an arc given to seconds. Find the log. sine (or cosine, &c.) for the next less minute or half-minute; take out the part for the seconds, or for the excess above $30''$.

For the sine, tangent, and secant, *add* the parts.

For the co-sine, co-tangent, and co-secant, *subtract* them.

Ex. 1. Find the log. sine of $53^\circ 25' 13''$.

$53^\circ 25' 0''$ sine	9.904711
13 parts	+ 20
LOG. SINE req.	9.904731

Ex. 2. Find the log. tan. of $11^\circ 19' 54''$.

$11^\circ 19' 30''$ tan.	9.301624
24 parts	+ 262
LOG. TAN. req.	9.301886

Ex. 3. Find the log. sec. of $38^\circ 42' 46''$.

$38^\circ 42' 30''$	0.107716
16 parts	+ 27
LOG. SEC. req.	0.107743

Ex. 4. Find the log. cosine of $72^\circ 10' 45''$.

$72^\circ 10' 30''$	9.485379
15 parts	- 98
LOG. COS. req.	9.485281

Ex. 5. Find the log. cotang. of $84^\circ 3' 22''$.

$84^\circ 3' 0''$ cot.	9.017959
20 parts 408	- 449
2 41	
LOG. COTANG. req.	9.017510

Ex. 6. Find the log. cosec. of $68^\circ 14' 11''$.

$68^\circ 14' 0''$ cosec.	0.032124
11 parts	- 9
LOG. COSEC. req.	0.032115

In working to five places, the last figure of the parts must be dropped, the remainder being increased by 1 when the figure dropped exceeds 5.

In working to 1st of time, the parts for $15''$ are to be employed. In the earlier part of the Table, *half* the D. for $30''$ may be conveniently employed.

It is convenient in dealing with parts of contrary application, to mark those *additive* with +, and *subtractive* with -; to sum each kind separately; and to take the diff. of the two sums, marking it with the sign of the greater. An example will be found, p. 264, top, the parts are, + 18, + 5, - 97, and + 35; the sum of the + ones is + 58, then the difference between 58 and 97 is 39, to be marked - 39, or subtractive.

Inverse Process. To find the Arc, to seconds, corresponding to a given log. sine &c.:

For the sine, tangent, or secant, take out the next *less*; for the co-sine, co-tangent, or co-secant, take out the next *greater*; and note the degree and minute, or half-minute, of the quantity thus taken out.

Take the diff. between this quantity and the given one; find the remainder in the column of Parts; take out the seconds corresponding and add them to the arc noted.

Ex. 1. Find the arc to the log. sine
9.24470.

	Given	9.202470
9° 10' 0"	Next less	202234
		18
	Rem.	236
Arc req.	9 10 18	

Ex. 2. Find the arc to the log. cosine
9.897796.

	Given	9.897796
17° 47' 0"	Next gr.	897810
		8
	Rem.	14
Arc req.	37 47 8	

When the parts are not given for seconds beyond 10 (as for the log. sine and tang. from 4° to 8°), if the remainder exceeds the parts given, take away the parts for 10" or 20" accordingly, and also the seconds corresponding to this last remainder.

Ex. 1. Find the arc to the log. tangent
9.127945.

	Given	9.127945
7° 38' 30"	Next less	127651
		294
10	Parts	160
8	Rem.	134
Arc req.	7 38 48	

Ex. 2. Find the arc to the log. cosec.
10.881005.

	Given	10.881005
7° 33' 0"	Next gr.	881433
		428
20	Parts	318
7	Rem.	110
Arc req.	7 33 27	

When greater precision than that afforded by the parts is required, the log. sine, &c., or the arc, may be found by means of the proportional part of the diff. between two terms, or for 30".

The log. cosec. is the arith. compl. of the log. sine.

The log. cotan. is the ar. co. of the log. tan.

The log. sec. is the ar. co. of the log. cosine.

The log. tan. is the sum of the log. sine and log. secant; thus all may be obtained from the log. sine.

TABLE 69. LOG. SINE SQUARE.*

The title is an abbreviation of *the logarithm of the square of the sine of half the arc*. The log. sine square is given to each 15" of arc or 1^m of time. In order to lessen the bulk of the table, the index, and one or two figures, are taken up at the head of the column, unless these figures change, when the whole is given in full. Five places only are inserted as far as 0^h 44^m, and six afterwards.

Each column contains 15', or 1^m; the minutes and quarters (of arc), above the next less 15', are given on the left-hand side, and the seconds of time on the right. Thus the log. sine square of 143° 37' 15", or 9.955473, is found under 143° 30' and against 7' 15", and corresponds to 9^h 34^m 29^s.

The parts for seconds, when not the same for the whole page, are given for the first and last columns; parts for intermediate columns are therefore between the given parts.

1. *Direct Process.* To find the log. sine square of an arc to the *nearest second*. Take the log. sin. sq. for the next less 15', and add the parts for the seconds.

To find the log. sine square for the *tenth of a second of time*. Consider

* This table is identical with the Log. Haversines of Inman's Tables.

the tenths as seconds of arc, take out the parts, increase them by half, and add the sum to the log. sine square of the whole second.

Ex. 1. Find the log. sine square of $38^{\circ} 11' 22''$ $38^{\circ} 11' 15''$ 7 parts Log. sin. sq. req.	$9^{\circ} 029400$ $\underline{43}$ $9^{\circ} 029443$	Ex. 2. Find the log. sine square of $3^h 42^m 57^s.3$ $3^h 42^m 57^s$ parts to $3''$, 12, 12 + 6 = Log. sin. sq. req.	$9^{\circ} 339466$ $\underline{18}$ $9^{\circ} 339484$
--	--	--	--

The log. sine square to seconds in the early part of the Table, where, on account of the great and irregular variation, no parts are given, is found by proportion.

Ex. Find the log. sine square of $1^{\circ} 36' 4''$. $1^{\circ} 36' 0''$ $1^{\circ} 36' 15''$ diff.	$6^{\circ} 28991$ $\underline{29217}$ 226	Then $15 : 226 :: 4 : 60$, the parts, and the LOG. SINE SQUARE required is $6^{\circ} 29051$.
--	---	--

2. *Inverse Process.* To find the arc, to $1'$, corresponding to a given log. sine square. From the given log. sine square subtract the next less in the Table, to which take out the arc, noting it down.

Find the seconds at the bottom corresponding to the difference, and add them to the arc.

Ex. Find the arc, to $1''$, corresponding to $9^{\circ} 029443$. Next less $9^{\circ} 029400$, arc $38^{\circ} 11' 15''$ given $9^{\circ} 029443$ diff. $\underline{43}$	43 at D. 90 gives $7''$, which added to $38^{\circ} 11' 15''$ give the arc required, $38^{\circ} 11' 22''$.
--	--

To find the time, to the tenth of a second, corresponding to a given log. sine square.

Find the time corresponding to the next less log. sine square in the table. Take the diff. between the given and the next less logs. Find this diff. among the parts; take out the seconds of arc corresponding, and subtract from it 1-3d of itself. The rem. is the number of tenths, to be added to the time of the next less.

The above is correct enough for common practice, but for greater precision the difference between two terms must be employed, and the result deduced by proportion.

To compute a Term. Take the log. sine of half the arc and double it.

TABLE 70. LOGARITHMS FOR COMPUTING THE REDUCTION TO THE MERIDIAN AT SEA.

The Table is entered with the Declination at the top and the Latitude at the side. The cases omitted are not eligible. See No. 700.

The cases which appear above the vacant spaces in Part I. are those in which the body passes the meridian between the pole and the zenith; those below the spaces are the more common cases, or those which occur between the tropics and the arctic circles.

To compute a Term. Add together 0.30103, the log. cosines of the lat. and decl., and the log. sec. of the meridian altitude.

The process of computing the meridian alt. may be avoided thus: when the lat. and decl. are of the same name, employ the log. cosec. of their difference (unless the body is below the pole, when employ the cosec. of their sum), when of contrary names, the cosec. of their sum.

Ex. 1. (<i>Same names.</i>) Lat. 9° N.,				Ex. 2. (<i>Contrary names.</i>) Lat. 9° N.,			
Decl. 17° N.				Decl. 17° S.			
Lat.	9°	cos.	0°3010	Lat.	9°	cos.	0°3010
Decl.	17	cos.	9°9946	Decl.	17	cos.	9°9946
Diff.	8	cosec.	0°8564	Sum	26	cosec.	0°3582
Log. required			1°1326	Log. required			0°6344

When the lat. exceeds 62° or the decl. exceeds 23°, the logarithm must be computed.

TABLE 71. LOGARITHMS FOR COMPUTING THE CORRECTION OF THE LATITUDE BY ACCOUNT.

The Table is entered with the two Azimuths, either of the same body at different times, or of two different bodies. See No. 752 (7).

The cases omitted are not eligible.

Part I. is used when both altitudes are taken on the *same* side both of the meridian and prime vertical, and Part II. when on *different* sides of either of these circles.

To compute the Log. for Part I. To 8·8239 add the log. cosecants of the azimuths, and the log. sine of their *difference*.

For Part II. To 8·8239 add the log. cosecants of the azimuths, and the log. sine of their *sum*.

Ex. 1. Azimuths S. 70° W. and S. 11° W. (<i>or same side</i>).				Ex. 2. Azimuths S. 70° W. and S. 11° W. (<i>or different sides</i>).			
Az.	70°	cosec.	8·8239	Az.	70°	cosec.	8·8239
Az.	11	cosec.	0°0270	Az.	11	cosec.	0°0270
Diff.	59	sin.	0°7194	Sum	81	sin.	0°7194
Log. required			9°9331	Log. required			9°9946

TABLE 72. LOGARITHMS FOR COMPUTING THE EQUATION OF EQUAL ALTITUDES.

These are given to each 10^m. See No. 806 (4).

To compute Log. A To 3·28534 add the log. of the interval (in seconds of time), and the log. cosec. of half the interval; take the arith. compl. of the sum.

To compute Log. B. To 3·28534 add the log. of the interval (in seconds), and the log. cot. of half the interval; take the arith. compl. of the sum.

Ex. Interval 4^h 30^m. Compute the logs. A. and B.

4 ^h 30 ^m = 16200 ^s log.				3°28534			
2 15 cosec.				4°20951			
				0°17511			
				7°66996			
Log. A.			2°24990	Log. B.			2°3300

TABLE 73. THE LOGARITHMIC DIFFERENCE.

This quantity is given for Fahrenheit's thermometer at 50°, and the Barometer at 30 inches.

The Table is entered like Table 39. The parts for " of parallax and " of alt. are applied as directed in the Table.

The parts for the sun's or star's alt. are given at the bottom.

To correct the log. diff. for any other height of the thermometer and barometer than those given in the Table. Find the correction of the mean refraction for each body by Tables 32 and 33.

With the moon's alt. and her atmospherical correction, thus found, as seconds of parallax, take out the parts.

With the sun's (or star's) alt. as the moon's alt., and his atmospher. corr. as seconds of parallax, take out the parts.

When the atmospherical correction is +, *add* the parts to the mean or ordinary log. diff.; when —, *subtract* them.

Ex. (Mean state.)		☉'s app. alt. $27^{\circ} 18'$;
Cor. par. $60' 42''$;		☉'s alt. $10^{\circ} 20'$.
$27^{\circ} 10'$ and $60'$		9.996721
8' parts —17		
42" —42		
☉ 10° —8		
		<u>—67</u>
Required Log. Diff.		9.996654

Ex. The same corrected for bar. $29\frac{1}{2}$, and therm. 84° .		
Mean log. diff.		9.996721
☉ Th. 84°	—8	pts. —67
Bar. $29\frac{1}{2}$	—3	
☉ Atmos. corr.	—11	—11
☉ Th. 84°	—20	
Bar. $29\frac{1}{2}$	—9	
☉ Atmos. corr.	—29	—11
		<u>—89</u>
		Log. Diff. 9.996632

When a planet is employed, consider it as a star, and its horizontal parallax as seconds of moon's parallax. With its alt. take out the parts and *subtract* them.

To compute the Log. Diff. Add together the log. secants of the app. alts., and the log. cosines of the true alts.; the sum is the log. diff.

Ex. ☉ A. Alt. $27^{\circ} 18'$, Hor. Par. $60' 42''$. ☉ A. Alt. $10^{\circ} 20'$: required the Log. Diff. for the mean state of the atmosphere, as also for the therm. 84° , and barom. $29\frac{1}{2}$ in.

Mean State.			
☉ $27^{\circ} 18'$	0"	sec.	0.051285
+ 52	5		
28 10	5	cos.	9.945255
☉ 10 20	0	sec.	0.007102
—5	2		
10 14	58	cos.	<u>9.993014</u>
		Log. Diff.	9.996656

Corrected for Therm. and Barom.			
☉ $27^{\circ} 18'$	0"	sec.	0.051285
+ 52	16		
28 10	16	cos.	9.945243
☉ 10 20	0	sec.	0.007102
—4	33		
10 15	27	cos.	<u>9.993003</u>
		Log. Diff.	9.996633

The results by the two methods agree as nearly as can be expected from processes in which each of the several parts employed has its own particular inaccuracy.

TABLE 74. PROPORTIONAL LOGARITHMS.

These logarithms are given to every second of time, or arc, for 3^h or 3° . The Table is entered with the hour or degree and the minute at the top, and the second at the side; thus the prop. log. of $1^{\circ} 2' 27''$ or of $1^h 2^m 27^s$ is 4597, that of $1^m 2^s$ is 2.2410. The index 0 proper to quantities above 19^m (or $19'$) is suppressed for convenience.

To find the prop. log. of an arc under $18'$, to the tenth of a second. Put the proper index, and find the decimal part due to ten times the arc.

Ex. Find the prop. log. of $7' 13''.7$; the index of $7' 13''$ is 1; the dec. part of the log. due to $70' 137''$, or $72' 17''$, is 3962, the prop. log. required is 1.3962 .

So the prop. log. of an arc, under $1' 48''$ may be found to the hundredth of a second by multiplying by 100.

To find the arc or time to the *tenth* of a second to a given prop. log. exceeding 1.0000. Look in the Table till the decimal part again occurs, and divide the arc by 10.

Ex. Find the time to the prop. log. 2.5106. Look for 1.5106; the nearest found is 1.5110, against 5^m 33^s, or 333^s; hence the time required is 33^s.3.

Four places are enough for common purposes; but since the fourth place ceases to change by 1 after 1^h 13^m, a greater time than this cannot be found truly to 1^a. So also, a time exceeding 2^h 25^m cannot be found truly to 2^a. This defect may be avoided in some cases by employing the complement of the interval to 3^h.

To convert a given log. sine of an arc less than 1° 30' into a prop. log. add 8.7190 to its arithmetical complement. To convert a prop. log. of an arc into a log. sine, less than 1^h, add 8.7190 to its arith. compl.

Ex. 1. Convert the log. sine 8.3507 into a prop. log.

log. sine	8.3507
ar. co.	1.6493
const.	8.7190
PROP. LOG.	0.3683

Arc 1° 17' 5"

Ex. 2. Convert the prop. log. of 0° 25' 0", or 8573, into a log. sine.

pr. log.	0.8573
ar. co.	9.1427
	8.7190
LOG. SINE	7.8617

When the terms of an analogy are all sexigesimals, the rules given in p. 20, Nos. 64, &c., apply to the proportional logarithms; but if two of the terms are not sexigesimals, the arith. complements of the logs. of these last must be used.*

To compute a Prop. Log. From 4.03342 (the log. of 10800, the number of seconds in 3^h or 3°) subtract the log. of the given time or arc in seconds; the result is the prop. log. required.

Ex. Find the prop. log. of 2^h 11^m 28^s.

	const.	4.03342
2 ^h 11 ^m 28 ^s = 7888 ^s ,	log.	3.89697
	PROP. LOG.	0.13645

The Tables close with the Abbreviations adopted in the Admiralty Charts, with explanatory notes. These should be committed to memory by sailors.

* The proportional logarithms are often convenient, but they might be replaced with advantage by common logarithms. The prop. logs., unlike the common logarithms, continually *decrease* instead of *increasing* with the argument. This progression is always repugnant to the mind, and should be avoided when the change involves no sacrifice. Again, these logarithms require every factor with which they are combined to be inverted, that is, for ex., instead of multiplying by 2, they oblige us to divide by 2. This, even to an expert computer, is the cause of perpetual mistakes in the changing of constants; but to a beginner it has the mischievous effect of entirely destroying, in processes which may nevertheless be identical, every vestige of analogy.

If common logarithms, with the same scale and the index prefixed, were employed, the logarithm attached, in the Nautical Almanac, to the lunar distance, would involve the constant for 3^h. Such logarithms would answer all the present purposes without being open to any of the above objections; the log. in the Nautical Almanac would then be additive instead of subtractive. The proportional logarithms, originally computed for the purpose of simplifying a single step in a single computation, are an example of the ill effects of sacrificing general utility to a partial end; and the substitution of others, at a favourable opportunity, is recommended as a reform deserving attention.

TABLES.

TRAVERSE TABLE TO DEGREES														
1°									0° 4"					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	1°0'	0°0'	61	61°0'	1°1'	121	121°0'	2°1'	181	181°0'	3°2'	241	241°0'	4°2'
2	2°0'	0°0'	62	62°0'	1°1'	122	122°0'	2°1'	182	182°0'	3°2'	242	242°0'	4°2'
3	3°0'	0°1'	63	63°0'	1°1'	123	123°0'	2°1'	183	183°0'	3°2'	243	243°0'	4°2'
4	4°0'	0°1'	64	64°0'	1°1'	124	124°0'	2°2'	184	184°0'	3°2'	244	244°0'	4°3'
5	5°0'	0°1'	65	65°0'	1°1'	125	125°0'	2°2'	185	185°0'	3°2'	245	245°0'	4°3'
6	6°0'	0°1'	66	66°0'	1°2'	126	126°0'	2°2'	186	186°0'	3°2'	246	246°0'	4°3'
7	7°0'	0°1'	67	67°0'	1°2'	127	127°0'	2°2'	187	187°0'	3°3'	247	247°0'	4°3'
8	8°0'	0°1'	68	68°0'	1°2'	128	128°0'	2°2'	188	188°0'	3°3'	248	248°0'	4°3'
9	9°0'	0°2'	69	69°0'	1°2'	129	129°0'	2°3'	189	189°0'	3°3'	249	249°0'	4°3'
10	10°0'	0°2'	70	70°0'	1°2'	130	130°0'	2°3'	190	190°0'	3°3'	250	250°0'	4°4'
11	11°0'	0°2'	71	71°0'	1°2'	131	131°0'	2°3'	191	191°0'	3°3'	251	251°0'	4°4'
12	12°0'	0°2'	72	72°0'	1°3'	132	132°0'	2°3'	192	192°0'	3°4'	252	252°0'	4°4'
13	13°0'	0°2'	73	73°0'	1°3'	133	133°0'	2°3'	193	193°0'	3°4'	253	253°0'	4°4'
14	14°0'	0°2'	74	74°0'	1°3'	134	134°0'	2°3'	194	194°0'	3°4'	254	254°0'	4°4'
15	15°0'	0°3'	75	75°0'	1°3'	135	135°0'	2°4'	195	195°0'	3°4'	255	255°0'	4°5'
16	16°0'	0°3'	76	76°0'	1°3'	136	136°0'	2°4'	196	196°0'	3°4'	256	256°0'	4°5'
17	17°0'	0°3'	77	77°0'	1°3'	137	137°0'	2°4'	197	197°0'	3°4'	257	257°0'	4°5'
18	18°0'	0°3'	78	78°0'	1°4'	138	138°0'	2°4'	198	198°0'	3°5'	258	258°0'	4°5'
19	19°0'	0°3'	79	79°0'	1°4'	139	139°0'	2°4'	199	199°0'	3°5'	259	259°0'	4°5'
20	20°0'	0°3'	80	80°0'	1°4'	140	140°0'	2°4'	200	200°0'	3°5'	260	260°0'	4°5'
21	21°0'	0°4'	81	81°0'	1°4'	141	141°0'	2°5'	201	201°0'	3°5'	261	261°0'	4°6'
22	22°0'	0°4'	82	82°0'	1°4'	142	142°0'	2°5'	202	202°0'	3°5'	262	262°0'	4°6'
23	23°0'	0°4'	83	83°0'	1°4'	143	143°0'	2°5'	203	203°0'	3°5'	263	263°0'	4°6'
24	24°0'	0°4'	84	84°0'	1°5'	144	144°0'	2°5'	204	204°0'	3°6'	264	264°0'	4°6'
25	25°0'	0°4'	85	85°0'	1°5'	145	145°0'	2°5'	205	205°0'	3°6'	265	265°0'	4°6'
26	26°0'	0°5'	86	86°0'	1°5'	146	146°0'	2°5'	206	206°0'	3°6'	266	266°0'	4°6'
27	27°0'	0°5'	87	87°0'	1°5'	147	147°0'	2°6'	207	207°0'	3°6'	267	267°0'	4°7'
28	28°0'	0°5'	88	88°0'	1°5'	148	148°0'	2°6'	208	208°0'	3°6'	268	268°0'	4°7'
29	29°0'	0°5'	89	89°0'	1°6'	149	149°0'	2°6'	209	209°0'	3°6'	269	269°0'	4°7'
30	30°0'	0°5'	90	90°0'	1°6'	150	150°0'	2°6'	210	210°0'	3°7'	270	270°0'	4°7'
31	31°0'	0°5'	91	91°0'	1°6'	151	151°0'	2°6'	211	211°0'	3°7'	271	271°0'	4°7'
32	32°0'	0°6'	92	92°0'	1°6'	152	152°0'	2°7'	212	212°0'	3°7'	272	272°0'	4°7'
33	33°0'	0°6'	93	93°0'	1°6'	153	153°0'	2°7'	213	213°0'	3°7'	273	273°0'	4°8'
34	34°0'	0°6'	94	94°0'	1°6'	154	154°0'	2°7'	214	214°0'	3°7'	274	274°0'	4°8'
35	35°0'	0°6'	95	95°0'	1°7'	155	155°0'	2°7'	215	215°0'	3°8'	275	275°0'	4°8'
36	36°0'	0°6'	96	96°0'	1°7'	156	156°0'	2°7'	216	216°0'	3°8'	276	276°0'	4°8'
37	37°0'	0°6'	97	97°0'	1°7'	157	157°0'	2°7'	217	217°0'	3°8'	277	277°0'	4°8'
38	38°0'	0°7'	98	98°0'	1°7'	158	158°0'	2°8'	218	218°0'	3°8'	278	278°0'	4°9'
39	39°0'	0°7'	99	99°0'	1°7'	159	159°0'	2°8'	219	219°0'	3°8'	279	279°0'	4°9'
40	40°0'	0°7'	100	100°0'	1°7'	160	160°0'	2°8'	220	220°0'	3°8'	280	280°0'	4°9'
41	41°0'	0°7'	101	101°0'	1°8'	161	161°0'	2°8'	221	221°0'	3°9'	281	281°0'	4°9'
42	42°0'	0°7'	102	102°0'	1°8'	162	162°0'	2°8'	222	222°0'	3°9'	282	282°0'	4°9'
43	43°0'	0°8'	103	103°0'	1°8'	163	163°0'	2°8'	223	223°0'	3°9'	283	283°0'	4°9'
44	44°0'	0°8'	104	104°0'	1°8'	164	164°0'	2°9'	224	224°0'	3°9'	284	284°0'	5°0'
45	45°0'	0°8'	105	105°0'	1°8'	165	165°0'	2°9'	225	225°0'	3°9'	285	285°0'	5°0'
46	46°0'	0°8'	106	106°0'	1°8'	166	166°0'	2°9'	226	226°0'	3°9'	286	286°0'	5°0'
47	47°0'	0°8'	107	107°0'	1°9'	167	167°0'	2°9'	227	227°0'	4°0'	287	287°0'	5°0'
48	48°0'	0°8'	108	108°0'	1°9'	168	168°0'	2°9'	228	228°0'	4°0'	288	288°0'	5°0'
49	49°0'	0°9'	109	109°0'	1°9'	169	169°0'	2°9'	229	229°0'	4°0'	289	289°0'	5°0'
50	50°0'	0°9'	110	110°0'	1°9'	170	170°0'	3°0'	230	230°0'	4°0'	290	290°0'	5°1'
51	51°0'	0°9'	111	111°0'	1°9'	171	171°0'	3°0'	231	231°0'	4°0'	291	291°0'	5°1'
52	52°0'	0°9'	112	112°0'	2°0'	172	172°0'	3°0'	232	232°0'	4°0'	292	292°0'	5°1'
53	53°0'	0°9'	113	113°0'	2°0'	173	173°0'	3°0'	233	233°0'	4°1'	293	293°0'	5°1'
54	54°0'	0°9'	114	114°0'	2°0'	174	174°0'	3°0'	234	234°0'	4°1'	294	294°0'	5°1'
55	55°0'	1°0'	115	115°0'	2°0'	175	175°0'	3°1'	235	235°0'	4°1'	295	295°0'	5°1'
56	56°0'	1°0'	116	116°0'	2°0'	176	176°0'	3°1'	236	236°0'	4°1'	296	296°0'	5°2'
57	57°0'	1°0'	117	117°0'	2°0'	177	177°0'	3°1'	237	237°0'	4°1'	297	297°0'	5°2'
58	58°0'	1°0'	118	118°0'	2°1'	178	178°0'	3°1'	238	238°0'	4°2'	298	298°0'	5°2'
59	59°0'	1°0'	119	119°0'	2°1'	179	179°0'	3°1'	239	239°0'	4°2'	299	299°0'	5°2'
60	60°0'	1°0'	120	120°0'	2°1'	180	180°0'	3°1'	240	240°0'	4°2'	300	300°0'	5°2'
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
89°									5° 56"					

TABLE 1

453

TRAVERSE TABLE TO DEGREES

1°									0 ^h 4 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	301°0	5'3	361	360°9	6'3	421	420°9	7'3	481	480°9	8'4	541	540°9	9'5
302	302°0	5'3	362	361°9	6'3	422	421°9	7'4	482	481°9	8'4	542	541°9	9'5
303	303°0	5'3	363	362°9	6'3	423	422°9	7'4	483	482°9	8'5	543	542°9	9'5
304	304°0	5'3	364	363°9	6'4	424	423°9	7'4	484	483°9	8'5	544	543°9	9'5
305	305°0	5'3	365	364°9	6'4	425	424°9	7'4	485	484°9	8'5	545	544°9	9'5
306	306°0	5'3	366	365°9	6'4	426	425°9	7'4	486	485°9	8'5	546	545°9	9'5
307	307°0	5'4	367	366°9	6'4	427	426°9	7'4	487	486°9	8'5	547	546°9	9'6
308	308°0	5'4	368	367°9	6'4	428	427°9	7'5	488	487°9	8'6	548	547°9	9'6
309	309°0	5'4	369	368°9	6'4	429	428°9	7'5	489	488°9	8'6	549	548°9	9'6
310	310°0	5'4	370	369°9	6'5	430	429°9	7'5	490	489°9	8'6	550	549°9	9'6
311	311°0	5'4	371	370°9	6'5	431	430°9	7'5	491	490°9	8'6	551	550°9	9'6
312	312°0	5'4	372	371°9	6'5	432	431°9	7'5	492	491°9	8'6	552	551°9	9'6
313	313°0	5'5	373	372°9	6'5	433	432°9	7'5	493	492°9	8'7	553	552°9	9'7
314	314°0	5'5	374	373°9	6'5	434	433°9	7'6	494	493°9	8'7	554	553°9	9'7
315	315°0	5'5	375	374°9	6'5	435	434°9	7'6	495	494°9	8'7	555	554°9	9'7
316	316°0	5'5	376	375°9	6'6	436	435°9	7'6	496	495°9	8'7	556	555°9	9'7
317	317°0	5'5	377	376°9	6'6	437	436°9	7'6	497	496°9	8'7	557	556°9	9'7
318	318°0	5'5	378	377°9	6'6	438	437°9	7'6	498	497°9	8'7	558	557°9	9'7
319	319°0	5'6	379	378°9	6'6	439	438°9	7'7	499	498°9	8'8	559	558°9	9'8
320	320°0	5'6	380	379°9	6'6	440	439°9	7'7	500	499°9	8'8	560	559°9	9'8
321	321°0	5'6	381	380°9	6'7	441	440°9	7'7	501	500°9	8'8	561	560°9	9'8
322	322°0	5'6	382	381°9	6'7	442	441°9	7'7	502	501°9	8'8	562	561°9	9'8
323	323°0	5'6	383	382°9	6'7	443	442°9	7'7	503	502°9	8'8	563	562°9	9'8
324	324°0	5'6	384	383°9	6'7	444	443°9	7'7	504	503°9	8'8	564	563°9	9'8
325	325°0	5'7	385	384°9	6'7	445	444°9	7'8	505	504°9	8'8	565	564°9	9'9
326	326°0	5'7	386	385°9	6'7	446	445°9	7'8	506	505°9	8'9	566	565°9	9'9
327	327°0	5'7	387	386°9	6'8	447	446°9	7'8	507	506°9	8'9	567	566°9	9'9
328	328°0	5'7	388	387°9	6'8	448	447°9	7'8	508	507°9	8'9	568	567°9	9'9
329	329°0	5'7	389	388°9	6'8	449	448°9	7'8	509	508°9	8'9	569	568°9	9'9
330	330°0	5'8	390	389°9	6'8	450	449°9	7'8	510	509°9	8'9	570	569°9	9'9
331	331°0	5'8	391	390°9	6'8	451	450°9	7'9	511	510°9	9'0	571	570°9	10°0
332	332°0	5'8	392	391°9	6'8	452	451°9	7'9	512	511°9	9'0	572	571°9	10°0
333	333°0	5'8	393	392°9	6'9	453	452°9	7'9	513	512°9	9'0	573	572°9	10°0
334	333°9	5'8	394	393°9	6'9	454	453°9	7'9	514	513°9	9'0	574	573°9	10°0
335	334°9	5'8	395	394°9	6'9	455	454°9	7'9	515	514°9	9'0	575	574°9	10°0
336	335°9	5'9	396	395°9	6'9	456	455°9	8°0	516	515°9	9'0	576	575°9	10°0
337	336°9	5'9	397	396°9	6'9	457	456°9	8°0	517	516°9	9'1	577	576°9	10°1
338	337°9	5'9	398	397°9	6'9	458	457°9	8°0	518	517°9	9'1	578	577°9	10°1
339	338°9	5'9	399	398°9	7°0	459	458°9	8°0	519	518°9	9'1	579	578°9	10°1
340	339°9	5'9	400	399°9	7°0	460	459°9	8°0	520	519°9	9'1	580	579°9	10°1
341	340°9	6°0	401	400°9	7°0	461	460°9	8°0	521	520°9	9'1	581	580°9	10°1
342	341°9	6°0	402	401°9	7°0	462	461°9	8°1	522	521°9	9'1	582	581°9	10°1
343	342°9	6°0	403	402°9	7°0	463	462°9	8°1	523	522°9	9'2	583	582°9	10°2
344	343°9	6°0	404	403°9	7°1	464	463°9	8°1	524	523°9	9'2	584	583°9	10°2
345	344°9	6°0	405	404°9	7°1	465	464°9	8°1	525	524°9	9'2	585	584°9	10°2
346	345°9	6°0	406	405°9	7°1	466	465°9	8°1	526	525°9	9'2	586	585°9	10°2
347	346°9	6°1	407	406°9	7°1	467	466°9	8°1	527	526°9	9'2	587	586°9	10°2
348	347°9	6°1	408	407°9	7°1	468	467°9	8°2	528	527°9	9'2	588	587°9	10°2
349	348°9	6°1	409	408°9	7°1	469	468°9	8°2	529	528°9	9'3	589	588°9	10°3
350	349°9	6°1	410	409°9	7°2	470	469°9	8°2	530	529°9	9'3	590	589°9	10°3
351	350°9	6°1	411	410°9	7°2	471	470°9	8°2	531	530°9	9'3	591	590°9	10°3
352	351°9	6°1	412	411°9	7°2	472	471°9	8°2	532	531°9	9'3	592	591°9	10°3
353	352°9	6°2	413	412°9	7°2	473	472°9	8°2	533	532°9	9'3	593	592°9	10°3
354	353°9	6°2	414	413°9	7°2	474	473°9	8°3	534	533°9	9'3	594	593°9	10°3
355	354°9	6°2	415	414°9	7°2	475	474°9	8°3	535	534°9	9'4	595	594°9	10°4
356	355°9	6°2	416	415°9	7°3	476	475°9	8°3	536	535°9	9'4	596	595°9	10°4
357	356°9	6°2	417	416°9	7°3	477	476°9	8°3	537	536°9	9'4	597	596°9	10°4
358	357°9	6°2	418	417°9	7°3	478	477°9	8°3	538	537°9	9'4	598	597°9	10°4
359	358°9	6°3	419	418°9	7°3	479	478°9	8°4	539	538°9	9'4	599	598°9	10°4
360	359°9	6°3	420	419°9	7°3	480	479°9	8°4	540	539°9	9'4	600	599°9	10°5
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

89°

5^h 56^m

TRAVERSE TABLE TO DEGREES														
2°									0 ^b 8 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	1°0'	0°0'	61	61°0'	2°1'	121	120°9'	4°2'	181	180°9'	6°3'	241	240°9'	8°4'
2	2°0'	0°1'	62	62°0'	2°2'	122	121°9'	4°3'	182	181°9'	6°4'	242	241°9'	8°4'
3	3°0'	0°1'	63	63°0'	2°2'	123	122°9'	4°3'	183	182°9'	6°4'	243	242°9'	8°5'
4	4°0'	0°1'	64	64°0'	2°2'	124	123°9'	4°3'	184	183°9'	6°4'	244	243°9'	8°5'
5	5°0'	0°2'	65	65°0'	2°3'	125	124°9'	4°4'	185	184°9'	6°5'	245	244°9'	8°6'
6	6°0'	0°2'	66	66°0'	2°3'	126	125°9'	4°4'	186	185°9'	6°5'	246	245°9'	8°6'
7	7°0'	0°2'	67	67°0'	2°3'	127	126°9'	4°4'	187	186°9'	6°5'	247	246°8'	8°6'
8	8°0'	0°3'	68	68°0'	2°4'	128	127°9'	4°5'	188	187°9'	6°6'	248	247°8'	8°7'
9	9°0'	0°3'	69	69°0'	2°4'	129	128°9'	4°5'	189	188°9'	6°6'	249	248°8'	8°7'
10	10°0'	0°3'	70	70°0'	2°4'	130	129°9'	4°5'	190	189°9'	6°6'	250	249°8'	8°7'
11	11°0'	0°4'	71	71°0'	2°5'	131	130°9'	4°6'	191	190°9'	6°7'	251	250°8'	8°8'
12	12°0'	0°4'	72	72°0'	2°5'	132	131°9'	4°6'	192	191°9'	6°7'	252	251°8'	8°8'
13	13°0'	0°5'	73	73°0'	2°5'	133	132°9'	4°6'	193	192°9'	6°7'	253	252°8'	8°8'
14	14°0'	0°5'	74	74°0'	2°6'	134	133°9'	4°7'	194	193°9'	6°8'	254	253°8'	8°9'
15	15°0'	0°5'	75	75°0'	2°6'	135	134°9'	4°7'	195	194°9'	6°8'	255	254°8'	8°9'
16	16°0'	0°6'	76	76°0'	2°7'	136	135°9'	4°7'	196	195°9'	6°8'	256	255°8'	8°9'
17	17°0'	0°6'	77	77°0'	2°7'	137	136°9'	4°8'	197	196°9'	6°9'	257	256°8'	9°0'
18	18°0'	0°6'	78	78°0'	2°7'	138	137°9'	4°8'	198	197°9'	6°9'	258	257°8'	9°0'
19	19°0'	0°7'	79	79°0'	2°8'	139	138°9'	4°9'	199	198°9'	6°9'	259	258°8'	9°0'
20	20°0'	0°7'	80	80°0'	2°8'	140	139°9'	4°9'	200	199°9'	7°0'	260	259°8'	9°1'
21	21°0'	0°8'	81	81°0'	2°8'	141	140°9'	4°9'	201	200°9'	7°0'	261	260°8'	9°1'
22	22°0'	0°8'	82	82°0'	2°9'	142	141°9'	5°0'	202	201°9'	7°0'	262	261°8'	9°1'
23	23°0'	0°8'	83	82°9'	2°9'	143	142°0'	5°0'	203	202°9'	7°1'	263	262°8'	9°2'
24	24°0'	0°8'	84	83°9'	2°9'	144	143°9'	5°0'	204	203°9'	7°1'	264	263°8'	9°2'
25	25°0'	0°9'	85	84°9'	3°0'	145	144°9'	5°1'	205	204°9'	7°2'	265	264°8'	9°2'
26	26°0'	0°9'	86	85°9'	3°0'	146	145°9'	5°1'	206	205°9'	7°2'	266	265°8'	9°3'
27	27°0'	0°9'	87	86°9'	3°0'	147	146°9'	5°1'	207	206°9'	7°2'	267	266°8'	9°3'
28	28°0'	1°0'	88	87°9'	3°1'	148	147°9'	5°2'	208	207°9'	7°3'	268	267°8'	9°4'
29	29°0'	1°0'	89	88°9'	3°1'	149	148°9'	5°2'	209	208°9'	7°3'	269	268°8'	9°4'
30	30°0'	1°0'	90	89°9'	3°1'	150	149°9'	5°2'	210	209°9'	7°3'	270	269°8'	9°4'
31	31°0'	1°1'	91	90°9'	3°2'	151	150°9'	5°3'	211	210°9'	7°4'	271	270°8'	9°5'
32	32°0'	1°1'	92	91°9'	3°2'	152	151°9'	5°3'	212	211°9'	7°4'	272	271°8'	9°5'
33	33°0'	1°2'	93	92°9'	3°2'	153	152°9'	5°3'	213	212°9'	7°4'	273	272°8'	9°5'
34	34°0'	1°2'	94	93°9'	3°3'	154	153°9'	5°4'	214	213°9'	7°5'	274	273°8'	9°6'
35	35°0'	1°2'	95	94°9'	3°3'	155	154°9'	5°4'	215	214°9'	7°5'	275	274°8'	9°6'
36	36°0'	1°3'	96	95°9'	3°4'	156	155°9'	5°4'	216	215°9'	7°5'	276	275°8'	9°6'
37	37°0'	1°3'	97	96°9'	3°4'	157	156°9'	5°5'	217	216°9'	7°6'	277	276°8'	9°7'
38	38°0'	1°3'	98	97°9'	3°4'	158	157°9'	5°5'	218	217°9'	7°6'	278	277°8'	9°7'
39	39°0'	1°4'	99	98°9'	3°5'	159	158°9'	5°5'	219	218°9'	7°6'	279	278°8'	9°7'
40	40°0'	1°4'	100	99°9'	3°5'	160	159°9'	5°6'	220	219°9'	7°7'	280	279°8'	9°8'
41	41°0'	1°4'	101	100°9'	3°5'	161	160°9'	5°6'	221	220°9'	7°7'	281	280°8'	9°8'
42	42°0'	1°5'	102	101°9'	3°6'	162	161°9'	5°7'	222	221°9'	7°7'	282	281°8'	9°8'
43	43°0'	1°5'	103	102°9'	3°6'	163	162°9'	5°7'	223	222°9'	7°8'	283	282°8'	9°9'
44	44°0'	1°5'	104	103°9'	3°6'	164	163°9'	5°7'	224	223°9'	7°8'	284	283°8'	9°9'
45	45°0'	1°6'	105	104°9'	3°7'	165	164°9'	5°8'	225	224°9'	7°9'	285	284°8'	9°9'
46	46°0'	1°6'	106	105°9'	3°7'	166	165°9'	5°8'	226	225°9'	7°9'	286	285°8'	10°0'
47	47°0'	1°6'	107	106°9'	3°7'	167	166°9'	5°8'	227	226°9'	7°9'	287	286°8'	10°0'
48	48°0'	1°7'	108	107°9'	3°8'	168	167°9'	5°9'	228	227°9'	8°0'	288	287°8'	10°1'
49	49°0'	1°7'	109	108°9'	3°8'	169	168°9'	5°9'	229	228°9'	8°0'	289	288°8'	10°1'
50	50°0'	1°7'	110	109°9'	3°8'	170	169°9'	5°9'	230	229°9'	8°0'	290	289°8'	10°1'
51	51°0'	1°8'	111	110°9'	3°9'	171	170°9'	6°0'	231	230°9'	8°1'	291	290°8'	10°2'
52	52°0'	1°8'	112	111°9'	3°9'	172	171°9'	6°0'	232	231°9'	8°1'	292	291°8'	10°2'
53	53°0'	1°8'	113	112°9'	3°9'	173	172°9'	6°0'	233	232°9'	8°1'	293	292°8'	10°2'
54	54°0'	1°9'	114	113°9'	4°0'	174	173°9'	6°1'	234	233°9'	8°2'	294	293°8'	10°3'
55	55°0'	1°9'	115	114°9'	4°0'	175	174°9'	6°1'	235	234°9'	8°2'	295	294°8'	10°3'
56	56°0'	2°0'	116	115°9'	4°0'	176	175°9'	6°1'	236	235°9'	8°2'	296	295°8'	10°3'
57	57°0'	2°0'	117	116°9'	4°1'	177	176°9'	6°2'	237	236°9'	8°3'	297	296°8'	10°4'
58	58°0'	2°0'	118	117°9'	4°1'	178	177°9'	6°2'	238	237°9'	8°3'	298	297°8'	10°4'
59	59°0'	2°1'	119	118°9'	4°2'	179	178°9'	6°2'	239	238°9'	8°3'	299	298°8'	10°4'
60	60°0'	2°1'	120	119°9'	4°2'	180	179°9'	6°3'	240	239°9'	8°4'	300	299°8'	10°5'
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
88°									5 ^b 52 ^m					

TABLE 1

TRAVERSE TABLE TO DEGREES														
2°												0h 5m		
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
801	300·8	10·5	361	360·8	12·6	421	420·8	14·7	481	480·7	16·8	541	540·7	18·9
802	301·8	10·5	362	361·8	12·6	422	421·8	14·7	482	481·7	16·8	542	541·7	18·9
803	302·8	10·6	363	362·8	12·7	423	422·8	14·7	483	482·7	16·8	543	542·7	18·9
804	303·8	10·6	364	363·8	12·7	424	423·8	14·8	484	483·7	16·9	544	543·7	19·0
805	304·8	10·6	365	364·8	12·7	425	424·8	14·8	485	484·7	16·9	545	544·7	19·0
806	305·8	10·7	366	365·8	12·8	426	425·7	14·9	486	485·7	16·9	546	545·7	19·0
807	306·8	10·7	367	366·8	12·8	427	426·7	14·9	487	486·7	17·0	547	546·7	19·1
808	307·8	10·7	368	367·8	12·8	428	427·7	14·9	488	487·7	17·0	548	547·7	19·1
809	308·8	10·8	369	368·8	12·9	429	428·7	15·0	489	488·7	17·0	549	548·7	19·1
810	309·8	10·8	370	369·8	12·9	430	429·7	15·0	490	489·7	17·1	550	549·7	19·2
811	310·8	10·8	371	370·8	12·9	431	430·7	15·0	491	490·7	17·1	551	550·7	19·2
812	311·8	10·9	372	371·8	13·0	432	431·7	15·1	492	491·7	17·1	552	551·7	19·2
813	312·8	10·9	373	372·8	13·0	433	432·7	15·1	493	492·7	17·2	553	552·7	19·3
814	313·8	10·9	374	373·8	13·0	434	433·7	15·1	494	493·7	17·2	554	553·7	19·3
815	314·8	11·0	375	374·8	13·1	435	434·7	15·2	495	494·7	17·2	555	554·7	19·3
816	315·8	11·0	376	375·8	13·1	436	435·7	15·2	496	495·7	17·3	556	555·7	19·4
817	316·8	11·0	377	376·8	13·1	437	436·7	15·2	497	496·7	17·3	557	556·7	19·4
818	317·8	11·1	378	377·8	13·2	438	437·7	15·3	498	497·7	17·3	558	557·7	19·4
819	318·8	11·1	379	378·8	13·2	439	438·7	15·3	499	498·7	17·4	559	558·7	19·5
820	319·8	11·2	380	379·8	13·2	440	439·7	15·3	500	499·7	17·4	560	559·7	19·5
821	320·8	11·2	381	380·8	13·3	441	440·7	15·4	501	500·7	17·5	561	560·7	19·5
822	321·8	11·2	382	381·8	13·3	442	441·7	15·4	502	501·7	17·5	562	561·7	19·6
823	322·8	11·3	383	382·8	13·3	443	442·7	15·4	503	502·7	17·5	563	562·7	19·6
824	323·8	11·3	384	383·8	13·4	444	443·7	15·5	504	503·7	17·6	564	563·7	19·6
825	324·8	11·3	385	384·8	13·4	445	444·7	15·5	505	504·7	17·6	565	564·7	19·7
826	325·8	11·4	386	385·8	13·5	446	445·7	15·6	506	505·7	17·6	566	565·7	19·7
827	326·8	11·4	387	386·8	13·5	447	446·7	15·6	507	506·7	17·7	567	566·7	19·7
828	327·8	11·4	388	387·8	13·5	448	447·7	15·6	508	507·7	17·7	568	567·7	19·8

TABLE 1

487

TRAVERSE TABLE TO DEGREES														
8°									0 ^h 12 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	300.6	15.7	361	360.5	18.9	421	420.4	22.0	481	480.3	25.2	541	540.2	28.3
302	301.6	15.8	362	361.5	19.0	422	421.4	22.1	482	481.3	25.2	542	541.2	28.4
303	302.6	15.9	363	362.5	19.0	423	422.4	22.2	483	482.3	25.3	543	542.2	28.4
304	303.5	15.9	364	363.5	19.1	424	423.4	22.2	484	483.3	25.3	544	543.2	28.5
305	304.5	16.0	365	364.5	19.1	425	424.4	22.3	485	484.3	25.4	545	544.2	28.5
306	305.5	16.0	366	365.5	19.2	426	425.4	22.3	486	485.3	25.4	546	545.2	28.6
307	306.5	16.1	367	366.5	19.2	427	426.4	22.4	487	486.3	25.5	547	546.2	28.6
308	307.5	16.1	368	367.5	19.3	428	427.4	22.4	488	487.3	25.5	548	547.2	28.7
309	308.5	16.2	369	368.5	19.3	429	428.4	22.5	489	488.3	25.6	549	548.2	28.7
310	309.5	16.2	370	369.5	19.4	430	429.4	22.5	490	489.3	25.6	550	549.2	28.8
311	310.5	16.3	371	370.5	19.4	431	430.4	22.6	491	490.3	25.7	551	550.2	28.8
312	311.5	16.3	372	371.5	19.5	432	431.4	22.6	492	491.3	25.7	552	551.2	28.9
313	312.5	16.4	373	372.5	19.5	433	432.4	22.7	493	492.3	25.8	553	552.2	28.9
314	313.5	16.4	374	373.5	19.6	434	433.4	22.7	494	493.3	25.9	554	553.2	29.0
315	314.5	16.5	375	374.5	19.6	435	434.4	22.8	495	494.3	25.9	555	554.2	29.1
316	315.5	16.6	376	375.5	19.7	436	435.4	22.8	496	495.3	26.0	556	555.2	29.1
317	316.5	16.6	377	376.5	19.8	437	436.4	22.9	497	496.3	26.0	557	556.2	29.2
318	317.5	16.7	378	377.4	19.8	438	437.4	22.9	498	497.3	26.1	558	557.2	29.2
319	318.5	16.7	379	378.4	19.9	439	438.4	23.0	499	498.3	26.1	559	558.2	29.3
320	319.5	16.8	380	379.4	19.9	440	439.4	23.0	500	499.3	26.2	560	559.2	29.3
321	320.5	16.8	381	380.4	20.0	441	440.4	23.1	501	500.3	26.2	561	560.2	29.4
322	321.5	16.9	382	381.4	20.0	442	441.4	23.1	502	501.3	26.3	562	561.2	29.4
323	322.5	16.9	383	382.4	20.1	443	442.4	23.2	503	502.3	26.3	563	562.2	29.5
324	323.5	17.0	384	383.4	20.1	444	443.4	23.3	504	503.3	26.4	564	563.2	29.5
325	324.5	17.0	385	384.4	20.2	445	444.4	23.3	505	504.3	26.4	565	564.2	29.6
326	325.5	17.1	386	385.4	20.2	446	445.4	23.4	506	505.3	26.5	566	565.2	29.6
327	326.5	17.1	387	386.4	20.3	447	446.4	23.4	507	506.3	26.5	567	566.2	29.7
328	327.5	17.2	388	387.4	20.3	448	447.4	23.5	508	507.3	26.6	568	567.2	29.7
329	328.5	17.2	389	388.4	20.4	449	448.4	23.5	509	508.3	26.6	569	568.2	29.8
330	329.5	17.3	390	389.4	20.4	450	449.3	23.6	510	509.3	26.7	570	569.2	29.8
331	330.5	17.3	391	390.4	20.5	451	450.3	23.6	511	510.3	26.7	571	570.2	29.9
332	331.5	17.4	392	391.4	20.5	452	451.3	23.7	512	511.3	26.8	572	571.2	29.9
333	332.5	17.5	393	392.4	20.6	453	452.3	23.7	513	512.3	26.8	573	572.2	30.0
334	333.5	17.5	394	393.4	20.6	454	453.3	23.8	514	513.3	26.9	574	573.2	30.0
335	334.5	17.6	395	394.4	20.7	455	454.3	23.8	515	514.3	27.0	575	574.2	30.1
336	335.5	17.6	396	395.4	20.7	456	455.3	23.9	516	515.3	27.0	576	575.2	30.1
337	336.5	17.7	397	396.4	20.8	457	456.3	23.9	517	516.3	27.1	577	576.2	30.2
338	337.5	17.7	398	397.4	20.8	458	457.3	24.0	518	517.3	27.1	578	577.2	30.2
339	338.5	17.8	399	398.4	20.9	459	458.3	24.0	519	518.3	27.2	579	578.2	30.3
340	339.5	17.8	400	399.4	20.9	460	459.3	24.1	520	519.3	27.2	580	579.2	30.3
341	340.5	17.9	401	400.4	21.0	461	460.3	24.1	521	520.3	27.3	581	580.2	30.4
342	341.5	17.9	402	401.4	21.1	462	461.3	24.2	522	521.3	27.3	582	581.2	30.4
343	342.5	18.0	403	402.4	21.1	463	462.3	24.2	523	522.3	27.4	583	582.2	30.5
344	343.5	18.0	404	403.4	21.2	464	463.3	24.3	524	523.3	27.4	584	583.2	30.5
345	344.5	18.1	405	404.4	21.2	465	464.3	24.4	525	524.3	27.5	585	584.2	30.6
346	345.5	18.1	406	405.4	21.3	466	465.3	24.4	526	525.3	27.5	586	585.2	30.6
347	346.5	18.2	407	406.4	21.3	467	466.3	24.5	527	526.3	27.6	587	586.2	30.7
348	347.5	18.2	408	407.4	21.4	468	467.3	24.5	528	527.3	27.6	588	587.2	30.7
349	348.5	18.3	409	408.4	21.4	469	468.3	24.6	529	528.3	27.7	589	588.2	30.8
350	349.5	18.3	410	409.4	21.5	470	469.3	24.6	530	529.3	27.7	590	589.2	30.9
351	350.5	18.4	411	410.4	21.5	471	470.3	24.7	531	530.3	27.8	591	590.2	30.9
352	351.5	18.4	412	411.4	21.6	472	471.3	24.7	532	531.3	27.8	592	591.2	31.0
353	352.5	18.5	413	412.4	21.6	473	472.3	24.8	533	532.3	27.9	593	592.2	31.0
354	353.5	18.5	414	413.4	21.7	474	473.3	24.8	534	533.3	27.9	594	593.2	31.1
355	354.5	18.6	415	414.4	21.7	475	474.3	24.9	535	534.3	28.0	595	594.2	31.1
356	355.5	18.6	416	415.4	21.8	476	475.3	24.9	536	535.3	28.1	596	595.2	31.2
357	356.5	18.7	417	416.4	21.8	477	476.3	25.0	537	536.3	28.1	597	596.2	31.2
358	357.5	18.8	418	417.4	21.9	478	477.3	25.0	538	537.3	28.2	598	597.2	31.3
359	358.5	18.8	419	418.4	21.9	479	478.3	25.1	539	538.3	28.2	599	598.2	31.3
360	359.5	18.9	420	419.4	22.0	480	479.3	25.1	540	539.3	28.3	600	599.2	31.4
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
87°									5 ^h 48 ^m					

TRAVERSE TABLE TO DEGREES														
4°									0° 16'					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	1°0	0.1	61	60.9	4.3	121	120.7	8.4	181	180.6	12.6	241	240.4	16.8
2	2°0	0.1	62	61.8	4.3	122	121.7	8.5	182	181.6	12.7	242	241.4	16.9
3	3°0	0.2	63	62.8	4.4	123	122.7	8.6	183	182.6	12.8	243	242.4	17.0
4	4°0	0.3	64	63.8	4.5	124	123.7	8.6	184	183.6	12.8	244	243.4	17.0
5	5°0	0.3	65	64.8	4.5	125	124.7	8.7	185	184.5	12.9	245	244.4	17.1
6	6°0	0.4	66	65.8	4.6	126	125.7	8.8	186	185.5	13.0	246	245.4	17.2
7	7°0	0.5	67	66.8	4.7	127	126.7	8.9	187	186.5	13.0	247	246.4	17.2
8	8°0	0.6	68	67.8	4.7	128	127.7	8.9	188	187.5	13.1	248	247.4	17.3
9	9°0	0.6	69	68.8	4.8	129	128.7	9.0	189	188.5	13.2	249	248.4	17.4
10	10°0	0.7	70	69.8	4.9	130	129.7	9.1	190	189.5	13.3	250	249.4	17.4
11	11°0	0.8	71	70.8	5.0	131	130.7	9.1	191	190.5	13.3	251	250.4	17.5
12	12°0	0.8	72	71.8	5.0	132	131.7	9.2	192	191.5	13.4	252	251.4	17.6
13	13°0	0.9	73	72.8	5.1	133	132.7	9.3	193	192.5	13.5	253	252.4	17.6
14	14°0	1.0	74	73.8	5.2	134	133.7	9.3	194	193.5	13.5	254	253.4	17.7
15	15°0	1.0	75	74.8	5.2	135	134.7	9.4	195	194.5	13.6	255	254.4	17.8
16	16°0	1.1	76	75.8	5.3	136	135.7	9.5	196	195.5	13.7	256	255.4	17.9
17	17°0	1.2	77	76.8	5.4	137	136.7	9.6	197	196.5	13.7	257	256.4	17.9
18	18°0	1.3	78	77.8	5.4	138	137.7	9.6	198	197.5	13.8	258	257.4	18.0
19	19°0	1.3	79	78.8	5.5	139	138.7	9.7	199	198.5	13.9	259	258.4	18.1
20	20°0	1.4	80	79.8	5.6	140	139.7	9.8	200	199.5	14.0	260	259.4	18.1
21	20°9	1.5	81	80.8	5.7	141	140.7	9.8	201	200.5	14.0	261	260.4	18.2
22	21°9	1.5	82	81.8	5.7	142	141.7	9.9	202	201.5	14.1	262	261.4	18.3
23	22°9	1.6	83	82.8	5.8	143	142.7	10.0	203	202.5	14.2	263	262.4	18.3
24	23°9	1.7	84	83.8	5.9	144	143.6	10.0	204	203.5	14.2	264	263.4	18.4
25	24°9	1.7	85	84.8	5.9	145	144.6	10.1	205	204.5	14.3	265	264.4	18.5
26	25°9	1.8	86	85.8	6.0	146	145.6	10.2	206	205.5	14.4	266	265.4	18.6
27	26°9	1.9	87	86.8	6.1	147	146.6	10.3	207	206.5	14.4	267	266.3	18.6
28	27°9	2.0	88	87.8	6.1	148	147.6	10.3	208	207.5	14.5	268	267.3	18.7
29	28°9	2.0	89	88.8	6.2	149	148.6	10.4	209	208.5	14.6	269	268.3	18.8
30	29°9	2.1	90	89.8	6.3	150	149.6	10.5	210	209.5	14.6	270	269.3	18.8
31	30°9	2.2	91	90.8	6.3	151	150.6	10.5	211	210.5	14.7	271	270.3	18.9
32	31°9	2.2	92	91.8	6.4	152	151.6	10.6	212	211.5	14.8	272	271.3	19.0
33	32°9	2.3	93	92.8	6.5	153	152.6	10.7	213	212.5	14.9	273	272.3	19.0
34	33°9	2.4	94	93.8	6.6	154	153.6	10.7	214	213.5	14.9	274	273.3	19.1
35	34°9	2.4	95	94.8	6.6	155	154.6	10.8	215	214.5	15.0	275	274.3	19.2
36	35°9	2.5	96	95.8	6.7	156	155.6	10.9	216	215.5	15.1	276	275.3	19.3
37	36°9	2.6	97	96.8	6.8	157	156.6	11.0	217	216.5	15.1	277	276.3	19.3
38	37°9	2.7	98	97.8	6.8	158	157.6	11.0	218	217.5	15.2	278	277.3	19.4
39	38°9	2.7	99	98.8	6.9	159	158.6	11.1	219	218.5	15.3	279	278.3	19.5
40	39°9	2.8	100	99.8	7.0	160	159.6	11.2	220	219.5	15.3	280	279.3	19.5
41	40°9	2.9	101	100.8	7.0	161	160.6	11.2	221	220.5	15.4	281	280.3	19.6
42	41°9	2.9	102	101.8	7.1	162	161.6	11.3	222	221.5	15.5	282	281.3	19.7
43	42°9	3.0	103	102.7	7.2	163	162.6	11.4	223	222.5	15.6	283	282.3	19.7
44	43°9	3.1	104	103.7	7.3	164	163.6	11.4	224	223.5	15.6	284	283.3	19.8
45	44°9	3.1	105	104.7	7.3	165	164.6	11.5	225	224.5	15.7	285	284.3	19.9
46	45°9	3.2	106	105.7	7.4	166	165.6	11.6	226	225.4	15.8	286	285.3	20.0
47	46°9	3.3	107	106.7	7.5	167	166.6	11.6	227	226.4	15.8	287	286.3	20.0
48	47°9	3.3	108	107.7	7.5	168	167.6	11.7	228	227.4	15.9	288	287.3	20.1
49	48°9	3.4	109	108.7	7.6	169	168.6	11.8	229	228.4	16.0	289	288.3	20.2
50	49°9	3.5	110	109.7	7.7	170	169.6	11.9	230	229.4	16.0	290	289.3	20.2
51	50°9	3.6	111	110.7	7.7	171	170.6	11.9	231	230.4	16.1	291	290.3	20.3
52	51°9	3.6	112	111.7	7.8	172	171.6	12.0	232	231.4	16.2	292	291.3	20.4
53	52°9	3.7	113	112.7	7.9	173	172.6	12.1	233	232.4	16.3	293	292.3	20.4
54	53°9	3.8	114	113.7	8.0	174	173.6	12.1	234	233.4	16.3	294	293.3	20.5
55	54°9	3.8	115	114.7	8.0	175	174.6	12.2	235	234.4	16.4	295	294.3	20.6
56	55°9	3.9	116	115.7	8.1	176	175.6	12.3	236	235.4	16.5	296	295.3	20.6
57	56°9	4.0	117	116.7	8.2	177	176.6	12.3	237	236.4	16.5	297	296.3	20.7
58	57°9	4.0	118	117.7	8.2	178	177.6	12.4	238	237.4	16.6	298	297.3	20.8
59	58°9	4.1	119	118.7	8.3	179	178.6	12.5	239	238.4	16.7	299	298.3	20.9
60	59°9	4.2	120	119.7	8.4	180	179.6	12.6	240	239.4	16.7	300	299.3	20.9
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

439

TRAVERSE TABLE TO DEGREES														
4°												0h 16m		
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
801	300.3	21.0	361	360.1	25.2	421	420.0	29.4	481	479.8	33.5	541	539.7	37.7
802	301.3	21.1	362	361.1	25.2	422	421.0	29.4	482	480.8	33.6	542	540.7	37.8
803	302.2	21.1	363	362.1	25.3	423	422.0	29.5	483	481.8	33.7	543	541.7	37.9
804	303.2	21.2	364	363.1	25.4	424	423.0	29.6	484	482.8	33.7	544	542.7	37.9
805	304.2	21.3	365	364.1	25.5	425	424.0	29.6	485	483.8	33.8	545	543.7	38.0
806	305.2	21.3	366	365.1	25.5	426	424.9	29.7	486	484.8	33.9	546	544.7	38.1
807	306.2	21.4	367	366.1	25.6	427	425.9	29.8	487	485.8	33.9	547	545.7	38.1
808	307.2	21.5	368	367.1	25.7	428	426.9	29.9	488	486.8	34.0	548	546.7	38.2
809	308.2	21.6	369	368.1	25.7	429	427.9	29.9	489	487.8	34.1	549	547.7	38.3
810	309.2	21.6	370	369.1	25.8	430	428.9	30.0	490	488.8	34.2	550	548.7	38.3
811	310.2	21.7	371	370.1	25.9	431	429.9	30.1	491	489.8	34.2	551	549.7	38.4
812	311.2	21.8	372	371.1	25.9	432	430.9	30.1	492	490.8	34.3	552	550.7	38.5
813	312.2	21.8	373	372.1	26.0	433	431.9	30.2	493	491.8	34.4	553	551.7	38.5
814	313.2	21.9	374	373.1	26.1	434	432.9	30.3	494	492.8	34.4	554	552.7	38.6
815	314.2	22.0	375	374.1	26.2	435	433.9	30.3	495	493.8	34.5	555	553.6	38.7
816	315.2	22.1	376	375.1	26.2	436	434.9	30.4	496	494.8	34.6	556	554.6	38.7
817	316.2	22.1	377	376.1	26.3	437	435.9	30.5	497	495.8	34.6	557	555.6	38.8
818	317.2	22.2	378	377.1	26.4	438	436.9	30.6	498	496.8	34.7	558	556.6	38.9
819	318.2	22.3	379	378.1	26.4	439	437.9	30.6	499	497.8	34.8	559	557.6	38.9
820	319.2	22.3	380	379.1	26.5	440	438.9	30.7	500	498.8	34.8	560	558.6	39.0
821	320.2	22.4	381	380.1	26.6	441	439.9	30.8	501	499.8	34.9	561	559.6	39.1
822	321.2	22.5	382	381.1	26.6	442	440.9	30.8	502	500.8	35.0	562	560.6	39.2
823	322.2	22.5	383	382.1	26.7	443	441.9	30.9	503	501.8	35.0	563	561.6	39.2
824	323.2	22.6	384	383.1	26.8	444	442.9	31.0	504	502.8	35.1	564	562.6	39.3
825	324.2	22.7	385	384.1	26.9	445	443.9	31.0	505	503.8	35.2	565	563.6	39.4
826	325.2	22.7	386	385.1	26.9	446	444.9	31.1	506	504.8	35.2	566	564.6	39.4
827	326.2	22.8	387	386.1	27.0	447	445.9	31.2	507	505.8	35.3	567	565.6	39.5
828	327.2	22.9	388	387.1	27.1	448	446.9	31.2	508	506.8	35.4	568	566.6	39.6
829	328.2	23.0	389	388.1	27.1	449	447.9	31.3	509	507.8	35.5	569	567.6	39.7
830	329.2	23.0	390	389.1	27.2	450	448.9	31.4	510	508.8	35.6	570	568.6	39.8
831	330.2	23.1	391	390.1	27.3	451	449.9	31.5	511	509.8	35.6	571	569.6	39.8
832	331.2	23.2	392	391.1	27.3	452	450.9	31.5	512	510.8	35.7	572	570.6	39.9
833	332.2	23.2	393	392.1	27.4	453	451.9	31.6	513	511.8	35.8	573	571.6	40.0
834	333.2	23.3	394	393.1	27.5	454	452.9	31.7	514	512.7	35.8	574	572.6	40.0
835	334.2	23.4	395	394.1	27.6	455	453.9	31.7	515	513.7	35.9	575	573.6	40.1
836	335.2	23.4	396	395.1	27.6	456	454.9	31.8	516	514.7	36.0	576	574.6	40.2
837	336.2	23.5	397	396.1	27.7	457	455.9	31.9	517	515.7	36.0	577	575.6	40.2
838	337.2	23.6	398	397.1	27.8	458	456.9	31.9	518	516.7	36.1	578	576.6	40.3
839	338.2	23.6	399	398.1	27.8	459	457.9	32.0	519	517.7	36.2	579	577.6	40.4
840	339.2	23.7	400	399.1	27.9	460	458.9	32.1	520	518.7	36.2	580	578.6	40.5
841	340.2	23.8	401	400.1	28.0	461	459.9	32.2	521	519.7	36.3	581	579.6	40.5
842	341.2	23.9	402	401.1	28.0	462	460.9	32.2	522	520.7	36.4	582	580.6	40.6
843	342.2	23.9	403	402.1	28.1	463	461.9	32.3	523	521.7	36.4	583	581.6	40.7
844	343.1	24.0	404	403.1	28.2	464	462.9	32.4	524	522.7	36.5	584	582.6	40.7
845	344.1	24.1	405	404.1	28.2	465	463.9	32.4	525	523.7	36.6	585	583.6	40.8
846	345.1	24.1	406	405.1	28.3	466	464.9	32.5	526	524.7	36.7	586	584.6	40.9
847	346.1	24.2	407	406.1	28.4	467	465.8	32.6	527	525.7	36.8	587	585.6	40.9
848	347.1	24.3	408	407.1	28.5	468	466.8	32.6	528	526.7	36.8	588	586.6	41.0
849	348.1	24.3	409	408.1	28.5	469	467.8	32.7	529	527.7	36.9	589	587.6	41.1
850	349.1	24.4	410	409.1	28.6	470	468.8	32.8	530	528.7	37.0	590	588.6	41.2
851	350.1	24.5	411	410.1	28.7	471	469.8	32.9	531	529.7	37.0	591	589.6	41.3
852	351.1	24.6	412	411.1	28.7	472	470.8	32.9	532	530.7	37.1	592	590.6	41.3
853	352.1	24.6	413	412.1	28.8	473	471.8	33.0	533	531.7	37.2	593	591.6	41.4
854	353.1	24.7	414	413.1	28.9	474	472.8	33.1	534	532.7	37.2	594	592.6	41.5
855	354.1	24.8	415	414.1	28.9	475	473.8	33.1	535	533.7	37.3	595	593.6	41.5
856	355.1	24.8	416	415.1	29.0	476	474.8	33.2	536	534.7	37.4	596	594.6	41.6
857	356.1	24.9	417	416.1	29.1	477	475.8	33.3	537	535.7	37.5	597	595.6	41.7
858	357.1	25.0	418	417.1	29.2	478	476.8	33.3	538	536.7	37.5	598	596.6	41.7
859	358.1	25.0	419	418.1	29.2	479	477.8	33.4	539	537.7	37.6	599	597.6	41.8
860	359.1	25.1	420	419.1	29.3	480	478.8	33.5	540	538.7	37.7	600	598.6	41.9
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
86°												5h 44m		

TABLE 1

TRAVERSE TABLE TO DEGREES														
5°									0h 20m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	299.9	26.2	361	359.6	31.5	421	419.4	36.7	481	479.2	41.9	541	538.9	47.3
302	300.8	26.3	362	360.6	31.6	422	420.4	36.8	482	480.2	42.0	542	539.9	47.3
303	301.8	26.4	363	361.6	31.6	423	421.4	36.9	483	481.2	42.1	543	540.9	47.4
304	302.8	26.5	364	362.6	31.7	424	422.4	37.0	484	482.2	42.2	544	541.9	47.5
305	303.8	26.6	365	363.6	31.8	425	423.4	37.1	485	483.2	42.3	545	542.9	47.6
306	304.8	26.7	366	364.6	31.9	426	424.4	37.1	486	484.1	42.4	546	543.9	47.7
307	305.8	26.8	367	365.6	32.0	427	425.4	37.2	487	485.1	42.4	547	544.9	47.7
308	306.8	26.9	368	366.6	32.1	428	426.4	37.3	488	486.1	42.5	548	545.9	47.8
309	307.8	26.9	369	367.6	32.2	429	427.4	37.4	489	487.1	42.6	549	546.9	47.9
310	308.8	27.0	370	368.6	32.3	430	428.4	37.5	490	488.1	42.7	550	547.9	48.0
311	309.8	27.1	371	369.6	32.3	431	429.4	37.6	491	489.1	42.8	551	548.9	48.1
312	310.8	27.2	372	370.6	32.4	432	430.4	37.7	492	490.1	42.9	552	549.9	48.2
313	311.8	27.3	373	371.6	32.5	433	431.3	37.7	493	491.1	43.0	553	550.9	48.3
314	312.8	27.4	374	372.6	32.6	434	432.3	37.8	494	492.1	43.1	554	551.9	48.4
315	313.8	27.5	375	373.6	32.7	435	433.3	37.9	495	493.1	43.1	555	552.9	48.4
316	314.8	27.5	376	374.6	32.8	436	434.3	38.0	496	494.1	43.2	556	553.9	48.5
317	315.8	27.6	377	375.6	32.9	437	435.3	38.1	497	495.1	43.3	557	554.9	48.6
318	316.8	27.7	378	376.6	33.0	438	436.3	38.2	498	496.1	43.4	558	555.9	48.7
319	317.8	27.8	379	377.6	33.0	439	437.3	38.3	499	497.1	43.5	559	556.9	48.8
320	318.8	27.9	380	378.6	33.1	440	438.3	38.4	500	498.1	43.6	560	557.9	48.8
321	319.8	28.0	381	379.5	33.2	441	439.3	38.4	501	499.1	43.7	561	558.8	48.9
322	320.8	28.1	382	380.5	33.3	442	440.3	38.5	502	500.1	43.8	562	559.8	49.0
323	321.8	28.2	383	381.5	33.4	443	441.3	38.6	503	501.1	43.8	563	560.8	49.1
324	322.8	28.2	384	382.5	33.5	444	442.3	38.7	504	502.1	43.9	564	561.8	49.2
325	323.8	28.3	385	383.5	33.6	445	443.3	38.8	505	503.1	44.0	565	562.8	49.3
326	324.8	28.4	386	384.5	33.7	446	444.3	38.9	506	504.1	44.1	566	563.8	49.4
327	325.8	28.5	387	385.5	33.7	447	445.3	39.0	507	505.1	44.1	567	564.8	49.5
328	326.7	28.6	388	386.5	33.8	448	446.3	39.1	508	506.1	44.3	568	565.8	49.6
329	327.7	28.7	389	387.5	33.9	449	447.3	39.1	509	507.1	44.4	569	566.8	49.7
330	328.7	28.8	390	388.5	34.0	450	448.3	39.2	510	508.1	44.5	570	567.8	49.7
331	329.7	28.9	391	389.5	34.1	451	449.3	39.3	511	509.0	44.5	571	568.8	49.8
332	330.7	28.9	392	390.5	34.2	452	450.3	39.4	512	510.0	44.6	572	569.8	49.9
333	331.7	29.0	393	391.5	34.3	453	451.3	39.5	513	511.0	44.7	573	570.8	50.0
334	332.7	29.1	394	392.5	34.3	454	452.3	39.6	514	512.0	44.8	574	571.8	50.1
335	333.7	29.2	395	393.5	34.4	455	453.3	39.7	515	513.0	44.9	575	572.8	50.2
336	334.7	29.3	396	394.5	34.5	456	454.3	39.8	516	514.0	45.0	576	573.8	50.3
337	335.7	29.4	397	395.5	34.6	457	455.3	39.8	517	515.0	45.1	577	574.8	50.4
338	336.7	29.5	398	396.5	34.7	458	456.3	39.9	518	516.0	45.2	578	575.8	50.4
339	337.7	29.6	399	397.5	34.8	459	457.3	40.0	519	517.0	45.2	579	576.8	50.5
340	338.7	29.6	400	398.5	34.9	460	458.2	40.1	520	518.0	45.3	580	577.8	50.6
341	339.7	29.7	401	399.5	35.0	461	459.2	40.2	521	519.0	45.4	581	578.8	50.7
342	340.7	29.8	402	400.5	35.0	462	460.2	40.3	522	520.0	45.5	582	579.8	50.8
343	341.7	29.9	403	401.5	35.1	463	461.2	40.4	523	521.0	45.6	583	580.8	50.9
344	342.7	30.0	404	402.5	35.2	464	462.2	40.4	524	522.0	45.7	584	581.8	50.9
345	343.7	30.1	405	403.5	35.3	465	463.2	40.5	525	523.0	45.8	585	582.8	51.0
346	344.7	30.2	406	404.5	35.4	466	464.2	40.6	526	524.0	45.9	586	583.8	51.1
347	345.7	30.3	407	405.4	35.5	467	465.2	40.7	527	525.0	45.9	587	584.8	51.2
348	346.7	30.3	408	406.4	35.6	468	466.2	40.8	528	526.0	46.0	588	585.8	51.3
349	347.7	30.4	409	407.4	35.7	469	467.2	40.9	529	527.0	46.1	589	586.8	51.4
350	348.7	30.5	410	408.4	35.7	470	468.2	41.0	530	528.0	46.2	590	587.8	51.5
351	349.7	30.6	411	409.4	35.8	471	469.2	41.1	531	529.0	46.3	591	588.7	51.6
352	350.7	30.7	412	410.4	35.9	472	470.2	41.1	532	530.0	46.4	592	589.7	51.6
353	351.7	30.8	413	411.4	36.0	473	471.2	41.2	533	531.0	46.5	593	590.7	51.7
354	352.6	30.9	414	412.4	36.1	474	472.2	41.3	534	532.0	46.6	594	591.7	51.8
355	353.6	30.9	415	413.4	36.2	475	473.2	41.4	535	533.0	46.6	595	592.7	51.9
356	354.6	31.0	416	414.4	36.3	476	474.2	41.5	536	533.9	46.7	596	593.7	52.0
357	355.6	31.1	417	415.4	36.4	477	475.2	41.6	537	534.9	46.8	597	594.7	52.1
358	356.6	31.2	418	416.4	36.4	478	476.2	41.7	538	535.9	46.9	598	595.7	52.2
359	357.6	31.3	419	417.4	36.5	479	477.2	41.8	539	536.9	47.0	599	596.7	52.3
360	358.6	31.4	420	418.4	36.6	480	478.2	41.8	540	537.9	47.1	600	597.7	52.3
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
85°									5h 40m					

TRAVERSE TABLE TO DEGREES														
0°									0° 24"					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	1'0	0'1	61	60'7	6'4	121	120'3	12'6	181	180'0	18'9	241	239'7	25'2
2	2'0	0'2	62	61'7	6'5	122	121'3	12'8	182	181'0	19'0	242	240'7	25'3
3	3'0	0'3	63	62'7	6'6	123	122'3	12'9	183	182'0	19'1	243	241'7	25'4
4	4'0	0'4	64	63'6	6'7	124	123'3	13'0	184	183'0	19'2	244	242'7	25'5
5	5'0	0'5	65	64'6	6'8	125	124'3	13'1	185	184'0	19'3	245	243'7	25'6
6	6'0	0'6	66	65'6	6'9	126	125'3	13'2	186	185'0	19'4	246	244'7	25'7
7	7'0	0'7	67	66'6	7'0	127	126'3	13'3	187	186'0	19'5	247	245'6	25'8
8	8'0	0'8	68	67'6	7'1	128	127'3	13'4	188	187'0	19'7	248	246'6	25'9
9	9'0	0'9	69	68'6	7'2	129	128'3	13'5	189	188'0	19'8	249	247'6	26'0
10	9'9	1'0	70	69'6	7'3	130	129'3	13'6	190	189'0	19'9	250	248'6	26'1
11	10'9	1'1	71	70'6	7'4	131	130'3	13'7	191	190'0	20'0	251	249'6	26'2
12	11'9	1'3	72	71'6	7'5	132	131'3	13'8	192	190'9	20'1	252	250'6	26'3
13	12'9	1'4	73	72'6	7'6	133	132'3	13'9	193	191'9	20'2	253	251'6	26'4
14	13'9	1'5	74	73'6	7'7	134	133'3	14'0	194	192'9	20'3	254	252'6	26'6
15	14'9	1'6	75	74'6	7'8	135	134'3	14'1	195	193'9	20'4	255	253'6	26'7
16	15'9	1'7	76	75'6	7'9	136	135'3	14'2	196	194'9	20'5	256	254'6	26'8
17	16'9	1'8	77	76'6	8'0	137	136'2	14'3	197	195'9	20'6	257	255'6	26'9
18	17'9	1'9	78	77'6	8'1	138	137'2	14'4	198	196'9	20'7	258	256'6	27'0
19	18'9	2'0	79	78'6	8'3	139	138'2	14'5	199	197'9	20'8	259	257'6	27'1
20	19'9	2'1	80	79'6	8'4	140	139'2	14'6	200	198'9	20'9	260	258'6	27'2
21	20'9	2'2	81	80'6	8'5	141	140'2	14'7	201	199'9	21'0	261	259'6	27'3
22	21'9	2'3	82	81'6	8'6	142	141'2	14'8	202	200'9	21'1	262	260'6	27'4
23	22'9	2'4	83	82'5	8'7	143	142'2	14'9	203	201'9	21'2	263	261'6	27'5
24	23'9	2'5	84	83'5	8'8	144	143'2	15'0	204	202'9	21'3	264	262'6	27'6
25	24'9	2'6	85	84'5	8'9	145	144'2	15'1	205	203'9	21'4	265	263'5	27'7
26	25'9	2'7	86	85'5	9'0	146	145'2	15'3	206	204'9	21'5	266	264'5	27'8
27	26'9	2'8	87	86'5	9'1	147	146'2	15'4	207	205'9	21'6	267	265'5	27'9
28	27'8	2'9	88	87'5	9'2	148	147'2	15'5	208	206'9	21'7	268	266'5	28'0
29	28'8	3'0	89	88'5	9'3	149	148'2	15'6	209	207'9	21'8	269	267'5	28'1
30	29'8	3'1	90	89'5	9'4	150	149'2	15'7	210	208'8	22'0	270	268'5	28'2
31	30'8	3'2	91	90'5	9'5	151	150'2	15'8	211	209'8	22'1	271	269'5	28'3
32	31'8	3'3	92	91'5	9'6	152	151'2	15'9	212	210'8	22'2	272	270'5	28'4
33	32'8	3'4	93	92'5	9'7	153	152'2	16'0	213	211'8	22'3	273	271'5	28'5
34	33'8	3'6	94	93'5	9'8	154	153'2	16'1	214	212'8	22'4	274	272'5	28'6
35	34'8	3'7	95	94'5	9'9	155	154'2	16'2	215	213'8	22'5	275	273'5	28'7
36	35'8	3'8	96	95'5	10'0	156	155'1	16'3	216	214'8	22'6	276	274'5	28'8
37	36'8	3'9	97	96'5	10'1	157	156'1	16'4	217	215'8	22'7	277	275'5	29'0
38	37'8	4'0	98	97'5	10'2	158	157'1	16'5	218	216'8	22'8	278	276'5	29'1
39	38'8	4'1	99	98'5	10'3	159	158'1	16'6	219	217'8	22'9	279	277'5	29'2
40	39'8	4'2	100	99'5	10'5	160	159'1	16'7	220	218'8	23'0	280	278'5	29'3
41	40'8	4'3	101	100'4	10'6	161	160'1	16'8	221	219'8	23'1	281	279'5	29'4
42	41'8	4'4	102	101'4	10'7	162	161'1	16'9	222	220'8	23'2	282	280'5	29'5
43	42'8	4'5	103	102'4	10'8	163	162'1	17'0	223	221'8	23'3	283	281'4	29'6
44	43'8	4'6	104	103'4	10'9	164	163'1	17'1	224	222'8	23'4	284	282'4	29'7
45	44'8	4'7	105	104'4	11'0	165	164'1	17'2	225	223'8	23'5	285	283'4	29'8
46	45'7	4'8	106	105'4	11'1	166	165'1	17'4	226	224'8	23'6	286	284'4	29'9
47	46'7	4'9	107	106'4	11'2	167	166'1	17'5	227	225'8	23'7	287	285'4	30'0
48	47'7	5'0	108	107'4	11'3	168	167'1	17'6	228	226'8	23'8	288	286'4	30'1
49	48'7	5'1	109	108'4	11'4	169	168'1	17'7	229	227'7	23'9	289	287'4	30'2
50	49'7	5'2	110	109'4	11'5	170	169'1	17'8	230	228'7	24'0	290	288'4	30'3
51	50'7	5'3	111	110'4	11'6	171	170'1	17'9	231	229'7	24'1	291	289'4	30'4
52	51'7	5'4	112	111'4	11'7	172	171'1	18'0	232	230'7	24'3	292	290'4	30'5
53	52'7	5'5	113	112'4	11'8	173	172'1	18'1	233	231'7	24'4	293	291'4	30'6
54	53'7	5'6	114	113'4	11'9	174	173'0	18'2	234	232'7	24'5	294	292'4	30'7
55	54'7	5'7	115	114'4	12'0	175	174'0	18'3	235	233'7	24'6	295	293'4	30'8
56	55'7	5'9	116	115'4	12'1	176	175'0	18'4	236	234'7	24'7	296	294'4	30'9
57	56'7	6'0	117	116'4	12'2	177	176'0	18'5	237	235'7	24'8	297	295'4	31'0
58	57'7	6'1	118	117'4	12'3	178	177'0	18'6	238	236'7	24'9	298	296'4	31'1
59	58'7	6'2	119	118'3	12'4	179	178'0	18'7	239	237'7	25'0	299	297'4	31'3
60	59'7	6'3	120	119'3	12'5	180	179'0	18'8	240	238'7	25'1	300	298'4	31'4
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

TRAVERSE TABLE TO DEGREES														
7°									0° 28'					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	1°0	0.1	61	60.5	7.4	121	120.1	14.7	181	179.7	22.1	241	239.2	29.4
2	2°0	0.2	62	61.5	7.6	122	121.1	14.9	182	180.6	22.2	242	240.2	29.5
3	3°0	0.4	63	62.5	7.7	123	122.1	15.0	183	181.6	22.3	243	241.2	29.6
4	4°0	0.5	64	63.5	7.8	124	123.1	15.1	184	182.6	22.4	244	242.2	29.7
5	5°0	0.6	65	64.5	7.9	125	124.1	15.2	185	183.6	22.5	245	243.2	29.9
6	6°0	0.7	66	65.5	8.0	126	125.1	15.4	186	184.6	22.7	246	244.2	30.0
7	7°0	0.9	67	66.5	8.2	127	126.1	15.5	187	185.6	22.8	247	245.2	30.1
8	7°9	1.0	68	67.5	8.3	128	127.0	15.6	188	186.6	22.9	248	246.2	30.2
9	8°9	1.1	69	68.5	8.4	129	128.0	15.7	189	187.6	23.0	249	247.1	30.3
10	9°9	1.2	70	69.5	8.5	130	129.0	15.8	190	188.6	23.2	250	248.1	30.5
11	10°9	1.3	71	70.5	8.7	131	130.0	16.0	191	189.6	23.3	251	249.1	30.6
12	11°9	1.5	72	71.5	8.8	132	131.0	16.1	192	190.6	23.4	252	250.1	30.7
13	12°9	1.6	73	72.5	8.9	133	132.0	16.2	193	191.6	23.5	253	251.1	30.8
14	13°9	1.7	74	73.4	9.0	134	133.0	16.3	194	192.6	23.6	254	252.1	31.0
15	14°9	1.8	75	74.4	9.1	135	134.0	16.5	195	193.5	23.8	255	253.1	31.1
16	15°9	1.9	76	75.4	9.3	136	135.0	16.6	196	194.5	23.9	256	254.1	31.2
17	16°9	2.1	77	76.4	9.4	137	136.0	16.7	197	195.5	24.0	257	255.1	31.3
18	17°9	2.2	78	77.4	9.5	138	137.0	16.8	198	196.5	24.1	258	256.1	31.4
19	18°9	2.3	79	78.4	9.6	139	138.0	16.9	199	197.5	24.3	259	257.1	31.6
20	19°9	2.4	80	79.4	9.7	140	139.0	17.1	200	198.5	24.4	260	258.1	31.7
21	20°8	2.6	81	80.4	9.9	141	139.9	17.2	201	199.5	24.5	261	259.1	31.8
22	21°8	2.7	82	81.4	10.0	142	140.9	17.3	202	200.5	24.6	262	260.0	31.9
23	22°8	2.8	83	82.4	10.1	143	141.9	17.4	203	201.5	24.7	263	261.0	32.1
24	23°8	2.9	84	83.4	10.2	144	142.9	17.5	204	202.5	24.9	264	262.0	32.2
25	24°8	3.0	85	84.4	10.4	145	143.9	17.7	205	203.5	25.0	265	263.0	32.3
26	25°8	3.2	86	85.4	10.5	146	144.9	17.8	206	204.5	25.1	266	264.0	32.4
27	26°8	3.3	87	86.4	10.6	147	145.9	17.9	207	205.5	25.2	267	265.0	32.5
28	27°8	3.4	88	87.3	10.7	148	146.9	18.0	208	206.4	25.3	268	266.0	32.7
29	28°8	3.5	89	88.3	10.8	149	147.9	18.2	209	207.4	25.5	269	267.0	32.8
30	29°8	3.7	90	89.3	11.0	150	148.9	18.3	210	208.4	25.6	270	268.0	32.9
31	30°8	3.8	91	90.3	11.1	151	149.9	18.4	211	209.4	25.7	271	269.0	33.0
32	31°8	3.9	92	91.3	11.2	152	150.9	18.5	212	210.4	25.8	272	270.0	33.1
33	32°8	4.0	93	92.3	11.3	153	151.9	18.6	213	211.4	26.0	273	271.0	33.3
34	33°7	4.1	94	93.3	11.5	154	152.9	18.8	214	212.4	26.1	274	272.0	33.4
35	34°7	4.3	95	94.3	11.6	155	153.8	18.9	215	213.4	26.2	275	273.0	33.5
36	35°7	4.4	96	95.3	11.7	156	154.8	19.0	216	214.4	26.3	276	273.9	33.6
37	36°7	4.5	97	96.3	11.8	157	155.8	19.1	217	215.4	26.4	277	274.9	33.8
38	37°7	4.6	98	97.3	11.9	158	156.8	19.3	218	216.4	26.6	278	275.9	33.9
39	38°7	4.8	99	98.3	12.1	159	157.8	19.4	219	217.4	26.7	279	276.9	34.0
40	39°7	4.9	100	99.3	12.2	160	158.8	19.5	220	218.4	26.8	280	277.9	34.1
41	40°7	5.0	101	100.2	12.3	161	159.8	19.6	221	219.4	26.9	281	278.9	34.2
42	41°7	5.1	102	101.2	12.4	162	160.8	19.7	222	220.3	27.1	282	279.9	34.4
43	42°7	5.2	103	102.2	12.6	163	161.8	19.9	223	221.3	27.2	283	280.9	34.5
44	43°7	5.4	104	103.2	12.7	164	162.8	20.0	224	222.3	27.3	284	281.9	34.6
45	44°7	5.5	105	104.2	12.8	165	163.8	20.1	225	223.3	27.4	285	282.9	34.7
46	45°7	5.6	106	105.2	12.9	166	164.8	20.2	226	224.3	27.5	286	283.9	34.9
47	46°6	5.7	107	106.2	13.0	167	165.8	20.4	227	225.3	27.7	287	284.9	35.0
48	47°6	5.8	108	107.2	13.2	168	166.7	20.5	228	226.3	27.8	288	285.9	35.1
49	48°6	6.0	109	108.2	13.3	169	167.7	20.6	229	227.3	27.9	289	286.8	35.2
50	49°6	6.1	110	109.2	13.4	170	168.7	20.7	230	228.3	28.0	290	287.8	35.3
51	50°6	6.2	111	110.2	13.5	171	169.7	20.8	231	229.3	28.2	291	288.8	35.5
52	51°6	6.3	112	111.2	13.6	172	170.7	21.0	232	230.3	28.3	292	289.8	35.6
53	52°6	6.5	113	112.2	13.8	173	171.7	21.1	233	231.3	28.4	293	290.8	35.7
54	53°6	6.6	114	113.2	13.9	174	172.7	21.2	234	232.3	28.5	294	291.8	35.8
55	54°6	6.7	115	114.1	14.0	175	173.7	21.3	235	233.2	28.6	295	292.8	36.0
56	55°6	6.8	116	115.1	14.1	176	174.7	21.4	236	234.2	28.8	296	293.8	36.1
57	56°6	6.9	117	116.1	14.3	177	175.7	21.6	237	235.2	28.9	297	294.8	36.2
58	57°6	7.1	118	117.1	14.4	178	176.7	21.7	238	236.2	29.0	298	295.8	36.3
59	58°6	7.2	119	118.1	14.5	179	177.7	21.8	239	237.2	29.1	299	296.8	36.4
60	59°6	7.3	120	119.1	14.6	180	178.7	21.9	240	238.2	29.2	300	297.8	36.6
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
83°									5° 32'					

TABLE 1

445

TRAVERSE TABLE TO DEGREES

7°

0h 28m

Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	298.7	36.7	361	358.3	44.0	421	417.9	51.3	481	477.4	58.6	541	537.0	65.9
302	299.7	36.8	362	359.3	44.1	422	418.8	51.4	482	478.4	58.7	542	537.9	66.0
303	300.7	36.9	363	360.3	44.2	423	419.8	51.5	483	479.4	58.8	543	538.9	66.2
304	301.7	37.0	364	361.3	44.4	424	420.8	51.7	484	480.4	59.0	544	539.9	66.3
305	302.7	37.2	365	362.3	44.5	425	421.8	51.8	485	481.4	59.1	545	540.9	66.4
306	303.7	37.3	366	363.3	44.6	426	422.8	51.9	486	482.4	59.2	546	541.9	66.6
307	304.7	37.4	367	364.3	44.7	427	423.8	52.0	487	483.4	59.4	547	542.9	66.7
308	305.7	37.5	368	365.2	44.8	428	424.8	52.2	488	484.3	59.5	548	543.9	66.8
309	306.7	37.7	369	366.2	45.0	429	425.8	52.3	489	485.3	59.6	549	544.9	66.9
310	307.7	37.8	370	367.2	45.1	430	426.8	52.4	490	486.3	59.7	550	545.9	67.0
311	308.7	37.9	371	368.2	45.2	431	427.8	52.5	491	487.3	59.8	551	546.9	67.1
312	309.7	38.0	372	369.2	45.3	432	428.8	52.6	492	488.3	59.9	552	547.9	67.2
313	310.7	38.1	373	370.2	45.5	433	429.8	52.8	493	489.3	60.1	553	548.9	67.4
314	311.7	38.3	374	371.2	45.6	434	430.8	52.9	494	490.3	60.2	554	549.9	67.5
315	312.6	38.4	375	372.2	45.7	435	431.7	53.0	495	491.3	60.3	555	550.8	67.6
316	313.6	38.5	376	373.2	45.8	436	432.7	53.1	496	492.3	60.5	556	551.8	67.8
317	314.6	38.6	377	374.2	45.9	437	433.7	53.3	497	493.3	60.6	557	552.8	67.9
318	315.6	38.7	378	375.2	46.1	438	434.7	53.4	498	494.3	60.7	558	553.8	68.0
319	316.6	38.9	379	376.2	46.2	439	435.7	53.5	499	495.3	60.8	559	554.8	68.1
320	317.6	39.0	380	377.2	46.3	440	436.7	53.6	500	496.3	61.0	560	555.8	68.3
321	318.6	39.1	381	378.1	46.4	441	437.7	53.7	501	497.2	61.1	561	556.8	68.4
322	319.6	39.2	382	379.1	46.5	442	438.7	53.9	502	498.2	61.2	562	557.8	68.5
323	320.6	39.4	383	380.1	46.7	443	439.7	54.0	503	499.2	61.3	563	558.8	68.6
324	321.6	39.5	384	381.1	46.8	444	440.7	54.1	504	500.2	61.4	564	559.8	68.7
325	322.6	39.6	385	382.1	46.9	445	441.7	54.2	505	501.2	61.5	565	560.8	68.9
326	323.6	39.7	386	383.1	47.0	446	442.7	54.3	506	502.2	61.6	566	561.8	69.0
327	324.6	39.8	387	384.1	47.2	447	443.7	54.5	507	503.2	61.8	567	562.8	69.1
328	325.5	40.0	388	385.1	47.3	448	444.7	54.6	508	504.2	61.9	568	563.8	69.2
329	326.5	40.1	389	386.1	47.4	449	445.6	54.7	509	505.2	62.0	569	564.8	69.3
330	327.5	40.2	390	387.1	47.5	450	446.6	54.8	510	506.2	62.1	570	565.8	69.4
331	328.5	40.3	391	388.1	47.6	451	447.6	55.0	511	507.2	62.3	571	566.7	69.6
332	329.5	40.5	392	389.1	47.8	452	448.6	55.1	512	508.2	62.4	572	567.7	69.7
333	330.5	40.6	393	390.1	47.9	453	449.6	55.2	513	509.2	62.5	573	568.7	69.8
334	331.5	40.7	394	391.1	48.0	454	450.6	55.3	514	510.2	62.6	574	569.7	69.9
335	332.5	40.8	395	392.0	48.1	455	451.6	55.4	515	511.1	62.7	575	570.7	70.1
336	333.5	40.9	396	393.0	48.3	456	452.6	55.6	516	512.1	62.9	576	571.7	70.2
337	334.5	41.1	397	394.0	48.4	457	453.6	55.7	517	513.1	63.0	577	572.7	70.3
338	335.5	41.2	398	395.0	48.5	458	454.6	55.8	518	514.1	63.1	578	573.7	70.4
339	336.5	41.3	399	396.0	48.6	459	455.6	55.9	519	515.1	63.2	579	574.7	70.5
340	337.5	41.4	400	397.0	48.7	460	456.6	56.1	520	516.1	63.4	580	575.7	70.7
341	338.4	41.6	401	398.0	48.9	461	457.6	56.2	521	517.1	63.5	581	576.7	70.8
342	339.4	41.7	402	399.0	49.0	462	458.5	56.3	522	518.1	63.6	582	577.6	70.9
343	340.4	41.8	403	400.0	49.1	463	459.5	56.4	523	519.1	63.7	583	578.6	71.0
344	341.4	41.9	404	401.0	49.2	464	460.5	56.5	524	520.1	63.8	584	579.6	71.2
345	342.4	42.0	405	402.0	49.4	465	461.5	56.7	525	521.1	64.0	585	580.6	71.3
346	343.4	42.2	406	403.0	49.5	466	462.5	56.8	526	522.1	64.1	586	581.6	71.4
347	344.4	42.3	407	404.0	49.6	467	463.5	56.9	527	523.1	64.2	587	582.6	71.5
348	345.4	42.4	408	405.0	49.7	468	464.5	57.0	528	524.1	64.3	588	583.6	71.6
349	346.4	42.5	409	405.9	49.8	469	465.5	57.2	529	525.0	64.5	589	584.6	71.8
350	347.4	42.6	410	406.9	50.0	470	466.5	57.3	530	526.0	64.6	590	585.6	71.9
351	348.4	42.8	411	407.9	50.1	471	467.5	57.4	531	527.0	64.7	591	586.6	72.0
352	349.4	42.9	412	408.9	50.2	472	468.5	57.5	532	528.0	64.8	592	587.6	72.1
353	350.4	43.0	413	409.9	50.3	473	469.5	57.6	533	529.0	64.9	593	588.6	72.2
354	351.4	43.1	414	410.9	50.4	474	470.5	57.8	534	530.0	65.1	594	589.6	72.4
355	352.3	43.3	415	411.9	50.6	475	471.5	57.9	535	531.0	65.2	595	590.6	72.5
356	353.3	43.4	416	412.9	50.7	476	472.4	58.0	536	532.0	65.3	596	591.5	72.6
357	354.3	43.5	417	413.9	50.8	477	473.4	58.1	537	533.0	65.4	597	592.5	72.7
358	355.3	43.6	418	414.9	50.9	478	474.4	58.2	538	534.0	65.6	598	593.5	72.9
359	356.3	43.7	419	415.9	51.1	479	475.4	58.4	539	535.0	65.7	599	594.5	73.0
360	357.3	43.9	420	416.9	51.2	480	476.4	58.5	540	536.0	65.8	600	595.5	73.1

83°

5h 32m

TABLE 1

447

TRAVERSE TABLE TO DEGREES														
8°										0h 32m				
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	298°0	41°9	361	357°5	50°2	421	416°9	58°6	481	476°3	66°9	541	535°7	75°2
302	299°0	42°0	362	358°5	50°4	422	417°9	58°7	482	477°3	67°1	542	536°7	75°4
303	300°0	42°2	363	359°4	50°5	423	418°9	58°9	483	478°3	67°2	543	537°7	75°5
304	301°0	42°3	364	360°4	50°7	424	419°8	59°0	484	479°3	67°4	544	538°7	75°7
305	302°0	42°5	365	361°4	50°8	425	420°8	59°2	485	480°3	67°5	545	539°7	75°8
306	303°0	42°6	366	362°4	50°9	426	421°8	59°3	486	481°2	67°6	546	540°6	75°9
307	304°0	42°7	367	363°4	51°1	427	422°8	59°4	487	482°2	67°8	547	541°6	76°1
308	305°0	42°9	368	364°4	51°2	428	423°8	59°6	488	483°2	67°9	548	542°6	76°2
309	306°0	43°0	369	365°4	51°4	429	424°8	59°7	489	484°2	68°1	549	543°6	76°4
310	307°0	43°1	370	366°4	51°5	430	425°8	59°8	490	485°2	68°2	550	544°6	76°5
311	307°9	43°3	371	367°4	51°6	431	426°8	60°0	491	486°2	68°3	551	545°6	76°6
312	308°9	43°4	372	368°4	51°8	432	427°8	60°1	492	487°2	68°5	552	546°6	76°8
313	309°9	43°6	373	369°3	51°9	433	428°8	60°3	493	488°2	68°6	553	547°6	76°9
314	310°9	43°7	374	370°3	52°1	434	429°8	60°4	494	489°2	68°8	554	548°6	77°1
315	311°9	43°8	375	371°3	52°2	435	430°7	60°5	495	490°2	68°9	555	549°6	77°2
316	312°9	44°0	376	372°3	52°3	436	431°7	60°7	496	491°2	69°0	556	550°6	77°4
317	313°9	44°1	377	373°3	52°5	437	432°7	60°8	497	492°1	69°2	557	551°5	77°5
318	314°9	44°3	378	374°3	52°6	438	433°7	61°0	498	493°1	69°3	558	552°5	77°6
319	315°9	44°4	379	375°3	52°7	439	434°7	61°1	499	494°1	69°5	559	553°5	77°8
320	316°9	44°5	380	376°3	52°9	440	435°7	61°2	500	495°1	69°6	560	554°5	77°9
321	317°9	44°7	381	377°3	53°0	441	436°7	61°4	501	496°1	69°7	561	555°5	78°1
322	318°8	44°8	382	378°3	53°2	442	437°7	61°5	502	497°1	69°9	562	556°5	78°2
323	319°8	45°0	383	379°2	53°3	443	438°7	61°7	503	498°1	70°0	563	557°5	78°3
324	320°8	45°1	384	380°2	53°4	444	439°7	61°8	504	499°1	70°2	564	558°5	78°5
325	321°8	45°2	385	381°2	53°6	445	440°6	61°9	505	500°1	70°3	565	559°5	78°6
326	322°8	45°4	386	382°2	53°7	446	441°6	62°1	506	501°0	70°4	566	560°5	78°8
327	323°8	45°5	387	383°2	53°9	447	442°6	62°2	507	502°0	70°6	567	561°5	78°9
328	324°8	45°7	388	384°2	54°0	448	443°6	62°4	508	503°0	70°7	568	562°5	79°0
329	325°8	45°8	389	385°2	54°1	449	444°6	62°5	509	504°0	70°8	569	563°5	79°1
330	326°8	45°9	390	386°2	54°3	450	445°6	62°6	510	505°0	70°9	570	564°5	79°3
331	327°8	46°1	391	387°2	54°4	451	446°6	62°8	511	506°0	71°1	571	565°4	79°4
332	328°7	46°2	392	388°2	54°6	452	447°6	62°9	512	507°0	71°2	572	566°4	79°6
333	329°7	46°3	393	389°1	54°7	453	448°6	63°0	513	508°0	71°4	573	567°4	79°7
334	330°7	46°5	394	390°1	54°8	454	449°6	63°2	514	509°0	71°5	574	568°4	79°8
335	331°7	46°6	395	391°1	55°0	455	450°5	63°3	515	510°0	71°6	575	569°4	80°0
336	332°7	46°8	396	392°1	55°1	456	451°5	63°5	516	510°9	71°8	576	570°4	80°1
337	333°7	46°9	397	393°1	55°3	457	452°5	63°6	517	511°9	71°9	577	571°4	80°2
338	334°7	47°0	398	394°1	55°4	458	453°5	63°7	518	512°9	72°0	578	572°4	80°4
339	335°7	47°2	399	395°1	55°5	459	454°5	63°9	519	513°9	72°2	579	573°4	80°5
340	336°7	47°3	400	396°1	55°7	460	455°5	64°0	520	514°9	72°3	580	574°4	80°6
341	337°7	47°5	401	397°1	55°8	461	456°5	64°2	521	515°9	72°4	581	575°4	80°8
342	338°6	47°6	402	398°1	56°0	462	457°5	64°3	522	516°9	72°6	582	576°4	80°9
343	339°6	47°7	403	399°1	56°1	463	458°5	64°4	523	517°9	72°8	583	577°4	81°1
344	340°6	47°9	404	400°0	56°2	464	459°5	64°6	524	518°9	73°0	584	578°4	81°3
345	341°6	48°0	405	401°0	56°4	465	460°4	64°7	525	519°9	73°1	585	579°4	81°4
346	342°6	48°2	406	402°0	56°5	466	461°4	64°9	526	520°9	73°2	586	580°3	81°6
347	343°6	48°3	407	403°0	56°6	467	462°4	65°0	527	521°8	73°4	587	581°3	81°7
348	344°6	48°4	408	404°0	56°8	468	463°4	65°1	528	522°8	73°5	588	582°3	81°8
349	345°6	48°6	409	405°0	56°9	469	464°4	65°3	529	523°8	73°7	589	583°3	82°0
350	346°6	48°7	410	406°0	57°1	470	465°4	65°4	530	524°8	73°8	590	584°3	82°1
351	347°6	48°9	411	407°0	57°2	471	466°4	65°6	531	525°8	73°9	591	585°3	82°2
352	348°5	49°0	412	408°0	57°3	472	467°4	65°7	532	526°8	74°1	592	586°3	82°4
353	349°5	49°1	413	409°0	57°5	473	468°4	65°8	533	527°8	74°2	593	587°3	82°5
354	350°5	49°3	414	409°9	57°6	474	469°4	66°0	534	528°8	74°3	594	588°3	82°6
355	351°5	49°4	415	410°9	57°8	475	470°4	66°1	535	529°8	74°5	595	589°3	82°8
356	352°5	49°5	416	411°9	57°9	476	471°3	66°2	536	530°8	74°6	596	590°3	83°0
357	353°5	49°7	417	412°9	58°0	477	472°3	66°4	537	531°7	74°7	597	591°2	83°1
358	354°5	49°8	418	413°9	58°2	478	473°3	66°5	538	532°7	74°9	598	592°2	83°2
359	355°5	50°0	419	414°9	58°3	479	474°3	66°7	539	533°7	75°0	599	593°2	83°3
360	356°5	50°1	420	415°9	58°5	480	475°3	66°8	540	534°7	75°1	600	594°2	83°5
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
82°										5h 22m				

TRAVERSE TABLE TO DEGREES

9°									0° 36'					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	1'0	0'2	61	60'2	9'5	121	119'5	18'9	181	178'8	28'3	241	238'0	37'7
2	2'0	0'3	62	61'2	9'7	122	120'5	19'1	182	179'8	28'5	242	239'0	37'9
3	3'0	0'5	63	62'2	9'9	123	121'5	19'2	183	180'7	28'6	243	240'0	38'0
4	4'0	0'6	64	63'2	10'0	124	122'5	19'4	184	181'7	28'8	244	241'0	38'2
5	4'9	0'8	65	64'2	10'2	125	123'5	19'6	185	182'7	28'9	245	242'0	38'3
6	5'9	0'9	66	65'2	10'3	126	124'4	19'7	186	183'7	29'1	246	243'0	38'5
7	6'9	1'1	67	66'2	10'5	127	125'4	19'9	187	184'7	29'3	247	244'0	38'6
8	7'9	1'3	68	67'2	10'6	128	126'4	20'0	188	185'7	29'4	248	244'9	38'8
9	8'9	1'4	69	68'2	10'8	129	127'4	20'2	189	186'7	29'6	249	245'9	39'0
10	9'9	1'6	70	69'1	11'0	130	128'4	20'3	190	187'7	29'7	250	246'9	39'1
11	10'9	1'7	71	70'1	11'1	131	129'4	20'5	191	188'6	29'9	251	247'9	39'3
12	11'9	1'9	72	71'1	11'3	132	130'4	20'6	192	189'6	30'0	252	248'9	39'4
13	12'8	2'0	73	72'1	11'4	133	131'4	20'8	193	190'6	30'2	253	249'9	39'6
14	13'8	2'2	74	73'1	11'6	134	132'4	21'0	194	191'6	30'3	254	250'9	39'7
15	14'8	2'3	75	74'1	11'7	135	133'3	21'1	195	192'6	30'5	255	251'9	39'9
16	15'8	2'5	76	75'1	11'9	136	134'3	21'3	196	193'6	30'7	256	252'8	40'0
17	16'8	2'7	77	76'1	12'0	137	135'3	21'4	197	194'6	30'8	257	253'8	40'2
18	17'8	2'8	78	77'0	12'2	138	136'3	21'6	198	195'6	31'0	258	254'8	40'4
19	18'8	3'0	79	78'0	12'4	139	137'3	21'7	199	196'5	31'1	259	255'8	40'5
20	19'8	3'1	80	79'0	12'5	140	138'3	21'9	200	197'5	31'3	260	256'8	40'7
21	20'7	3'3	81	80'0	12'7	141	139'3	22'1	201	198'5	31'4	261	257'8	40'8
22	21'7	3'4	82	81'0	12'8	142	140'3	22'2	202	199'5	31'6	262	258'8	41'0
23	22'7	3'6	83	82'0	13'0	143	141'2	22'4	203	200'5	31'8	263	259'8	41'1
24	23'7	3'8	84	83'0	13'1	144	142'2	22'5	204	201'5	31'9	264	260'7	41'3
25	24'7	3'9	85	84'0	13'3	145	143'2	22'7	205	202'5	32'1	265	261'7	41'5
26	25'7	4'1	86	84'9	13'5	146	144'2	22'8	206	203'5	32'2	266	262'7	41'6
27	26'7	4'2	87	85'9	13'6	147	145'2	23'0	207	204'5	32'4	267	263'7	41'8
28	27'7	4'4	88	86'9	13'8	148	146'2	23'2	208	205'4	32'5	268	264'7	41'9
29	28'6	4'5	89	87'9	13'9	149	147'2	23'3	209	206'4	32'7	269	265'7	42'1
30	29'6	4'7	90	88'9	14'1	150	148'2	23'5	210	207'4	32'9	270	266'7	42'2
31	30'6	4'8	91	89'9	14'2	151	149'1	23'6	211	208'4	33'0	271	267'7	42'4
32	31'6	5'0	92	90'9	14'4	152	150'1	23'8	212	209'4	33'2	272	268'7	42'6
33	32'6	5'2	93	91'9	14'5	153	151'1	23'9	213	210'4	33'3	273	269'6	42'7
34	33'6	5'3	94	92'8	14'7	154	152'1	24'1	214	211'4	33'5	274	270'6	42'9
35	34'6	5'5	95	93'8	14'9	155	153'1	24'2	215	212'4	33'6	275	271'6	43'0
36	35'6	5'6	96	94'8	15'0	156	154'1	24'4	216	213'3	33'8	276	272'6	43'2
37	36'5	5'8	97	95'8	15'2	157	155'1	24'6	217	214'3	33'9	277	273'6	43'3
38	37'5	5'9	98	96'8	15'3	158	156'1	24'7	218	215'3	34'1	278	274'6	43'5
39	38'5	6'1	99	97'8	15'5	159	157'0	24'9	219	216'3	34'3	279	275'6	43'6
40	39'5	6'3	100	98'8	15'6	160	158'0	25'0	220	217'3	34'4	280	276'6	43'8
41	40'5	6'4	101	99'8	15'8	161	159'0	25'2	221	218'3	34'6	281	277'5	44'0
42	41'5	6'6	102	100'7	16'0	162	160'0	25'3	222	219'3	34'7	282	278'5	44'1
43	42'5	6'7	103	101'7	16'1	163	161'0	25'5	223	220'3	34'9	283	279'5	44'3
44	43'5	6'9	104	102'7	16'3	164	162'0	25'7	224	221'2	35'0	284	280'5	44'4
45	44'4	7'0	105	103'7	16'4	165	163'0	25'8	225	222'2	35'2	285	281'5	44'6
46	45'4	7'2	106	104'7	16'6	166	164'0	26'0	226	223'2	35'4	286	282'5	44'7
47	46'4	7'4	107	105'7	16'7	167	164'9	26'1	227	224'2	35'5	287	283'5	44'9
48	47'4	7'5	108	106'7	16'9	168	165'9	26'3	228	225'2	35'7	288	284'5	45'1
49	48'4	7'7	109	107'7	17'1	169	166'9	26'4	229	226'2	35'8	289	285'4	45'2
50	49'4	7'8	110	108'6	17'2	170	167'9	26'6	230	227'2	36'0	290	286'4	45'4
51	50'4	8'0	111	109'6	17'4	171	168'9	26'8	231	228'2	36'1	291	287'4	45'5
52	51'4	8'1	112	110'6	17'5	172	169'9	26'9	232	229'1	36'3	292	288'4	45'7
53	52'3	8'3	113	111'6	17'7	173	170'9	27'1	233	230'1	36'4	293	289'4	45'8
54	53'3	8'4	114	112'6	17'8	174	171'9	27'2	234	231'1	36'6	294	290'4	46'0
55	54'3	8'6	115	113'6	18'0	175	172'8	27'4	235	232'1	36'8	295	291'4	46'1
56	55'3	8'8	116	114'6	18'1	176	173'8	27'5	236	233'1	36'9	296	292'4	46'3
57	56'3	8'9	117	115'6	18'3	177	174'8	27'7	237	234'1	37'1	297	293'3	46'5
58	57'3	9'1	118	116'5	18'5	178	175'8	27'8	238	235'1	37'2	298	294'3	46'6
59	58'3	9'2	119	117'5	18'6	179	176'8	28'0	239	236'1	37'4	299	295'3	46'8
60	59'3	9'4	120	118'5	18'8	180	177'8	28'2	240	237'0	37'5	300	296'3	46'9
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

TRAVERSE TABLE TO DEGREES														
9°									0° 86m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	297.3	47.1	361	356.6	56.5	421	415.8	65.9	481	475.1	75.2	541	534.4	84.6
302	298.3	47.2	362	357.5	56.7	422	416.8	66.0	482	476.1	75.3	542	535.4	84.7
303	299.3	47.4	363	358.5	56.8	423	417.8	66.2	483	477.1	75.5	543	536.3	84.9
304	300.3	47.6	364	359.5	56.9	424	418.8	66.3	484	478.0	75.6	544	537.3	85.1
305	301.2	47.7	365	360.5	57.1	425	419.8	66.5	485	479.0	75.8	545	538.3	85.3
306	302.2	47.9	366	361.5	57.3	426	420.8	66.6	486	480.0	75.9	546	539.3	85.4
307	303.2	48.0	367	362.5	57.4	427	421.7	66.8	487	481.0	76.1	547	540.3	85.6
308	304.2	48.2	368	363.5	57.6	428	422.7	67.0	488	482.0	76.2	548	541.3	85.7
309	305.2	48.3	369	364.5	57.7	429	423.7	67.1	489	483.0	76.4	549	542.3	85.9
310	306.2	48.5	370	365.4	57.9	430	424.7	67.3	490	484.0	76.5	550	543.3	86.0
311	307.2	48.7	371	366.4	58.1	431	425.7	67.4	491	485.0	76.7	551	544.3	86.2
312	308.2	48.8	372	367.4	58.2	432	426.7	67.6	492	485.9	76.8	552	545.2	86.3
313	309.1	49.0	373	368.4	58.4	433	427.7	67.7	493	486.9	77.0	553	546.2	86.5
314	310.1	49.1	374	369.4	58.5	434	428.7	67.9	494	487.9	77.1	554	547.2	86.6
315	311.1	49.3	375	370.4	58.7	435	429.6	68.1	495	488.9	77.3	555	548.2	86.8
316	312.1	49.4	376	371.4	58.8	436	430.6	68.2	496	489.9	77.5	556	549.2	87.0
317	313.1	49.6	377	372.4	59.0	437	431.6	68.4	497	490.9	77.7	557	550.2	87.1
318	314.1	49.8	378	373.3	59.1	438	432.6	68.5	498	491.9	77.9	558	551.2	87.3
319	315.1	49.9	379	374.3	59.3	439	433.6	68.7	499	492.9	78.0	559	552.2	87.4
320	316.1	50.1	380	375.3	59.5	440	434.6	68.8	500	493.8	78.2	560	553.1	87.6
321	317.0	50.2	381	376.3	59.6	441	435.6	69.0	501	494.8	78.4	561	554.1	87.7
322	318.0	50.4	382	377.3	59.8	442	436.6	69.1	502	495.8	78.5	562	555.1	87.9
323	319.0	50.5	383	378.3	59.9	443	437.5	69.3	503	496.8	78.7	563	556.1	88.0
324	320.0	50.7	384	379.3	60.1	444	438.5	69.5	504	497.8	78.8	564	557.1	88.2
325	321.0	50.8	385	380.3	60.2	445	439.5	69.6	505	498.8	79.0	565	558.1	88.3
326	322.0	51.0	386	381.2	60.4	446	440.5	69.8	506	499.8	79.1	566	559.1	88.5
327	323.0	51.2	387	382.2	60.5	447	441.5	69.9	507	500.8	79.2	567	560.1	88.6
328	324.0	51.3	388	383.2	60.7	448	442.5	70.1	508	501.7	79.4	568	561.0	88.8
329	324.9	51.5	389	384.2	60.9	449	443.5	70.2	509	502.7	79.5	569	562.0	88.9
330	325.9	51.7	390	385.2	61.0	450	444.5	70.4	510	503.7	79.7	570	563.0	89.1
331	326.9	51.8	391	386.2	61.2	451	445.4	70.6	511	504.7	79.8	571	564.0	89.2
332	327.9	51.9	392	387.2	61.3	452	446.4	70.7	512	505.7	80.1	572	565.0	89.4
333	328.9	52.1	393	388.2	61.5	453	447.4	70.9	513	506.7	80.2	573	566.0	89.5
334	329.9	52.3	394	389.1	61.6	454	448.4	71.0	514	507.7	80.3	574	567.0	89.7
335	330.9	52.4	395	390.1	61.8	455	449.4	71.2	515	508.7	80.5	575	568.0	89.9
336	331.9	52.6	396	391.1	62.0	456	450.4	71.3	516	509.6	80.6	576	568.9	90.1
337	332.8	52.7	397	392.1	62.1	457	451.4	71.5	517	510.6	80.8	577	569.9	90.2
338	333.8	52.9	398	393.1	62.3	458	452.4	71.7	518	511.6	80.9	578	570.9	90.3
339	334.8	53.0	399	394.1	62.4	459	453.3	71.8	519	512.6	81.1	579	571.9	90.5
340	335.8	53.2	400	395.1	62.6	460	454.3	72.0	520	513.6	81.3	580	572.9	90.7
341	336.8	53.3	401	396.1	62.7	461	455.3	72.1	521	514.6	81.4	581	573.9	90.9
342	337.8	53.5	402	397.0	62.9	462	456.3	72.3	522	515.6	81.6	582	574.9	91.0
343	338.8	53.7	403	398.0	63.0	463	457.3	72.4	523	516.6	81.8	583	575.9	91.2
344	339.8	53.8	404	399.0	63.2	464	458.3	72.6	524	517.6	81.9	584	576.9	91.3
345	340.8	54.0	405	400.0	63.4	465	459.3	72.7	525	518.6	82.1	585	577.9	91.5
346	341.7	54.1	406	401.0	63.5	466	460.3	72.9	526	519.5	82.3	586	578.8	91.7
347	342.7	54.3	407	402.0	63.7	467	461.2	73.1	527	520.5	82.4	587	579.8	91.8
348	343.7	54.4	408	403.0	63.8	468	462.2	73.2	528	521.5	82.6	588	580.8	92.0
349	344.7	54.6	409	404.0	64.0	469	463.2	73.4	529	522.5	82.7	589	581.8	92.1
350	345.7	54.8	410	405.0	64.1	470	464.2	73.5	530	523.5	82.9	590	582.8	92.2
351	346.7	54.9	411	405.9	64.3	471	465.2	73.7	531	524.5	83.1	591	583.8	92.4
352	347.7	55.1	412	406.9	64.5	472	466.2	73.8	532	525.5	83.2	592	584.8	92.5
353	348.7	55.2	413	407.9	64.6	473	467.2	74.0	533	526.5	83.4	593	585.7	92.7
354	349.6	55.4	414	408.9	64.8	474	468.2	74.2	534	527.5	83.5	594	586.7	92.9
355	350.6	55.5	415	409.9	64.9	475	469.2	74.3	535	528.4	83.7	595	587.7	93.1
356	351.6	55.7	416	410.9	65.1	476	470.1	74.5	536	529.4	83.8	596	588.7	93.2
357	352.6	55.9	417	411.9	65.2	477	471.1	74.6	537	530.4	84.0	597	589.7	93.4
358	353.6	56.0	418	412.9	65.4	478	472.1	74.8	538	531.4	84.1	598	590.7	93.5
359	354.6	56.2	419	413.8	65.6	479	473.1	74.9	539	532.4	84.3	599	591.7	93.7
360	355.6	56.3	420	414.8	65.7	480	474.1	75.0	540	533.4	84.4	600	592.6	93.8
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

81°

8° 24m

TRAVERSE TABLE TO DEGREES														
10°									0° 40'					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	1°0	0.2	61	60.1	10.6	121	119.2	21.0	181	178.3	31.4	241	237.3	41.8
2	2°0	0.3	62	61.1	10.8	122	120.1	21.2	182	179.2	31.6	242	238.3	42.0
3	3°0	0.5	63	62.0	10.9	123	121.1	21.4	183	180.2	31.8	243	239.3	42.2
4	3°9	0.7	64	63.0	11.1	124	122.1	21.5	184	181.2	32.0	244	240.3	42.4
5	4°9	0.9	65	64.0	11.3	125	123.1	21.7	185	182.2	32.1	245	241.3	42.5
6	5°9	1.0	66	65.0	11.5	126	124.1	21.9	186	183.2	32.3	246	242.3	42.7
7	6°9	1.2	67	66.0	11.6	127	125.1	22.1	187	184.2	32.5	247	243.2	42.9
8	7°9	1.4	68	67.0	11.8	128	126.1	22.2	188	185.1	32.6	248	244.2	43.1
9	8°9	1.6	69	68.0	12.0	129	127.0	22.4	189	186.1	32.8	249	245.2	43.2
10	9°8	1.7	70	68.9	12.2	130	128.0	22.6	190	187.1	33.0	250	246.2	43.4
11	10°8	1.9	71	69.9	12.3	131	129.0	22.7	191	188.1	33.2	251	247.2	43.6
12	11°8	2.1	72	70.9	12.5	132	130.0	22.9	192	189.1	33.3	252	248.2	43.8
13	12°8	2.3	73	71.9	12.7	133	131.0	23.1	193	190.1	33.5	253	249.2	43.9
14	13°8	2.4	74	72.9	12.8	134	132.0	23.3	194	191.1	33.7	254	250.1	44.1
15	14°8	2.6	75	73.9	13.0	135	132.9	23.4	195	192.0	33.9	255	251.1	44.3
16	15°8	2.8	76	74.8	13.2	136	133.9	23.6	196	193.0	34.0	256	252.1	44.5
17	16°7	3.0	77	75.8	13.4	137	134.9	23.8	197	194.0	34.2	257	253.1	44.6
18	17°7	3.1	78	76.8	13.5	138	135.9	24.0	198	195.0	34.4	258	254.1	44.8
19	18°7	3.3	79	77.8	13.7	139	136.9	24.1	199	196.0	34.6	259	255.1	45.0
20	19°7	3.5	80	78.8	13.9	140	137.9	24.3	200	197.0	34.7	260	256.1	45.1
21	20°7	3.6	81	79.8	14.1	141	138.9	24.5	201	197.9	34.9	261	257.0	45.3
22	21°7	3.8	82	80.8	14.2	142	139.8	24.7	202	198.9	35.1	262	258.0	45.5
23	22°7	4.0	83	81.7	14.4	143	140.8	24.8	203	199.9	35.3	263	259.0	45.7
24	23°6	4.2	84	82.7	14.6	144	141.8	25.0	204	200.9	35.4	264	260.0	45.8
25	24°6	4.3	85	83.7	14.8	145	142.8	25.2	205	201.9	35.6	265	261.0	46.0
26	25°6	4.5	86	84.7	14.9	146	143.8	25.4	206	202.9	35.8	266	262.0	46.2
27	26°6	4.7	87	85.7	15.1	147	144.8	25.5	207	203.9	35.9	267	262.9	46.4
28	27°6	4.9	88	86.7	15.3	148	145.8	25.7	208	204.8	36.1	268	263.9	46.5
29	28°6	5.0	89	87.6	15.5	149	146.7	25.9	209	205.8	36.3	269	264.9	46.7
30	29°5	5.2	90	88.6	15.6	150	147.7	26.0	210	206.8	36.5	270	265.9	46.9
31	30°5	5.4	91	89.6	15.8	151	148.7	26.2	211	207.8	36.6	271	266.9	47.1
32	31°5	5.6	92	90.6	16.0	152	149.7	26.4	212	208.8	36.8	272	267.9	47.2
33	32°5	5.7	93	91.6	16.1	153	150.7	26.6	213	209.8	37.0	273	268.9	47.4
34	33°5	5.9	94	92.6	16.3	154	151.7	26.7	214	210.7	37.2	274	269.8	47.6
35	34°5	6.1	95	93.6	16.5	155	152.6	26.9	215	211.7	37.3	275	270.8	47.8
36	35°5	6.3	96	94.5	16.7	156	153.6	27.1	216	212.7	37.5	276	271.8	47.9
37	36°4	6.4	97	95.5	16.8	157	154.6	27.3	217	213.7	37.7	277	272.8	48.1
38	37°4	6.6	98	96.5	17.0	158	155.6	27.4	218	214.7	37.9	278	273.8	48.3
39	38°4	6.8	99	97.5	17.2	159	156.6	27.6	219	215.7	38.0	279	274.8	48.4
40	39°4	6.9	100	98.5	17.4	160	157.6	27.8	220	216.7	38.2	280	275.7	48.6
41	40°4	7.1	101	99.5	17.5	161	158.6	28.0	221	217.6	38.4	281	276.7	48.8
42	41°4	7.3	102	100.5	17.7	162	159.5	28.1	222	218.6	38.5	282	277.7	49.0
43	42°3	7.5	103	101.4	17.9	163	160.5	28.3	223	219.6	38.7	283	278.7	49.1
44	43°3	7.6	104	102.4	18.1	164	161.5	28.5	224	220.6	38.9	284	279.7	49.3
45	44°3	7.8	105	103.4	18.2	165	162.5	28.7	225	221.6	39.1	285	280.7	49.5
46	45°3	8.0	106	104.4	18.4	166	163.5	28.8	226	222.6	39.2	286	281.7	49.7
47	46°3	8.2	107	105.4	18.6	167	164.5	29.0	227	223.6	39.4	287	282.6	49.8
48	47°3	8.3	108	106.4	18.8	168	165.4	29.2	228	224.5	39.6	288	283.6	50.0
49	48°3	8.5	109	107.3	18.9	169	166.4	29.3	229	225.5	39.8	289	284.6	50.2
50	49°2	8.7	110	108.3	19.1	170	167.4	29.5	230	226.5	39.9	290	285.6	50.4
51	50°2	8.9	111	109.3	19.3	171	168.4	29.7	231	227.5	40.1	291	286.6	50.5
52	51°2	9.0	112	110.3	19.4	172	169.4	29.9	232	228.5	40.3	292	287.6	50.7
53	52°2	9.2	113	111.3	19.6	173	170.4	30.0	233	229.5	40.5	293	288.5	50.9
54	53°2	9.4	114	112.3	19.8	174	171.4	30.2	234	230.4	40.6	294	289.5	51.1
55	54°2	9.6	115	113.3	20.0	175	172.3	30.4	235	231.4	40.8	295	290.5	51.2
56	55°1	9.7	116	114.2	20.1	176	173.3	30.6	236	232.4	41.0	296	291.5	51.4
57	56°1	9.9	117	115.2	20.3	177	174.3	30.7	237	233.4	41.2	297	292.5	51.6
58	57°1	10.1	118	116.2	20.5	178	175.3	30.9	238	234.4	41.3	298	293.5	51.7
59	58°1	10.2	119	117.2	20.7	179	176.3	31.1	239	235.4	41.5	299	294.5	51.9
60	59°1	10.4	120	118.2	20.8	180	177.3	31.3	240	236.4	41.7	300	295.4	52.1
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
80°									5° 20'					

TABLE 1

451

TRAVERSE TABLE TO DEGREES														
10°									0h 40m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	296.4	52.3	361	355.5	62.7	421	414.6	73.1	481	473.7	83.5	541	532.8	93.9
302	297.4	52.5	362	356.5	62.9	422	415.6	73.3	482	474.7	83.7	542	533.8	94.1
303	298.4	52.6	363	357.5	63.0	423	416.6	73.5	483	475.7	83.9	543	534.8	94.3
304	299.4	52.8	364	358.5	63.2	424	417.6	73.6	484	476.6	84.1	544	535.7	94.5
305	300.4	53.0	365	359.5	63.4	425	418.5	73.8	485	477.6	84.2	545	536.7	94.6
306	301.4	53.1	366	360.4	63.6	426	419.5	74.0	486	478.6	84.4	546	537.7	94.8
307	302.3	53.3	367	361.4	63.7	427	420.5	74.2	487	479.6	84.6	547	538.7	95.0
308	303.3	53.5	368	362.4	63.9	428	421.5	74.3	488	480.6	84.7	548	539.7	95.1
309	304.3	53.7	369	363.4	64.1	429	422.5	74.5	489	481.6	84.9	549	540.7	95.3
310	305.3	53.8	370	364.4	64.3	430	423.5	74.7	490	482.6	85.1	550	541.6	95.5
311	306.3	54.0	371	365.4	64.4	431	424.5	74.9	491	483.5	85.2	551	542.6	95.6
312	307.3	54.2	372	366.4	64.6	432	425.4	75.0	492	484.5	85.4	552	543.6	95.8
313	308.2	54.3	373	367.3	64.8	433	426.4	75.2	493	485.5	85.6	553	544.6	96.0
314	309.2	54.5	374	368.3	65.0	434	427.4	75.4	494	486.5	85.8	554	545.6	96.2
315	310.2	54.7	375	369.3	65.1	435	428.4	75.5	495	487.5	85.9	555	546.6	96.3
316	311.2	54.9	376	370.3	65.3	436	429.4	75.7	496	488.5	86.1	556	547.5	96.5
317	312.2	55.1	377	371.3	65.5	437	430.4	75.9	497	489.4	86.3	557	548.5	96.7
318	313.2	55.2	378	372.3	65.6	438	431.3	76.1	498	490.4	86.5	558	549.5	96.9
319	314.2	55.4	379	373.2	65.8	439	432.3	76.2	499	491.4	86.6	559	550.5	97.0
320	315.1	55.6	380	374.2	66.0	440	433.3	76.4	500	492.4	86.8	560	551.5	97.2
321	316.1	55.8	381	375.2	66.2	441	434.3	76.6	501	493.4	87.0	561	552.5	97.4
322	317.1	55.9	382	376.2	66.3	442	435.3	76.8	502	494.4	87.2	562	553.5	97.6
323	318.1	56.1	383	377.2	66.5	443	436.3	76.9	503	495.3	87.3	563	554.4	97.7
324	319.1	56.3	384	378.2	66.7	444	437.3	77.1	504	496.3	87.5	564	555.4	97.9
325	320.1	56.4	385	379.2	66.9	445	438.2	77.3	505	497.3	87.7	565	556.4	98.1
326	321.0	56.6	386	380.1	67.0	446	439.2	77.5	506	498.3	87.9	566	557.4	98.3
327	322.0	56.8	387	381.1	67.2	447	440.2	77.6	507	499.3	88.0	567	558.4	98.4
328	323.0	57.0	388	382.1	67.4	448	441.2	77.8	508	500.3	88.2	568	559.4	98.6
329	324.0	57.1	389	383.1	67.6	449	442.2	78.0	509	501.3	88.4	569	560.3	98.8
330	325.0	57.3	390	384.1	67.7	450	443.2	78.2	510	502.2	88.6	570	561.3	99.0
331	326.0	57.5	391	385.1	67.9	451	444.2	78.3	511	503.2	88.7	571	562.3	99.1
332	327.0	57.7	392	386.0	68.1	452	445.1	78.5	512	504.2	88.9	572	563.3	99.3
333	327.9	57.8	393	387.0	68.2	453	446.1	78.7	513	505.2	89.1	573	564.3	99.5
334	328.9	58.0	394	388.0	68.4	454	447.1	78.8	514	506.2	89.2	574	565.3	99.6
335	329.9	58.2	395	389.0	68.6	455	448.1	79.0	515	507.2	89.4	575	566.3	99.8
336	330.9	58.4	396	390.0	68.8	456	449.1	79.2	516	508.2	89.6	576	567.2	100.0
337	331.9	58.5	397	391.0	68.9	457	450.1	79.4	517	509.1	89.8	577	568.2	100.2
338	332.9	58.7	398	392.0	69.1	458	451.0	79.5	518	510.1	89.9	578	569.2	100.3
339	333.9	58.9	399	392.9	69.3	459	452.0	79.7	519	511.1	90.1	579	570.2	100.5
340	334.8	59.1	400	393.9	69.5	460	453.0	79.9	520	512.1	90.3	580	571.2	100.7
341	335.8	59.2	401	394.9	69.6	461	454.0	80.1	521	513.1	90.5	581	572.2	100.9
342	336.8	59.4	402	395.9	69.8	462	455.0	80.2	522	514.1	90.6	582	573.2	101.0
343	337.8	59.6	403	396.9	70.0	463	456.0	80.4	523	515.1	90.8	583	574.1	101.2
344	338.8	59.8	404	397.9	70.2	464	457.0	80.6	524	516.0	91.0	584	575.1	101.4
345	339.8	59.9	405	398.9	70.3	465	457.9	80.8	525	517.0	91.2	585	576.1	101.6
346	340.7	60.1	406	399.8	70.5	466	458.9	80.9	526	518.0	91.3	586	577.1	101.7
347	341.7	60.3	407	400.8	70.7	467	459.9	81.1	527	519.0	91.5	587	578.1	101.9
348	342.7	60.4	408	401.8	70.9	468	460.9	81.3	528	520.0	91.7	588	579.1	102.1
349	343.7	60.6	409	402.8	71.0	469	461.9	81.5	529	521.0	91.9	589	580.0	102.3
350	344.7	60.8	410	403.8	71.2	470	462.9	81.6	530	521.9	92.0	590	581.0	102.4
351	345.7	61.0	411	404.8	71.4	471	463.8	81.8	531	522.9	92.2	591	582.0	102.6
352	346.7	61.1	412	405.7	71.6	472	464.8	82.0	532	523.9	92.4	592	583.0	102.8
353	347.6	61.3	413	406.7	71.7	473	465.8	82.1	533	524.9	92.5	593	584.0	102.9
354	348.6	61.5	414	407.7	71.9	474	466.8	82.3	534	525.9	92.7	594	585.0	103.1
355	349.6	61.7	415	408.7	72.1	475	467.8	82.5	535	526.9	92.9	595	586.0	103.3
356	350.6	61.8	416	409.7	72.2	476	468.8	82.7	536	527.9	93.1	596	586.9	103.5
357	351.6	62.0	417	410.7	72.4	477	469.8	82.8	537	528.8	93.2	597	587.9	103.6
358	352.6	62.2	418	411.7	72.6	478	470.7	83.0	538	529.8	93.4	598	588.9	103.8
359	353.5	62.4	419	412.6	72.8	479	471.7	83.2	539	530.8	93.6	599	589.9	104.0
360	354.5	62.5	420	413.6	72.9	480	472.7	83.4	540	531.8	93.8	600	590.9	104.2
80°									5h 20m					
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TRAVERSE TABLE TO DEGREES														
11°										0° 44'				
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	1°0	0°2	61	59°9	11°6	121	118°8	23°1	181	177°7	34°5	241	236°6	46°0
2	2°0	0°4	62	60°9	11°8	122	119°8	23°3	182	178°7	34°7	242	237°6	46°2
3	3°0	0°6	63	61°8	12°0	123	120°7	23°5	183	179°6	34°9	243	238°5	46°4
4	3°9	0°8	64	62°8	12°2	124	121°7	23°7	184	180°6	35°1	244	239°5	46°6
5	4°9	1°0	65	63°8	12°4	125	122°7	23°9	185	181°6	35°3	245	240°5	46°7
6	5°9	1°1	66	64°8	12°6	126	123°7	24°0	186	182°6	35°5	246	241°5	46°9
7	6°9	1°3	67	65°8	12°8	127	124°7	24°2	187	183°6	35°7	247	242°5	47°1
8	7°9	1°5	68	66°8	13°0	128	125°6	24°4	188	184°5	35°9	248	243°4	47°3
9	8°8	1°7	69	67°7	13°2	129	126°6	24°6	189	185°5	36°1	249	244°4	47°5
10	9°8	1°9	70	68°7	13°4	130	127°6	24°8	190	186°5	36°3	250	245°4	47°7
11	10°8	2°1	71	69°7	13°5	131	128°6	25°0	191	187°5	36°4	251	246°4	47°9
12	11°8	2°3	72	70°7	13°7	132	129°6	25°2	192	188°5	36°6	252	247°4	48°1
13	12°8	2°5	73	71°7	13°9	133	130°6	25°4	193	189°5	36°8	253	248°4	48°3
14	13°7	2°7	74	72°6	14°1	134	131°5	25°6	194	190°4	37°0	254	249°3	48°5
15	14°7	2°9	75	73°6	14°3	135	132°5	25°8	195	191°4	37°2	255	250°3	48°7
16	15°7	3°1	76	74°6	14°5	136	133°5	26°0	196	192°4	37°4	256	251°3	48°8
17	16°7	3°2	77	75°6	14°7	137	134°5	26°1	197	193°4	37°6	257	252°3	49°0
18	17°7	3°4	78	76°6	14°9	138	135°5	26°3	198	194°4	37°8	258	253°3	49°2
19	18°7	3°6	79	77°5	15°1	139	136°4	26°5	199	195°3	38°0	259	254°2	49°4
20	19°6	3°8	80	78°5	15°3	140	137°4	26°7	200	196°3	38°2	260	255°2	49°6
21	20°6	4°0	81	79°5	15°5	141	138°4	26°9	201	197°3	38°4	261	256°2	49°8
22	21°6	4°2	82	80°5	15°6	142	139°4	27°1	202	198°3	38°5	262	257°2	50°0
23	22°6	4°4	83	81°5	15°8	143	140°4	27°3	203	199°3	38°7	263	258°2	50°2
24	23°6	4°6	84	82°5	16°0	144	141°4	27°5	204	200°3	38°9	264	259°1	50°4
25	24°5	4°8	85	83°4	16°2	145	142°3	27°7	205	201°2	39°1	265	260°1	50°6
26	25°5	5°0	86	84°4	16°4	146	143°3	27°9	206	202°2	39°3	266	261°1	50°8
27	26°5	5°2	87	85°4	16°6	147	144°3	28°0	207	203°2	39°5	267	262°1	50°9
28	27°5	5°3	88	86°4	16°8	148	145°3	28°2	208	204°2	39°7	268	263°1	51°1
29	28°5	5°5	89	87°4	17°0	149	146°3	28°4	209	205°2	39°9	269	264°1	51°3
30	29°4	5°7	90	88°3	17°2	150	147°2	28°6	210	206°1	40°1	270	265°0	51°5
31	30°4	5°9	91	89°3	17°4	151	148°2	28°8	211	207°1	40°3	271	266°0	51°7
32	31°4	6°1	92	90°3	17°6	152	149°2	29°0	212	208°1	40°5	272	267°0	51°9
33	32°4	6°3	93	91°3	17°7	153	150°2	29°2	213	209°1	40°6	273	268°0	52°1
34	33°4	6°5	94	92°3	17°9	154	151°2	29°4	214	210°1	40°8	274	269°0	52°3
35	34°4	6°7	95	93°3	18°1	155	152°2	29°6	215	211°0	41°0	275	269°9	52°5
36	35°3	6°9	96	94°2	18°3	156	153°1	29°8	216	212°0	41°2	276	270°9	52°7
37	36°3	7°1	97	95°2	18°5	157	154°1	30°0	217	213°0	41°4	277	271°9	52°9
38	37°3	7°3	98	96°2	18°7	158	155°1	30°1	218	214°0	41°6	278	272°9	53°0
39	38°3	7°4	99	97°2	18°9	159	156°1	30°3	219	215°0	41°8	279	273°9	53°2
40	39°3	7°6	100	98°2	19°1	160	157°1	30°5	220	216°0	42°0	280	274°9	53°4
41	40°2	7°8	101	99°1	19°3	161	158°0	30°7	221	216°9	42°2	281	275°8	53°6
42	41°2	8°0	102	100°1	19°5	162	159°0	30°9	222	217°9	42°4	282	276°8	53°8
43	42°2	8°2	103	101°1	19°7	163	160°0	31°1	223	218°9	42°6	283	277°8	54°0
44	43°2	8°4	104	102°1	19°8	164	161°0	31°3	224	219°9	42°7	284	278°8	54°2
45	44°2	8°6	105	103°1	20°0	165	162°0	31°5	225	220°9	42°9	285	279°8	54°4
46	45°2	8°8	106	104°1	20°2	166	163°0	31°7	226	221°8	43°1	286	280°7	54°6
47	46°1	9°0	107	105°0	20°4	167	163°9	31°9	227	222°8	43°3	287	281°7	54°8
48	47°1	9°2	108	106°0	20°6	168	164°9	32°1	228	223°8	43°5	288	282°7	55°0
49	48°1	9°3	109	107°0	20°8	169	165°9	32°2	229	224°8	43°7	289	283°7	55°1
50	49°1	9°5	110	108°0	21°0	170	166°9	32°4	230	225°8	43°9	290	284°7	55°3
51	50°1	9°7	111	109°0	21°2	171	167°9	32°6	231	226°8	44°1	291	285°7	55°5
52	51°0	9°9	112	109°9	21°4	172	168°8	32°8	232	227°7	44°3	292	286°6	55°7
53	52°0	10°1	113	110°9	21°6	173	169°8	33°0	233	228°7	44°5	293	287°6	55°9
54	53°0	10°3	114	111°9	21°8	174	170°8	33°2	234	229°7	44°6	294	288°6	56°1
55	54°0	10°5	115	112°9	21°9	175	171°8	33°4	235	230°7	44°8	295	289°6	56°3
56	55°0	10°7	116	113°9	22°1	176	172°8	33°6	236	231°7	44°8	296	290°6	56°5
57	56°0	10°9	117	114°9	22°3	177	173°7	33°8	237	232°6	45°2	297	291°5	56°7
58	56°9	11°1	118	115°8	22°5	178	174°7	34°0	238	233°6	45°4	298	292°5	56°9
59	57°9	11°3	119	116°8	22°7	179	175°7	34°2	239	234°6	45°6	299	293°5	57°1
60	58°9	11°4	120	117°8	22°9	180	176°7	34°3	240	235°6	45°8	300	294°5	57°2
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
79°										5° 16'				

TABLE 1

453

TRAVERSE TABLE TO DEGREES

11°									0h 44m						
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	
301	295.4	57.4	361	354.3	68.9	421	413.2	80.3	481	472.1	91.8	541	531.0	103.2	
302	296.4	57.6	362	355.3	69.1	422	414.2	80.5	482	473.1	92.0	542	532.0	103.4	
303	297.4	57.8	363	356.3	69.3	423	415.2	80.7	483	474.1	92.2	543	533.0	103.6	
304	298.4	58.0	364	357.3	69.5	424	416.2	80.9	484	475.1	92.4	544	534.0	103.8	
305	299.4	58.2	365	358.3	69.6	425	417.2	81.1	485	476.1	92.6	545	535.0	104.0	
306	300.3	58.4	366	359.2	69.8	426	418.1	81.3	486	477.0	92.8	546	535.9	104.2	
307	301.3	58.6	367	360.2	70.0	427	419.1	81.5	487	478.0	93.0	547	536.9	104.4	
308	302.3	58.8	368	361.2	70.2	428	420.1	81.7	488	479.0	93.2	548	537.9	104.6	
309	303.3	59.0	369	362.2	70.4	429	421.1	81.9	489	480.0	93.3	549	538.9	104.8	
310	304.3	59.2	370	363.2	70.6	430	422.1	82.1	490	481.0	93.5	550	539.9	105.0	
311	305.3	59.3	371	364.1	70.8	431	423.0	82.2	491	481.9	93.6	551	540.8	105.1	
312	306.2	59.5	372	365.1	71.0	432	424.0	82.4	492	482.9	93.8	552	541.8	105.3	
313	307.2	59.7	373	366.1	71.2	433	425.0	82.6	493	483.9	94.0	553	542.8	105.5	
314	308.2	59.9	374	367.1	71.4	434	426.0	82.8	494	484.9	94.2	554	543.8	105.7	
315	309.2	60.1	375	368.1	71.6	435	427.0	83.0	495	485.9	94.4	555	544.8	105.9	
316	310.2	60.3	376	369.1	71.7	436	428.0	83.2	496	486.9	94.6	556	545.8	106.1	
317	311.1	60.5	377	370.0	71.9	437	428.9	83.4	497	487.8	94.8	557	546.7	106.3	
318	312.1	60.7	378	371.0	72.1	438	429.9	83.6	498	488.8	95.0	558	547.7	106.5	
319	313.1	60.9	379	372.0	72.3	439	430.9	83.8	499	489.8	95.2	559	548.7	106.7	
320	314.1	61.1	380	373.0	72.5	440	431.9	84.0	500	490.8	95.4	560	549.7	106.9	
321	315.1	61.3	381	374.0	72.7	441	432.9	84.1	501	491.8	95.6	561	550.7	107.1	
322	316.1	61.4	382	374.9	72.9	442	433.8	84.3	502	492.7	95.8	562	551.6	107.2	
323	317.0	61.6	383	375.9	73.1	443	434.8	84.5	503	493.7	96.0	563	552.6	107.4	
324	318.0	61.8	384	376.9	73.3	444	435.8	84.7	504	494.7	96.2	564	553.6	107.6	
325	319.0	62.0	385	377.9	73.5	445	436.8	84.9	505	495.7	96.4	565	554.6	107.8	
326	320.0	62.2	386	378.9	73.7	446	437.8	85.1	506	496.7	96.6	566	555.6	108.0	
327	321.0	62.4	387	379.9	73.8	447	438.8	85.3	507	497.7	96.8	567	556.6	108.2	
328	321.9	62.6	388	380.8	74.0	448	439.7	85.5	508	498.6	97.0	568	557.6	108.4	
329	322.9	62.8	389	381.8	74.2	449	440.7	85.7	509	499.6	97.2	569	558.6	108.6	
330	323.9	63.0	390	382.8	74.4	450	441.7	85.9	510	500.6	97.3	570	559.5	108.8	
331	324.9	63.2	391	383.8	74.6	451	442.7	86.1	511	501.6	97.5	571	560.5	109.0	
332	325.9	63.4	392	384.8	74.8	452	443.7	86.2	512	502.6	97.6	572	561.5	109.1	
333	326.8	63.5	393	385.7	75.0	453	444.6	86.4	513	503.5	97.8	573	562.5	109.3	
334	327.8	63.7	394	386.7	75.2	454	445.6	86.6	514	504.5	98.0	574	563.5	109.5	
335	328.8	63.9	395	387.7	75.4	455	446.6	86.8	515	505.5	98.2	575	564.5	109.7	
336	329.8	64.1	396	388.7	75.6	456	447.6	87.0	516	506.5	98.4	576	565.4	109.9	
337	330.8	64.3	397	389.7	75.8	457	448.6	87.2	517	507.5	98.6	577	566.4	110.1	
338	331.8	64.5	398	390.7	75.9	458	449.6	87.4	518	508.5	98.8	578	567.4	110.3	
339	332.7	64.7	399	391.6	76.1	459	450.5	87.6	519	509.4	99.0	579	568.3	110.5	
340	333.7	64.9	400	392.6	76.3	460	451.5	87.8	520	510.4	99.2	580	569.3	110.7	
341	334.7	65.1	401	393.6	76.5	461	452.5	88.0	521	511.4	99.4	581	570.3	110.9	
342	335.7	65.3	402	394.6	76.7	462	453.5	88.2	522	512.4	99.6	582	571.3	111.1	
343	336.7	65.5	403	395.6	76.9	463	454.5	88.3	523	513.4	99.8	583	572.3	111.3	
344	337.6	65.6	404	396.5	77.1	464	455.4	88.5	524	514.3	100.0	584	573.2	111.5	
345	338.6	65.8	405	397.5	77.3	465	456.4	88.7	525	515.3	100.2	585	574.2	111.7	
346	339.6	66.0	406	398.5	77.5	466	457.4	88.9	526	516.3	100.4	586	575.2	111.8	
347	340.6	66.2	407	399.5	77.7	467	458.4	89.1	527	517.3	100.6	587	576.2	112.1	
348	341.6	66.4	408	400.5	77.9	468	459.4	89.3	528	518.3	100.8	588	577.2	112.3	
349	342.6	66.6	409	401.5	78.1	469	460.4	89.5	529	519.3	101.0	589	578.2	112.4	
350	343.5	66.8	410	402.4	78.2	470	461.3	89.7	530	520.2	101.2	590	579.1	112.6	
351	344.5	67.0	411	403.4	78.4	471	462.3	89.9	531	521.2	101.4	591	580.1	112.8	
352	345.5	67.2	412	404.4	78.6	472	463.3	90.1	532	522.2	101.6	592	581.1	113.0	
353	346.5	67.4	413	405.4	78.8	473	464.3	90.3	533	523.2	101.7	593	582.1	113.2	
354	347.5	67.5	414	406.4	79.0	474	465.3	90.4	534	524.2	101.8	594	583.1	113.3	
355	348.4	67.7	415	407.3	79.2	475	466.2	90.6	535	525.1	102.0	595	584.0	113.5	
356	349.4	67.9	416	408.3	79.4	476	467.2	90.8	536	526.1	102.2	596	585.0	113.7	
357	350.4	68.1	417	409.3	79.6	477	468.2	91.0	537	527.1	102.4	597	586.0	113.9	
358	351.4	68.3	418	410.3	79.8	478	469.2	91.2	538	528.1	102.6	598	587.0	114.1	
359	352.4	68.5	419	411.3	80.0	479	470.2	91.4	539	529.1	102.8	599	588.0	114.3	
360	353.4	68.7	420	412.3	80.1	480	471.1	91.6	540	530.1	103.0	600	589.0	114.5	
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	

79°

5h 16m

TABLE 1

TRAVERSE TABLE TO DEGREES														
12°										0° 48'				
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	1°0	0'2	61	59'7	12'7	121	118'4	25'2	181	177'0	37'6	241	235'7	50'1
2	2°0	0'4	62	60'6	12'9	122	119'3	25'4	182	178'0	37'8	242	236'7	50'3
3	2°9	0'6	63	61'6	13'1	123	120'3	25'6	183	179'0	38'0	243	237'7	50'5
4	3°9	0'8	64	62'6	13'3	124	121'3	25'8	184	180'0	38'3	244	238'7	50'7
5	4°9	1'0	65	63'6	13'5	125	122'3	26'0	185	181'0	38'5	245	239'6	50'9
6	5°9	1'2	66	64'6	13'7	126	123'2	26'2	186	181'9	38'7	246	240'6	51'1
7	6°8	1'5	67	65'5	13'9	127	124'2	26'4	187	182'9	38'9	247	241'6	51'4
8	7°8	1'7	68	66'5	14'2	128	125'2	26'6	188	183'9	39'1	248	242'6	51'6
9	8°8	1'9	69	67'5	14'3	129	126'2	26'8	189	184'9	39'3	249	243'6	51'8
10	9°8	2'1	70	68'5	14'6	130	127'2	27'0	190	185'8	39'5	250	244'5	52'0
11	10°8	2'3	71	69'4	14'8	131	128'1	27'2	191	186'8	39'7	251	245'5	52'2
12	11°7	2'5	72	70'4	15'0	132	129'1	27'4	192	187'8	39'9	252	246'5	52'4
13	12°7	2'7	73	71'4	15'2	133	130'1	27'7	193	188'8	40'1	253	247'5	52'6
14	13°7	2'9	74	72'4	15'4	134	131'1	27'9	194	189'8	40'3	254	248'4	52'8
15	14°7	3'1	75	73'4	15'6	135	132'0	28'1	195	190'7	40'5	255	249'4	53'0
16	15°7	3'3	76	74'3	15'8	136	133'0	28'3	196	191'7	40'8	256	250'4	53'2
17	16°6	3'5	77	75'3	16'0	137	134'0	28'5	197	192'7	41'0	257	251'4	53'4
18	17°6	3'7	78	76'3	16'2	138	135'0	28'7	198	193'7	41'2	258	252'4	53'6
19	18°6	4'0	79	77'3	16'4	139	136'0	28'9	199	194'7	41'4	259	253'3	53'8
20	19°6	4'2	80	78'3	16'6	140	136'9	29'1	200	195'6	41'6	260	254'3	54'1
21	20°5	4'4	81	79'2	16'8	141	137'9	29'3	201	196'6	41'8	261	255'3	54'3
22	21°5	4'6	82	80'2	17'0	142	138'9	29'5	202	197'6	42'0	262	256'3	54'5
23	22°5	4'8	83	81'2	17'3	143	139'9	29'7	203	198'6	42'2	263	257'3	54'7
24	23°5	5'0	84	82'2	17'5	144	140'9	29'9	204	199'5	42'4	264	258'2	54'9
25	24°5	5'2	85	83'1	17'7	145	141'8	30'1	205	200'5	42'6	265	259'2	55'1
26	25°4	5'5	86	84'1	17'9	146	142'8	30'4	206	201'5	42'8	266	260'2	55'3
27	26°4	5'6	87	85'1	18'1	147	143'8	30'6	207	202'5	43'0	267	261'2	55'5
28	27°4	5'8	88	86'1	18'3	148	144'8	30'8	208	203'5	43'2	268	262'1	55'7
29	28°4	6'0	89	87'1	18'5	149	145'7	31'0	209	204'4	43'5	269	263'1	55'9
30	29°3	6'2	90	88'0	18'7	150	146'7	31'2	210	205'4	43'7	270	264'1	56'1
31	30°3	6'4	91	89'0	18'9	151	147'7	31'4	211	206'4	43'9	271	265'1	56'3
32	31°3	6'7	92	90'0	19'1	152	148'7	31'6	212	207'4	44'1	272	266'1	56'6
33	32°3	6'9	93	91'0	19'3	153	149'7	31'8	213	208'3	44'3	273	267'0	56'8
34	33°3	7'1	94	91'9	19'5	154	150'6	32'0	214	209'3	44'5	274	268'0	57'0
35	34°2	7'3	95	92'9	19'8	155	151'6	32'2	215	210'3	44'7	275	269'0	57'2
36	35°2	7'5	96	93'9	20'0	156	152'6	32'4	216	211'3	44'9	276	270'0	57'4
37	36°2	7'7	97	94'9	20'2	157	153'6	32'6	217	212'3	45'1	277	270'9	57'6
38	37°2	7'9	98	95'9	20'4	158	154'5	32'9	218	213'2	45'3	278	271'9	57'8
39	38°1	8'1	99	96'8	20'6	159	155'5	33'1	219	214'2	45'5	279	272'9	58'0
40	39°1	8'3	100	97'8	20'8	160	156'5	33'3	220	215'2	45'7	280	273'9	58'2
41	40°1	8'5	101	98'8	21'0	161	157'5	33'5	221	216'2	45'9	281	274'9	58'4
42	41°1	8'7	102	99'8	21'2	162	158'5	33'7	222	217'1	46'2	282	275'8	58'6
43	42°1	8'9	103	100'7	21'4	163	159'4	33'9	223	218'1	46'4	283	276'8	58'8
44	43°0	9'1	104	101'7	21'6	164	160'4	34'1	224	219'1	46'6	284	277'8	59'0
45	44°0	9'4	105	102'7	21'8	165	161'4	34'3	225	220'1	46'8	285	278'8	59'3
46	45°0	9'6	106	103'7	22'0	166	162'4	34'5	226	221'1	47'0	286	279'8	59'5
47	46°0	9'8	107	104'7	22'2	167	163'4	34'7	227	222'0	47'2	287	280'7	59'7
48	47°0	10'0	108	105'6	22'5	168	164'3	34'9	228	223'0	47'4	288	281'7	59'9
49	47°9	10'2	109	106'6	22'7	169	165'3	35'1	229	224'0	47'6	289	282'7	60'1
50	48°9	10'4	110	107'6	22'9	170	166'3	35'3	230	225'0	47'8	290	283'7	60'3
51	49°9	10'6	111	108'6	23'1	171	167'3	35'6	231	226'0	48'0	291	284'6	60'5
52	50°9	10'8	112	109'6	23'3	172	168'2	35'8	232	226'9	48'2	292	285'6	60'7
53	51°8	11'0	113	110'5	23'5	173	169'2	36'0	233	227'9	48'4	293	286'6	60'9
54	52°8	11'2	114	111'5	23'7	174	170'2	36'2	234	228'9	48'7	294	287'6	61'1
55	53°8	11'4	115	112'5	23'9	175	171'2	36'4	235	229'9	48'9	295	288'6	61'3
56	54°8	11'6	116	113'5	24'1	176	172'2	36'6	236	230'8	49'1	296	289'5	61'5
57	55°8	11'9	117	114'4	24'3	177	173'1	36'8	237	231'8	49'3	297	290'5	61'7
58	56°7	12'1	118	115'4	24'5	178	174'1	37'0	238	232'8	49'5	298	291'5	62'0
59	57°7	12'3	119	116'4	24'7	179	175'1	37'2	239	233'8	49'7	299	292'5	62'2
60	58°7	12'5	120	117'4	24'9	180	176'1	37'4	240	234'8	49'9	300	293'4	62'4
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

78°

5h 12m

TABLE 1

455

TRAVERSE TABLE TO DEGREES														
12°									0h 48m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	294.4	62.6	361	353.1	75.0	421	411.8	87.5	481	470.5	100.0	541	529.2	112.5
302	295.4	62.8	362	354.1	75.2	422	412.8	87.7	482	471.5	100.2	542	530.2	112.7
303	296.4	63.0	363	355.1	75.4	423	413.8	87.9	483	472.5	100.4	543	531.1	112.9
304	297.4	63.2	364	356.0	75.7	424	414.7	88.1	484	473.4	100.6	544	532.1	113.1
305	298.3	63.4	365	357.0	75.9	425	415.7	88.3	485	474.4	100.8	545	533.1	113.3
306	299.3	63.6	366	358.0	76.1	426	416.7	88.6	486	475.4	101.0	546	534.1	113.5
307	300.3	63.8	367	359.0	76.3	427	417.7	88.8	487	476.4	101.2	547	535.1	113.7
308	301.3	64.0	368	360.0	76.5	428	418.6	89.0	488	477.3	101.4	548	536.0	113.9
309	302.2	64.2	369	360.9	76.7	429	419.6	89.2	489	478.3	101.6	549	537.0	114.1
310	303.2	64.4	370	361.9	76.9	430	420.6	89.4	490	479.3	101.9	550	538.0	114.4
311	304.2	64.6	371	362.9	77.1	431	421.6	89.6	491	480.3	102.1	551	538.9	114.6
312	305.2	64.8	372	363.9	77.3	432	422.6	89.8	492	481.2	102.3	552	539.9	114.8
313	306.2	65.1	373	364.8	77.5	433	423.5	90.0	493	482.2	102.5	553	540.9	115.0
314	307.1	65.3	374	365.8	77.7	434	424.5	90.2	494	483.2	102.7	554	541.9	115.2
315	308.1	65.5	375	366.8	77.9	435	425.5	90.4	495	484.2	102.9	555	542.9	115.4
316	309.1	65.7	376	367.8	78.2	436	426.5	90.6	496	485.2	103.1	556	543.8	115.6
317	310.1	65.9	377	368.8	78.4	437	427.5	90.8	497	486.1	103.3	557	544.8	115.8
318	311.1	66.1	378	369.7	78.6	438	428.4	91.0	498	487.1	103.5	558	545.8	116.0
319	312.0	66.3	379	370.7	78.8	439	429.4	91.3	499	488.1	103.8	559	546.8	116.2
320	313.0	66.5	380	371.7	79.0	440	430.4	91.5	500	489.1	104.0	560	547.8	116.4
321	314.0	66.7	381	372.7	79.2	441	431.4	91.7	501	490.0	104.2	561	548.7	116.6
322	315.0	66.9	382	373.7	79.4	442	432.3	91.9	502	491.0	104.4	562	549.7	116.8
323	315.9	67.1	383	374.6	79.6	443	433.3	92.1	503	492.0	104.6	563	550.7	117.0
324	316.9	67.3	384	375.6	79.8	444	434.3	92.3	504	493.0	104.8	564	551.7	117.2
325	317.9	67.5	385	376.6	80.0	445	435.3	92.5	505	494.0	105.0	565	552.7	117.4
326	318.9	67.8	386	377.6	80.2	446	436.3	92.7	506	495.0	105.2	566	553.7	117.6
327	319.9	68.0	387	378.5	80.4	447	437.2	92.9	507	495.9	105.4	567	554.6	117.8
328	320.8	68.2	388	379.5	80.7	448	438.2	93.1	508	496.9	105.6	568	555.6	118.0
329	321.8	68.4	389	380.5	80.9	449	439.2	93.3	509	497.9	105.8	569	556.6	118.2
330	322.8	68.6	390	381.5	81.1	450	440.2	93.5	510	498.9	106.0	570	557.5	118.5
331	323.8	68.8	391	382.5	81.3	451	441.1	93.7	511	499.8	106.2	571	558.5	118.7
332	324.7	69.0	392	383.4	81.5	452	442.1	93.9	512	500.8	106.4	572	559.5	118.9
333	325.7	69.2	393	384.4	81.7	453	443.1	94.1	513	501.8	106.6	573	560.5	119.1
334	326.7	69.4	394	385.4	81.9	454	444.1	94.4	514	502.8	106.8	574	561.5	119.3
335	327.7	69.6	395	386.4	82.1	455	445.1	94.6	515	503.7	107.0	575	562.4	119.5
336	328.7	69.8	396	387.3	82.3	456	446.0	94.8	516	504.7	107.2	576	563.4	119.7
337	329.6	70.0	397	388.3	82.5	457	447.0	95.0	517	505.7	107.4	577	564.4	119.9
338	330.6	70.3	398	389.3	82.7	458	448.0	95.2	518	506.7	107.6	578	565.4	120.1
339	331.6	70.5	399	390.3	82.9	459	449.0	95.4	519	507.7	107.8	579	566.4	120.3
340	332.6	70.7	400	391.3	83.1	460	450.0	95.6	520	508.7	108.1	580	567.4	120.6
341	333.5	70.9	401	392.2	83.4	461	450.9	95.8	521	509.6	108.3	581	568.3	120.8
342	334.5	71.1	402	393.2	83.6	462	451.9	96.0	522	510.6	108.5	582	569.3	121.0
343	335.5	71.3	403	394.2	83.8	463	452.9	96.2	523	511.6	108.7	583	570.3	121.2
344	336.5	71.5	404	395.2	84.0	464	453.9	96.5	524	512.5	108.9	584	571.2	121.4
345	337.5	71.7	405	396.2	84.2	465	454.8	96.7	525	513.5	109.2	585	572.2	121.6
346	338.4	71.9	406	397.1	84.4	466	455.8	96.9	526	514.5	109.4	586	573.2	121.8
347	339.4	72.1	407	398.1	84.6	467	456.8	97.1	527	515.5	109.6	587	574.2	122.0
348	340.4	72.3	408	399.1	84.8	468	457.8	97.3	528	516.5	109.8	588	575.2	122.2
349	341.4	72.5	409	400.1	85.0	469	458.8	97.5	529	517.5	110.0	589	576.2	122.4
350	342.4	72.7	410	401.0	85.2	470	459.7	97.7	530	518.4	110.2	590	577.1	122.6
351	343.3	73.0	411	402.0	85.4	471	460.7	97.9	531	519.4	110.4	591	578.1	122.8
352	344.3	73.2	412	403.0	85.6	472	461.7	98.1	532	520.4	110.6	592	579.1	123.0
353	345.3	73.4	413	404.0	85.8	473	462.7	98.3	533	521.3	110.8	593	580.0	123.2
354	346.3	73.6	414	405.0	86.1	474	463.6	98.5	534	522.3	111.0	594	581.0	123.4
355	347.2	73.8	415	405.9	86.3	475	464.6	98.7	535	523.3	111.2	595	582.0	123.6
356	348.2	74.0	416	406.9	86.5	476	465.6	98.9	536	524.3	111.4	596	583.0	123.9
357	349.2	74.2	417	407.9	86.7	477	466.6	99.1	537	525.3	111.6	597	584.0	124.1
358	350.2	74.4	418	408.9	86.9	478	467.6	99.4	538	526.2	111.8	598	584.9	124.3
359	351.2	74.6	419	409.8	87.1	479	468.5	99.6	539	527.2	112.0	599	585.9	124.5
360	352.1	74.8	420	410.8	87.3	480	469.5	99.8	540	528.2	112.3	600	586.9	124.7
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

78°

5h 12m

TRAVERSE TABLE TO DEGREES														
18°									0° 52'					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	1°0	0'2	61	59'4	13'7	121	117'9	27'2	181	176'4	40'7	241	234'8	54'2
2	1'9	0'4	62	60'4	13'9	122	118'9	27'4	182	177'3	40'9	242	235'8	54'4
3	2'9	0'7	63	61'4	14'2	123	119'8	27'7	183	178'3	41'2	243	236'8	54'7
4	3'9	0'9	64	62'4	14'4	124	120'8	27'9	184	179'3	41'4	244	237'7	54'9
5	4'9	1'1	65	63'3	14'6	125	121'8	28'1	185	180'3	41'6	245	238'7	55'1
6	5'8	1'3	66	64'3	14'8	126	122'8	28'3	186	181'2	41'8	246	239'7	55'3
7	6'8	1'6	67	65'3	15'1	127	123'7	28'6	187	182'2	42'1	247	240'7	55'6
8	7'8	1'8	68	66'3	15'3	128	124'7	28'8	188	183'2	42'3	248	241'6	55'8
9	8'8	2'0	69	67'2	15'5	129	125'7	29'0	189	184'2	42'5	249	242'6	56'0
10	9'7	2'2	70	68'2	15'7	130	126'7	29'2	190	185'1	42'7	250	243'6	56'2
11	10'7	2'5	71	69'2	16'0	131	127'6	29'5	191	186'1	43'0	251	244'6	56'5
12	11'7	2'7	72	70'2	16'2	132	128'6	29'7	192	187'1	43'2	252	245'5	56'7
13	12'7	2'9	73	71'1	16'4	133	129'6	29'9	193	188'1	43'4	253	246'5	56'9
14	13'6	3'1	74	72'1	16'6	134	130'6	30'1	194	189'2	43'6	254	247'5	57'1
15	14'6	3'4	75	73'1	16'9	135	131'5	30'4	195	190'0	43'9	255	248'5	57'4
16	15'6	3'6	76	74'1	17'1	136	132'5	30'6	196	191'0	44'1	256	249'4	57'6
17	16'6	3'8	77	75'0	17'3	137	133'5	30'8	197	192'0	44'3	257	250'4	57'8
18	17'5	4'0	78	76'0	17'5	138	134'5	31'0	198	192'9	44'5	258	251'4	58'0
19	18'5	4'3	79	77'0	17'8	139	135'4	31'3	199	193'9	44'8	259	252'4	58'3
20	19'5	4'5	80	78'0	18'0	140	136'4	31'5	200	194'9	45'0	260	253'3	58'5
21	20'5	4'7	81	78'9	18'2	141	137'4	31'7	201	195'8	45'2	261	254'3	58'7
22	21'4	4'9	82	79'9	18'4	142	138'4	31'9	202	196'8	45'4	262	255'3	58'9
23	22'4	5'2	83	80'9	18'7	143	139'3	32'2	203	197'8	45'7	263	256'3	59'2
24	23'4	5'4	84	81'8	18'9	144	140'3	32'4	204	198'8	45'9	264	257'2	59'4
25	24'4	5'6	85	82'8	19'1	145	141'3	32'6	205	199'7	46'1	265	258'2	59'6
26	25'3	5'8	86	83'8	19'3	146	142'3	32'8	206	200'7	46'3	266	259'2	59'8
27	26'3	6'1	87	84'8	19'6	147	143'2	33'1	207	201'7	46'6	267	260'2	60'1
28	27'3	6'3	88	85'7	19'8	148	144'2	33'3	208	202'7	46'8	268	261'1	60'3
29	28'3	6'5	89	86'7	20'0	149	145'2	33'5	209	203'6	47'0	269	262'1	60'5
30	29'2	6'7	90	87'7	20'2	150	146'2	33'7	210	204'6	47'2	270	263'1	60'7
31	30'2	7'0	91	88'7	20'5	151	147'1	34'0	211	205'6	47'5	271	264'1	61'0
32	31'2	7'2	92	89'6	20'7	152	148'1	34'2	212	206'6	47'7	272	265'0	61'2
33	32'2	7'4	93	90'6	20'9	153	149'1	34'4	213	207'5	47'9	273	266'0	61'4
34	33'1	7'6	94	91'6	21'1	154	150'1	34'6	214	208'5	48'1	274	267'0	61'6
35	34'1	7'9	95	92'6	21'4	155	151'0	34'9	215	209'5	48'4	275	268'0	61'9
36	35'1	8'1	96	93'5	21'6	156	152'0	35'1	216	210'5	48'6	276	268'9	62'1
37	36'1	8'3	97	94'5	21'8	157	153'0	35'3	217	211'4	48'8	277	269'9	62'3
38	37'0	8'5	98	95'5	22'0	158	154'0	35'5	218	212'4	49'0	278	270'9	62'5
39	38'0	8'8	99	96'5	22'3	159	154'9	35'8	219	213'4	49'3	279	271'8	62'8
40	39'0	9'0	100	97'4	22'5	160	155'9	36'0	220	214'4	49'5	280	272'8	63'0
41	39'9	9'2	101	98'4	22'7	161	156'9	36'2	221	215'3	49'7	281	273'8	63'2
42	40'9	9'4	102	99'4	22'9	162	157'8	36'4	222	216'3	49'9	282	274'8	63'4
43	41'9	9'7	103	100'4	23'2	163	158'8	36'7	223	217'3	50'2	283	275'7	63'7
44	42'9	9'9	104	101'3	23'4	164	159'8	36'9	224	218'3	50'4	284	276'7	63'9
45	43'8	10'1	105	102'3	23'6	165	160'8	37'1	225	219'2	50'6	285	277'7	64'1
46	44'8	10'3	106	103'3	23'8	166	161'7	37'3	226	220'2	50'8	286	278'7	64'3
47	45'8	10'6	107	104'3	24'1	167	162'7	37'6	227	221'2	51'1	287	279'6	64'6
48	46'8	10'8	108	105'2	24'3	168	163'7	37'8	228	222'2	51'3	288	280'6	64'8
49	47'7	11'0	109	106'2	24'5	169	164'7	38'0	229	223'1	51'5	289	281'6	65'0
50	48'7	11'2	110	107'2	24'7	170	165'6	38'2	230	224'1	51'7	290	282'6	65'2
51	49'7	11'5	111	108'2	25'0	171	166'6	38'5	231	225'1	52'0	291	283'5	65'5
52	50'7	11'7	112	109'1	25'2	172	167'6	38'7	232	226'1	52'2	292	284'5	65'7
53	51'6	11'9	113	110'1	25'4	173	168'6	38'9	233	227'0	52'4	293	285'5	65'9
54	52'6	12'1	114	111'1	25'6	174	169'5	39'1	234	228'0	52'6	294	286'5	66'1
55	53'6	12'4	115	112'1	25'9	175	170'5	39'4	235	229'0	52'9	295	287'4	66'4
56	54'6	12'6	116	113'0	26'1	176	171'5	39'6	236	230'0	53'1	296	288'4	66'6
57	55'5	12'8	117	114'0	26'3	177	172'5	39'8	237	230'9	53'3	297	289'4	66'8
58	56'5	13'0	118	115'0	26'5	178	173'4	40'0	238	231'9	53'5	298	290'4	67'0
59	57'5	13'3	119	116'0	26'8	179	174'4	40'3	239	232'9	53'8	299	291'3	67'3
60	58'5	13'5	120	116'9	27'0	180	175'4	40'5	240	233'8	54'0	300	292'3	67'5
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

467

TRAVERSE TABLE TO DEGREES														
18°										0 ^h 52 ^m				
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	293.3	67.7	361	351.8	81.2	421	410.2	94.7	481	468.7	108.2	541	527.2	121.7
302	294.3	67.9	362	352.7	81.4	422	411.2	94.9	482	469.7	108.4	542	528.1	121.9
303	295.2	68.1	363	353.7	81.6	423	412.2	95.1	483	470.6	108.6	543	529.1	122.1
304	296.2	68.4	364	354.7	81.9	424	413.1	95.3	484	471.6	108.8	544	530.1	122.3
305	297.2	68.6	365	355.6	82.1	425	414.1	95.6	485	472.6	109.0	545	531.1	122.5
306	298.2	68.8	366	356.6	82.3	426	415.1	95.8	486	473.6	109.3	546	532.0	122.8
307	299.1	69.0	367	357.6	82.5	427	416.1	96.0	487	474.5	109.5	547	533.0	123.0
308	300.1	69.3	368	358.6	82.8	428	417.0	96.2	488	475.5	109.7	548	534.0	123.2
309	301.1	69.5	369	359.5	83.0	429	418.0	96.5	489	476.5	109.9	549	535.0	123.4
310	302.1	69.7	370	360.5	83.2	430	419.0	96.7	490	477.5	110.1	550	535.9	123.7
311	303.0	69.9	371	361.5	83.4	431	420.0	96.9	491	478.4	110.4	551	536.9	123.9
312	304.0	70.2	372	362.5	83.7	432	420.9	97.1	492	479.4	110.6	552	537.9	124.1
313	305.0	70.4	373	363.4	83.9	433	421.9	97.4	493	480.4	110.9	553	538.9	124.4
314	306.0	70.6	374	364.4	84.1	434	422.9	97.6	494	481.4	111.1	554	539.8	124.6
315	306.9	70.8	375	365.4	84.3	435	423.9	97.8	495	482.3	111.3	555	540.8	124.9
316	307.9	71.1	376	366.4	84.6	436	424.8	98.0	496	483.3	111.5	556	541.8	125.1
317	308.9	71.3	377	367.3	84.8	437	425.8	98.3	497	484.3	111.8	557	542.8	125.3
318	309.9	71.5	378	368.3	85.0	438	426.8	98.5	498	485.3	112.0	558	543.7	125.5
319	310.8	71.7	379	369.3	85.2	439	427.8	98.7	499	486.2	112.2	559	544.7	125.8
320	311.8	72.0	380	370.3	85.5	440	428.7	98.9	500	487.2	112.4	560	545.7	126.0
321	312.8	72.2	381	371.2	85.7	441	429.7	99.2	501	488.2	112.6	561	546.7	126.2
322	313.8	72.4	382	372.2	85.9	442	430.7	99.4	502	489.2	112.9	562	547.6	126.4
323	314.7	72.6	383	373.2	86.1	443	431.6	99.6	503	490.1	113.1	563	548.6	126.7
324	315.7	72.9	384	374.2	86.4	444	432.6	99.8	504	491.1	113.3	564	549.6	126.9
325	316.7	73.1	385	375.1	86.6	445	433.6	100.1	505	492.1	113.5	565	550.6	127.1
326	317.6	73.3	386	376.1	86.8	446	434.6	100.3	506	493.1	113.8	566	551.5	127.3
327	318.6	73.5	387	377.1	87.0	447	435.5	100.5	507	494.0	114.0	567	552.5	127.6
328	319.6	73.8	388	378.1	87.3	448	436.5	100.7	508	495.0	114.2	568	553.5	127.8
329	320.6	74.0	389	379.0	87.5	449	437.5	101.0	509	496.0	114.5	569	554.5	128.0
330	321.5	74.2	390	380.0	87.7	450	438.5	101.2	510	496.9	114.7	570	555.4	128.3
331	322.5	74.4	391	381.0	87.9	451	439.4	101.4	511	497.9	114.9	571	556.4	128.5
332	323.5	74.7	392	382.0	88.2	452	440.4	101.6	512	498.9	115.1	572	557.4	128.7
333	324.5	74.9	393	382.9	88.4	453	441.4	101.9	513	499.9	115.4	573	558.4	128.9
334	325.4	75.1	394	383.9	88.6	454	442.4	102.1	514	500.8	115.6	574	559.3	129.2
335	326.4	75.3	395	384.9	88.8	455	443.3	102.3	515	501.8	115.8	575	560.3	129.4
336	327.4	75.6	396	385.9	89.1	456	444.3	102.5	516	502.8	116.0	576	561.3	129.6
337	328.4	75.8	397	386.8	89.3	457	445.3	102.8	517	503.8	116.3	577	562.3	129.8
338	329.3	76.0	398	387.8	89.5	458	446.3	103.0	518	504.7	116.5	578	563.2	130.0
339	330.3	76.2	399	388.8	89.7	459	447.2	103.2	519	505.7	116.7	579	564.2	130.2
340	331.3	76.5	400	389.8	90.0	460	448.2	103.4	520	506.7	116.9	580	565.2	130.4
341	332.3	76.7	401	390.7	90.2	461	449.2	103.7	521	507.7	117.2	581	566.2	130.7
342	333.2	76.9	402	391.7	90.4	462	450.2	103.9	522	508.6	117.5	582	567.1	131.0
343	334.2	77.1	403	392.7	90.6	463	451.1	104.1	523	509.6	117.7	583	568.1	131.2
344	335.2	77.4	404	393.6	90.8	464	452.1	104.3	524	510.6	117.9	584	569.1	131.4
345	336.2	77.6	405	394.6	91.1	465	453.1	104.6	525	511.6	118.1	585	570.1	131.6
346	337.1	77.8	406	395.6	91.3	466	454.1	104.8	526	512.5	118.3	586	571.0	131.8
347	338.1	78.0	407	396.6	91.5	467	455.0	105.0	527	513.5	118.5	587	572.0	132.0
348	339.1	78.3	408	397.5	91.7	468	456.0	105.2	528	514.5	118.7	588	573.0	132.3
349	340.1	78.5	409	398.5	92.0	469	457.0	105.5	529	515.5	119.0	589	573.9	132.5
350	341.0	78.7	410	399.5	92.2	470	458.0	105.7	530	516.4	119.2	590	574.9	132.8
351	342.0	78.9	411	400.5	92.4	471	458.9	105.9	531	517.4	119.4	591	575.9	133.0
352	343.0	79.2	412	401.4	92.6	472	459.9	106.1	532	518.4	119.6	592	576.9	133.2
353	344.0	79.4	413	402.4	92.9	473	460.9	106.4	533	519.4	119.9	593	577.8	133.4
354	344.9	79.6	414	403.4	93.1	474	461.9	106.6	534	520.3	120.1	594	578.8	133.6
355	345.9	79.8	415	404.4	93.3	475	462.8	106.8	535	521.3	120.3	595	579.8	133.8
356	346.9	80.1	416	405.3	93.5	476	463.8	107.0	536	522.3	120.5	596	580.8	134.0
357	347.9	80.3	417	406.3	93.8	477	464.8	107.3	537	523.3	120.8	597	581.7	134.3
358	348.8	80.5	418	407.3	94.0	478	465.8	107.5	538	524.2	121.0	598	582.7	134.5
359	349.8	80.7	419	408.3	94.2	479	466.7	107.7	539	525.2	121.2	599	583.7	134.8
360	350.8	81.0	420	409.2	94.4	480	467.7	107.9	540	526.2	121.5	600	584.6	135.0
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

77°

5^h 8^m

TRAVERSE TABLE TO DEGREES														
18°									0° 52'					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	1°0	0'2	61	59'4	13'7	121	117'9	27'2	181	176'4	40'7	241	234'8	54'2
2	1'9	0'4	62	60'4	13'9	122	118'9	27'4	182	177'3	40'9	242	235'8	54'4
3	2'9	0'7	63	61'4	14'2	123	119'8	27'7	183	178'3	41'2	243	236'8	54'7
4	3'9	0'9	64	62'4	14'4	124	120'8	27'9	184	179'3	41'4	244	237'7	54'9
5	4'9	1'1	65	63'3	14'6	125	121'8	28'1	185	180'3	41'6	245	238'7	55'1
6	5'8	1'3	66	64'3	14'8	126	122'8	28'3	186	181'2	41'8	246	239'7	55'3
7	6'8	1'6	67	65'3	15'1	127	123'7	28'6	187	182'2	42'1	247	240'7	55'6
8	7'8	1'8	68	66'3	15'3	128	124'7	28'8	188	183'2	42'3	248	241'6	55'8
9	8'8	2'0	69	67'2	15'5	129	125'7	29'0	189	184'2	42'5	249	242'6	56'0
10	9'7	2'2	70	68'2	15'7	130	126'7	29'2	190	185'1	42'7	250	243'6	56'2
11	10'7	2'5	71	69'2	16'0	131	127'6	29'5	191	186'1	43'0	251	244'6	56'5
12	11'7	2'7	72	70'2	16'2	132	128'6	29'7	192	187'1	43'2	252	245'5	56'7
13	12'7	2'9	73	71'1	16'4	133	129'6	29'9	193	188'1	43'4	253	246'5	56'9
14	13'6	3'1	74	72'1	16'6	134	130'6	30'1	194	189'0	43'6	254	247'5	57'1
15	14'6	3'4	75	73'1	16'9	135	131'5	30'4	195	190'0	43'9	255	248'5	57'4
16	15'6	3'6	76	74'1	17'1	136	132'5	30'6	196	191'0	44'1	256	249'4	57'6
17	16'6	3'8	77	75'0	17'3	137	133'5	30'8	197	192'0	44'3	257	250'4	57'8
18	17'5	4'0	78	76'0	17'5	138	134'5	31'0	198	192'9	44'5	258	251'4	58'0
19	18'5	4'3	79	77'0	17'8	139	135'4	31'3	199	193'9	44'8	259	252'4	58'3
20	19'5	4'5	80	78'0	18'0	140	136'4	31'5	200	194'9	45'0	260	253'3	58'5
21	20'5	4'7	81	78'9	18'2	141	137'4	31'7	201	195'8	45'2	261	254'3	58'7
22	21'4	4'9	82	79'9	18'4	142	138'4	31'9	202	196'8	45'4	262	255'3	58'9
23	22'4	5'2	83	80'9	18'7	143	139'3	32'2	203	197'8	45'7	263	256'3	59'2
24	23'4	5'4	84	81'8	18'9	144	140'3	32'4	204	198'8	45'9	264	257'2	59'4
25	24'4	5'6	85	82'8	19'1	145	141'3	32'6	205	199'7	46'1	265	258'2	59'6
26	25'3	5'8	86	83'8	19'3	146	142'3	32'8	206	200'7	46'3	266	259'2	59'8
27	26'3	6'1	87	84'8	19'6	147	143'2	33'1	207	201'7	46'6	267	260'2	60'1
28	27'3	6'3	88	85'7	19'8	148	144'2	33'3	208	202'7	46'8	268	261'1	60'3
29	28'3	6'5	89	86'7	20'0	149	145'2	33'5	209	203'6	47'0	269	262'1	60'5
30	29'2	6'7	90	87'7	20'2	150	146'2	33'7	210	204'6	47'2	270	263'1	60'7
31	30'2	7'0	91	88'7	20'5	151	147'1	34'0	211	205'6	47'5	271	264'1	61'0
32	31'2	7'2	92	89'6	20'7	152	148'1	34'2	212	206'6	47'7	272	265'0	61'2
33	32'2	7'4	93	90'6	20'9	153	149'1	34'4	213	207'5	47'9	273	266'0	61'4
34	33'1	7'6	94	91'6	21'1	154	150'1	34'6	214	208'5	48'1	274	267'0	61'6
35	34'1	7'9	95	92'6	21'4	155	151'0	34'9	215	209'5	48'4	275	268'0	61'9
36	35'1	8'1	96	93'5	21'6	156	152'0	35'1	216	210'5	48'6	276	268'9	62'1
37	36'1	8'3	97	94'5	21'8	157	153'0	35'3	217	211'4	48'8	277	269'9	62'3
38	37'0	8'5	98	95'5	22'0	158	154'0	35'5	218	212'4	49'0	278	270'9	62'5
39	38'0	8'8	99	96'5	22'3	159	154'9	35'8	219	213'4	49'3	279	271'8	62'8
40	39'0	9'0	100	97'4	22'5	160	155'9	36'0	220	214'4	49'5	280	272'8	63'0
41	39'9	9'2	101	98'4	22'7	161	156'9	36'2	221	215'3	49'7	281	273'8	63'2
42	40'9	9'4	102	99'4	22'9	162	157'8	36'4	222	216'3	49'9	282	274'8	63'4
43	41'9	9'7	103	100'4	23'2	163	158'8	36'7	223	217'3	50'2	283	275'7	63'7
44	42'9	9'9	104	101'3	23'4	164	159'8	36'9	224	218'3	50'4	284	276'7	63'9
45	43'8	10'1	105	102'3	23'6	165	160'8	37'1	225	219'2	50'6	285	277'7	64'1
46	44'8	10'3	106	103'3	23'8	166	161'7	37'3	226	220'2	50'8	286	278'7	64'3
47	45'8	10'6	107	104'3	24'1	167	162'7	37'6	227	221'2	51'1	287	279'6	64'6
48	46'8	10'8	108	105'2	24'3	168	163'7	37'8	228	222'2	51'3	288	280'6	64'8
49	47'7	11'0	109	106'2	24'5	169	164'7	38'0	229	223'1	51'5	289	281'6	65'0
50	48'7	11'2	110	107'2	24'7	170	165'6	38'2	230	224'1	51'7	290	282'6	65'2
51	49'7	11'5	111	108'2	25'0	171	166'6	38'5	231	225'1	52'0	291	283'5	65'5
52	50'7	11'7	112	109'1	25'2	172	167'6	38'7	232	226'1	52'2	292	284'5	65'7
53	51'6	11'9	113	110'1	25'4	173	168'6	38'9	233	227'0	52'4	293	285'5	65'9
54	52'6	12'1	114	111'1	25'6	174	169'5	39'1	234	228'0	52'6	294	286'5	66'1
55	53'6	12'4	115	112'1	25'9	175	170'5	39'4	235	229'0	52'9	295	287'4	66'4
56	54'6	12'6	116	113'0	26'1	176	171'5	39'6	236	230'0	53'1	296	288'4	66'6
57	55'5	12'8	117	114'0	26'3	177	172'5	39'8	237	230'9	53'3	297	289'4	66'8
58	56'5	13'0	118	115'0	26'5	178	173'4	40'0	238	231'9	53'5	298	290'4	67'0
59	57'5	13'3	119	116'0	26'8	179	174'4	40'3	239	232'9	53'8	299	291'3	67'3
60	58'5	13'5	120	116'9	27'0	180	175'4	40'5	240	233'8	54'0	300	292'3	67'5
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

467

TRAVERSE TABLE TO DEGREES														
18°										0 ^h 52 ^m				
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	293.3	67.7	361	351.8	81.2	421	410.2	94.7	481	468.7	108.2	541	527.2	121.7
302	294.3	67.9	362	352.7	81.4	422	411.2	94.9	482	469.7	108.4	542	528.1	121.9
303	295.2	68.1	363	353.7	81.6	423	412.2	95.1	483	470.6	108.6	543	529.1	122.1
304	296.2	68.4	364	354.7	81.9	424	413.1	95.3	484	471.6	108.8	544	530.1	122.3
305	297.2	68.6	365	355.6	82.1	425	414.1	95.6	485	472.6	109.0	545	531.1	122.5
306	298.2	68.8	366	356.6	82.3	426	415.1	95.8	486	473.6	109.3	546	532.0	122.8
307	299.1	69.0	367	357.6	82.5	427	416.1	96.0	487	474.5	109.5	547	533.0	123.0
308	300.1	69.3	368	358.6	82.8	428	417.0	96.2	488	475.5	109.7	548	534.0	123.2
309	301.1	69.5	369	359.5	83.0	429	418.0	96.5	489	476.5	109.9	549	535.0	123.4
310	302.1	69.7	370	360.5	83.2	430	419.0	96.7	490	477.5	110.1	550	535.9	123.7
311	303.0	69.9	371	361.5	83.4	431	420.0	96.9	491	478.4	110.4	551	536.9	123.9
312	304.0	70.2	372	362.5	83.7	432	420.9	97.1	492	479.4	110.6	552	537.9	124.1
313	305.0	70.4	373	363.4	83.9	433	421.9	97.4	493	480.4	110.9	553	538.9	124.4
314	306.0	70.6	374	364.4	84.1	434	422.9	97.6	494	481.4	111.1	554	539.8	124.6
315	306.9	70.8	375	365.4	84.3	435	423.9	97.8	495	482.3	111.3	555	540.8	124.9
316	307.9	71.1	376	366.4	84.6	436	424.8	98.0	496	483.3	111.5	556	541.8	125.1
317	308.9	71.3	377	367.3	84.8	437	425.8	98.3	497	484.3	111.8	557	542.8	125.3
318	309.9	71.5	378	368.3	85.0	438	426.8	98.5	498	485.3	112.0	558	543.7	125.5
319	310.8	71.7	379	369.3	85.2	439	427.8	98.7	499	486.2	112.2	559	544.7	125.8
320	311.8	72.0	380	370.3	85.5	440	428.7	98.9	500	487.2	112.4	560	545.7	126.0
321	312.8	72.2	381	371.2	85.7	441	429.7	99.2	501	488.2	112.6	561	546.7	126.2
322	313.8	72.4	382	372.2	85.9	442	430.7	99.4	502	489.2	112.9	562	547.6	126.4
323	314.7	72.6	383	373.2	86.1	443	431.6	99.6	503	490.1	113.1	563	548.6	126.7
324	315.7	72.9	384	374.2	86.4	444	432.6	99.8	504	491.1	113.3	564	549.6	126.9
325	316.7	73.1	385	375.1	86.6	445	433.6	100.1	505	492.1	113.5	565	550.6	127.1
326	317.6	73.3	386	376.1	86.8	446	434.6	100.3	506	493.1	113.8	566	551.5	127.3
327	318.6	73.5	387	377.1	87.0	447	435.5	100.5	507	494.0	114.0	567	552.5	127.6
328	319.6	73.8	388	378.1	87.3	448	436.5	100.7	508	495.0	114.2	568	553.5	127.8
329	320.6	74.0	389	379.0	87.5	449	437.5	101.0	509	496.0	114.5	569	554.5	128.0
330	321.5	74.2	390	380.0	87.7	450	438.5	101.2	510	496.9	114.7	570	555.4	128.3
331	322.5	74.4	391	381.0	87.9	451	439.4	101.4	511	497.9	114.9	571	556.4	128.5
332	323.5	74.7	392	382.0	88.2	452	440.4	101.6	512	498.9	115.1	572	557.4	128.7
333	324.5	74.9	393	382.9	88.4	453	441.4	101.9	513	499.9	115.4	573	558.4	128.9
334	325.4	75.1	394	383.9	88.6	454	442.4	102.1	514	500.8	115.6	574	559.3	129.2
335	326.4	75.3	395	384.9	88.8	455	443.3	102.3	515	501.8	115.8	575	560.3	129.4
336	327.4	75.6	396	385.9	89.1	456	444.3	102.5	516	502.8	116.0	576	561.3	129.6
337	328.4	75.8	397	386.8	89.3	457	445.3	102.8	517	503.8	116.3	577	562.3	129.8
338	329.3	76.0	398	387.8	89.5	458	446.3	103.0	518	504.7	116.5	578	563.2	130.0
339	330.3	76.2	399	388.8	89.7	459	447.2	103.2	519	505.7	116.7	579	564.2	130.2
340	331.3	76.5	400	389.8	90.0	460	448.2	103.4	520	506.7	116.9	580	565.2	130.4
341	332.3	76.7	401	390.7	90.2	461	449.2	103.7	521	507.7	117.2	581	566.2	130.7
342	333.2	76.9	402	391.7	90.4	462	450.2	103.9	522	508.6	117.5	582	567.1	131.0
343	334.2	77.1	403	392.7	90.6	463	451.1	104.1	523	509.6	117.7	583	568.1	131.2
344	335.2	77.4	404	393.6	90.8	464	452.1	104.3	524	510.6	117.9	584	569.1	131.4
345	336.2	77.6	405	394.6	91.1	465	453.1	104.6	525	511.6	118.1	585	570.1	131.6
346	337.1	77.8	406	395.6	91.3	466	454.1	104.8	526	512.5	118.3	586	571.0	131.8
347	338.1	78.0	407	396.6	91.5	467	455.0	105.0	527	513.5	118.5	587	572.0	132.0
348	339.1	78.3	408	397.5	91.7	468	456.0	105.2	528	514.5	118.7	588	573.0	132.3
349	340.1	78.5	409	398.5	92.0	469	457.0	105.5	529	515.5	119.0	589	573.9	132.5
350	341.0	78.7	410	399.5	92.2	470	458.0	105.7	530	516.4	119.2	590	574.9	132.8
351	342.0	78.9	411	400.5	92.4	471	458.9	105.9	531	517.4	119.4	591	575.9	133.0
352	343.0	79.2	412	401.4	92.6	472	459.9	106.1	532	518.4	119.6	592	576.9	133.2
353	344.0	79.4	413	402.4	92.9	473	460.9	106.4	533	519.4	119.9	593	577.8	133.4
354	344.9	79.6	414	403.4	93.1	474	461.9	106.6	534	520.3	120.1	594	578.8	133.6
355	345.9	79.8	415	404.4	93.3	475	462.8	106.8	535	521.3	120.3	595	579.8	133.8
356	346.9	80.1	416	405.3	93.5	476	463.8	107.0	536	522.3	120.5	596	580.8	134.0
357	347.9	80.3	417	406.3	93.8	477	464.8	107.3	537	523.3	120.8	597	581.7	134.3
358	348.8	80.5	418	407.3	94.0	478	465.8	107.5	538	524.2	121.0	598	582.7	134.5
359	349.8	80.7	419	408.3	94.2	479	466.7	107.7	539	525.2	121.2	599	583.7	134.8
360	350.8	81.0	420	409.2	94.4	480	467.7	107.9	540	526.2	121.5	600	584.6	135.0
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

77°

5^h 8^m

TRAVERSE TABLE TO DEGREES														
14°									0 ^h 56 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	1°0	0°2	61	59°2	14°8	121	117°4	29°3	181	175°6	43°8	241	233°8	58°3
2	1°9	0°5	62	60°2	15°0	122	118°4	29°5	182	176°6	44°0	242	234°8	58°5
3	2°9	0°7	63	61°1	15°2	123	119°3	29°8	183	177°6	44°3	243	235°8	58°8
4	3°9	1°0	64	62°1	15°5	124	120°3	30°0	184	178°5	44°5	244	236°8	59°0
5	4°9	1°2	65	63°1	15°7	125	121°3	30°2	185	179°5	44°8	245	237°7	59°3
6	5°8	1°5	66	64°0	16°0	126	122°3	30°5	186	180°5	45°0	246	238°7	59°5
7	6°8	1°7	67	65°0	16°2	127	123°2	30°7	187	181°4	45°2	247	239°7	59°8
8	7°8	1°9	68	66°0	16°5	128	124°2	31°0	188	182°4	45°5	248	240°6	60°0
9	8°7	2°2	69	67°0	16°7	129	125°2	31°2	189	183°4	45°7	249	241°6	60°2
10	9°7	2°4	70	67°9	16°9	130	126°1	31°4	190	184°4	46°0	250	242°6	60°5
11	10°7	2°7	71	68°9	17°2	131	127°1	31°7	191	185°3	46°2	251	243°5	60°7
12	11°6	2°9	72	69°9	17°4	132	128°1	31°9	192	186°3	46°4	252	244°5	61°0
13	12°6	3°1	73	70°8	17°7	133	129°0	32°2	193	187°3	46°7	253	245°5	61°2
14	13°6	3°4	74	71°8	17°9	134	130°0	32°4	194	188°2	46°9	254	246°5	61°4
15	14°6	3°6	75	72°8	18°1	135	131°0	32°7	195	189°2	47°2	255	247°4	61°7
16	15°5	3°9	76	73°7	18°4	136	132°0	32°9	196	190°2	47°4	256	248°4	61°9
17	16°5	4°1	77	74°7	18°6	137	132°9	33°1	197	191°1	47°7	257	249°4	62°2
18	17°5	4°4	78	75°7	18°9	138	133°9	33°4	198	192°1	47°9	258	250°3	62°4
19	18°4	4°6	79	76°7	19°1	139	134°9	33°6	199	193°1	48°1	259	251°3	62°7
20	19°4	4°8	80	77°6	19°4	140	135°8	33°9	200	194°1	48°4	260	252°3	62°9
21	20°4	5°1	81	78°6	19°6	141	136°8	34°1	201	195°0	48°6	261	253°2	63°1
22	21°3	5°3	82	79°6	19°8	142	137°8	34°4	202	196°0	48°9	262	254°2	63°4
23	22°3	5°6	83	80°5	20°1	143	138°8	34°6	203	197°0	49°1	263	255°2	63°6
24	23°3	5°8	84	81°5	20°3	144	139°7	34°8	204	197°9	49°4	264	256°2	63°9
25	24°3	6°0	85	82°5	20°6	145	140°7	35°1	205	198°9	49°6	265	257°1	64°1
26	25°2	6°3	86	83°4	20°8	146	141°7	35°3	206	199°9	49°8	266	258°1	64°4
27	26°2	6°5	87	84°4	21°0	147	142°6	35°6	207	200°9	50°1	267	259°1	64°6
28	27°2	6°8	88	85°4	21°3	148	143°6	35°8	208	201°8	50°3	268	260°0	64°8
29	28°1	7°0	89	86°4	21°5	149	144°6	36°0	209	202°8	50°6	269	261°0	65°1
30	29°1	7°3	90	87°3	21°8	150	145°5	36°3	210	203°8	50°8	270	262°0	65°3
31	30°1	7°5	91	88°3	22°0	151	146°5	36°5	211	204°7	51°0	271	263°0	65°6
32	31°0	7°7	92	89°3	22°3	152	147°5	36°8	212	205°7	51°3	272	263°9	65°8
33	32°0	8°0	93	90°2	22°5	153	148°5	37°0	213	206°7	51°5	273	264°9	66°0
34	33°0	8°2	94	91°2	22°7	154	149°4	37°3	214	207°6	51°8	274	265°9	66°3
35	34°0	8°5	95	92°2	23°0	155	150°4	37°5	215	208°6	52°0	275	266°8	66°5
36	34°9	8°7	96	93°1	23°2	156	151°4	37°7	216	209°6	52°3	276	267°8	66°8
37	35°9	9°0	97	94°1	23°5	157	152°3	38°0	217	210°6	52°5	277	268°8	67°0
38	36°9	9°2	98	95°1	23°7	158	153°3	38°2	218	211°5	52°7	278	269°7	67°3
39	37°8	9°4	99	96°1	24°0	159	154°3	38°5	219	212°5	53°0	279	270°7	67°5
40	38°8	9°7	100	97°0	24°2	160	155°2	38°7	220	213°5	53°2	280	271°7	67°7
41	39°8	9°9	101	98°0	24°4	161	156°2	38°9	221	214°4	53°5	281	272°7	68°0
42	40°8	10°2	102	99°0	24°7	162	157°2	39°2	222	215°4	53°7	282	273°6	68°2
43	41°7	10°4	103	99°9	24°9	163	158°2	39°4	223	216°4	53°9	283	274°6	68°5
44	42°7	10°6	104	100°9	25°2	164	159°1	39°7	224	217°3	54°2	284	275°6	68°7
45	43°7	10°9	105	101°9	25°4	165	160°1	39°9	225	218°3	54°4	285	276°5	68°9
46	44°6	11°1	106	102°9	25°6	166	161°1	40°2	226	219°3	54°7	286	277°5	69°2
47	45°6	11°4	107	103°8	25°9	167	162°0	40°4	227	220°3	54°9	287	278°5	69°4
48	46°6	11°6	108	104°8	26°1	168	163°0	40°6	228	221°2	55°2	288	279°4	69°7
49	47°5	11°9	109	105°8	26°4	169	164°0	40°9	229	222°2	55°4	289	280°4	69°9
50	48°5	12°1	110	106°7	26°6	170	165°0	41°1	230	223°2	55°6	290	281°4	70°2
51	49°5	12°3	111	107°7	26°9	171	165°9	41°4	231	224°1	55°9	291	282°4	70°4
52	50°5	12°6	112	108°7	27°1	172	166°9	41°6	232	225°1	56°1	292	283°3	70°6
53	51°4	12°8	113	109°6	27°3	173	167°9	41°9	233	226°1	56°4	293	284°3	70°9
54	52°4	13°1	114	110°6	27°6	174	168°8	42°1	234	227°0	56°6	294	285°3	71°1
55	53°4	13°3	115	111°6	27°8	175	169°8	42°3	235	228°0	56°9	295	286°2	71°4
56	54°3	13°5	116	112°6	28°1	176	170°8	42°6	236	229°0	57°1	296	287°2	71°6
57	55°3	13°8	117	113°5	28°3	177	171°7	42°8	237	230°0	57°3	297	288°2	71°9
58	56°3	14°0	118	114°5	28°5	178	172°7	43°1	238	230°9	57°6	298	289°1	72°1
59	57°2	14°3	119	115°5	28°8	179	173°7	43°3	239	231°9	57°8	299	290°1	72°3
60	58°2	14°5	120	116°4	29°0	180	174°7	43°5	240	232°9	58°1	300	291°1	72°6
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

459

TRAVERSE TABLE TO DEGREES														
14°									0h 56m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	292°0	72°8	361	350°2	87°3	421	408°5	101°8	481	466°7	116°3	541	525°0	130°9
302	293°0	73°0	362	351°2	87°6	422	409°4	102°1	482	467°7	116°6	542	525°9	131°2
303	294°0	73°3	363	352°2	87°8	423	410°4	102°3	483	468°6	116°8	543	526°9	131°4
304	294°9	73°5	364	353°2	88°0	424	411°4	102°6	484	469°6	117°1	544	527°9	131°6
305	295°9	73°8	365	354°1	88°3	425	412°3	102°8	485	470°6	117°3	545	528°8	131°9
306	296°9	74°0	366	355°1	88°5	426	413°3	103°0	486	471°5	117°6	546	529°8	132°1
307	297°8	74°2	367	356°1	88°8	427	414°3	103°3	487	472°5	117°8	547	530°8	132°3
308	298°8	74°5	368	357°0	89°0	428	415°3	103°5	488	473°5	118°0	548	531°7	132°6
309	299°8	74°7	369	358°0	89°2	429	416°2	103°8	489	474°5	118°3	549	532°7	132°8
310	300°8	75°0	370	359°0	89°5	430	417°2	104°0	490	475°4	118°5	550	533°7	133°0
311	301°7	75°2	371	359°9	89°7	431	418°2	104°2	491	476°4	118°8	551	534°6	133°3
312	302°7	75°5	372	360°9	90°0	432	419°1	104°5	492	477°4	119°0	552	535°6	133°6
313	303°7	75°7	373	361°9	90°2	433	420°1	104°7	493	478°3	119°2	553	536°6	133°8
314	304°6	75°9	374	362°9	90°5	434	421°1	105°0	494	479°3	119°5	554	537°5	134°0
315	305°6	76°2	375	363°8	90°7	435	422°0	105°2	495	480°3	119°7	555	538°5	134°3
316	306°6	76°4	376	364°8	90°9	436	423°0	105°5	496	481°3	120°0	556	539°5	134°5
317	307°6	76°7	377	365°8	91°2	437	424°0	105°7	497	482°2	120°2	557	540°5	134°8
318	308°5	76°9	378	366°7	91°4	438	425°0	105°9	498	483°2	120°4	558	541°4	135°0
319	309°5	77°2	379	367°7	91°7	439	425°9	106°2	499	484°2	120°7	559	542°4	135°2
320	310°5	77°4	380	368°7	91°9	440	426°9	106°4	500	485°1	121°0	560	543°4	135°5
321	311°4	77°6	381	369°6	92°2	441	427°9	106°7	501	486°1	121°2	561	544°3	135°7
322	312°4	77°9	382	370°6	92°4	442	428°8	106°9	502	487°1	121°4	562	545°3	135°9
323	313°4	78°1	383	371°6	92°6	443	429°8	107°1	503	488°0	121°7	563	546°3	136°2
324	314°3	78°4	384	372°6	92°9	444	430°8	107°4	504	489°0	122°0	564	547°2	136°5
325	315°3	78°6	385	373°5	93°1	445	431°7	107°6	505	490°0	122°1	565	548°2	136°6
326	316°3	78°8	386	374°5	93°4	446	432°7	107°9	506	491°0	122°4	566	549°2	136°9
327	317°3	79°1	387	375°5	93°6	447	433°7	108°1	507	491°9	122°6	567	550°1	137°1
328	318°2	79°3	388	376°4	93°8	448	434°7	108°4	508	492°9	122°9	568	551°1	137°4
329	319°2	79°6	389	377°4	94°1	449	435°6	108°6	509	493°9	123°1	569	552°1	137°6
330	320°2	79°8	390	378°4	94°3	450	436°6	108°8	510	494°9	123°4	570	553°1	137°9
331	321°1	80°1	391	379°4	94°6	451	437°6	109°1	511	495°8	123°6	571	554°0	138°1
332	322°1	80°3	392	380°3	94°8	452	438°5	109°3	512	496°8	123°8	572	555°0	138°3
333	323°1	80°5	393	381°3	95°1	453	439°5	109°6	513	497°8	124°1	573	556°0	138°6
334	324°0	80°8	394	382°3	95°3	454	440°5	109°8	514	498°7	124°3	574	557°0	138°8
335	325°0	81°0	395	383°2	95°5	455	441°5	110°1	515	499°7	124°6	575	557°9	139°1
336	326°0	81°3	396	384°2	95°8	456	442°4	110°3	516	500°7	124°8	576	558°9	139°3
337	327°0	81°5	397	385°2	96°0	457	443°4	110°5	517	501°7	125°0	577	559°9	139°5
338	327°9	81°7	398	386°1	96°3	458	444°4	110°8	518	502°6	125°3	578	560°9	139°8
339	328°9	82°0	399	387°1	96°5	459	445°3	111°0	519	503°6	125°6	579	561°8	140°0
340	329°9	82°2	400	388°1	96°7	460	446°3	111°3	520	504°6	125°8	580	562°8	140°3
341	330°8	82°5	401	389°1	97°0	461	447°3	111°5	521	505°5	126°0	581	563°8	140°5
342	331°8	82°7	402	390°0	97°2	462	448°2	111°7	522	506°5	126°2	582	564°7	140°8
343	332°8	83°0	403	391°0	97°5	463	449°2	112°0	523	507°5	126°5	583	565°7	141°0
344	333°7	83°2	404	392°0	97°7	464	450°2	112°2	524	508°4	126°8	584	566°7	141°3
345	334°7	83°4	405	392°9	98°0	465	451°2	112°5	525	509°4	127°0	585	567°6	141°5
346	335°7	83°7	406	393°9	98°2	466	452°1	112°7	526	510°4	127°2	586	568°6	141°8
347	336°7	83°9	407	394°9	98°4	467	453°1	113°0	527	511°4	127°5	587	569°6	142°0
348	337°6	84°2	408	395°8	98°7	468	454°1	113°2	528	512°3	127°8	588	570°6	142°3
349	338°6	84°4	409	396°8	98°9	469	455°0	113°4	529	513°3	128°0	589	571°5	142°5
350	339°6	84°7	410	397°8	99°2	470	456°0	113°7	530	514°3	128°2	590	572°5	142°8
351	340°5	84°9	411	398°8	99°4	471	457°0	113°9	531	515°3	128°5	591	573°5	143°0
352	341°5	85°1	412	399°7	99°7	472	457°9	114°2	532	516°2	128°8	592	574°4	143°3
353	342°5	85°4	413	400°7	99°9	473	458°9	114°4	533	517°2	129°0	593	575°4	143°5
354	343°5	85°6	414	401°7	100°1	474	459°9	114°6	534	518°2	129°2	594	576°4	143°8
355	344°4	85°9	415	402°6	100°4	475	460°9	114°9	535	519°1	129°4	595	577°3	144°0
356	345°4	86°1	416	403°6	100°6	476	461°8	115°1	536	520°1	129°7	596	578°3	144°2
357	346°4	86°3	417	404°6	100°9	477	462°8	115°4	537	521°1	129°9	597	579°3	144°5
358	347°3	86°6	418	405°5	101°1	478	463°8	115°6	538	522°1	130°2	598	580°3	144°7
359	348°3	86°8	419	406°5	101°3	479	464°7	115°9	539	523°0	130°4	599	581°2	144°9
360	349°3	87°1	420	407°5	101°6	480	465°7	116°1	540	524°0	130°6	600	582°2	145°1
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

78°

5h 4m

TRAVERSE TABLE TO DEGREES														
15°										1° 0'				
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	1° 0'	0' 3"	61	58° 9'	15° 8'	121	116° 9'	31° 3'	181	174° 8'	46° 8'	241	232° 8'	62° 4'
2	1° 9'	0° 5'	62	59° 9'	16° 0'	122	117° 8'	31° 6'	182	175° 8'	47° 1'	242	233° 8'	62° 6'
3	2° 9'	0° 8'	63	60° 9'	16° 3'	123	118° 8'	31° 8'	183	176° 8'	47° 4'	243	234° 7'	62° 9'
4	3° 9'	1° 0'	64	61° 8'	16° 6'	124	119° 8'	32° 1'	184	177° 7'	47° 6'	244	235° 7'	63° 2'
5	4° 8'	1° 3'	65	62° 8'	16° 8'	125	120° 7'	32° 4'	185	178° 7'	47° 9'	245	236° 7'	63° 4'
6	5° 8'	1° 6'	66	63° 8'	17° 1'	126	121° 7'	32° 6'	186	179° 7'	48° 1'	246	237° 6'	63° 7'
7	6° 8'	1° 8'	67	64° 7'	17° 3'	127	122° 7'	32° 9'	187	180° 6'	48° 4'	247	238° 6'	63° 9'
8	7° 7'	2° 1'	68	65° 7'	17° 6'	128	123° 6'	33° 1'	188	181° 6'	48° 7'	248	239° 5'	64° 2'
9	8° 7'	2° 3'	69	66° 6'	17° 9'	129	124° 6'	33° 4'	189	182° 6'	48° 9'	249	240° 5'	64° 4'
10	9° 7'	2° 6'	70	67° 6'	18° 1'	130	125° 6'	33° 6'	190	183° 5'	49° 2'	250	241° 5'	64° 7'
11	10° 6'	2° 8'	71	68° 6'	18° 4'	131	126° 5'	33° 9'	191	184° 5'	49° 4'	251	242° 4'	65° 0'
12	11° 6'	3° 1'	72	69° 5'	18° 6'	132	127° 5'	34° 2'	192	185° 5'	49° 7'	252	243° 4'	65° 2'
13	12° 6'	3° 4'	73	70° 5'	18° 9'	133	128° 5'	34° 4'	193	186° 4'	50° 0'	253	244° 4'	65° 5'
14	13° 5'	3° 6'	74	71° 5'	19° 2'	134	129° 4'	34° 7'	194	187° 4'	50° 2'	254	245° 3'	65° 7'
15	14° 5'	3° 9'	75	72° 4'	19° 4'	135	130° 4'	34° 9'	195	188° 4'	50° 5'	255	246° 3'	66° 0'
16	15° 5'	4° 1'	76	73° 4'	19° 7'	136	131° 4'	35° 2'	196	189° 3'	50° 7'	256	247° 3'	66° 3'
17	16° 4'	4° 4'	77	74° 4'	19° 9'	137	132° 3'	35° 5'	197	190° 3'	51° 0'	257	248° 2'	66° 5'
18	17° 4'	4° 7'	78	75° 3'	20° 2'	138	133° 3'	35° 7'	198	191° 3'	51° 2'	258	249° 2'	66° 8'
19	18° 4'	4° 9'	79	76° 3'	20° 4'	139	134° 3'	36° 0'	199	192° 2'	51° 5'	259	250° 2'	67° 0'
20	19° 3'	5° 2'	80	77° 3'	20° 7'	140	135° 2'	36° 2'	200	193° 2'	51° 8'	260	251° 1'	67° 3'
21	20° 3'	5° 4'	81	78° 2'	21° 0'	141	136° 2'	36° 5'	201	194° 2'	52° 0'	261	252° 1'	67° 6'
22	21° 2'	5° 7'	82	79° 2'	21° 2'	142	137° 2'	36° 8'	202	195° 1'	52° 3'	262	253° 1'	67° 8'
23	22° 2'	6° 0'	83	80° 2'	21° 5'	143	138° 1'	37° 0'	203	196° 1'	52° 5'	263	254° 0'	68° 1'
24	23° 2'	6° 2'	84	81° 1'	21° 7'	144	139° 1'	37° 3'	204	197° 0'	52° 8'	264	255° 0'	68° 3'
25	24° 1'	6° 5'	85	82° 1'	22° 0'	145	140° 1'	37° 5'	205	198° 0'	53° 1'	265	256° 0'	68° 6'
26	25° 1'	6° 7'	86	83° 1'	22° 3'	146	141° 0'	37° 8'	206	199° 0'	53° 3'	266	256° 9'	68° 8'
27	26° 1'	7° 0'	87	84° 0'	22° 5'	147	142° 0'	38° 0'	207	199° 9'	53° 6'	267	257° 9'	69° 1'
28	27° 0'	7° 2'	88	85° 0'	22° 8'	148	143° 0'	38° 3'	208	200° 9'	53° 8'	268	258° 9'	69° 4'
29	28° 0'	7° 5'	89	86° 0'	23° 0'	149	143° 9'	38° 6'	209	201° 9'	54° 1'	269	259° 8'	69° 6'
30	29° 0'	7° 8'	90	86° 9'	23° 3'	150	144° 9'	38° 8'	210	202° 8'	54° 4'	270	260° 8'	69° 9'
31	29° 9'	8° 0'	91	87° 9'	23° 6'	151	145° 9'	39° 1'	211	203° 8'	54° 6'	271	261° 8'	70° 1'
32	30° 9'	8° 3'	92	88° 9'	23° 8'	152	146° 8'	39° 3'	212	204° 8'	54° 9'	272	262° 7'	70° 4'
33	31° 9'	8° 5'	93	89° 8'	24° 1'	153	147° 8'	39° 6'	213	205° 7'	55° 1'	273	263° 7'	70° 7'
34	32° 8'	8° 8'	94	90° 8'	24° 3'	154	148° 8'	39° 9'	214	206° 7'	55° 4'	274	264° 7'	70° 9'
35	33° 8'	9° 1'	95	91° 8'	24° 6'	155	149° 7'	40° 1'	215	207° 7'	55° 6'	275	265° 6'	71° 2'
36	34° 8'	9° 3'	96	92° 7'	24° 8'	156	150° 7'	40° 4'	216	208° 6'	55° 9'	276	266° 6'	71° 4'
37	35° 7'	9° 6'	97	93° 7'	25° 1'	157	151° 7'	40° 6'	217	209° 6'	56° 2'	277	267° 6'	71° 7'
38	36° 7'	9° 8'	98	94° 7'	25° 4'	158	152° 6'	40° 9'	218	210° 6'	56° 4'	278	268° 5'	72° 0'
39	37° 7'	10° 1'	99	95° 6'	25° 6'	159	153° 6'	41° 2'	219	211° 5'	56° 7'	279	269° 5'	72° 2'
40	38° 6'	10° 4'	100	96° 6'	25° 9'	160	154° 5'	41° 4'	220	212° 5'	56° 9'	280	270° 5'	72° 5'
41	39° 6'	10° 6'	101	97° 6'	26° 1'	161	155° 5'	41° 7'	221	213° 5'	57° 2'	281	271° 4'	72° 7'
42	40° 6'	10° 9'	102	98° 5'	26° 4'	162	156° 5'	41° 9'	222	214° 4'	57° 5'	282	272° 4'	73° 0'
43	41° 5'	11° 1'	103	99° 5'	26° 7'	163	157° 4'	42° 2'	223	215° 4'	57° 7'	283	273° 4'	73° 2'
44	42° 5'	11° 4'	104	100° 5'	26° 9'	164	158° 4'	42° 4'	224	216° 4'	58° 0'	284	274° 3'	73° 5'
45	43° 5'	11° 6'	105	101° 4'	27° 2'	165	159° 4'	42° 7'	225	217° 3'	58° 2'	285	275° 3'	73° 8'
46	44° 4'	11° 9'	106	102° 4'	27° 4'	166	160° 3'	43° 0'	226	218° 3'	58° 5'	286	276° 3'	74° 0'
47	45° 4'	12° 2'	107	103° 4'	27° 7'	167	161° 3'	43° 2'	227	219° 3'	58° 8'	287	277° 2'	74° 3'
48	46° 4'	12° 4'	108	104° 3'	28° 0'	168	162° 3'	43° 5'	228	220° 2'	59° 0'	288	278° 2'	74° 5'
49	47° 3'	12° 7'	109	105° 3'	28° 2'	169	163° 2'	43° 7'	229	221° 2'	59° 3'	289	279° 2'	74° 8'
50	48° 3'	12° 9'	110	106° 3'	28° 5'	170	164° 2'	44° 0'	230	222° 2'	59° 5'	290	280° 1'	75° 1'
51	49° 3'	13° 2'	111	107° 2'	28° 7'	171	165° 2'	44° 3'	231	223° 1'	59° 8'	291	281° 1'	75° 3'
52	50° 2'	13° 5'	112	108° 2'	29° 0'	172	166° 1'	44° 5'	232	224° 1'	60° 0'	292	282° 1'	75° 6'
53	51° 2'	13° 7'	113	109° 1'	29° 2'	173	167° 1'	44° 8'	233	225° 1'	60° 3'	293	283° 0'	75° 8'
54	52° 2'	14° 0'	114	110° 1'	29° 5'	174	168° 1'	45° 0'	234	226° 0'	60° 6'	294	284° 0'	76° 1'
55	53° 1'	14° 2'	115	111° 1'	29° 8'	175	169° 0'	45° 3'	235	227° 0'	60° 8'	295	284° 9'	76° 4'
56	54° 1'	14° 5'	116	112° 0'	30° 0'	176	170° 0'	45° 6'	236	228° 0'	61° 1'	296	285° 9'	76° 6'
57	55° 1'	14° 8'	117	113° 0'	30° 3'	177	171° 0'	45° 8'	237	228° 9'	61° 3'	297	286° 9'	76° 9'
58	56° 0'	15° 0'	118	114° 0'	30° 5'	178	171° 9'	46° 1'	238	229° 9'	61° 6'	298	287° 8'	77° 1'
59	57° 0'	15° 3'	119	114° 9'	30° 8'	179	172° 9'	46° 3'	239	230° 9'	61° 9'	299	288° 8'	77° 4'
60	58° 0'	15° 5'	120	115° 9'	31° 1'	180	173° 9'	46° 6'	240	231° 8'	62° 1'	300	289° 8'	77° 6'
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
75°										5° 0'				

TABLE 1

461

TRAVERSE TABLE TO DEGREES

15°

1^h 0^m

Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	290.7	77.9	361	348.7	93.4	421	406.6	109.0	481	464.6	124.5	541	522.6	140.0
302	291.7	78.2	362	349.6	93.7	422	407.6	109.2	482	465.6	124.8	542	523.5	140.3
303	292.7	78.4	363	350.6	94.0	423	408.6	109.5	483	466.5	125.0	543	524.5	140.5
304	293.6	78.7	364	351.6	94.2	424	409.5	109.7	484	467.5	125.3	544	525.5	140.8
305	294.6	78.9	365	352.5	94.5	425	410.5	110.0	485	468.5	125.6	545	526.4	141.1
306	295.6	79.2	366	353.5	94.7	426	411.5	110.3	486	469.4	125.8	546	527.4	141.4
307	296.5	79.5	367	354.5	95.0	427	412.4	110.5	487	470.4	126.1	547	528.4	141.6
308	297.5	79.7	368	355.4	95.3	428	413.4	110.8	488	471.4	126.4	548	529.3	141.9
309	298.4	80.0	369	356.4	95.5	429	414.4	111.0	489	472.3	126.6	549	530.3	142.1
310	299.4	80.2	370	357.4	95.8	430	415.3	111.3	490	473.3	126.9	550	531.3	142.4
311	300.4	80.5	371	358.3	96.0	431	416.3	111.6	491	474.3	127.1	551	532.2	142.6
312	301.3	80.8	372	359.3	96.3	432	417.3	111.8	492	475.2	127.4	552	533.2	142.9
313	302.3	81.0	373	360.3	96.5	433	418.2	112.1	493	476.2	127.6	553	534.2	143.1
314	303.3	81.3	374	361.2	96.8	434	419.2	112.3	494	477.2	127.9	554	535.1	143.4
315	304.2	81.5	375	362.2	97.1	435	420.2	112.6	495	478.1	128.1	555	536.1	143.7
316	305.2	81.8	376	363.2	97.3	436	421.1	112.9	496	479.1	128.4	556	537.1	143.9
317	306.2	82.1	377	364.1	97.6	437	422.1	113.1	497	480.1	128.6	557	538.0	144.2
318	307.1	82.3	378	365.1	97.8	438	423.1	113.4	498	481.0	128.9	558	539.0	144.4
319	308.1	82.6	379	366.1	98.1	439	424.0	113.6	499	482.0	129.1	559	540.0	144.7
320	309.1	82.8	380	367.0	98.4	440	425.0	113.9	500	483.0	129.4	560	540.9	144.9
321	310.0	83.1	381	368.0	98.6	441	426.0	114.1	501	483.9	129.7	561	541.9	145.2
322	311.0	83.3	382	369.0	98.9	442	426.9	114.4	502	484.9	129.9	562	542.9	145.4
323	312.0	83.6	383	369.9	99.1	443	427.9	114.7	503	485.9	130.2	563	543.8	145.7
324	312.9	83.9	384	370.9	99.4	444	428.8	114.9	504	486.8	130.4	564	544.8	146.0
325	313.9	84.1	385	371.9	99.6	445	429.8	115.2	505	487.8	130.7	565	545.8	146.2
326	314.9	84.4	386	372.8	99.9	446	430.8	115.4	506	488.8	131.0	566	546.7	146.5
327	315.8	84.6	387	373.8	100.2	447	431.7	115.7	507	489.7	131.2	567	547.7	146.7
328	316.8	84.9	388	374.8	100.4	448	432.7	116.0	508	490.7	131.5	568	548.7	147.0
329	317.8	85.1	389	375.7	100.7	449	433.7	116.2	509	491.7	131.7	569	549.6	147.2
330	318.7	85.4	390	376.7	100.9	450	434.6	116.5	510	492.6	132.0	570	550.6	147.5
331	319.7	85.7	391	377.7	101.2	451	435.6	116.7	511	493.6	132.3	571	551.6	147.8
332	320.7	85.9	392	378.6	101.5	452	436.6	117.0	512	494.5	132.5	572	552.5	148.0
333	321.6	86.2	393	379.6	101.7	453	437.5	117.3	513	495.5	132.8	573	553.5	148.3
334	322.6	86.5	394	380.6	102.0	454	438.5	117.5	514	496.5	133.0	574	554.4	148.5
335	323.6	86.7	395	381.5	102.2	455	439.5	117.8	515	497.4	133.3	575	555.4	148.8
336	324.5	87.0	396	382.5	102.5	456	440.4	118.0	516	498.4	133.5	576	556.4	149.0
337	325.5	87.2	397	383.4	102.8	457	441.4	118.3	517	499.4	133.8	577	557.3	149.3
338	326.5	87.5	398	384.4	103.0	458	442.4	118.5	518	500.3	134.0	578	558.3	149.5
339	327.4	87.7	399	385.4	103.3	459	443.3	118.8	519	501.3	134.3	579	559.3	149.8
340	328.4	88.0	400	386.3	103.5	460	444.3	119.1	520	502.3	134.6	580	560.2	150.1
341	329.4	88.3	401	387.3	103.8	461	445.3	119.3	521	503.2	134.8	581	561.2	150.3
342	330.3	88.5	402	388.3	104.1	462	446.2	119.6	522	504.2	135.1	582	562.2	150.6
343	331.3	88.8	403	389.2	104.3	463	447.2	119.8	523	505.2	135.3	583	563.1	150.8
344	332.3	89.0	404	390.2	104.6	464	448.2	120.1	524	506.1	135.6	584	564.1	151.1
345	333.2	89.3	405	391.2	104.8	465	449.1	120.4	525	507.1	135.9	585	565.1	151.4
346	334.2	89.6	406	392.1	105.1	466	450.1	120.6	526	508.1	136.1	586	566.0	151.6
347	335.2	89.8	407	393.1	105.3	467	451.1	120.9	527	509.0	136.4	587	567.0	151.9
348	336.1	90.1	408	394.1	105.6	468	452.0	121.1	528	510.0	136.6	588	568.0	152.2
349	337.1	90.3	409	395.0	105.9	469	453.0	121.4	529	511.0	136.9	589	568.9	152.4
350	338.1	90.6	410	396.0	106.1	470	454.0	121.7	530	511.9	137.2	590	569.9	152.7
351	339.0	90.9	411	397.0	106.4	471	454.9	121.9	531	512.9	137.4	591	570.9	153.0
352	340.0	91.1	412	397.9	106.6	472	455.9	122.2	532	513.9	137.7	592	571.8	153.2
353	340.9	91.4	413	398.9	106.9	473	456.9	122.4	533	514.8	137.9	593	572.8	153.5
354	341.9	91.6	414	399.9	107.2	474	457.8	122.7	534	515.8	138.2	594	573.8	153.7
355	342.9	91.9	415	400.8	107.4	475	458.8	122.9	535	516.8	138.4	595	574.7	154.0
356	343.8	92.1	416	401.8	107.7	476	459.8	123.2	536	517.7	138.7	596	575.7	154.2
357	344.8	92.4	417	402.8	107.9	477	460.7	123.5	537	518.7	139.0	597	576.7	154.5
358	345.8	92.7	418	403.7	108.2	478	461.7	123.7	538	519.7	139.2	598	577.6	154.8
359	346.7	92.9	419	404.7	108.5	479	462.7	124.0	539	520.6	139.5	599	578.6	155.0
360	347.7	93.2	420	405.7	108.7	480	463.6	124.2	540	521.6	139.7	600	579.5	155.3

75°

5^h 0^m

TABLE 1

463

TRAVERSE TABLE TO DEGREES														
16°									1 ^h 4 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	289.3	82.9	361	347.0	99.5	421	404.7	116.0	481	462.4	132.5	541	520.1	149.1
302	290.3	83.2	362	348.0	99.7	422	405.6	116.3	482	463.3	132.8	542	521.0	149.4
303	291.2	83.5	363	348.9	100.0	423	406.6	116.6	483	464.3	133.1	543	522.0	149.7
304	292.2	83.8	364	349.9	100.3	424	407.6	116.8	484	465.2	133.4	544	523.0	150.0
305	293.2	84.0	365	350.8	100.6	425	408.5	117.1	485	466.2	133.6	545	523.9	150.2
306	294.1	84.3	366	351.8	100.8	426	409.5	117.4	486	467.2	133.9	546	524.9	150.4
307	295.1	84.6	367	352.8	101.1	427	410.4	117.7	487	468.1	134.2	547	525.9	150.7
308	296.0	84.9	368	353.7	101.4	428	411.4	117.9	488	469.1	134.5	548	526.8	151.0
309	297.0	85.1	369	354.7	101.7	429	412.4	118.2	489	470.1	134.8	549	527.8	151.3
310	298.0	85.4	370	355.6	101.9	430	413.3	118.5	490	471.0	135.0	550	528.7	151.6
311	298.9	85.7	371	356.6	102.2	431	414.3	118.8	491	472.0	135.3	551	529.7	151.9
312	299.9	86.0	372	357.6	102.5	432	415.2	119.0	492	472.9	135.6	552	530.6	152.2
313	300.9	86.2	373	358.5	102.8	433	416.2	119.3	493	473.9	135.9	553	531.6	152.5
314	301.8	86.5	374	359.5	103.1	434	417.2	119.6	494	474.9	136.2	554	532.6	152.8
315	302.8	86.8	375	360.4	103.3	435	418.1	119.9	495	475.8	136.4	555	533.5	153.0
316	303.7	87.1	376	361.4	103.6	436	419.1	120.1	496	476.8	136.7	556	534.5	153.2
317	304.7	87.3	377	362.4	103.9	437	420.0	120.4	497	477.7	137.0	557	535.4	153.5
318	305.7	87.6	378	363.3	104.2	438	421.0	120.7	498	478.7	137.3	558	536.4	153.8
319	306.6	87.9	379	364.3	104.4	439	422.0	121.0	499	479.7	137.5	559	537.4	154.1
320	307.6	88.2	380	365.3	104.7	440	422.9	121.2	500	480.6	137.8	560	538.3	154.4
321	308.5	88.4	381	366.2	105.0	441	423.9	121.5	501	481.6	138.1	561	539.3	154.7
322	309.5	88.7	382	367.2	105.3	442	424.9	121.8	502	482.6	138.3	562	540.3	154.9
323	310.5	89.0	383	368.1	105.5	443	425.8	122.1	503	483.5	138.6	563	541.2	155.2
324	311.4	89.3	384	369.1	105.8	444	426.8	122.3	504	484.5	138.9	564	542.2	155.4
325	312.4	89.5	385	370.1	106.1	445	427.7	122.6	505	485.4	139.2	565	543.1	155.7
326	313.3	89.8	386	371.0	106.4	446	428.7	122.9	506	486.4	139.4	566	544.1	156.0
327	314.3	90.1	387	372.0	106.6	447	429.7	123.2	507	487.3	139.7	567	545.1	156.3
328	315.3	90.4	388	372.9	106.9	448	430.6	123.4	508	488.3	140.0	568	546.0	156.6
329	316.2	90.6	389	373.9	107.2	449	431.6	123.7	509	489.3	140.3	569	547.0	156.9
330	317.2	90.9	390	374.9	107.5	450	432.6	124.0	510	490.2	140.6	570	547.9	157.1
331	318.2	91.2	391	375.8	107.7	451	433.5	124.3	511	491.2	140.8	571	548.9	157.3
332	319.1	91.5	392	376.8	108.0	452	434.5	124.6	512	492.1	141.1	572	549.8	157.6
333	320.1	91.8	393	377.8	108.3	453	435.4	124.8	513	493.1	141.4	573	550.8	157.9
334	321.0	92.0	394	378.7	108.6	454	436.4	125.1	514	494.1	141.7	574	551.8	158.2
335	322.0	92.3	395	379.7	108.8	455	437.4	125.4	515	495.0	141.9	575	552.7	158.4
336	323.0	92.6	396	380.6	109.1	456	438.3	125.7	516	496.0	142.2	576	553.7	158.7
337	323.9	92.9	397	381.6	109.4	457	439.3	125.9	517	496.9	142.5	577	554.6	159.0
338	324.9	93.1	398	382.6	109.7	458	440.2	126.2	518	497.9	142.8	578	555.6	159.3
339	325.8	93.4	399	383.5	109.9	459	441.2	126.5	519	498.9	143.0	579	556.5	159.5
340	326.8	93.7	400	384.5	110.2	460	442.2	126.8	520	499.8	143.3	580	557.5	159.8
341	327.8	94.0	401	385.4	110.5	461	443.1	127.0	521	500.8	143.6	581	558.4	160.1
342	328.7	94.2	402	386.4	110.8	462	444.1	127.3	522	501.7	143.9	582	559.4	160.4
343	329.7	94.5	403	387.4	111.0	463	445.0	127.6	523	502.7	144.1	583	560.4	160.6
344	330.7	94.8	404	388.3	111.3	464	446.0	127.9	524	503.7	144.4	584	561.3	161.0
345	331.6	95.1	405	389.3	111.6	465	447.0	128.1	525	504.6	144.7	585	562.3	161.3
346	332.6	95.3	406	390.2	111.9	466	447.9	128.4	526	505.6	145.0	586	563.2	161.6
347	333.5	95.6	407	391.2	112.1	467	448.9	128.7	527	506.6	145.3	587	564.2	161.8
348	334.5	95.9	408	392.2	112.4	468	449.8	129.0	528	507.5	145.6	588	565.2	162.1
349	335.5	96.2	409	393.1	112.7	469	450.8	129.2	529	508.5	145.8	589	566.1	162.4
350	336.4	96.4	410	394.1	113.0	470	451.8	129.5	530	509.4	146.1	590	567.1	162.7
351	337.4	96.7	411	395.1	113.3	471	452.7	129.8	531	510.4	146.4	591	568.1	162.9
352	338.3	97.0	412	396.0	113.5	472	453.7	130.1	532	511.4	146.7	592	569.0	163.2
353	339.3	97.3	413	397.0	113.8	473	454.7	130.3	533	512.3	146.9	593	570.0	163.5
354	340.3	97.5	414	397.9	114.1	474	455.6	130.6	534	513.3	147.2	594	571.0	163.8
355	341.2	97.8	415	398.9	114.4	475	456.6	130.9	535	514.3	147.5	595	571.9	164.0
356	342.2	98.1	416	399.9	114.6	476	457.5	131.2	536	515.2	147.8	596	572.9	164.3
357	343.1	98.4	417	400.8	114.9	477	458.5	131.4	537	516.2	148.0	597	573.9	164.6
358	344.1	98.6	418	401.8	115.2	478	459.5	131.7	538	517.2	148.2	598	574.8	164.9
359	345.1	98.9	419	402.7	115.5	479	460.4	132.0	539	518.1	148.5	599	575.8	165.1
360	346.0	99.2	420	403.7	115.8	480	461.4	132.3	540	519.1	148.8	600	576.8	165.4
74°									4 ^h 56 ^m					
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

465

TRAVERSE TABLE TO DEGREES														
17°									1 ^h 8 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	287.8	88.0	361	345.2	105.5	421	402.6	123.1	481	460.0	140.6	541	517.3	158.2
302	288.8	88.3	362	346.1	105.8	422	403.5	123.4	482	460.9	140.9	542	518.3	158.5
303	289.7	88.6	363	347.1	106.1	423	404.5	123.7	483	461.9	141.2	543	519.2	158.8
304	290.7	88.9	364	348.1	106.4	424	405.4	124.0	484	462.8	141.5	544	520.2	159.1
305	291.6	89.2	365	349.0	106.7	425	406.4	124.3	485	463.8	141.8	545	521.2	159.3
306	292.6	89.5	366	350.0	107.0	426	407.3	124.6	486	464.7	142.1	546	522.1	159.6
307	293.5	89.8	367	350.9	107.3	427	408.3	124.8	487	465.7	142.3	547	523.1	159.9
308	294.5	90.1	368	351.9	107.6	428	409.3	125.1	488	466.7	142.6	548	524.0	160.2
309	295.5	90.3	369	352.8	107.9	429	410.2	125.4	489	467.6	142.9	549	525.0	160.5
310	296.4	90.6	370	353.8	108.2	430	411.2	125.7	490	468.6	143.2	550	526.0	160.8
311	297.4	90.9	371	354.8	108.5	431	412.1	126.0	491	469.5	143.5	551	526.9	161.1
312	298.3	91.2	372	355.7	108.8	432	413.1	126.3	492	470.5	143.8	552	527.9	161.4
313	299.3	91.5	373	356.7	109.1	433	414.0	126.6	493	471.4	144.1	553	528.8	161.7
314	300.2	91.8	374	357.6	109.4	434	415.0	126.9	494	472.4	144.4	554	529.8	162.0
315	301.2	92.1	375	358.6	109.6	435	416.0	127.2	495	473.4	144.7	555	530.8	162.3
316	302.2	92.4	376	359.5	109.9	436	416.9	127.5	496	474.3	145.0	556	531.7	162.6
317	303.1	92.7	377	360.5	110.2	437	417.9	127.8	497	475.3	145.3	557	532.7	162.9
318	304.1	93.0	378	361.4	110.5	438	418.8	128.1	498	476.2	145.6	558	533.6	163.2
319	305.0	93.3	379	362.4	110.8	439	419.8	128.4	499	477.2	145.9	559	534.6	163.5
320	306.0	93.6	380	363.4	111.1	440	420.7	128.6	500	478.1	146.2	560	535.5	163.8
321	306.9	93.9	381	364.3	111.4	441	421.7	128.9	501	479.1	146.5	561	536.5	164.1
322	307.9	94.1	382	365.3	111.7	442	422.7	129.2	502	480.1	146.8	562	537.5	164.4
323	308.8	94.4	383	366.2	112.0	443	423.6	129.5	503	481.0	147.1	563	538.4	164.6
324	309.8	94.7	384	367.2	112.3	444	424.6	129.8	504	482.0	147.4	564	539.4	164.8
325	310.8	95.0	385	368.1	112.6	445	425.5	130.1	505	482.9	147.7	565	540.3	165.1
326	311.7	95.3	386	369.1	112.9	446	426.5	130.4	506	483.9	148.0	566	541.3	165.4
327	312.7	95.6	387	370.1	113.2	447	427.4	130.7	507	484.8	148.3	567	542.2	165.7
328	313.6	95.9	388	371.0	113.4	448	428.4	131.0	508	485.8	148.6	568	543.2	166.0
329	314.6	96.2	389	372.0	113.7	449	429.3	131.3	509	486.7	148.9	569	544.1	166.4
330	315.5	96.5	390	372.9	114.0	450	430.3	131.6	510	487.7	149.1	570	545.1	166.7
331	316.5	96.8	391	373.9	114.3	451	431.3	131.9	511	488.7	149.4	571	546.1	167.0
332	317.5	97.1	392	374.8	114.6	452	432.2	132.2	512	489.6	149.7	572	547.0	167.2
333	318.4	97.4	393	375.8	114.9	453	433.2	132.4	513	490.6	150.0	573	548.0	167.5
334	319.4	97.7	394	376.7	115.2	454	434.1	132.7	514	491.5	150.2	574	548.9	167.8
335	320.3	97.9	395	377.7	115.5	455	435.1	133.0	515	492.5	150.5	575	549.9	168.1
336	321.3	98.2	396	378.7	115.8	456	436.0	133.3	516	493.4	150.8	576	550.8	168.4
337	322.2	98.5	397	379.6	116.1	457	437.0	133.6	517	494.4	151.1	577	551.8	168.7
338	323.2	98.8	398	380.6	116.4	458	438.0	133.9	518	495.3	151.4	578	552.7	169.0
339	324.2	99.1	399	381.5	116.7	459	438.9	134.2	519	496.3	151.7	579	553.7	169.3
340	325.1	99.4	400	382.5	117.0	460	439.9	134.5	520	497.2	152.0	580	554.6	169.6
341	326.1	99.7	401	383.4	117.2	461	440.8	134.8	521	498.2	152.3	581	555.6	169.9
342	327.0	100.0	402	384.4	117.5	462	441.8	135.1	522	499.2	152.6	582	556.5	170.2
343	328.0	100.3	403	385.4	117.8	463	442.7	135.4	523	500.1	152.9	583	557.5	170.5
344	328.9	100.6	404	386.3	118.1	464	443.7	135.7	524	501.1	153.2	584	558.4	170.8
345	329.9	100.9	405	387.3	118.4	465	444.6	136.0	525	502.0	153.5	585	559.4	171.1
346	330.8	101.2	406	388.2	118.7	466	445.6	136.2	526	503.0	153.8	586	560.4	171.3
347	331.8	101.5	407	389.2	119.0	467	446.6	136.5	527	503.9	154.1	587	561.3	171.6
348	332.8	101.8	408	390.1	119.3	468	447.5	136.8	528	504.9	154.4	588	562.3	171.9
349	333.7	102.0	409	391.1	119.6	469	448.5	137.1	529	505.9	154.7	589	563.2	172.2
350	334.7	102.3	410	392.0	119.9	470	449.4	137.4	530	506.8	155.0	590	564.2	172.5
351	335.6	102.6	411	393.0	120.2	471	450.4	137.7	531	507.8	155.3	591	565.1	172.8
352	336.6	102.9	412	394.0	120.5	472	451.3	138.0	532	508.7	155.6	592	566.1	173.1
353	337.5	103.2	413	394.9	120.8	473	452.3	138.3	533	509.7	155.9	593	567.1	173.4
354	338.5	103.5	414	395.9	121.0	474	453.3	138.6	534	510.6	156.2	594	568.0	173.7
355	339.5	103.8	415	396.8	121.3	475	454.2	138.9	535	511.6	156.5	595	569.0	174.0
356	340.4	104.1	416	397.8	121.6	476	455.2	139.2	536	512.6	156.8	596	569.9	174.3
357	341.4	104.4	417	398.7	121.9	477	456.1	139.5	537	513.5	157.1	597	570.9	174.6
358	342.3	104.7	418	399.7	122.2	478	457.1	139.8	538	514.5	157.3	598	571.8	174.9
359	343.3	105.0	419	400.7	122.5	479	458.0	140.0	539	515.4	157.6	599	572.8	175.2
360	344.2	105.3	420	401.6	122.8	480	459.0	140.3	540	516.4	157.9	600	573.8	175.4
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

78°

4^h 52^m

H H

TRAVERSE TABLE TO DEGREES														
18°									1 ^h 12 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	1°0	0°3	61	58°0	18°9	121	115°1	37°4	181	172°1	55°9	241	229°2	74°5
2	1°9	0°6	62	59°0	19°2	122	116°0	37°7	182	173°1	56°2	242	230°2	74°8
3	2°9	0°9	63	59°9	19°5	123	117°0	38°0	183	174°0	56°6	243	231°1	75°1
4	3°8	1°2	64	60°9	19°8	124	117°9	38°3	184	175°0	56°9	244	232°1	75°4
5	4°8	1°5	65	61°8	20°1	125	118°9	38°6	185	175°9	57°2	245	233°0	75°7
6	5°7	1°9	66	62°8	20°4	126	119°8	38°9	186	176°9	57°5	246	234°0	76°0
7	6°7	2°2	67	63°7	20°7	127	120°8	39°2	187	177°8	57°8	247	234°9	76°3
8	7°6	2°5	68	64°7	21°0	128	121°7	39°6	188	178°8	58°1	248	235°9	76°6
9	8°6	2°8	69	65°6	21°3	129	122°7	39°9	189	179°7	58°4	249	236°8	76°9
10	9°5	3°1	70	66°6	21°6	130	123°6	40°2	190	180°7	58°7	250	237°8	77°3
11	10°5	3°4	71	67°5	21°9	131	124°6	40°5	191	181°7	59°0	251	238°7	77°6
12	11°4	3°7	72	68°5	22°2	132	125°5	40°8	192	182°6	59°3	252	239°7	77°9
13	12°4	4°0	73	69°4	22°6	133	126°5	41°1	193	183°6	59°6	253	240°6	78°2
14	13°3	4°3	74	70°4	22°9	134	127°4	41°4	194	184°5	59°9	254	241°6	78°5
15	14°3	4°6	75	71°3	23°2	135	128°4	41°7	195	185°5	60°3	255	242°5	78°8
16	15°2	4°9	76	72°3	23°5	136	129°3	42°0	196	186°4	60°6	256	243°5	79°1
17	16°2	5°3	77	73°2	23°8	137	130°3	42°3	197	187°4	60°9	257	244°4	79°4
18	17°1	5°6	78	74°2	24°1	138	131°3	42°6	198	188°3	61°2	258	245°4	79°7
19	18°1	5°9	79	75°1	24°4	139	132°2	43°0	199	189°3	61°5	259	246°3	80°0
20	19°0	6°2	80	76°1	24°7	140	133°1	43°3	200	190°2	61°8	260	247°3	80°3
21	20°0	6°5	81	77°0	25°0	141	134°1	43°6	201	191°2	62°1	261	248°2	80°7
22	20°9	6°8	82	78°0	25°3	142	135°1	43°9	202	192°1	62°4	262	249°2	81°0
23	21°9	7°1	83	78°9	25°6	143	136°0	44°2	203	193°1	62°7	263	250°1	81°3
24	22°8	7°4	84	79°9	26°0	144	137°0	44°5	204	194°0	63°0	264	251°1	81°6
25	23°8	7°7	85	80°8	26°3	145	137°9	44°8	205	195°0	63°3	265	252°0	81°9
26	24°7	8°0	86	81°8	26°6	146	138°9	45°1	206	195°9	63°7	266	253°0	82°2
27	25°7	8°3	87	82°7	26°9	147	139°8	45°4	207	196°9	64°0	267	253°9	82°5
28	26°6	8°7	88	83°7	27°2	148	140°8	45°7	208	197°8	64°3	268	254°9	82°8
29	27°6	9°0	89	84°6	27°5	149	141°7	46°0	209	198°8	64°6	269	255°8	83°1
30	28°5	9°3	90	85°6	27°8	150	142°7	46°4	210	199°7	64°9	270	256°8	83°4
31	29°5	9°6	91	86°5	28°1	151	143°6	46°7	211	200°7	65°2	271	257°7	83°7
32	30°4	9°9	92	87°5	28°4	152	144°6	47°0	212	201°6	65°5	272	258°7	84°1
33	31°4	10°2	93	88°4	28°7	153	145°5	47°3	213	202°6	65°8	273	259°6	84°4
34	32°3	10°5	94	89°4	29°0	154	146°5	47°6	214	203°5	66°1	274	260°6	84°7
35	33°3	10°8	95	90°4	29°4	155	147°4	47°9	215	204°5	66°4	275	261°5	85°0
36	34°2	11°1	96	91°3	29°7	156	148°4	48°2	216	205°4	66°7	276	262°5	85°3
37	35°2	11°4	97	92°3	30°0	157	149°3	48°5	217	206°4	67°1	277	263°4	85°6
38	36°1	11°7	98	93°2	30°3	158	150°3	48°8	218	207°3	67°4	278	264°4	85°9
39	37°1	12°1	99	94°2	30°6	159	151°2	49°1	219	208°3	67°7	279	265°3	86°2
40	38°0	12°4	100	95°1	30°9	160	152°2	49°4	220	209°2	68°0	280	266°3	86°5
41	39°0	12°7	101	96°1	31°2	161	153°1	49°8	221	210°2	68°3	281	267°2	86°8
42	39°9	13°0	102	97°0	31°5	162	154°1	50°1	222	211°1	68°6	282	268°2	87°1
43	40°9	13°3	103	98°0	31°8	163	155°0	50°4	223	212°1	68°9	283	269°1	87°5
44	41°8	13°6	104	98°9	32°1	164	156°0	50°7	224	213°0	69°2	284	270°1	87°8
45	42°8	13°9	105	99°9	32°4	165	156°9	51°0	225	214°0	69°5	285	271°1	88°1
46	43°7	14°2	106	100°8	32°8	166	157°9	51°3	226	214°9	69°8	286	272°0	88°4
47	44°7	14°5	107	101°8	33°1	167	158°8	51°6	227	215°9	70°1	287	273°0	88°7
48	45°7	14°8	108	102°7	33°4	168	159°8	51°9	228	216°8	70°5	288	273°9	89°0
49	46°6	15°1	109	103°7	33°7	169	160°7	52°2	229	217°8	70°8	289	274°9	89°3
50	47°6	15°5	110	104°6	34°0	170	161°7	52°5	230	218°7	71°1	290	275°8	89°6
51	48°5	15°8	111	105°6	34°3	171	162°6	52°8	231	219°7	71°4	291	276°8	89°9
52	49°5	16°1	112	106°5	34°6	172	163°6	53°2	232	220°6	71°7	292	277°7	90°2
53	50°4	16°4	113	107°5	34°9	173	164°5	53°5	233	221°6	72°0	293	278°7	90°5
54	51°4	16°7	114	108°4	35°2	174	165°5	53°8	234	222°5	72°3	294	279°6	90°9
55	52°3	17°0	115	109°4	35°5	175	166°4	54°1	235	223°5	72°6	295	280°6	91°2
56	53°3	17°3	116	110°3	35°8	176	167°4	54°4	236	224°4	72°9	296	281°5	91°5
57	54°2	17°6	117	111°3	36°2	177	168°3	54°7	237	225°4	73°2	297	282°5	91°8
58	55°2	17°9	118	112°2	36°5	178	169°3	55°0	238	226°4	73°5	298	283°4	92°1
59	56°1	18°2	119	113°2	36°8	179	170°2	55°3	239	227°3	73°9	299	284°4	92°4
60	57°1	18°5	120	114°1	37°1	180	171°2	55°6	240	228°3	74°2	300	285°3	92°7
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE I

467

TRAVERSE TABLE TO DEGREES														
18°									1 ^h 12 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	286.3	93.0	361	343.3	111.6	421	400.4	130.1	481	457.5	148.6	541	514.5	167.2
302	287.2	93.7	362	344.3	111.9	422	401.4	130.4	482	458.5	148.9	542	515.5	167.5
303	288.2	94.7	363	345.2	112.2	423	402.3	130.7	483	459.4	149.3	543	516.4	167.9
304	289.1	94.0	364	346.2	112.5	424	403.3	131.0	484	460.4	149.6	544	517.4	168.2
305	290.1	94.3	365	347.1	112.8	425	404.2	131.3	485	461.3	149.9	545	518.3	168.5
306	291.0	94.6	366	348.1	113.1	426	405.2	131.7	486	462.3	150.2	546	519.3	168.8
307	292.0	94.9	367	349.0	113.4	427	406.1	132.0	487	463.2	150.5	547	520.2	169.1
308	292.9	95.2	368	350.0	113.7	428	407.1	132.3	488	464.2	150.8	548	521.2	169.4
309	293.9	95.5	369	350.9	114.0	429	408.0	132.6	489	465.1	151.1	549	522.1	169.7
310	294.8	95.8	370	351.9	114.3	430	409.0	132.9	490	466.1	151.4	550	523.1	170.0
311	295.8	96.1	371	352.9	114.7	431	409.9	133.2	491	467.0	151.7	551	524.0	170.3
312	296.7	96.4	372	353.8	115.0	432	410.9	133.5	492	468.0	152.0	552	525.0	170.6
313	297.7	96.7	373	354.8	115.3	433	411.8	133.8	493	468.9	152.3	553	525.9	170.9
314	298.6	97.0	374	355.7	115.6	434	412.8	134.1	494	469.8	152.6	554	526.9	171.2
315	299.6	97.4	375	356.7	115.9	435	413.7	134.4	495	470.8	153.0	555	527.8	171.5
316	300.5	97.7	376	357.6	116.2	436	414.7	134.7	496	471.7	153.3	556	528.8	171.8
317	301.5	98.0	377	358.6	116.5	437	415.6	135.1	497	472.7	153.6	557	529.7	172.1
318	302.4	98.3	378	359.5	116.8	438	416.6	135.4	498	473.6	153.9	558	530.7	172.4
319	303.4	98.6	379	360.5	117.1	439	417.5	135.7	499	474.6	154.2	559	531.6	172.7
320	304.3	98.9	380	361.4	117.4	440	418.5	136.0	500	475.5	154.5	560	532.6	173.0
321	305.3	99.2	381	362.4	117.7	441	419.4	136.3	501	476.5	154.8	561	533.5	173.3
322	306.2	99.5	382	363.3	118.1	442	420.4	136.6	502	477.4	155.1	562	534.5	173.6
323	307.2	99.8	383	364.3	118.4	443	421.3	136.9	503	478.4	155.4	563	535.4	173.9
324	308.2	100.1	384	365.2	118.7	444	422.3	137.2	504	479.3	155.7	564	536.4	174.2
325	309.1	100.4	385	366.2	119.0	445	423.2	137.5	505	480.3	156.0	565	537.3	174.6
326	310.1	100.7	386	367.1	119.3	446	424.2	137.8	506	481.2	156.4	566	538.3	174.9
327	311.0	101.1	387	368.1	119.6	447	425.1	138.1	507	482.2	156.7	567	539.2	175.2
328	312.0	101.4	388	369.0	119.9	448	426.1	138.4	508	483.2	157.0	568	540.2	175.5
329	312.9	101.7	389	370.0	120.2	449	427.0	138.8	509	484.1	157.3	569	541.1	175.8
330	313.9	102.0	390	370.9	120.5	450	428.0	139.1	510	485.1	157.6	570	542.1	176.1
331	314.8	102.3	391	371.9	120.8	451	428.9	139.4	511	486.0	157.9	571	543.0	176.4
332	315.8	102.6	392	372.8	121.1	452	429.9	139.7	512	487.0	158.2	572	544.0	176.7
333	316.7	102.9	393	373.8	121.5	453	430.8	140.0	513	487.9	158.5	573	544.9	177.0
334	317.7	103.2	394	374.7	121.8	454	431.8	140.3	514	488.9	158.8	574	545.9	177.3
335	318.6	103.5	395	375.7	122.1	455	432.7	140.6	515	489.8	159.1	575	546.8	177.6
336	319.6	103.8	396	376.6	122.4	456	433.7	140.9	516	490.8	159.4	576	547.8	178.0
337	320.5	104.1	397	377.6	122.7	457	434.6	141.2	517	491.7	159.7	577	548.7	178.3
338	321.5	104.5	398	378.5	123.0	458	435.6	141.5	518	492.7	160.0	578	549.7	178.6
339	322.4	104.8	399	379.5	123.3	459	436.5	141.8	519	493.6	160.3	579	550.6	178.9
340	323.4	105.1	400	380.4	123.6	460	437.5	142.2	520	494.6	160.7	580	551.6	179.2
341	324.3	105.4	401	381.4	123.9	461	438.4	142.5	521	495.5	161.0	581	552.5	179.5
342	325.3	105.7	402	382.3	124.2	462	439.4	142.8	522	496.5	161.3	582	553.5	179.8
343	326.2	106.0	403	383.3	124.5	463	440.3	143.1	523	497.4	161.6	583	554.4	180.1
344	327.2	106.3	404	384.2	124.9	464	441.3	143.4	524	498.4	161.9	584	555.4	180.4
345	328.1	106.6	405	385.2	125.2	465	442.2	143.7	525	499.3	162.2	585	556.3	180.7
346	329.1	106.9	406	386.1	125.5	466	443.2	144.0	526	500.3	162.5	586	557.3	181.1
347	330.0	107.2	407	387.1	125.8	467	444.2	144.3	527	501.2	162.9	587	558.2	181.4
348	331.0	107.5	408	388.0	126.1	468	445.1	144.6	528	502.2	163.2	588	559.2	181.7
349	331.9	107.9	409	389.0	126.4	469	446.1	144.9	529	503.1	163.5	589	560.1	182.0
350	332.9	108.2	410	389.9	126.7	470	447.0	145.2	530	504.1	163.8	590	561.1	182.3
351	333.8	108.5	411	390.9	127.0	471	448.0	145.6	531	505.0	164.1	591	562.0	182.7
352	334.8	108.8	412	391.8	127.3	472	448.9	145.9	532	506.0	164.4	592	563.0	183.0
353	335.7	109.1	413	392.8	127.6	473	449.9	146.2	533	506.9	164.7	593	563.9	183.3
354	336.7	109.4	414	393.7	127.9	474	450.8	146.5	534	507.9	165.0	594	564.9	183.6
355	337.6	109.7	415	394.7	128.3	475	451.8	146.8	535	508.8	165.3	595	565.8	183.9
356	338.6	110.0	416	395.6	128.6	476	452.7	147.1	536	509.8	165.6	596	566.8	184.2
357	339.5	110.3	417	396.6	128.9	477	453.7	147.4	537	510.7	165.9	597	567.7	184.5
358	340.5	110.6	418	397.5	129.2	478	454.6	147.7	538	511.7	166.2	598	568.7	184.8
359	341.4	110.9	419	398.5	129.5	479	455.6	148.0	539	512.6	166.5	599	569.6	185.1
360	342.4	111.3	420	399.5	129.8	480	456.5	148.3	540	513.6	166.9	600	570.6	185.4
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
72°									4 ^h 48 ^m					

TABLE 1

TRAVERSE TABLE TO DEGREES

19°												1° 16"		
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0°9	0°3	61	57°7	19°9	121	114°4	39°4	181	171°1	58°9	241	227°9	78°5
2	1°9	0°7	62	58°6	20°2	122	115°4	39°7	182	172°1	59°3	242	228°8	78°8
3	2°8	1°0	63	59°6	20°5	123	116°3	40°0	183	173°0	59°6	243	229°8	79°1
4	3°8	1°3	64	60°5	20°8	124	117°2	40°4	184	174°0	59°9	244	230°7	79°4
5	4°7	1°6	65	61°5	21°2	125	118°2	40°7	185	174°9	60°2	245	231°7	79°8
6	5°7	2°0	66	62°4	21°5	126	119°1	41°0	186	175°9	60°6	246	232°6	80°1
7	6°6	2°3	67	63°3	21°8	127	120°1	41°3	187	176°8	60°9	247	233°5	80°4
8	7°6	2°6	68	64°3	22°1	128	121°0	41°7	188	177°8	61°2	248	234°5	80°7
9	8°5	2°9	69	65°2	22°5	129	122°0	42°0	189	178°7	61°5	249	235°4	81°1
10	9°5	3°3	70	66°2	22°8	130	122°9	42°3	190	179°6	61°9	250	236°4	81°4
11	10°4	3°6	71	67°1	23°1	131	123°9	42°6	191	180°6	62°2	251	237°3	81°7
12	11°3	3°9	72	68°1	23°4	132	124°8	43°0	192	181°5	62°5	252	238°3	82°0
13	12°3	4°2	73	69°0	23°8	133	125°8	43°3	193	182°5	62°8	253	239°2	82°4
14	13°2	4°6	74	70°0	24°1	134	126°7	43°6	194	183°4	63°2	254	240°2	82°7
15	14°2	4°9	75	70°9	24°4	135	127°6	44°0	195	184°4	63°5	255	241°1	83°0
16	15°1	5°2	76	71°9	24°7	136	128°6	44°3	196	185°3	63°8	256	242°1	83°3
17	16°1	5°5	77	72°8	25°1	137	129°5	44°6	197	186°3	64°1	257	243°0	83°7
18	17°0	5°9	78	73°8	25°4	138	130°5	44°9	198	187°2	64°5	258	243°9	84°0
19	18°0	6°2	79	74°7	25°7	139	131°4	45°3	199	188°2	64°8	259	244°9	84°3
20	18°9	6°5	80	75°6	26°0	140	132°4	45°6	200	189°1	65°1	260	245°8	84°6
21	19°9	6°8	81	76°6	26°4	141	133°3	45°9	201	190°0	65°4	261	246°8	85°0
22	20°8	7°2	82	77°5	26°7	142	134°3	46°2	202	191°0	65°8	262	247°7	85°3
23	21°7	7°5	83	78°5	27°0	143	135°2	46°6	203	191°9	66°1	263	248°7	85°6
24	22°7	7°8	84	79°4	27°3	144	136°2	46°9	204	192°9	66°4	264	249°6	86°0
25	23°6	8°1	85	80°4	27°7	145	137°1	47°2	205	193°8	66°7	265	250°6	86°3
26	24°6	8°5	86	81°3	28°0	146	138°0	47°5	206	194°8	67°1	266	251°5	86°6
27	25°5	8°8	87	82°3	28°3	147	139°0	47°9	207	195°7	67°4	267	252°5	86°9
28	26°5	9°1	88	83°2	28°6	148	139°9	48°2	208	196°7	67°7	268	253°4	87°3
29	27°4	9°4	89	84°2	29°0	149	140°9	48°5	209	197°6	68°0	269	254°3	87°6
30	28°3	9°8	90	85°1	29°									

469

TRAVERSE TABLE TO DEGREES														
19°									1h 16m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
801	284.6	98.0	861	341.3	117.5	421	398.1	137.0	481	454.8	156.6	541	511.5	176.1
802	285.5	98.3	862	342.3	117.8	422	399.0	137.4	482	455.7	156.9	542	512.4	176.4
803	286.5	98.6	863	343.2	118.2	423	400.0	137.7	483	456.7	157.2	543	513.4	176.8
804	287.4	99.0	864	344.2	118.5	424	400.9	138.0	484	457.6	157.6	544	514.3	177.1
805	288.4	99.3	865	345.1	118.8	425	401.8	138.4	485	458.6	157.9	545	515.3	177.4
806	289.3	99.6	866	346.1	119.1	426	402.8	138.7	486	459.5	158.2	546	516.2	177.7
807	290.3	99.9	867	347.0	119.5	427	403.7	139.0	487	460.5	158.5	547	517.2	178.1
808	291.2	100.3	868	348.0	119.8	428	404.7	139.3	488	461.4	158.9	548	518.1	178.4
809	292.2	100.6	869	348.9	120.1	429	405.6	139.7	489	462.4	159.2	549	519.1	178.7
810	293.1	100.9	870	349.8	120.4	430	406.6	140.0	490	463.3	159.5	550	520.0	179.0
811	294.1	101.2	871	350.8	120.8	431	407.5	140.3	491	464.3	159.8	551	521.0	179.4
812	295.0	101.6	872	351.7	121.1	432	408.5	140.6	492	465.2	160.2	552	521.9	179.7
813	295.9	101.9	873	352.7	121.4	433	409.4	141.0	493	466.1	160.5	553	522.8	180.0
814	296.9	102.2	874	353.6	121.7	434	410.4	141.3	494	467.1	160.8	554	523.8	180.3
815	297.8	102.5	875	354.6	122.1	435	411.3	141.6	495	468.0	161.1	555	524.7	180.7
816	298.8	102.9	876	355.5	122.4	436	412.2	141.9	496	469.0	161.5	556	525.7	181.0
817	299.7	103.2	877	356.5	122.7	437	413.2	142.3	497	469.9	161.8	557	526.6	181.3
818	300.7	103.5	878	357.4	123.0	438	414.1	142.6	498	470.9	162.1	558	527.6	181.6
819	301.6	103.8	879	358.4	123.4	439	415.1	142.9	499	471.8	162.4	559	528.5	182.0
820	302.6	104.2	880	359.3	123.7	440	416.0	143.2	500	472.8	162.8	560	529.5	182.3
821	303.5	104.5	881	360.2	124.0	441	417.0	143.6	501	473.7	163.1	561	530.4	182.6
822	304.5	104.8	882	361.2	124.4	442	417.9	143.9	502	474.7	163.4	562	531.4	182.9
823	305.4	105.1	883	362.1	124.7	443	418.9	144.2	503	475.6	163.7	563	532.3	183.3
824	306.3	105.5	884	363.1	125.0	444	419.8	144.5	504	476.5	164.1	564	533.2	183.6
825	307.3	105.8	885	364.0	125.3	445	420.8	144.9	505	477.5	164.4	565	534.2	183.9
826	308.2	106.1	886	365.0	125.7	446	421.7	145.2	506	478.4	164.7	566	535.1	184.2
827	309.2	106.4	887	365.9	126.0	447	422.6	145.5	507	479.4	165.0	567	536.1	184.6
828														

TABLE 1

TRAVERSE TABLE TO DEGREES														
20°												1 ^h 20 ^m		
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0°9	0°3	61	57°3	20°9	121	113°7	41°4	181	170°1	61°9	241	226°5	82°4
2	1°9	0°7	62	58°3	21°2	122	114°6	41°7	182	171°0	62°2	242	227°4	82°8
3	2°8	1°0	63	59°2	21°5	123	115°6	42°1	183	172°0	62°6	243	228°3	83°1
4	3°8	1°4	64	60°1	21°9	124	116°5	42°4	184	172°9	62°9	244	229°3	83°5
5	4°7	1°7	65	61°1	22°2	125	117°5	42°8	185	173°8	63°3	245	230°2	83°8
6	5°6	2°1	66	62°0	22°6	126	118°4	43°1	186	174°8	63°6	246	231°2	84°1
7	6°6	2°4	67	63°0	22°9	127	119°3	43°4	187	175°7	64°0	247	232°1	84°5
8	7°5	2°7	68	63°9	23°3	128	120°3	43°8	188	176°7	64°3	248	233°0	84°8
9	8°5	3°1	69	64°8	23°6	129	121°2	44°1	189	177°6	64°6	249	234°0	85°2
10	9°4	3°4	70	65°8	23°9	130	122°2	44°5	190	178°5	65°0	250	234°9	85°5
11	10°3	3°8	71	66°7	24°3	131	123°1	44°8	191	179°5	65°3	251	235°9	85°8
12	11°3	4°1	72	67°7	24°6	132	124°0	45°1	192	180°4	65°7	252	236°8	86°2
13	12°2	4°4	73	68°6	25°0	133	125°0	45°5	193	181°4	66°0	253	237°7	86°5
14	13°2	4°8	74	69°5	25°3	134	125°9	45°8	194	182°3	66°4	254	238°7	86°9
15	14°1	5°1	75	70°5	25°7	135	126°9	46°2	195	183°2	66°7	255	239°6	87°2
16	15°0	5°5	76	71°4	26°0	136	127°8	46°5	196	184°2	67°0	256	240°6	87°6
17	16°0	5°8	77	72°4	26°3	137	128°7	46°9	197	185°1	67°4	257	241°5	87°9
18	16°9	6°2	78	73°3	26°7	138	129°7	47°2	198	186°1	67°7	258	242°4	88°2
19	17°9	6°5	79	74°2	27°0	139	130°6	47°5	199	187°0	68°1	259	243°4	88°6
20	18°8	6°8	80	75°2	27°4	140	131°6	47°9	200	187°9	68°4	260	244°3	88°9
21	19°7	7°2	81	76°1	27°7	141	132°5	48°2	201	188°9	68°7	261	245°3	89°3
22	20°7	7°5	82	77°1	28°0	142	133°4	48°6	202	189°8	69°1	262	246°2	89°6
23	21°6	7°9	83	78°0	28°4	143	134°4	48°9	203	190°8	69°4	263	247°1	90°0
24	22°6	8°2	84	78°9	28°7	144	135°3	49°3	204	191°7	69°8	264	248°1	90°3
25	23°5	8°6	85	79°9	29°1	145	136°3	49°6	205	192°6	70°1	265	249°0	90°6
26	24°4	8°9	86	80°8	29°4	146	137°2	49°9	206	193°6	70°5	266	250°0	91°0
27	25°4	9°2	87	81°8	29°8	147	138°1	50°3	207	194°5	70°8	267	250°9	91°3
28	26°3	9°6	88	82°7	30°1	148	139°1	50°6	208	195°5	71°1	268	251°8	91°7
29	27°3	9°9	89	83°6	30°4	149	140°0	51°0	209	196°4	71°5	269	252°8	92°0
30	28°2	10°3	90	84°6	30°8	150	141°0	51°3	210	197°3	71°8	270	253°7	92°3
31	29°1	10°6	91	85°5	31°1	151	141°9	51°6	211	198°3	72°2	271	254°7	92°7
32	30°1	10°9	92	86°5	31°5	152	142°8	52°0	212	199°2	72°5	272	255°6	93°0
33	31°0	11°3	93	87°4	31°8	153	143°8	52°3	213	200°2	72°9	273	256°5	93°4
34	31°9	11°6	94	88°3	32°1	154	144°7	52°7	214	201°1	73°2	274	257°5	93°7
35	32°9	12°0	95	89°3	32°5	155	145°7	53°0	215	202°0	73°5	275	258°4	94°1
36	33°8	12°3	96	90°2	32°8	156	146°6	53°4	216	203°0	73°9	276	259°4	94°4
37	34°8	12°7	97	91°2	33°2	157	147°5	53°7	217	203°9	74°2	277	260°3	94°7
38	35°7	13°0	98	92°1	33°5	158	148°5	54°0	218	204°9	74°6	278	261°2	95°1
39	36°6	13°3	99	93°0	33°9	159	149°4	54°4	219	205°8	74°9	279	262°2	95°4
40	37°6	13°7	100	94°0	34°2	160	150°4	54°7	220	206°7	75°2	280	263°1	95°8
41	38°5	14°0	101	94°9	34°5	161	151°3	55°1	221	207°7	75°6	281	264°1	96°1
42	39°5	14°4	102	95°8	34°9	162	152°2	55°4	222	208°6	75°9	282	265°0	96°4
43	40°4	14°7	103	96°8	35°2	163	153°2	55°7	223	209°6	76°3	283	265°9	96°8
44	41°3	15°0	104	97°7	35°6	164	154°1	56°1	224	210°5	76°6	284	266°9	97°1
45	42°3	15°4	105	98°7	35°9	165	155°0	56°4	225	211°4	77°0	285	267°8	97°5
46	43°2	15°7	106	99°6	36°3	166	156°0	56°8	226	212°4	77°3	286	268°8	97°8
47	44°2	16°1	107	100°5	36°6	167	156°9	57°1	227	213°3	77°6	287	269°7	98°2
48	45°1	16°4	108	101°5	36°9	168	157°9	57°5	228	214°2	78°0	288	270°6	98°5
49	46°0	16°8	109	102°4	37°3	169	158°8	57°8	229	215°2	78°3	289	271°6	98°8
50	47°0	17°1	110	103°4	37°6	170	159°7	58°1	230	216°1	78°7	290	272°5	99°2
51	47°9	17°4	111	104°3	38°0	171	160°7	58°5	231	217°1	79°0	291	273°5	99°5
52	48°9	17°8	112	105°2	38°3	172	161°6	58°8	232	218°0	79°3	292	274°4	99°9
53	49°8	18°1	113	106°2	38°6	173	162°6	59°2	233	218°9	79°7	293	275°3	100°2
54	50°7	18°5	114	107°1	39°0	174	163°5	59°5	234	219°9	80°0	294	276°3	100°6
55	51°7	18°8	115	108°1	39°3	175	164°4	59°9	235	220°8	80°4	295	277°2	100°9
56	52°6	19°2	116	109°0	39°7	176	165°4	60°2	236	221°8	80°7	296	278°1	101°2
57	53°6	19°5	117	109°9	40°0	177	166°3	60°5	237	222°7	81°1	297	279°1	101°6
58	54°5	19°8	118	110°9	40°4	178	167°3	60°9	238	223°6	81°4	298	280°0	101°9
59	55°4	20°2	119	111°8	40°7	179	168°2	61°2	239	224°6	81°7	299	281°0	102°3
60	56°4	20°5	120	112°8	41°0	180	169°1	61°6	240	225°5	82°1	300	281°9	102°6
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
70°												4 ^h 40 ^m		

TABLE 1

471

TRAVERSE TABLE TO DEGREES														
20°										1 ^h 20 ^m				
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	282.9	103.0	361	339.2	123.5	421	395.6	144.0	481	452.0	164.5	541	508.4	185.0
302	283.8	103.3	362	340.2	123.8	422	396.6	144.3	482	453.0	164.8	542	509.3	185.4
303	284.7	103.6	363	341.1	124.2	423	397.5	144.7	483	453.9	165.2	543	510.3	185.7
304	285.7	104.0	364	342.1	124.5	424	398.4	145.0	484	454.8	165.5	544	511.2	186.0
305	286.6	104.3	365	343.0	124.8	425	399.4	145.4	485	455.8	165.9	545	512.1	186.4
306	287.6	104.7	366	343.9	125.2	426	400.3	145.7	486	456.7	166.3	546	513.1	186.8
307	288.5	105.0	367	344.9	125.5	427	401.3	146.1	487	457.7	166.6	547	514.0	187.1
308	289.4	105.4	368	345.8	125.9	428	402.2	146.4	488	458.6	166.9	548	515.0	187.4
309	290.4	105.7	369	346.8	126.2	429	403.1	146.7	489	459.5	167.3	549	515.9	187.8
310	291.3	106.0	370	347.7	126.6	430	404.1	147.1	490	460.5	167.7	550	516.8	188.2
311	292.3	106.4	371	348.6	126.9	431	405.0	147.4	491	461.4	168.0	551	517.8	188.5
312	293.2	106.7	372	349.5	127.2	432	406.0	147.8	492	462.4	168.3	552	518.7	188.8
313	294.1	107.1	373	350.5	127.6	433	406.9	148.1	493	463.3	168.6	553	519.7	189.1
314	295.1	107.4	374	351.5	127.9	434	407.8	148.4	494	464.2	168.9	554	520.6	189.4
315	296.0	107.7	375	352.4	128.3	435	408.8	148.8	495	465.2	169.3	555	521.5	189.8
316	297.0	108.1	376	353.3	128.6	436	409.7	149.1	496	466.1	169.6	556	522.5	190.2
317	297.9	108.4	377	354.3	129.0	437	410.7	149.5	497	467.0	170.0	557	523.4	190.5
318	298.8	108.8	378	355.2	129.3	438	411.6	149.8	498	468.0	170.3	558	524.4	190.8
319	299.8	109.1	379	356.2	129.6	439	412.5	150.2	499	468.9	170.7	559	525.3	191.2
320	300.7	109.5	380	357.1	130.0	440	413.5	150.5	500	469.9	171.0	560	526.2	191.6
321	301.6	109.8	381	358.0	130.3	441	414.4	150.8	501	470.8	171.3	561	527.2	191.9
322	302.6	110.1	382	359.0	130.7	442	415.4	151.2	502	471.7	171.7	562	528.1	192.2
323	303.5	110.5	383	359.9	131.0	443	416.3	151.5	503	472.7	172.0	563	529.0	192.5
324	304.5	110.8	384	360.8	131.3	444	417.2	151.9	504	473.6	172.4	564	530.0	192.9
325	305.4	111.2	385	361.8	131.7	445	418.2	152.2	505	474.5	172.7	565	530.9	193.2
326	306.3	111.5	386	362.7	132.0	446	419.1	152.5	506	475.4	173.0	566	531.8	193.6
327	307.3	111.8	387	363.7	132.4	447	420.0	152.9	507	476.4	173.4	567	532.8	193.9
328	308.2	112.2	388	364.6	132.7	448	421.0	153.2	508	477.3	173.7	568	533.7	194.2
329	309.2	112.5	389	365.5	133.1	449	421.9	153.6	509	478.3	174.1	569	534.7	194.6
330	310.1	112.9	390	366.5	133.4	450	422.9	153.9	510	479.2	174.4	570	535.6	195.0
331	311.0	113.2	391	367.4	133.7	451	423.8	154.3	511	480.2	174.8	571	536.6	195.3
332	312.0	113.6	392	368.4	134.1	452	424.7	154.6	512	481.1	175.1	572	537.5	195.6
333	312.9	113.9	393	369.3	134.4	453	425.7	154.9	513	482.1	175.4	573	538.5	195.9
334	313.9	114.2	394	370.2	134.8	454	426.6	155.3	514	483.0	175.8	574	539.4	196.3
335	314.8	114.6	395	371.2	135.1	455	427.6	155.6	515	484.0	176.1	575	540.3	196.6
336	315.7	114.9	396	372.1	135.4	456	428.5	156.0	516	484.9	176.5	576	541.3	197.0
337	316.7	115.3	397	373.1	135.8	457	429.4	156.3	517	485.8	176.8	577	542.2	197.3
338	317.6	115.6	398	374.0	136.1	458	430.4	156.7	518	486.8	177.2	578	543.2	197.7
339	318.6	116.0	399	374.9	136.5	459	431.3	157.0	519	487.7	177.5	579	544.1	198.0
340	319.5	116.3	400	375.9	136.8	460	432.3	157.4	520	488.7	177.9	580	545.0	198.4
341	320.4	116.6	401	376.8	137.2	461	433.2	157.7	521	489.6	178.2	581	546.0	198.7
342	321.4	117.0	402	377.8	137.5	462	434.1	158.0	522	490.5	178.5	582	546.9	199.0
343	322.3	117.3	403	378.7	137.8	463	435.1	158.4	523	491.5	178.9	583	547.9	199.4
344	323.3	117.7	404	379.6	138.2	464	436.0	158.7	524	492.4	179.2	584	548.8	199.8
345	324.2	118.0	405	380.6	138.5	465	437.0	159.0	525	493.4	179.6	585	549.8	200.1
346	325.1	118.4	406	381.5	138.9	466	437.9	159.4	526	494.3	179.9	586	550.7	200.4
347	326.1	118.7	407	382.5	139.2	467	438.8	159.7	527	495.3	180.2	587	551.7	200.8
348	327.0	119.0	408	383.4	139.6	468	439.8	160.1	528	496.2	180.6	588	552.6	201.2
349	328.0	119.4	409	384.3	139.9	469	440.7	160.4	529	497.1	181.0	589	553.5	201.5
350	328.9	119.7	410	385.3	140.2	470	441.7	160.8	530	498.1	181.3	590	554.4	201.8
351	329.8	120.1	411	386.2	140.6	471	442.6	161.1	531	499.0	181.6	591	555.4	202.1
352	330.8	120.4	412	387.2	140.9	472	443.5	161.4	532	499.9	181.9	592	556.3	202.4
353	331.7	120.7	413	388.1	141.3	473	444.5	161.8	533	500.9	182.2	593	557.3	202.8
354	332.7	121.1	414	389.0	141.6	474	445.4	162.1	534	501.8	182.6	594	558.2	203.2
355	333.6	121.4	415	390.0	141.9	475	446.4	162.5	535	502.7	183.0	595	559.1	203.5
356	334.5	121.8	416	390.9	142.3	476	447.3	162.8	536	503.7	183.3	596	560.0	203.8
357	335.5	122.1	417	391.9	142.6	477	448.2	163.2	537	504.6	183.7	597	561.0	204.2
358	336.4	122.5	418	392.8	143.0	478	449.2	163.5	538	505.5	184.0	598	561.9	204.6
359	337.4	122.8	419	393.7	143.3	479	450.1	163.8	539	506.5	184.3	599	562.9	204.9
360	338.3	123.1	420	394.7	143.7	480	451.1	164.2	540	507.4	184.7	600	563.8	205.2
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
70°										4 ^h 40 ^m				

TRAVERSE TABLE TO DEGREES

21°												1 ^h 24 ^m		
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0.9	0.4	61	56.9	21.9	121	113.0	43.4	181	169.0	64.9	241	225.0	86.4
2	1.9	0.7	62	57.9	22.2	122	113.9	43.7	182	169.9	65.2	242	225.9	86.7
3	2.8	1.1	63	58.8	22.6	123	114.8	44.1	183	170.8	65.6	243	226.9	87.1
4	3.7	1.4	64	59.7	22.9	124	115.8	44.4	184	171.8	65.9	244	227.8	87.4
5	4.7	1.8	65	60.7	23.3	125	116.7	44.8	185	172.7	66.3	245	228.7	87.8
6	5.6	2.2	66	61.6	23.7	126	117.6	45.2	186	173.6	66.7	246	229.7	88.2
7	6.5	2.5	67	62.5	24.0	127	118.6	45.5	187	174.6	67.0	247	230.6	88.5
8	7.5	2.9	68	63.5	24.4	128	119.5	45.9	188	175.5	67.4	248	231.5	88.9
9	8.4	3.2	69	64.4	24.7	129	120.4	46.2	189	176.4	67.7	249	232.5	89.2
10	9.3	3.6	70	65.4	25.1	130	121.4	46.6	190	177.4	68.1	250	233.4	89.6
11	10.3	3.9	71	66.3	25.4	131	122.3	46.9	191	178.3	68.4	251	234.3	90.0
12	11.2	4.3	72	67.2	25.8	132	123.2	47.3	192	179.2	68.8	252	235.3	90.3
13	12.1	4.7	73	68.2	26.2	133	124.2	47.7	193	180.2	69.2	253	236.2	90.7
14	13.1	5.0	74	69.1	26.5	134	125.1	48.0	194	181.1	69.5	254	237.1	91.0
15	14.0	5.4	75	70.0	26.9	135	126.0	48.4	195	182.0	69.9	255	238.1	91.4
16	14.9	5.7	76	71.0	27.2	136	127.0	48.7	196	183.0	70.2	256	239.0	91.7
17	15.9	6.1	77	71.9	27.6	137	127.9	49.1	197	183.9	70.6	257	239.9	92.1
18	16.8	6.5	78	72.8	28.0	138	128.8	49.5	198	184.8	71.0	258	240.9	92.5
19	17.7	6.8	79	73.8	28.3	139	129.8	49.8	199	185.8	71.3	259	241.8	92.8
20	18.7	7.2	80	74.7	28.7	140	130.7	50.2	200	186.7	71.7	260	242.7	93.2
21	19.6	7.5	81	75.6	29.0	141	131.6	50.5	201	187.6	72.0	261	243.7	93.5
22	20.5	7.9	82	76.6	29.4	142	132.6	50.9	202	188.6	72.4	262	244.6	93.9
23	21.5	8.2	83	77.5	29.7	143	133.5	51.2	203	189.5	72.7	263	245.5	94.3
24	22.4	8.6	84	78.4	30.1	144	134.4	51.6	204	190.5	73.1	264	246.5	94.6
25	23.3	9.0	85	79.4	30.5	145	135.4	52.0	205	191.4	73.5	265	247.4	95.0
26	24.3	9.3	86	80.3	30.8	146	136.3	52.3	206	192.3	73.8	266	248.3	95.3
27	25.2	9.7	87	81.2	31.2	147	137.2	52.7	207	193.3	74.2	267	249.3	95.7
28	26.1	10.0	88	82.2	31.5	148	138.2	53.0	208	194.2	74.5	268	250.2	96.0
29	27.1	10.4	89	83.1	31.9	149	139.1	53.4	209	195.1	74.9	269	251.1	96.4
30	28.0	10.8	90	84.0	32.3	150	140.0	53.8	210	196.1	75.3	270	252.1	96.8
31	28.9	11.1	91	85.0	32.6	151	141.0	54.1	211	197.0	75.6	271	253.0	97.1
32	29.9	11.5	92	85.9	33.0	152	141.9	54.5	212	197.9	76.0	272	253.9	97.5
33	30.8	11.8	93	86.8	33.3	153	142.8	54.8	213	198.9	76.3	273	254.9	97.8
34	31.7	12.2	94	87.8	33.7	154	143.8	55.2	214	199.8	76.7	274	255.8	98.2
35	32.7	12.5	95	88.7	34.0	155	144.7	55.5	215	200.7	77.0	275	256.7	98.6
36	33.6	12.9	96	89.6	34.4	156	145.6	55.9	216	201.7	77.4	276	257.7	98.9
37	34.5	13.3	97	90.6	34.8	157	146.6	56.3	217	202.6	77.8	277	258.6	99.3
38	35.5	13.6	98	91.5	35.1	158	147.5	56.6	218	203.5	78.1	278	259.5	99.6
39	36.4	14.0	99	92.4	35.5	159	148.4	57.0	219	204.5	78.5	279	260.5	100.0
40	37.3	14.3	100	93.4	35.8	160	149.4	57.3	220	205.4	78.8	280	261.4	100.3
41	38.3	14.7	101	94.3	36.2	161	150.3	57.7	221	206.3	79.2	281	262.3	100.7
42	39.2	15.1	102	95.2	36.6	162	151.2	58.1	222	207.3	79.6	282	263.3	101.1
43	40.1	15.4	103	96.2	36.9	163	152.2	58.4	223	208.2	79.9	283	264.2	101.4
44	41.1	15.8	104	97.1	37.3	164	153.1	58.8	224	209.1	80.3	284	265.1	101.8
45	42.0	16.1	105	98.0	37.6	165	154.0	59.1	225	210.1	80.6	285	266.1	102.1
46	42.9	16.5	106	99.0	38.0	166	155.0	59.5	226	211.0	81.0	286	267.0	102.5
47	43.9	16.8	107	99.9	38.3	167	155.9	59.8	227	211.9	81.3	287	267.9	102.9
48	44.8	17.2	108	100.8	38.7	168	156.8	60.2	228	212.9	81.7	288	268.9	103.2
49	45.7	17.6	109	101.8	39.1	169	157.8	60.6	229	213.8	82.1	289	269.8	103.6
50	46.7	17.9	110	102.7	39.4	170	158.7	60.9	230	214.7	82.4	290	270.7	103.9
51	47.6	18.3	111	103.6	39.8	171	159.6	61.3	231	215.7	82.8	291	271.7	104.3
52	48.5	18.6	112	104.6	40.1	172	160.6	61.6	232	216.6	83.1	292	272.6	104.6
53	49.5	19.0	113	105.5	40.5	173	161.5	62.0	233	217.5	83.5	293	273.5	105.0
54	50.4	19.4	114	106.4	40.9	174	162.4	62.4	234	218.5	83.9	294	274.5	105.4
55	51.3	19.7	115	107.4	41.2	175	163.4	62.7	235	219.4	84.2	295	275.4	105.7
56	52.3	20.1	116	108.3	41.6	176	164.3	63.1	236	220.3	84.6	296	276.3	106.1
57	53.2	20.4	117	109.2	41.9	177	165.2	63.4	237	221.3	84.9	297	277.3	106.4
58	54.1	20.8	118	110.2	42.3	178	166.2	63.8	238	222.2	85.3	298	278.2	106.8
59	55.1	21.1	119	111.1	42.6	179	167.1	64.1	239	223.1	85.6	299	279.1	107.2
60	56.0	21.5	120	112.0	43.0	180	168.0	64.5	240	224.1	86.0	300	280.1	107.5
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

473

TRAVERSE TABLE TO DEGREES

21°

1^h 24^m

Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	281°0	107.9	361	337°0	129.4	421	393°0	150.9	481	449°0	172.4	541	505°1	193.9
302	281°9	108.2	362	337°9	129.7	422	394°0	151.2	482	450°0	172.7	542	506°0	194.2
303	282°9	108.6	363	338°9	130.1	423	394°9	151.6	483	450°9	173.1	543	507°0	194.6
304	283°8	108.9	364	339°8	130.4	424	395°8	152.0	484	451°8	173.5	544	507°9	195°0
305	284°7	109.3	365	340°7	130.8	425	396°8	152.3	485	452°8	173.8	545	508°8	195°3
306	285°7	109.7	366	341°7	131.2	426	397°7	152.7	486	453°7	174.2	546	509°8	195°7
307	286°6	110°0	367	342°6	131°5	427	398°6	153°0	487	454°6	174°5	547	510°7	196°0
308	287°5	110°4	368	343°5	131°9	428	399°6	153°4	488	455°6	174°9	548	511°6	196°4
309	288°5	110°7	369	344°5	132°2	429	400°5	153°7	489	456°5	175°2	549	512°6	196°8
310	289°4	111°1	370	345°4	132°6	430	401°4	154°1	490	457°4	175°6	550	513°5	197°1
311	290°3	111°5	371	346°3	133°0	431	402°4	154°5	491	458°4	176°0	551	514°4	197°5
312	291°3	111°8	372	347°3	133°3	432	403°3	154°8	492	459°3	176°3	552	515°4	197°8
313	292°2	112°2	373	348°2	133°7	433	404°2	155°2	493	460°2	176°7	553	516°3	198°2
314	293°1	112°5	374	349°1	134°0	434	405°2	155°5	494	461°2	177°0	554	517°2	198°6
315	294°1	112°9	375	350°1	134°4	435	406°1	155°9	495	462°1	177°4	555	518°2	198°9
316	295°0	113°2	376	351°0	134°7	436	407°0	156°3	496	463°0	177°8	556	519°1	199°3
317	295°9	113°6	377	351°9	135°1	437	408°0	156°6	497	464°0	178°1	557	520°0	199°6
318	296°9	114°0	378	352°9	135°5	438	408°9	157°0	498	464°9	178°5	558	521°0	200°0
319	297°8	114°3	379	353°8	135°8	439	409°8	157°3	499	465°8	178°8	559	521°9	200°3
320	298°7	114°7	380	354°7	136°2	440	410°8	157°7	500	466°8	179°2	560	522°8	200°7
321	299°7	115°0	381	355°7	136°5	441	411°7	158°0	501	467°7	179°5	561	523°8	201°0
322	300°6	115°4	382	356°6	136°9	442	412°6	158°4	502	468°6	179°9	562	524°7	201°4
323	301°5	115°8	383	357°5	137°3	443	413°6	158°8	503	469°6	180°3	563	525°6	201°8
324	302°5	116°1	384	358°5	137°6	444	414°5	159°1	504	470°5	180°6	564	526°6	202°1
325	303°4	116°5	385	359°4	138°0	445	415°4	159°5	505	471°5	181°0	565	527°5	202°5
326	304°3	116°8	386	360°3	138°3	446	416°4	159°8	506	472°4	181°3	566	528°4	202°8
327	305°3	117°2	387	361°3	138°7	447	417°3	160°2	507	473°3	181°7	567	529°4	203°2
328	306°2	117°5	388	362°2	139°1	448	418°2	160°5	508	474°3	182°0	568	530°3	203°5
329	307°1	117°9	389	363°1	139°4	449	419°2	160°9	509	475°2	182°4	569	531°2	203°9
330	308°1	118°3	390	364°1	139°8	450	420°1	161°3	510	476°1	182°8	570	532°2	204°3
331	309°0	118°6	391	365°0	140°1	451	421°0	161°6	511	477°1	183°1	571	533°1	204°6
332	309°9	119°0	392	365°9	140°5	452	422°0	162°0	512	478°0	183°5	572	534°0	205°0
333	310°9	119°3	393	366°9	140°8	453	422°9	162°3	513	478°9	183°8	573	535°0	205°4
334	311°8	119°7	394	367°8	141°2	454	423°8	162°7	514	479°9	184°2	574	535°9	205°7
335	312°7	120°1	395	368°7	141°6	455	424°8	163°1	515	480°8	184°6	575	536°8	206°1
336	313°7	120°4	396	369°7	141°9	456	425°7	163°4	516	481°7	184°9	576	537°8	206°4
337	314°6	120°8	397	370°6	142°3	457	426°6	163°8	517	482°7	185°3	577	538°7	206°8
338	315°5	121°1	398	371°5	142°6	458	427°6	164°1	518	483°6	185°6	578	539°6	207°1
339	316°5	121°5	399	372°5	143°0	459	428°5	164°5	519	484°5	186°0	579	540°6	207°5
340	317°4	121°8	400	373°4	143°4	460	429°4	164°9	520	485°5	186°4	580	541°5	207°9
341	318°3	122°2	401	374°3	143°7	461	430°4	165°2	521	486°4	186°7	581	542°4	208°2
342	319°3	122°6	402	375°3	144°1	462	431°3	165°6	522	487°3	187°1	582	543°4	208°6
343	320°2	122°9	403	376°2	144°4	463	432°2	165°9	523	488°3	187°4	583	544°3	208°9
344	321°1	123°2	404	377°1	144°8	464	433°2	166°3	524	489°2	187°8	584	545°2	209°3
345	322°1	123°6	405	378°1	145°1	465	434°1	166°6	525	490°1	188°1	585	546°2	209°6
346	323°0	124°0	406	379°0	145°5	466	435°0	167°0	526	491°1	188°5	586	547°1	210°0
347	323°9	124°4	407	379°9	145°9	467	436°0	167°4	527	492°0	188°9	587	548°0	210°4
348	324°9	124°7	408	380°9	146°2	468	436°9	167°7	528	492°9	189°2	588	549°0	210°7
349	325°8	125°1	409	381°8	146°6	469	437°8	168°1	529	493°9	189°6	589	549°9	211°1
350	326°7	125°4	410	382°7	146°9	470	438°8	168°4	530	494°8	189°9	590	550°8	211°4
351	327°7	125°8	411	383°7	147°3	471	439°7	168°8	531	495°7	190°3	591	551°8	211°8
352	328°6	126°1	412	384°6	147°7	472	440°6	169°2	532	496°7	190°7	592	552°7	212°2
353	329°5	126°5	413	385°5	148°0	473	441°6	169°5	533	497°6	191°0	593	553°6	212°5
354	330°5	126°9	414	386°5	148°4	474	442°5	169°9	534	498°5	191°4	594	554°6	212°9
355	331°4	127°2	415	387°4	148°7	475	443°4	170°2	535	499°5	191°7	595	555°5	213°2
356	332°3	127°6	416	388°4	149°1	476	444°4	170°6	536	500°4	192°1	596	556°4	213°6
357	333°3	127°9	417	389°3	149°4	477	445°3	170°9	537	501°3	192°4	597	557°4	213°9
358	334°2	128°3	418	390°2	149°8	478	446°2	171°3	538	502°3	192°8	598	558°2	214°3
359	335°1	128°7	419	391°2	150°2	479	447°2	171°7	539	503°2	193°2	599	559°2	214°7
360	336°1	129°0	420	392°1	150°5	480	448°1	172°0	540	504°1	193°5	600	560°1	215°0
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

69°

4^h 86^m

TRAVERSE TABLE TO DEGREES														
22°												1 ^h 28 ^m		
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0.9	0.4	61	56.6	22.9	121	112.2	45.3	181	167.8	67.8	241	223.5	90.3
2	1.9	0.7	62	57.5	23.2	122	113.1	45.7	182	168.7	68.2	242	224.4	90.7
3	2.8	1.1	63	58.4	23.6	123	114.0	46.1	183	169.7	68.6	243	225.3	91.0
4	3.7	1.5	64	59.3	24.0	124	115.0	46.5	184	170.6	68.9	244	226.2	91.4
5	4.6	1.9	65	60.3	24.3	125	115.9	46.8	185	171.5	69.3	245	227.2	91.8
6	5.6	2.2	66	61.2	24.7	126	116.8	47.2	186	172.5	69.7	246	228.1	92.2
7	6.5	2.6	67	62.1	25.1	127	117.8	47.6	187	173.4	70.1	247	229.0	92.5
8	7.4	3.0	68	63.0	25.5	128	118.7	47.9	188	174.3	70.4	248	229.9	92.9
9	8.3	3.4	69	64.0	25.8	129	119.6	48.3	189	175.2	70.8	249	230.9	93.3
10	9.3	3.7	70	64.9	26.2	130	120.5	48.7	190	176.2	71.2	250	231.8	93.7
11	10.2	4.1	71	65.8	26.6	131	121.5	49.1	191	177.1	71.5	251	232.7	94.0
12	11.1	4.5	72	66.8	27.0	132	122.4	49.4	192	178.0	71.9	252	233.7	94.4
13	12.1	4.9	73	67.7	27.3	133	123.3	49.8	193	178.9	72.3	253	234.6	94.8
14	13.0	5.2	74	68.6	27.7	134	124.2	50.2	194	179.9	72.7	254	235.5	95.2
15	13.9	5.6	75	69.5	28.1	135	125.2	50.6	195	180.8	73.0	255	236.4	95.5
16	14.8	6.0	76	70.5	28.5	136	126.1	50.9	196	181.7	73.4	256	237.4	95.9
17	15.8	6.4	77	71.4	28.8	137	127.0	51.3	197	182.7	73.8	257	238.3	96.3
18	16.7	6.7	78	72.3	29.2	138	128.0	51.7	198	183.6	74.2	258	239.2	96.6
19	17.6	7.1	79	73.2	29.6	139	128.9	52.1	199	184.5	74.5	259	240.1	97.0
20	18.5	7.5	80	74.2	30.0	140	129.8	52.4	200	185.4	74.9	260	241.1	97.4
21	19.5	7.9	81	75.1	30.3	141	130.7	52.8	201	186.4	75.3	261	242.0	97.8
22	20.4	8.2	82	76.0	30.7	142	131.7	53.2	202	187.3	75.7	262	242.9	98.1
23	21.3	8.6	83	77.0	31.1	143	132.6	53.6	203	188.2	76.0	263	243.8	98.5
24	22.3	9.0	84	77.9	31.5	144	133.5	53.9	204	189.1	76.4	264	244.8	98.9
25	23.2	9.4	85	78.8	31.8	145	134.4	54.3	205	190.1	76.8	265	245.7	99.3
26	24.1	9.7	86	79.7	32.2	146	135.4	54.7	206	191.0	77.2	266	246.6	99.6
27	25.0	10.1	87	80.7	32.6	147	136.3	55.1	207	191.9	77.5	267	247.6	100.0
28	26.0	10.5	88	81.6	33.0	148	137.2	55.4	208	192.9	77.9	268	248.5	100.4
29	26.9	10.9	89	82.5	33.3	149	138.2	55.8	209	193.8	78.3	269	249.4	100.8
30	27.8	11.2	90	83.4	33.7	150	139.1	56.2	210	194.7	78.7	270	250.3	101.1
31	28.7	11.6	91	84.4	34.1	151	140.0	56.6	211	195.6	79.0	271	251.3	101.5
32	29.7	12.0	92	85.3	34.5	152	140.9	56.9	212	196.6	79.4	272	252.2	101.9
33	30.6	12.4	93	86.2	34.8	153	141.9	57.3	213	197.5	79.8	273	253.1	102.3
34	31.5	12.7	94	87.2	35.2	154	142.8	57.7	214	198.4	80.2	274	254.0	102.6
35	32.5	13.1	95	88.1	35.6	155	143.7	58.1	215	199.3	80.5	275	255.0	103.0
36	33.4	13.5	96	89.0	36.0	156	144.6	58.4	216	200.3	80.9	276	255.9	103.4
37	34.3	13.9	97	89.9	36.3	157	145.6	58.8	217	201.2	81.3	277	256.8	103.8
38	35.2	14.2	98	90.9	36.7	158	146.5	59.2	218	202.1	81.7	278	257.8	104.1
39	36.2	14.6	99	91.8	37.1	159	147.4	59.6	219	203.1	82.0	279	258.7	104.5
40	37.1	15.0	100	92.7	37.5	160	148.3	59.9	220	204.0	82.4	280	259.6	104.9
41	38.0	15.4	101	93.6	37.8	161	149.3	60.3	221	204.9	82.8	281	260.5	105.3
42	38.9	15.7	102	94.6	38.2	162	150.2	60.7	222	205.8	83.2	282	261.5	105.6
43	39.9	16.1	103	95.5	38.6	163	151.1	61.1	223	206.8	83.5	283	262.4	106.0
44	40.8	16.5	104	96.4	39.0	164	152.1	61.4	224	207.7	83.9	284	263.3	106.4
45	41.7	16.9	105	97.4	39.3	165	153.0	61.8	225	208.6	84.3	285	264.2	106.8
46	42.7	17.2	106	98.3	39.7	166	153.9	62.2	226	209.5	84.7	286	265.2	107.1
47	43.6	17.6	107	99.2	40.1	167	154.8	62.6	227	210.5	85.0	287	266.1	107.5
48	44.5	18.0	108	100.1	40.5	168	155.8	62.9	228	211.4	85.4	288	267.0	107.9
49	45.4	18.4	109	101.1	40.8	169	156.7	63.3	229	212.3	85.8	289	268.0	108.3
50	46.4	18.7	110	102.0	41.2	170	157.6	63.7	230	213.3	86.2	290	268.9	108.6
51	47.3	19.1	111	102.9	41.6	171	158.5	64.1	231	214.2	86.5	291	269.8	109.0
52	48.2	19.5	112	103.8	42.0	172	159.5	64.4	232	215.1	86.9	292	270.7	109.4
53	49.1	19.9	113	104.8	42.3	173	160.4	64.8	233	216.0	87.3	293	271.7	109.8
54	50.1	20.2	114	105.7	42.7	174	161.3	65.2	234	217.0	87.7	294	272.6	110.1
55	51.0	20.6	115	106.6	43.1	175	162.3	65.6	235	217.9	88.0	295	273.5	110.5
56	51.9	21.0	116	107.6	43.5	176	163.2	65.9	236	218.8	88.4	296	274.4	110.9
57	52.8	21.4	117	108.5	43.8	177	164.1	66.3	237	219.7	88.8	297	275.4	111.3
58	53.8	21.7	118	109.4	44.2	178	165.0	66.7	238	220.7	89.2	298	276.3	111.6
59	54.7	22.1	119	110.3	44.6	179	166.0	67.1	239	221.6	89.5	299	277.2	112.0
60	55.6	22.5	120	111.3	45.0	180	166.9	67.4	240	222.5	89.9	300	278.2	112.4
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
68°												4 ^h 32 ^m		

TABLE 1

475

TRAVERSE TABLE TO DEGREES														
22°									1° 28'					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	279°1	112°7	361	334°7	135°2	421	390°3	157°7	481	446°0	180°2	541	501°6	202°7
302	280°0	113°1	362	335°6	135°6	422	391°3	158°1	482	446°9	180°6	542	502°5	203°1
303	280°9	113°5	363	336°6	136°0	423	392°2	158°4	483	447°8	180°9	543	503°4	203°5
304	281°9	113°9	364	337°5	136°3	424	393°1	158°8	484	448°8	181°3	544	504°4	203°8
305	282°8	114°2	365	338°4	136°7	425	394°1	159°2	485	449°7	181°7	545	505°3	204°2
306	283°7	114°6	366	339°3	137°1	426	395°0	159°6	486	450°6	182°1	546	506°2	204°6
307	284°6	115°0	367	340°3	137°5	427	395°9	159°9	487	451°6	182°4	547	507°2	205°0
308	285°6	115°4	368	341°2	137°8	428	396°8	160°3	488	452°5	182°8	548	508°1	205°3
309	286°5	115°7	369	342°1	138°2	429	397°8	160°7	489	453°4	183°2	549	509°0	205°7
310	287°4	116°1	370	343°1	138°6	430	398°7	161°1	490	454°3	183°6	550	510°0	206°1
311	288°4	116°5	371	344°0	139°0	431	399°6	161°4	491	455°3	184°0	551	510°9	206°5
312	289°3	116°8	372	344°9	139°3	432	400°5	161°8	492	456°2	184°3	552	511°8	206°8
313	290°2	117°2	373	345°8	139°7	433	401°5	162°2	493	457°1	184°7	553	512°7	207°2
314	291°1	117°6	374	346°8	140°1	434	402°4	162°6	494	458°0	185°1	554	513°6	207°6
315	292°1	118°0	375	347°7	140°5	435	403°3	162°9	495	459°0	185°4	555	514°6	208°0
316	293°0	118°3	376	348°6	140°8	436	404°3	163°3	496	459°9	185°8	556	515°5	208°3
317	293°9	118°7	377	349°5	141°2	437	405°2	163°7	497	460°8	186°2	557	516°4	208°7
318	294°8	119°1	378	350°5	141°6	438	406°1	164°1	498	461°8	186°6	558	517°3	209°1
319	295°8	119°5	379	351°4	141°9	439	407°0	164°4	499	462°7	186°9	559	518°3	209°4
320	296°7	119°8	380	352°3	142°3	440	408°0	164°8	500	463°6	187°3	560	519°2	209°8
321	297°6	120°2	381	353°3	142°7	441	408°9	165°2	501	464°5	187°7	561	520°1	210°2
322	298°6	120°6	382	354°2	143°1	442	409°8	165°5	502	465°4	188°0	562	521°0	210°5
323	299°5	121°0	383	355°1	143°4	443	410°7	165°9	503	466°4	188°4	563	522°0	210°9
324	300°4	121°3	384	356°0	143°8	444	411°7	166°3	504	467°3	188°8	564	522°9	211°3
325	301°3	121°7	385	357°0	144°2	445	412°6	166°7	505	468°2	189°2	565	523°8	211°7
326	302°3	122°1	386	357°9	144°6	446	413°5	167°0	506	469°2	189°5	566	524°8	212°0
327	303°2	122°5	387	358°8	144°9	447	414°5	167°4	507	470°1	189°9	567	525°7	212°4
328	304°1	122°8	388	359°7	145°3	448	415°4	167°8	508	471°0	190°3	568	526°6	212°8
329	305°0	123°2	389	360°7	145°7	449	416°3	168°2	509	471°9	190°7	569	527°5	213°2
330	306°0	123°6	390	361°6	146°1	450	417°2	168°5	510	472°9	191°1	570	528°5	213°5
331	306°9	124°0	391	362°5	146°4	451	418°2	168°9	511	473°8	191°4	571	529°4	213°9
332	307°8	124°3	392	363°5	146°8	452	419°1	169°3	512	474°7	191°8	572	530°3	214°3
333	308°8	124°7	393	364°4	147°2	453	420°0	169°7	513	475°6	192°2	573	531°2	214°7
334	309°7	125°1	394	365°3	147°6	454	420°9	170°0	514	476°6	192°5	574	532°2	215°0
335	310°6	125°5	395	366°2	147°9	455	421°9	170°4	515	477°5	192°9	575	533°1	215°4
336	311°5	125°8	396	367°2	148°3	456	422°8	170°8	516	478°4	193°3	576	534°0	215°8
337	312°5	126°2	397	368°1	148°7	457	423°7	171°2	517	479°3	193°7	577	534°9	216°2
338	313°4	126°6	398	369°0	149°1	458	424°6	171°5	518	480°3	194°0	578	535°9	216°5
339	314°3	127°0	399	369°9	149°4	459	425°6	171°9	519	481°2	194°4	579	536°8	216°9
340	315°2	127°3	400	370°9	149°8	460	426°5	172°3	520	482°1	194°8	580	537°7	217°3
341	316°2	127°7	401	371°8	150°2	461	427°4	172°7	521	483°0	195°2	581	538°6	217°7
342	317°1	128°1	402	372°7	150°6	462	428°4	173°0	522	484°0	195°5	582	539°6	218°0
343	318°0	128°5	403	373°7	150°9	463	429°3	173°4	523	484°9	195°9	583	540°5	218°4
344	319°0	128°8	404	374°6	151°3	464	430°2	173°8	524	485°8	196°3	584	541°4	218°8
345	319°9	129°2	405	375°5	151°7	465	431°1	174°2	525	486°7	196°7	585	542°4	219°2
346	320°8	129°6	406	376°4	152°1	466	432°1	174°5	526	487°7	197°0	586	543°3	219°5
347	321°7	130°0	407	377°4	152°4	467	433°0	174°9	527	488°6	197°4	587	544°2	219°9
348	322°7	130°3	408	378°3	152°8	468	433°9	175°3	528	489°5	197°8	588	545°1	220°3
349	323°6	130°7	409	379°2	153°2	469	434°8	175°7	529	490°4	198°2	589	546°1	220°7
350	324°5	131°1	410	380°1	153°6	470	435°8	176°0	530	491°4	198°5	590	547°0	221°0
351	325°4	131°5	411	381°1	153°9	471	436°7	176°4	531	492°3	198°9	591	547°9	221°4
352	326°4	131°8	412	382°0	154°3	472	437°6	176°8	532	493°2	199°3	592	548°9	221°8
353	327°3	132°2	413	382°9	154°7	473	438°6	177°2	533	494°2	199°7	593	549°8	222°2
354	328°2	132°6	414	383°9	155°1	474	439°5	177°5	534	495°1	200°0	594	550°7	222°5
355	329°2	133°0	415	384°8	155°4	475	440°4	177°9	535	496°0	200°4	595	551°7	222°9
356	330°1	133°3	416	385°7	155°8	476	441°3	178°3	536	496°9	200°8	596	552°6	223°3
357	331°0	133°7	417	386°6	156°2	477	442°3	178°7	537	497°9	201°2	597	553°5	223°7
358	332°0	134°1	418	387°6	156°6	478	443°2	179°0	538	498°8	201°5	598	554°4	224°0
359	332°9	134°5	419	388°5	156°9	479	444°1	179°4	539	499°7	201°9	599	555°4	224°4
360	333°8	134°8	420	389°4	157°3	480	445°0	179°8	540	500°7	202°3	600	556°3	224°8
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

68°

4° 82'

TRAVERSE TABLE TO DEGREES														
23°									1 ^h 32 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0°9	0°4	61	56°2	23°8	121	111°4	47°3	181	166°6	70°7	241	221°8	94°2
2	1°8	0°8	62	57°1	24°2	122	112°3	47°7	182	167°5	71°1	242	222°8	94°6
3	2°8	1°2	63	58°0	24°6	123	113°2	48°1	183	168°5	71°5	243	223°7	94°9
4	3°7	1°6	64	58°9	25°0	124	114°1	48°5	184	169°4	71°9	244	224°6	95°3
5	4°6	2°0	65	59°8	25°4	125	115°1	48°8	185	170°3	72°3	245	225°5	95°7
6	5°5	2°3	66	60°8	25°8	126	116°0	49°2	186	171°2	72°7	246	226°4	96°1
7	6°4	2°7	67	61°7	26°2	127	116°9	49°6	187	172°1	73°1	247	227°4	96°5
8	7°4	3°1	68	62°6	26°6	128	117°8	50°0	188	173°1	73°5	248	228°3	96°9
9	8°3	3°5	69	63°5	27°0	129	118°7	50°4	189	174°0	73°8	249	229°2	97°3
10	9°2	3°9	70	64°4	27°4	130	119°7	50°8	190	174°9	74°2	250	230°1	97°7
11	10°1	4°3	71	65°4	27°7	131	120°6	51°2	191	175°8	74°6	251	231°0	98°1
12	11°0	4°7	72	66°3	28°1	132	121°5	51°6	192	176°7	75°0	252	232°0	98°5
13	12°0	5°1	73	67°2	28°5	133	122°4	52°0	193	177°7	75°4	253	232°9	98°9
14	12°9	5°5	74	68°1	28°9	134	123°3	52°4	194	178°6	75°8	254	233°8	99°2
15	13°8	5°9	75	69°0	29°3	135	124°3	52°7	195	179°5	76°2	255	234°7	99°6
16	14°7	6°3	76	70°0	29°7	136	125°2	53°1	196	180°4	76°6	256	235°6	100°0
17	15°6	6°6	77	70°9	30°1	137	126°1	53°5	197	181°3	77°0	257	236°6	100°4
18	16°6	7°0	78	71°8	30°5	138	127°0	53°9	198	182°3	77°4	258	237°5	100°8
19	17°5	7°4	79	72°7	30°9	139	128°0	54°3	199	183°2	77°8	259	238°4	101°2
20	18°4	7°8	80	73°6	31°3	140	128°9	54°7	200	184°1	78°1	260	239°3	101°6
21	19°3	8°2	81	74°6	31°6	141	129°8	55°1	201	185°0	78°5	261	240°3	102°0
22	20°3	8°6	82	75°5	32°0	142	130°7	55°5	202	185°9	78°9	262	241°2	102°4
23	21°2	9°0	83	76°4	32°4	143	131°6	55°9	203	186°9	79°3	263	242°1	102°8
24	22°1	9°4	84	77°3	32°8	144	132°6	56°3	204	187°8	79°7	264	243°0	103°2
25	23°0	9°8	85	78°2	33°2	145	133°5	56°7	205	188°7	80°1	265	243°9	103°5
26	23°9	10°2	86	79°2	33°6	146	134°4	57°0	206	189°6	80°5	266	244°9	103°9
27	24°9	10°5	87	80°1	34°0	147	135°3	57°4	207	190°5	80°9	267	245°8	104°3
28	25°8	10°9	88	81°0	34°4	148	136°2	57°8	208	191°5	81°3	268	246°7	104°7
29	26°7	11°3	89	81°9	34°8	149	137°2	58°2	209	192°4	81°7	269	247°6	105°1
30	27°6	11°7	90	82°8	35°2	150	138°1	58°6	210	193°3	82°1	270	248°5	105°5
31	28°5	12°1	91	83°8	35°6	151	139°0	59°0	211	194°2	82°4	271	249°5	105°9
32	29°5	12°5	92	84°7	35°9	152	139°9	59°4	212	195°1	82°8	272	250°4	106°3
33	30°4	12°9	93	85°6	36°3	153	140°8	59°8	213	196°1	83°2	273	251°3	106°7
34	31°3	13°3	94	86°5	36°7	154	141°8	60°2	214	197°0	83°6	274	252°2	107°1
35	32°2	13°7	95	87°4	37°1	155	142°7	60°6	215	197°9	84°0	275	253°1	107°5
36	33°1	14°1	96	88°4	37°5	156	143°6	61°0	216	198°8	84°4	276	254°1	107°8
37	34°1	14°5	97	89°3	37°9	157	144°5	61°3	217	199°7	84°8	277	255°0	108°2
38	35°0	14°8	98	90°2	38°3	158	145°4	61°7	218	200°7	85°2	278	255°9	108°6
39	35°9	15°2	99	91°1	38°7	159	146°4	62°1	219	201°6	85°6	279	256°8	109°0
40	36°8	15°6	100	92°1	39°1	160	147°3	62°5	220	202°5	86°0	280	257°7	109°4
41	37°7	16°0	101	93°0	39°5	161	148°2	62°9	221	203°4	86°4	281	258°7	109°8
42	38°7	16°4	102	93°9	39°9	162	149°1	63°3	222	204°4	86°7	282	259°6	110°2
43	39°6	16°8	103	94°8	40°2	163	150°0	63°7	223	205°3	87°1	283	260°5	110°6
44	40°5	17°2	104	95°7	40°6	164	151°0	64°1	224	206°2	87°5	284	261°4	111°0
45	41°4	17°6	105	96°7	41°0	165	151°9	64°5	225	207°1	87°9	285	262°3	111°4
46	42°3	18°0	106	97°6	41°4	166	152°8	64°9	226	208°0	88°3	286	263°3	111°7
47	43°3	18°4	107	98°5	41°8	167	153°7	65°3	227	209°0	88°7	287	264°2	112°1
48	44°2	18°8	108	99°4	42°2	168	154°6	65°6	228	209°9	89°1	288	265°1	112°5
49	45°1	19°1	109	100°3	42°6	169	155°6	66°0	229	210°8	89°5	289	266°0	112°9
50	46°0	19°5	110	101°3	43°0	170	156°5	66°4	230	211°7	89°9	290	266°9	113°3
51	46°9	19°9	111	102°2	43°4	171	157°4	66°8	231	212°6	90°3	291	267°9	113°7
52	47°9	20°3	112	103°1	43°8	172	158°3	67°2	232	213°6	90°6	292	268°8	114°1
53	48°8	20°7	113	104°0	44°2	173	159°2	67°6	233	214°5	91°0	293	269°7	114°5
54	49°7	21°1	114	104°9	44°5	174	160°2	68°0	234	215°4	91°4	294	270°6	114°9
55	50°6	21°5	115	105°9	44°9	175	161°1	68°4	235	216°3	91°8	295	271°5	115°3
56	51°5	21°9	116	106°8	45°3	176	162°0	68°8	236	217°2	92°2	296	272°5	115°7
57	52°5	22°3	117	107°7	45°7	177	162°9	69°2	237	218°2	92°6	297	273°4	116°0
58	53°4	22°7	118	108°6	46°1	178	163°8	69°6	238	219°1	93°0	298	274°3	116°4
59	54°3	23°1	119	109°5	46°5	179	164°8	69°9	239	220°0	93°4	299	275°2	116°8
60	55°2	23°4	120	110°5	46°9	180	165°7	70°3	240	220°9	93°8	300	276°2	117°2
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

477

TRAVERSE TABLE TO DEGREES														
23°									1h 82m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	277.1	117.6	361	332.3	141.1	421	387.5	164.5	481	442.7	188.0	541	498.0	211.4
302	278.0	118.0	362	333.2	141.5	422	388.5	164.9	482	443.7	188.4	542	498.9	211.8
303	278.9	118.4	363	334.1	141.8	423	389.4	165.3	483	444.6	188.8	543	499.8	212.2
304	279.8	118.8	364	335.1	142.2	424	390.3	165.7	484	445.5	189.2	544	500.7	212.6
305	280.8	119.2	365	336.0	142.6	425	391.2	166.1	485	446.4	189.5	545	501.7	213.0
306	281.7	119.6	366	336.9	143.0	426	392.1	166.5	486	447.3	189.9	546	502.6	213.4
307	282.6	120.0	367	337.8	143.4	427	393.1	166.8	487	448.3	190.2	547	503.5	213.8
308	283.5	120.4	368	338.7	143.8	428	394.0	167.2	488	449.2	190.6	548	504.4	214.2
309	284.4	120.8	369	339.7	144.2	429	394.9	167.6	489	450.1	191.0	549	505.3	214.6
310	285.4	121.2	370	340.6	144.6	430	395.8	168.0	490	451.0	191.4	550	506.3	215.0
311	286.3	121.6	371	341.5	145.0	431	396.7	168.4	491	451.9	191.8	551	507.2	215.3
312	287.2	121.9	372	342.4	145.4	432	397.7	168.8	492	452.9	192.2	552	508.1	215.6
313	288.1	122.3	373	343.4	145.7	433	398.6	169.2	493	453.8	192.6	553	509.0	216.0
314	289.0	122.7	374	344.3	146.1	434	399.5	169.6	494	454.7	193.0	554	509.9	216.4
315	290.0	123.1	375	345.2	146.5	435	400.4	170.0	495	455.6	193.4	555	510.9	216.8
316	290.9	123.5	376	346.1	146.9	436	401.3	170.4	496	456.6	193.8	556	511.8	217.2
317	291.8	123.9	377	347.0	147.3	437	402.3	170.8	497	457.5	194.2	557	512.7	217.6
318	292.7	124.3	378	348.0	147.7	438	403.2	171.1	498	458.4	194.6	558	513.6	218.0
319	293.6	124.6	379	348.9	148.1	439	404.1	171.5	499	459.3	195.0	559	514.5	218.4
320	294.6	125.0	380	349.8	148.5	440	405.0	171.9	500	460.2	195.4	560	515.5	218.8
321	295.5	125.4	381	350.7	148.9	441	405.9	172.3	501	461.2	195.8	561	516.4	219.2
322	296.4	125.8	382	351.6	149.3	442	406.9	172.7	502	462.1	196.2	562	517.3	219.6
323	297.3	126.2	383	352.6	149.7	443	407.8	173.1	503	463.0	196.6	563	518.2	220.0
324	298.2	126.6	384	353.5	150.0	444	408.7	173.5	504	463.9	197.0	564	519.2	220.4
325	299.2	127.0	385	354.4	150.4	445	409.6	173.9	505	464.9	197.4	565	520.1	220.8
326	300.1	127.4	386	355.3	150.8	446	410.5	174.3	506	465.8	197.8	566	521.0	221.2
327	301.0	127.8	387	356.2	151.2	447	411.5	174.7	507	466.7	198.1	567	521.9	221.6
328	301.9	128.2	388	357.2	151.6	448	412.4	175.1	508	467.6	198.5	568	522.8	222.0
329	302.8	128.6	389	358.1	152.0	449	413.3	175.4	509	468.5	198.8	569	523.8	222.3
330	303.8	128.9	390	359.0	152.4	450	414.2	175.8	510	469.5	199.3	570	524.7	222.7
331	304.7	129.3	391	359.9	152.8	451	415.2	176.2	511	470.4	199.7	571	525.6	223.1
332	305.6	129.7	392	360.8	153.2	452	416.1	176.6	512	471.3	200.0	572	526.5	223.4
333	306.5	130.1	393	361.8	153.6	453	417.0	177.0	513	472.2	200.4	573	527.4	223.8
334	307.5	130.5	394	362.7	154.0	454	417.9	177.4	514	473.1	200.8	574	528.4	224.2
335	308.4	130.9	395	363.6	154.3	455	418.8	177.8	515	474.0	201.2	575	529.3	224.6
336	309.3	131.3	396	364.5	154.7	456	419.8	178.2	516	475.0	201.6	576	530.2	225.0
337	310.2	131.7	397	365.4	155.1	457	420.7	178.6	517	475.9	202.0	577	531.1	225.4
338	311.1	132.1	398	366.4	155.5	458	421.6	179.0	518	476.8	202.4	578	532.0	225.8
339	312.1	132.5	399	367.3	155.9	459	422.5	179.4	519	477.7	202.8	579	533.0	226.2
340	313.0	132.9	400	368.2	156.3	460	423.4	179.7	520	478.6	203.2	580	533.9	226.6
341	313.9	133.2	401	369.1	156.7	461	424.4	180.1	521	479.6	203.6	581	534.8	227.0
342	314.8	133.6	402	370.0	157.1	462	425.3	180.5	522	480.5	204.0	582	535.7	227.4
343	315.7	134.0	403	371.0	157.5	463	426.2	180.9	523	481.4	204.4	583	536.6	227.8
344	316.7	134.4	404	371.9	157.9	464	427.1	181.3	524	482.3	204.8	584	537.6	228.2
345	317.6	134.8	405	372.8	158.3	465	428.0	181.7	525	483.2	205.2	585	538.5	228.6
346	318.5	135.2	406	373.7	158.6	466	429.0	182.1	526	484.2	205.5	586	539.4	229.0
347	319.4	135.6	407	374.6	159.0	467	429.9	182.5	527	485.1	205.9	587	540.3	229.4
348	320.3	136.0	408	375.6	159.4	468	430.8	182.9	528	486.0	206.3	588	541.2	229.8
349	321.3	136.4	409	376.5	159.8	469	431.7	183.3	529	486.9	206.7	589	542.2	230.2
350	322.2	136.8	410	377.4	160.2	470	432.6	183.7	530	487.8	207.1	590	543.1	230.6
351	323.1	137.2	411	378.3	160.6	471	433.6	184.0	531	488.8	207.4	591	544.0	231.0
352	324.0	137.5	412	379.3	161.0	472	434.5	184.4	532	489.7	207.8	592	544.9	231.3
353	324.9	137.9	413	380.2	161.4	473	435.4	184.8	533	490.6	208.2	593	545.8	231.7
354	325.9	138.3	414	381.1	161.8	474	436.3	185.2	534	491.5	208.6	594	546.8	232.0
355	326.8	138.7	415	382.0	162.2	475	437.2	185.6	535	492.5	209.0	595	547.7	232.4
356	327.7	139.1	416	382.9	162.5	476	438.2	186.0	536	493.4	209.4	596	548.6	232.8
357	328.6	139.5	417	383.9	162.9	477	439.1	186.4	537	494.3	209.8	597	549.5	233.2
358	329.5	139.9	418	384.8	163.3	478	440.0	186.8	538	495.2	210.2	598	550.4	233.6
359	330.5	140.3	419	385.7	163.7	479	440.9	187.2	539	496.1	210.6	599	551.3	234.0
360	331.4	140.7	420	386.6	164.1	480	441.8	187.6	540	497.1	211.0	600	552.3	234.4
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

67°

4h 28m

TRAVERSE TABLE TO DEGREES														
24°									1 ^h 36 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0.9	0.4	61	55.7	24.8	121	110.5	49.2	181	165.4	73.6	241	220.2	98.0
2	1.8	0.8	62	56.6	25.2	122	111.5	49.6	182	166.3	74.0	242	221.1	98.4
3	2.7	1.2	63	57.6	25.6	123	112.4	50.0	183	167.2	74.4	243	222.0	98.8
4	3.7	1.6	64	58.5	26.0	124	113.3	50.4	184	168.1	74.8	244	222.9	99.2
5	4.6	2.0	65	59.4	26.4	125	114.2	50.8	185	169.0	75.2	245	223.8	99.7
6	5.5	2.4	66	60.3	26.8	126	115.1	51.2	186	169.9	75.7	246	224.7	100.1
7	6.4	2.8	67	61.2	27.3	127	116.0	51.7	187	170.8	76.1	247	225.6	100.5
8	7.3	3.3	68	62.1	27.7	128	116.9	52.1	188	171.7	76.5	248	226.6	100.9
9	8.2	3.7	69	63.0	28.1	129	117.8	52.5	189	172.7	76.9	249	227.5	101.3
10	9.1	4.1	70	63.9	28.5	130	118.8	52.9	190	173.6	77.3	250	228.4	101.7
11	10.0	4.5	71	64.9	28.9	131	119.7	53.3	191	174.5	77.7	251	229.3	102.1
12	11.0	4.9	72	65.8	29.3	132	120.6	53.7	192	175.4	78.1	252	230.2	102.5
13	11.9	5.3	73	66.7	29.7	133	121.5	54.1	193	176.3	78.5	253	231.1	102.9
14	12.8	5.7	74	67.6	30.1	134	122.4	54.5	194	177.2	78.9	254	232.0	103.3
15	13.7	6.1	75	68.5	30.5	135	123.3	54.9	195	178.1	79.3	255	233.0	103.7
16	14.6	6.5	76	69.4	30.9	136	124.2	55.3	196	179.1	79.7	256	233.9	104.1
17	15.5	6.9	77	70.3	31.3	137	125.2	55.7	197	180.0	80.1	257	234.8	104.5
18	16.4	7.3	78	71.3	31.7	138	126.1	56.1	198	180.9	80.5	258	235.7	104.9
19	17.4	7.7	79	72.2	32.1	139	127.0	56.5	199	181.8	80.9	259	236.6	105.3
20	18.3	8.1	80	73.1	32.5	140	127.9	56.9	200	182.7	81.3	260	237.5	105.8
21	19.2	8.5	81	74.0	32.9	141	128.8	57.3	201	183.6	81.8	261	238.4	106.2
22	20.1	8.9	82	74.9	33.4	142	129.7	57.8	202	184.5	82.2	262	239.3	106.6
23	21.0	9.4	83	75.8	33.8	143	130.6	58.2	203	185.4	82.6	263	240.3	107.0
24	21.9	9.8	84	76.7	34.2	144	131.6	58.6	204	186.4	83.0	264	241.2	107.4
25	22.8	10.2	85	77.7	34.6	145	132.5	59.0	205	187.3	83.4	265	242.1	107.8
26	23.8	10.6	86	78.6	35.0	146	133.4	59.4	206	188.2	83.8	266	243.0	108.2
27	24.7	11.0	87	79.5	35.4	147	134.3	59.8	207	189.1	84.2	267	243.9	108.6
28	25.6	11.4	88	80.4	35.8	148	135.2	60.2	208	190.0	84.6	268	244.8	109.0
29	26.5	11.8	89	81.3	36.2	149	136.1	60.6	209	190.9	85.0	269	245.7	109.4
30	27.4	12.2	90	82.2	36.6	150	137.0	61.0	210	191.8	85.4	270	246.7	109.8
31	28.3	12.6	91	83.1	37.0	151	137.9	61.4	211	192.8	85.8	271	247.6	110.2
32	29.2	13.0	92	84.0	37.4	152	138.9	61.8	212	193.7	86.2	272	248.5	110.6
33	30.1	13.4	93	85.0	37.8	153	139.8	62.2	213	194.6	86.6	273	249.4	111.0
34	31.1	13.8	94	85.9	38.2	154	140.7	62.6	214	195.5	87.0	274	250.3	111.4
35	32.0	14.2	95	86.8	38.6	155	141.6	63.0	215	196.4	87.4	275	251.2	111.9
36	32.9	14.6	96	87.7	39.0	156	142.5	63.5	216	197.3	87.9	276	252.1	112.3
37	33.8	15.0	97	88.6	39.5	157	143.4	63.9	217	198.2	88.3	277	253.1	112.7
38	34.7	15.5	98	89.5	39.9	158	144.3	64.3	218	199.2	88.7	278	254.0	113.1
39	35.6	15.9	99	90.4	40.3	159	145.3	64.7	219	200.1	89.1	279	254.9	113.5
40	36.5	16.3	100	91.4	40.7	160	146.2	65.1	220	201.0	89.5	280	255.8	113.9
41	37.5	16.7	101	92.3	41.1	161	147.1	65.5	221	201.9	89.9	281	256.7	114.3
42	38.4	17.1	102	93.2	41.5	162	148.0	65.9	222	202.8	90.3	282	257.6	114.7
43	39.3	17.5	103	94.1	41.9	163	148.9	66.3	223	203.7	90.7	283	258.5	115.1
44	40.2	17.9	104	95.0	42.3	164	149.8	66.7	224	204.6	91.1	284	259.4	115.5
45	41.1	18.3	105	95.9	42.7	165	150.7	67.1	225	205.5	91.5	285	260.4	115.9
46	42.0	18.7	106	96.8	43.1	166	151.6	67.5	226	206.5	91.9	286	261.3	116.3
47	42.9	19.1	107	97.7	43.5	167	152.6	67.9	227	207.4	92.3	287	262.2	116.7
48	43.9	19.5	108	98.7	43.9	168	153.5	68.3	228	208.3	92.7	288	263.1	117.1
49	44.8	19.9	109	99.6	44.3	169	154.4	68.7	229	209.2	93.1	289	264.0	117.5
50	45.7	20.3	110	100.5	44.7	170	155.3	69.1	230	210.1	93.5	290	264.9	118.0
51	46.6	20.7	111	101.4	45.1	171	156.2	69.6	231	211.0	94.0	291	265.8	118.4
52	47.5	21.2	112	102.3	45.6	172	157.1	70.0	232	211.9	94.4	292	266.8	118.8
53	48.4	21.6	113	103.2	46.0	173	158.0	70.4	233	212.9	94.8	293	267.7	119.2
54	49.3	22.0	114	104.1	46.4	174	159.0	70.8	234	213.8	95.2	294	268.6	119.6
55	50.2	22.4	115	105.1	46.8	175	159.9	71.2	235	214.7	95.6	295	269.5	120.0
56	51.2	22.8	116	106.0	47.2	176	160.8	71.6	236	215.6	96.0	296	270.4	120.4
57	52.1	23.2	117	106.9	47.6	177	161.7	72.0	237	216.5	96.4	297	271.3	120.8
58	53.0	23.6	118	107.8	48.0	178	162.6	72.4	238	217.4	96.8	298	272.2	121.2
59	53.9	24.0	119	108.7	48.4	179	163.5	72.8	239	218.3	97.2	299	273.2	121.6
60	54.8	24.4	120	109.6	48.8	180	164.4	73.2	240	219.3	97.6	300	274.1	122.0
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
66°									4 ^h 24 ^m					

TRAVERSE TABLE TO DEGREES														
25°									1° 40'					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0'9	0'4	61	55'3	25'8	121	109'7	51'1	181	164'0	76'5	241	218'4	101'9
2	1'8	0'8	62	56'2	26'2	122	110'6	51'6	182	164'9	76'9	242	219'3	102'3
3	2'7	1'3	63	57'1	26'6	123	111'5	52'0	183	165'9	77'3	243	220'2	102'7
4	3'6	1'7	64	58'0	27'0	124	112'4	52'4	184	166'8	77'8	244	221'1	103'1
5	4'5	2'1	65	58'9	27'5	125	113'3	52'8	185	167'7	78'2	245	222'0	103'5
6	5'4	2'5	66	59'8	27'9	126	114'2	53'2	186	168'6	78'6	246	223'0	104'0
7	6'3	3'0	67	60'7	28'3	127	115'1	53'7	187	169'5	79'0	247	223'9	104'4
8	7'3	3'4	68	61'6	28'7	128	116'0	54'1	188	170'4	79'5	248	224'8	104'8
9	8'2	3'8	69	62'5	29'2	129	116'9	54'5	189	171'3	79'9	249	225'7	105'2
10	9'1	4'2	70	63'4	29'6	130	117'8	54'9	190	172'2	80'3	250	226'6	105'7
11	10'0	4'6	71	64'3	30'0	131	118'7	55'4	191	173'1	80'7	251	227'5	106'1
12	10'9	5'1	72	65'3	30'4	132	119'6	55'8	192	174'0	81'1	252	228'4	106'5
13	11'8	5'5	73	66'2	30'9	133	120'5	56'2	193	174'9	81'6	253	229'3	106'9
14	12'7	5'9	74	67'1	31'3	134	121'4	56'6	194	175'8	82'0	254	230'2	107'3
15	13'6	6'3	75	68'0	31'7	135	122'4	57'1	195	176'7	82'4	255	231'1	107'8
16	14'5	6'8	76	68'9	32'1	136	123'3	57'5	196	177'6	82'8	256	232'0	108'2
17	15'4	7'2	77	69'8	32'5	137	124'2	57'9	197	178'5	83'3	257	232'9	108'6
18	16'3	7'6	78	70'7	33'0	138	125'1	58'3	198	179'4	83'7	258	233'8	109'0
19	17'2	8'0	79	71'6	33'4	139	126'0	58'7	199	180'4	84'1	259	234'7	109'5
20	18'1	8'5	80	72'5	33'8	140	126'9	59'2	200	181'3	84'5	260	235'6	109'9
21	19'0	8'9	81	73'4	34'2	141	127'8	59'6	201	182'2	84'9	261	236'5	110'3
22	19'9	9'3	82	74'3	34'7	142	128'7	60'0	202	183'1	85'4	262	237'5	110'7
23	20'8	9'7	83	75'2	35'1	143	129'6	60'4	203	184'0	85'8	263	238'4	111'1
24	21'8	10'1	84	76'1	35'5	144	130'5	60'9	204	184'9	86'2	264	239'3	111'6
25	22'7	10'6	85	77'0	35'9	145	131'4	61'3	205	185'8	86'6	265	240'2	112'0
26	23'6	11'0	86	77'9	36'3	146	132'3	61'7	206	186'7	87'1	266	241'1	112'4
27	24'5	11'4	87	78'8	36'8	147	133'2	62'1	207	187'6	87'5	267	242'0	112'8
28	25'4	11'8	88	79'8	37'2	148	134'1	62'5	208	188'5	87'9	268	242'9	113'3
29	26'3	12'3	89	80'7	37'6	149	135'0	63'0	209	189'4	88'3	269	243'8	113'7
30	27'2	12'7	90	81'6	38'0	150	135'9	63'4	210	190'3	88'7	270	244'7	114'1
31	28'1	13'1	91	82'5	38'5	151	136'9	63'8	211	191'2	89'2	271	245'6	114'5
32	29'0	13'5	92	83'4	38'9	152	137'8	64'2	212	192'1	89'6	272	246'5	115'0
33	29'9	13'9	93	84'3	39'3	153	138'7	64'7	213	193'0	90'0	273	247'4	115'4
34	30'8	14'4	94	85'2	39'7	154	139'6	65'1	214	193'9	90'4	274	248'3	115'8
35	31'7	14'8	95	86'1	40'1	155	140'5	65'5	215	194'9	90'9	275	249'2	116'2
36	32'6	15'2	96	87'0	40'6	156	141'4	65'9	216	195'8	91'3	276	250'1	116'6
37	33'5	15'6	97	87'9	41'0	157	142'3	66'4	217	196'7	91'7	277	251'0	117'1
38	34'4	16'1	98	88'8	41'4	158	143'2	66'8	218	197'6	92'1	278	252'0	117'5
39	35'3	16'5	99	89'7	41'8	159	144'1	67'2	219	198'5	92'6	279	252'9	117'9
40	36'3	16'9	100	90'6	42'3	160	145'0	67'6	220	199'4	93'0	280	253'8	118'3
41	37'2	17'3	101	91'5	42'7	161	145'9	68'0	221	200'3	93'4	281	254'7	118'8
42	38'1	17'7	102	92'4	43'1	162	146'8	68'5	222	201'2	93'8	282	255'6	119'2
43	39'0	18'2	103	93'3	43'5	163	147'7	68'9	223	202'1	94'2	283	256'5	119'6
44	39'9	18'6	104	94'3	44'0	164	148'6	69'3	224	203'0	94'7	284	257'4	120'0
45	40'8	19'0	105	95'2	44'4	165	149'5	69'7	225	203'9	95'1	285	258'3	120'4
46	41'7	19'4	106	96'1	44'8	166	150'4	70'2	226	204'8	95'5	286	259'2	120'9
47	42'6	19'9	107	97'0	45'2	167	151'4	70'6	227	205'7	95'9	287	260'1	121'3
48	43'5	20'3	108	97'9	45'6	168	152'3	71'0	228	206'6	96'4	288	261'0	121'7
49	44'4	20'7	109	98'8	46'1	169	153'2	71'4	229	207'5	96'8	289	261'9	122'1
50	45'3	21'1	110	99'7	46'5	170	154'1	71'8	230	208'5	97'2	290	262'8	122'6
51	46'2	21'6	111	100'6	46'9	171	155'0	72'3	231	209'4	97'6	291	263'7	123'0
52	47'1	22'0	112	101'5	47'3	172	155'9	72'7	232	210'3	98'0	292	264'6	123'4
53	48'0	22'4	113	102'4	47'8	173	156'8	73'1	233	211'2	98'5	293	265'5	123'8
54	48'9	22'8	114	103'3	48'2	174	157'7	73'5	234	212'1	98'9	294	266'4	124'2
55	49'8	23'2	115	104'2	48'6	175	158'6	74'0	235	213'0	99'3	295	267'4	124'7
56	50'8	23'7	116	105'1	49'0	176	159'5	74'4	236	213'9	99'7	296	268'3	125'1
57	51'7	24'1	117	106'0	49'4	177	160'4	74'8	237	214'8	100'2	297	269'2	125'5
58	52'6	24'5	118	106'9	49'9	178	161'3	75'2	238	215'7	100'6	298	270'1	125'9
59	53'5	24'9	119	107'9	50'3	179	162'2	75'6	239	216'6	101'0	299	271'0	126'4
60	54'4	25'4	120	108'8	50'7	180	163'1	76'1	240	217'5	101'4	300	271'9	126'8
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

481

TRAVERSE TABLE TO DEGREES														
25°														
1 ^h 40 ^m														
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	272.8	127.2	361	327.1	152.5	421	381.5	177.9	481	435.9	203.3	541	490.3	228.6
302	273.7	127.6	362	328.0	153.0	422	382.4	178.3	482	436.8	203.7	542	491.2	229.0
303	274.6	128.0	363	329.0	153.4	423	383.3	178.7	483	437.7	204.1	543	492.1	229.4
304	275.5	128.4	364	329.9	153.8	424	384.2	179.2	484	438.6	204.5	544	493.0	229.9
305	276.4	128.9	365	330.8	154.2	425	385.1	179.6	485	439.5	204.9	545	493.9	230.3
306	277.3	129.3	366	331.7	154.6	426	386.0	180.0	486	440.4	205.4	546	494.8	230.7
307	278.2	129.7	367	332.6	155.1	427	387.0	180.4	487	441.3	205.8	547	495.7	231.1
308	279.1	130.1	368	333.5	155.5	428	387.9	180.9	488	442.2	206.2	548	496.6	231.6
309	280.0	130.6	369	334.4	155.9	429	388.8	181.3	489	443.1	206.6	549	497.5	232.0
310	280.9	131.0	370	335.3	156.3	430	389.7	181.7	490	444.0	207.1	550	498.4	232.4
311	281.8	131.4	371	336.2	156.8	431	390.6	182.1	491	444.9	207.5	551	499.3	232.8
312	282.7	131.8	372	337.1	157.2	432	391.5	182.5	492	445.9	207.9	552	500.2	233.2
313	283.6	132.2	373	338.0	157.6	433	392.4	183.0	493	446.8	208.3	553	501.1	233.7
314	284.5	132.7	374	338.9	158.0	434	393.3	183.4	494	447.7	208.7	554	502.0	234.1
315	285.4	133.1	375	339.8	158.5	435	394.2	183.8	495	448.6	209.1	555	503.0	234.5
316	286.4	133.5	376	340.7	158.9	436	395.1	184.2	496	449.5	209.6	556	503.9	235.0
317	287.3	133.9	377	341.6	159.3	437	396.0	184.7	497	450.4	210.0	557	504.8	235.4
318	288.2	134.4	378	342.5	159.7	438	396.9	185.1	498	451.3	210.4	558	505.7	235.8
319	289.1	134.8	379	343.5	160.1	439	397.8	185.5	499	452.2	210.9	559	506.6	236.2
320	290.0	135.2	380	344.4	160.6	440	398.7	185.9	500	453.1	211.3	560	507.5	236.6
321	290.9	135.6	381	345.3	161.0	441	399.6	186.3	501	454.0	211.7	561	508.4	237.1
322	291.8	136.1	382	346.2	161.4	442	400.6	186.8	502	454.9	212.1	562	509.3	237.5
323	292.7	136.5	383	347.1	161.8	443	401.5	187.2	503	455.8	212.5	563	510.2	237.9
324	293.6	136.9	384	348.0	162.3	444	402.4	187.6	504	456.7	213.0	564	511.1	238.3
325	294.5	137.3	385	348.9	162.7	445	403.3	188.0	505	457.7	213.4	565	512.0	238.7
326	295.4	137.7	386	349.8	163.1	446	404.2	188.5	506	458.6	213.8	566	512.9	239.2
327	296.3	138.2	387	350.7	163.5	447	405.1	188.9	507	459.5	214.2	567	513.8	239.6
328	297.2	138.6	388	351.6	163.9	448	406.0	189.3	508	460.4	214.7	568	514.8	240.1
329	298.1	139.0	389	352.5	164.4	449	406.9	189.7	509	461.3	215.1	569	515.7	240.5
330	299.0	139.4	390	353.4	164.8	450	407.8	190.1	510	462.2	215.5	570	516.6	240.9
331	300.0	139.9	391	354.3	165.2	451	408.7	190.6	511	463.1	215.9	571	517.5	241.3
332	300.9	140.3	392	355.2	165.6	452	409.6	191.0	512	464.0	216.4	572	518.4	241.7
333	301.8	140.7	393	356.1	166.1	453	410.5	191.4	513	464.9	216.8	573	519.3	242.1
334	302.7	141.1	394	357.0	166.5	454	411.4	191.8	514	465.8	217.2	574	520.2	242.6
335	303.6	141.5	395	358.0	166.9	455	412.3	192.3	515	466.7	217.7	575	521.1	243.0
336	304.5	142.0	396	358.9	167.3	456	413.2	192.7	516	467.6	218.1	576	522.0	243.4
337	305.4	142.4	397	359.8	167.7	457	414.1	193.1	517	468.5	218.5	577	522.9	243.8
338	306.3	142.8	398	360.7	168.2	458	415.1	193.5	518	469.4	218.9	578	523.8	244.3
339	307.2	143.2	399	361.6	168.6	459	416.0	194.0	519	470.3	219.3	579	524.7	244.7
340	308.1	143.7	400	362.5	169.0	460	416.9	194.4	520	471.2	219.8	580	525.6	245.1
341	309.0	144.1	401	363.4	169.4	461	417.8	194.8	521	472.2	220.2	581	526.5	245.5
342	309.9	144.5	402	364.3	169.9	462	418.7	195.2	522	473.1	220.6	582	527.4	246.0
343	310.8	144.9	403	365.2	170.3	463	419.6	195.6	523	474.0	221.0	583	528.3	246.4
344	311.7	145.4	404	366.1	170.7	464	420.5	196.1	524	474.9	221.4	584	529.3	246.8
345	312.6	145.8	405	367.0	171.1	465	421.4	196.5	525	475.8	221.9	585	530.2	247.2
346	313.5	146.2	406	367.9	171.6	466	422.3	196.9	526	476.7	222.3	586	531.1	247.7
347	314.5	146.6	407	368.8	172.0	467	423.2	197.3	527	477.6	222.7	587	532.0	248.1
348	315.4	147.0	408	369.7	172.4	468	424.1	197.8	528	478.5	223.2	588	532.9	248.5
349	316.3	147.5	409	370.6	172.8	469	425.0	198.2	529	479.4	223.6	589	533.8	248.9
350	317.2	147.9	410	371.5	173.2	470	425.9	198.6	530	480.3	224.0	590	534.7	249.4
351	318.1	148.3	411	372.5	173.7	471	426.8	199.0	531	481.2	224.4	591	535.6	249.8
352	319.0	148.7	412	373.4	174.1	472	427.7	199.4	532	482.1	224.8	592	536.5	250.2
353	319.9	149.2	413	374.3	174.5	473	428.6	199.9	533	483.0	225.3	593	537.4	250.6
354	320.8	149.6	414	375.2	174.9	474	429.6	200.3	534	483.9	225.7	594	538.3	251.1
355	321.7	150.0	415	376.1	175.4	475	430.5	200.7	535	484.8	226.1	595	539.2	251.5
356	322.6	150.4	416	377.0	175.8	476	431.4	201.1	536	485.7	226.5	596	540.1	251.9
357	323.5	150.8	417	377.9	176.2	477	432.3	201.6	537	486.6	226.9	597	541.0	252.3
358	324.4	151.3	418	378.8	176.6	478	433.2	202.0	538	487.6	227.4	598	541.9	252.7
359	325.3	151.7	419	379.7	177.0	479	434.1	202.4	539	488.5	227.8	599	542.8	253.1
360	326.2	152.1	420	380.6	177.5	480	435.0	202.8	540	489.4	228.2	600	543.8	253.6
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
65°														
4 ^h 20 ^m														

TABLE 1

489

TRAVERSE TABLE TO DEGREES

26°												1 ^h 44 ^m		
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
801	270°5	132°0	361	324°5	158°3	421	378°4	184°6	481	432°3	210°9	541	486°2	237°2
802	271°4	132°4	362	325°4	158°7	422	379°3	185°0	482	433°2	211°3	542	487°1	237°6
803	272°3	132°8	363	326°3	159°1	423	380°2	185°4	483	434°1	211°7	543	488°0	238°0
804	273°2	133°3	364	327°2	159°6	424	381°1	185°9	484	435°0	212°2	544	488°9	238°5
805	274°1	133°7	365	328°1	160°0	425	382°0	186°3	485	435°9	212°6	545	489°8	238°9
806	275°0	134°1	366	329°0	160°4	426	382°9	186°7	486	436°8	213°0	546	490°7	239°3
807	275°9	134°6	367	329°9	160°9	427	383°8	187°2	487	437°7	213°5	547	491°6	239°8
808	276°8	135°0	368	330°8	161°3	428	384°7	187°6	488	438°6	213°9	548	492°5	240°2
809	277°7	135°5	369	331°7	161°8	429	385°6	188°1	489	439°5	214°4	549	493°4	240°7
810	278°6	135°9	370	332°6	162°2	430	386°5	188°5	490	440°4	214°8	550	494°3	241°1
811	279°5	136°3	371	333°5	162°6	431	387°4	188°9	491	441°3	215°2	551	495°2	241°5
812	280°4	136°8	372	334°4	163°1	432	388°3	189°4	492	442°2	215°7	552	496°1	242°0
813	281°3	137°2	373	335°3	163°5	433	389°2	189°8	493	443°1	216°1	553	497°0	242°4
814	282°2	137°7	374	336°2	164°0	434	390°1	190°3	494	444°0	216°6	554	497°9	242°9
815	283°1	138°1	375	337°1	164°4	435	391°0	190°7	495	444°9	217°0	555	498°8	243°3
816	284°0	138°5	376	338°0	164°8	436	391°9	191°1	496	445°8	217°4	556	499°7	243°7
817	284°9	139°0	377	338°9	165°3	437	392°8	191°6	497	446°7	217°9	557	500°6	244°2
818	285°8	139°4	378	339°8	165°7	438	393°7	192°0	498	447°6	218°3	558	501°5	244°6
819	286°7	139°8	379	340°7	166°2	439	394°6	192°4	499	448°5	218°7	559	502°4	245°0
820	287°6	140°3	380	341°5	166°6	440	395°5	192°9	500	449°4	219°2	560	503°3	245°5
821	288°5	140°7	381	342°4	167°0	441	396°4	193°3	501	450°3	219°6	561	504°2	245°9
822	289°4	141°2	382	343°3	167°5	442	397°3	193°8	502	451°2	220°1	562	505°1	246°4
823	290°3	141°6	383	344°2	167°9	443	398°2	194°2	503	452°1	220°5	563	506°0	246°8
824	291°2	142°0	384	345°1	168°3	444	399°1	194°7	504	453°0	221°0	564	506°9	247°3
825	292°1	142°5	385	346°0	168°8	445	400°0	195°1	505	453°9	221°4	565	507°8	247°7
826	293°0	142°9	386	346°9	169°2	446	400°9	195°5	506	454°8	221°8	566	508°7	248°1
827	293°9	143°4	387	347°8	169°7	447	401°8	196°0	507	455°7	222°3	567	509°6	248°6
828	294°8	143°8	388	348°7	170°1	448	402°7	196°4	508	456°6	222°7	568	510°5	249°0
829	295°7	144°2	389	349°6	170°5	449	403°6	196°8	509	457°5	223°1	569	511°4	249°4
830	296°6	144°7	390	350°5	171°0	450	404°5	197°3	510	458°4	223°6	570	512°3	249°9
831	297°5	145°1	391	351°4	171°4	451	405°4	197°7	511	459°3	224°0	571	513°2	250°3
832	298°4	145°6	392	352°3	171°8	452	406°3	198°1	512	460°2	224°4	572	514°1	250°8
833	299°3	146°0	393	353°2	172°3	453	407°2	198°6	513	461°1	224°9	573	515°0	251°2
834	300°2	146°4	394	354°1	172°7	454	408°1	199°0	514	462°0	225°3	574	515°9	251°6
835	301°1	146°9	395	355°0	173°2	455	409°0	199°5	515	462°9	225°8	575	516°8	252°1
836	302°0	147°3	396	355°9	173°6	456	409°9	199°9	516	463°8	226°2	576	517°7	252°5
837	302°9	147°7	397	356°8	174°0	457	410°8	200°3	517	464°7	226°6	577	518°6	252°9
838	303°8	148°2	398	357°7	174°5	458	411°7	200°8	518	465°6	227°1	578	519°5	253°4
839	304°7	148°6	399	358°6	174°9	459	412°6	201°2	519	466°5	227°5	579	520°4	253°8
840	305°6	149°0	400	359°5	175°4	460	413°5	201°7	520	467°4	228°0	580	521°3	254°3
841	306°5	149°5	401	360°4	175°8	461	414°4	202°1	521	468°3	228°4	581	522°2	254°7
842	307°4	149°9	402	361°3	176°2	462	415°2	202°5	522	469°2	228°8	582	523°1	255°1
843	308°3	150°4	403	362°2	176°7	463	416°1	203°0	523	470°1	229°3	583	524°0	255°6
844	309°2	150°8	404	363°1	177°1	464	417°0	203°4	524	471°0	229°7	584	524°9	256°0
845	310°1	151°2	405	364°0	177°5	465	417°9	203°8	525	471°9	230°1	585	525°8	256°4
846	311°0	151°7	406	364°9	178°0	466	418°8	204°3	526	472°8	230°6	586	526°7	256°9
847	311°9	152°1	407	365°8	178°4	467	419°7	204°7	527	473°7	231°0	587	527°6	257°3
848	312°8	152°6	408	366°7	178°9	468	420°6	205°2	528	474°6	231°5	588	528°5	257°8
849	313°7	153°0	409	367°6	179°3	469	421°5	205°6	529	475°5	231°9	589	529°4	258°2
850	314°6	153°4	410	368°5	179°7	470	422°4	206°0	530	476°4	232°3	590	530°3	258°6
851	315°5	153°9	411	369°4	180°2	471	423°3	206°5	531	477°3	232°8	591	531°2	259°1
852	316°4	154°3	412	370°3	180°6	472	424°2	206°9	532	478°2	233°2	592	532°1	259°5
853	317°3	154°7	413	371°2	181°1	473	425°1	207°3	533	479°1	233°6	593	533°0	259°9
854	318°2	155°2	414	372°1	181°5	474	426°0	207°8	534	480°0	234°1	594	533°9	260°4
855	319°1	155°6	415	373°0	181°9	475	426°9	208°2	535	480°9	234°5	595	534°8	260°8
856	320°0	156°1	416	373°9	182°4	476	427°8	208°7	536	481°8	235°0	596	535°7	261°3
857	320°9	156°5	417	374°8	182°8	477	428°7	209°1	537	482°7	235°4	597	536°6	261°7
858	321°8	156°9	418	375°7	183°2	478	429°6	209°5	538	483°6	235°8	598	537°5	262°1
859	322°7	157°4	419	376°6	183°7	479	430°5	210°0	539	484°5	236°3	599	538°4	262°6
860	323°6	157°8	420	377°5	184°1	480	431°4	210°4	540	485°3	236°7	600	539°3	263°0
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
64°												4 ^h 16 ^m		

TRAVERSE TABLE TO DEGREES

27°												1 ^h 48 ^m		
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0°9	0°5	61	54°4	27°7	121	107°8	54°9	181	161°3	82°2	241	214°7	109°4
2	1°8	0°9	62	55°2	28°1	122	108°7	55°4	182	162°2	82°6	242	215°6	109°9
3	2°7	1°4	63	56°1	28°6	123	109°6	55°8	183	163°1	83°1	243	216°5	110°3
4	3°6	1°8	64	57°0	29°1	124	110°5	56°3	184	163°9	83°5	244	217°4	110°8
5	4°5	2°3	65	57°9	29°5	125	111°4	56°7	185	164°8	84°0	245	218°3	111°2
6	5°3	2°7	66	58°8	30°0	126	112°3	57°2	186	165°7	84°4	246	219°2	111°7
7	6°2	3°2	67	59°7	30°4	127	113°2	57°7	187	166°6	84°9	247	220°1	112°1
8	7°1	3°6	68	60°6	30°9	128	114°0	58°1	188	167°5	85°4	248	221°0	112°6
9	8°0	4°1	69	61°5	31°3	129	114°9	58°6	189	168°4	85°8	249	221°9	113°0
10	8°9	4°5	70	62°4	31°8	130	115°8	59°0	190	169°3	86°3	250	222°8	113°5
11	9°8	5°0	71	63°3	32°2	131	116°7	59°5	191	170°2	86°7	251	223°6	114°0
12	10°7	5°4	72	64°2	32°7	132	117°6	59°9	192	171°1	87°2	252	224°5	114°4
13	11°6	5°9	73	65°0	33°1	133	118°5	60°4	193	172°0	87°6	253	225°4	114°9
14	12°5	6°4	74	65°9	33°6	134	119°4	60°8	194	172°9	88°1	254	226°3	115°3
15	13°4	6°8	75	66°8	34°0	135	120°3	61°3	195	173°7	88°5	255	227°2	115°8
16	14°3	7°3	76	67°7	34°5	136	121°2	61°7	196	174°6	89°0	256	228°1	116°2
17	15°1	7°7	77	68°6	35°0	137	122°1	62°2	197	175°5	89°4	257	229°0	116°7
18	16°0	8°2	78	69°5	35°4	138	123°0	62°7	198	176°4	89°9	258	229°9	117°1
19	16°9	8°6	79	70°4	35°9	139	123°8	63°1	199	177°3	90°3	259	230°8	117°6
20	17°8	9°1	80	71°3	36°3	140	124°7	63°6	200	178°2	90°8	260	231°7	118°0
21	18°7	9°5	81	72°2	36°8	141	125°6	64°0	201	179°1	91°3	261	232°6	118°5
22	19°6	10°0	82	73°1	37°2	142	126°5	64°5	202	180°0	91°7	262	233°4	118°9
23	20°5	10°4	83	74°0	37°7	143	127°4	64°9	203	180°9	92°2	263	234°3	119°4
24	21°4	10°9	84	74°8	38°1	144	128°3	65°4	204	181°8	92°6	264	235°2	119°9
25	22°3	11°3	85	75°7	38°6	145	129°2	65°8	205	182°7	93°1	265	236°1	120°3
26	23°2	11°8	86	76°6	39°0	146	130°1	66°3	206	183°5	93°5	266	237°0	120°8
27	24°1	12°3	87	77°5	39°5	147	131°0	66°7	207	184°4	94°0	267	237°9	121°2
28	24°9	12°7	88	78°4	40°0	148	131°9	67°2	208	185°3	94°4	268	238°8	121°7
29	25°8	13°2	89	79°3	40°4	149	132°8	67°6	209	186°2	94°9	269	239°7	122°1
30	26°7	13°6	90	80°2	40°9	150	133°7	68°1	210	187°1	95°3	270	240°6	122°6
31	27°6	14°1	91	81°1	41°3	151	134°5	68°6	211	188°0	95°8	271	241°5	123°0
32	28°5	14°5	92	82°0	41°8	152	135°4	69°0	212	188°9	96°2	272	242°4	123°5
33	29°4	15°0	93	82°9	42°2	153	136°3	69°5	213	189°8	96°7	273	243°2	123°9
34	30°3	15°4	94	83°8	42°7	154	137°2	69°9	214	190°7	97°2	274	244°1	124°4
35	31°2	15°9	95	84°6	43°1	155	138°1	70°4	215	191°6	97°6	275	245°0	124°8
36	32°1	16°3	96	85°5	43°6	156	139°0	70°8	216	192°5	98°1	276	245°9	125°3
37	33°0	16°8	97	86°4	44°0	157	139°9	71°3	217	193°3	98°5	277	246°8	125°8
38	33°9	17°3	98	87°3	44°5	158	140°8	71°7	218	194°2	99°0	278	247°7	126°2
39	34°7	17°7	99	88°2	44°9	159	141°7	72°2	219	195°1	99°4	279	248°6	126°7
40	35°6	18°2	100	89°1	45°4	160	142°6	72°6	220	196°0	99°9	280	249°5	127°1
41	36°5	18°6	101	90°0	45°9	161	143°5	73°1	221	196°9	100°3	281	250°4	127°6
42	37°4	19°1	102	90°9	46°3	162	144°3	73°5	222	197°8	100°8	282	251°3	128°0
43	38°3	19°5	103	91°8	46°8	163	145°2	74°0	223	198°7	101°2	283	252°2	128°5
44	39°2	20°0	104	92°7	47°2	164	146°1	74°5	224	199°6	101°7	284	253°0	128°9
45	40°1	20°4	105	93°6	47°7	165	147°0	74°9	225	200°5	102°1	285	253°9	129°4
46	41°0	20°9	106	94°4	48°1	166	147°9	75°4	226	201°4	102°6	286	254°8	129°8
47	41°9	21°3	107	95°3	48°6	167	148°8	75°8	227	202°3	103°1	287	255°7	130°3
48	42°8	21°8	108	96°2	49°0	168	149°7	76°3	228	203°1	103°5	288	256°6	130°7
49	43°7	22°2	109	97°1	49°5	169	150°6	76°7	229	204°0	104°0	289	257°5	131°2
50	44°6	22°7	110	98°0	49°9	170	151°5	77°2	230	204°9	104°4	290	258°4	131°7
51	45°4	23°2	111	98°9	50°4	171	152°4	77°6	231	205°8	104°9	291	259°3	132°1
52	46°3	23°6	112	99°8	50°8	172	153°3	78°1	232	206°7	105°3	292	260°2	132°6
53	47°2	24°1	113	100°7	51°3	173	154°1	78°5	233	207°6	105°8	293	261°1	133°0
54	48°1	24°5	114	101°6	51°8	174	155°0	79°0	234	208°5	106°2	294	262°0	133°5
55	49°0	25°0	115	102°5	52°2	175	155°9	79°4	235	209°4	106°7	295	262°8	133°9
56	49°9	25°4	116	103°4	52°7	176	156°8	79°9	236	210°3	107°1	296	263°7	134°4
57	50°8	25°9	117	104°2	53°1	177	157°7	80°4	237	211°2	107°6	297	264°6	134°8
58	51°7	26°3	118	105°1	53°6	178	158°6	80°8	238	212°1	108°0	298	265°5	135°3
59	52°6	26°8	119	106°0	54°0	179	159°5	81°3	239	213°0	108°5	299	266°4	135°7
60	53°5	27°2	120	106°9	54°5	180	160°4	81°7	240	213°8	109°0	300	267°3	136°2
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
63°												4 ^h 12 ^m		

TABLE 1

485

TRAVERSE TABLE TO DEGREES														
27°									1 ^h 48 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	268.2	136.7	361	321.7	163.9	421	375.1	191.1	481	428.6	218.3	541	482.0	245.6
302	269.1	137.1	362	322.5	164.4	422	376.0	191.6	482	429.4	218.8	542	482.9	246.1
303	270.0	137.6	363	323.4	164.8	423	376.9	192.0	483	430.3	219.2	543	483.8	246.5
304	270.9	138.0	364	324.3	165.3	424	377.8	192.5	484	431.2	219.7	544	484.7	247.0
305	271.8	138.5	365	325.2	165.7	425	378.7	193.0	485	432.1	220.1	545	485.6	247.4
306	272.7	138.9	366	326.1	166.2	426	379.6	193.4	486	433.0	220.6	546	486.4	247.9
307	273.5	139.4	367	327.0	166.6	427	380.5	193.9	487	433.9	221.1	547	487.3	248.4
308	274.4	139.8	368	327.9	167.1	428	381.4	194.3	488	434.8	221.5	548	488.2	248.8
309	275.3	140.3	369	328.8	167.5	429	382.2	194.8	489	435.7	222.0	549	489.1	249.2
310	276.2	140.7	370	329.7	168.0	430	383.1	195.2	490	436.6	222.4	550	490.0	249.7
311	277.1	141.2	371	330.6	168.4	431	384.0	195.7	491	437.5	222.9	551	490.9	250.1
312	278.0	141.7	372	331.5	168.9	432	384.9	196.1	492	438.3	223.3	552	491.8	250.6
313	278.9	142.1	373	332.3	169.3	433	385.8	196.6	493	439.2	223.8	553	492.7	251.0
314	279.8	142.6	374	333.2	169.8	434	386.7	197.0	494	440.1	224.2	554	493.6	251.5
315	280.7	143.0	375	334.1	170.3	435	387.6	197.5	495	441.0	224.7	555	494.5	252.0
316	281.6	143.5	376	335.0	170.7	436	388.5	197.9	496	441.9	225.2	556	495.4	252.4
317	282.5	143.9	377	335.9	171.2	437	389.4	198.4	497	442.8	225.6	557	496.3	252.9
318	283.3	144.4	378	336.8	171.6	438	390.3	198.9	498	443.7	226.1	558	497.2	253.3
319	284.2	144.8	379	337.7	172.1	439	391.2	199.3	499	444.6	226.5	559	498.1	253.8
320	285.1	145.3	380	338.6	172.5	440	392.0	199.8	500	445.5	227.0	560	499.0	254.2
321	286.0	145.7	381	339.5	173.0	441	392.9	200.2	501	446.4	227.5	561	499.8	254.7
322	286.9	146.2	382	340.4	173.4	442	393.8	200.7	502	447.3	227.9	562	500.7	255.1
323	287.8	146.6	383	341.3	173.9	443	394.7	201.1	503	448.2	228.4	563	501.6	255.6
324	288.7	147.1	384	342.1	174.3	444	395.6	201.6	504	449.0	228.8	564	502.5	256.0
325	289.6	147.6	385	343.0	174.8	445	396.5	202.0	505	449.9	229.3	565	503.4	256.5
326	290.5	148.0	386	343.9	175.2	446	397.4	202.5	506	450.8	229.8	566	504.3	257.0
327	291.4	148.5	387	344.8	175.7	447	398.3	202.9	507	451.7	230.2	567	505.2	257.4
328	292.3	148.9	388	345.7	176.2	448	399.2	203.4	508	452.6	230.6	568	506.1	257.9
329	293.2	149.4	389	346.6	176.6	449	400.1	203.8	509	453.5	231.0	569	507.0	258.3
330	294.0	149.8	390	347.5	177.1	450	401.0	204.3	510	454.4	231.5	570	507.9	258.8
331	294.9	150.3	391	348.4	177.5	451	401.8	204.7	511	455.3	231.9	571	508.7	259.2
332	295.8	150.7	392	349.3	178.0	452	402.7	205.2	512	456.2	232.4	572	509.6	259.7
333	296.7	151.2	393	350.2	178.4	453	403.6	205.7	513	457.1	232.9	573	510.5	260.1
334	297.6	151.6	394	351.1	178.9	454	404.5	206.1	514	458.0	233.3	574	511.4	260.6
335	298.5	152.1	395	352.0	179.3	455	405.4	206.6	515	458.8	233.8	575	512.3	261.1
336	299.4	152.5	396	352.8	179.8	456	406.3	207.0	516	459.7	234.2	576	513.2	261.5
337	300.3	153.0	397	353.7	180.2	457	407.2	207.5	517	460.6	234.7	577	514.1	262.0
338	301.2	153.5	398	354.6	180.7	458	408.1	207.9	518	461.5	235.2	578	515.0	262.4
339	302.1	153.9	399	355.5	181.2	459	409.0	208.4	519	462.4	235.7	579	515.9	262.9
340	302.9	154.4	400	356.4	181.6	460	409.9	208.8	520	463.3	236.1	580	516.8	263.4
341	303.8	154.8	401	357.3	182.1	461	410.8	209.3	521	464.2	236.6	581	517.7	263.8
342	304.7	155.3	402	358.2	182.5	462	411.6	209.8	522	465.1	237.0	582	518.5	264.3
343	305.6	155.7	403	359.1	183.0	463	412.5	210.2	523	466.0	237.5	583	519.4	264.7
344	306.5	156.2	404	360.0	183.4	464	413.4	210.7	524	466.9	237.9	584	520.3	265.2
345	307.4	156.6	405	360.9	183.9	465	414.3	211.1	525	467.8	238.4	585	521.2	265.6
346	308.3	157.1	406	361.8	184.3	466	415.2	211.6	526	468.7	238.8	586	522.1	266.0
347	309.2	157.5	407	362.6	184.8	467	416.1	212.0	527	469.5	239.3	587	523.0	266.5
348	310.1	158.0	408	363.5	185.2	468	417.0	212.5	528	470.4	239.7	588	523.9	267.0
349	311.0	158.5	409	364.4	185.7	469	417.9	212.9	529	471.3	240.2	589	524.8	267.4
350	311.9	158.9	410	365.3	186.1	470	418.8	213.4	530	472.2	240.6	590	525.7	267.9
351	312.7	159.4	411	366.2	186.6	471	419.7	213.8	531	473.1	241.1	591	526.6	268.3
352	313.6	159.8	412	367.1	187.1	472	420.6	214.3	532	474.0	241.5	592	527.5	268.8
353	314.5	160.3	413	368.0	187.5	473	421.4	214.7	533	474.9	242.0	593	528.4	269.2
354	315.4	160.7	414	368.9	188.0	474	422.3	215.2	534	475.8	242.4	594	529.3	269.7
355	316.3	161.2	415	369.8	188.4	475	423.2	215.7	535	476.7	242.9	595	530.1	270.1
356	317.2	161.6	416	370.7	188.9	476	424.1	216.1	536	477.6	243.4	596	531.0	270.6
357	318.1	162.1	417	371.6	189.3	477	425.0	216.6	537	478.4	243.8	597	531.9	271.1
358	319.0	162.5	418	372.4	189.8	478	425.9	217.0	538	479.3	244.3	598	532.8	271.5
359	319.9	163.0	419	373.3	190.2	479	426.8	217.5	539	480.2	244.7	599	533.7	272.0
360	320.8	163.4	420	374.2	190.7	480	427.7	217.9	540	481.1	245.2	600	534.6	272.4
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

69°

4^h 12^m

TRAVERSE TABLE TO DEGREES														
28°									1° 52'					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0°9	0°5	61	53°9	28°6	121	106°8	56°8	181	159°8	85°0	241	212°8	113°1
2	1°8	0°9	62	54°7	29°1	122	107°7	57°3	182	160°7	85°4	242	213°7	113°6
3	2°6	1°4	63	55°6	29°6	123	108°6	57°7	183	161°6	85°9	243	214°6	114°1
4	3°5	1°9	64	56°5	30°0	124	109°5	58°2	184	162°5	86°4	244	215°4	114°6
5	4°4	2°3	65	57°4	30°5	125	110°4	58°7	185	163°3	86°9	245	216°3	115°0
6	5°3	2°8	66	58°3	31°0	126	111°3	59°2	186	164°2	87°3	246	217°2	115°5
7	6°2	3°3	67	59°2	31°5	127	112°1	59°6	187	165°1	87°8	247	218°1	116°0
8	7°1	3°8	68	60°0	31°9	128	113°0	60°1	188	166°0	88°3	248	219°0	116°4
9	7°9	4°2	69	60°9	32°4	129	113°9	60°6	189	166°9	88°7	249	219°9	116°9
10	8°8	4°7	70	61°8	32°9	130	114°8	61°0	190	167°8	89°2	250	220°7	117°4
11	9°7	5°2	71	62°7	33°3	131	115°7	61°5	191	168°6	89°7	251	221°6	117°8
12	10°6	5°6	72	63°6	33°8	132	116°5	62°0	192	169°5	90°1	252	222°5	118°3
13	11°5	6°1	73	64°5	34°3	133	117°4	62°4	193	170°4	90°6	253	223°4	118°8
14	12°4	6°6	74	65°3	34°7	134	118°3	62°9	194	171°3	91°1	254	224°3	119°2
15	13°2	7°0	75	66°2	35°2	135	119°2	63°4	195	172°2	91°5	255	225°2	119°7
16	14°1	7°5	76	67°1	35°7	136	120°1	63°8	196	173°1	92°0	256	226°0	120°2
17	15°0	8°0	77	68°0	36°1	137	121°0	64°3	197	173°9	92°5	257	226°9	120°7
18	15°9	8°5	78	68°9	36°6	138	121°8	64°8	198	174°8	93°0	258	227°8	121°1
19	16°8	8°9	79	69°8	37°1	139	122°7	65°3	199	175°7	93°4	259	228°7	121°6
20	17°7	9°4	80	70°6	37°6	140	123°6	65°7	200	176°6	93°9	260	229°6	122°1
21	18°5	9°9	81	71°5	38°0	141	124°5	66°2	201	177°5	94°4	261	230°4	122°5
22	19°4	10°3	82	72°4	38°5	142	125°4	66°7	202	178°4	94°8	262	231°3	123°0
23	20°3	10°8	83	73°3	39°0	143	126°3	67°1	203	179°2	95°3	263	232°2	123°5
24	21°2	11°3	84	74°2	39°4	144	127°1	67°6	204	180°1	95°8	264	233°1	123°9
25	22°1	11°7	85	75°1	39°9	145	128°0	68°1	205	181°0	96°2	265	234°0	124°4
26	23°0	12°2	86	75°9	40°4	146	128°9	68°5	206	181°9	96°7	266	234°9	124°9
27	23°8	12°7	87	76°8	40°8	147	129°8	69°0	207	182°8	97°2	267	235°7	125°3
28	24°7	13°1	88	77°7	41°3	148	130°7	69°5	208	183°7	97°7	268	236°6	125°8
29	25°6	13°6	89	78°6	41°8	149	131°6	70°0	209	184°5	98°1	269	237°5	126°3
30	26°5	14°1	90	79°5	42°3	150	132°4	70°4	210	185°4	98°6	270	238°4	126°8
31	27°4	14°6	91	80°3	42°7	151	133°3	70°9	211	186°3	99°1	271	239°3	127°2
32	28°3	15°0	92	81°2	43°2	152	134°2	71°4	212	187°2	99°5	272	240°2	127°7
33	29°1	15°5	93	82°1	43°7	153	135°1	71°8	213	188°1	100°0	273	241°0	128°2
34	30°0	16°0	94	83°0	44°1	154	136°0	72°3	214	189°0	100°5	274	241°9	128°6
35	30°9	16°4	95	83°9	44°6	155	136°9	72°8	215	189°8	100°9	275	242°8	129°1
36	31°8	16°9	96	84°8	45°1	156	137°7	73°2	216	190°7	101°4	276	243°7	129°6
37	32°7	17°4	97	85°6	45°5	157	138°6	73°7	217	191°6	101°9	277	244°6	130°0
38	33°6	17°8	98	86°5	46°0	158	139°5	74°2	218	192°5	102°3	278	245°5	130°5
39	34°4	18°3	99	87°4	46°5	159	140°4	74°6	219	193°4	102°8	279	246°3	131°0
40	35°3	18°8	100	88°3	46°9	160	141°3	75°1	220	194°2	103°3	280	247°2	131°5
41	36°2	19°2	101	89°2	47°4	161	142°2	75°6	221	195°1	103°8	281	248°1	131°9
42	37°1	19°7	102	90°1	47°9	162	143°0	76°1	222	196°0	104°2	282	249°0	132°4
43	38°0	20°2	103	90°9	48°4	163	143°9	76°5	223	196°9	104°7	283	249°9	132°9
44	38°8	20°7	104	91°8	48°8	164	144°8	77°0	224	197°8	105°2	284	250°8	133°3
45	39°7	21°1	105	92°7	49°3	165	145°7	77°5	225	198°7	105°6	285	251°6	133°8
46	40°6	21°6	106	93°6	49°8	166	146°6	77°9	226	199°5	106°1	286	252°5	134°3
47	41°5	22°1	107	94°5	50°2	167	147°5	78°4	227	200°4	106°6	287	253°4	134°7
48	42°4	22°5	108	95°4	50°7	168	148°3	78°9	228	201°3	107°0	288	254°3	135°2
49	43°3	23°0	109	96°2	51°2	169	149°2	79°3	229	202°2	107°5	289	255°2	135°7
50	44°1	23°5	110	97°1	51°6	170	150°1	79°8	230	203°1	108°0	290	256°1	136°1
51	45°0	23°9	111	98°0	52°1	171	151°0	80°3	231	204°0	108°4	291	256°9	136°6
52	45°9	24°4	112	98°9	52°6	172	151°9	80°7	232	204°8	108°9	292	257°8	137°1
53	46°8	24°9	113	99°8	53°1	173	152°7	81°2	233	205°7	109°4	293	258°7	137°6
54	47°7	25°4	114	100°7	53°5	174	153°6	81°7	234	206°6	109°9	294	259°6	138°0
55	48°6	25°8	115	101°5	54°0	175	154°5	82°2	235	207°5	110°3	295	260°5	138°5
56	49°4	26°3	116	102°4	54°5	176	155°4	82°6	236	208°4	110°8	296	261°3	139°0
57	50°3	26°8	117	103°3	54°9	177	156°3	83°1	237	209°3	111°3	297	262°2	139°4
58	51°2	27°2	118	104°2	55°4	178	157°2	83°6	238	210°1	111°7	298	263°1	139°9
59	52°1	27°7	119	105°1	55°9	179	158°0	84°0	239	211°0	112°2	299	264°0	140°4
60	53°0	28°2	120	106°0	56°3	180	158°9	84°5	240	211°9	112°7	300	264°9	140°8
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

487

TRAVERSE TABLE TO DEGREES														
28°									1 ^h 52 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	265.7	141.3	361	318.7	169.5	421	371.7	197.7	481	424.7	225.8	541	477.7	254.0
302	266.6	141.8	362	319.6	170.0	422	372.6	198.1	482	425.6	226.3	542	478.6	254.5
303	267.5	142.3	363	320.5	170.4	423	373.5	198.6	483	426.5	226.8	543	479.4	255.0
304	268.4	142.7	364	321.4	170.9	424	374.3	199.1	484	427.4	227.3	544	480.3	255.5
305	269.3	143.2	365	322.2	171.4	425	375.2	199.5	485	428.3	227.7	545	481.1	255.9
306	270.2	143.7	366	323.1	171.8	426	376.1	200.0	486	429.2	228.2	546	482.0	256.4
307	271.0	144.1	367	324.0	172.3	427	377.0	200.5	487	430.1	228.6	547	482.9	256.9
308	271.9	144.6	368	324.9	172.8	428	377.9	200.9	488	430.9	229.1	548	483.8	257.3
309	272.8	145.1	369	325.8	173.2	429	378.8	201.4	489	431.8	229.6	549	484.7	257.8
310	273.7	145.5	370	326.7	173.7	430	379.6	201.9	490	432.6	230.0	550	485.6	258.2
311	274.6	146.0	371	327.5	174.2	431	380.5	202.3	491	433.5	230.5	551	486.5	258.7
312	275.5	146.5	372	328.4	174.6	432	381.4	202.8	492	434.4	231.0	552	487.4	259.1
313	276.3	146.9	373	329.3	175.1	433	382.3	203.3	493	435.3	231.4	553	488.3	259.6
314	277.2	147.4	374	330.2	175.6	434	383.2	203.8	494	436.2	231.9	554	489.2	260.1
315	278.1	147.9	375	331.1	176.1	435	384.1	204.2	495	437.1	232.4	555	490.1	260.6
316	279.0	148.4	376	332.0	176.5	436	384.9	204.7	496	437.9	232.9	556	490.9	261.0
317	279.9	148.8	377	332.8	177.0	437	385.8	205.2	497	438.8	233.4	557	491.8	261.5
318	280.7	149.3	378	333.7	177.5	438	386.7	205.6	498	439.7	233.8	558	492.7	262.0
319	281.6	149.8	379	334.6	177.9	439	387.6	206.1	499	440.6	234.3	559	493.5	262.5
320	282.5	150.2	380	335.5	178.4	440	388.5	206.6	500	441.5	234.7	560	494.4	262.9
321	283.4	150.7	381	336.4	178.9	441	389.4	207.0	501	442.3	235.2	561	495.3	263.4
322	284.3	151.2	382	337.3	179.3	442	390.2	207.5	502	443.2	235.6	562	496.2	263.8
323	285.2	151.6	383	338.1	179.8	443	391.1	208.0	503	444.1	236.1	563	497.1	264.3
324	286.0	152.1	384	339.0	180.3	444	392.0	208.4	504	445.0	236.6	564	498.0	264.7
325	286.9	152.6	385	339.9	180.8	445	392.9	208.9	505	445.9	237.1	565	498.9	265.2
326	287.8	153.1	386	340.8	181.2	446	393.8	209.4	506	446.8	237.5	566	499.8	265.7
327	288.7	153.5	387	341.7	181.7	447	394.6	209.9	507	447.6	238.0	567	500.7	266.2
328	289.6	154.0	388	342.6	182.2	448	395.5	210.3	508	448.5	238.5	568	501.6	266.6
329	290.5	154.5	389	343.4	182.6	449	396.4	210.8	509	449.4	239.0	569	502.4	267.1
330	291.3	154.9	390	344.3	183.1	450	397.3	211.3	510	450.3	239.4	570	503.3	267.6
331	292.2	155.4	391	345.2	183.6	451	398.2	211.7	511	451.2	239.9	571	504.2	268.0
332	293.1	155.9	392	346.1	184.0	452	399.1	212.2	512	452.1	240.4	572	505.1	268.5
333	294.0	156.3	393	347.0	184.5	453	399.9	212.7	513	452.9	240.8	573	505.9	269.0
334	294.9	156.8	394	347.9	185.0	454	400.8	213.1	514	453.8	241.3	574	506.8	269.4
335	295.8	157.3	395	348.7	185.4	455	401.7	213.6	515	454.7	241.8	575	507.7	269.9
336	296.6	157.7	396	349.6	185.9	456	402.6	214.1	516	455.6	242.2	576	508.6	270.4
337	297.5	158.2	397	350.5	186.4	457	403.5	214.6	517	456.4	242.7	577	509.4	270.9
338	298.4	158.7	398	351.4	186.9	458	404.4	215.0	518	457.3	243.2	578	510.3	271.3
339	299.3	159.2	399	352.3	187.3	459	405.2	215.5	519	458.2	243.7	579	511.2	271.8
340	300.2	159.6	400	353.1	187.8	460	406.1	216.0	520	459.1	244.1	580	512.1	272.3
341	301.0	160.1	401	354.0	188.3	461	407.0	216.4	521	460.0	244.6	581	513.0	272.7
342	301.9	160.6	402	354.9	188.7	462	407.9	216.9	522	460.9	245.0	582	513.9	273.2
343	302.8	161.0	403	355.8	189.2	463	408.8	217.4	523	461.8	245.5	583	514.8	273.7
344	303.7	161.5	404	356.7	189.7	464	409.7	217.8	524	462.7	246.0	584	515.7	274.2
345	304.6	162.0	405	357.6	190.1	465	410.5	218.3	525	463.5	246.5	585	516.5	274.7
346	305.5	162.4	406	358.4	190.6	466	411.4	218.8	526	464.4	246.9	586	517.4	275.1
347	306.4	162.9	407	359.3	191.1	467	412.3	219.2	527	465.3	247.4	587	518.3	275.5
348	307.2	163.4	408	360.2	191.5	468	413.2	219.7	528	466.2	247.9	588	519.2	276.0
349	308.1	163.8	409	361.1	192.0	469	414.1	220.2	529	467.1	248.3	589	520.1	276.5
350	309.0	164.3	410	362.0	192.5	470	415.0	220.7	530	468.0	248.8	590	521.0	277.0
351	309.9	164.8	411	362.9	193.0	471	415.8	221.1	531	468.9	249.3	591	521.8	277.4
352	310.8	165.3	412	363.7	193.4	472	416.7	221.6	532	469.8	249.8	592	522.6	277.9
353	311.7	165.7	413	364.6	193.9	473	417.6	222.1	533	470.7	250.2	593	523.5	278.4
354	312.5	166.2	414	365.5	194.4	474	418.5	222.5	534	471.5	250.7	594	524.4	278.8
355	313.4	166.7	415	366.4	194.8	475	419.4	223.0	535	472.4	251.1	595	525.3	279.3
356	314.3	167.1	416	367.3	195.3	476	420.3	223.5	536	473.3	251.6	596	526.2	279.8
357	315.2	167.6	417	368.2	195.8	477	421.1	223.9	537	474.2	252.1	597	527.1	280.3
358	316.1	168.1	418	369.0	196.2	478	422.0	224.4	538	475.1	252.6	598	528.0	280.8
359	316.9	168.5	419	369.9	196.7	479	422.9	224.9	539	476.0	253.1	599	528.9	281.3
360	317.8	169.0	420	370.8	197.2	480	423.8	225.3	540	476.8	253.6	600	529.8	281.7
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

62°

4^h 8^m

TABLE 1

TRAVERSE TABLE TO DEGREES														
29°									1° 50'					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0.9	0.5	61	53.4	29.6	121	105.8	58.7	181	158.3	87.8	241	210.8	116.8
2	1.7	1.0	62	54.2	30.1	122	106.7	59.1	182	159.2	88.2	242	211.7	117.3
3	2.6	1.5	63	55.1	30.5	123	107.6	59.6	183	160.1	88.7	243	212.5	117.8
4	3.5	1.9	64	56.0	31.0	124	108.5	60.1	184	160.9	89.2	244	213.4	118.3
5	4.4	2.4	65	56.9	31.5	125	109.3	60.6	185	161.8	89.7	245	214.3	118.8
6	5.2	2.9	66	57.7	32.0	126	110.2	61.1	186	162.7	90.2	246	215.2	119.3
7	6.1	3.4	67	58.6	32.5	127	111.1	61.6	187	163.6	90.7	247	216.0	119.7
8	7.0	3.9	68	59.5	33.0	128	112.0	62.1	188	164.4	91.1	248	216.9	120.2
9	7.9	4.4	69	60.3	33.5	129	112.8	62.5	189	165.3	91.6	249	217.8	120.7
10	8.7	4.8	70	61.2	33.9	130	113.7	63.0	190	166.2	92.1	250	218.7	121.2
11	9.6	5.3	71	62.1	34.4	131	114.6	63.5	191	167.1	92.6	251	219.5	121.7
12	10.5	5.8	72	63.0	34.9	132	115.4	64.0	192	167.9	93.1	252	220.4	122.2
13	11.4	6.3	73	63.8	35.4	133	116.3	64.5	193	168.8	93.6	253	221.3	122.7
14	12.2	6.8	74	64.7	35.9	134	117.2	65.0	194	169.7	94.1	254	222.2	123.1
15	13.1	7.3	75	65.6	36.4	135	118.1	65.4	195	170.6	94.5	255	223.0	123.6
16	14.0	7.8	76	66.5	36.8	136	118.9	65.9	196	171.4	95.0	256	223.9	124.1
17	14.9	8.2	77	67.3	37.3	137	119.8	66.4	197	172.3	95.5	257	224.8	124.6
18	15.7	8.7	78	68.2	37.8	138	120.7	66.9	198	173.2	96.0	258	225.7	125.1
19	16.6	9.2	79	69.1	38.3	139	121.6	67.4	199	174.0	96.5	259	226.5	125.6
20	17.5	9.7	80	70.0	38.8	140	122.4	67.9	200	174.9	97.0	260	227.4	126.1
21	18.4	10.2	81	70.8	39.3	141	123.3	68.4	201	175.8	97.4	261	228.3	126.5
22	19.2	10.7	82	71.7	39.8	142	124.2	68.8	202	176.7	97.9	262	229.2	127.0
23	20.1	11.2	83	72.6	40.2	143	125.1	69.3	203	177.5	98.4	263	230.0	127.5
24	21.0	11.6	84	73.5	40.7	144	125.9	69.8	204	178.4	98.9	264	230.9	128.0
25	21.9	12.1	85	74.3	41.2	145	126.8	70.3	205	179.3	99.4	265	231.8	128.5
26	22.7	12.6	86	75.2	41.7	146	127.7	70.8	206	180.2	99.9	266	232.6	129.0
27	23.6	13.1	87	76.1	42.2	147	128.6	71.3	207	181.0	100.4	267	233.5	129.4
28	24.5	13.6	88	77.0	42.7	148	129.4	71.8	208	181.9	100.8	268	234.4	129.9
29	25.4	14.1	89	77.8	43.1	149	130.3	72.2	209	182.8	101.3	269	235.3	130.4
30	26.2	14.5	90	78.7	43.6	150	131.2	72.7	210	183.7	101.8	270	236.1	130.9
31	27.1	15.0	91	79.6	44.1	151	132.1	73.2	211	184.5	102.3	271	237.0	131.4
32	28.0	15.5	92	80.5	44.6	152	132.9	73.7	212	185.4	102.8	272	237.9	131.9
33	28.9	16.0	93	81.3	45.1	153	133.8	74.2	213	186.3	103.3	273	238.8	132.4
34	29.7	16.5	94	82.2	45.6	154	134.7	74.7	214	187.2	103.7	274	239.6	132.8
35	30.6	17.0	95	83.1	46.1	155	135.6	75.1	215	188.0	104.2	275	240.5	133.3
36	31.5	17.5	96	84.0	46.5	156	136.4	75.6	216	188.9	104.7	276	241.4	133.8
37	32.4	17.9	97	84.8	47.0	157	137.3	76.1	217	189.8	105.2	277	242.3	134.3
38	33.2	18.4	98	85.7	47.5	158	138.2	76.6	218	190.7	105.7	278	243.1	134.8
39	34.1	18.9	99	86.6	48.0	159	139.1	77.1	219	191.5	106.2	279	244.0	135.3
40	35.0	19.4	100	87.5	48.5	160	139.9	77.6	220	192.4	106.7	280	244.9	135.7
41	35.9	19.9	101	88.3	49.0	161	140.8	78.1	221	193.3	107.1	281	245.8	136.2
42	36.7	20.4	102	89.2	49.5	162	141.7	78.5	222	194.2	107.6	282	246.6	136.7
43	37.6	20.8	103	90.1	49.9	163	142.6	79.0	223	195.0	108.1	283	247.5	137.2
44	38.5	21.3	104	91.0	50.4	164	143.4	79.5	224	195.9	108.6	284	248.4	137.7
45	39.4	21.8	105	91.8	50.9	165	144.3	80.0	225	196.8	109.1	285	249.3	138.2
46	40.2	22.3	106	92.7	51.4	166	145.2	80.5	226	197.7	109.6	286	250.1	138.7
47	41.1	22.8	107	93.6	51.9	167	146.1	81.0	227	198.5	110.1	287	251.0	139.1
48	42.0	23.3	108	94.5	52.4	168	146.9	81.4	228	199.4	110.5	288	251.9	139.6
49	42.9	23.8	109	95.3	52.8	169	147.8	81.9	229	200.3	111.0	289	252.8	140.1
50	43.7	24.2	110	96.2	53.3	170	148.7	82.4	230	201.2	111.5	290	253.6	140.6
51	44.6	24.7	111	97.1	53.8	171	149.6	82.9	231	202.0	112.0	291	254.5	141.1
52	45.5	25.2	112	98.0	54.3	172	150.4	83.4	232	202.9	112.5	292	255.4	141.6
53	46.4	25.7	113	98.8	54.8	173	151.3	83.9	233	203.8	113.0	293	256.3	142.0
54	47.2	26.2	114	99.7	55.3	174	152.2	84.4	234	204.7	113.4	294	257.1	142.5
55	48.1	26.7	115	100.6	55.8	175	153.1	84.8	235	205.5	113.9	295	258.0	143.0
56	49.0	27.1	116	101.5	56.2	176	153.9	85.3	236	206.4	114.4	296	258.9	143.5
57	49.9	27.6	117	102.3	56.7	177	154.8	85.8	237	207.3	114.9	297	259.8	144.0
58	50.7	28.1	118	103.2	57.2	178	155.7	86.3	238	208.2	115.4	298	260.6	144.5
59	51.6	28.6	119	104.1	57.7	179	156.6	86.8	239	209.0	115.9	299	261.5	145.0
60	52.5	29.1	120	105.0	58.2	180	157.4	87.3	240	209.9	116.4	300	262.4	145.4
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

489

TRAVERSE TABLE TO DEGREES

29°									1 ^h 56 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	263.2	145.9	361	315.7	175.0	421	368.2	204.1	481	420.7	233.2	541	473.2	262.3
302	264.1	146.4	362	316.6	175.5	422	369.1	204.6	482	421.5	233.7	542	474.0	262.8
303	265.0	146.9	363	317.5	176.0	423	369.9	205.1	483	422.4	234.2	543	474.9	263.2
304	265.9	147.4	364	318.3	176.5	424	370.8	205.6	484	423.3	234.6	544	475.8	263.7
305	266.7	147.9	365	319.2	177.0	425	371.7	206.0	485	424.2	235.1	545	476.6	264.2
306	267.6	148.4	366	320.1	177.4	426	372.6	206.5	486	425.0	235.6	546	477.5	264.7
307	268.5	148.8	367	321.0	177.9	427	373.4	207.0	487	425.9	236.1	547	478.4	265.2
308	269.4	149.3	368	321.8	178.4	428	374.3	207.5	488	426.8	236.6	548	479.3	265.7
309	270.2	149.8	369	322.7	178.9	429	375.2	208.0	489	427.7	237.1	549	480.1	266.2
310	271.1	150.3	370	323.6	179.4	430	376.1	208.5	490	428.5	237.6	550	481.0	266.6
311	272.0	150.8	371	324.5	179.9	431	376.9	209.0	491	429.4	238.0	551	481.9	267.1
312	272.9	151.3	372	325.3	180.4	432	377.8	209.4	492	430.3	238.5	552	482.8	267.6
313	273.7	151.7	373	326.2	180.8	433	378.7	209.9	493	431.2	239.0	553	483.6	268.1
314	274.6	152.2	374	327.1	181.3	434	379.6	210.4	494	432.0	239.5	554	484.5	268.6
315	275.5	152.7	375	328.0	181.8	435	380.4	210.9	495	432.9	240.0	555	485.4	269.1
316	276.3	153.2	376	328.8	182.3	436	381.3	211.4	496	433.8	240.5	556	486.3	269.5
317	277.2	153.7	377	329.7	182.8	437	382.2	211.9	497	434.7	240.9	557	487.1	270.0
318	278.1	154.2	378	330.6	183.3	438	383.1	212.3	498	435.5	241.4	558	488.0	270.5
319	279.0	154.7	379	331.4	183.7	439	383.9	212.8	499	436.4	241.9	559	488.9	271.0
320	279.8	155.1	380	332.3	184.2	440	384.8	213.3	500	437.3	242.4	560	489.8	271.5
321	280.7	155.6	381	333.2	184.7	441	385.7	213.8	501	438.2	242.9	561	490.6	272.0
322	281.6	156.1	382	334.1	185.2	442	386.6	214.3	502	439.0	243.4	562	491.5	272.5
323	282.5	156.6	383	334.9	185.7	443	387.4	214.8	503	439.9	243.9	563	492.4	272.9
324	283.3	157.1	384	335.8	186.2	444	388.3	215.3	504	440.8	244.3	564	493.2	273.4
325	284.2	157.6	385	336.7	186.7	445	389.2	215.7	505	441.6	244.8	565	494.1	273.9
326	285.1	158.1	386	337.6	187.1	446	390.0	216.2	506	442.5	245.3	566	495.0	274.4
327	286.0	158.5	387	338.4	187.6	447	390.9	216.7	507	443.4	245.8	567	495.9	274.9
328	286.8	159.0	388	339.3	188.1	448	391.8	217.2	508	444.3	246.3	568	496.8	275.4
329	287.7	159.5	389	340.2	188.6	449	392.7	217.7	509	445.2	246.8	569	497.7	275.9
330	288.6	160.0	390	341.1	189.1	450	393.5	218.2	510	446.1	247.3	570	498.5	276.3
331	289.5	160.5	391	341.9	189.6	451	394.4	218.7	511	447.0	247.8	571	499.4	276.8
332	290.3	161.0	392	342.8	190.0	452	395.3	219.1	512	447.8	248.2	572	500.3	277.3
333	291.2	161.4	393	343.7	190.5	453	396.2	219.6	513	448.6	248.7	573	501.1	277.8
334	292.1	161.9	394	344.6	191.0	454	397.0	220.1	514	449.5	249.2	574	502.0	278.3
335	293.0	162.4	395	345.4	191.5	455	397.9	220.6	515	450.4	249.7	575	502.9	278.8
336	293.8	162.9	396	346.3	192.0	456	398.8	221.1	516	451.3	250.2	576	503.7	279.2
337	294.7	163.4	397	347.2	192.5	457	399.7	221.6	517	452.2	250.6	577	504.6	279.7
338	295.6	163.9	398	348.1	193.0	458	400.5	222.0	518	453.1	251.1	578	505.5	280.2
339	296.5	164.4	399	348.9	193.4	459	401.4	222.5	519	453.9	251.6	579	506.4	280.7
340	297.3	164.8	400	349.8	193.9	460	402.3	223.0	520	454.8	252.1	580	507.2	281.2
341	298.2	165.3	401	350.7	194.4	461	403.2	223.5	521	455.6	252.6	581	508.1	281.7
342	299.1	165.8	402	351.6	194.9	462	404.0	224.0	522	456.5	253.1	582	509.0	282.2
343	300.0	166.3	403	352.4	195.4	463	404.9	224.5	523	457.4	253.6	583	509.9	282.7
344	300.8	166.8	404	353.3	195.9	464	405.8	225.0	524	458.3	254.0	584	510.7	283.2
345	301.7	167.3	405	354.2	196.3	465	406.7	225.4	525	459.1	254.5	585	511.6	283.6
346	302.6	167.7	406	355.1	196.8	466	407.5	225.9	526	460.0	255.0	586	512.5	284.1
347	303.5	168.2	407	355.9	197.3	467	408.4	226.4	527	460.9	255.5	587	513.4	284.6
348	304.3	168.7	408	356.8	197.8	468	409.3	226.9	528	461.8	256.0	588	514.3	285.0
349	305.2	169.2	409	357.7	198.3	469	410.2	227.4	529	462.6	256.5	589	515.1	285.5
350	306.1	169.7	410	358.6	198.8	470	411.0	227.9	530	463.5	256.9	590	516.0	286.0
351	307.0	170.2	411	359.4	199.3	471	411.9	228.3	531	464.4	257.4	591	516.9	286.5
352	307.8	170.7	412	360.3	199.7	472	412.8	228.8	532	465.3	257.9	592	517.7	287.0
353	308.7	171.1	413	361.2	200.2	473	413.7	229.3	533	466.1	258.4	593	518.6	287.5
354	309.6	171.6	414	362.1	200.7	474	414.5	229.8	534	467.0	258.9	594	519.5	288.0
355	310.5	172.1	415	362.9	201.2	475	415.4	230.3	535	467.9	259.4	595	520.4	288.5
356	311.3	172.6	416	363.8	201.7	476	416.3	230.8	536	468.8	259.9	596	521.2	288.9
357	312.2	173.1	417	364.7	202.2	477	417.2	231.3	537	469.6	260.3	597	522.1	289.4
358	313.1	173.6	418	365.6	202.7	478	418.0	231.7	538	470.5	260.8	598	523.0	289.9
359	314.0	174.0	419	366.4	203.1	479	418.9	232.2	539	471.4	261.3	599	523.9	290.4
360	314.8	174.5	420	367.3	203.6	480	419.8	232.7	540	472.3	261.8	600	524.8	290.9
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

61°

4^h 4^m

TRAVERSE TABLE TO DEGREES														
30°									2° 0'					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0.9	0.5	61	52.8	30.5	121	104.8	60.5	181	156.8	90.5	241	208.7	120.5
2	1.7	1.0	62	53.7	31.0	122	105.7	61.0	182	157.6	91.0	242	209.6	121.0
3	2.6	1.5	63	54.6	31.5	123	106.5	61.5	183	158.5	91.5	243	210.4	121.5
4	3.5	2.0	64	55.4	32.0	124	107.4	62.0	184	159.3	92.0	244	211.3	122.0
5	4.3	2.5	65	56.3	32.5	125	108.3	62.5	185	160.2	92.5	245	212.2	122.5
6	5.2	3.0	66	57.2	33.0	126	109.1	63.0	186	161.1	93.0	246	213.0	123.0
7	6.1	3.5	67	58.0	33.5	127	110.0	63.5	187	161.9	93.5	247	213.9	123.5
8	6.9	4.0	68	58.9	34.0	128	110.9	64.0	188	162.8	94.0	248	214.8	124.0
9	7.8	4.5	69	59.8	34.5	129	111.7	64.5	189	163.7	94.5	249	215.6	124.5
10	8.7	5.0	70	60.6	35.0	130	112.6	65.0	190	164.5	95.0	250	216.5	125.0
11	9.5	5.5	71	61.5	35.5	131	113.4	65.5	191	165.4	95.5	251	217.4	125.5
12	10.4	6.0	72	62.4	36.0	132	114.3	66.0	192	166.3	96.0	252	218.2	126.0
13	11.3	6.5	73	63.2	36.5	133	115.2	66.5	193	167.1	96.5	253	219.1	126.5
14	12.1	7.0	74	64.1	37.0	134	116.0	67.0	194	168.0	97.0	254	220.0	127.0
15	13.0	7.5	75	65.0	37.5	135	116.9	67.5	195	168.9	97.5	255	220.8	127.5
16	13.9	8.0	76	65.8	38.0	136	117.8	68.0	196	169.7	98.0	256	221.7	128.0
17	14.7	8.5	77	66.7	38.5	137	118.6	68.5	197	170.6	98.5	257	222.6	128.5
18	15.6	9.0	78	67.5	39.0	138	119.5	69.0	198	171.5	99.0	258	223.4	129.0
19	16.5	9.5	79	68.4	39.5	139	120.4	69.5	199	172.3	99.5	259	224.3	129.5
20	17.3	10.0	80	69.3	40.0	140	121.2	70.0	200	173.2	100.0	260	225.2	130.0
21	18.2	10.5	81	70.1	40.5	141	122.1	70.5	201	174.1	100.5	261	226.0	130.5
22	19.1	11.0	82	71.0	41.0	142	123.0	71.0	202	174.9	101.0	262	226.9	131.0
23	19.9	11.5	83	71.9	41.5	143	123.8	71.5	203	175.8	101.5	263	227.8	131.5
24	20.8	12.0	84	72.7	42.0	144	124.7	72.0	204	176.7	102.0	264	228.6	132.0
25	21.7	12.5	85	73.6	42.5	145	125.6	72.5	205	177.5	102.5	265	229.5	132.5
26	22.5	13.0	86	74.5	43.0	146	126.4	73.0	206	178.4	103.0	266	230.4	133.0
27	23.4	13.5	87	75.3	43.5	147	127.3	73.5	207	179.3	103.5	267	231.2	133.5
28	24.2	14.0	88	76.2	44.0	148	128.2	74.0	208	180.1	104.0	268	232.1	134.0
29	25.1	14.5	89	77.1	44.5	149	129.0	74.5	209	181.0	104.5	269	233.0	134.5
30	26.0	15.0	90	77.9	45.0	150	129.9	75.0	210	181.9	105.0	270	233.8	135.0
31	26.8	15.5	91	78.8	45.5	151	130.8	75.5	211	182.7	105.5	271	234.7	135.5
32	27.7	16.0	92	79.7	46.0	152	131.6	76.0	212	183.6	106.0	272	235.6	136.0
33	28.6	16.5	93	80.5	46.5	153	132.5	76.5	213	184.5	106.5	273	236.4	136.5
34	29.4	17.0	94	81.4	47.0	154	133.4	77.0	214	185.3	107.0	274	237.3	137.0
35	30.3	17.5	95	82.3	47.5	155	134.2	77.5	215	186.2	107.5	275	238.2	137.5
36	31.2	18.0	96	83.1	48.0	156	135.1	78.0	216	187.1	108.0	276	239.0	138.0
37	32.0	18.5	97	84.0	48.5	157	136.0	78.5	217	187.9	108.5	277	239.9	138.5
38	32.9	19.0	98	84.9	49.0	158	136.8	79.0	218	188.8	109.0	278	240.8	139.0
39	33.8	19.5	99	85.7	49.5	159	137.7	79.5	219	189.7	109.5	279	241.6	139.5
40	34.6	20.0	100	86.6	50.0	160	138.6	80.0	220	190.5	110.0	280	242.5	140.0
41	35.5	20.5	101	87.5	50.5	161	139.4	80.5	221	191.4	110.5	281	243.4	140.5
42	36.4	21.0	102	88.3	51.0	162	140.3	81.0	222	192.3	111.0	282	244.2	141.0
43	37.2	21.5	103	89.2	51.5	163	141.2	81.5	223	193.1	111.5	283	245.1	141.5
44	38.1	22.0	104	90.1	52.0	164	142.0	82.0	224	194.0	112.0	284	246.0	142.0
45	39.0	22.5	105	90.9	52.5	165	142.9	82.5	225	194.9	112.5	285	246.8	142.5
46	39.8	23.0	106	91.8	53.0	166	143.8	83.0	226	195.7	113.0	286	247.7	143.0
47	40.7	23.5	107	92.7	53.5	167	144.6	83.5	227	196.6	113.5	287	248.5	143.5
48	41.6	24.0	108	93.5	54.0	168	145.5	84.0	228	197.5	114.0	288	249.4	144.0
49	42.4	24.5	109	94.4	54.5	169	146.4	84.5	229	198.3	114.5	289	250.3	144.5
50	43.3	25.0	110	95.3	55.0	170	147.2	85.0	230	199.2	115.0	290	251.1	145.0
51	44.2	25.5	111	96.1	55.5	171	148.1	85.5	231	200.1	115.5	291	252.0	145.5
52	45.0	26.0	112	97.0	56.0	172	149.0	86.0	232	200.9	116.0	292	252.9	146.0
53	45.9	26.5	113	97.9	56.5	173	149.8	86.5	233	201.8	116.5	293	253.7	146.5
54	46.8	27.0	114	98.7	57.0	174	150.7	87.0	234	202.6	117.0	294	254.6	147.0
55	47.6	27.5	115	99.6	57.5	175	151.6	87.5	235	203.5	117.5	295	255.5	147.5
56	48.5	28.0	116	100.5	58.0	176	152.4	88.0	236	204.4	118.0	296	256.3	148.0
57	49.4	28.5	117	101.3	58.5	177	153.3	88.5	237	205.2	118.5	297	257.2	148.5
58	50.2	29.0	118	102.2	59.0	178	154.2	89.0	238	206.1	119.0	298	258.1	149.0
59	51.1	29.5	119	103.1	59.5	179	155.0	89.5	239	207.0	119.5	299	258.9	149.5
60	52.0	30.0	120	103.9	60.0	180	155.9	90.0	240	207.8	120.0	300	259.8	150.0
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
60°									4° 0'					

TRAVERSE TABLE TO DEGREES

31°															2 ^h 4 ^m		
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0.9	0.5	61	52.3	31.4	121	103.7	62.3	181	155.1	93.2	241	206.6	124.1			
2	1.7	1.0	62	53.1	31.9	122	104.6	62.8	182	156.0	93.7	242	207.4	124.6			
3	2.6	1.5	63	54.0	32.4	123	105.4	63.3	183	156.9	94.3	243	208.3	125.2			
4	3.4	2.1	64	54.9	33.0	124	106.3	63.9	184	157.7	94.8	244	209.1	125.7			
5	4.3	2.6	65	55.7	33.5	125	107.1	64.4	185	158.6	95.3	245	210.0	126.2			
6	5.1	3.1	66	56.6	34.0	126	108.0	64.9	186	159.4	95.8	246	210.9	126.7			
7	6.0	3.6	67	57.4	34.5	127	108.9	65.4	187	160.3	96.3	247	211.7	127.2			
8	6.9	4.1	68	58.3	35.0	128	109.7	65.9	188	161.1	96.8	248	212.6	127.7			
9	7.7	4.6	69	59.1	35.5	129	110.6	66.4	189	162.0	97.3	249	213.4	128.2			
10	8.6	5.2	70	60.0	36.1	130	111.4	67.0	190	162.9	97.9	250	214.3	128.8			
11	9.4	5.7	71	60.9	36.6	131	112.3	67.5	191	163.7	98.4	251	215.1	129.3			
12	10.3	6.2	72	61.7	37.1	132	113.1	68.0	192	164.6	98.9	252	216.0	129.8			
13	11.1	6.7	73	62.6	37.6	133	114.0	68.5	193	165.4	99.4	253	216.9	130.3			
14	12.0	7.2	74	63.4	38.1	134	114.9	69.0	194	166.3	99.9	254	217.7	130.8			
15	12.9	7.7	75	64.3	38.6	135	115.7	69.5	195	167.1	100.4	255	218.6	131.3			
16	13.7	8.2	76	65.1	39.1	136	116.6	70.0	196	168.0	100.9	256	219.4	131.8			
17	14.6	8.8	77	66.0	39.7	137	117.4	70.6	197	168.9	101.5	257	220.3	132.4			
18	15.4	9.3	78	66.9	40.2	138	118.3	71.1	198	169.7	102.0	258	221.1	132.9			
19	16.3	9.8	79	67.7	40.7	139	119.1	71.6	199	170.6	102.5	259	222.0	133.4			
20	17.1	10.3	80	68.6	41.2	140	120.0	72.1	200	171.4	103.0	260	222.9	133.9			
21	18.0	10.8	81	69.4	41.7	141	120.9	72.6	201	172.3	103.5	261	223.7	134.4			
22	18.9	11.3	82	70.3	42.2	142	121.7	73.1	202	173.1	104.0	262	224.6	134.9			
23	19.7	11.8	83	71.1	42.7	143	122.6	73.7	203	174.0	104.6	263	225.4	135.5			
24	20.6	12.4	84	72.0	43.3	144	123.4	74.2	204	174.9	105.1	264	226.3	136.0			
25	21.4	12.9	85	72.9	43.8	145	124.3	74.7	205	175.7	105.6	265	227.1	136.5			
26	22.3	13.4	86	73.7	44.3	146	125.1	75.2	206	176.6	106.1	266	228.0	137.0			
27	23.1	13.9	87	74.6	44.8	147	126.0	75.7	207	177.4	106.6	267	228.9	137.5			
28	24.0	14.4	88	75.4	45.3	148	126.9	76.2	208	178.3	107.1	268	229.7	138.0			
29	24.9	14.9	89	76.3	45.8	149	127.7	76.7	209	179.1	107.6	269	230.6	138.5			
30	25.7	15.5	90	77.1	46.4	150	128.6	77.3	210	180.0	108.2	270	231.4	139.1			
31	26.6	16.0	91	78.0	46.9	151	129.4	77.8	211	180.9	108.7	271	232.3	139.6			
32	27.4	16.5	92	78.9	47.4	152	130.3	78.3	212	181.7	109.2	272	233.1	140.1			
33	28.3	17.0	93	79.7	47.9	153	131.1	78.8	213	182.6	109.7	273	234.0	140.6			
34	29.1	17.5	94	80.6	48.4	154	132.0	79.3	214	183.4	110.2	274	234.9	141.1			
35	30.0	18.0	95	81.4	48.9	155	132.9	79.8	215	184.3	110.7	275	235.7	141.6			
36	30.9	18.5	96	82.3	49.4	156	133.7	80.3	216	185.1	111.2	276	236.6	142.2			
37	31.7	19.1	97	83.1	50.0	157	134.6	80.9	217	186.0	111.8	277	237.4	142.7			
38	32.6	19.6	98	84.0	50.5	158	135.4	81.4	218	186.9	112.3	278	238.3	143.2			
39	33.4	20.1	99	84.9	51.0	159	136.3	81.9	219	187.7	112.8	279	239.1	143.7			
40	34.3	20.6	100	85.7	51.5	160	137.1	82.4	220	188.6	113.3	280	240.0	144.2			
41	35.1	21.1	101	86.6	52.0	161	138.0	82.9	221	189.4	113.8	281	240.9	144.7			
42	36.0	21.6	102	87.4	52.5	162	138.9	83.4	222	190.3	114.3	282	241.7	145.2			
43	36.9	22.1	103	88.3	53.0	163	139.7	84.0	223	191.1	114.9	283	242.6	145.8			
44	37.7	22.7	104	89.1	53.6	164	140.6	84.5	224	192.0	115.4	284	243.4	146.3			
45	38.6	23.2	105	90.0	54.1	165	141.4	85.0	225	192.9	115.9	285	244.3	146.8			
46	39.4	23.7	106	90.9	54.6	166	142.3	85.5	226	193.7	116.4	286	245.1	147.3			
47	40.3	24.2	107	91.7	55.1	167	143.1	86.0	227	194.6	116.9	287	246.0	147.8			
48	41.1	24.7	108	92.6	55.6	168	144.0	86.5	228	195.4	117.4	288	246.9	148.3			
49	42.0	25.2	109	93.4	56.1	169	144.9	87.0	229	196.3	117.9	289	247.7	148.8			
50	42.9	25.8	110	94.3	56.7	170	145.7	87.6	230	197.1	118.5	290	248.6	149.4			
51	43.7	26.3	111	95.1	57.2	171	146.6	88.1	231	198.0	119.0	291	249.4	149.9			
52	44.6	26.8	112	96.0	57.7	172	147.4	88.6	232	198.9	119.5	292	250.3	150.4			
53	45.4	27.3	113	96.9	58.2	173	148.3	89.1	233	199.7	120.0	293	251.2	150.9			
54	46.3	27.8	114	97.7	58.7	174	149.1	89.6	234	200.6	120.5	294	252.0	151.4			
55	47.1	28.3	115	98.6	59.2	175	150.0	90.1	235	201.4	121.0	295	252.9	151.9			
56	48.0	28.8	116	99.4	59.7	176	150.9	90.6	236	202.3	121.5	296	253.7	152.5			
57	48.9	29.4	117	100.3	60.3	177	151.7	91.2	237	203.1	122.1	297	254.6	153.0			
58	49.7	29.9	118	101.1	60.8	178	152.6	91.7	238	204.0	122.6	298	255.4	153.5			
59	50.6	30.4	119	102.0	61.3	179	153.4	92.2	239	204.9	123.1	299	256.3	154.0			
60	51.4	30.9	120	102.9	61.8	180	154.3	92.7	240	205.7	123.6	300	257.1	154.5			
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	59°		
															3 ^h 56 ^m		

TABLE 1

489

TRAVERSE TABLE TO DEGREES														
81°									2h 4 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	258.0	155.0	361	309.4	185.9	421	360.9	216.8	481	412.3	247.7	541	463.7	278.6
302	258.9	155.5	362	310.3	186.4	422	361.7	217.3	482	413.2	248.2	542	464.6	279.1
303	259.7	156.1	363	311.2	187.0	423	362.6	217.9	483	414.0	248.8	543	465.4	279.7
304	260.6	156.6	364	312.0	187.5	424	363.4	218.4	484	414.9	249.3	544	466.3	280.2
305	261.4	157.1	365	312.9	188.0	425	364.3	218.9	485	415.7	249.8	545	467.2	280.7
306	262.3	157.6	366	313.7	188.5	426	365.2	219.4	486	416.6	250.3	546	468.0	281.2
307	263.2	158.1	367	314.6	189.0	427	366.0	219.9	487	417.4	250.8	547	468.9	281.7
308	264.0	158.6	368	315.4	189.5	428	366.9	220.4	488	418.3	251.3	548	469.7	282.3
309	264.9	159.2	369	316.3	190.1	429	367.7	221.0	489	419.2	251.9	549	470.6	282.8
310	265.7	159.7	370	317.2	190.6	430	368.6	221.5	490	420.0	252.4	550	471.4	283.3
311	266.6	160.2	371	318.0	191.1	431	369.4	222.0	491	420.9	252.9	551	472.3	283.8
312	267.4	160.7	372	318.9	191.6	432	370.3	222.5	492	421.7	253.4	552	473.2	284.3
313	268.3	161.2	373	319.7	192.1	433	371.2	223.0	493	422.6	253.9	553	474.0	284.8
314	269.2	161.7	374	320.6	192.6	434	372.0	223.5	494	423.4	254.4	554	474.9	285.3
315	270.0	162.2	375	321.4	193.1	435	372.9	224.0	495	424.3	254.9	555	475.7	285.8
316	270.9	162.8	376	322.3	193.7	436	373.7	224.6	496	425.2	255.5	556	476.6	286.4
317	271.7	163.3	377	323.2	194.2	437	374.6	225.1	497	426.0	256.0	557	477.4	286.9
318	272.6	163.8	378	324.0	194.7	438	375.4	225.6	498	426.9	256.5	558	478.3	287.4
319	273.4	164.3	379	324.9	195.2	439	376.3	226.1	499	427.7	257.0	559	479.2	287.9
320	274.3	164.8	380	325.7	195.7	440	377.2	226.6	500	428.6	257.5	560	480.0	288.4
321	275.2	165.3	381	326.6	196.2	441	378.0	227.1	501	429.4	258.0	561	480.9	288.9
322	276.0	165.8	382	327.4	196.7	442	378.9	227.7	502	430.3	258.6	562	481.7	289.5
323	276.9	166.4	383	328.3	197.3	443	379.7	228.2	503	431.2	259.1	563	482.6	290.0
324	277.7	166.9	384	329.2	197.8	444	380.6	228.7	504	432.0	259.6	564	483.4	290.5
325	278.6	167.4	385	330.0	198.3	445	381.4	229.2	505	432.9	260.1	565	484.3	291.0
326	279.4	167.9	386	330.9	198.8	446	382.3	229.7	506	433.7	260.6	566	485.2	291.5
327	280.3	168.4	387	331.7	199.3	447	383.2	230.2	507	434.6	261.1	567	486.0	292.0
328	281.2	168.9	388	332.6	199.8	448	384.0	230.7	508	435.4	261.6	568	486.9	292.5
329	282.0	169.5	389	333.4	200.4	449	384.9	231.3	509	436.3	262.2	569	487.7	293.1
330	282.9	170.0	390	334.3	200.9	450	385.7	231.8	510	437.2	262.7	570	488.6	293.6
331	283.7	170.5	391	335.2	201.4	451	386.6	232.3	511	438.0	263.2	571	489.4	294.1
332	284.6	171.0	392	336.0	201.9	452	387.4	232.8	512	438.9	263.7	572	490.3	294.6
333	285.4	171.5	393	336.9	202.4	453	388.3	233.3	513	439.7	264.2	573	491.2	295.1
334	286.3	172.0	394	337.7	202.9	454	389.2	233.8	514	440.6	264.7	574	492.0	295.6
335	287.2	172.5	395	338.6	203.4	455	390.0	234.3	515	441.4	265.2	575	492.9	296.1
336	288.0	173.1	396	339.4	204.0	456	390.9	234.9	516	442.3	265.8	576	493.7	296.7
337	288.9	173.6	397	340.3	204.5	457	391.7	235.4	517	443.2	266.3	577	494.6	297.2
338	289.7	174.1	398	341.2	205.0	458	392.6	235.9	518	444.0	266.8	578	495.4	297.7
339	290.6	174.6	399	342.0	205.5	459	393.4	236.4	519	444.9	267.3	579	496.3	298.2
340	291.4	175.1	400	342.9	206.0	460	394.3	236.9	520	445.7	267.8	580	497.2	298.7
341	292.3	175.6	401	343.7	206.5	461	395.2	237.4	521	446.6	268.3	581	498.0	299.2
342	293.2	176.1	402	344.6	207.0	462	396.0	238.0	522	447.4	268.9	582	498.9	299.8
343	294.0	176.7	403	345.4	207.6	463	396.9	238.5	523	448.3	269.4	583	499.7	300.3
344	294.9	177.2	404	346.3	208.1	464	397.7	239.0	524	449.2	269.9	584	500.6	300.8
345	295.7	177.7	405	347.2	208.6	465	398.6	239.5	525	450.0	270.4	585	501.4	301.3
346	296.6	178.2	406	348.0	209.1	466	399.4	240.0	526	450.9	270.9	586	502.3	301.8
347	297.4	178.7	407	348.9	209.6	467	400.3	240.5	527	451.7	271.4	587	503.2	302.3
348	298.3	179.2	408	349.7	210.1	468	401.2	241.0	528	452.6	271.9	588	504.0	302.8
349	299.2	179.8	409	350.6	210.7	469	402.0	241.5	529	453.4	272.4	589	504.9	303.3
350	300.0	180.3	410	351.4	211.2	470	402.9	242.1	530	454.3	273.0	590	505.7	303.9
351	300.9	180.8	411	352.3	211.7	471	403.7	242.6	531	455.2	273.5	591	506.6	304.4
352	301.7	181.3	412	353.2	212.2	472	404.6	243.1	532	456.0	274.0	592	507.4	304.9
353	302.6	181.8	413	354.0	212.7	473	405.4	243.6	533	456.9	274.5	593	508.3	305.4
354	303.4	182.3	414	354.9	213.2	474	406.3	244.1	534	457.7	275.0	594	509.2	305.9
355	304.3	182.8	415	355.7	213.7	475	407.2	244.6	535	458.6	275.5	595	510.0	306.4
356	305.2	183.4	416	356.6	214.3	476	408.0	245.2	536	459.4	276.1	596	510.9	307.0
357	306.0	183.9	417	357.4	214.8	477	408.9	245.7	537	460.3	276.6	597	511.7	307.5
358	306.9	184.4	418	358.3	215.3	478	409.7	246.2	538	461.2	277.1	598	512.6	308.0
359	307.7	184.9	419	359.2	215.8	479	410.6	246.7	539	462.0	277.6	599	513.4	308.5
360	308.6	185.4	420	360.0	216.3	480	411.4	247.2	540	462.9	278.1	600	514.3	309.0
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
59°									8h 56 ^m					

TRAVERSE TABLE TO DEGREES														
33°														
2 ^h 8 ^m														
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0.8	0.5	61	51.7	32.3	121	102.6	64.1	181	153.5	95.9	241	204.4	127.7
2	1.7	1.1	62	52.6	32.9	122	103.5	64.7	182	154.3	96.4	242	205.2	128.2
3	2.5	1.6	63	53.4	33.4	123	104.3	65.2	183	155.2	97.0	243	206.1	128.8
4	3.4	2.1	64	54.3	33.9	124	105.2	65.7	184	156.0	97.5	244	206.9	129.3
5	4.2	2.6	65	55.1	34.4	125	106.0	66.2	185	156.9	98.0	245	207.8	129.8
6	5.1	3.2	66	56.0	35.0	126	106.9	66.8	186	157.7	98.6	246	208.6	130.4
7	5.9	3.7	67	56.8	35.5	127	107.7	67.3	187	158.6	99.1	247	209.5	130.9
8	6.8	4.2	68	57.7	36.0	128	108.6	67.8	188	159.4	99.6	248	210.3	131.4
9	7.6	4.8	69	58.5	36.6	129	109.4	68.4	189	160.3	100.2	249	211.2	131.9
10	8.5	5.3	70	59.4	37.1	130	110.2	68.9	190	161.1	100.7	250	212.0	132.5
11	9.3	5.8	71	60.2	37.6	131	111.1	69.4	191	162.0	101.2	251	212.9	133.0
12	10.2	6.4	72	61.1	38.2	132	111.9	69.9	192	162.8	101.7	252	213.7	133.5
13	11.0	6.9	73	61.9	38.7	133	112.8	70.5	193	163.7	102.3	253	214.6	134.1
14	11.9	7.4	74	62.8	39.2	134	113.6	71.0	194	164.5	102.8	254	215.4	134.6
15	12.7	7.9	75	63.6	39.7	135	114.5	71.5	195	165.4	103.3	255	216.3	135.1
16	13.6	8.5	76	64.5	40.3	136	115.3	72.1	196	166.2	103.9	256	217.1	135.7
17	14.4	9.0	77	65.3	40.8	137	116.2	72.6	197	167.1	104.4	257	217.9	136.2
18	15.3	9.5	78	66.1	41.3	138	117.0	73.1	198	167.9	104.9	258	218.8	136.7
19	16.1	10.1	79	67.0	41.9	139	117.9	73.7	199	168.8	105.5	259	219.6	137.2
20	17.0	10.6	80	67.8	42.4	140	118.7	74.2	200	169.6	106.0	260	220.5	137.8
21	17.8	11.1	81	68.7	42.9	141	119.6	74.7	201	170.5	106.5	261	221.3	138.3
22	18.7	11.7	82	69.5	43.5	142	120.4	75.2	202	171.3	107.0	262	222.2	138.8
23	19.5	12.2	83	70.4	44.0	143	121.3	75.8	203	172.2	107.6	263	223.0	139.4
24	20.4	12.7	84	71.2	44.5	144	122.1	76.3	204	173.1	108.1	264	223.9	139.9
25	21.2	13.2	85	72.1	45.0	145	123.0	76.8	205	173.8	108.6	265	224.7	140.4
26	22.0	13.8	86	72.9	45.6	146	123.8	77.4	206	174.7	109.2	266	225.6	141.0
27	22.9	14.3	87	73.8	46.1	147	124.7	77.9	207	175.5	109.7	267	226.4	141.5
28	23.7	14.8	88	74.6	46.6	148	125.5	78.4	208	176.4	110.2	268	227.3	142.0
29	24.6	15.4	89	75.5	47.2	149	126.4	79.0	209	177.2	110.8	269	228.1	142.5
30	25.4	15.9	90	76.3	47.7	150	127.2	79.5	210	178.1	111.3	270	229.0	143.1
31	26.3	16.4	91	77.2	48.2	151	128.1	80.0	211	178.9	111.8	271	229.8	143.6
32	27.1	17.0	92	78.0	48.8	152	128.9	80.5	212	179.8	112.3	272	230.7	144.1
33	28.0	17.5	93	78.9	49.3	153	129.8	81.1	213	180.6	112.9	273	231.5	144.7
34	28.8	18.0	94	79.7	49.8	154	130.6	81.6	214	181.5	113.4	274	232.4	145.2
35	29.7	18.5	95	80.6	50.3	155	131.4	82.1	215	182.3	113.9	275	233.2	145.7
36	30.5	19.1	96	81.4	50.9	156	132.3	82.7	216	183.2	114.5	276	234.1	146.3
37	31.4	19.6	97	82.3	51.4	157	133.1	83.2	217	184.0	115.0	277	234.9	146.8
38	32.2	20.1	98	83.1	51.9	158	134.0	83.7	218	184.9	115.5	278	235.8	147.3
39	33.1	20.7	99	84.0	52.5	159	134.8	84.3	219	185.7	116.1	279	236.6	147.8
40	33.9	21.2	100	84.8	53.0	160	135.7	84.8	220	186.6	116.6	280	237.5	148.4
41	34.8	21.7	101	85.7	53.5	161	136.5	85.3	221	187.4	117.1	281	238.3	148.9
42	35.6	22.3	102	86.5	54.1	162	137.4	85.8	222	188.3	117.6	282	239.1	149.4
43	36.5	22.8	103	87.3	54.6	163	138.2	86.4	223	189.1	118.2	283	240.0	150.0
44	37.3	23.3	104	88.2	55.1	164	139.1	86.9	224	190.0	118.7	284	240.8	150.5
45	38.2	23.8	105	89.0	55.6	165	139.9	87.4	225	190.8	119.2	285	241.7	151.0
46	39.0	24.4	106	89.9	56.2	166	140.8	88.0	226	191.7	119.8	286	242.5	151.6
47	39.9	24.9	107	90.7	56.7	167	141.6	88.5	227	192.5	120.3	287	243.4	152.1
48	40.7	25.4	108	91.6	57.2	168	142.5	89.0	228	193.4	120.8	288	244.2	152.6
49	41.6	26.0	109	92.4	57.8	169	143.3	89.6	229	194.2	121.4	289	245.1	153.1
50	42.4	26.5	110	93.3	58.3	170	144.2	90.1	230	195.1	121.9	290	245.9	153.7
51	43.3	27.0	111	94.1	58.8	171	145.0	90.6	231	195.9	122.4	291	246.8	154.2
52	44.1	27.6	112	95.0	59.4	172	145.9	91.1	232	196.7	122.9	292	247.6	154.7
53	44.9	28.1	113	95.8	59.9	173	146.7	91.7	233	197.6	123.5	293	248.5	155.3
54	45.8	28.6	114	96.7	60.4	174	147.6	92.2	234	198.4	124.0	294	249.3	155.8
55	46.6	29.1	115	97.5	60.9	175	148.4	92.7	235	199.3	124.5	295	250.2	156.3
56	47.5	29.7	116	98.4	61.5	176	149.3	93.3	236	200.1	125.1	296	251.0	156.9
57	48.3	30.2	117	99.2	62.0	177	150.1	93.8	237	201.0	125.6	297	251.9	157.4
58	49.2	30.7	118	100.1	62.5	178	151.0	94.3	238	201.8	126.1	298	252.7	157.9
59	50.0	31.3	119	100.9	63.1	179	151.8	94.9	239	202.7	126.7	299	253.6	158.4
60	50.9	31.8	120	101.8	63.6	180	152.6	95.4	240	203.5	127.2	300	254.4	159.0
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

495

TRAVERSE TABLE TO DEGREES

32°														2 ^h 8 ^m	
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	
801	255°3	159°5	361	306°2	191°3	421	357°0	223°1	481	407°9	254°9	541	458°8	286°7	
802	256°1	160°0	362	307°0	191°8	422	357°9	223°6	482	408°8	255°4	542	459°6	287°2	
803	257°0	160°5	363	307°9	192°3	423	358°7	224°1	483	409°6	255°9	543	460°5	287°7	
804	257°8	161°1	364	308°7	192°9	424	359°6	224°7	484	410°5	256°5	544	461°3	288°3	
805	258°7	161°6	365	309°5	193°4	425	360°4	225°2	485	411°3	257°0	545	462°2	288°8	
806	259°5	162°1	366	310°4	193°9	426	361°3	225°7	486	412°2	257°5	546	463°0	289°3	
807	260°4	162°7	367	311°2	194°5	427	362°1	226°3	487	413°0	258°1	547	463°9	289°9	
808	261°2	163°2	368	312°1	195°0	428	363°0	226°8	488	413°9	258°6	548	464°7	290°4	
809	262°1	163°7	369	312°9	195°5	429	363°8	227°3	489	414°7	259°1	549	465°6	290°9	
810	262°9	164°3	370	313°8	196°0	430	364°7	227°8	490	415°6	259°6	550	466°4	291°5	
811	263°8	164°8	371	314°6	196°6	431	365°5	228°4	491	416°4	260°2	551	467°3	292°0	
812	264°6	165°3	372	315°5	197°1	432	366°4	228°9	492	417°3	260°7	552	468°1	292°5	
813	265°4	165°8	373	316°3	197°6	433	367°2	229°4	493	418°1	261°2	553	469°0	293°0	
814	266°3	166°4	374	317°2	198°2	434	368°1	230°0	494	419°0	261°8	554	469°8	293°6	
815	267°1	166°9	375	318°0	198°7	435	368°9	230°5	495	419°8	262°3	555	470°7	294°1	
816	268°0	167°4	376	318°9	199°2	436	369°8	231°0	496	420°6	262°8	556	471°5	294°6	
817	268°8	168°0	377	319°7	199°8	437	370°6	231°6	497	421°5	263°4	557	472°4	295°2	
818	269°7	168°5	378	320°6	200°3	438	371°5	232°1	498	422°3	263°9	558	473°2	295°7	
819	270°5	169°0	379	321°4	200°8	439	372°3	232°6	499	423°2	264°4	559	474°1	296°2	
820	271°4	169°6	380	322°3	201°3	440	373°2	233°1	500	424°0	265°0	560	474°9	296°7	
821	272°2	170°1	381	323°1	201°9	441	374°0	233°7	501	424°9	265°5	561	475°8	297°3	
822	273°1	170°6	382	324°0	202°4	442	374°8	234°2	502	425°7	266°0	562	476°6	297°8	
823	273°9	171°1	383	324°8	202°9	443	375°7	234°7	503	426°6	266°5	563	477°5	298°3	
824	274°8	171°7	384	325°7	203°5	444	376°5	235°3	504	427°4	267°1	564	478°3	298°9	
825	275°6	172°2	385	326°5	204°0	445	377°4	235°8	505	428°3	267°6	565	479°2	299°4	
826	276°5	172°7	386	327°4	204°5	446	378°2	236°3	506	429°1	268°1	566	480°0	299°9	
827	277°3	173°3	387	328°2	205°1	447	379°1	236°9	507	430°0	268°7	567	480°9	300°5	
828	278°2	173°8	388	329°1	205°6	448	379°9	237°4	508	430°8	269°2	568	481°7	301°0	
829	279°0	174°3	389	329°9	206°1	449	380°8	237°9	509	431°7	269°7	569	482°6	301°5	
830	279°9	174°9	390	330°8	206°6	450	381°6	238°4	510	432°5	270°3	570	483°4	302°1	
831	280°7	175°4	391	331°6	207°2	451	382°5	239°0	511	433°4	270°8	571	484°3	302°6	
832	281°6	175°9	392	332°5	207°7	452	383°3	239°5	512	434°2	271°4	572	485°1	303°2	
833	282°4	176°4	393	333°3	208°2	453	384°2	240°0	513	435°1	271°9	573	486°0	303°7	
834	283°3	177°0	394	334°2	208°8	454	385°0	240°6	514	435°9	272°4	574	486°8	304°2	
835	284°1	177°5	395	335°0	209°3	455	385°9	241°1	515	436°8	272°9	575	487°7	304°7	
836	285°0	178°0	396	335°8	209°8	456	386°7	241°6	516	437°6	273°5	576	488°5	305°3	
837	285°8	178°6	397	336°7	210°4	457	387°6	242°2	517	438°5	274°0	577	489°4	305°8	
838	286°7	179°1	398	337°5	210°9	458	388°4	242°7	518	439°3	274°5	578	490°2	306°3	
839	287°5	179°6	399	338°4	211°4	459	389°3	243°2	519	440°2	275°0	579	491°1	306°8	
840	288°3	180°2	400	339°2	211°9	460	390°1	243°8	520	441°0	275°6	580	491°9	307°4	
841	289°2	180°7	401	340°1	212°5	461	391°0	244°3	521	441°9	276°1	581	492°8	307°9	
842	290°0	181°2	402	340°9	213°0	462	391°8	244°8	522	442°7	276°6	582	493°6	308°4	
843	290°9	181°7	403	341°8	213°5	463	392°7	245°4	523	443°6	277°2	583	494°5	309°0	
844	291°7	182°3	404	342°6	214°1	464	393°5	245°9	524	444°4	277°7	584	495°3	309°5	
845	292°6	182°8	405	343°5	214°6	465	394°4	246°4	525	445°3	278°2	585	496°2	310°0	
846	293°4	183°3	406	344°3	215°1	466	395°2	246°9	526	446°1	278°7	586	497°0	310°5	
847	294°3	183°9	407	345°2	215°7	467	396°0	247°5	527	446°9	279°3	587	497°8	311°1	
848	295°1	184°4	408	346°0	216°2	468	396°9	248°0	528	447°8	279°8	588	498°7	311°6	
849	296°0	184°9	409	346°9	216°7	469	397°7	248°5	529	448°6	280°3	589	499°5	312°1	
850	296°8	185°4	410	347°7	217°2	470	398°6	249°0	530	449°5	280°9	590	500°3	312°6	
851	297°7	186°0	411	348°6	217°8	471	399°4	249°6	531	450°3	281°4	591	501°2	313°2	
852	298°5	186°5	412	349°4	218°3	472	400°3	250°1	532	451°1	281°9	592	502°0	313°7	
853	299°4	187°0	413	350°3	218°8	473	401°1	250°6	533	452°0	282°4	593	502°9	314°2	
854	300°2	187°6	414	351°1	219°4	474	402°0	251°2	534	452°8	283°0	594	503°7	314°8	
855	301°1	188°1	415	352°0	219°9	475	402°8	251°7	535	453°7	283°5	595	504°6	315°3	
856	301°9	188°6	416	352°8	220°4	476	403°7	252°2	536	454°5	284°0	596	505°4	315°8	
857	302°8	189°2	417	353°6	221°0	477	404°5	252°8	537	455°4	284°6	597	506°2	316°4	
858	303°6	189°7	418	354°5	221°5	478	405°4	253°3	538	456°2	285°1	598	507°1	316°9	
859	304°5	190°2	419	355°3	222°0	479	406°2	253°8	539	457°1	285°6	599	508°0	317°4	
860	305°3	190°8	420	356°2	222°5	480	407°1	254°3	540	457°9	286°2	600	508°8	318°0	
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	
58°														3 ^h 52 ^m	

TRAVERSE TABLE TO DEGREES															
33°															
								2 ^h 12 ^m							
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.
1	0.8	0.5	61	51.2	33.2	121	101.5	65.9	181	151.8	98.6	241	202.1	131.3	
2	1.7	1.1	62	52.0	33.8	122	102.3	66.4	182	152.6	99.1	242	203.0	131.8	
3	2.5	1.6	63	52.8	34.3	123	103.2	67.0	183	153.5	99.7	243	203.8	132.3	
4	3.4	2.2	64	53.7	34.9	124	104.0	67.5	184	154.3	100.2	244	204.6	132.9	
5	4.2	2.7	65	54.5	35.4	125	104.8	68.1	185	155.2	100.8	245	205.5	133.4	
6	5.0	3.3	66	55.4	35.9	126	105.7	68.6	186	156.0	101.3	246	206.3	134.0	
7	5.9	3.8	67	56.2	36.5	127	106.5	69.2	187	156.8	101.8	247	207.2	134.5	
8	6.7	4.4	68	57.0	37.0	128	107.3	69.7	188	157.7	102.4	248	208.0	135.1	
9	7.5	4.9	69	57.9	37.6	129	108.2	70.3	189	158.5	102.9	249	208.8	135.6	
10	8.4	5.4	70	58.7	38.1	130	109.0	70.8	190	159.3	103.5	250	209.7	136.2	
11	9.2	6.0	71	59.5	38.7	131	109.9	71.3	191	160.2	104.0	251	210.5	136.7	
12	10.1	6.5	72	60.4	39.2	132	110.7	71.9	192	161.0	104.6	252	211.3	137.2	
13	10.9	7.1	73	61.2	39.8	133	111.5	72.4	193	161.9	105.1	253	212.2	137.8	
14	11.7	7.6	74	62.1	40.3	134	112.4	73.0	194	162.7	105.7	254	213.0	138.3	
15	12.6	8.2	75	62.9	40.8	135	113.2	73.5	195	163.5	106.2	255	213.9	138.9	
16	13.4	8.7	76	63.7	41.4	136	114.1	74.1	196	164.4	106.7	256	214.7	139.4	
17	14.3	9.3	77	64.6	41.9	137	114.9	74.6	197	165.2	107.3	257	215.5	140.0	
18	15.1	9.8	78	65.4	42.5	138	115.7	75.2	198	166.1	107.8	258	216.4	140.5	
19	15.9	10.3	79	66.3	43.0	139	116.6	75.7	199	166.9	108.4	259	217.2	141.1	
20	16.8	10.9	80	67.1	43.6	140	117.4	76.2	200	167.7	108.9	260	218.1	141.6	
21	17.6	11.4	81	67.9	44.1	141	118.3	76.8	201	168.6	109.5	261	218.9	142.2	
22	18.5	12.0	82	68.8	44.7	142	119.1	77.3	202	169.4	110.0	262	219.7	142.7	
23	19.3	12.5	83	69.6	45.2	143	119.9	77.9	203	170.3	110.6	263	220.6	143.2	
24	20.1	13.1	84	70.4	45.7	144	120.8	78.4	204	171.1	111.1	264	221.4	143.8	
25	21.0	13.6	85	71.3	46.3	145	121.6	79.0	205	171.9	111.7	265	222.2	144.3	
26	21.8	14.2	86	72.1	46.8	146	122.4	79.5	206	172.8	112.2	266	223.1	144.9	
27	22.6	14.7	87	73.0	47.4	147	123.3	80.1	207	173.6	112.7	267	223.9	145.4	
28	23.5	15.2	88	73.8	47.9	148	124.1	80.6	208	174.4	113.3	268	224.8	146.0	
29	24.3	15.8	89	74.6	48.5	149	125.0	81.2	209	175.3	113.8	269	225.6	146.5	
30	25.2	16.3	90	75.5	49.0	150	125.8	81.7	210	176.1	114.4	270	226.4	147.1	
31	26.0	16.9	91	76.3	49.6	151	126.6	82.2	211	177.0	114.9	271	227.3	147.6	
32	26.8	17.4	92	77.2	50.1	152	127.5	82.8	212	177.8	115.5	272	228.1	148.1	
33	27.7	18.0	93	78.0	50.7	153	128.3	83.3	213	178.6	116.0	273	229.0	148.7	
34	28.5	18.5	94	78.8	51.2	154	129.2	83.9	214	179.5	116.6	274	229.8	149.2	
35	29.4	19.1	95	79.7	51.7	155	130.0	84.4	215	180.3	117.1	275	230.6	149.8	
36	30.2	19.6	96	80.5	52.3	156	130.8	85.0	216	181.2	117.6	276	231.5	150.3	
37	31.0	20.2	97	81.4	52.8	157	131.7	85.5	217	182.0	118.2	277	232.3	150.9	
38	31.9	20.7	98	82.2	53.4	158	132.5	86.1	218	182.8	118.7	278	233.2	151.4	
39	32.7	21.2	99	83.0	53.9	159	133.3	86.6	219	183.7	119.3	279	234.0	152.0	
40	33.5	21.8	100	83.9	54.5	160	134.2	87.1	220	184.5	119.8	280	234.8	152.5	
41	34.4	22.3	101	84.7	55.0	161	135.0	87.7	221	185.3	120.4	281	235.7	153.0	
42	35.2	22.9	102	85.5	55.6	162	135.9	88.2	222	186.2	120.9	282	236.5	153.6	
43	36.1	23.4	103	86.4	56.1	163	136.7	88.8	223	187.0	121.5	283	237.3	154.1	
44	36.9	24.0	104	87.2	56.6	164	137.5	89.3	224	187.9	122.0	284	238.2	154.7	
45	37.7	24.5	105	88.1	57.2	165	138.4	89.9	225	188.7	122.5	285	239.0	155.2	
46	38.6	25.1	106	88.9	57.7	166	139.2	90.4	226	189.5	123.1	286	239.9	155.8	
47	39.4	25.6	107	89.7	58.3	167	140.1	91.0	227	190.4	123.6	287	240.7	156.3	
48	40.3	26.1	108	90.6	58.8	168	140.9	91.5	228	191.2	124.2	288	241.5	156.9	
49	41.1	26.7	109	91.4	59.4	169	141.7	92.0	229	192.1	124.7	289	242.4	157.4	
50	41.9	27.2	110	92.3	59.9	170	142.6	92.6	230	192.9	125.3	290	243.2	157.9	
51	42.8	27.8	111	93.1	60.5	171	143.4	93.1	231	193.7	125.8	291	244.1	158.5	
52	43.6	28.3	112	93.9	61.0	172	144.3	93.7	232	194.6	126.4	292	244.9	159.0	
53	44.4	28.9	113	94.8	61.5	173	145.1	94.2	233	195.4	126.9	293	245.7	159.6	
54	45.3	29.4	114	95.6	62.1	174	145.9	94.8	234	196.2	127.4	294	246.6	160.1	
55	46.1	30.0	115	96.4	62.6	175	146.8	95.3	235	197.1	128.0	295	247.4	160.7	
56	47.0	30.5	116	97.3	63.2	176	147.6	95.9	236	197.9	128.5	296	248.2	161.2	
57	47.8	31.0	117	98.1	63.7	177	148.4	96.4	237	198.8	129.1	297	249.1	161.8	
58	48.6	31.6	118	99.0	64.3	178	149.3	96.9	238	199.6	129.6	298	249.9	162.3	
59	49.5	32.1	119	99.8	64.8	179	150.1	97.5	239	200.4	130.2	299	250.8	162.8	
60	50.3	32.7	120	100.6	65.4	180	151.0	98.0	240	201.3	130.7	300	251.6	163.4	
37°															
								3 ^h 48 ^m							
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.

TABLE 1

497

TRAVERSE TABLE TO DEGREES

88°

2h 12m

Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	252.4	163.9	361	302.8	196.6	421	353.1	229.3	481	403.4	262.0	541	453.7	294.6
302	253.3	164.4	362	303.6	197.1	422	353.9	229.8	482	404.2	262.5	542	454.6	295.2
303	254.1	165.0	363	304.4	197.7	423	354.7	230.4	483	405.1	263.1	543	455.4	295.7
304	255.0	165.5	364	305.3	198.2	424	355.6	230.9	484	405.9	263.6	544	456.2	296.2
305	255.8	166.1	365	306.1	198.8	425	356.4	231.4	485	406.7	264.1	545	457.1	296.8
306	256.6	166.6	366	307.0	199.3	426	357.3	232.0	486	407.6	264.7	546	457.9	297.3
307	257.5	167.2	367	307.8	199.8	427	358.1	232.5	487	408.4	265.2	547	458.8	297.9
308	258.3	167.7	368	308.6	200.4	428	359.0	233.1	488	409.3	265.8	548	459.6	298.4
309	259.2	168.3	369	309.5	200.9	429	359.8	233.6	489	410.1	266.3	549	460.4	299.0
310	260.0	168.8	370	310.3	201.5	430	360.6	234.2	490	411.0	266.8	550	461.3	299.5
311	260.8	169.3	371	311.2	202.0	431	361.5	234.7	491	411.8	267.4	551	462.1	300.1
312	261.7	169.9	372	312.0	202.6	432	362.3	235.3	492	412.6	267.9	552	463.0	300.6
313	262.5	170.4	373	312.8	203.1	433	363.1	235.8	493	413.5	268.5	553	463.8	301.2
314	263.3	171.0	374	313.7	203.7	434	364.0	236.3	494	414.3	269.0	554	464.6	301.7
315	264.2	171.5	375	314.5	204.2	435	364.8	236.9	495	415.1	269.6	555	465.5	302.3
316	265.0	172.1	376	315.3	204.7	436	365.7	237.4	496	416.0	270.1	556	466.3	302.9
317	265.9	172.6	377	316.2	205.3	437	366.5	238.0	497	416.8	270.7	557	467.2	303.4
318	266.7	173.2	378	317.0	205.8	438	367.3	238.5	498	417.6	271.2	558	468.0	303.9
319	267.5	173.7	379	317.9	206.4	439	368.2	239.1	499	418.5	271.8	559	468.8	304.5
320	268.4	174.2	380	318.7	206.9	440	369.0	239.6	500	419.3	272.3	560	469.7	305.0
321	269.2	174.8	381	319.5	207.5	441	369.9	240.1	501	420.2	272.8	561	470.5	305.5
322	270.1	175.3	382	320.4	208.0	442	370.7	240.7	502	421.0	273.4	562	471.3	306.1
323	270.9	175.9	383	321.2	208.6	443	371.5	241.2	503	421.9	273.9	563	472.2	306.6
324	271.7	176.4	384	322.1	209.1	444	372.4	241.8	504	422.7	274.5	564	473.0	307.2
325	272.6	177.0	385	322.9	209.6	445	373.2	242.3	505	423.5	275.0	565	473.8	307.7
326	273.4	177.5	386	323.7	210.2	446	374.1	242.9	506	424.4	275.6	566	474.7	308.3
327	274.2	178.1	387	324.6	210.7	447	374.9	243.4	507	425.2	276.1	567	475.5	308.8
328	275.1	178.6	388	325.4	211.3	448	375.7	244.0	508	426.0	276.7	568	476.4	309.4
329	275.9	179.1	389	326.2	211.8	449	376.6	244.5	509	426.9	277.2	569	477.2	309.9
330	276.8	179.7	390	327.1	212.4	450	377.4	245.1	510	427.7	277.8	570	478.0	310.4
331	277.6	180.2	391	327.9	212.9	451	378.2	245.6	511	428.5	278.3	571	478.9	311.0
332	278.4	180.8	392	328.8	213.5	452	379.1	246.1	512	429.4	278.8	572	479.7	311.5
333	279.3	181.3	393	329.6	214.0	453	379.9	246.7	513	430.2	279.4	573	480.6	312.0
334	280.1	181.9	394	330.4	214.6	454	380.8	247.2	514	431.1	279.9	574	481.4	312.6
335	281.0	182.4	395	331.3	215.1	455	381.6	247.8	515	431.9	280.4	575	482.2	313.1
336	281.8	183.0	396	332.1	215.6	456	382.4	248.3	516	432.7	281.0	576	483.1	313.7
337	282.6	183.5	397	333.0	216.2	457	383.3	248.9	517	433.6	281.5	577	483.9	314.2
338	283.5	184.1	398	333.8	216.7	458	384.1	249.4	518	434.4	282.1	578	484.7	314.8
339	284.3	184.6	399	334.6	217.3	459	385.0	250.0	519	435.3	282.6	579	485.6	315.3
340	285.2	185.1	400	335.5	217.8	460	385.8	250.5	520	436.1	283.2	580	486.4	315.9
341	286.0	185.7	401	336.3	218.4	461	386.6	251.0	521	436.9	283.7	581	487.2	316.4
342	286.8	186.2	402	337.1	218.9	462	387.5	251.6	522	437.8	284.3	582	488.1	317.0
343	287.7	186.8	403	338.0	219.5	463	388.3	252.1	523	438.6	284.8	583	488.9	317.5
344	288.5	187.3	404	338.8	220.0	464	389.1	252.7	524	439.4	285.4	584	489.8	318.1
345	289.3	187.9	405	339.7	220.5	465	390.0	253.2	525	440.3	285.9	585	490.6	318.6
346	290.2	188.4	406	340.5	221.1	466	390.8	253.8	526	441.1	286.5	586	491.5	319.2
347	291.0	189.0	407	341.3	221.6	467	391.7	254.3	527	442.0	287.0	587	492.3	319.7
348	291.9	189.5	408	342.2	222.2	468	392.5	254.9	528	442.8	287.5	588	493.1	320.2
349	292.7	190.0	409	343.0	222.7	469	393.3	255.4	529	443.6	288.1	589	494.0	320.8
350	293.5	190.6	410	343.9	223.3	470	394.2	255.9	530	444.5	288.6	590	494.8	321.3
351	294.4	191.1	411	344.7	223.8	471	395.0	256.5	531	445.3	289.2	591	495.7	321.9
352	295.2	191.7	412	345.5	224.4	472	395.8	257.0	532	446.1	289.7	592	496.5	322.4
353	296.1	192.2	413	346.4	224.9	473	396.7	257.6	533	447.0	290.3	593	497.3	322.9
354	296.9	192.8	414	347.2	225.4	474	397.5	258.1	534	447.8	290.8	594	498.1	323.5
355	297.7	193.3	415	348.1	226.0	475	398.3	258.7	535	448.7	291.4	595	499.0	324.1
356	298.6	193.9	416	348.9	226.5	476	399.2	259.2	536	449.5	291.9	596	499.8	324.6
357	299.4	194.4	417	349.7	227.1	477	400.0	259.8	537	450.3	292.5	597	500.6	325.1
358	300.2	194.9	418	350.6	227.6	478	400.9	260.3	538	451.2	293.0	598	501.5	325.7
359	301.1	195.5	419	351.4	228.2	479	401.7	260.9	539	452.0	293.6	599	502.3	326.2
360	301.9	196.0	420	352.2	228.7	480	402.6	261.4	540	452.9	294.1	600	503.2	326.8

57°

8h 48m

K K

TRAVERSE TABLE TO DEGREES														
34°									2° 16'					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0.8	0.6	61	50.6	34.1	121	100.3	67.7	181	150.1	101.2	241	199.8	134.8
2	1.7	1.1	62	51.4	34.7	122	101.1	68.2	182	150.9	101.8	242	200.6	135.3
3	2.5	1.7	63	52.2	35.2	123	102.0	68.8	183	151.7	102.3	243	201.5	135.9
4	3.3	2.2	64	53.1	35.8	124	102.8	69.3	184	152.5	102.9	244	202.3	136.4
5	4.1	2.8	65	53.9	36.3	125	103.6	69.9	185	153.4	103.5	245	203.1	137.0
6	5.0	3.4	66	54.7	36.9	126	104.5	70.5	186	154.2	104.0	246	203.9	137.6
7	5.8	3.9	67	55.5	37.5	127	105.3	71.0	187	155.0	104.6	247	204.8	138.1
8	6.6	4.5	68	56.4	38.0	128	106.1	71.6	188	155.9	105.1	248	205.6	138.7
9	7.5	5.0	69	57.2	38.6	129	106.9	72.1	189	156.7	105.7	249	206.4	139.2
10	8.3	5.6	70	58.0	39.1	130	107.8	72.7	190	157.5	106.2	250	207.3	139.8
11	9.1	6.2	71	58.9	39.7	131	108.6	73.3	191	158.3	106.8	251	208.1	140.4
12	9.9	6.7	72	59.7	40.3	132	109.4	73.8	192	159.2	107.4	252	208.9	140.9
13	10.8	7.3	73	60.5	40.8	133	110.3	74.4	193	160.0	107.9	253	209.7	141.5
14	11.6	7.8	74	61.3	41.4	134	111.1	74.9	194	160.8	108.5	254	210.6	142.0
15	12.4	8.4	75	62.2	41.9	135	111.9	75.5	195	161.7	109.0	255	211.4	142.6
16	13.3	8.9	76	63.0	42.5	136	112.7	76.1	196	162.5	109.6	256	212.2	143.2
17	14.1	9.5	77	63.8	43.1	137	113.6	76.6	197	163.3	110.2	257	213.1	143.7
18	14.9	10.1	78	64.7	43.6	138	114.4	77.2	198	164.1	110.7	258	213.9	144.3
19	15.8	10.6	79	65.5	44.2	139	115.2	77.7	199	165.0	111.3	259	214.7	144.8
20	16.6	11.2	80	66.3	44.7	140	116.1	78.3	200	165.8	111.8	260	215.5	145.4
21	17.4	11.7	81	67.2	45.3	141	116.9	78.8	201	166.6	112.4	261	216.4	145.9
22	18.2	12.3	82	68.0	45.9	142	117.7	79.4	202	167.5	113.0	262	217.2	146.5
23	19.1	12.9	83	68.8	46.4	143	118.6	80.0	203	168.3	113.5	263	218.0	147.1
24	19.9	13.4	84	69.6	47.0	144	119.4	80.5	204	169.1	114.1	264	218.9	147.6
25	20.7	14.0	85	70.5	47.5	145	120.2	81.1	205	170.0	114.6	265	219.7	148.2
26	21.6	14.5	86	71.3	48.1	146	121.0	81.6	206	170.8	115.2	266	220.5	148.7
27	22.4	15.1	87	72.1	48.6	147	121.9	82.2	207	171.6	115.8	267	221.4	149.3
28	23.2	15.7	88	73.0	49.2	148	122.7	82.8	208	172.4	116.3	268	222.2	149.9
29	24.0	16.2	89	73.8	49.8	149	123.5	83.3	209	173.3	116.9	269	223.0	150.4
30	24.9	16.8	90	74.6	50.3	150	124.4	83.9	210	174.1	117.4	270	223.8	151.0
31	25.7	17.3	91	75.4	50.9	151	125.2	84.4	211	174.9	118.0	271	224.7	151.5
32	26.5	17.9	92	76.3	51.4	152	126.0	85.0	212	175.8	118.5	272	225.5	152.1
33	27.4	18.5	93	77.1	52.0	153	126.8	85.6	213	176.6	119.1	273	226.3	152.7
34	28.2	19.0	94	77.9	52.6	154	127.7	86.1	214	177.4	119.7	274	227.2	153.2
35	29.0	19.6	95	78.8	53.1	155	128.5	86.7	215	178.2	120.2	275	228.0	153.8
36	29.8	20.1	96	79.6	53.7	156	129.3	87.2	216	179.1	120.8	276	228.8	154.3
37	30.7	20.7	97	80.4	54.2	157	130.2	87.8	217	179.9	121.3	277	229.6	154.9
38	31.5	21.2	98	81.2	54.8	158	131.0	88.4	218	180.7	121.9	278	230.5	155.5
39	32.3	21.8	99	82.1	55.4	159	131.8	88.9	219	181.6	122.5	279	231.3	156.0
40	33.2	22.4	100	82.9	55.9	160	132.6	89.5	220	182.4	123.0	280	232.1	156.6
41	34.0	22.9	101	83.7	56.5	161	133.5	90.0	221	183.2	123.6	281	233.0	157.1
42	34.8	23.5	102	84.6	57.0	162	134.3	90.6	222	184.0	124.1	282	233.8	157.7
43	35.6	24.0	103	85.4	57.6	163	135.1	91.1	223	184.9	124.7	283	234.6	158.3
44	36.5	24.6	104	86.2	58.2	164	136.0	91.7	224	185.7	125.3	284	235.4	158.8
45	37.3	25.2	105	87.0	58.7	165	136.8	92.3	225	186.5	125.8	285	236.3	159.4
46	38.1	25.7	106	87.9	59.3	166	137.6	92.8	226	187.4	126.4	286	237.1	159.9
47	39.0	26.3	107	88.7	59.8	167	138.4	93.4	227	188.2	126.9	287	237.9	160.5
48	39.8	26.8	108	89.5	60.4	168	139.3	93.9	228	189.0	127.5	288	238.8	161.0
49	40.6	27.4	109	90.4	61.0	169	140.1	94.5	229	189.8	128.1	289	239.6	161.6
50	41.5	28.0	110	91.2	61.5	170	140.9	95.1	230	190.7	128.6	290	240.4	162.2
51	42.3	28.5	111	92.0	62.1	171	141.8	95.6	231	191.5	129.2	291	241.2	162.7
52	43.1	29.1	112	92.9	62.6	172	142.6	96.2	232	192.3	129.7	292	242.1	163.3
53	43.9	29.6	113	93.7	63.2	173	143.4	96.7	233	193.2	130.3	293	242.9	163.8
54	44.8	30.2	114	94.5	63.7	174	144.3	97.3	234	194.0	130.9	294	243.7	164.4
55	45.6	30.8	115	95.3	64.3	175	145.1	97.9	235	194.8	131.4	295	244.6	165.0
56	46.4	31.3	116	96.2	64.9	176	145.9	98.4	236	195.7	132.0	296	245.4	165.5
57	47.3	31.9	117	97.0	65.4	177	146.7	99.0	237	196.5	132.5	297	246.2	166.1
58	48.1	32.4	118	97.8	66.0	178	147.6	99.5	238	197.3	133.1	298	247.1	166.6
59	48.9	33.0	119	98.7	66.5	179	148.4	100.1	239	198.1	133.6	299	247.9	167.2
60	49.7	33.6	120	99.5	67.1	180	149.2	100.7	240	199.0	134.2	300	248.7	167.8
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
56°									3° 44'					

TABLE 1

499

TRAVERSE TABLE TO DEGREES															
84°												2 ^d 16 ^m			
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	
301	249.5	168.3	361	299.3	201.9	421	349.0	235.4	481	398.8	269.0	541	448.5	302.5	
302	250.4	168.9	362	300.1	202.4	422	349.9	236.0	482	399.6	269.5	542	449.4	303.1	
303	251.2	169.4	363	300.9	203.0	423	350.7	236.5	483	400.4	270.1	543	450.2	303.6	
304	252.0	170.0	364	301.8	203.5	424	351.5	237.1	484	401.3	270.6	544	451.0	304.2	
305	252.9	170.6	365	302.6	204.1	425	352.3	237.7	485	402.1	271.2	545	451.8	304.8	
306	253.7	171.1	366	303.4	204.7	426	353.2	238.2	486	402.9	271.8	546	452.6	305.3	
307	254.5	171.7	367	304.3	205.2	427	354.0	238.8	487	403.8	272.3	547	453.5	305.9	
308	255.3	172.2	368	305.1	205.8	428	354.8	239.3	488	404.6	272.8	548	454.3	306.4	
309	256.2	172.8	369	305.9	206.3	429	355.7	239.9	489	405.4	273.4	549	455.2	307.0	
310	257.0	173.3	370	306.7	206.9	480	356.5	240.4	490	406.2	274.0	550	456.0	307.5	
311	257.8	173.9	371	307.6	207.5	431	357.3	241.0	491	407.1	274.6	551	456.8	308.1	
312	258.7	174.5	372	308.4	208.0	432	358.1	241.6	492	407.9	275.1	552	457.6	308.7	
313	259.5	175.0	373	309.2	208.6	433	359.0	242.1	493	408.7	275.7	553	458.4	309.2	
314	260.3	175.6	374	310.1	209.1	434	359.8	242.7	494	409.5	276.2	554	459.3	309.8	
315	261.2	176.1	375	310.9	209.7	435	360.6	243.2	495	410.4	276.8	555	460.1	310.3	
316	262.0	176.7	376	311.7	210.3	436	361.5	243.8	496	411.2	277.4	556	460.9	310.9	
317	262.8	177.3	377	312.6	210.8	437	362.3	244.4	497	412.0	277.9	557	461.7	311.5	
318	263.7	177.8	378	313.4	211.4	438	363.1	244.9	498	412.8	278.4	558	462.6	312.0	
319	264.5	178.4	379	314.2	211.9	439	364.0	245.5	499	413.7	279.0	559	463.4	312.6	
320	265.3	178.9	380	315.0	212.5	440	364.8	246.0	500	414.5	279.6	560	464.2	313.1	
321	266.1	179.5	381	315.9	213.0	441	365.6	246.6	501	415.3	280.1	561	465.1	313.7	
322	267.0	180.1	382	316.7	213.6	442	366.4	247.2	502	416.2	280.7	562	465.9	314.3	
323	267.8	180.6	383	317.5	214.2	443	367.3	247.7	503	417.0	281.3	563	466.8	314.8	
324	268.6	181.2	384	318.4	214.7	444	368.1	248.3	504	417.8	281.8	564	467.6	315.4	
325	269.5	181.7	385	319.2	215.3	445	368.9	248.8	505	418.6	282.4	565	468.4	315.9	
326	270.3	182.3	386	320.0	215.8	446	369.8	249.4	506	419.4	282.9	566	469.2	316.5	
327	271.1	182.9	387	320.8	216.4	447	370.6	250.0	507	420.3	283.5	567	470.1	317.1	
328	271.9	183.4	388	321.7	217.0	448	371.4	250.5	508	421.1	284.1	568	470.9	317.6	
329	272.8	184.0	389	322.5	217.5	449	372.2	251.1	509	421.9	284.6	569	471.7	318.2	
330	273.6	184.5	390	323.3	218.1	450	373.1	251.6	510	422.8	285.2	570	472.6	318.7	
331	274.4	185.1	391	324.2	218.6	451	373.9	252.2	511	423.6	285.8	571	473.4	319.3	
332	275.2	185.6	392	325.0	219.2	452	374.7	252.8	512	424.4	286.3	572	474.2	319.9	
333	276.1	186.2	393	325.8	219.8	453	375.6	253.3	513	425.3	286.9	573	475.0	320.4	
334	276.9	186.8	394	326.6	220.3	454	376.4	253.9	514	426.1	287.4	574	475.9	321.0	
335	277.7	187.3	395	327.5	220.9	455	377.2	254.4	515	426.9	288.0	575	476.7	321.5	
336	278.6	187.9	396	328.3	221.4	456	378.0	255.0	516	427.8	288.5	576	477.5	322.1	
337	279.4	188.4	397	329.1	222.0	457	378.9	255.5	517	428.6	289.1	577	478.3	322.7	
338	280.2	189.0	398	330.0	222.6	458	379.7	256.1	518	429.4	289.6	578	479.2	323.2	
339	281.0	189.6	399	330.8	223.1	459	380.5	256.7	519	430.3	290.2	579	480.0	323.8	
340	281.9	190.1	400	331.6	223.7	460	381.3	257.2	520	431.1	290.8	580	480.8	324.3	
341	282.7	190.7	401	332.4	224.2	461	382.2	257.8	521	431.9	291.3	581	481.6	324.9	
342	283.5	191.2	402	333.3	224.8	462	383.0	258.3	522	432.8	291.9	582	482.5	325.4	
343	284.4	191.8	403	334.1	225.4	463	383.8	258.9	523	433.6	292.5	583	483.3	326.0	
344	285.2	192.4	404	334.9	225.9	464	384.7	259.5	524	434.4	293.0	584	484.1	326.6	
345	286.0	192.9	405	335.8	226.5	465	385.5	260.0	525	435.3	293.6	585	485.0	327.2	
346	286.9	193.5	406	336.6	227.0	466	386.3	260.6	526	436.1	294.1	586	485.8	327.7	
347	287.7	194.0	407	337.4	227.6	467	387.2	261.1	527	436.9	294.7	587	486.6	328.2	
348	288.5	194.6	408	338.3	228.1	468	388.0	261.7	528	437.8	295.3	588	487.5	328.8	
349	289.3	195.2	409	339.1	228.7	469	388.8	262.3	529	438.6	295.8	589	488.3	329.4	
350	290.2	195.7	410	339.9	229.3	470	389.7	262.8	530	439.4	296.4	590	489.2	329.9	
351	291.0	196.3	411	340.7	229.8	471	390.5	263.4	531	440.3	296.9	591	490.0	330.5	
352	291.8	196.8	412	341.6	230.4	472	391.3	263.9	532	441.1	297.4	592	490.8	331.0	
353	292.7	197.4	413	342.4	230.9	473	392.1	264.5	533	441.9	298.0	593	491.6	331.6	
354	293.5	198.0	414	343.2	231.5	474	393.0	265.0	534	442.7	298.6	594	492.5	332.2	
355	294.3	198.5	415	344.1	232.1	475	393.8	265.6	535	443.6	299.1	595	493.3	332.7	
356	295.1	199.1	416	344.9	232.6	476	394.6	266.2	536	444.4	299.7	596	494.1	333.3	
357	296.0	199.6	417	345.7	233.2	477	395.5	266.7	537	445.3	300.2	597	494.9	333.8	
358	296.8	200.2	418	346.5	233.7	478	396.3	267.3	538	446.1	300.8	598	495.8	334.4	
359	297.6	200.7	419	347.4	234.3	479	397.1	267.9	539	446.9	301.4	599	496.6	334.9	
360	298.5	201.3	420	348.2	234.9	480	397.9	268.4	540	447.7	302.0	600	497.4	335.5	
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	
56°												8 ^h 41 ^m			

TRAVERSE TABLE TO DEGREES

85°														
2h 20m														
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
801	246.6	172.6	361	295.7	207.0	421	344.9	241.5	481	394.0	275.9	541	443.2	310.3
802	247.4	173.2	362	296.5	207.6	422	345.7	242.0	482	394.8	276.4	542	444.0	310.9
803	248.2	173.8	363	297.4	208.2	423	346.5	242.6	483	395.7	277.0	543	444.8	311.4
804	249.0	174.3	364	298.2	208.8	424	347.3	243.2	484	396.5	277.6	544	445.6	312.0
805	249.9	174.9	365	299.0	209.3	425	348.1	243.8	485	397.3	278.2	545	446.4	312.6
806	250.7	175.5	366	299.8	209.9	426	349.0	244.3	486	398.1	278.7	546	447.3	313.2
807	251.5	176.1	367	300.6	210.5	427	349.8	244.9	487	398.9	279.3	547	448.1	313.7
808	252.3	176.6	368	301.5	211.1	428	350.6	245.5	488	399.8	279.9	548	448.9	314.3
809	253.1	177.2	369	302.3	211.6	429	351.4	246.0	489	400.6	280.5	549	449.7	314.9
810	253.9	177.8	370	303.1	212.2	430	352.2	246.6	490	401.4	281.0	550	450.5	315.4
811	254.8	178.4	371	303.9	212.8	431	353.1	247.2	491	402.2	281.6	551	451.4	316.0
812	255.6	178.9	372	304.7	213.4	432	353.9	247.8	492	403.0	282.2	552	452.2	316.6
813	256.4	179.5	373	305.6	213.9	433	354.7	248.3	493	403.9	282.8	553	453.0	317.2
814	257.2	180.1	374	306.4	214.5	434	355.5	248.9	494	404.7	283.3	554	453.8	317.7
815	258.0	180.7	375	307.2	215.1	435	356.3	249.5	495	405.5	283.9	555	454.6	318.3
816	258.9	181.2	376	308.0	215.6	436	357.2	250.1	496	406.3	284.5	556	455.5	318.9
817	259.7	181.8	377	308.8	216.2	437	358.0	250.6	497	407.1	285.1	557	456.3	319.5
818	260.5	182.4	378	309.6	216.8	438	358.8	251.2	498	408.0	285.6	558	457.1	320.0
819	261.3	183.0	379	310.5	217.4	439	359.6	251.8	499	408.8	286.2	559	457.9	320.6
820	262.1	183.5	380	311.3	217.9	440	360.4	252.4	500	409.6	286.8	560	458.7	321.2
821	263.0	184.1	381	312.1	218.5	441	361.3	252.9	501	410.4	287.4	561	459.6	321.8
822	263.8	184.7	382	312.9	219.1	442	362.1	253.5	502	411.2	287.9	562	460.4	322.3
823	264.6	185.2	383	313.7	219.7	443	362.9	254.1	503	412.1	288.5	563	461.2	322.9
824	265.4	185.8	384	314.6	220.2	444	363.7	254.7	504	412.9	289.1	564	462.0	323.5
825	266.2	186.4	385	315.4	220.8	445	364.5	255.2	505	413.7	289.7	565	462.8	324.1
826	267.1	187.0	386	316.2	221.4	446	365.4	255.8	506	414.5	290.2	566	463.7	324.6
827	267.9	187.5	387	317.0	222.0	447	366.2	256.4	507	415.3	290.8	567	464.5	325.2
828	268.7	188.1	388	317.8	222.5	448	367.0	256.9	508	416.1	291.4	568	465.3	325.8
829	269.5	188.7	389	318.7	223.1	449	367.8	257.5	509	417.0	291.9	569	466.1	326.4
830	270.3	189.3	390	319.5	223.7	450	368.6	258.1	510	417.8	292.5	570	466.9	326.9
831	271.1	189.8	391	320.3	224.3	451	369.4	258.7	511	418.6	293.1	571	467.8	327.5
832	272.0	190.4	392	321.1	224.8	452	370.3	259.2	512	419.4	293.7	572	468.6	328.1
833	272.8	191.0	393	321.9	225.4	453	371.1	259.8	513	420.2	294.2	573	469.4	328.7
834	273.6	191.6	394	322.8	226.0	454	371.9	260.4	514	421.1	294.8	574	470.2	329.2
835	274.4	192.1	395	323.6	226.5	455	372.7	261.0	515	421.9	295.4	575	471.0	329.8
836	275.2	192.7	396	324.4	227.1	456	373.5	261.5	516	422.7	296.0	576	471.9	330.4
837	276.1	193.3	397	325.2	227.7	457	374.4	262.1	517	423.5	296.5	577	472.7	331.0
838	276.9	193.9	398	326.0	228.3	458	375.2	262.7	518	424.3	297.1	578	473.5	331.5
839	277.7	194.4	399	326.9	228.8	459	376.0	263.3	519	425.2	297.7	579	474.3	332.1
840	278.5	195.0	400	327.7	229.4	460	376.8	263.8	520	426.0	298.3	580	475.1	332.7
841	279.3	195.6	401	328.5	230.0	461	377.6	264.4	521	426.8	298.8	581	476.0	333.3
842	280.2	196.1	402	329.3	230.6	462	378.5	265.0	522	427.6	299.4	582	476.8	333.8
843	281.0	196.7	403	330.1	231.1	463	379.3	265.5	523	428.4	300.0	583	477.6	334.4
844	281.8	197.3	404	330.9	231.7	464	380.1	266.1	524	429.3	300.5	584	478.4	335.0
845	282.6	197.9	405	331.8	232.3	465	380.9	266.7	525	430.1	301.1	585	479.2	335.6
846	283.4	198.4	406	332.6	232.9	466	381.7	267.3	526	430.9	301.7	586	480.1	336.1
847	284.3	199.0	407	333.4	233.4	467	382.6	267.8	527	431.7	302.3	587	480.9	336.7
848	285.1	199.6	408	334.2	234.0	468	383.4	268.4	528	432.5	302.8	588	481.7	337.3
849	285.9	200.2	409	335.0	234.6	469	384.2	269.0	529	433.4	303.4	589	482.5	337.9
850	286.7	200.7	410	335.9	235.1	470	385.0	269.6	530	434.2	304.0	590	483.3	338.4
851	287.5	201.3	411	336.7	235.7	471	385.8	270.1	531	435.0	304.5	591	484.2	339.0
852	288.3	201.9	412	337.5	236.3	472	386.6	270.7	532	435.8	305.1	592	485.0	339.6
853	289.2	202.5	413	338.3	236.9	473	387.5	271.3	533	436.6	305.7	593	485.8	340.2
854	290.0	203.0	414	339.1	237.4	474	388.3	271.9	534	437.5	306.3	594	486.6	340.7
855	290.8	203.6	415	340.0	238.0	475	389.1	272.4	535	438.3	306.8	595	487.4	341.3
856	291.6	204.2	416	340.8	238.6	476	389.9	273.0	536	439.1	307.4	596	488.3	341.9
857	292.4	204.7	417	341.6	239.2	477	390.7	273.6	537	439.9	308.0	597	489.1	342.5
858	293.3	205.3	418	342.4	239.7	478	391.6	274.2	538	440.7	308.6	598	489.9	343.0
859	294.1	205.9	419	343.2	240.3	479	392.4	274.7	539	441.5	309.1	599	490.7	343.6
860	294.9	206.5	420	344.1	240.9	480	393.2	275.3	540	442.3	309.7	600	491.5	344.1
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

TRAVERSE TABLE TO DEGREES																	
86°																	
2h 24m																	
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	243.5	176.9	361	292.1	212.2	421	340.6	247.5	481	389.1	282.7	541	437.7	318.0			
302	244.3	177.5	362	292.9	212.8	422	341.4	248.1	482	390.0	283.3	542	438.5	318.6			
303	245.1	178.1	363	293.7	213.4	423	342.2	248.6	483	390.8	283.9	543	439.3	319.1			
304	246.0	178.7	364	294.5	214.0	424	343.0	249.2	484	391.6	284.5	544	440.2	319.7			
305	246.8	179.3	365	295.3	214.6	425	343.8	249.8	485	392.4	285.1	545	441.0	320.3			
306	247.6	179.9	366	296.1	215.1	426	344.7	250.4	486	393.2	285.6	546	441.8	320.9			
307	248.4	180.5	367	296.9	215.7	427	345.5	251.0	487	394.0	286.2	547	442.6	321.5			
308	249.2	181.1	368	297.7	216.3	428	346.3	251.6	488	394.8	286.8	548	443.4	322.1			
309	250.0	181.6	369	298.5	216.9	429	347.1	252.2	489	395.6	287.4	549	444.2	322.7			
310	250.8	182.2	370	299.3	217.5	430	347.9	252.8	490	396.4	288.0	550	445.0	323.3			
311	251.6	182.8	371	300.2	218.1	431	348.7	253.3	491	397.3	288.6	551	445.8	323.8			
312	252.4	183.4	372	301.0	218.7	432	349.5	253.9	492	398.1	289.2	552	446.6	324.4			
313	253.2	184.0	373	301.8	219.3	433	350.3	254.5	493	398.9	289.8	553	447.4	325.0			
314	254.0	184.6	374	302.6	219.8	434	351.1	255.1	494	399.7	290.3	554	448.2	325.6			
315	254.9	185.2	375	303.4	220.4	435	351.9	255.7	495	400.5	290.9	555	449.0	326.2			
316	255.7	185.8	376	304.2	221.0	436	352.7	256.3	496	401.3	291.5	556	449.8	326.8			
317	256.5	186.4	377	305.0	221.6	437	353.6	256.9	497	402.1	292.1	557	450.7	327.4			
318	257.3	186.9	378	305.8	222.2	438	354.4	257.5	498	402.9	292.7	558	451.5	328.0			
319	258.1	187.5	379	306.6	222.8	439	355.2	258.0	499	403.7	293.3	559	452.3	328.5			
320	258.9	188.1	380	307.4	223.4	440	356.0	258.6	500	404.5	293.9	560	453.1	329.1			
321	259.7	188.7	381	308.2	224.0	441	356.8	259.2	501	405.3	294.5	561	453.9	329.7			
322	260.5	189.3	382	309.1	224.5	442	357.6	259.8	502	406.1	295.0	562	454.7	330.3			
323	261.3	189.9	383	309.9	225.1	443	358.4	260.4	503	407.0	295.6	563	455.5	330.9			
324	262.1	190.5	384	310.7	225.7	444	359.2	261.0	504	407.8	296.2	564	456.3	331.5			
325	262.9	191.0	385	311.5	226.3	445	360.0	261.6	505	408.6	296.8	565					

TRAVERSE TABLE TO DEGREES														
37°									2 ^h 28 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0°8	0°6	61	48°7	36°7	121	96°6	72°8	181	144°6	108°9	241	192°5	145°0
2	1°6	1°2	62	49°5	37°3	122	97°4	73°4	182	145°4	109°5	242	193°3	145°6
3	2°4	1°8	63	50°3	37°9	123	98°2	74°0	183	146°2	110°1	243	194°1	146°2
4	3°2	2°4	64	51°1	38°5	124	99°0	74°6	184	146°9	110°7	244	194°9	146°8
5	4°0	3°0	65	51°9	39°1	125	99°8	75°2	185	147°7	111°3	245	195°7	147°4
6	4°8	3°6	66	52°7	39°7	126	100°6	75°8	186	148°5	111°9	246	196°5	148°0
7	5°6	4°2	67	53°5	40°3	127	101°4	76°4	187	149°3	112°5	247	197°3	148°6
8	6°4	4°8	68	54°3	40°9	128	102°2	77°0	188	150°1	113°1	248	198°1	149°3
9	7°2	5°4	69	55°1	41°5	129	103°0	77°6	189	150°9	113°7	249	198°9	149°9
10	8°0	6°0	70	55°9	42°1	130	103°8	78°2	190	151°7	114°3	250	199°7	150°5
11	8°8	6°6	71	56°7	42°7	131	104°6	78°8	191	152°5	114°9	251	200°5	151°1
12	9°6	7°2	72	57°5	43°3	132	105°4	79°4	192	153°3	115°5	252	201°3	151°7
13	10°4	7°8	73	58°3	43°9	133	106°2	80°0	193	154°1	116°2	253	202°1	152°3
14	11°2	8°4	74	59°1	44°5	134	107°0	80°6	194	154°9	116°8	254	202°9	152°9
15	12°0	9°0	75	59°9	45°1	135	107°8	81°2	195	155°7	117°4	255	203°7	153°5
16	12°8	9°6	76	60°7	45°7	136	108°6	81°8	196	156°5	118°0	256	204°5	154°1
17	13°6	10°2	77	61°5	46°3	137	109°4	82°4	197	157°3	118°6	257	205°3	154°7
18	14°4	10°8	78	62°3	46°9	138	110°2	83°1	198	158°1	119°2	258	206°0	155°3
19	15°2	11°4	79	63°1	47°5	139	111°0	83°7	199	158°9	119°8	259	206°8	155°9
20	16°0	12°0	80	63°9	48°1	140	111°8	84°3	200	159°7	120°4	260	207°6	156°5
21	16°8	12°6	81	64°7	48°7	141	112°6	84°9	201	160°5	121°0	261	208°4	157°1
22	17°6	13°2	82	65°5	49°3	142	113°4	85°5	202	161°3	121°6	262	209°2	157°7
23	18°4	13°8	83	66°3	50°0	143	114°2	86°1	203	162°1	122°2	263	210°0	158°3
24	19°2	14°4	84	67°1	50°6	144	115°0	86°7	204	162°9	122°8	264	210°8	158°9
25	20°0	15°0	85	67°9	51°2	145	115°8	87°3	205	163°7	123°4	265	211°6	159°5
26	20°8	15°6	86	68°7	51°8	146	116°6	87°9	206	164°5	124°0	266	212°4	160°1
27	21°6	16°2	87	69°5	52°4	147	117°4	88°5	207	165°3	124°6	267	213°2	160°7
28	22°4	16°9	88	70°3	53°0	148	118°2	89°1	208	166°1	125°2	268	214°0	161°3
29	23°2	17°5	89	71°1	53°6	149	119°0	89°7	209	166°9	125°8	269	214°8	161°9
30	24°0	18°1	90	71°9	54°2	150	119°8	90°3	210	167°7	126°4	270	215°6	162°5
31	24°8	18°7	91	72°7	54°8	151	120°6	90°9	211	168°5	127°0	271	216°4	163°1
32	25°6	19°3	92	73°5	55°4	152	121°4	91°5	212	169°3	127°6	272	217°2	163°7
33	26°4	19°9	93	74°3	56°0	153	122°2	92°1	213	170°1	128°2	273	218°0	164°3
34	27°2	20°5	94	75°1	56°6	154	123°0	92°7	214	170°9	128°8	274	218°8	164°9
35	28°0	21°1	95	75°9	57°2	155	123°8	93°3	215	171°7	129°4	275	219°6	165°5
36	28°8	21°7	96	76°7	57°8	156	124°6	93°9	216	172°5	130°0	276	220°4	166°1
37	29°5	22°3	97	77°5	58°4	157	125°4	94°5	217	173°3	130°6	277	221°2	166°7
38	30°3	22°9	98	78°3	59°0	158	126°2	95°1	218	174°1	131°2	278	222°0	167°3
39	31°1	23°5	99	79°1	59°6	159	127°0	95°7	219	174°9	131°8	279	222°8	167°9
40	31°9	24°1	100	79°9	60°2	160	127°8	96°3	220	175°7	132°4	280	223°6	168°5
41	32°7	24°7	101	80°7	60°8	161	128°6	96°9	221	176°5	133°0	281	224°4	169°1
42	33°5	25°3	102	81°5	61°4	162	129°4	97°5	222	177°3	133°6	282	225°2	169°7
43	34°3	25°9	103	82°3	62°0	163	130°2	98°1	223	178°1	134°2	283	226°0	170°3
44	35°1	26°5	104	83°1	62°6	164	131°0	98°7	224	178°9	134°8	284	226°8	170°9
45	35°9	27°1	105	83°9	63°2	165	131°8	99°3	225	179°7	135°4	285	227°6	171°5
46	36°7	27°7	106	84°7	63°8	166	132°6	99°9	226	180°5	136°0	286	228°4	172°1
47	37°5	28°3	107	85°5	64°4	167	133°4	100°5	227	181°3	136°6	287	229°2	172°7
48	38°3	28°9	108	86°3	65°0	168	134°2	101°1	228	182°1	137°2	288	230°0	173°3
49	39°1	29°5	109	87°1	65°6	169	135°0	101°7	229	182°9	137°8	289	230°8	173°9
50	39°9	30°1	110	87°8	66°2	170	135°8	102°3	230	183°7	138°4	290	231°6	174°5
51	40°7	30°7	111	88°6	66°8	171	136°6	102°9	231	184°5	139°0	291	232°4	175°1
52	41°5	31°3	112	89°4	67°4	172	137°4	103°5	232	185°3	139°6	292	233°2	175°7
53	42°3	31°9	113	90°2	68°0	173	138°2	104°1	233	186°1	140°2	293	234°0	176°3
54	43°1	32°5	114	91°0	68°6	174	139°0	104°7	234	186°9	140°8	294	234°8	176°9
55	43°9	33°1	115	91°8	69°2	175	139°8	105°3	235	187°7	141°4	295	235°6	177°5
56	44°7	33°7	116	92°6	69°8	176	140°6	105°9	236	188°5	142°0	296	236°4	178°1
57	45°5	34°3	117	93°4	70°4	177	141°4	106°5	237	189°3	142°6	297	237°2	178°7
58	46°3	34°9	118	94°2	71°0	178	142°2	107°1	238	190°1	143°2	298	238°0	179°3
59	47°1	35°5	119	95°0	71°6	179	143°0	107°7	239	190°9	143°8	299	238°8	179°9
60	47°9	36°1	120	95°8	72°2	180	143°8	108°3	240	191°7	144°4	300	239°6	180°5
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TRAVERSE TABLE TO DEGREES														
38°									2° 32'					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0.8	0.6	61	48.1	37.6	121	95.3	74.5	181	142.6	111.4	241	189.9	148.4
2	1.6	1.2	62	48.9	38.2	122	96.1	75.1	182	143.4	112.1	242	190.7	149.0
3	2.4	1.8	63	49.6	38.8	123	96.9	75.7	183	144.2	112.7	243	191.5	149.6
4	3.2	2.5	64	50.4	39.4	124	97.7	76.3	184	145.0	113.3	244	192.3	150.2
5	3.9	3.1	65	51.2	40.0	125	98.5	77.0	185	145.8	113.9	245	193.1	150.8
6	4.7	3.7	66	52.0	40.6	126	99.3	77.6	186	146.6	114.5	246	193.9	151.5
7	5.5	4.3	67	52.8	41.2	127	100.1	78.2	187	147.4	115.1	247	194.6	152.1
8	6.3	4.9	68	53.6	41.9	128	100.9	78.8	188	148.1	115.7	248	195.4	152.7
9	7.1	5.5	69	54.4	42.5	129	101.7	79.4	189	148.9	116.4	249	196.2	153.3
10	7.9	6.2	70	55.2	43.1	130	102.4	80.0	190	149.7	117.0	250	197.0	153.9
11	8.7	6.8	71	55.9	43.7	131	103.2	80.7	191	150.5	117.6	251	197.8	154.5
12	9.5	7.4	72	56.7	44.3	132	104.0	81.3	192	151.3	118.2	252	198.6	155.1
13	10.2	8.0	73	57.5	44.9	133	104.8	81.9	193	152.1	118.8	253	199.4	155.8
14	11.0	8.6	74	58.3	45.6	134	105.6	82.5	194	152.9	119.4	254	200.2	156.4
15	11.8	9.2	75	59.1	46.2	135	106.4	83.1	195	153.7	120.1	255	200.9	157.0
16	12.6	9.9	76	59.9	46.8	136	107.2	83.7	196	154.5	120.7	256	201.7	157.6
17	13.4	10.5	77	60.7	47.4	137	108.0	84.3	197	155.2	121.3	257	202.5	158.2
18	14.2	11.1	78	61.5	48.0	138	108.7	85.0	198	156.0	121.9	258	203.3	158.8
19	15.0	11.7	79	62.3	48.6	139	109.5	85.6	199	156.8	122.5	259	204.1	159.5
20	15.8	12.3	80	63.0	49.3	140	110.3	86.2	200	157.6	123.1	260	204.9	160.1
21	16.5	12.9	81	63.8	49.9	141	111.1	86.8	201	158.4	123.7	261	205.7	160.7
22	17.3	13.5	82	64.6	50.5	142	111.9	87.4	202	159.2	124.4	262	206.5	161.3
23	18.1	14.2	83	65.4	51.1	143	112.7	88.0	203	160.0	125.0	263	207.3	161.9
24	18.9	14.8	84	66.2	51.7	144	113.5	88.7	204	160.8	125.6	264	208.0	162.5
25	19.7	15.4	85	67.0	52.3	145	114.3	89.3	205	161.5	126.2	265	208.8	163.2
26	20.5	16.0	86	67.8	52.9	146	115.0	89.9	206	162.3	126.8	266	209.6	163.8
27	21.3	16.6	87	68.6	53.6	147	115.8	90.5	207	163.1	127.4	267	210.4	164.4
28	22.1	17.2	88	69.3	54.2	148	116.6	91.1	208	163.9	128.1	268	211.2	165.0
29	22.9	17.9	89	70.1	54.8	149	117.4	91.7	209	164.7	128.7	269	212.0	165.6
30	23.6	18.5	90	70.9	55.4	150	118.2	92.3	210	165.5	129.3	270	212.8	166.2
31	24.4	19.1	91	71.7	56.0	151	119.0	93.0	211	166.3	129.9	271	213.6	166.8
32	25.2	19.7	92	72.5	56.6	152	119.8	93.6	212	167.1	130.5	272	214.3	167.5
33	26.0	20.3	93	73.3	57.3	153	120.6	94.2	213	167.8	131.1	273	215.1	168.1
34	26.8	20.9	94	74.1	57.9	154	121.4	94.8	214	168.6	131.8	274	215.9	168.7
35	27.6	21.5	95	74.9	58.5	155	122.1	95.4	215	169.4	132.4	275	216.7	169.3
36	28.4	22.2	96	75.6	59.1	156	122.9	96.0	216	170.2	133.0	276	217.5	169.9
37	29.2	22.8	97	76.4	59.7	157	123.7	96.7	217	171.0	133.6	277	218.3	170.5
38	29.9	23.4	98	77.2	60.3	158	124.5	97.3	218	171.8	134.2	278	219.1	171.2
39	30.7	24.0	99	78.0	61.0	159	125.3	97.9	219	172.6	134.8	279	219.9	171.8
40	31.5	24.6	100	78.8	61.6	160	126.1	98.5	220	173.4	135.4	280	220.6	172.4
41	32.3	25.2	101	79.6	62.2	161	126.9	99.1	221	174.2	136.1	281	221.4	173.0
42	33.1	25.9	102	80.4	62.8	162	127.7	99.7	222	174.9	136.7	282	222.2	173.6
43	33.9	26.5	103	81.2	63.4	163	128.4	100.4	223	175.7	137.3	283	223.0	174.2
44	34.7	27.1	104	82.0	64.0	164	129.2	101.0	224	176.5	137.9	284	223.8	174.8
45	35.5	27.7	105	82.7	64.6	165	130.0	101.6	225	177.3	138.5	285	224.6	175.5
46	36.2	28.3	106	83.5	65.3	166	130.8	102.2	226	178.1	139.1	286	225.4	176.1
47	37.0	28.9	107	84.3	65.9	167	131.6	102.8	227	178.9	139.8	287	226.2	176.7
48	37.8	29.6	108	85.1	66.5	168	132.4	103.4	228	179.7	140.4	288	226.9	177.3
49	38.6	30.2	109	85.9	67.1	169	133.2	104.0	229	180.5	141.0	289	227.7	177.9
50	39.4	30.8	110	86.7	67.7	170	134.0	104.7	230	181.2	141.6	290	228.5	178.5
51	40.2	31.4	111	87.5	68.3	171	134.7	105.3	231	182.0	142.2	291	229.3	179.2
52	41.0	32.0	112	88.3	69.0	172	135.5	105.9	232	182.8	142.8	292	230.1	179.8
53	41.8	32.6	113	89.0	69.6	173	136.3	106.5	233	183.6	143.4	293	230.9	180.4
54	42.6	33.2	114	89.8	70.2	174	137.1	107.1	234	184.4	144.1	294	231.7	181.0
55	43.3	33.9	115	90.6	70.8	175	137.9	107.7	235	185.2	144.7	295	232.5	181.6
56	44.1	34.5	116	91.4	71.4	176	138.7	108.4	236	186.0	145.3	296	233.3	182.2
57	44.9	35.1	117	92.2	72.0	177	139.5	109.0	237	186.8	145.9	297	234.0	182.9
58	45.7	35.7	118	93.0	72.6	178	140.3	109.6	238	187.5	146.5	298	234.8	183.5
59	46.5	36.3	119	93.8	73.3	179	141.1	110.2	239	188.3	147.1	299	235.6	184.1
60	47.3	36.9	120	94.6	73.9	180	141.8	110.8	240	189.1	147.8	300	236.4	184.7
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
52°									3° 28'					

507

TRAVERSE TABLE TO DEGREES														
38°												2h 32m		
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	D. p.	Dist.	D. Lat.	Dep.
301	237.2	185.3	361	284.5	222.3	421	331.8	259.2	481	379.0	296.2	541	426.3	333.1
302	238.0	185.9	362	285.3	222.9	422	332.5	259.8	482	379.8	296.8	542	427.1	333.7
303	238.8	186.6	363	286.0	223.5	423	333.3	260.4	483	380.6	297.4	543	427.9	334.3
304	239.6	187.2	364	286.8	224.1	424	334.1	261.0	484	381.4	298.0	544	428.7	335.0
305	240.3	187.8	365	287.6	224.7	425	334.9	261.7	485	382.2	298.6	545	429.5	335.6
306	241.1	188.4	366	288.4	225.3	426	335.7	262.3	486	383.0	299.2	546	430.3	336.3
307	241.9	189.0	367	289.2	226.0	427	336.5	262.9	487	383.8	299.8	547	431.0	336.8
308	242.7	189.6	368	290.0	226.6	428	337.3	263.5	488	384.5	300.4	548	431.8	337.4
309	243.5	190.2	369	290.8	227.2	429	338.1	264.1	489	385.3	301.1	549	432.6	338.0
310	244.3	190.9	370	291.6	227.8	430	338.8	264.7	490	386.1	301.7	550	433.4	338.6
311	245.1	191.5	371	292.4	228.4	431	339.6	265.4	491	386.9	302.3	551	434.2	339.3
312	245.9	192.1	372	293.1	229.0	432	340.4	266.0	492	387.7	302.9	552	435.0	339.9
313	246.6	192.7	373	293.9	229.6	433	341.2	266.6	493	388.5	303.5	553	435.8	340.5
314	247.4	193.3	374	294.7	230.3	434	342.0	267.2	494	389.3	304.2	554	436.6	341.1
315	248.2	193.9	375	295.5	230.9	435	342.8	267.8	495	390.1	304.8	555	437.4	341.7
316	249.0	194.6	376	296.3	231.5	436	343.6	268.4	496	390.9	305.4	556	438.1	342.3
317	249.8	195.2	377	297.1	232.1	437	344.4	269.1	497	391.6	306.0	557	438.9	343.0
318	250.6	195.8	378	297.9	232.7	438	345.2	269.7	498	392.4	306.6	558	439.7	343.6
319	251.4	196.4	379	298.7	233.3	439	345.9	270.3	499	393.2	307.2	559	440.5	344.2
320	252.2	197.0	380	299.4	234.0	440	346.7	270.9	500	394.0	307.8	560	441.3	344.8
321	253.0	197.6	381	300.2	234.6	441	347.5	271.5	501	394.8	308.4	561	442.1	345.4
322	253.7	198.2	382	301.0	235.2	442	348.3	272.1	502	395.6	309.1	562	442.9	346.0
323	254.5	198.9	383	301.8	235.8	443	349.1	272.7	503	396.4	309.7	563	443.7	346.6
324	255.3	199.5	384	302.6	236.4	444	349.9	273.4	504	397.2	310.3	564	444.4	347.2
325	256.1	200.1	385	303.4	237.0	445	350.7	274.0	505	397.9	310.9	565	445.2	347.8
326	256.9	200.7	386	304.2	237.7	446	351.5	274.6	506	398.7	311.6	566	446.0	348.5
327	257.7	201.3	387	305.0	238.3	447	352.2	275.2	507	399.5	312.2	567	446.8	349.1

TRAVERSE TABLE TO DEGREES														
39°							2° 36'							
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0.8	0.6	61	47.4	38.4	121	94.0	76.1	181	140.7	113.9	241	187.3	151.7
2	1.6	1.3	62	48.2	39.0	122	94.8	76.8	182	141.4	114.5	242	188.1	152.3
3	2.3	1.9	63	49.0	39.6	123	95.6	77.4	183	142.2	115.2	243	188.8	152.9
4	3.1	2.5	64	49.7	40.3	124	96.4	78.0	184	143.0	115.8	244	189.6	153.6
5	3.9	3.1	65	50.5	40.9	125	97.1	78.7	185	143.8	116.4	245	190.4	154.2
6	4.7	3.8	66	51.3	41.5	126	97.9	79.3	186	144.5	117.1	246	191.2	154.8
7	5.4	4.4	67	52.1	42.2	127	98.7	79.9	187	145.3	117.7	247	192.0	155.4
8	6.2	5.0	68	52.8	42.8	128	99.5	80.6	188	146.1	118.3	248	192.7	156.1
9	7.0	5.7	69	53.6	43.4	129	100.3	81.2	189	146.9	118.9	249	193.5	156.7
10	7.8	6.3	70	54.4	44.1	130	101.0	81.8	190	147.7	119.6	250	194.3	157.3
11	8.5	6.9	71	55.2	44.7	131	101.8	82.4	191	148.4	120.2	251	195.1	158.0
12	9.3	7.6	72	56.0	45.3	132	102.6	83.1	192	149.2	120.8	252	195.8	158.6
13	10.1	8.2	73	56.7	45.9	133	103.4	83.7	193	150.0	121.5	253	196.6	159.2
14	10.9	8.8	74	57.5	46.6	134	104.1	84.3	194	150.8	122.1	254	197.4	159.8
15	11.7	9.4	75	58.3	47.2	135	104.9	85.0	195	151.5	122.7	255	198.2	160.5
16	12.4	10.1	76	59.1	47.8	136	105.7	85.6	196	152.3	123.3	256	198.9	161.1
17	13.2	10.7	77	59.8	48.5	137	106.5	86.2	197	153.1	124.0	257	199.7	161.7
18	14.0	11.3	78	60.6	49.1	138	107.2	86.8	198	153.9	124.6	258	200.5	162.4
19	14.8	12.0	79	61.4	49.7	139	108.0	87.5	199	154.7	125.2	259	201.3	163.0
20	15.5	12.6	80	62.2	50.3	140	108.8	88.1	200	155.4	125.9	260	202.1	163.6
21	16.3	13.2	81	62.9	51.0	141	109.6	88.7	201	156.2	126.5	261	202.8	164.3
22	17.1	13.8	82	63.7	51.6	142	110.4	89.4	202	157.0	127.1	262	203.6	164.9
23	17.9	14.5	83	64.5	52.2	143	111.1	90.0	203	157.8	127.8	263	204.4	165.5
24	18.7	15.1	84	65.3	52.9	144	111.9	90.6	204	158.5	128.4	264	205.2	166.1
25	19.4	15.7	85	66.1	53.5	145	112.7	91.3	205	159.3	129.0	265	205.9	166.8
26	20.2	16.4	86	66.8	54.1	146	113.5	91.9	206	160.1	129.6	266	206.7	167.4
27	21.0	17.0	87	67.6	54.8	147	114.2	92.5	207	160.9	130.3	267	207.5	168.0
28	21.8	17.6	88	68.4	55.4	148	115.0	93.1	208	161.6	130.9	268	208.3	168.7
29	22.5	18.3	89	69.2	56.0	149	115.8	93.8	209	162.4	131.5	269	209.1	169.3
30	23.3	18.9	90	69.9	56.6	150	116.6	94.4	210	163.2	132.2	270	209.8	169.9
31	24.1	19.5	91	70.7	57.3	151	117.3	95.0	211	164.0	132.8	271	210.6	170.5
32	24.9	20.1	92	71.5	57.9	152	118.1	95.7	212	164.8	133.4	272	211.4	171.2
33	25.6	20.8	93	72.3	58.5	153	118.9	96.3	213	165.5	134.0	273	212.2	171.8
34	26.4	21.4	94	73.1	59.2	154	119.7	96.9	214	166.3	134.7	274	212.9	172.4
35	27.2	22.0	95	73.8	59.8	155	120.5	97.5	215	167.1	135.3	275	213.7	173.1
36	28.0	22.7	96	74.6	60.4	156	121.2	98.2	216	167.9	135.9	276	214.5	173.7
37	28.8	23.3	97	75.4	61.0	157	122.0	98.8	217	168.6	136.6	277	215.3	174.3
38	29.5	23.9	98	76.2	61.7	158	122.8	99.4	218	169.4	137.2	278	216.0	175.0
39	30.3	24.5	99	76.9	62.3	159	123.6	100.1	219	170.2	137.8	279	216.8	175.6
40	31.1	25.2	100	77.7	62.9	160	124.3	100.7	220	171.0	138.5	280	217.6	176.2
41	31.9	25.8	101	78.5	63.6	161	125.1	101.3	221	171.7	139.1	281	218.4	176.8
42	32.6	26.4	102	79.3	64.2	162	125.9	101.9	222	172.5	139.7	282	219.2	177.5
43	33.4	27.1	103	80.0	64.8	163	126.7	102.6	223	173.3	140.3	283	219.9	178.1
44	34.2	27.7	104	80.8	65.4	164	127.5	103.2	224	174.1	141.0	284	220.7	178.7
45	35.0	28.3	105	81.6	66.1	165	128.2	103.8	225	174.9	141.6	285	221.5	179.4
46	35.7	28.9	106	82.4	66.7	166	129.0	104.5	226	175.6	142.2	286	222.3	180.0
47	36.5	29.6	107	83.2	67.3	167	129.8	105.1	227	176.4	142.9	287	223.0	180.6
48	37.3	30.2	108	83.9	68.0	168	130.6	105.7	228	177.2	143.5	288	223.8	181.2
49	38.1	30.8	109	84.7	68.6	169	131.3	106.4	229	178.0	144.1	289	224.6	181.9
50	38.9	31.5	110	85.5	69.2	170	132.1	107.0	230	178.7	144.7	290	225.4	182.5
51	39.6	32.1	111	86.3	69.9	171	132.9	107.6	231	179.5	145.4	291	226.1	183.1
52	40.4	32.7	112	87.0	70.5	172	133.7	108.2	232	180.3	146.0	292	226.9	183.8
53	41.2	33.4	113	87.8	71.1	173	134.4	108.9	233	181.1	146.6	293	227.7	184.4
54	42.0	34.0	114	88.6	71.7	174	135.2	109.5	234	181.9	147.3	294	228.5	185.0
55	42.7	34.6	115	89.4	72.4	175	136.0	110.1	235	182.6	147.9	295	229.3	185.6
56	43.5	35.2	116	90.1	73.0	176	136.8	110.8	236	183.4	148.5	296	230.0	186.3
57	44.3	35.9	117	90.9	73.6	177	137.6	111.4	237	184.2	149.1	297	230.8	186.9
58	45.1	36.5	118	91.7	74.3	178	138.3	112.0	238	185.0	149.8	298	231.6	187.5
59	45.9	37.1	119	92.5	74.9	179	139.1	112.6	239	185.7	150.4	299	232.4	188.2
60	46.6	37.8	120	93.3	75.5	180	139.9	113.3	240	186.5	151.0	300	233.1	188.8
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

509

TRAVERSE TABLE TO DEGREES															
89°												2h 36m			
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	
301	233.9	189.4	361	280.6	227.1	421	327.2	264.9	481	373.8	302.6	541	420.4	340.4	
302	234.7	190.0	362	281.3	227.8	422	328.0	265.5	482	374.6	303.3	542	421.2	341.0	
303	235.5	190.6	363	282.1	228.4	423	328.7	266.2	483	375.4	303.9	543	422.0	341.7	
304	236.3	191.3	364	282.9	229.0	424	329.5	266.8	484	376.1	304.5	544	422.7	342.3	
305	237.0	191.9	365	283.7	229.7	425	330.3	267.4	485	376.9	305.2	545	423.5	342.9	
306	237.8	192.5	366	284.4	230.3	426	331.1	268.0	486	377.7	305.8	546	424.3	343.6	
307	238.6	193.2	367	285.2	230.9	427	331.9	268.7	487	378.5	306.4	547	425.1	344.2	
308	239.4	193.8	368	286.0	231.5	428	332.6	269.3	488	379.3	307.1	548	425.9	344.8	
309	240.1	194.4	369	286.8	232.2	429	333.4	269.9	489	380.0	307.7	549	426.6	345.5	
310	240.9	195.0	370	287.6	232.8	430	334.2	270.6	490	380.8	308.3	550	427.4	346.1	
311	241.7	195.7	371	288.3	233.4	431	335.0	271.2	491	381.6	308.9	551	428.2	346.7	
312	242.5	196.3	372	289.1	234.1	432	335.7	271.8	492	382.4	309.6	552	429.0	347.4	
313	243.3	196.9	373	289.9	234.7	433	336.5	272.5	493	383.1	310.2	553	429.7	348.0	
314	244.0	197.6	374	290.7	235.3	434	337.3	273.1	494	383.9	310.8	554	430.5	348.6	
315	244.8	198.2	375	291.4	236.0	435	338.1	273.7	495	384.7	311.5	555	431.3	349.2	
316	245.6	198.8	376	292.2	236.6	436	338.8	274.3	496	385.5	312.1	556	432.1	349.9	
317	246.4	199.5	377	293.0	237.2	437	339.6	275.0	497	386.2	312.7	557	432.8	350.5	
318	247.1	200.1	378	293.8	237.8	438	340.4	275.6	498	387.0	313.3	558	433.6	351.1	
319	247.9	200.7	379	294.5	238.5	439	341.2	276.2	499	387.8	314.0	559	434.4	351.7	
320	248.7	201.3	380	295.3	239.1	440	342.0	276.9	500	388.6	314.7	560	435.2	352.4	
321	249.5	202.0	381	296.1	239.7	441	342.7	277.5	501	389.4	315.3	561	435.9	353.0	
322	250.3	202.6	382	296.9	240.4	442	343.5	278.1	502	390.1	315.9	562	436.7	353.6	
323	251.0	203.2	383	297.7	241.0	443	344.3	278.7	503	390.9	316.5	563	437.5	354.3	
324	251.8	203.9	384	298.4	241.6	444	345.1	279.4	504	391.7	317.1	564	438.3	354.9	
325	252.6	204.5	385	299.2	242.2	445	345.8	280.0	505	392.5	317.8	565	439.1	355.5	
326	253.4	205.1	386	300.0	242.9	446	346.6	280.6	506	393.2	318.4	566	439.8	356.2	
327	254.1	205.7	387	300.8	243.5	447	347.4	281.3	507	394.0	319.0	567	440.6	356.8	
328	254.9	206.4	388	301.5	244.1	448	348.2	281.9	508	394.8	319.6	568	441.4	357.4	
329	255.7	207.0	389	302.3	244.8	449	349.0	282.5	509	395.6	320.3	569	442.2	358.1	
330	256.5	207.6	390	303.1	245.4	450	349.7	283.2	510	396.3	320.9	570	443.0	358.7	
331	257.2	208.3	391	303.9	246.0	451	350.5	283.8	511	397.1	321.6	571	443.7	359.3	
332	258.0	208.9	392	304.7	246.7	452	351.3	284.4	512	397.9	322.2	572	444.5	359.9	
333	258.8	209.5	393	305.4	247.3	453	352.1	285.0	513	398.7	322.8	573	445.3	360.6	
334	259.6	210.2	394	306.2	247.9	454	352.8	285.7	514	399.4	323.4	574	446.1	361.2	
335	260.4	210.8	395	307.0	248.5	455	353.6	286.3	515	400.2	324.1	575	446.9	361.8	
336	261.1	211.4	396	307.8	249.2	456	354.4	286.9	516	401.0	324.7	576	447.6	362.4	
337	261.9	212.0	397	308.5	249.8	457	355.2	287.6	517	401.8	325.3	577	448.4	363.1	
338	262.7	212.7	398	309.3	250.4	458	355.9	288.2	518	402.5	325.9	578	449.2	363.7	
339	263.5	213.3	399	310.1	251.1	459	356.7	288.8	519	403.3	326.6	579	450.0	364.3	
340	264.2	213.9	400	310.9	251.7	460	357.5	289.4	520	404.1	327.2	580	450.7	365.0	
341	265.0	214.6	401	311.6	252.3	461	358.3	290.1	521	404.9	327.8	581	451.5	365.6	
342	265.8	215.2	402	312.4	252.9	462	359.1	290.7	522	405.7	328.5	582	452.3	366.2	
343	266.6	215.8	403	313.2	253.6	463	359.8	291.3	523	406.4	329.1	583	453.1	366.9	
344	267.3	216.4	404	314.0	254.2	464	360.6	292.0	524	407.2	329.7	584	453.9	367.5	
345	268.1	217.1	405	314.8	254.8	465	361.4	292.6	525	408.0	330.4	585	454.6	368.1	
346	268.9	217.7	406	315.5	255.5	466	362.2	293.2	526	408.8	331.0	586	455.4	368.8	
347	269.7	218.3	407	316.3	256.1	467	362.9	293.8	527	409.5	331.6	587	456.2	369.4	
348	270.5	219.0	408	317.1	256.7	468	363.7	294.5	528	410.3	332.3	588	457.0	370.0	
349	271.2	219.6	409	317.9	257.3	469	364.5	295.1	529	411.1	332.9	589	457.8	370.6	
350	272.0	220.2	410	318.6	258.0	470	365.3	295.7	530	411.9	333.5	590	458.5	371.3	
351	272.8	220.8	411	319.4	258.6	471	366.0	296.4	531	412.6	334.1	591	459.3	371.9	
352	273.6	221.5	412	320.2	259.2	472	366.8	297.0	532	413.4	334.8	592	460.1	372.5	
353	274.3	222.1	413	321.0	259.9	473	367.6	297.6	533	414.2	335.4	593	460.9	373.2	
354	275.1	222.7	414	321.8	260.5	474	368.4	298.3	534	415.0	336.1	594	461.6	373.8	
355	275.9	223.4	415	322.5	261.1	475	369.2	298.9	535	415.8	336.7	595	462.4	374.4	
356	276.7	224.0	416	323.3	261.8	476	369.9	299.5	536	416.5	337.3	596	463.2	375.1	
357	277.5	224.6	417	324.1	262.4	477	370.7	300.1	537	417.3	337.9	597	464.0	375.7	
358	278.2	225.3	418	324.9	263.0	478	371.5	300.8	538	418.1	338.5	598	464.8	376.3	
359	279.0	225.9	419	325.6	263.6	479	372.3	301.4	539	418.9	339.1	599	465.5	376.9	
360	279.8	226.5	420	326.4	264.3	480	373.0	302.0	540	419.6	339.8	600	466.3	377.6	
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	
51°												3h 24m			

TRAVERSE TABLE TO DEGREES.

40°									2° 40'					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0.8	0.6	61	46.7	39.2	121	92.7	77.8	181	138.7	116.3	241	184.6	154.9
2	1.5	1.3	62	47.5	39.9	122	93.5	78.4	182	139.4	117.0	242	185.4	155.6
3	2.3	1.9	63	48.3	40.5	123	94.3	79.1	183	140.2	117.6	243	186.1	156.2
4	3.1	2.6	64	49.0	41.1	124	95.0	79.7	184	141.0	118.3	244	186.9	156.8
5	3.8	3.2	65	49.8	41.8	125	95.8	80.3	185	141.7	118.9	245	187.7	157.5
6	4.6	3.9	66	50.6	42.4	126	96.5	81.0	186	142.5	119.6	246	188.4	158.1
7	5.4	4.5	67	51.3	43.1	127	97.3	81.6	187	143.3	120.2	247	189.2	158.8
8	6.1	5.1	68	52.1	43.7	128	98.1	82.3	188	144.0	120.8	248	190.0	159.4
9	6.9	5.8	69	52.9	44.4	129	98.8	82.9	189	144.8	121.5	249	190.7	160.1
10	7.7	6.4	70	53.6	45.0	130	99.6	83.6	190	145.5	122.1	250	191.5	160.7
11	8.4	7.1	71	54.4	45.6	131	100.4	84.2	191	146.3	122.8	251	192.3	161.3
12	9.2	7.7	72	55.2	46.3	132	101.1	84.8	192	147.1	123.4	252	193.0	162.0
13	10.0	8.4	73	55.9	46.9	133	101.9	85.5	193	147.8	124.1	253	193.8	162.6
14	10.7	9.0	74	56.7	47.6	134	102.6	86.1	194	148.6	124.7	254	194.6	163.3
15	11.5	9.6	75	57.5	48.2	135	103.4	86.8	195	149.4	125.3	255	195.3	163.9
16	12.3	10.3	76	58.2	48.9	136	104.2	87.4	196	150.1	126.0	256	196.1	164.6
17	13.0	10.9	77	59.0	49.5	137	104.9	88.1	197	150.9	126.6	257	196.9	165.2
18	13.8	11.6	78	59.8	50.1	138	105.7	88.7	198	151.7	127.3	258	197.6	165.8
19	14.6	12.2	79	60.5	50.8	139	106.5	89.3	199	152.4	127.9	259	198.4	166.5
20	15.3	12.9	80	61.3	51.4	140	107.2	90.0	200	153.2	128.6	260	199.2	167.1
21	16.1	13.5	81	62.0	52.1	141	108.0	90.6	201	154.0	129.2	261	199.9	167.8
22	16.9	14.1	82	62.8	52.7	142	108.8	91.3	202	154.7	129.8	262	200.7	168.4
23	17.6	14.8	83	63.6	53.4	143	109.5	91.9	203	155.5	130.5	263	201.5	169.1
24	18.4	15.4	84	64.3	54.0	144	110.3	92.6	204	156.3	131.1	264	202.2	169.7
25	19.2	16.1	85	65.1	54.6	145	111.1	93.2	205	157.0	131.8	265	203.0	170.3
26	19.9	16.7	86	65.9	55.3	146	111.8	93.8	206	157.8	132.4	266	203.8	171.0
27	20.7	17.4	87	66.6	55.9	147	112.6	94.5	207	158.6	133.1	267	204.5	171.6
28	21.4	18.0	88	67.4	56.6	148	113.4	95.1	208	159.3	133.7	268	205.3	172.3
29	22.2	18.6	89	68.2	57.2	149	114.1	95.8	209	160.1	134.3	269	206.1	172.9
30	23.0	19.3	90	68.9	57.9	150	114.9	96.4	210	160.9	135.0	270	206.8	173.6
31	23.7	19.9	91	69.7	58.5	151	115.7	97.1	211	161.6	135.6	271	207.6	174.2
32	24.5	20.6	92	70.5	59.1	152	116.4	97.7	212	162.4	136.3	272	208.4	174.8
33	25.3	21.2	93	71.2	59.8	153	117.2	98.3	213	163.2	136.9	273	209.1	175.5
34	26.0	21.9	94	72.0	60.4	154	118.0	99.0	214	163.9	137.6	274	209.9	176.1
35	26.8	22.5	95	72.8	61.1	155	118.7	99.6	215	164.7	138.2	275	210.7	176.8
36	27.6	23.1	96	73.5	61.7	156	119.5	100.3	216	165.5	138.8	276	211.4	177.4
37	28.3	23.8	97	74.3	62.4	157	120.3	100.9	217	166.2	139.5	277	212.2	178.1
38	29.1	24.4	98	75.1	63.0	158	121.0	101.6	218	167.0	140.1	278	213.0	178.7
39	29.9	25.1	99	75.8	63.6	159	121.8	102.2	219	167.8	140.8	279	213.7	179.3
40	30.6	25.7	100	76.6	64.3	160	122.6	102.8	220	168.5	141.4	280	214.5	180.0
41	31.4	26.4	101	77.4	64.9	161	123.3	103.5	221	169.3	142.1	281	215.3	180.6
42	32.2	27.0	102	78.1	65.6	162	124.1	104.1	222	170.1	142.7	282	216.0	181.3
43	32.9	27.6	103	78.9	66.2	163	124.9	104.8	223	170.8	143.3	283	216.8	181.9
44	33.7	28.3	104	79.7	66.8	164	125.6	105.4	224	171.6	144.0	284	217.6	182.6
45	34.5	28.9	105	80.4	67.5	165	126.4	106.1	225	172.4	144.6	285	218.3	183.2
46	35.2	29.6	106	81.2	68.1	166	127.2	106.7	226	173.1	145.3	286	219.1	183.8
47	36.0	30.2	107	82.0	68.8	167	127.9	107.3	227	173.9	145.9	287	219.9	184.5
48	36.8	30.9	108	82.7	69.4	168	128.7	108.0	228	174.7	146.6	288	220.6	185.1
49	37.5	31.5	109	83.5	70.1	169	129.5	108.6	229	175.4	147.2	289	221.4	185.8
50	38.3	32.1	110	84.3	70.7	170	130.2	109.3	230	176.2	147.8	290	222.2	186.4
51	39.1	32.8	111	85.0	71.3	171	131.0	109.9	231	177.0	148.5	291	222.9	187.1
52	39.8	33.4	112	85.8	72.0	172	131.8	110.6	232	177.7	149.1	292	223.7	187.7
53	40.6	34.1	113	86.6	72.6	173	132.5	111.2	233	178.5	149.8	293	224.5	188.3
54	41.4	34.7	114	87.3	73.3	174	133.3	111.8	234	179.3	150.4	294	225.2	189.0
55	42.1	35.4	115	88.1	73.9	175	134.1	112.5	235	180.0	151.1	295	226.0	189.6
56	42.9	36.0	116	88.9	74.6	176	134.8	113.1	236	180.8	151.7	296	226.7	190.3
57	43.7	36.6	117	89.6	75.2	177	135.6	113.8	237	181.6	152.3	297	227.5	190.9
58	44.4	37.3	118	90.4	75.8	178	136.4	114.4	238	182.3	153.0	298	228.3	191.6
59	45.2	37.9	119	91.2	76.5	179	137.1	115.1	239	183.1	153.6	299	229.0	192.2
60	46.0	38.6	120	91.9	77.1	180	137.9	115.7	240	183.9	154.3	300	229.8	192.8
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

511

TRAVERSE TABLE TO DEGREES														
40°									2h 40m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	230.6	193.5	361	276.5	232.1	421	322.5	270.6	481	368.5	309.2	541	414.4	347.7
302	231.3	194.1	362	277.3	232.7	422	323.3	271.3	482	369.2	309.8	542	415.2	348.4
303	232.1	194.8	363	278.1	233.3	423	324.0	271.9	483	370.0	310.5	543	416.0	349.0
304	232.9	195.4	364	278.8	234.0	424	324.8	272.6	484	370.8	311.1	544	416.7	349.7
305	233.6	196.1	365	279.6	234.6	425	325.6	273.2	485	371.5	311.7	545	417.5	350.3
306	234.4	196.7	366	280.4	235.3	426	326.3	273.8	486	372.3	312.4	546	418.3	351.0
307	235.2	197.3	367	281.1	235.9	427	327.1	274.5	487	373.1	313.0	547	419.0	351.6
308	235.9	198.0	368	281.9	236.6	428	327.9	275.1	488	373.8	313.6	548	419.8	352.2
309	236.7	198.6	369	282.7	237.2	429	328.6	275.8	489	374.6	314.3	549	420.6	352.9
310	237.5	199.3	370	283.4	237.8	430	329.4	276.4	490	375.4	314.9	550	421.3	353.5
311	238.2	199.9	371	284.2	238.5	431	330.2	277.1	491	376.1	315.6	551	422.1	354.2
312	239.0	200.6	372	285.0	239.1	432	330.9	277.7	492	376.9	316.2	552	422.9	354.8
313	239.8	201.2	373	285.7	239.7	433	331.7	278.3	493	377.7	316.9	553	423.6	355.5
314	240.5	201.8	374	286.5	240.4	434	332.5	279.0	494	378.4	317.5	554	424.4	356.1
315	241.3	202.5	375	287.3	241.0	435	333.2	279.6	495	379.2	318.2	555	425.2	356.8
316	242.1	203.1	376	288.0	241.7	436	334.0	280.3	496	380.0	318.8	556	425.9	357.4
317	242.8	203.8	377	288.8	242.3	437	334.8	280.9	497	380.7	319.5	557	426.7	358.0
318	243.6	204.4	378	289.6	243.0	438	335.5	281.6	498	381.5	320.1	558	427.5	358.7
319	244.4	205.1	379	290.3	243.6	439	336.3	282.2	499	382.3	320.8	559	428.2	359.3
320	245.1	205.7	380	291.1	244.3	440	337.1	282.8	500	383.0	321.4	560	429.0	360.0
321	245.9	206.3	381	291.9	244.9	441	337.8	283.5	501	383.8	322.0	561	429.8	360.6
322	246.7	207.0	382	292.6	245.6	442	338.6	284.1	502	384.6	322.7	562	430.5	361.2
323	247.4	207.6	383	293.4	246.2	443	339.4	284.8	503	385.3	323.3	563	431.3	361.9
324	248.2	208.3	384	294.2	246.8	444	340.1	285.4	504	386.1	324.0	564	432.1	362.5
325	249.0	208.9	385	294.9	247.5	445	340.9	286.0	505	386.8	324.6	565	432.8	363.2
326	249.7	209.6	386	295.7	248.1	446	341.7	286.7	506	387.6	325.2	566	433.6	363.8
327	250.5	210.2	387	296.5	248.8	447	342.4	287.3	507	388.4	325.9	567	434.3	364.5
328	251.3	210.8	388	297.2	249.4	448	343.2	288.0	508	389.2	326.5	568	435.1	365.1
329	252.0	211.5	389	298.0	250.1	449	344.0	288.6	509	389.9	327.1	569	435.9	365.8
330	252.8	212.1	390	298.8	250.7	450	344.7	289.3	510	390.7	327.8	570	436.6	366.4
331	253.6	212.8	391	299.5	251.3	451	345.5	289.9	511	391.5	328.4	571	437.4	367.0
332	254.3	213.4	392	300.3	252.0	452	346.3	290.5	512	392.2	329.1	572	438.2	367.7
333	255.1	214.1	393	301.1	252.6	453	347.0	291.2	513	393.0	329.7	573	438.9	368.3
334	255.9	214.7	394	301.8	253.3	454	347.8	291.8	514	393.8	330.4	574	439.7	369.0
335	256.6	215.3	395	302.6	253.9	455	348.6	292.5	515	394.5	331.0	575	440.5	369.6
336	257.4	216.0	396	303.4	254.6	456	349.3	293.1	516	395.3	331.6	576	441.2	370.2
337	258.2	216.6	397	304.1	255.2	457	350.1	293.8	517	396.1	332.3	577	442.0	370.9
338	258.9	217.3	398	304.9	255.8	458	350.8	294.4	518	396.8	332.9	578	442.8	371.5
339	259.7	217.9	399	305.7	256.5	459	351.6	295.0	519	397.6	333.6	579	443.5	372.2
340	260.5	218.6	400	306.4	257.1	460	352.4	295.7	520	398.3	334.2	580	444.3	372.8
341	261.2	219.2	401	307.2	257.8	461	353.1	296.3	521	399.1	334.9	581	445.1	373.5
342	262.0	219.8	402	308.0	258.4	462	353.9	297.0	522	399.9	335.5	582	445.8	374.1
343	262.8	220.5	403	308.7	259.1	463	354.7	297.6	523	400.6	336.1	583	446.6	374.8
344	263.5	221.1	404	309.5	259.7	464	355.4	298.3	524	401.4	336.8	584	447.4	375.4
345	264.3	221.8	405	310.2	260.3	465	356.2	298.9	525	402.2	337.4	585	448.1	376.0
346	265.1	222.4	406	311.0	261.0	466	357.0	299.5	526	402.9	338.1	586	448.9	376.7
347	265.8	223.1	407	311.8	261.6	467	357.7	300.2	527	403.7	338.7	587	449.7	377.3
348	266.6	223.7	408	312.5	262.3	468	358.5	300.8	528	404.5	339.4	588	450.4	378.0
349	267.4	224.3	409	313.3	262.9	469	359.3	301.5	529	405.2	340.0	589	451.2	378.6
350	268.1	225.0	410	314.1	263.6	470	360.0	302.1	530	406.0	340.6	590	452.0	379.2
351	268.9	225.6	411	314.8	264.2	471	360.8	302.8	531	406.8	341.3	591	452.7	379.9
352	269.6	226.3	412	315.6	264.8	472	361.6	303.4	532	407.5	341.9	592	453.5	380.5
353	270.4	226.9	413	316.4	265.5	473	362.3	304.0	533	408.3	342.6	593	454.3	381.2
354	271.2	227.6	414	317.1	266.1	474	363.1	304.7	534	409.1	343.2	594	455.0	381.8
355	271.9	228.2	415	317.9	266.8	475	363.9	305.3	535	409.8	343.9	595	455.8	382.4
356	272.7	228.8	416	318.7	267.4	476	364.6	306.0	536	410.6	344.5	596	456.6	383.1
357	273.5	229.5	417	319.4	268.1	477	365.4	306.6	537	411.4	345.2	597	457.3	383.7
358	274.2	230.1	418	320.2	268.7	478	366.2	307.3	538	412.1	345.8	598	458.1	384.4
359	275.0	230.8	419	321.0	269.3	479	366.9	307.9	539	412.9	346.4	599	458.9	385.0
360	275.8	231.4	420	321.7	270.0	480	367.7	308.5	540	413.7	347.1	600	459.6	385.7
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
50°									3h 20m					

TRAVERSE TABLE TO DEGREES														
41°									2° 44'					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0°8	0°7	61	46°0	40°0	121	91°3	79°4	181	136°6	118°7	241	181°9	158°1
2	1°5	1°3	62	46°8	40°7	122	92°1	80°0	182	137°4	119°4	242	182°6	158°8
3	2°3	2°0	63	47°5	41°3	123	92°8	80°7	183	138°1	120°1	243	183°4	159°4
4	3°0	2°6	64	48°3	42°0	124	93°6	81°4	184	138°9	120°7	244	184°1	160°1
5	3°8	3°3	65	49°1	42°6	125	94°3	82°0	185	139°6	121°4	245	184°9	160°7
6	4°5	3°9	66	49°8	43°3	126	95°1	82°7	186	140°4	122°0	246	185°7	161°4
7	5°3	4°6	67	50°6	44°0	127	95°8	83°3	187	141°1	122°7	247	186°4	162°0
8	6°0	5°2	68	51°3	44°6	128	96°6	84°0	188	141°9	123°3	248	187°2	162°7
9	6°8	5°9	69	52°1	45°3	129	97°4	84°6	189	142°6	124°0	249	187°9	163°4
10	7°5	6°6	70	52°8	45°9	130	98°1	85°3	190	143°4	124°7	250	188°7	164°0
11	8°3	7°2	71	53°6	46°6	131	98°9	85°9	191	144°1	125°3	251	189°4	164°7
12	9°1	7°9	72	54°3	47°4	132	99°6	86°6	192	144°9	126°0	252	190°2	165°3
13	9°8	8°5	73	55°1	47°9	133	100°4	87°3	193	145°7	126°6	253	190°9	166°0
14	10°6	9°2	74	55°8	48°5	134	101°1	87°9	194	146°4	127°3	254	191°7	166°6
15	11°3	9°8	75	56°6	49°2	135	101°9	88°6	195	147°2	127°9	255	192°5	167°3
16	12°1	10°5	76	57°4	49°9	136	102°6	89°2	196	147°9	128°6	256	193°2	168°0
17	12°8	11°2	77	58°1	50°5	137	103°4	89°9	197	148°7	129°2	257	194°0	168°6
18	13°6	11°8	78	58°9	51°2	138	104°1	90°5	198	149°4	129°9	258	194°7	169°3
19	14°3	12°5	79	59°6	51°8	139	104°9	91°2	199	150°2	130°6	259	195°5	169°9
20	15°1	13°1	80	60°4	52°5	140	105°7	91°8	200	150°9	131°2	260	196°2	170°6
21	15°8	13°8	81	61°1	53°1	141	106°4	92°5	201	151°7	131°9	261	197°0	171°2
22	16°6	14°4	82	61°9	53°8	142	107°2	93°2	202	152°5	132°5	262	197°7	171°9
23	17°4	15°1	83	62°6	54°5	143	107°9	93°8	203	153°2	133°2	263	198°5	172°5
24	18°1	15°7	84	63°4	55°1	144	108°7	94°5	204	154°0	133°8	264	199°2	173°2
25	18°9	16°4	85	64°2	55°8	145	109°4	95°1	205	154°7	134°5	265	200°0	173°9
26	19°6	17°1	86	64°9	56°4	146	110°2	95°8	206	155°5	135°1	266	200°8	174°5
27	20°4	17°7	87	65°7	57°1	147	110°9	96°4	207	156°2	135°8	267	201°5	175°2
28	21°1	18°4	88	66°4	57°7	148	111°7	97°1	208	157°0	136°5	268	202°3	175°8
29	21°9	19°0	89	67°2	58°4	149	112°5	97°8	209	157°7	137°1	269	203°0	176°5
30	22°6	19°7	90	67°9	59°0	150	113°2	98°4	210	158°5	137°8	270	203°8	177°1
31	23°4	20°3	91	68°7	59°7	151	114°0	99°1	211	159°2	138°4	271	204°5	177°8
32	24°2	21°0	92	69°4	60°4	152	114°7	99°7	212	160°0	139°1	272	205°3	178°4
33	24°9	21°6	93	70°2	61°0	153	115°5	100°4	213	160°8	139°7	273	206°0	179°1
34	25°7	22°3	94	70°9	61°7	154	116°2	101°0	214	161°5	140°4	274	206°8	179°8
35	26°4	23°0	95	71°7	62°3	155	117°0	101°7	215	162°3	141°1	275	207°5	180°4
36	27°2	23°6	96	72°5	63°0	156	117°7	102°3	216	163°0	141°7	276	208°3	181°1
37	27°9	24°3	97	73°2	63°6	157	118°5	103°0	217	163°8	142°4	277	209°1	181°7
38	28°7	24°9	98	74°0	64°3	158	119°2	103°7	218	164°5	143°0	278	209°8	182°4
39	29°4	25°6	99	74°7	64°9	159	120°0	104°3	219	165°3	143°7	279	210°6	183°0
40	30°2	26°2	100	75°5	65°6	160	120°8	105°0	220	166°0	144°3	280	211°3	183°7
41	30°9	26°9	101	76°2	66°3	161	121°5	105°6	221	166°8	145°0	281	212°1	184°4
42	31°7	27°6	102	77°0	66°9	162	122°3	106°3	222	167°5	145°6	282	212°8	185°0
43	32°5	28°2	103	77°7	67°6	163	123°0	106°9	223	168°3	146°3	283	213°6	185°7
44	33°2	28°9	104	78°5	68°2	164	123°8	107°6	224	169°1	147°0	284	214°3	186°3
45	34°0	29°5	105	79°2	68°9	165	124°5	108°2	225	169°8	147°6	285	215°1	187°0
46	34°7	30°2	106	80°0	69°5	166	125°3	108°9	226	170°6	148°3	286	215°8	187°6
47	35°5	30°8	107	80°8	70°2	167	126°0	109°6	227	171°3	148°9	287	216°6	188°3
48	36°2	31°5	108	81°5	70°9	168	126°8	110°2	228	172°1	149°6	288	217°4	188°9
49	37°0	32°1	109	82°3	71°5	169	127°5	110°9	229	172°8	150°2	289	218°1	189°6
50	37°7	32°8	110	83°0	72°2	170	128°3	111°5	230	173°6	150°9	290	218°9	190°3
51	38°5	33°5	111	83°8	72°8	171	129°1	112°2	231	174°3	151°5	291	219°6	190°9
52	39°2	34°1	112	84°5	73°5	172	129°8	112°8	232	175°1	152°2	292	220°4	191°6
53	40°0	34°8	113	85°3	74°1	173	130°6	113°5	233	175°8	152°9	293	221°1	192°2
54	40°8	35°4	114	86°0	74°8	174	131°3	114°2	234	176°6	153°5	294	221°9	192°9
55	41°5	36°1	115	86°8	75°4	175	132°1	114°8	235	177°4	154°2	295	222°6	193°5
56	42°3	36°7	116	87°5	76°1	176	132°8	115°5	236	178°1	154°8	296	223°4	194°2
57	43°0	37°4	117	88°3	76°8	177	133°6	116°1	237	178°9	155°5	297	224°1	194°8
58	43°8	38°1	118	89°1	77°4	178	134°3	116°8	238	179°6	156°1	298	224°9	195°5
59	44°5	38°7	119	89°8	78°1	179	135°1	117°4	239	180°4	156°8	299	225°7	196°2
60	45°3	39°4	120	90°6	78°7	180	135°8	118°1	240	181°1	157°5	300	226°4	196°8
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
49°									3° 16'					

TABLE 1

513

TRAVERSE TABLE TO DEGREES														
41°									2h 44m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	227.2	197.5	361	272.5	236.9	421	317.7	276.2	481	363.0	315.6	541	408.3	354.9
302	227.9	198.1	362	273.2	237.5	422	318.5	276.9	482	363.8	316.2	542	409.0	355.6
303	228.7	198.8	363	274.0	238.2	423	319.2	277.5	483	364.5	316.9	543	409.8	356.2
304	229.4	199.4	364	274.7	238.8	424	320.0	278.2	484	365.3	317.5	544	410.6	356.9
305	230.2	200.1	365	275.5	239.5	425	320.8	278.8	485	366.0	318.2	545	411.3	357.5
306	230.9	200.8	366	276.2	240.1	426	321.5	279.5	486	366.8	318.8	546	412.1	358.2
307	231.7	201.4	367	277.0	240.8	427	322.3	280.1	487	367.5	319.5	547	412.8	358.8
308	232.5	202.1	368	277.7	241.4	428	323.0	280.8	488	368.3	320.1	548	413.6	359.5
309	233.2	202.7	369	278.5	242.1	429	323.8	281.5	489	369.0	320.8	549	414.3	360.2
310	234.0	203.4	370	279.2	242.7	430	324.5	282.1	490	369.8	321.5	550	415.1	360.8
311	234.7	204.0	371	280.0	243.4	431	325.3	282.8	491	370.6	322.1	551	415.8	361.5
312	235.5	204.7	372	280.8	244.1	432	326.0	283.4	492	371.3	322.8	552	416.6	362.1
313	236.2	205.4	373	281.5	244.7	433	326.8	284.1	493	372.1	323.4	553	417.3	362.8
314	237.0	206.0	374	282.3	245.4	434	327.5	284.7	494	372.8	324.1	554	418.1	363.4
315	237.7	206.7	375	283.0	246.0	435	328.3	285.4	495	373.6	324.7	555	418.9	364.1
316	238.5	207.3	376	283.8	246.7	436	329.1	286.0	496	374.3	325.4	556	419.6	364.8
317	239.2	208.0	377	284.5	247.3	437	329.8	286.7	497	375.1	326.0	557	420.4	365.4
318	240.0	208.6	378	285.3	248.0	438	330.6	287.4	498	375.8	326.7	558	421.1	366.1
319	240.8	209.3	379	286.0	248.7	439	331.3	288.0	499	376.6	327.4	559	421.9	366.7
320	241.5	209.9	380	286.8	249.3	440	332.1	288.7	500	377.3	328.0	560	422.6	367.4
321	242.3	210.6	381	287.5	250.0	441	332.8	289.3	501	378.1	328.7	561	423.4	368.0
322	243.0	211.3	382	288.3	250.6	442	333.6	290.0	502	378.9	329.3	562	424.1	368.7
323	243.8	211.9	383	289.1	251.3	443	334.3	290.6	503	379.6	330.0	563	424.9	369.4
324	244.5	212.6	384	289.8	251.9	444	335.1	291.3	504	380.4	330.6	564	425.7	370.0
325	245.3	213.2	385	290.6	252.6	445	335.8	292.0	505	381.1	331.3	565	426.4	370.7
326	246.0	213.9	386	291.3	253.2	446	336.6	292.6	506	381.9	332.0	566	427.2	371.3
327	246.8	214.5	387	292.1	253.9	447	337.4	293.3	507	382.6	332.6	567	427.9	372.0
328	247.5	215.2	388	292.8	254.6	448	338.1	293.9	508	383.4	333.3	568	428.7	372.6
329	248.3	215.9	389	293.6	255.2	449	338.9	294.6	509	384.1	333.9	569	429.4	373.3
330	249.1	216.5	390	294.3	255.9	450	339.6	295.2	510	384.9	334.6	570	430.2	374.0
331	249.8	217.2	391	295.1	256.5	451	340.4	295.9	511	385.7	335.2	571	430.9	374.6
332	250.6	217.8	392	295.8	257.2	452	341.1	296.5	512	386.4	335.9	572	431.7	375.3
333	251.3	218.5	393	296.6	257.8	453	341.9	297.2	513	387.2	336.5	573	432.4	375.9
334	252.1	219.1	394	297.4	258.5	454	342.6	297.9	514	387.9	337.2	574	433.2	376.6
335	252.8	219.8	395	298.1	259.2	455	343.4	298.5	515	388.7	337.9	575	434.0	377.2
336	253.6	220.4	396	298.9	259.8	456	344.1	299.2	516	389.4	338.5	576	434.7	377.9
337	254.3	221.1	397	299.6	260.5	457	344.9	299.8	517	390.2	339.2	577	435.5	378.5
338	255.1	221.8	398	300.4	261.1	458	345.7	300.5	518	390.9	339.8	578	436.2	379.2
339	255.8	222.4	399	301.1	261.8	459	346.4	301.1	519	391.7	340.5	579	437.0	379.8
340	256.6	223.1	400	301.9	262.4	460	347.2	301.8	520	392.4	341.1	580	437.7	380.5
341	257.4	223.7	401	302.6	263.1	461	347.9	302.5	521	393.2	341.8	581	438.5	381.2
342	258.1	224.4	402	303.4	263.7	462	348.7	303.1	522	394.0	342.5	582	439.2	381.8
343	258.9	225.0	403	304.2	264.4	463	349.4	303.8	523	394.7	343.1	583	440.0	382.5
344	259.6	225.7	404	304.9	265.1	464	350.2	304.4	524	395.5	343.8	584	440.7	383.2
345	260.4	226.3	405	305.7	265.7	465	350.9	305.1	525	396.2	344.4	585	441.5	383.8
346	261.1	227.0	406	306.4	266.4	466	351.7	305.7	526	397.0	345.1	586	442.3	384.5
347	261.9	227.7	407	307.2	267.0	467	352.5	306.4	527	397.7	345.7	587	443.0	385.1
348	262.6	228.3	408	307.9	267.7	468	353.2	307.0	528	398.5	346.4	588	443.8	385.8
349	263.4	229.0	409	308.7	268.3	469	354.0	307.7	529	399.2	347.0	589	444.5	386.4
350	264.2	229.6	410	309.4	269.0	470	354.7	308.4	530	400.0	347.7	590	445.3	387.1
351	264.9	230.3	411	310.2	269.6	471	355.5	309.0	531	400.7	348.4	591	446.0	387.7
352	265.7	230.9	412	310.9	270.3	472	356.2	309.7	532	401.5	349.0	592	446.8	388.4
353	266.4	231.6	413	311.7	271.0	473	357.0	310.3	533	402.2	349.7	593	447.5	389.1
354	267.2	232.3	414	312.5	271.6	474	357.7	311.0	534	403.0	350.3	594	448.3	389.7
355	267.9	232.9	415	313.2	272.3	475	358.5	311.6	535	403.8	351.0	595	449.1	390.4
356	268.7	233.6	416	314.0	272.9	476	359.2	312.3	536	404.5	351.6	596	449.8	391.0
357	269.4	234.2	417	314.7	273.6	477	360.0	312.9	537	405.3	352.3	597	450.6	391.7
358	270.2	234.9	418	315.5	274.2	478	360.8	313.6	538	406.0	352.9	598	451.3	392.3
359	270.9	235.5	419	316.2	274.9	479	361.5	314.3	539	406.8	353.6	599	452.1	393.0
360	271.7	236.2	420	317.0	275.6	480	362.3	314.9	540	407.5	354.3	600	452.8	393.6
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
49°									3h 16m					

L L

TRAVERSE TABLE TO DEGREES

42°									2° 48'								
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0.7	0.7	61	45.3	40.8	121	89.9	81.0	181	134.5	121.1	241	179.1	161.3			
2	1.5	1.3	62	46.1	41.5	122	90.7	81.6	182	135.3	121.8	242	179.8	161.9			
3	2.2	2.0	63	46.8	42.2	123	91.4	82.3	183	136.0	122.5	243	180.6	162.6			
4	3.0	2.7	64	47.6	42.8	124	92.1	83.0	184	136.7	123.1	244	181.3	163.3			
5	3.7	3.3	65	48.3	43.5	125	92.9	83.6	185	137.4	123.8	245	182.1	163.9			
6	4.5	4.0	66	49.0	44.2	126	93.6	84.3	186	138.2	124.5	246	182.8	164.6			
7	5.2	4.7	67	49.8	44.8	127	94.4	85.0	187	139.0	125.1	247	183.6	165.3			
8	5.9	5.4	68	50.5	45.5	128	95.1	85.6	188	139.7	125.8	248	184.3	165.9			
9	6.7	6.0	69	51.3	46.2	129	95.9	86.3	189	140.5	126.5	249	185.0	166.6			
10	7.4	6.7	70	52.0	46.8	130	96.6	87.0	190	141.2	127.1	250	185.8	167.3			
11	8.2	7.4	71	52.8	47.5	131	97.4	87.7	191	141.9	127.8	251	186.5	168.0			
12	8.9	8.0	72	53.5	48.2	132	98.1	88.3	192	142.7	128.5	252	187.3	168.6			
13	9.7	8.7	73	54.2	48.8	133	98.8	89.0	193	143.4	129.1	253	188.0	169.3			
14	10.4	9.4	74	55.0	49.5	134	99.6	89.7	194	144.2	129.8	254	188.8	170.0			
15	11.1	10.0	75	55.7	50.2	135	100.3	90.3	195	144.9	130.5	255	189.5	170.6			
16	11.9	10.7	76	56.5	50.9	136	101.1	91.0	196	145.7	131.1	256	190.2	171.3			
17	12.6	11.4	77	57.2	51.5	137	101.8	91.7	197	146.4	131.8	257	191.0	172.0			
18	13.4	12.0	78	58.0	52.2	138	102.6	92.3	198	147.1	132.5	258	191.7	172.6			
19	14.1	12.7	79	58.7	52.9	139	103.3	93.0	199	147.9	133.2	259	192.5	173.3			
20	14.9	13.4	80	59.5	53.5	140	104.0	93.7	200	148.6	133.8	260	193.2	174.0			
21	15.6	14.1	81	60.2	54.2	141	104.8	94.3	201	149.4	134.5	261	194.0	174.6			
22	16.3	14.7	82	60.9	54.9	142	105.5	95.0	202	150.1	135.2	262	194.7	175.3			
23	17.1	15.4	83	61.7	55.5	143	106.3	95.7	203	150.9	135.8	263	195.4	176.0			
24	17.8	16.1	84	62.4	56.2	144	107.0	96.4	204	151.6	136.5	264	196.2	176.7			
25	18.6	16.7	85	63.2	56.9	145	107.8	97.0	205	152.3	137.2	265	196.9	177.3			
26	19.3	17.4	86	63.9	57.5	146	108.5	97.7	206	153.1	137.8	266	197.7	178.0			
27	20.1	18.1	87	64.7	58.2	147	109.2	98.4	207	153.8	138.5	267	198.4	178.7			
28	20.8	18.7	88	65.4	58.9	148	110.0	99.0	208	154.6	139.2	268	199.2	179.3			
29	21.6	19.4	89	66.1	59.6	149	110.7	99.7	209	155.3	139.8	269	199.9	180.0			
30	22.3	20.1	90	66.9	60.2	150	111.5	100.4	210	156.1	140.5	270	200.6	180.7			
31	23.0	20.7	91	67.6	60.9	151	112.2	101.0	211	156.8	141.2	271	201.4	181.3			
32	23.8	21.4	92	68.4	61.6	152	113.0	101.7	212	157.5	141.9	272	202.1	182.0			
33	24.5	22.1	93	69.1	62.2	153	113.7	102.4	213	158.3	142.5	273	202.9	182.7			
34	25.3	22.8	94	69.9	62.9	154	114.4	103.0	214	159.0	143.2	274	203.6	183.3			
35	26.0	23.4	95	70.6	63.6	155	115.2	103.7	215	159.8	143.9	275	204.4	184.0			
36	26.8	24.1	96	71.3	64.2	156	115.9	104.4	216	160.5	144.5	276	205.1	184.7			
37	27.5	24.8	97	72.1	64.9	157	116.7	105.1	217	161.3	145.2	277	205.9	185.3			
38	28.2	25.4	98	72.8	65.6	158	117.4	105.7	218	162.0	145.9	278	206.6	186.0			
39	29.0	26.1	99	73.6	66.2	159	118.2	106.4	219	162.7	146.5	279	207.3	186.7			
40	29.7	26.8	100	74.3	66.9	160	118.9	107.1	220	163.5	147.2	280	208.1	187.4			
41	30.5	27.4	101	75.1	67.6	161	119.6	107.7	221	164.2	147.9	281	208.8	188.0			
42	31.2	28.1	102	75.8	68.3	162	120.4	108.4	222	165.0	148.5	282	209.6	188.7			
43	32.0	28.8	103	76.5	68.9	163	121.1	109.1	223	165.7	149.2	283	210.3	189.4			
44	32.7	29.4	104	77.3	69.6	164	121.9	109.7	224	166.5	149.9	284	211.1	190.0			
45	33.4	30.1	105	78.0	70.3	165	122.6	110.4	225	167.2	150.6	285	211.8	190.7			
46	34.2	30.8	106	78.8	70.9	166	123.4	111.1	226	168.0	151.2	286	212.5	191.4			
47	34.9	31.4	107	79.5	71.6	167	124.1	111.7	227	168.7	151.9	287	213.3	192.0			
48	35.7	32.1	108	80.3	72.3	168	124.8	112.4	228	169.4	152.6	288	214.0	192.7			
49	36.4	32.8	109	81.0	72.9	169	125.6	113.1	229	170.2	153.2	289	214.8	193.4			
50	37.2	33.5	110	81.7	73.6	170	126.3	113.8	230	170.9	153.9	290	215.5	194.0			
51	37.9	34.1	111	82.5	74.3	171	127.1	114.4	231	171.7	154.6	291	216.3	194.7			
52	38.6	34.8	112	83.2	74.9	172	127.8	115.1	232	172.4	155.2	292	217.0	195.4			
53	39.4	35.5	113	84.0	75.6	173	128.6	115.8	233	173.2	155.9	293	217.7	196.1			
54	40.1	36.1	114	84.7	76.3	174	129.3	116.4	234	173.9	156.6	294	218.5	196.7			
55	40.9	36.8	115	85.5	77.0	175	130.1	117.1	235	174.6	157.2	295	219.2	197.4			
56	41.6	37.5	116	86.2	77.6	176	130.8	117.8	236	175.4	157.9	296	220.0	198.1			
57	42.4	38.1	117	86.9	78.3	177	131.5	118.4	237	176.1	158.6	297	220.7	198.7			
58	43.1	38.8	118	87.7	79.0	178	132.3	119.1	238	176.9	159.3	298	221.5	199.4			
59	43.8	39.5	119	88.4	79.6	179	133.0	119.8	239	177.6	159.9	299	222.2	200.1			
60	44.6	40.1	120	89.2	80.3	180	133.8	120.4	240	178.4	160.6	300	222.9	200.7			
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

515

TRAVERSE TABLE TO DEGREES

42°														
2h 48m														
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	223.7	201.4	361	268.3	241.6	421	312.9	281.7	481	357.5	321.9	541	402.1	362.0
302	224.4	202.1	362	269.0	242.2	422	313.6	282.4	482	358.2	322.5	542	402.8	362.7
303	225.2	202.8	363	269.8	242.9	423	314.4	283.0	483	358.9	323.2	543	403.5	363.3
304	225.9	203.4	364	270.5	243.6	424	315.1	283.7	484	359.7	323.9	544	404.3	364.0
305	226.6	204.1	365	271.2	244.2	425	315.8	284.4	485	360.4	324.6	545	405.0	364.7
306	227.4	204.8	366	272.0	244.9	426	316.6	285.1	486	361.2	325.2	546	405.8	365.4
307	228.1	205.4	367	272.7	245.6	427	317.3	285.7	487	361.9	325.9	547	406.5	366.0
308	228.9	206.1	368	273.5	246.2	428	318.1	286.4	488	362.7	326.6	548	407.2	366.7
309	229.6	206.8	369	274.2	246.9	429	318.8	287.1	489	363.4	327.2	549	408.0	367.4
310	230.4	207.4	370	275.0	247.6	430	319.6	287.7	490	364.1	327.9	550	408.7	368.0
311	231.1	208.1	371	275.7	248.3	431	320.3	288.4	491	364.9	328.6	551	409.5	368.7
312	231.9	208.8	372	276.5	248.9	432	321.0	289.1	492	365.6	329.2	552	410.2	369.4
313	232.6	209.4	373	277.2	249.6	433	321.8	289.7	493	366.4	329.9	553	411.0	370.0
314	233.3	210.1	374	277.9	250.3	434	322.5	290.4	494	367.1	330.6	554	411.7	370.7
315	234.1	210.8	375	278.7	250.9	435	323.3	291.1	495	367.9	331.3	555	412.4	371.4
316	234.8	211.5	376	279.4	251.6	436	324.0	291.7	496	368.6	331.9	556	413.2	372.0
317	235.6	212.1	377	280.2	252.3	437	324.8	292.4	497	369.3	332.5	557	413.9	372.7
318	236.3	212.8	378	280.9	252.9	438	325.5	293.1	498	370.1	333.3	558	414.7	373.4
319	237.1	213.5	379	281.7	253.6	439	326.2	293.8	499	370.8	333.9	559	415.4	374.1
320	237.8	214.1	380	282.4	254.3	440	327.0	294.4	500	371.6	334.6	560	416.2	374.7
321	238.6	214.8	381	283.1	254.9	441	327.7	295.1	501	372.3	335.3	561	416.9	375.4
322	239.3	215.5	382	283.9	255.6	442	328.5	295.8	502	373.1	335.9	562	417.6	376.1
323	240.0	216.1	383	284.6	256.3	443	329.2	296.4	503	373.8	336.6	563	418.4	376.7
324	240.8	216.8	384	285.4	257.0	444	330.0	297.1	504	374.5	337.2	564	419.1	377.4
325	241.5	217.5	385	286.1	257.6	445	330.7	297.8	505	375.3	337.9	565	419.9	378.1
326	242.3	218.1	386	286.9	258.3	446	331.4	298.4	506	376.0	338.6	566	420.6	378.7
327	243.0	218.8	387	287.6	259.0	447	332.2	299.1	507	376.8	339.3	567	421.4	379.4
328	243.8	219.5	388	288.3	259.6	448	332.9	299.8	508	377.5	339.9	568	422.1	380.1
329	244.5	220.1	389	289.1	260.3	449	333.7	300.4	509	378.3	340.6	569	422.8	380.7
330	245.2	220.8	390	289.8	261.0	450	334.4	301.1	510	379.0	341.3	570	423.6	381.4
331	246.0	221.5	391	290.6	261.6	451	335.2	301.8	511	379.7	341.9	571	424.3	382.1
332	246.7	222.2	392	291.3	262.3	452	335.9	302.5	512	380.5	342.6	572	425.1	382.8
333	247.5	222.8	393	292.1	263.0	453	336.6	303.1	513	381.2	343.3	573	425.8	383.4
334	248.2	223.5	394	292.8	263.6	454	337.4	303.8	514	382.0	343.9	574	426.6	384.1
335	249.0	224.2	395	293.5	264.3	455	338.1	304.5	515	382.7	344.6	575	427.3	384.8
336	249.7	224.8	396	294.3	265.0	456	338.9	305.1	516	383.5	345.3	576	428.0	385.4
337	250.4	225.5	397	295.0	265.7	457	339.6	305.8	517	384.2	346.0	577	428.8	386.1
338	251.2	226.2	398	295.8	266.3	458	340.4	306.5	518	384.9	346.6	578	429.5	386.8
339	251.9	226.8	399	296.5	267.0	459	341.1	307.1	519	385.7	347.3	579	430.3	387.4
340	252.7	227.5	400	297.3	267.7	460	341.8	307.8	520	386.4	348.0	580	431.0	388.1
341	253.4	228.2	401	298.0	268.3	461	342.6	308.5	521	387.2	348.6	581	431.8	388.8
342	254.2	228.8	402	298.7	269.0	462	343.3	309.1	522	387.9	349.3	582	432.5	389.4
343	254.9	229.5	403	299.5	269.7	463	344.1	309.8	523	388.7	350.0	583	433.2	390.1
344	255.6	230.2	404	300.2	270.3	464	344.8	310.5	524	389.4	350.6	584	434.0	390.8
345	256.4	230.9	405	301.0	271.0	465	345.6	311.2	525	390.1	351.3	585	434.7	391.4
346	257.1	231.5	406	301.7	271.7	466	346.3	311.8	526	390.9	352.0	586	435.5	392.1
347	257.9	232.2	407	302.5	272.3	467	347.0	312.5	527	391.6	352.6	587	436.2	392.8
348	258.6	232.9	408	303.2	273.0	468	347.8	313.2	528	392.4	353.3	588	437.0	393.4
349	259.4	233.5	409	303.9	273.7	469	348.5	313.8	529	393.1	354.0	589	437.7	394.1
350	260.1	234.2	410	304.7	274.3	470	349.3	314.5	530	393.9	354.6	590	438.4	394.8
351	260.8	234.9	411	305.4	275.0	471	350.0	315.2	531	394.6	355.3	591	439.2	395.4
352	261.6	235.5	412	306.2	275.7	472	350.8	315.8	532	395.3	356.0	592	440.0	396.1
353	262.3	236.2	413	306.9	276.4	473	351.5	316.5	533	396.1	356.6	593	440.7	396.8
354	263.1	236.9	414	307.7	277.0	474	352.3	317.2	534	396.8	357.3	594	441.4	397.5
355	263.8	237.5	415	308.4	277.7	475	353.0	317.8	535	397.6	358.0	595	442.2	398.1
356	264.6	238.2	416	309.1	278.4	476	353.7	318.5	536	398.3	358.6	596	442.9	398.8
357	265.3	238.9	417	309.9	279.0	477	354.5	319.2	537	399.1	359.3	597	443.7	399.5
358	266.0	239.6	418	310.6	279.7	478	355.2	319.9	538	399.8	360.0	598	444.4	400.1
359	266.8	240.2	419	311.4	280.4	479	356.0	320.5	539	400.6	360.6	599	445.2	400.8
360	267.5	240.9	420	312.1	281.0	480	356.7	321.2	540	401.3	361.3	600	445.9	401.5
48°														
3h 12m														
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TRAVERSE TABLE TO DEGREES														
45°												2° 52'		
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0'7	0'7	61	44'6	41'6	121	88'5	82'5	181	132'4	123'4	241	176'3	164'4
2	1'5	1'4	62	45'3	42'3	122	89'2	83'2	182	133'1	124'1	242	177'0	165'0
3	2'2	2'0	63	46'1	43'0	123	90'0	83'9	183	133'8	124'8	243	177'7	165'7
4	2'9	2'7	64	46'8	43'6	124	90'7	84'6	184	134'6	125'5	244	178'5	166'4
5	3'7	3'4	65	47'5	44'3	125	91'4	85'2	185	135'3	126'2	245	179'2	167'1
6	4'4	4'1	66	48'3	45'0	126	92'2	85'9	186	136'0	126'9	246	179'9	167'8
7	5'1	4'8	67	49'0	45'7	127	92'9	86'6	187	136'8	127'5	247	180'6	168'5
8	5'9	5'5	68	49'7	46'4	128	93'6	87'3	188	137'5	128'2	248	181'4	169'1
9	6'6	6'1	69	50'5	47'1	129	94'3	88'0	189	138'2	128'9	249	182'1	169'8
10	7'3	6'8	70	51'2	47'7	130	95'1	88'7	190	139'0	129'6	250	182'8	170'5
11	8'0	7'5	71	51'9	48'4	131	95'8	89'3	191	139'7	130'3	251	183'6	171'2
12	8'8	8'2	72	52'7	49'1	132	96'5	90'0	192	140'4	130'9	252	184'3	171'9
13	9'5	8'9	73	53'4	49'8	133	97'3	90'7	193	141'2	131'6	253	185'0	172'5
14	10'2	9'5	74	54'1	50'5	134	98'0	91'4	194	141'9	132'3	254	185'8	173'2
15	11'0	10'2	75	54'9	51'1	135	98'7	92'1	195	142'6	133'0	255	186'5	173'9
16	11'7	10'9	76	55'6	51'8	136	99'5	92'8	196	143'3	133'7	256	187'2	174'6
17	12'4	11'6	77	56'3	52'5	137	100'2	93'4	197	144'1	134'4	257	188'0	175'3
18	13'2	12'3	78	57'0	53'2	138	100'9	94'1	198	144'8	135'0	258	188'7	176'0
19	13'9	13'0	79	57'8	53'9	139	101'7	94'8	199	145'5	135'7	259	189'4	176'6
20	14'6	13'6	80	58'5	54'6	140	102'4	95'5	200	146'3	136'4	260	190'2	177'3
21	15'4	14'3	81	59'2	55'2	141	103'1	96'2	201	147'0	137'1	261	190'9	178'0
22	16'1	15'0	82	60'0	55'9	142	103'9	96'8	202	147'7	137'8	262	191'6	178'7
23	16'8	15'7	83	60'7	56'6	143	104'6	97'5	203	148'5	138'4	263	192'3	179'4
24	17'6	16'4	84	61'4	57'3	144	105'3	98'2	204	149'2	139'1	264	193'1	180'0
25	18'3	17'0	85	62'2	58'0	145	106'0	98'9	205	149'9	139'8	265	193'8	180'7
26	19'0	17'7	86	62'9	58'7	146	106'8	99'6	206	150'7	140'5	266	194'5	181'4
27	19'7	18'4	87	63'6	59'3	147	107'5	100'3	207	151'4	141'2	267	195'3	182'1
28	20'5	19'1	88	64'4	60'0	148	108'2	100'9	208	152'1	141'9	268	196'0	182'8
29	21'2	19'8	89	65'1	60'7	149	109'0	101'6	209	152'9	142'5	269	196'7	183'5
30	21'9	20'5	90	65'8	61'4	150	109'7	102'3	210	153'6	143'2	270	197'5	184'1
31	22'7	21'1	91	66'6	62'1	151	110'4	103'0	211	154'3	143'9	271	198'2	184'8
32	23'4	21'8	92	67'3	62'7	152	111'2	103'7	212	155'0	144'6	272	198'9	185'5
33	24'1	22'5	93	68'0	63'4	153	111'9	104'3	213	155'8	145'3	273	199'7	186'2
34	24'9	23'2	94	68'7	64'1	154	112'6	105'0	214	156'5	145'9	274	200'4	186'9
35	25'6	23'9	95	69'5	64'8	155	113'4	105'7	215	157'2	146'6	275	201'1	187'5
36	26'3	24'6	96	70'2	65'5	156	114'1	106'4	216	158'0	147'3	276	201'9	188'2
37	27'1	25'2	97	70'9	66'2	157	114'8	107'1	217	158'7	148'0	277	202'6	188'9
38	27'8	25'9	98	71'7	66'8	158	115'6	107'8	218	159'4	148'7	278	203'3	189'6
39	28'5	26'6	99	72'4	67'5	159	116'3	108'4	219	160'2	149'4	279	204'0	190'3
40	29'3	27'3	100	73'1	68'2	160	117'0	109'1	220	160'9	150'0	280	204'8	191'0
41	30'0	28'0	101	73'9	68'9	161	117'7	109'8	221	161'6	150'7	281	205'5	191'6
42	30'7	28'6	102	74'6	69'6	162	118'5	110'5	222	162'4	151'4	282	206'2	192'3
43	31'4	29'3	103	75'3	70'2	163	119'2	111'2	223	163'1	152'1	283	207'0	193'0
44	32'2	30'0	104	76'1	70'9	164	119'9	111'8	224	163'8	152'8	284	207'7	193'7
45	32'9	30'7	105	76'8	71'6	165	120'7	112'5	225	164'6	153'4	285	208'4	194'4
46	33'6	31'4	106	77'5	72'3	166	121'4	113'2	226	165'3	154'1	286	209'2	195'1
47	34'4	32'1	107	78'3	73'0	167	122'1	113'9	227	166'0	154'8	287	209'9	195'7
48	35'1	32'7	108	79'0	73'7	168	122'9	114'6	228	166'7	155'5	288	210'6	196'4
49	35'8	33'4	109	79'7	74'3	169	123'6	115'3	229	167'5	156'2	289	211'4	197'1
50	36'6	34'1	110	80'4	75'0	170	124'3	115'9	230	168'2	156'9	290	212'1	197'8
51	37'3	34'8	111	81'2	75'7	171	125'1	116'6	231	168'9	157'5	291	212'8	198'5
52	38'0	35'5	112	81'9	76'4	172	125'8	117'3	232	169'7	158'2	292	213'6	199'1
53	38'8	36'1	113	82'6	77'1	173	126'5	118'0	233	170'4	158'9	293	214'3	199'8
54	39'5	36'8	114	83'4	77'7	174	127'3	118'7	234	171'1	159'6	294	215'0	200'5
55	40'2	37'5	115	84'1	78'4	175	128'0	119'3	235	171'9	160'3	295	215'7	201'2
56	41'0	38'2	116	84'8	79'1	176	128'7	120'0	236	172'6	161'0	296	216'5	201'9
57	41'7	38'9	117	85'6	79'8	177	129'4	120'7	237	173'3	161'6	297	217'2	202'6
58	42'4	39'6	118	86'3	80'5	178	130'2	121'4	238	174'1	162'3	298	217'9	203'2
59	43'1	40'2	119	87'0	81'2	179	130'9	122'1	239	174'8	163'0	299	218'7	203'9
60	43'9	40'9	120	87'8	81'8	180	131'6	122'8	240	175'5	163'7	300	219'4	204'6
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

517

TRAVERSE TABLE TO DEGREES

48°									2 ^h 52 ^m					
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	220.1	205.3	361	264.0	246.2	421	307.9	287.1	481	351.8	328.1	541	395.7	369.0
302	220.9	206.0	362	264.8	246.9	422	308.6	287.8	482	352.5	328.7	542	396.4	369.7
303	221.6	206.7	363	265.5	247.6	423	309.4	288.5	483	353.2	329.4	543	397.1	370.3
304	222.3	207.3	364	266.2	248.3	424	310.1	289.2	484	354.0	330.1	544	397.9	371.0
305	223.1	208.0	365	267.0	249.0	425	310.8	289.9	485	354.7	330.8	545	398.6	371.7
306	223.8	208.7	366	267.7	249.6	426	311.6	290.5	486	355.4	331.4	546	399.3	372.4
307	224.5	209.4	367	268.4	250.3	427	312.3	291.2	487	356.2	332.1	547	400.1	373.1
308	225.3	210.1	368	269.1	251.0	428	313.0	291.9	488	356.9	332.8	548	400.8	373.7
309	226.0	210.7	369	269.9	251.7	429	313.8	292.6	489	357.7	333.5	549	401.5	374.4
310	226.7	211.4	370	270.6	252.3	430	314.5	293.3	490	358.4	334.2	550	402.2	375.1
311	227.5	212.1	371	271.3	253.0	431	315.2	293.9	491	359.1	334.9	551	403.0	375.8
312	228.2	212.8	372	272.1	253.7	432	316.0	294.6	492	359.8	335.5	552	403.7	376.5
313	228.9	213.5	373	272.8	254.4	433	316.7	295.3	493	360.6	336.2	553	404.4	377.1
314	229.7	214.2	374	273.5	255.1	434	317.4	296.0	494	361.3	336.9	554	405.2	377.8
315	230.4	214.8	375	274.3	255.8	435	318.1	296.7	495	362.0	337.6	555	405.9	378.5
316	231.1	215.5	376	275.0	256.4	436	318.9	297.4	496	362.8	338.3	556	406.6	379.2
317	231.8	216.2	377	275.7	257.1	437	319.6	298.0	497	363.5	338.9	557	407.4	379.9
318	232.6	216.9	378	276.5	257.8	438	320.3	298.7	498	364.2	339.6	558	408.1	380.6
319	233.3	217.6	379	277.2	258.5	439	321.1	299.4	499	364.9	340.3	559	408.8	381.2
320	234.0	218.2	380	277.9	259.2	440	321.8	300.1	500	365.7	341.0	560	409.6	381.9
321	234.8	218.9	381	278.7	259.8	441	322.5	300.8	501	366.4	341.7	561	410.3	382.6
322	235.5	219.6	382	279.4	260.5	442	323.3	301.4	502	367.1	342.4	562	411.0	383.3
323	236.2	220.3	383	280.1	261.2	443	324.0	302.1	503	367.8	343.0	563	411.8	384.0
324	237.0	221.0	384	280.8	261.9	444	324.7	302.8	504	368.6	343.7	564	412.5	384.6
325	237.7	221.7	385	281.6	262.6	445	325.5	303.5	505	369.3	344.4	565	413.2	385.3
326	238.4	222.3	386	282.3	263.3	446	326.2	304.2	506	370.0	345.1	566	414.0	386.0
327	239.2	223.0	387	283.0	263.9	447	326.9	304.9	507	370.8	345.8	567	414.7	386.7
328	239.9	223.7	388	283.7	264.6	448	327.7	305.5	508	371.5	346.5	568	415.4	387.4
329	240.6	224.4	389	284.5	265.3	449	328.4	306.2	509	372.3	347.1	569	416.2	388.1
330	241.4	225.1	390	285.2	266.0	450	329.1	306.9	510	373.0	347.8	570	416.9	388.7
331	242.1	225.7	391	286.0	266.7	451	329.9	307.6	511	373.8	348.5	571	417.6	389.4
332	242.8	226.4	392	286.7	267.3	452	330.6	308.3	512	374.5	349.2	572	418.3	390.1
333	243.5	227.1	393	287.4	268.0	453	331.3	309.0	513	375.2	349.9	573	419.1	390.8
334	244.3	227.8	394	288.2	268.7	454	332.1	309.6	514	376.0	350.5	574	419.8	391.5
335	245.0	228.5	395	288.9	269.4	455	332.8	310.3	515	376.6	351.2	575	420.5	392.2
336	245.7	229.2	396	289.6	270.1	456	333.5	311.0	516	377.4	351.9	576	421.3	392.8
337	246.5	229.8	397	290.4	270.8	457	334.3	311.7	517	378.2	352.6	577	422.0	393.5
338	247.2	230.5	398	291.1	271.4	458	335.0	312.4	518	378.9	353.3	578	422.7	394.2
339	247.9	231.2	399	291.8	272.1	459	335.7	313.0	519	379.6	354.0	579	423.5	394.9
340	248.7	231.9	400	292.6	272.8	460	336.5	313.7	520	380.3	354.6	580	424.2	395.6
341	249.4	232.6	401	293.3	273.5	461	337.2	314.4	521	381.1	355.3	581	424.9	396.2
342	250.1	233.2	402	294.0	274.2	462	337.9	315.1	522	381.8	356.0	582	425.7	396.9
343	250.9	233.9	403	294.7	274.9	463	338.7	315.8	523	382.6	356.7	583	426.4	397.6
344	251.6	234.6	404	295.5	275.5	464	339.4	316.5	524	383.3	357.4	584	427.1	398.3
345	252.3	235.3	405	296.2	276.2	465	340.1	317.1	525	384.0	358.1	585	427.9	399.0
346	253.1	236.0	406	296.9	276.9	466	340.8	317.8	526	384.7	358.8	586	428.6	399.6
347	253.8	236.7	407	297.7	277.6	467	341.6	318.5	527	385.5	359.4	587	429.3	400.3
348	254.5	237.3	408	298.4	278.3	468	342.3	319.2	528	386.2	360.1	588	430.1	401.0
349	255.3	238.0	409	299.1	278.9	469	343.0	319.9	529	386.9	360.8	589	430.8	401.7
350	256.0	238.7	410	299.9	279.6	470	343.7	320.5	530	387.6	361.5	590	431.5	402.4
351	256.7	239.4	411	300.6	280.3	471	344.5	321.2	531	388.4	362.1	591	432.3	403.1
352	257.4	240.1	412	301.3	281.0	472	345.2	321.9	532	389.1	362.8	592	433.0	403.7
353	258.2	240.8	413	302.1	281.7	473	345.9	322.6	533	389.9	363.5	593	433.7	404.4
354	258.9	241.4	414	302.8	282.4	474	346.7	323.3	534	390.6	364.2	594	434.5	405.1
355	259.6	242.1	415	303.5	283.0	475	347.4	324.0	535	391.3	364.9	595	435.2	405.8
356	260.4	242.8	416	304.3	283.7	476	348.1	324.6	536	392.0	365.5	596	435.9	406.5
357	261.1	243.5	417	305.0	284.4	477	348.9	325.3	537	392.8	366.2	597	436.7	407.2
358	261.8	244.2	418	305.7	285.1	478	349.6	326.0	538	393.5	366.9	598	437.4	407.8
359	262.6	244.8	419	306.4	285.8	479	350.3	326.7	539	394.2	367.6	599	438.1	408.5
360	263.3	245.5	420	307.2	286.4	480	351.1	327.4	540	394.9	368.3	600	438.8	409.2
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

47°

8^h 8^m

TRAVERSE TABLE TO DEGREES

44°												2° 56'		
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
1	0.7	0.7	61	43.9	42.4	121	87.0	84.1	181	130.2	125.7	241	173.4	167.4
2	1.4	1.4	62	44.6	43.1	122	87.8	84.7	182	130.9	126.4	242	174.1	168.1
3	2.2	2.1	63	45.3	43.8	123	88.5	85.4	183	131.6	127.1	243	174.8	168.8
4	2.9	2.8	64	46.0	44.5	124	89.2	86.1	184	132.4	127.8	244	175.5	169.5
5	3.6	3.5	65	46.8	45.2	125	89.9	86.8	185	133.1	128.5	245	176.2	170.2
6	4.3	4.2	66	47.5	45.8	126	90.6	87.5	186	133.8	129.2	246	177.0	170.9
7	5.0	4.9	67	48.2	46.5	127	91.4	88.2	187	134.5	129.9	247	177.7	171.6
8	5.8	5.6	68	48.9	47.2	128	92.1	88.9	188	135.2	130.6	248	178.4	172.3
9	6.5	6.3	69	49.6	47.9	129	92.8	89.6	189	136.0	131.3	249	179.1	173.0
10	7.2	6.9	70	50.4	48.6	130	93.5	90.3	190	136.7	132.0	250	179.8	173.7
11	7.9	7.6	71	51.1	49.3	131	94.2	91.0	191	137.4	132.7	251	180.6	174.4
12	8.6	8.3	72	51.8	50.0	132	95.0	91.7	192	138.1	133.4	252	181.3	175.1
13	9.4	9.0	73	52.5	50.7	133	95.7	92.4	193	138.8	134.1	253	182.0	175.7
14	10.1	9.7	74	53.2	51.4	134	96.4	93.1	194	139.6	134.8	254	182.7	176.4
15	10.8	10.4	75	54.0	52.1	135	97.1	93.8	195	140.3	135.5	255	183.4	177.1
16	11.5	11.1	76	54.7	52.8	136	97.8	94.5	196	141.0	136.2	256	184.2	177.8
17	12.2	11.8	77	55.4	53.5	137	98.5	95.2	197	141.7	136.8	257	184.9	178.5
18	12.9	12.5	78	56.1	54.2	138	99.3	95.9	198	142.4	137.5	258	185.6	179.2
19	13.7	13.2	79	56.8	54.9	139	100.0	96.6	199	143.1	138.2	259	186.3	179.9
20	14.4	13.9	80	57.5	55.6	140	100.7	97.3	200	143.9	138.9	260	187.0	180.6
21	15.1	14.6	81	58.3	56.3	141	101.4	97.9	201	144.6	139.6	261	187.7	181.3
22	15.8	15.3	82	59.0	57.0	142	102.1	98.6	202	145.3	140.3	262	188.5	182.0
23	16.5	16.0	83	59.7	57.7	143	102.9	99.3	203	146.0	141.0	263	189.2	182.7
24	17.3	16.7	84	60.4	58.4	144	103.6	100.0	204	146.7	141.7	264	189.9	183.4
25	18.0	17.4	85	61.1	59.0	145	104.3	100.7	205	147.5	142.4	265	190.6	184.1
26	18.7	18.1	86	61.9	59.7	146	105.0	101.4	206	148.2	143.1	266	191.3	184.8
27	19.4	18.8	87	62.6	60.4	147	105.7	102.1	207	148.9	143.8	267	192.1	185.5
28	20.1	19.5	88	63.3	61.1	148	106.5	102.8	208	149.6	144.5	268	192.8	186.2
29	20.9	20.1	89	64.0	61.8	149	107.2	103.5	209	150.3	145.2	269	193.5	186.9
30	21.6	20.8	90	64.7	62.5	150	107.9	104.2	210	151.1	145.9	270	194.2	187.6
31	22.3	21.5	91	65.5	63.2	151	108.6	104.9	211	151.8	146.6	271	194.9	188.3
32	23.0	22.2	92	66.2	63.9	152	109.3	105.6	212	152.5	147.3	272	195.7	188.9
33	23.7	22.9	93	66.9	64.6	153	110.1	106.3	213	153.2	148.0	273	196.4	189.6
34	24.5	23.6	94	67.6	65.3	154	110.8	107.0	214	153.9	148.7	274	197.1	190.3
35	25.2	24.3	95	68.3	66.0	155	111.5	107.7	215	154.7	149.4	275	197.8	191.0
36	25.9	25.0	96	69.1	66.7	156	112.2	108.4	216	155.4	150.0	276	198.5	191.7
37	26.6	25.7	97	69.8	67.4	157	112.9	109.1	217	156.1	150.7	277	199.3	192.4
38	27.3	26.4	98	70.5	68.1	158	113.7	109.8	218	156.8	151.4	278	200.0	193.1
39	28.1	27.1	99	71.2	68.8	159	114.4	110.5	219	157.5	152.1	279	200.7	193.8
40	28.8	27.8	100	71.9	69.5	160	115.1	111.2	220	158.3	152.8	280	201.4	194.5
41	29.5	28.5	101	72.7	70.2	161	115.8	111.8	221	159.0	153.5	281	202.1	195.2
42	30.2	29.2	102	73.4	70.9	162	116.5	112.5	222	159.7	154.2	282	202.9	195.9
43	30.9	29.9	103	74.1	71.5	163	117.3	113.2	223	160.4	154.9	283	203.6	196.6
44	31.7	30.6	104	74.8	72.2	164	118.0	113.9	224	161.1	155.6	284	204.3	197.3
45	32.4	31.3	105	75.5	72.9	165	118.7	114.6	225	161.9	156.3	285	205.0	198.0
46	33.1	32.0	106	76.3	73.6	166	119.4	115.3	226	162.6	157.0	286	205.7	198.7
47	33.8	32.6	107	77.0	74.3	167	120.1	116.0	227	163.3	157.7	287	206.5	199.4
48	34.5	33.3	108	77.7	75.0	168	120.8	116.7	228	164.0	158.4	288	207.2	200.1
49	35.2	34.0	109	78.4	75.7	169	121.6	117.4	229	164.7	159.1	289	207.9	200.8
50	36.0	34.7	110	79.1	76.4	170	122.3	118.1	230	165.4	159.8	290	208.6	201.5
51	36.7	35.4	111	79.8	77.1	171	123.0	118.8	231	166.2	160.5	291	209.3	202.1
52	37.4	36.1	112	80.6	77.8	172	123.7	119.5	232	166.9	161.2	292	210.0	202.8
53	38.1	36.8	113	81.3	78.5	173	124.4	120.2	233	167.6	161.9	293	210.8	203.5
54	38.8	37.5	114	82.0	79.2	174	125.2	120.9	234	168.3	162.6	294	211.5	204.2
55	39.6	38.2	115	82.7	79.9	175	125.9	121.6	235	169.0	163.3	295	212.2	204.9
56	40.3	38.9	116	83.4	80.6	176	126.6	122.3	236	169.8	163.9	296	212.9	205.6
57	41.0	39.6	117	84.2	81.3	177	127.3	123.0	237	170.5	164.6	297	213.6	206.3
58	41.7	40.3	118	84.9	82.0	178	128.0	123.6	238	171.2	165.3	298	214.4	207.0
59	42.4	41.0	119	85.6	82.7	179	128.8	124.3	239	171.9	166.0	299	215.1	207.7
60	43.2	41.7	120	86.3	83.4	180	129.5	125.0	240	172.6	166.7	300	215.8	208.4
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TRAVERSE TABLE TO DEGREES

44°												2h 56m		
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	216.5	209.1	361	259.7	250.8	421	302.8	292.5	481	346.0	334.1	541	389.2	375.8
302	217.2	209.8	362	260.4	251.5	422	303.6	293.2	482	346.7	334.8	542	389.9	376.5
303	218.0	210.5	363	261.1	252.2	423	304.3	293.8	483	347.4	335.5	543	390.6	377.2
304	218.7	211.2	364	261.8	252.9	424	305.0	294.5	484	348.2	336.2	544	391.3	377.9
305	219.4	211.9	365	262.6	253.6	425	305.7	295.2	485	348.9	336.9	545	392.0	378.6
306	220.1	212.6	366	263.3	254.3	426	306.4	295.9	486	349.6	337.6	546	392.8	379.3
307	220.8	213.3	367	264.0	254.9	427	307.2	256.6	487	350.3	338.3	547	393.5	380.0
308	221.6	214.0	368	264.7	255.6	428	307.9	297.3	488	351.0	339.0	548	394.2	380.7
309	222.3	214.7	369	265.4	256.3	429	308.6	298.0	489	351.7	339.7	549	394.9	381.4
310	223.0	215.4	370	266.2	257.0	430	309.3	298.7	490	352.5	340.4	550	395.6	382.1
311	223.7	216.0	371	266.9	257.7	431	310.0	299.4	491	353.2	341.1	551	396.4	382.8
312	224.4	216.7	372	267.6	258.4	432	310.8	300.1	492	353.9	341.8	552	397.1	383.4
313	225.2	217.4	373	268.3	259.1	433	311.5	300.8	493	354.6	342.5	553	397.8	384.1
314	225.9	218.1	374	269.0	259.8	434	312.2	301.5	494	355.3	343.2	554	398.5	384.8
315	226.6	218.8	375	269.8	260.5	435	312.9	302.2	495	356.0	343.9	555	399.2	385.5
316	227.3	219.5	376	270.5	261.2	436	313.6	302.9	496	356.8	344.6	556	400.0	386.2
317	228.0	220.2	377	271.2	261.9	437	314.4	303.6	497	357.5	345.2	557	400.7	386.9
318	228.8	220.9	378	271.9	262.6	438	315.1	304.3	498	358.2	345.9	558	401.4	387.6
319	229.5	221.6	379	272.6	263.3	439	315.8	305.0	499	358.9	346.6	559	402.1	388.3
320	230.2	222.3	380	273.4	264.0	440	316.5	305.7	500	359.7	347.3	560	402.8	389.0
321	230.9	223.0	381	274.1	264.7	441	317.2	306.4	501	360.4	348.0	561	403.6	389.7
322	231.6	223.7	382	274.8	265.4	442	318.0	307.0	502	361.1	348.7	562	404.3	390.4
323	232.3	224.4	383	275.5	266.1	443	318.7	307.7	503	361.8	349.4	563	405.0	391.1
324	233.1	225.1	384	276.2	266.8	444	319.4	308.4	504	362.5	350.1	564	405.7	391.8
325	233.8	225.8	385	276.9	267.5	445	320.1	309.1	505	363.3	350.8	565	406.4	392.5
326	234.5	226.5	386	277.7	268.1	446	320.8	309.8	506	364.0	351.5	566	407.2	393.2
327	235.2	227.2	387	278.4	268.8	447	321.5	310.5	507	364.7	352.2	567	407.9	393.9
328	235.9	227.9	388	279.1	269.5	448	322.3	311.2	508	365.4	352.9	568	408.6	394.6
329	236.7	228.6	389	279.8	270.2	449	323.0	311.9	509	366.1	353.6	569	409.3	395.3
330	237.4	229.2	390	280.5	270.9	450	323.7	312.6	510	366.9	354.3	570	410.0	396.0
331	238.1	229.9	391	281.3	271.6	451	324.4	313.3	511	367.6	355.0	571	410.7	396.7
332	238.8	230.6	392	282.0	272.3	452	325.2	314.0	512	368.3	355.7	572	411.5	397.3
333	239.5	231.3	393	282.7	273.0	453	325.9	314.7	513	369.0	356.4	573	412.2	398.0
334	240.3	232.0	394	283.4	273.7	454	326.6	315.4	514	369.7	357.1	574	412.9	398.7
335	241.0	232.7	395	284.1	274.4	455	327.3	316.1	515	370.5	357.8	575	413.6	399.4
336	241.7	233.4	396	284.9	275.1	456	328.0	316.8	516	371.2	358.4	576	414.3	400.1
337	242.4	234.1	397	285.6	275.8	457	328.7	317.5	517	371.9	359.1	577	415.1	400.8
338	243.1	234.8	398	286.3	276.5	458	329.5	318.2	518	372.6	359.8	578	415.8	401.5
339	243.9	235.5	399	287.0	277.2	459	330.2	318.9	519	373.3	360.5	579	416.5	402.2
340	244.6	236.2	400	287.7	277.9	460	330.9	319.6	520	374.1	361.2	580	417.2	402.9
341	245.3	236.9	401	288.5	278.6	461	331.6	320.2	521	374.8	361.9	581	417.9	403.6
342	246.0	237.6	402	289.2	279.3	462	332.3	320.9	522	375.5	362.6	582	418.7	404.3
343	246.7	238.3	403	289.9	280.0	463	333.1	321.6	523	376.2	363.3	583	419.4	405.0
344	247.5	239.0	404	290.6	280.7	464	333.8	322.3	524	376.9	364.0	584	420.1	405.7
345	248.2	239.7	405	291.3	281.3	465	334.5	323.0	525	377.7	364.7	585	420.8	406.4
346	248.9	240.4	406	292.1	282.0	466	335.2	323.7	526	378.4	365.4	586	421.5	407.1
347	249.6	241.1	407	292.8	282.7	467	335.9	324.4	527	379.1	366.1	587	422.3	407.8
348	250.3	241.7	408	293.5	283.4	468	336.7	325.1	528	379.8	366.8	588	423.0	408.5
349	251.1	242.4	409	294.2	284.1	469	337.4	325.8	529	380.5	367.5	589	423.7	409.1
350	251.8	243.1	410	294.9	284.8	470	338.1	326.5	530	381.2	368.2	590	424.4	409.9
351	252.5	243.8	411	295.7	285.5	471	338.8	327.2	531	382.0	368.9	591	425.1	410.5
352	253.2	244.5	412	296.4	286.2	472	339.5	327.9	532	382.7	369.6	592	425.9	411.2
353	253.9	245.2	413	297.1	286.9	473	340.3	328.6	533	383.4	370.3	593	426.6	411.9
354	254.6	245.9	414	297.8	287.6	474	341.0	329.3	534	384.1	371.0	594	427.3	412.6
355	255.4	246.6	415	298.5	288.3	475	341.7	330.0	535	384.8	371.7	595	428.0	413.3
356	256.1	247.3	416	299.2	289.0	476	342.4	330.7	536	385.6	372.4	596	428.7	414.0
357	256.8	248.0	417	300.0	289.7	477	343.1	331.4	537	386.3	373.1	597	429.5	414.7
358	257.5	248.7	418	300.7	290.4	478	343.8	332.1	538	387.0	373.8	598	430.2	415.4
359	258.2	249.4	419	301.4	291.1	479	344.6	332.7	539	387.7	374.5	599	430.9	416.1
360	259.0	250.1	420	302.1	291.8	480	345.3	333.4	540	388.4	375.1	600	431.6	416.8
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.

TABLE 1

521

TRAVERSE TABLE TO DEGREES

45°												8h 0 ^m		
Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.	Dist.	D. Lat.	Dep.
301	212.8	212.8	361	255.3	255.3	421	297.7	297.7	481	340.1	340.1	541	382.5	382.5
302	213.5	213.5	362	256.0	256.0	422	298.4	298.4	482	340.8	340.8	542	383.2	383.2
303	214.3	214.3	363	256.7	256.7	423	299.1	299.1	483	341.5	341.5	543	383.9	383.9
304	215.0	215.0	364	257.4	257.4	424	299.8	299.8	484	342.2	342.2	544	384.7	384.7
305	215.7	215.7	365	258.1	258.1	425	300.5	300.5	485	342.9	342.9	545	385.4	385.4
306	216.4	216.4	366	258.8	258.8	426	301.2	301.2	486	343.6	343.6	546	386.1	386.1
307	217.1	217.1	367	259.5	259.5	427	301.9	301.9	487	344.3	344.3	547	386.8	386.8
308	217.8	217.8	368	260.2	260.2	428	302.6	302.6	488	345.1	345.1	548	387.5	387.5
309	218.5	218.5	369	260.9	260.9	429	303.4	303.4	489	345.8	345.8	549	388.2	388.2
310	219.2	219.2	370	261.6	261.6	430	304.1	304.1	490	346.5	346.5	550	388.9	388.9
311	219.9	219.9	371	262.3	262.3	431	304.8	304.8	491	347.2	347.2	551	389.6	389.6
312	220.6	220.6	372	263.0	263.0	432	305.5	305.5	492	347.9	347.9	552	390.3	390.3
313	221.3	221.3	373	263.8	263.8	433	306.2	306.2	493	348.6	348.6	553	391.0	391.0
314	222.0	222.0	374	264.5	264.5	434	306.9	306.9	494	349.3	349.3	554	391.7	391.7
315	222.7	222.7	375	265.2	265.2	435	307.6	307.6	495	350.0	350.0	555	392.4	392.4
316	223.4	223.4	376	265.9	265.9	436	308.3	308.3	496	350.7	350.7	556	393.1	393.1
317	224.2	224.2	377	266.6	266.6	437	309.0	309.0	497	351.4	351.4	557	393.9	393.9
318	224.9	224.9	378	267.3	267.3	438	309.7	309.7	498	352.1	352.1	558	394.6	394.6
319	225.6	225.6	379	268.0	268.0	439	310.4	310.4	499	352.8	352.8	559	395.3	395.3
320	226.3	226.3	380	268.7	268.7	440	311.1	311.1	500	353.5	353.5	560	396.0	396.0
321	227.0	227.0	381	269.4	269.4	441	311.8	311.8	501	354.3	354.3	561	396.7	396.7
322	227.7	227.7	382	270.1	270.1	442	312.5	312.5	502	355.0	355.0	562	397.4	397.4
323	228.4	228.4	383	270.8	270.8	443	313.3	313.3	503	355.7	355.7	563	398.1	398.1
324	229.1	229.1	384	271.5	271.5	444	314.0	314.0	504	356.4	356.4	564	398.8	398.8
325	229.8	229.8	385	272.2	272.2	445	314.7	314.7	505	357.1	357.1	565	399.5	399.5
326	230.5	230.5	386	272.9	272.9	446	315.4	315.4	506	357.8	357.8	566	400.2	400.2
327	231.2	231.2	387	273.7	273.7	447	316.1	316.1	507	358.5	358.5	567	400.9	400.9
328	231.9	231.9	388	274.4	274.4	448	316.8	316.8	508	359.2	359.2	568	401.6	401.6
329	232.6	232.6	389	275.1	275.1	449	317.5	317.5	509	359.9	359.9	569	402.3	402.3
330	233.3	233.3	390	275.8	275.8	450	318.2	318.2	510	360.6	360.6	570	403.0	403.0
331	234.1	234.1	391	276.5	276.5	451	318.9	318.9	511	361.3	361.3	571	403.8	403.8
332	234.8	234.8	392	277.2	277.2	452	319.6	319.6	512	362.0	362.0	572	404.5	404.5
333	235.5	235.5	393	277.9	277.9	453	320.3	320.3	513	362.7	362.7	573	405.2	405.2
334	236.2	236.2	394	278.6	278.6	454	321.0	321.0	514	363.5	363.5	574	405.9	405.9
335	236.9	236.9	395	279.3	279.3	455	321.7	321.7	515	364.2	364.2	575	406.6	406.6
336	237.6	237.6	396	280.0	280.0	456	322.4	322.4	516	364.9	364.9	576	407.3	407.3
337	238.3	238.3	397	280.7	280.7	457	323.2	323.2	517	365.6	365.6	577	408.0	408.0
338	239.0	239.0	398	281.4	281.4	458	323.9	323.9	518	366.3	366.3	578	408.7	408.7
339	239.7	239.7	399	282.1	282.1	459	324.6	324.6	519	367.0	367.0	579	409.4	409.4
340	240.4	240.4	400	282.8	282.8	460	325.3	325.3	520	367.7	367.7	580	410.1	410.1
341	241.1	241.1	401	283.6	283.6	461	326.0	326.0	521	368.4	368.4	581	410.8	410.8
342	241.8	241.8	402	284.3	284.3	462	326.7	326.7	522	369.1	369.1	582	411.5	411.5
343	242.5	242.5	403	285.0	285.0	463	327.4	327.4	523	369.8	369.8	583	412.2	412.2
344	243.2	243.2	404	285.7	285.7	464	328.1	328.1	524	370.5	370.5	584	412.9	412.9
345	244.0	244.0	405	286.4	286.4	465	328.8	328.8	525	371.2	371.2	585	413.7	413.7
346	244.7	244.7	406	287.1	287.1	466	329.5	329.5	526	371.9	371.9	586	414.4	414.4
347	245.4	245.4	407	287.8	287.8	467	330.2	330.2	527	372.6	372.6	587	415.1	415.1
348	246.1	246.1	408	288.5	288.5	468	330.9	330.9	528	373.3	373.3	588	415.8	415.8
349	246.8	246.8	409	289.2	289.2	469	331.6	331.6	529	374.1	374.1	589	416.5	416.5
350	247.5	247.5	410	289.9	289.9	470	332.3	332.3	530	374.8	374.8	590	417.2	417.2
351	248.2	248.2	411	290.6	290.6	471	333.1	333.1	531	375.5	375.5	591	417.9	417.9
352	248.9	248.9	412	291.3	291.3	472	333.8	333.8	532	376.2	376.2	592	418.6	418.6
353	249.6	249.6	413	292.0	292.0	473	334.5	334.5	533	376.9	376.9	593	419.3	419.3
354	250.3	250.3	414	292.7	292.7	474	335.2	335.2	534	377.6	377.6	594	420.0	420.0
355	251.0	251.0	415	293.5	293.5	475	335.9	335.9	535	378.3	378.3	595	420.7	420.7
356	251.7	251.7	416	294.2	294.2	476	336.6	336.6	536	379.0	379.0	596	421.4	421.4
357	252.4	252.4	417	294.9	294.9	477	337.3	337.3	537	379.7	379.7	597	422.1	422.1
358	253.1	253.1	418	295.6	295.6	478	338.0	338.0	538	380.4	380.4	598	422.8	422.8
359	253.9	253.9	419	296.3	296.3	479	338.7	338.7	539	381.1	381.1	599	423.6	423.6
360	254.6	254.6	420	297.0	297.0	480	339.4	339.4	540	381.8	381.8	600	424.3	424.3
Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.	Dist.	Dep.	D. Lat.
45°												8h 0 ^m		

DEPARTURE AND CORRESPONDING DIFFERENCE OF LONGITUDE														
Lat.	DEPARTURE										PARTS			
	1	2	3	4	5	6	7	8	9	10	D ^{to} 1°	15'	30'	45'
0°	1'00	2'00	3'00	4'00	5'00	6'00	7'00	8'00	9'00	10'00	0'04	0'01	0'02	0'03
1	1'00	2'00	3'01	4'01	5'01	6'01	7'02	8'01	9'02	10'02	0'08	0'02	0'04	0'06
2	1'01	2'01	3'02	4'02	5'03	6'03	7'04	8'04	9'05	10'06	0'12	0'03	0'06	0'09
3	1'01	2'02	3'03	4'04	5'05	6'06	7'07	8'08	9'09	10'10	0'14	0'03	0'07	0'10
4	1'02	2'03	3'05	4'06	5'08	6'09	7'11	8'11	9'14	10'15	0'16	0'04	0'08	0'12
5	1'02	2'04	3'07	4'09	5'11	6'13	7'16	8'18	9'20	10'22	0'18	0'04	0'08	0'13
6	1'03	2'06	3'09	4'12	5'15	6'18	7'21	8'24	9'28	10'31	0'20	0'05	0'10	0'15
7	1'04	2'07	3'11	4'14	5'18	6'21	7'25	8'28	9'32	10'35	0'22	0'05	0'11	0'16
8	1'04	2'08	3'12	4'16	5'20	6'24	7'28	8'32	9'36	10'40	0'24	0'06	0'12	0'18
9	1'05	2'09	3'14	4'18	5'23	6'27	7'32	8'37	9'41	10'46	0'26	0'06	0'13	0'19
10	1'05	2'10	3'15	4'21	5'26	6'31	7'36	8'41	9'46	10'51	0'28	0'07	0'14	0'21
11	1'06	2'12	3'17	4'23	5'29	6'35	7'40	8'46	9'52	10'58	0'30	0'07	0'15	0'22
12	1'06	2'13	3'19	4'26	5'32	6'39	7'45	8'51	9'58	10'64	0'32	0'08	0'16	0'24
13	1'07	2'14	3'21	4'28	5'36	6'43	7'50	8'57	9'64	10'71	0'34	0'08	0'17	0'25
14	1'08	2'16	3'24	4'31	5'39	6'47	7'55	8'63	9'71	10'79	0'36	0'09	0'18	0'27
15	1'09	2'17	3'26	4'35	5'43	6'52	7'60	8'69	9'78	10'86	0'38	0'09	0'19	0'28
16	1'09	2'19	3'28	4'38	5'47	6'57	7'66	8'76	9'85	10'95	0'40	0'10	0'20	0'30
17	1'10	2'21	3'31	4'41	5'52	6'62	7'72	8'83	9'93	11'03	0'42	0'10	0'21	0'31
18	1'11	2'23	3'34	4'45	5'56	6'68	7'79	8'90	10'01	11'13	0'44	0'11	0'22	0'33
19	1'12	2'24	3'37	4'49	5'61	6'73	7'86	8'98	10'10	11'22	0'46	0'11	0'23	0'34
20	1'13	2'27	3'40	4'53	5'66	6'80	7'93	9'06	10'19	11'33	0'48	0'12	0'24	0'36
21	1'14	2'29	3'43	4'57	5'72	6'86	8'00	9'15	10'29	11'43	0'50	0'12	0'25	0'37
22	1'15	2'31	3'46	4'62	5'77	6'93	8'08	9'24	10'39	11'55	0'52	0'13	0'26	0'39
23	1'17	2'33	3'50	4'67	5'83	7'00	8'17	9'33	10'50	11'67	0'54	0'13	0'27	0'40
24	1'18	2'36	3'54	4'72	5'90	7'08	8'25	9'43	10'61	11'79	0'56	0'13	0'28	0'41
25	1'19	2'38	3'58	4'77	5'96	7'15	8'35	9'54	10'73	11'92	0'58	0'14	0'29	0'43
26	1'21	2'41	3'62	4'82	6'03	7'24	8'44	9'65	10'86	12'06	0'60	0'15	0'30	0'45
27	1'22	2'44	3'66	4'88	6'10	7'32	8'54	9'76	10'99	12'21	0'62	0'15	0'31	0'46
28	1'24	2'47	3'71	4'94	6'18	7'42	8'65	9'89	11'12	12'36	0'64	0'16	0'32	0'48
29	1'25	2'50	3'76	5'01	6'26	7'51	8'76	10'02	11'27	12'52	0'66	0'16	0'33	0'49
30	1'27	2'54	3'81	5'08	6'35	7'61	8'88	10'15	11'42	12'69	0'68	0'17	0'34	0'51
31	1'29	2'57	3'86	5'15	6'43	7'72	9'01	10'29	11'58	12'87	0'70	0'17	0'35	0'52
32	1'31	2'61	3'92	5'22	6'53	7'83	9'14	10'44	11'75	13'05	0'72	0'18	0'36	0'54
33	1'33	2'65	3'98	5'30	6'63	7'95	9'28	10'60	11'93	13'25	0'74	0'18	0'37	0'55
34	1'35	2'69	4'04	5'38	6'73	8'07	9'42	10'77	12'11	13'46	0'76	0'19	0'38	0'57
35	1'37	2'73	4'10	5'47	6'84	8'20	9'57	10'94	12'31	13'67	0'78	0'19	0'39	0'58
36	1'39	2'78	4'17	5'56	6'95	8'34	9'73	11'12	12'51	13'90	0'80	0'20	0'40	0'60
37	1'41	2'83	4'24	5'66	7'07	8'49	9'90	11'31	12'73	14'14	0'82	0'20	0'41	0'61
38	1'44	2'88	4'32	5'76	7'20	8'64	10'08	11'52	12'96	14'40	0'84	0'21	0'42	0'63
39	1'47	2'93	4'40	5'87	7'33	8'80	10'26	11'73	13'20	14'66	0'86	0'21	0'43	0'64
40	1'49	2'99	4'48	5'98	7'47	8'97	10'46	11'96	13'45	14'94	0'88	0'22	0'44	0'66
41	1'52	3'05	4'57	6'10	7'62	9'15	10'67	12'19	13'72	15'24	0'90	0'22	0'45	0'67
42	1'56	3'11	4'67	6'22	7'78	9'33	10'89	12'45	14'00	15'56	0'92	0'23	0'46	0'69
43	1'59	3'18	4'77	6'36	7'95	9'53	11'12	12'71	14'30	15'89	0'94	0'23	0'47	0'70
44	1'62	3'25	4'87	6'50	8'12	9'75	11'37	12'99	14'62	16'24	0'96	0'24	0'48	0'72
45	1'66	3'32	4'98	6'65	8'31	9'97	11'63	13'29	14'95	16'62	0'98	0'24	0'49	0'73
46	1'70	3'40	5'10	6'81	8'51	10'21	11'91	13'61	15'31	17'01	1'00	0'25	0'50	0'75
47	1'74	3'49	5'23	6'97	8'72	10'46	12'20	13'95	15'69	17'43	1'02	0'25	0'51	0'76
48	1'79	3'58	5'36	7'15	8'94	10'73	12'52	14'31	16'09	17'88	1'04	0'26	0'52	0'78
49	1'84	3'67	5'51	7'34	9'18	11'02	12'85	14'67	16'52	18'36	1'06	0'26	0'53	0'79
50	1'89	3'77	5'66	7'55	9'44	11'32	13'21	15'10	16'98	18'87	1'08	0'27	0'54	0'81
51	1'94	3'88	5'82	7'77	9'71	11'65	13'59	15'53	17'47	19'42	1'10	0'27	0'55	0'82
52	2'00	4'00	6'00	8'00	10'00	12'00	14'00	16'00	18'00	20'00	1'12	0'28	0'56	0'84
53	2'06	4'13	6'19	8'25	10'31	12'38	14'44	16'50	18'56	20'63	1'14	0'28	0'57	0'85
54	2'13	4'26	6'39	8'52	10'65	12'78	14'91	17'04	19'17	21'30	1'16	0'29	0'58	0'87
55	2'20	4'41	6'61	8'81	11'01	13'22	15'42	17'62	19'82	22'03	1'18	0'29	0'59	0'88
56	2'28	4'56	6'84	9'12	11'41	13'69	15'97	18'25	20'53	22'81	1'20	0'30	0'60	0'90
57	2'37	4'73	7'10	9'46	11'83	14'20	16'56	18'93	21'30	23'66	1'22	0'30	0'61	0'91
58	2'46	4'92	7'38	9'83	12'29	14'75	17'21	19'67	22'13	24'59	1'24	0'31	0'62	0'93
59	2'56	5'12	7'68	10'24	12'80	15'36	17'92	20'47	23'03	25'59	1'26	0'31	0'63	0'94
60	2'67	5'34	8'01	10'68	13'35	16'02	18'69	21'36	24'03	26'69	1'28	0'32	0'64	0'96
61	2'79	5'58	8'37	11'16	13'95	16'74	19'53	22'32	25'11	27'90	1'30	0'32	0'65	0'97

TABLE 4

523

DIFFERENCE OF LONGITUDE AND CORRESPONDING DEPARTURE

Lat.	DIFFERENCE OF LONGITUDE										PART			
	1	2	3	4	5	6	7	8	9	10	Dto 1°	15'	30'	45'
0°	1'00	2'00	3'00	4'00	5'00	6'00	7'00	8'00	9'00	10'00	0'01	0'00	0'00	0'01
1	1'00	2'00	2'99	3'99	4'99	5'99	6'98	7'98	8'98	9'98	0'02	0'00	0'01	0'02
2	0'99	1'99	2'98	3'98	4'97	5'97	6'96	7'96	8'95	9'95	0'03	0'01	0'02	0'03
3	0'99	1'98	2'97	3'96	4'95	5'94	6'93	7'92	8'91	9'90	0'04	0'01	0'02	0'03
4	0'98	1'97	2'95	3'94	4'92	5'91	6'89	7'88	8'86	9'85	0'05	0'01	0'03	0'04
5	0'98	1'96	2'93	3'91	4'89	5'87	6'85	7'83	8'80	9'78	0'06	0'02	0'03	0'05
6	0'97	1'94	2'91	3'88	4'85	5'82	6'79	7'76	8'73	9'70	0'07	0'02	0'04	0'05
7	0'97	1'93	2'90	3'86	4'83	5'80	6'76	7'73	8'69	9'66	0'08	0'02	0'04	0'06
8	0'96	1'92	2'88	3'85	4'81	5'77	6'73	7'69	8'65	9'61	0'09	0'02	0'05	0'07
9	0'96	1'91	2'87	3'83	4'78	5'74	6'69	7'65	8'61	9'56	0'10	0'03	0'05	0'08
10	0'95	1'90	2'85	3'80	4'76	5'71	6'66	7'61	8'56	9'51	0'11	0'03	0'06	0'08
11	0'95	1'89	2'84	3'78	4'73	5'67	6'62	7'56	8'51	9'46	0'12	0'03	0'06	0'09
12	0'94	1'88	2'82	3'76	4'70	5'64	6'58	7'52	8'46	9'40	0'13	0'03	0'07	0'10
13	0'93	1'87	2'80	3'73	4'67	5'60	6'54	7'47	8'40	9'34	0'14	0'04	0'07	0'11
14	0'93	1'85	2'78	3'71	4'64	5'56	6'49	7'42	8'34	9'27	0'15	0'04	0'08	0'11
15	0'92	1'84	2'76	3'68	4'60	5'52	6'44	7'36	8'28	9'21	0'16	0'04	0'08	0'12
16	0'91	1'83	2'74	3'65	4'57	5'48	6'39	7'31	8'22	9'14	0'17	0'04	0'09	0'13
17	0'91	1'81	2'72	3'63	4'53	5'44	6'34	7'25	8'16	9'06				
18	0'90	1'80	2'70	3'60	4'49	5'39	6'29	7'19	8'09	8'99				
19	0'89	1'78	2'67	3'56	4'46	5'35	6'24	7'13	8'02	8'91				
20	0'88	1'77	2'65	3'53	4'44	5'30	6'18	7'06	7'95	8'83				
21	0'87	1'75	2'62	3'50	4'37	5'25	6'12	7'00	7'87	8'75				
22	0'87	1'73	2'60	3'46	4'33	5'20	6'06	6'93	7'79	8'66				
23	0'86	1'71	2'57	3'43	4'29	5'14	6'00	6'86	7'71	8'57				
24	0'85	1'70	2'54	3'39	4'24	5'09	5'94	6'78	7'63	8'48				
25	0'84	1'68	2'52	3'35	4'19	5'03	5'87	6'71	7'55	8'39				
26	0'83	1'66	2'49	3'32	4'15	4'97	5'80	6'63	7'46	8'29				
27	0'82	1'64	2'46	3'28	4'10	4'91	5'73	6'55	7'37	8'19				
28	0'81	1'62	2'43	3'24	4'05	4'85	5'66	6'47	7'28	8'09				
29	0'80	1'60	2'40	3'19	3'99	4'79	5'59	6'39	7'19	7'99				
30	0'79	1'58	2'36	3'15	3'94	4'73	5'52	6'30	7'09	7'88				
31	0'78	1'55	2'33	3'11	3'89	4'66	5'44	6'22	6'99	7'77				
32	0'77	1'53	2'30	3'06	3'83	4'60	5'36	6'13	6'89	7'66				
33	0'75	1'51	2'26	3'02	3'77	4'53	5'28	6'04	6'79	7'55				
34	0'74	1'49	2'23	2'97	3'72	4'46	5'20	5'95	6'69	7'43				
35	0'73	1'46	2'19	2'93	3'66	4'39	5'12	5'85	6'58	7'31				
36	0'72	1'44	2'16	2'88	3'60	4'32	5'04	5'75	6'47	7'19				
37	0'71	1'41	2'12	2'83	3'54	4'24	4'95	5'66	6'36	7'07				
38	0'69	1'39	2'08	2'78	3'47	4'17	4'86	5'56	6'25	6'95				
39	0'68	1'36	2'04	2'73	3'41	4'09	4'77	5'46	6'14	6'82				
40	0'67	1'34	2'01	2'68	3'35	4'01	4'68	5'35	6'02	6'69				
41	0'66	1'31	1'57	2'62	3'28	3'94	4'59	5'25	5'90	6'56				
42	0'64	1'29	1'93	2'57	3'21	3'86	4'50	5'14	5'79	6'43				
43	0'63	1'26	1'89	2'52	3'15	3'78	4'41	5'03	5'66	6'29				
44	0'62	1'23	1'85	2'46	3'08	3'69	4'31	4'93	5'54	6'16				
45	0'60	1'20	1'81	2'41	3'01	3'61	4'21	4'81	5'42	6'02				
46	0'59	1'18	1'76	2'35	2'94	3'53	4'11	4'70	5'29	5'88				
47	0'57	1'16	1'72	2'29	2'87	3'44	4'02	4'59	5'16	5'74				
48	0'56	1'12	1'68	2'24	2'80	3'35	3'91	4'47	5'03	5'59				
49	0'54	1'09	1'63	2'18	2'72	3'27	3'81	4'36	4'90	5'45				
50	0'53	1'06	1'59	2'12	2'65	3'18	3'71	4'24	4'77	5'30				
51	0'52	1'03	1'55	2'06	2'58	3'09	3'61	4'12	4'64	5'16				
52	0'50	1'00	1'50	2'00	2'50	3'00	3'50	4'00	4'50	5'00				
53	0'48	0'97	1'45	1'94	2'42	2'91	3'39	3'88	4'36	4'85				
54	0'47	0'94	1'41	1'88	2'35	2'82	3'29	3'76	4'23	4'69				
55	0'45	0'91	1'36	1'82	2'27	2'72	3'18	3'63	4'09	4'54				
56	0'44	0'88	1'32	1'75	2'19	2'63	3'07	3'51	3'95	4'38				
57	0'42	0'85	1'27	1'69	2'11	2'54	2'96	3'38	3'80	4'23				
58	0'41	0'81	1'22	1'63	2'03	2'44	2'85	3'25	3'66	4'07				
59	0'39	0'78	1'17	1'56	1'95	2'34	2'74	3'13	3'52	3'91				
60	0'37	0'75	1'12	1'50	1'87	2'25	2'62	3'00	3'37	3'75				
61	0'36	0'72	1'08	1'43	1'79	2'15	2'51	2'87	3'23	3'58				

SPHERICAL TRAVERSE TABLE

°	0°		1°		2°		3°		4°		5°		6°	
	M	N	M	N	M	N	M	N	M	N	M	N	M	N
0	100°0	0												
1	100°0	0	100°0	0°0										
2	100°1	0	100°1	0°1	100°1	0°1								
3	100°1	0	100°1	0°1	100°1	0°2	100°3	0°3						
4	100°2	0	100°3	0°1	100°3	0°2	100°4	0°4	100°5	0°5				
5	100°4	0	100°4	0°1	100°4	0°3	100°5	0°5	100°6	0°6	100°8	0°8		
6	100°5	0	100°6	0°2	100°6	0°4	100°7	0°5	100°8	0°7	100°9	0°9	101°1	1°1
7	100°7	0	100°8	0°2	100°8	0°4	100°9	0°6	101°0	0°9	101°1	1°1	101°3	1°3
8	101°0	0	101°0	0°2	101°0	0°5	101°1	0°7	101°2	1°0	101°4	1°2	101°5	1°5
9	101°2	0	101°3	0°3	101°3	0°5	101°4	0°8	101°5	1°1	101°6	1°4	101°8	1°7
10	101°5	0	101°6	0°3	101°6	0°6	101°7	0°9	101°8	1°2	101°9	1°5	102°1	1°8
11	101°9	0	101°9	0°3	101°9	0°7	102°0	1°0	102°1	1°4	102°3	1°7	102°4	2°0
12	102°2	0	102°2	0°4	102°3	0°7	102°4	1°1	102°5	1°5	102°6	1°9	102°8	2°2
13	102°6	0	102°6	0°4	102°7	0°8	102°8	1°2	102°9	1°6	103°3	2°0	103°2	2°4
14	103°1	0	103°1	0°4	103°1	0°9	103°2	1°3	103°3	1°7	103°5	2°2	103°6	2°6
15	103°5	0	103°5	0°5	103°6	0°9	103°7	1°4	103°8	1°9	103°9	2°3	104°1	2°8
16	104°0	0	104°0	0°5	104°1	1°0	104°2	1°5	104°3	2°0	104°4	2°5	104°6	3°0
17	104°6	0	104°6	0°5	104°6	1°1	104°7	1°6	104°8	2°1	104°7	2°7	105°1	3°2
18	105°1	0	105°2	0°6	105°2	1°1	105°3	1°7	105°4	2°3	105°5	2°8	105°7	3°4
19	105°8	0	105°8	0°6	105°8	1°2	105°9	1°8	106°0	2°4	106°2	3°0	106°3	3°6
20	106°4	0	106°4	0°6	106°5	1°3	106°6	1°9	106°7	2°5	106°8	3°2	107°0	3°8
21	107°1	0	107°1	0°7	107°2	1°3	107°3	2°0	107°4	2°7	107°5	3°4	107°7	4°0
22	107°8	0	107°9	0°7	107°9	1°4	108°0	2°1	108°1	2°8	108°3	3°5	108°4	4°2
23	108°6	0	108°6	0°7	108°7	1°5	108°8	2°2	108°9	3°0	109°0	3°7	109°2	4°5
24	109°5	0	109°5	0°8	109°5	1°5	109°6	2°3	109°7	3°1	109°9	3°9	110°1	4°7
25	110°3	0	110°4	0°8	110°1	1°6	110°5	2°4	110°6	3°3	110°8	4°1	110°9	4°9
26	111°3	0	111°3	0°8	111°3	1°7	111°4	2°6	111°5	3°4	111°7	4°3	111°9	5°1
27	112°2	0	112°2	0°9	112°3	1°8	112°4	2°7	112°5	3°5	112°7	4°5	112°8	5°3
28	113°3	0	113°3	0°9	113°3	1°9	113°4	2°8	113°5	3°7	113°7	4°7	113°9	5°6
29	114°3	0	114°4	1°0	114°4	1°9	114°5	2°9	114°6	3°9	114°8	4°8	115°0	5°8
30	115°5	0	115°5	1°0	115°4	2°0	115°6	3°0	115°7	4°0	115°9	5°0	116°1	6°1
31	116°7	0	116°7	1°0	116°7	2°1	116°8	3°1	116°9	4°2	117°1	5°3	117°3	6°3
32	117°9	0	117°9	1°1	118°0	2°2	118°1	3°3	118°2	4°4	118°4	5°5	118°6	6°6
33	119°2	0	119°3	1°1	119°3	2°3	119°4	3°4	119°5	4°5	119°7	5°7	119°9	6°8
34	120°6	0	120°6	1°2	120°7	2°4	120°8	3°5	120°9	4°7	121°1	5°9	121°3	7°1
35	122°1	0	122°1	1°2	122°1	2°4	122°2	3°7	122°4	4°9	122°5	6°2	122°7	7°4
36	123°6	0	123°6	1°3	123°7	2°5	123°8	3°8	123°9	5°1	124°1	6°4	124°3	7°6
37	125°2	0	125°2	1°3	125°3	2°6	125°4	3°9	125°5	5°3	125°7	6°6	125°9	7°9
38	126°9	0	126°9	1°4	127°0	2°7	127°1	4°1	127°2	5°5	127°4	6°8	127°6	8°2
39	128°7	0	128°7	1°4	128°8	2°8	128°9	4°2	129°0	5°7	129°2	7°1	129°4	8°5
40	130°5	0	130°6	1°5	130°6	2°9	130°7	4°4	130°9	5°9	131°0	7°3	131°3	8°8
41	132°5	0	132°5	1°5	132°6	3°0	132°7	4°6	132°8	6°1	133°0	7°6	133°2	9°1
42	134°6	0	134°6	1°6	134°6	3°1	134°7	4°7	134°9	6°3	135°1	7°9	135°3	9°5
43	136°7	0	136°8	1°6	136°8	3°3	136°9	4°9	137°1	6°5	137°3	8°2	137°5	9°8
44	139°0	0	139°0	1°7	139°1	3°4	139°2	5°1	139°4	6°7	139°5	8°4	139°8	10°1
45	141°4	0	141°4	1°7	141°5	3°5	141°6	5°2	141°8	7°0	142°0	8°7	142°2	10°5
46	144°0	0	144°0	1°8	144°0	3°6	144°2	5°4	144°3	7°2	144°5	9°1	144°7	10°9
47	146°6	0	146°6	1°9	146°7	3°7	146°8	5°6	147°0	7°5	147°2	9°4	147°4	11°3
48	149°4	0	149°5	1°9	149°5	3°9	149°7	5°8	149°8	7°8	150°0	9°7	150°3	11°7
49	152°4	0	152°4	2°0	152°5	4°0	152°6	6°0	152°1	8°0	153°0	10°1	153°3	12°1
50	155°6	0	155°6	2°1	155°7	4°2	155°8	6°2	155°7	8°3	156°2	10°4	156°4	12°5
51	158°9	0	158°9	2°2	159°0	4°3	159°1	6°5	159°3	8°6	159°5	10°8	159°8	13°0
52	162°4	0	162°5	2°2	162°5	4°5	162°6	6°7	162°8	8°9	163°0	11°2	163°3	13°4
53	166°2	0	166°2	2°3	166°3	4°6	166°4	6°9	166°6	9°3	166°8	11°6	167°1	13°9
54	170°1	0	170°2	2°4	170°2	4°8	170°4	7°2	170°5	9°6	170°8	12°0	171°1	14°5
55	174°3	0	174°4	2°5	174°4	5°0	174°6	7°5	174°8	10°0	175°0	12°5	175°2	15°0
56	178°8	0	178°9	2°6	178°9	5°2	179°5	7°8	179°3	10°4	179°5	13°0	179°8	15°6
57	183°6	0	183°6	2°7	183°7	5°4	183°9	8°1	184°1	10°8	184°3	13°5	184°6	16°2
58	188°7	0	188°7	2°8	188°2	5°6	189°0	8°4	189°2	11°2	189°4	14°0	189°7	16°8
59	194°2	0	194°2	2°9	194°3	5°8	194°4	8°7	194°6	11°6	194°9	14°6	195°2	17°5
60	200°0	0	200°0	3°0	200°1	6°0	200°3	9°1	200°5	12°1	200°8	15°1	201°1	18°2

TABLE 5

SPHERICAL TRAVERSE TABLE														
0°			1°		2°		3°		4°		5°		6°	
°	M	N	M	N	M	N	M	N	M	N	M	N	M	N
61	206.3	0	206.3	3.1	206.4	6.3	206.5	9.4	206.8	12.6	207.1	15.8	207.4	19.0
62	213.0	0	213.0	3.3	213.2	6.6	213.3	9.9	213.5	13.1	213.8	16.4	214.2	19.8
63	220.3	0	220.3	3.4	220.4	6.8	220.6	10.3	220.8	13.7	221.1	17.2	221.5	20.6
64	228.1	0	228.2	3.6	228.3	7.2	228.4	10.7	228.7	14.3	229.0	17.9	229.4	21.5
65	236.6	0	236.7	3.7	236.8	7.5	236.9	11.2	237.2	15.0	237.5	18.8	237.9	22.5
66	245.8	0	245.9	3.9	246.0	7.8	246.2	11.8	246.5	15.7	246.8	19.6	247.2	23.6
67	255.9	0	256.0	4.1	256.1	8.2	256.2	12.3	256.6	16.5	256.9	20.6	257.3	24.8
68	266.9	0	267.0	4.3	267.1	8.6	267.3	13.0	267.6	17.3	268.0	21.7	268.4	26.0
69	279.0	0	279.1	4.5	279.2	9.1	279.4	13.6	279.7	18.2	280.1	22.8	280.6	27.4
70	292.4	0	292.4	4.8	292.6	9.6	292.8	14.4	293.1	19.2	293.5	24.0	294.0	28.9
71	307.2	0	307.2	5.1	307.3	10.1	307.6	15.2	307.9	20.3	308.3	25.4	308.9	30.5
72	323.6	0	323.7	5.4	323.8	10.7	324.1	16.1	324.4	21.5	324.8	26.9	325.4	32.3
73	342.0	0	342.1	5.7	342.2	11.4	342.4	17.1	342.9	22.9	343.3	28.6	343.9	34.4
74	362.8	0	362.9	6.1	363.0	12.2	363.3	18.3	363.7	24.4	364.2	30.5	364.8	36.6
75	386.4	0	386.4	6.5	386.6	13.0	386.9	19.6	387.3	26.1	387.8	32.6	388.5	39.2
76	413.3	0	404.0	7.0	413.6	14.0	413.9	21.0	414.4	28.0	414.9	35.1	415.6	42.2
77	444.5	0	444.6	7.6	444.8	15.1	445.2	22.7	445.6	30.3	446.1	37.9	447.0	43.5
78	481.0	0	481.0	8.2	481.3	16.4	481.6	24.6	482.1	32.9	482.8	41.2	483.6	49.4
79	524.1	0	524.2	9.0	524.4	18.0	524.8	27.0	525.4	36.0	526.1	45.0	527.0	54.1
80	575.9	0	576.0	9.9	576.2	19.8	576.7	29.7	577.3	39.7	578.2	49.6	579.1	59.6
7°			8°		9°		10°		11°		12°		13°	
°	M	N	M	N	M	N	M	N	M	N	M	N	M	N
7	101.5	1.5												
8	101.7	1.7	102.0	2.0										
9	102.0	1.9	102.2	2.2	102.5	2.5								
10	102.3	2.2	102.5	2.5	102.8	2.8	103.1	3.1						
11	102.6	2.4	102.9	2.7	103.1	3.1	103.4	3.4	103.8	5.8				
12	103.0	2.6	103.2	3.0	103.5	3.4	103.8	3.7	104.1	4.1	104.5	4.5		
13	103.4	2.8	103.6	3.2	103.9	3.7	104.2	4.1	104.5	4.5	104.9	4.9	105.3	5.3
14	103.8	3.1	104.1	3.5	104.3	3.9	104.6	4.4	105.0	4.8	105.4	5.3	105.8	5.8
15	104.3	3.3	104.5	3.8	104.8	4.2	105.1	4.7	105.5	5.2	105.8	5.7	106.2	6.2
16	104.8	3.5	105.0	4.0	105.3	4.5	105.6	5.1	106.0	5.6	106.4	6.1	106.8	6.6
17	105.3	3.7	105.6	4.3	105.9	4.8	106.2	5.4	106.5	5.9	106.9	6.5	107.3	7.1
18	106.0	4.0	106.2	4.6	106.5	5.1	106.8	5.7	107.1	6.3	107.5	6.9	107.9	7.5
19	106.6	4.2	106.8	4.8	107.1	5.5	107.4	6.1	107.7	6.7	108.1	7.3	108.5	7.9
20	107.2	4.5	107.5	5.1	107.7	5.8	108.1	6.4	108.4	7.1	108.8	7.7	109.2	8.4
21	107.9	4.7	108.2	5.4	108.4	6.1	108.8	6.8	109.1	7.5	109.5	8.2	109.9	8.9
22	108.7	5.0	108.9	5.7	109.2	6.4	109.5	7.1	109.9	7.8	110.3	8.6	110.7	9.3
23	109.4	5.2	109.7	6.0	110.0	6.7	110.3	7.5	110.7	8.3	111.1	9.0	111.5	9.8
24	110.3	5.5	110.5	6.3	110.8	7.0	111.0	7.9	111.5	8.7	111.9	9.5	112.3	10.3
25	111.2	5.7	111.4	6.6	111.7	7.4	111.9	8.2	112.4	9.1	112.8	9.9	113.2	10.8
26	112.1	6.0	112.4	6.8	112.6	7.7	112.9	8.6	113.4	9.5	113.7	10.4	114.2	11.3
27	113.1	6.3	113.3	7.2	113.6	8.1	114.0	9.0	114.3	9.9	114.7	10.8	115.2	11.8
28	114.1	6.5	114.4	7.5	114.7	8.4	115.1	9.4	115.4	10.3	115.8	11.3	116.2	12.3
29	115.2	6.8	115.5	7.8	115.8	8.8	116.1	9.8	116.5	10.8	116.9	11.8	117.3	12.8
30	116.3	7.1	116.6	8.1	116.9	9.1	117.2	10.2	117.6	11.2	118.0	12.3	118.5	13.3
31	117.5	7.4	117.8	8.4	118.1	9.5	118.5	10.6	118.8	11.7	119.3	12.8	119.7	13.9
32	118.6	7.7	119.1	8.8	119.4	9.9	119.8	11.0	120.1	12.1	120.6	13.3	121.0	14.4
33	120.1	8.0	120.4	9.1	120.7	10.3	121.1	11.4	121.5	12.6	121.9	13.8	122.7	15.0
34	121.5	8.3	121.8	9.5	122.1	10.7	122.5	11.9	122.9	13.1	123.3	14.3	123.8	15.6
35	123.0	8.6	123.3	9.8	123.6	11.1	124.0	12.3	124.4	13.6	124.8	14.9	125.3	16.2
36	124.5	8.9	124.8	10.2	125.1	11.5	125.5	12.8	125.9	14.1	126.4	15.4	126.9	16.7
37	126.2	9.3	126.4	10.6	126.8	11.9	127.1	13.3	127.6	14.6	128.0	16.0	128.5	17.4
38	127.9	9.6	128.1	11.0	128.5	12.4	128.9	13.8	129.3	15.2	129.7	16.6	130.2	18.0
39	129.6	9.9	129.9	11.4	130.3	12.8	130.7	14.3	131.1	15.7	131.5	17.2	132.1	18.7
40	131.5	10.3	131.8	11.8	132.2	13.3	132.6	14.8	133.0	16.3	133.5	17.8	134.0	19.4
41	133.5	10.7	133.8	12.2	134.1	13.8	134.5	15.3	135.0	16.9	135.5	18.5	136.0	20.1
42	135.6	11.1	135.9	12.6	136.2	14.3	136.6	15.9	137.1	17.5	137.6	19.1	138.1	20.8
43	137.8	11.4	138.1	13.1	138.4	14.8	138.8	16.4	139.3	18.1	139.8	19.8	140.3	21.5

SPHERICAL TRAVERSE TABLE

	7°		8°		9°		10°		11°		12°		13°	
°	M	N	M	N	M	N	M	N	M	N	M	N	M	N
44	140°1	11°9	140°4	13°6	140°7	15°4	141°2	17°0	141°6	18°8	142°1	20°5	142°7	22°3
45	142°5	12°3	142°8	14°0	143°2	15°8	143°6	17°6	144°1	19°4	144°6	21°3	145°1	23°1
46	145°0	12°7	145°4	14°5	145°7	16°4	146°2	18°3	146°6	20°1	147°2	22°0	147°7	23°9
47	147°7	13°2	148°1	15°1	148°5	17°0	148°9	18°9	149°4	20°8	149°9	22°8	150°8	24°8
48	150°6	13°6	150°9	15°6	151°3	17°6	151°7	19°6	152°2	21°6	152°8	23°6	153°4	25°6
49	153°6	14°1	153°9	16°2	154°3	18°2	154°8	20°3	155°3	22°4	155°9	24°4	156°4	26°6
50	156°7	14°6	157°1	16°7	157°5	18°9	158°0	21°0	158°5	23°2	159°0	25°3	159°7	27°5
51	160°1	15°2	160°5	17°4	160°9	19°6	161°4	21°8	161°9	24°0	162°5	26°2	163°1	28°5
52	163°6	15°7	164°0	18°0	164°4	20°3	165°0	22°6	165°5	24°9	166°1	27°2	166°7	29°5
53	166°4	16°3	167°8	18°6	168°2	21°0	168°7	23°4	169°3	25°8	169°9	28°2	170°5	30°6
54	171°4	16°9	171°8	19°3	172°2	21°8	172°8	24°3	173°3	26°8	173°9	29°3	174°6	31°8
55	175°7	17°5	176°1	20°1	176°5	22°6	177°0	25°2	177°6	27°8	178°2	30°4	178°9	33°0
56	180°2	18°2	180°6	20°8	181°1	23°5	181°6	26°1	182°2	28°8	182°8	31°5	183°5	34°2
57	185°0	18°9	185°4	21°6	185°9	24°4	186°4	27°1	187°0	29°9	187°7	32°7	188°4	35°5
58	190°1	19°6	190°6	22°5	191°1	25°3	191°6	28°2	189°2	31°1	192°9	34°0	193°6	36°9
59	195°6	20°4	196°1	23°4	196°6	26°4	197°2	29°3	197°8	32°3	198°5	35°4	199°3	38°4
60	201°5	21°3	202°0	24°3	202°5	27°4	203°1	30°5	203°7	33°7	204°5	36°8	205°3	40°0
61	207°8	22°1	208°3	25°3	208°8	28°6	209°9	31°8	210°1	35°1	210°9	38°3	211°7	41°6
62	214°6	23°1	215°1	26°4	215°7	29°8	216°3	33°2	217°0	36°6	217°8	40°0	218°6	43°4
63	221°9	24°1	222°4	27°6	223°0	31°1	223°7	34°6	224°4	38°1	225°2	41°7	226°1	45°3
64	229°8	25°2	230°4	28°8	231°0	32°5	231°6	36°1	232°4	39°8	233°2	43°6	234°1	47°3
65	238°4	26°3	238°9	30°1	239°6	34°0	240°3	37°8	241°0	41°7	241°9	45°6	242°8	49°5
66	247°9	27°6	248°4	31°6	248°9	35°6	249°7	39°6	250°5	43°7	251°4	47°7	252°3	51°8
67	257°7	28°9	258°4	33°1	259°1	37°3	259°9	41°5	260°7	45°8	261°6	50°1	262°7	54°4
68	269°0	30°4	269°6	34°8	270°3	39°2	271°1	43°6	271°9	48°1	272°9	52°6	274°0	57°1
69	281°1	32°0	281°8	36°6	282°5	41°3	283°4	45°9	284°3	50°6	285°3	55°4	286°4	60°1
70	294°6	33°7	295°3	38°6	296°0	43°5	296°9	48°4	297°9	53°4	298°9	58°4	300°1	65°4
71	309°5	35°7	310°2	40°8	311°0	46°0	311°9	51°2	312°9	56°4	314°0	61°7	315°2	67°0
72	326°0	37°8	326°8	43°2	327°6	48°7	328°6	54°3	329°6	59°8	330°8	65°4	332°1	71°0
73	344°6	40°2	345°4	46°0	346°3	51°8	347°3	57°7	348°4	63°6	349°7	69°5	351°0	75°5
74	365°5	42°8	366°4	49°0	367°3	55°2	368°4	61°7	369°6	67°8	370°9	74°1	372°3	80°5
75	389°0	45°8	390°2	52°5	391°2	59°1	392°3	65°8	393°6	72°5	395°1	79°3	396°5	86°2
76	416°5	49°2	417°4	56°4	418°5	63°5	419°7	70°7	421°1	78°0	422°6	85°2	424°3	92°6
77	447°9	53°2	448°9	60°9	450°1	68°6	451°4	76°4	452°9	84°2	454°5	92°1	456°2	100°0
78	484°6	57°8	485°7	66°1	487°0	74°5	488°4	83°0	490°0	91°4	491°7	100°0	493°6	108°6
79	528°0	63°1	529°2	72°3	530°6	81°5	532°2	90°7	533°9	100°0	535°8	109°3	537°9	118°8
80	580°2	69°6	581°5	79°7	583°1	89°8	584°8	100°0	586°7	110°2	588°7	120°9	591°0	130°9
	14°		15°		16°		17°		18°		19°		20°	
°	M	N	M	N	M	N	M	N	M	N	M	N	M	N
14	106°2	6°2												
15	106°7	6°7	107°2	7°2										
16	107°2	7°1	107°7	7°7	108°2	8°2								
17	107°8	7°6	108°3	8°2	108°8	8°8	109°3	9°3						
18	108°4	8°1	108°9	8°7	109°3	9°3	109°9	9°9	110°6	10°6				
19	109°0	8°6	109°5	9°2	110°0	9°9	110°6	10°5	111°2	11°2	111°9	11°9		
20	109°7	9°1	110°2	9°8	110°7	10°4	111°3	11°1	111°9	11°8	112°5	12°5	113°2	13°2
21	111°4	9°6	110°9	10°3	111°4	10°0	112°0	11°7	112°6	12°5	113°3	13°2	114°0	14°0
22	111°2	10°1	111°7	10°8	112°2	11°6	112°8	12°3	113°4	13°1	114°1	13°9	114°8	14°7
23	112°0	10°6	112°5	11°4	113°0	12°2	113°6	13°0	114°2	13°8	114°9	14°6	115°6	15°4
24	112°8	11°1	113°3	11°9	113°9	12°8	114°5	13°6	115°1	14°5	115°8	15°3	116°5	16°2
25	113°7	11°6	114°2	12°5	114°8	13°4	115°4	14°3	116°0	15°1	116°7	16°1	117°4	17°0
26	114°6	12°2	115°2	13°1	115°7	14°0	116°3	14°9	117°0	15°8	117°7	17°0	118°4	17°7
27	115°7	12°7	116°2	13°6	116°8	14°6	117°4	15°6	118°0	16°6	118°8	17°5	119°4	18°5
28	116°7	13°3	117°3	14°2	117°8	15°2	118°4	16°3	119°1	17°3	119°8	18°3	120°5	19°3
29	117°8	13°8	118°4	14°8	118°9	15°9	119°6	16°9	120°2	18°0	120°9	19°1	121°7	20°2
30	119°0	14°4	119°5	15°5	120°1	16°6	120°7	17°6	121°4	18°8	122°1	19°9	122°9	21°0
31	120°2	15°0	120°8	16°1	121°4	17°2	122°0	18°4	122°7	19°5	123°4	20°7	124°1	21°9
32	121°5	15°6	122°1	16°7	122°7	17°9	123°3	19°1	124°0	20°3	124°7	21°5	125°5	22°7

SPHERICAL TRAVERSE TABLE

°	14°		15°		16°		17°		18°		19°		20°	
	M	N	M	N	M	N	M	N	M	N	M	N	M	N
33	122.9	16.2	123.4	17.4	124.0	18.6	124.7	19.9	125.4	21.1	126.1	22.4	126.9	23.6
34	124.3	16.8	124.9	18.1	125.5	19.3	126.1	20.6	126.8	21.9	127.6	23.2	128.4	24.6
35	125.8	17.5	126.4	18.8	127.0	20.1	127.7	21.4	128.4	22.7	129.1	24.1	129.9	25.5
36	127.4	18.1	128.0	19.5	128.6	20.8	129.2	22.2	130.0	23.6	130.7	25.0	131.5	26.4
37	129.0	18.8	129.6	20.2	130.3	21.6	130.9	23.0	131.7	24.5	132.4	25.9	133.2	27.4
38	130.8	19.5	131.4	20.9	132.0	22.4	132.7	23.9	133.4	25.4	134.2	26.9	135.0	28.4
39	132.6	20.2	133.2	21.7	133.9	23.2	134.6	24.8	135.3	26.3	136.1	27.9	136.9	29.5
40	134.5	20.9	135.1	22.5	135.8	24.1	136.5	25.6	137.3	27.3	138.1	28.9	138.9	30.5
41	136.5	21.7	137.2	23.3	137.8	24.9	138.6	26.6	139.3	28.2	140.1	29.9	141.0	31.6
42	138.7	22.4	139.3	24.1	140.0	25.8	140.7	27.5	141.5	29.3	142.3	31.0	143.2	32.8
43	140.9	23.2	141.6	25.0	142.2	26.7	143.0	28.5	143.8	30.3	144.6	32.1	145.5	33.9
44	143.3	24.1	143.9	25.9	144.6	27.7	145.4	29.5	146.2	31.4	147.0	33.2	147.9	35.1
45	145.7	24.9	146.4	26.8	147.1	28.7	147.9	30.6	148.7	32.5	149.6	34.4	150.5	36.4
46	148.4	25.8	149.0	27.7	149.8	29.7	150.5	31.7	151.4	33.6	152.2	35.7	153.2	37.7
47	151.1	26.7	151.8	28.7	152.5	30.7	153.3	32.8	154.2	34.8	155.1	36.9	156.0	39.0
48	154.0	27.7	154.7	29.8	155.5	31.8	156.3	34.0	157.1	36.1	158.1	38.2	159.0	40.4
49	157.1	28.7	157.8	30.8	158.6	33.0	159.4	35.2	160.3	37.4	161.2	39.6	162.2	41.9
50	160.3	29.7	161.1	31.9	161.8	34.2	162.7	36.4	163.6	38.7	164.5	41.1	165.6	43.4
51	163.8	30.8	164.5	33.1	165.3	35.4	166.2	37.8	167.1	40.1	168.1	42.5	169.1	44.9
52	167.4	31.9	168.2	34.3	169.0	36.7	169.8	39.1	170.8	41.6	171.8	44.1	172.8	46.6
53	171.2	33.1	172.0	35.6	172.9	38.0	173.8	40.6	174.7	43.1	175.7	45.7	176.8	48.3
54	175.3	34.3	176.1	36.9	177.0	39.5	177.9	42.1	178.9	44.7	179.9	47.4	181.0	50.1
55	179.7	35.6	180.5	38.3	181.4	40.9	182.3	43.7	183.3	46.4	184.4	49.2	185.5	52.0
56	184.3	37.0	185.1	39.7	186.0	42.5	187.0	45.3	188.0	48.2	189.1	51.0	190.3	54.0
57	189.2	38.4	190.1	41.3	191.0	44.2	192.0	47.1	193.1	50.0	194.2	53.0	195.4	56.0
58	194.5	39.9	195.3	42.9	196.3	45.9	197.3	48.9	198.4	52.0	199.6	55.1	200.8	58.2
59	200.1	41.5	201.0	44.6	202.0	47.7	203.0	50.9	204.2	54.1	205.3	57.3	206.6	60.6
60	206.1	43.2	207.1	46.4	208.1	49.7	209.1	53.0	210.3	56.3	211.5	59.6	212.8	63.0
61	212.6	45.0	213.5	48.3	214.6	51.7	215.7	55.2	216.9	58.6	218.2	62.1	219.5	65.7
62	219.5	46.9	220.5	50.4	221.6	53.9	222.7	57.5	224.0	61.1	225.3	64.8	226.7	68.4
63	227.0	48.9	228.0	52.6	229.1	56.3	230.3	60.0	231.6	63.8	233.0	67.6	234.4	71.4
64	235.1	51.1	236.2	54.9	237.3	58.8	238.5	62.7	239.9	66.6	241.3	70.6	242.8	74.6
65	243.9	53.5	245.0	57.5	246.2	61.5	247.4	65.6	248.8	69.7	250.3	73.8	251.8	78.1
66	253.4	56.0	254.5	60.2	255.8	64.4	257.1	68.7	258.5	73.1	260.0	77.3	261.6	81.7
67	263.8	58.7	265.0	63.2	266.2	67.5	267.6	72.0	269.1	76.5	270.7	81.1	272.4	85.7
68	275.1	61.7	276.4	66.3	277.7	71.0	279.1	75.7	280.7	80.4	282.3	85.2	284.1	90.1
69	287.6	64.9	288.9	69.8	290.3	74.7	291.8	79.6	293.4	84.6	295.1	89.7	296.9	94.8
70	301.3	68.5	302.7	73.6	304.2	78.8	305.7	84.0	307.4	89.3	309.2	94.6	311.1	100.0
71	316.6	72.4	318.0	77.8	319.5	83.3	321.2	88.8	323.0	94.4	324.9	100.0	326.9	105.7
72	325.5	76.7	327.0	82.5	328.7	88.3	330.4	94.1	340.3	100.0	342.3	106.0	344.4	112.0
73	352.5	81.5	354.1	87.6	355.8	93.8	357.7	100.0	359.6	106.3	361.7	112.6	364.0	119.0
74	373.9	86.9	375.6	93.4	377.4	100.0	379.4	106.6	381.5	113.3	383.7	120.1	386.1	126.9
75	398.2	93.0	400.0	100.0	401.9	107.0	404.0	114.1	406.3	121.3	408.6	128.5	411.2	135.8
76	426.0	100.0	427.9	107.5	430.0	115.1	432.2	122.6	434.6	130.3	437.2	138.1	439.9	146.0
77	458.2	108.0	460.2	116.1	462.5	124.2	464.8	132.4	467.4	140.7	471.2	149.1	473.1	157.7
78	495.7	117.3	497.9	127.6	500.4	134.9	502.8	143.8	505.7	152.9	508.7	162.0	511.8	171.2
79	540.1	128.3	542.6	137.8	548.2	147.5	548.0	157.3	551.1	167.2	554.3	177.1	557.7	187.2
80	593.5	141.1	596.2	152.0	599.1	162.6	602.2	173.4	605.5	184.3	609.1	195.3	612.8	206.4
°	21°		22°		23°		24°		25°		26°		27°	
	M	N	M	N	M	N	M	N	M	N	M	N	M	N
21	114.7	14.7												
22	115.5	15.5	116.3	16.3										
23	116.4	16.3	117.2	17.1	118.0	18.0								
24	117.2	17.1	118.1	18.0	118.9	18.9	119.8	19.8						
25	118.2	17.9	119.0	18.8	119.9	19.8	120.8	20.8	121.7	21.7				
26	119.2	18.7	120.0	19.7	120.9	20.7	121.8	21.7	122.8	22.8	123.8	23.8		
27	120.2	19.6	121.0	20.6	121.9	21.6	122.8	22.7	123.8	23.8	124.9	24.8	126.0	26.0
28	121.3	20.4	122.1	21.5	123.0	22.6	124.0	23.7	125.0	24.8	126.0	25.9	127.1	27.1

SPHERICAL TRAVERSE TABLE

°	21°		22°		23°		24°		25°		26°		27°	
	M	N	M	N	M	N	M	N	M	N	M	N	M	N
29	122.5	21.3	123.3	22.4	124.2	23.5	125.2	24.7	126.2	25.8	127.2	27.0	128.3	28.2
30	123.2	22.2	124.5	23.3	125.4	24.5	126.4	25.7	127.4	26.9	128.2	28.2	129.6	29.4
31	125.0	23.1	125.8	24.3	126.7	25.5	127.7	26.7	128.7	28.0	129.8	29.3	130.9	30.6
32	126.3	24.0	127.2	25.2	128.1	26.5	129.1	27.8	130.1	29.1	131.2	30.5	132.3	31.8
33	127.7	24.9	128.6	26.2	129.5	27.6	130.5	28.9	131.6	30.3	132.7	31.7	133.8	33.1
34	129.2	25.9	130.1	27.2	131.0	28.6	132.0	30.0	133.1	31.4	134.2	32.9	135.4	34.4
35	130.8	26.9	131.7	28.3	132.6	29.7	133.6	31.2	134.7	32.6	135.8	34.1	137.0	35.7
36	132.4	27.9	133.3	29.4	134.3	30.8	135.3	32.3	136.4	33.9	137.5	35.4	138.7	37.0
37	134.1	28.9	135.0	30.4	136.0	32.0	137.1	33.5	138.2	35.1	139.3	36.7	140.5	38.4
38	135.9	30.0	136.9	31.6	137.9	33.2	138.9	34.8	140.0	36.4	141.2	38.1	142.4	39.8
39	137.8	31.1	138.8	32.7	139.5	34.4	140.9	36.0	142.0	37.8	143.2	39.5	144.4	41.2
40	139.8	32.2	140.8	33.9	141.8	35.6	142.9	37.4	144.0	39.1	145.2	40.9	146.5	42.8
41	141.9	33.4	142.9	35.1	143.9	36.9	145.0	38.7	146.2	40.5	147.4	42.4	148.7	44.3
42	144.1	34.6	145.1	36.4	146.2	38.2	147.3	40.1	148.5	42.0	149.7	43.9	151.0	45.9
43	146.5	35.8	147.5	37.7	148.5	39.6	149.7	41.5	150.9	43.5	152.1	45.5	153.5	47.5
44	148.9	37.1	149.9	39.0	151.0	41.0	152.2	43.0	153.4	45.0	154.7	47.1	156.0	49.2
45	151.5	38.4	152.5	40.4	153.6	42.4	154.8	44.5	156.0	46.6	157.3	48.8	158.7	50.4
46	154.2	39.7	155.3	41.8	156.4	44.0	157.6	46.1	158.8	48.3	160.2	50.5	161.6	52.8
47	157.1	41.2	158.1	43.3	159.3	45.5	160.5	47.8	161.8	50.0	163.1	52.3	164.6	54.6
48	160.1	42.6	161.2	44.9	162.3	47.1	163.6	49.4	164.9	51.8	166.3	54.2	167.7	56.6
49	163.3	44.2	164.4	46.5	165.6	48.8	166.8	51.2	168.2	53.6	169.6	56.1	171.1	58.6
50	166.6	45.7	167.8	48.1	169.0	50.6	170.3	53.1	171.6	55.6	173.1	58.1	174.6	60.7
51	170.2	47.4	171.4	49.9	172.7	52.4	173.9	55.0	175.3	57.6	176.8	60.2	178.3	62.9
52	174.0	49.1	175.2	51.7	176.4	54.3	177.8	57.0	179.2	59.7	180.7	62.4	182.3	65.2
53	178.0	50.9	179.2	53.6	180.5	56.3	181.9	59.1	183.3	61.9	184.9	64.7	186.5	67.6
54	182.2	52.8	183.5	55.6	184.8	58.4	186.2	61.3	187.7	64.2	189.3	67.1	190.9	70.1
55	186.7	54.8	188.0	57.7	189.4	60.6	190.8	63.6	192.4	66.6	194.0	69.7	195.7	72.8
56	191.6	56.9	192.9	59.9	194.3	62.9	195.7	66.0	197.3	69.1	199.0	72.3	200.7	75.5
57	196.7	59.1	198.0	62.2	199.5	65.4	201.0	68.6	202.6	71.8	204.3	75.1	206.1	78.5
58	202.1	61.4	203.5	64.7	205.0	67.9	206.6	71.2	208.2	74.6	210.0	78.0	211.8	81.5
59	208.0	63.9	209.4	67.2	210.9	70.6	212.5	74.1	214.2	77.6	216.0	81.2	217.9	84.8
60	214.2	66.5	215.7	70.0	217.3	73.5	218.9	77.1	220.7	80.8	222.5	84.5	224.5	88.2
61	220.9	69.2	222.5	72.9	224.1	76.6	225.8	80.3	227.6	84.1	229.5	88.0	231.5	91.9
62	228.2	72.2	229.7	76.0	231.4	79.8	233.2	83.7	235.0	87.7	237.0	91.7	239.1	95.8
63	235.9	75.3	237.6	79.3	239.3	83.3	241.1	87.4	243.0	91.5	245.1	95.7	247.2	100.0
64	244.3	78.7	246.0	82.8	247.8	87.0	249.7	91.3	251.7	95.6	253.8	100.0	256.0	104.5
65	253.5	82.3	255.2	86.6	257.1	91.0	259.0	95.5	261.1	100.0	263.3	104.6	265.6	109.3
66	263.4	86.2	265.2	90.7	267.1	95.1	269.1	100.0	271.3	104.7	273.5	109.5	275.9	114.4
67	274.1	90.4	276.0	95.2	278.0	100.0	280.1	104.9	282.4	109.9	284.7	114.9	287.2	120.0
68	285.9	95.0	287.9	100.0	290.0	105.1	292.2	110.2	294.5	115.4	297.0	120.7	299.6	126.1
69	298.9	100.0	301.0	105.3	303.1	110.6	305.4	116.0	307.9	121.5	310.5	127.1	313.2	132.7
70	313.2	105.5	315.3	111.0	317.6	116.6	320.1	122.3	322.6	128.1	325.3	134.0	328.1	140.0
71	329.0	111.5	331.3	117.3	333.7	123.3	336.2	129.3	338.9	135.4	341.7	141.6	344.7	148.0
72	346.6	118.1	349.0	124.3	351.6	130.6	354.2	137.0	357.1	143.5	360.0	150.1	363.2	156.8
73	366.4	125.6	368.9	132.1	371.6	138.8	374.4	145.6	377.4	152.5	380.5	159.5	383.9	166.7
74	388.6	133.9	391.3	140.9	394.1	148.0	397.1	155.3	400.3	162.6	403.6	170.1	407.2	177.7
75	413.9	143.3	416.7	150.8	419.7	158.4	422.9	166.5	426.3	174.0	429.9	182.0	432.6	190.2
76	442.8	154.0	445.8	162.0	449.0	170.3	452.5	178.6	456.1	187.0	459.9	195.6	463.9	204.4
77	476.2	166.3	479.4	175.0	482.9	183.9	486.6	192.8	490.5	202.0	494.6	211.3	498.9	220.7
78	515.2	180.6	518.7	190.9	522.5	199.7	526.5	209.5	530.7	219.4	535.1	229.5	539.8	239.7
79	561.4	197.5	565.3	207.8	569.3	218.4	573.7	229.1	578.3	239.9	583.1	250.9	588.2	262.1
80	616.9	217.7	621.1	229.1	625.6	240.7	630.4	252.5	635.4	264.5	640.7	276.6	646.3	289.0
°	28°		29°		30°		31°		32°		33°		34°	
	M	N	M	N	M	N	M	N	M	N	M	N	M	N
28	128.3	28.3												
29	129.5	29.5	130.7	30.7										
30	130.8	30.7	132.0	32.0	133.3	33.3								
31	132.1	31.9	133.4	33.3	134.7	34.7	136.1	36.1						
32	133.5	33.2	134.8	34.6	136.2	36.1	137.6	37.5	139.0	39.0				
33	135.0	34.5	136.3	36.0	137.7	37.5	139.1	39.0	140.6	40.6	142.2	42.2		

TABLE 5

529

SPHERICAL TRAVERSE TABLE

°	28°		29°		30°		31°		32°		33°		34°	
	M	N	M	N	M	N	M	N	M	N	M	N	M	N
34	136.6	35.9	137.9	37.4	139.3	38.9	140.7	40.5	142.2	42.1	143.8	43.8	145.5	45.5
35	138.3	37.2	139.6	38.8	141.0	40.4	142.4	42.1	143.9	43.8	145.6	45.5	147.3	47.2
36	140.0	38.6	141.3	40.3	142.7	41.9	144.2	43.7	145.8	45.4	147.4	47.2	149.1	49.0
37	141.8	40.1	143.2	41.8	144.6	43.5	146.1	45.3	147.6	47.1	149.3	48.9	151.0	50.8
38	143.7	41.5	145.1	43.3	146.5	45.1	148.0	46.9	149.6	48.8	151.3	50.7	153.1	52.7
39	145.7	43.1	147.1	44.9	148.6	46.7	150.1	48.7	151.7	50.6	153.4	52.6	155.2	54.6
40	147.8	44.6	149.3	46.5	150.7	48.4	152.3	50.4	153.9	52.4	155.7	54.5	157.5	56.6
41	150.1	46.2	151.5	48.2	153.0	50.2	154.6	52.2	156.2	54.3	158.0	56.4	159.8	58.6
42	152.4	47.9	153.9	49.9	155.4	52.0	157.0	54.1	158.7	56.3	160.4	58.5	162.3	60.8
43	154.9	49.6	156.3	51.7	157.9	53.8	159.5	56.0	161.2	58.3	163.0	60.6	164.9	62.9
44	157.5	51.3	158.9	53.5	160.5	55.8	162.2	58.0	163.9	60.3	165.8	62.7	167.7	65.1
45	160.2	53.2	161.7	55.4	163.3	57.7	165.0	60.1	166.8	62.5	168.6	64.9	170.6	67.4
46	163.0	55.1	164.6	57.4	166.2	59.8	167.9	62.2	169.7	64.7	171.6	67.2	173.6	69.8
47	166.1	57.0	167.6	59.4	169.3	61.9	171.1	64.4	172.9	67.0	174.8	69.6	176.9	72.3
48	169.3	59.0	170.9	61.6	172.6	64.1	174.3	66.7	176.2	69.4	178.2	72.1	180.3	74.9
49	172.6	61.2	174.3	63.8	176.0	66.4	177.8	69.1	179.7	71.9	181.7	74.7	183.9	77.6
50	176.2	63.4	177.9	66.1	179.1	68.8	181.5	71.6	183.4	74.5	185.5	77.4	187.7	80.4
51	180.0	65.7	181.7	68.4	183.5	70.3	185.4	74.2	187.4	77.2	189.5	80.2	191.7	83.3
52	184.0	68.1	185.7	70.9	187.6	73.9	189.5	76.9	191.5	80.0	193.7	83.1	195.9	86.3
53	188.2	70.6	190.0	73.6	191.9	76.6	193.8	79.7	195.9	82.9	198.1	86.2	200.4	89.5
54	192.7	73.2	194.5	76.3	196.4	79.5	198.5	82.7	200.6	86.0	202.9	89.4	205.2	92.8
55	197.5	75.9	199.3	79.2	201.3	82.4	203.4	85.8	205.6	89.2	207.9	92.7	210.3	96.3
56	202.5	78.8	204.5	82.2	206.5	85.6	208.6	89.1	210.9	92.6	213.2	96.3	215.7	100.0
57	207.9	80.0	209.9	85.4	212.0	88.9	214.2	92.5	216.6	96.2	218.9	100.0	221.5	103.9
58	213.7	85.1	215.8	88.7	217.9	92.4	220.2	96.2	222.5	100.0	225.0	103.9	227.6	107.9
59	219.9	88.5	222.0	92.2	224.2	96.1	226.5	100.0	228.9	104.0	231.5	108.1	234.2	112.3
60	226.5	92.1	228.7	96.0	230.9	100.0	233.3	104.1	235.8	108.2	238.5	112.5	241.2	116.8
61	233.6	95.9	235.8	100.0	238.2	104.2	240.6	108.4	243.2	112.7	245.9	117.2	248.8	121.7
62	241.2	100.0	243.5	104.2	246.0	108.6	248.5	113.0	251.2	117.5	254.0	122.1	256.9	126.9
63	249.5	104.3	251.8	108.8	254.3	113.3	257.0	117.9	259.7	122.6	262.6	127.5	265.7	132.4
64	258.4	109.0	260.8	113.6	263.4	118.4	266.1	123.2	269.0	128.1	272.0	133.1	275.2	138.5
65	268.0	114.0	270.5	118.9	273.2	123.8	276.0	128.9	279.0	134.0	282.1	139.3	285.4	144.6
66	278.5	119.4	281.1	124.5	283.9	129.7	286.8	135.0	289.9	140.3	293.2	145.9	296.6	151.5
67	289.9	125.3	292.6	130.6	295.5	136.0	298.6	141.6	301.8	147.2	305.2	153.0	308.6	158.9
68	302.3	131.6	305.2	137.2	308.2	142.9	311.4	148.7	314.8	154.7	318.3	160.7	322.0	167.0
69	316.0	138.5	319.0	144.4	322.2	150.4	325.5	156.5	329.0	162.8	332.7	169.2	336.6	175.7
70	331.1	146.1	334.3	152.3	337.6	158.6	341.1	165.1	344.8	171.7	348.6	178.4	352.7	185.3
71	347.9	154.4	351.2	161.0	354.7	167.7	358.3	174.5	362.2	181.5	366.2	188.6	370.5	195.9
72	366.5	163.6	370.0	170.6	373.7	177.7	377.5	184.9	381.6	192.3	385.9	199.9	390.3	207.6
73	387.4	173.9	391.1	181.3	394.9	188.8	399.0	196.5	403.3	204.4	407.8	212.4	412.6	220.6
74	410.9	185.4	414.8	193.9	413.9	201.3	423.2	209.5	427.8	217.9	432.6	226.5	437.6	235.2
75	437.6	198.4	441.8	206.8	446.1	215.5	450.7	224.2	455.6	234.3	460.7	242.4	466.0	251.7
76	468.2	213.3	472.6	222.3	477.3	231.6	482.2	241.0	487.4	250.6	492.9	260.5	498.6	270.5
77	503.5	230.3	508.3	240.1	513.3	250.1	518.6	260.3	524.2	270.7	530.1	281.3	536.2	292.1
78	544.7	250.1	549.9	260.8	555.4	271.6	561.1	282.9	567.2	294.0	573.5	305.5	580.2	317.3
79	593.6	273.5	599.2	285.2	605.2	297.0	611.4	309.1	618.0	321.5	624.9	334.1	632.2	347.0
80	652.2	301.5	658.4	314.4	665.0	327.4	671.8	340.8	679.0	354.4	686.7	368.3	694.6	382.5
°	35°		36°		37°		38°		39°		40°		41°	
	M	N	M	N	M	N	M	N	M	N	M	N	M	N
35	149.0	49.0												
36	150.9	50.9	152.8	52.8										
37	152.9	52.8	154.8	54.7	156.8	56.8								
38	154.9	54.7	156.9	56.8	158.9	58.9	161.0	61.0						
39	157.1	56.7	159.0	58.8	161.1	61.0	163.3	63.3	165.6	65.6				
40	159.4	58.8	161.4	61.0	163.5	63.2	165.7	65.6	168.0	67.9	170.4	70.4		
41	161.8	60.9	163.8	63.2	166.0	65.5	168.1	67.9	170.5	70.4	173.0	72.9	175.6	75.6
42	164.3	63.0	166.3	65.4	168.2	67.8	170.8	70.3	173.1	72.9	175.7	75.5	178.4	78.3
43	166.9	65.3	169.0	67.7	171.2	70.3	173.5	72.9	175.9	75.5	178.5	78.2	181.2	81.1
44	169.7	67.6	171.8	70.2	174.1	72.8	176.4	75.4	178.9	78.2	181.5	81.0	184.2	83.9

SPHERICAL TRAVERSE TABLE

	35°		36°		37°		38°		39°		40°		41°	
°	M	N	M	N	M	N	M	N	M	N	M	N	M	N
45	172.6	70.0	174.8	72.7	177.1	75.4	179.5	78.1	182.0	81.0	184.6	83.9	187.4	86.9
46	176.7	72.5	177.9	75.2	180.2	78.0	182.7	80.9	185.2	83.9	187.9	86.9	190.7	90.0
47	179.0	75.1	181.2	77.9	183.6	80.8	186.1	83.8	188.7	86.8	191.4	90.0	194.3	93.2
48	182.5	77.8	184.7	80.7	187.1	83.7	189.6	86.8	192.3	89.9	195.1	93.2	198.0	96.5
49	186.1	80.5	188.4	83.6	190.9	86.7	192.4	89.9	196.1	93.2	199.0	96.5	202.0	100.0
50	189.9	83.4	192.3	86.6	194.8	89.8	197.4	93.1	200.2	96.5	203.1	100.0	206.1	103.6
51	194.0	86.5	196.4	89.7	199.0	93.1	201.6	96.5	204.5	100.0	207.4	103.6	210.5	107.3
52	198.3	89.6	200.0	93.0	203.4	96.4	206.1	100.0	209.0	103.6	212.0	107.4	215.2	111.3
53	202.8	92.9	205.4	96.4	208.1	100.0	210.9	103.7	213.8	107.5	216.9	111.3	220.2	115.4
54	207.7	96.4	210.3	100.0	213.0	103.7	215.9	107.5	218.9	111.5	222.1	115.5	225.4	119.6
55	212.8	100.0	215.5	103.8	218.3	107.6	221.2	111.6	224.3	115.6	227.6	119.8	231.0	124.1
56	218.3	103.8	221.0	107.7	223.9	111.7	226.9	115.8	230.1	120.1	233.4	124.4	237.0	128.9
57	224.1	107.8	226.9	111.9	229.9	116.0	233.0	120.3	236.3	124.7	239.7	129.2	243.3	133.9
58	230.4	112.1	233.3	116.3	236.3	120.6	239.5	125.0	242.8	129.6	246.3	134.3	250.0	139.1
59	237.0	116.5	240.0	121.0	243.1	125.4	246.4	130.0	249.8	134.8	253.5	139.7	257.7	144.7
60	244.2	121.3	247.2	125.8	250.4	130.5	253.8	135.3	257.4	140.3	261.1	145.3	265.0	150.6
61	251.8	126.3	255.0	131.1	258.3	135.9	261.8	140.9	265.4	146.1	269.3	151.4	273.3	156.8
62	260.0	131.7	263.2	136.6	266.7	141.7	270.3	146.9	274.1	152.3	278.1	157.8	282.2	163.5
63	268.9	137.4	272.3	142.6	275.8	147.9	279.5	153.3	283.4	158.9	287.5	164.7	291.9	170.6
64	278.5	143.6	282.0	149.0	285.6	154.5	289.5	160.2	293.5	166.0	297.8	172.0	302.3	178.2
65	288.9	150.2	292.4	155.8	296.3	161.6	300.3	167.5	304.5	173.7	308.9	179.9	313.5	186.4
66	300.1	157.3	303.9	163.2	307.9	169.2	312.0	175.5	316.4	181.9	321.0	188.5	325.8	195.2
67	312.4	165.0	316.3	171.2	320.5	177.5	324.8	184.1	329.3	190.8	334.1	197.7	333.1	204.8
68	325.9	173.3	330.0	179.8	334.3	186.5	338.8	193.4	343.5	200.4	348.5	207.7	353.7	215.1
69	340.7	182.4	344.9	189.3	349.4	196.3	354.1	203.5	359.1	211.0	364.3	218.6	369.7	226.5
70	356.9	192.4	361.4	199.6	366.1	207.0	371.0	214.6	376.2	222.5	381.7	230.5	387.4	238.8
71	375.0	203.4	379.7	211.0	384.6	218.8	389.8	226.9	395.2	235.2	401.0	243.7	407.0	252.5
72	395.1	215.5	400.0	223.6	405.2	231.9	410.7	240.5	416.4	249.2	422.4	258.2	428.8	267.5
73	417.5	229.0	422.8	237.6	428.3	246.5	434.0	255.5	440.1	264.9	446.5	274.5	453.2	284.5
74	442.9	244.2	448.4	253.4	454.3	262.8	460.4	272.5	466.8	282.4	473.6	292.6	480.7	303.2
75	471.7	261.3	477.6	271.1	483.8	281.2	490.3	291.6	497.2	302.2	504.4	313.3	511.9	324.5
76	504.6	280.8	510.9	291.4	517.6	302.2	524.6	313.4	531.9	324.8	539.6	336.5	547.7	348.7
77	542.7	303.3	549.5	314.7	556.6	326.4	564.1	338.4	572.0	350.8	580.3	363.5	589.0	376.5
78	587.2	329.4	594.5	341.8	602.2	354.5	610.4	367.6	618.9	381.0	627.9	394.8	637.3	409.0
79	639.8	360.2	647.8	373.8	656.2	387.7	665.1	401.9	674.4	416.6	684.1	431.7	694.4	447.2
80	703.0	397.1	711.8	412.1	721.1	427.4	730.8	443.1	741.0	459.2	751.8	475.9	763.0	493.0
	42°		43°		44°		45°		46°		47°		48°	
°	M	N	M	N	M	N	M	N	M	N	M	N	M	N
42	181.1	81.1												
43	184.0	84.0												
44	187.1	86.9	187.0	87.0										
45	190.3	90.0	193.4	93.3	196.6	96.6	200.0	100.0						
46	193.7	93.2	196.8	96.6	200.1	100.0	203.6	103.5	207.2	107.2				
47	197.3	96.6	200.5	100.0	203.8	103.6	207.4	107.2	211.1	111.0	215.0	115.0		
48	201.1	100.0	204.3	103.6	207.8	107.3	211.3	111.1	215.1	115.0	219.1	119.1	223.3	123.3
49	205.1	103.6	208.4	107.3	211.9	111.1	215.6	115.0	219.4	119.1	223.5	123.4	227.8	127.8
50	209.3	107.3	212.7	111.1	216.3	115.1	220.0	119.2	224.0	123.4	228.2	127.8	232.5	132.4
51	213.8	111.2	217.3	115.2	220.9	119.3	224.7	123.5	228.7	127.9	233.0	132.4	237.5	137.2
52	218.6	115.2	222.1	119.4	225.8	123.6	229.7	128.0	233.8	132.5	238.2	137.3	242.7	142.2
53	223.6	119.5	227.2	123.7	231.0	128.2	235.0	132.7	239.2	137.4	243.6	142.3	248.3	147.4
54	228.9	123.9	232.6	128.3	236.5	132.9	240.6	137.6	244.9	142.5	249.5	147.6	254.3	152.9
55	234.6	128.6	238.4	133.2	242.4	137.9	246.6	142.8	251.0	147.9	255.6	153.1	260.6	158.6
56	240.6	133.5	244.5	138.2	248.6	143.2	252.9	148.3	257.4	153.5	262.2	159.0	267.3	164.7
57	247.7	138.6	251.0	143.6	255.2	148.7	259.7	154.0	264.3	159.5	269.2	165.1	274.4	171.0
58	253.9	144.1	258.0	149.3	263.2	154.5	268.9	160.0	271.7	165.7	276.7	171.6	282.0	177.7
59	261.3	149.9	265.5	155.2	269.9	160.7	274.6	166.4	279.5	172.3	284.7	178.5	290.2	184.8
60	269.1	156.0	273.5	161.5	278.0	167.3	282.8	173.2	287.9	179.4	293.3	185.7	298.9	192.4
61	277.6	162.4	282.0	168.2	286.7	174.2	291.7	180.4	296.9	186.8	302.4	193.5	308.3	200.4

SPHERICAL TRAVERSE TABLE

°	42°		43°		44°		45°		46°		47°		48°	
	M	N	M	N	M	N	M	N	M	N	M	N	M	N
32	286.6	169.3	291.2	175.4	296.1	181.6	301.2	188.1	306.6	194.8	312.3	201.7	318.3	208.9
33	296.4	176.7	301.2	183.0	306.2	189.5	311.5	196.3	317.1	203.2	323.0	210.5	329.2	218.0
34	307.0	184.6	311.9	191.2	317.3	198.0	322.6	205.0	328.4	212.3	334.5	219.9	340.9	227.7
35	318.4	193.1	323.5	200.0	328.9	207.1	334.6	214.4	340.6	222.1	347.0	230.0	353.6	238.2
36	330.8	202.2	336.2	209.4	341.8	216.9	347.7	224.6	353.9	232.6	360.5	240.9	367.4	249.5
37	344.4	212.1	349.9	219.7	355.8	227.5	361.9	235.6	368.4	244.0	375.3	252.6	382.5	261.7
38	359.2	222.9	365.1	230.8	371.1	239.0	377.5	247.5	384.3	256.3	391.4	265.4	398.9	274.9
39	375.5	234.6	381.5	242.9	387.9	251.6	394.6	260.5	401.7	269.8	409.2	279.4	417.0	289.3
40	393.4	247.4	399.8	256.2	406.5	265.3	413.5	274.7	420.9	284.5	428.7	294.6	437.0	305.1
41	413.3	261.5	420.0	270.8	427.0	280.5	434.4	290.4	442.2	300.7	450.4	311.4	459.0	322.6
42	435.5	277.1	442.5	287.0	449.9	297.2	457.6	307.8	465.9	318.7	474.5	330.0	483.6	341.8
43	460.2	294.5	467.7	305.0	475.5	315.9	483.7	327.1	492.4	338.7	501.5	350.8	511.2	363.3
44	488.2	314.0	496.1	325.2	504.3	336.8	513.1	348.7	522.3	361.1	532.0	374.0	542.2	387.3
45	519.9	336.2	528.3	348.0	537.1	360.4	546.4	373.2	556.2	386.5	566.5	400.2	577.4	414.5
46	556.2	361.1	565.2	374.0	574.6	387.3	584.6	401.1	595.0	415.3	606.1	430.1	617.7	445.5
47	598.2	390.0	607.8	403.9	618.0	418.3	628.7	433.2	639.9	448.5	651.8	464.5	664.4	481.1
48	647.2	423.6	657.6	438.7	668.6	453.4	680.2	470.5	692.4	487.2	705.2	504.5	718.8	522.5
49	705.2	463.2	716.6	479.7	728.6	496.8	741.2	514.5	754.4	532.7	768.5	551.7	783.2	571.4
50	774.9	510.6	787.4	528.9	800.6	547.7	814.4	567.1	829.0	587.3	844.4	608.2	860.6	629.9
°	49°		50°		51°		52°		53°		54°		55°	
	M	N	M	N	M	N	M	N	M	N	M	N	M	N
49	232.3	132.3												
50	237.1	137.1	242.0	142.0										
51	242.2	142.1	247.2	147.2	252.5	152.5								
52	247.6	147.2	252.7	152.5	258.1	158.1	263.8	163.8						
53	253.3	152.7	258.5	158.2	264.0	163.9	269.9	169.9	276.1	176.1				
54	259.3	158.3	264.7	164.0	270.3	170.0	276.3	176.2	282.7	182.7	289.4	189.4		
55	265.7	164.3	271.2	170.2	277.0	176.4	283.2	182.8	289.7	189.5	296.6	196.6	304.0	204.0
56	272.6	170.5	278.2	176.7	284.2	183.1	290.5	189.8	297.2	196.7	304.2	204.1	311.8	211.7
57	279.9	177.1	285.6	183.5	291.8	190.2	298.2	197.1	305.1	204.3	312.4	211.9	320.1	219.9
58	287.6	184.1	293.6	190.7	299.9	197.6	306.5	204.8	313.6	212.4	321.0	220.3	329.0	228.5
59	296.0	191.5	302.1	198.3	308.5	205.5	315.4	213.0	322.6	220.9	330.3	229.1	338.5	237.7
60	304.9	199.2	311.1	206.4	317.8	213.9	324.9	221.7	332.3	229.9	340.3	238.4	348.7	247.4
61	314.4	207.5	320.9	215.0	327.8	222.8	335.0	230.9	342.7	239.4	350.9	248.3	359.6	257.6
62	324.7	216.4	331.4	224.1	338.5	232.3	346.0	240.7	353.9	249.6	362.4	258.9	371.3	268.6
63	335.7	225.8	342.7	233.9	350.0	242.4	357.8	251.2	366.0	260.4	374.7	270.1	384.0	280.3
64	347.7	235.9	354.9	244.3	362.5	253.2	370.5	262.4	379.1	272.1	388.1	282.2	397.7	292.8
65	360.7	246.7	368.1	255.6	376.0	264.8	384.3	274.5	393.2	284.6	402.6	295.2	412.5	306.3
66	374.8	258.4	382.5	267.7	390.6	277.4	399.3	287.5	408.5	298.1	418.3	309.1	418.9	320.8
67	390.1	271.0	398.2	280.8	406.6	290.9	415.7	301.5	425.3	312.6	435.4	324.3	446.2	336.4
68	406.9	284.7	415.3	295.2	424.1	305.6	433.6	316.8	443.6	328.5	454.2	340.7	465.4	353.5
69	425.3	299.7	434.1	310.5	443.3	321.7	453.2	333.4	463.7	345.7	474.7	358.6	486.5	372.0
70	445.7	316.1	454.9	327.2	464.6	339.3	474.9	351.7	485.8	364.6	497.4	378.2	509.8	392.4
71	468.2	334.1	477.8	346.1	488.1	358.6	498.9	371.7	510.4	385.4	522.6	399.7	535.5	414.8
72	493.3	354.0	503.4	366.8	514.2	380.1	525.6	393.9	537.7	408.4	550.6	423.6	564.2	439.5
73	521.3	376.3	531.1	389.8	543.5	403.9	555.5	418.6	568.3	434.1	581.9	450.2	596.3	467.1
74	553.0	401.2	564.4	415.6	576.5	430.7	589.3	446.4	602.8	462.8	617.2	480.0	632.5	498.0
75	588.9	429.3	601.1	444.8	613.9	460.9	627.6	477.7	642.0	495.3	657.3	513.7	673.6	533.0
76	630.1	461.4	643.1	478.0	656.8	495.3	671.4	513.4	686.8	532.3	703.2	552.0	720.7	572.8
77	677.6	498.3	691.6	516.2	706.4	534.9	722.1	554.4	738.7	574.8	756.3	596.2	775.0	618.6
78	733.1	541.2	748.3	560.7	764.3	581.0	781.2	602.2	799.2	624.3	818.3	647.5	838.6	671.5
79	798.8	591.8	815.3	613.1	832.8	635.3	851.3	658.5	870.8	682.7	891.6	708.1	913.7	734.7
80	877.8	652.4	895.9	675.9	915.1	700.3	935.4	725.9	956.0	752.6	979.7	780.6	1004	809.9

SPHERICAL TRAVERSE TABLE

°	56°		57°		58°		59°		60°		61°		62°	
	M	N	M	N	M	N	M	N	M	N	M	N	M	N
56	319.8	219.8												
57	328.3	228.3	337.1	237.2										
58	337.5	237.3	346.5	246.4	356.1	256.1								
59	347.2	246.7	356.5	256.3	366.4	266.3	377.0	277.0						
60	357.7	256.8	367.2	266.1	377.4	277.2	383.3	288.3	400.0	300.0				
61	368.9	267.5	378.7	277.8	389.5	288.7	400.5	300.2	412.5	312.5	425.5	325.5		
62	380.9	278.8	391.1	289.6	402.0	301.0	413.6	313.0	426.0	325.8	439.4	339.3	453.7	353.7
63	393.9	291.0	404.4	302.2	415.7	314.1	427.7	326.6	440.5	339.9	454.3	354.1	469.2	369.1
64	407.9	303.9	418.8	315.7	430.5	328.1	442.9	341.2	456.2	355.1	470.5	36.9	485.9	385.6
65	423.1	317.9	434.0	330.2	446.5	343.2	459.4	356.9	473.2	371.4	488.1	386.9	504.0	403.3
66	439.7	333.0	451.4	345.9	464.0	359.4	477.4	373.8	491.7	389.0	507.1	405.2	523.7	422.4
67	457.7	349.3	469.9	362.8	483.0	377.0	496.9	392.1	511.9	398.8	527.9	425.0	545.1	443.1
68	477.4	366.9	490.1	381.1	503.7	396.1	518.3	411.9	533.9	428.7	550.6	446.5	568.6	465.5
69	499.0	386.2	512.3	401.1	526.6	416.9	541.8	433.6	558.1	451.2	575.6	470.0	594.4	489.9
70	522.9	407.3	536.8	423.1	551.7	429.7	567.7	457.3	584.8	475.9	603.1	495.7	622.8	516.7
71	549.3	430.6	564.0	447.2	579.6	464.8	596.4	483.3	614.3	503.0	633.6	523.9	654.3	546.2
72	578.7	456.3	594.2	473.9	610.7	492.5	628.3	512.2	647.2	533.1	667.5	555.2	689.3	578.8
73	611.6	484.9	628.0	503.7	645.4	523.4	664.1	544.4	684.1	566.7	705.5	590.1	728.5	615.2
74	648.8	517.0	666.1	537.0	684.6	558.1	704.4	580.5	725.6	604.0	748.3	629.1	772.8	655.9
75	690.9	553.3	709.4	574.7	729.1	597.3	756.2	621.1	772.7	646.4	796.9	673.3	823.0	701.9
76	739.2	594.6	758.9	617.6	780.0	641.9	802.6	667.5	826.7	694.7	852.6	723.6	880.5	754.3
77	795.0	642.2	816.2	667.0	838.9	693.2	863.1	720.9	889.1	750.2	916.9	781.4	946.9	814.6
78	860.1	697.5	883.1	724.5	907.6	752.9	933.9	783.0	961.9	814.9	992.1	848.8	1024	884.8
79	937.2	762.7	962.3	792.2	989.0	823.3	1018	856.2	1048	891.1	1081	928.1	1116	967.6
80	1030	840.8	1057	873.3	1087	907.6	1118	943.9	1152	982.3	1188	1023	1227	1067
°	63°		64°		65°		66°		67°		68°		69°	
	M	N	M	N	M	N	M	N	M	N	M	N	M	N
63	485.2	385.2												
64	502.5	402.4	520.4	420.4										
65	521.2	420.9	539.8	439.7	559.9	459.9								
66	541.6	440.8	560.9	460.5	581.8	481.7	604.5	504.5						
67	563.7	462.4	583.8	483.0	605.6	505.2	629.2	529.1	655.0	555.0				
68	588.0	485.8	608.9	507.5	631.6	530.8	656.3	555.9	683.2	583.1	712.6	612.6		
69	614.6	511.3	636.5	534.1	660.3	558.7	686.1	595.1	714.2	613.7	744.9	644.8	778.6	678.6
70	644.0	539.2	667.0	563.3	691.8	589.2	718.9	617.1	748.3	647.3	780.5	680.0	815.9	715.7
71	676.6	570.0	700.7	595.4	726.8	622.8	755.2	653.3	786.1	684.2	819.9	718.8	857.1	756.6
72	712.8	604.0	738.2	631.0	765.7	660.0	795.6	691.3	828.2	725.1	863.9	761.7	903.0	801.8
73	753.4	641.9	780.2	670.6	809.3	701.4	840.9	734.6	875.3	770.6	913.0	809.6	954.4	852.1
74	799.1	684.4	827.6	715.0	858.4	747.9	892.0	783.3	928.5	821.6	968.5	863.2	1002	908.5
75	851.0	732.5	881.4	765.2	914.2	800.4	949.9	838.2	988.8	879.2	1031	923.7	1078	972.2
76	910.5	787.2	942.9	832.3	978.1	860.1	1016	900.8	1058	944.9	1103	992.7	1153	1045
77	979.2	850.1	1014	888.1	1052	928.9	1093	972.9	1138	1020	1187	1072	1241	1128
78	1059	923.3	1097	964.6	1087	1009	1183	1057	1231	1108	1284	1164	1342	1226
79	1154	1010	1196	1055	1240	1103	1288	1155	1341	1212	1399	1273	1462	1340
80	1268	1113	1314	1163	1363	1216	1416	1274	1474	1336	1537	1404	1607	1477
°	70°		71°		72°		73°		74°		75°		76°	
	M	N	M	N	M	N	M	N	M	N	M	N	M	N
70	854.9	754.9												
71	898.1	797.9	943.5	843.5										
72	946.2	845.6	994.0	893.8	1047	947.2								
73	1000	898.6	1051	949.9	1107	1008	1170	1070						
74	1061	958.1	1114	1013	1174	1073	1241	1141	1316	1216				
75	1130	1025	1187	1084	1250	1149	1321	1221	1402	1301	1493	1394		
76	1209	1102	1270	1165	1338	1234	1414	1312	1500	1399	1597	1497	1709	1609
77	1300	1190	1366	1258	1439	1333	1520	1417	1613	1511	1718	1617	1838	1737
78	1406	1293	1477	1366	1556	1448	1645	1539	1745	1641	1858	1756	1988	1887
79	1532	1413	1610	1494	1696	1583	1793	1683	1901	1794	2025	1920	2116	2063
80	1684	1558	1769	1647	1864	1745	1970	1856	2089	1978	2225	2117	2380	2275

TABLE 6

533

MERIDIONAL PARTS

LATITUDE

	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°	16°	17°	18°
0	0	60	120	180	240	300	361	421	482	542	603	664	725	787	848	910	973	1035	1098
1	1	61	121	181	241	301	362	422	483	543	604	665	726	788	850	911	974	1036	1099
2	2	62	122	182	242	302	363	423	484	544	605	666	727	789	851	913	975	1037	1100
3	3	63	123	183	243	303	364	424	485	545	606	667	728	790	852	914	976	1038	1101
4	4	64	124	184	244	304	365	425	486	546	607	668	729	791	853	915	977	1039	1102
5	5	65	125	185	245	305	366	426	487	547	608	669	730	792	854	916	978	1041	1103
6	6	66	126	186	246	306	367	427	488	548	609	670	731	793	855	917	979	1042	1105
7	7	67	127	187	247	307	368	428	489	549	610	671	732	794	856	918	980	1043	1106
8	8	68	128	188	248	308	369	429	490	550	611	672	733	795	857	919	981	1044	1107
9	9	69	129	189	249	309	370	430	491	551	612	673	735	796	858	920	982	1045	1108
10	10	70	130	190	250	310	371	431	492	552	613	674	736	797	859	921	983	1046	1109
11	11	71	131	191	251	311	372	432	493	553	614	675	737	798	860	922	984	1047	1110
12	12	72	132	192	252	312	373	433	494	554	615	676	738	799	861	923	985	1048	1111
13	13	73	133	193	253	313	374	434	495	555	616	677	739	800	862	924	986	1049	1112
14	14	74	134	194	254	314	375	435	496	556	617	678	740	801	863	925	987	1050	1113
15	15	75	135	195	255	315	376	436	497	557	618	679	741	802	864	926	988	1051	1114
16	16	76	136	196	256	316	377	437	498	558	619	680	742	803	865	927	989	1052	1115
17	17	77	137	197	257	317	378	438	499	559	620	681	743	804	866	928	990	1053	1116
18	18	78	138	198	258	318	379	439	500	560	621	682	744	805	867	929	991	1054	1117
19	19	79	139	199	259	319	380	440	501	561	622	683	745	806	868	930	993	1055	1118
20	20	80	140	200	260	320	381	441	502	562	623	684	746	807	869	931	994	1056	1119
21	21	81	141	201	261	321	382	442	503	563	624	685	747	808	870	932	995	1057	1120
22	22	82	142	202	262	322	383	443	504	564	625	686	748	809	871	933	996	1058	1121
23	23	83	143	203	263	323	384	444	505	565	626	687	749	810	872	934	997	1059	1122
24	24	84	144	204	264	324	385	445	506	566	627	688	750	811	873	935	998	1060	1123
25	25	85	145	205	265	325	386	446	507	567	628	689	751	812	874	936	999	1061	1125
26	26	86	146	206	266	326	387	447	508	568	629	690	752	813	875	937	1000	1063	1126
27	27	87	147	207	267	327	388	448	509	570	631	692	753	815	876	938	1001	1064	1127
28	28	88	148	208	268	328	389	449	510	571	632	693	754	816	877	939	1002	1065	1128
29	29	89	149	209	269	330	390	450	511	572	633	694	755	817	878	941	1003	1066	1129
30	30	90	150	210	270	331	391	451	512	573	634	695	756	818	879	942	1004	1067	1130
31	31	91	151	211	271	332	392	452	513	574	635	696	757	819	880	943	1005	1068	1131
32	32	92	152	212	272	333	393	453	514	575	636	697	758	820	881	944	1006	1069	1132
33	33	93	153	213	273	334	394	454	515	576	637	698	759	821	883	945	1007	1070	1133
34	34	94	154	214	274	335	395	455	516	577	638	699	760	822	884	946	1008	1071	1134
35	35	95	155	215	275	336	396	456	517	578	639	700	761	823	885	947	1009	1072	1135
36	36	96	156	216	276	337	397	457	518	579	640	701	762	824	886	948	1010	1073	1136
37	37	97	157	217	277	338	398	458	519	580	641	702	763	825	887	949	1011	1074	1137
38	38	98	158	218	278	339	399	459	520	581	642	703	764	826	888	950	1012	1075	1138
39	39	99	159	219	279	340	400	460	521	582	643	704	765	827	889	951	1013	1076	1139
40	40	100	160	220	280	341	401	461	522	583	644	705	766	828	890	952	1014	1077	1140
41	41	101	161	221	281	342	402	462	523	584	645	706	767	829	891	953	1015	1078	1141
42	42	102	162	222	282	343	403	463	524	585	646	707	768	830	892	954	1016	1079	1142
43	43	103	163	223	283	344	404	464	525	586	647	708	769	831	893	955	1018	1080	1144
44	44	104	164	224	284	345	405	465	526	587	648	709	770	832	894	956	1019	1081	1145
45	45	105	165	225	285	346	406	466	527	588	649	710	771	833	895	957	1020	1082	1146
46	46	106	166	226	286	347	407	467	528	589	650	711	772	834	896	958	1021	1084	1147
47	47	107	167	227	287	348	408	468	529	590	651	712	773	835	897	959	1022	1085	1148
48	48	108	168	228	288	349	409	469	530	591	652	713	774	836	898	960	1023	1086	1149
49	49	109	169	229	289	350	410	470	531	592	653	714	775	837	899	961	1024	1087	1150
50	50	110	170	230	290	351	411	471	532	593	654	715	777	838	900	962	1025	1088	1151
51	51	111	171	231	291	352	412	472	533	594	655	716	778	839	901	963	1026	1089	1152
52	52	112	172	232	292	353	413	473	534	595	656	717	779	840	902	964	1027	1090	1153
53	53	113	173	233	293	354	414	474	535	596	657	718	780	841	903	965	1028	1091	1154
54	54	114	174	234	294	355	415	475	536	597	658	719	781	842	904	966	1029	1092	1155
55	55	115	175	235	295	356	416	476	537	598	659	720	782	843	905	967	1030	1093	1156
56	56	116	176	236	296	357	417	477	538	599	660	721	783	844	906	969	1031	1094	1157
57	57	117	177	237	297	358	418	478	539	600	661	722	784	845	907	970	1032	1095	1158
58	58	118	178	238	298	359	419	480	540	601	662	723	785	846	908	971	1033	1096	1159
59	59	119	179	239	299	360	420	481	541	602	663	724	786	847	909	972	1034	1097	1160
	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°	16°	17°	18°

MERIDIONAL PARTS

LATITUDE															
	19°	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	30°	31°	32°	33°
0	1161	1225	1289	1354	1419	1484	1550	1616	1684	1751	1819	1888	1958	2028	2100
1	1163	1226	1290	1355	1420	1485	1551	1618	1685	1752	1821	1890	1959	2030	2101
2	1164	1227	1291	1356	1421	1486	1552	1619	1686	1753	1822	1891	1960	2031	2102
3	1165	1228	1292	1357	1422	1487	1553	1620	1687	1755	1823	1892	1962	2032	2103
4	1166	1229	1293	1358	1423	1488	1554	1621	1688	1756	1824	1893	1963	2033	2104
5	1167	1230	1295	1359	1424	1490	1556	1622	1689	1757	1825	1894	1964	2034	2105
6	1168	1232	1296	1360	1425	1491	1557	1623	1690	1758	1826	1895	1965	2035	2107
7	1169	1233	1297	1361	1426	1492	1558	1624	1691	1759	1827	1896	1966	2037	2108
8	1170	1234	1298	1362	1427	1493	1559	1625	1693	1760	1829	1898	1967	2038	2109
9	1171	1235	1299	1363	1428	1494	1560	1626	1694	1761	1830	1899	1969	2039	2110
10	1172	1236	1300	1364	1430	1495	1561	1628	1695	1762	1831	1900	1970	2040	2111
11	1173	1237	1301	1366	1431	1496	1562	1629	1696	1764	1832	1901	1971	2041	2113
12	1174	1238	1302	1367	1432	1497	1563	1630	1697	1765	1833	1902	1972	2043	2114
13	1175	1239	1303	1368	1433	1498	1564	1631	1698	1766	1834	1903	1973	2044	2115
14	1176	1240	1304	1369	1434	1499	1565	1632	1699	1767	1835	1905	1974	2045	2116
15	1177	1241	1305	1370	1435	1500	1567	1633	1700	1768	1837	1906	1976	2046	2117
16	1178	1242	1306	1371	1436	1502	1568	1634	1701	1769	1838	1907	1977	2047	2119
17	1179	1243	1307	1372	1437	1503	1569	1635	1703	1770	1839	1908	1978	2048	2120
18	1181	1244	1308	1373	1438	1504	1570	1637	1704	1772	1840	1909	1979	2050	2121
19	1182	1245	1310	1374	1439	1505	1571	1638	1705	1773	1841	1910	1980	2051	2122
20	1183	1246	1311	1375	1440	1506	1572	1639	1706	1774	1842	1912	1981	2052	2123
21	1184	1248	1312	1376	1441	1507	1573	1640	1707	1775	1843	1913	1983	2053	2125
22	1185	1249	1313	1377	1443	1508	1574	1641	1708	1776	1845	1914	1984	2054	2126
23	1186	1250	1314	1379	1444	1509	1575	1642	1709	1777	1846	1915	1985	2056	2127
24	1187	1251	1315	1380	1445	1510	1577	1643	1711	1778	1847	1916	1986	2057	2128
25	1188	1252	1316	1381	1446	1511	1578	1644	1712	1780	1848	1917	1987	2058	2129
26	1189	1253	1317	1382	1447	1513	1579	1645	1713	1781	1849	1918	1988	2059	2131
27	1190	1254	1318	1383	1448	1514	1580	1647	1714	1782	1850	1920	1990	2060	2132
28	1191	1255	1319	1384	1449	1515	1581	1648	1715	1783	1852	1921	1991	2061	2133
29	1192	1256	1320	1385	1450	1516	1582	1649	1716	1784	1853	1922	1992	2063	2134
30	1193	1257	1321	1386	1451	1517	1583	1650	1717	1785	1854	1923	1993	2064	2135
31	1194	1258	1322	1387	1452	1518	1584	1651	1718	1786	1855	1924	1994	2065	2137
32	1195	1259	1324	1388	1453	1519	1585	1652	1720	1787	1856	1925	1995	2066	2138
33	1196	1260	1325	1389	1455	1520	1586	1653	1721	1789	1857	1927	1997	2067	2139
34	1198	1261	1326	1390	1456	1521	1588	1654	1722	1790	1858	1928	1998	2069	2140
35	1199	1262	1327	1392	1457	1522	1589	1656	1723	1791	1860	1929	1999	2070	2141
36	1200	1264	1328	1393	1458	1524	1590	1657	1724	1792	1861	1930	2000	2071	2143
37	1201	1265	1329	1394	1459	1525	1591	1658	1725	1793	1862	1931	2001	2072	2144
38	1202	1266	1330	1395	1460	1526	1592	1659	1726	1794	1863	1932	2002	2073	2145
39	1203	1267	1331	1396	1461	1527	1593	1660	1727	1795	1864	1934	2004	2075	2146
40	1204	1268	1332	1397	1462	1528	1594	1661	1729	1797	1865	1935	2005	2076	2147
41	1205	1269	1333	1398	1463	1529	1595	1662	1730	1798	1866	1936	2006	2077	2149
42	1206	1270	1334	1399	1464	1530	1596	1663	1731	1799	1868	1937	2007	2078	2150
43	1207	1271	1335	1400	1465	1531	1598	1664	1732	1800	1869	1938	2008	2079	2151
44	1208	1272	1336	1401	1467	1532	1599	1666	1733	1801	1870	1939	2010	2080	2152
45	1209	1273	1338	1402	1468	1533	1600	1667	1734	1802	1871	1941	2011	2082	2153
46	1210	1274	1339	1403	1469	1535	1601	1668	1735	1803	1872	1942	2012	2083	2155
47	1211	1275	1340	1405	1470	1536	1602	1669	1736	1805	1873	1943	2013	2084	2156
48	1212	1276	1341	1406	1471	1537	1603	1670	1738	1806	1875	1944	2014	2085	2157
49	1213	1277	1342	1407	1472	1538	1604	1671	1739	1807	1876	1945	2015	2086	2158
50	1215	1278	1343	1408	1473	1539	1605	1672	1740	1808	1877	1946	2017	2088	2159
51	1216	1280	1344	1409	1474	1540	1606	1673	1741	1809	1878	1948	2018	2089	2161
52	1217	1281	1345	1410	1475	1541	1608	1675	1742	1810	1879	1949	2019	2090	2162
53	1218	1282	1346	1411	1476	1542	1609	1676	1743	1811	1880	1950	2020	2091	2163
54	1219	1283	1347	1412	1477	1543	1610	1677	1744	1813	1881	1951	2021	2092	2164
55	1220	1284	1348	1413	1479	1544	1611	1678	1746	1814	1883	1952	2022	2094	2165
56	1221	1285	1349	1414	1480	1546	1612	1679	1747	1815	1884	1953	2024	2095	2167
57	1222	1286	1350	1415	1481	1547	1613	1680	1748	1816	1885	1955	2025	2096	2168
58	1223	1287	1352	1416	1482	1548	1614	1681	1749	1817	1886	1956	2026	2097	2169
59	1224	1288	1353	1418	1483	1549	1615	1682	1750	1818	1887	1957	2027	2098	2170
	19°	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	30°	31°	32°	33°

TABLE 6.

535

MERIDIONAL PARTS

LATITUDE															
	34°	35°	36°	37°	38°	39°	40°	41°	42°	43°	44°	45°	46°	47°	48°
0	2171	2244	2318	2393	2468	2545	2623	2702	2782	2863	2946	3030	3116	3203	3292
1	2173	2246	2319	2394	2470	2546	2624	2703	2783	2864	2947	3031	3117	3204	3293
2	2174	2247	2320	2395	2471	2548	2625	2704	2784	2866	2949	3033	3118	3206	3295
3	2175	2248	2322	2396	2472	2549	2627	2706	2786	2867	2950	3034	3120	3207	3296
4	2176	2249	2323	2398	2473	2550	2628	2707	2787	2869	2951	3036	3121	3209	3298
5	2178	2250	2324	2399	2475	2551	2629	2708	2788	2870	2953	3037	3123	3210	3299
6	2179	2252	2325	2400	2476	2552	2631	2710	2790	2871	2954	3038	3124	3212	3301
7	2180	2253	2327	2401	2477	2554	2632	2711	2791	2873	2956	3040	3126	3213	3302
8	2181	2254	2328	2403	2478	2555	2633	2712	2792	2874	2957	3041	3127	3214	3303
9	2182	2255	2329	2404	2480	2557	2634	2714	2794	2875	2958	3043	3129	3216	3305
10	2184	2257	2330	2405	2481	2558	2636	2715	2795	2877	2960	3044	3130	3217	3306
11	2185	2258	2332	2406	2482	2559	2637	2716	2797	2878	2961	3046	3131	3219	3308
12	2186	2259	2333	2408	2484	2560	2638	2718	2798	2880	2963	3047	3133	3220	3309
13	2187	2260	2334	2409	2485	2562	2640	2719	2799	2881	2964	3048	3134	3222	3311
14	2188	2261	2335	2410	2486	2563	2641	2720	2801	2882	2965	3050	3136	3223	3312
15	2190	2263	2337	2411	2487	2564	2642	2722	2802	2884	2967	3051	3137	3225	3314
16	2191	2264	2338	2413	2489	2566	2644	2723	2803	2885	2968	3053	3139	3226	3316
17	2192	2265	2339	2414	2490	2567	2645	2724	2805	2886	2970	3054	3140	3228	3317
18	2193	2266	2340	2415	2491	2568	2646	2726	2806	2888	2971	3055	3142	3229	3319
19	2194	2268	2342	2416	2492	2569	2648	2727	2807	2889	2972	3057	3143	3231	3320
20	2196	2269	2343	2418	2494	2571	2649	2728	2809	2891	2974	3058	3144	3232	3322
21	2197	2270	2344	2419	2495	2572	2650	2729	2810	2892	2975	3060	3146	3234	3323
22	2198	2271	2345	2420	2496	2573	2651	2731	2811	2893	2976	3061	3147	3235	3325
23	2199	2272	2346	2422	2498	2575	2653	2732	2813	2895	2978	3063	3149	3237	3326
24	2200	2274	2348	2423	2499	2576	2654	2733	2814	2896	2979	3064	3150	3238	3328
25	2202	2275	2349	2424	2500	2577	2655	2735	2815	2897	2981	3065	3152	3240	3329
26	2203	2276	2350	2425	2501	2578	2657	2736	2817	2899	2982	3067	3153	3241	3331
27	2204	2277	2351	2427	2503	2580	2658	2737	2818	2900	2983	3068	3155	3242	3332
28	2205	2279	2353	2428	2504	2581	2659	2739	2820	2902	2985	3070	3156	3244	3334
29	2207	2280	2354	2429	2505	2582	2661	2740	2821	2903	2986	3071	3157	3245	3335
30	2208	2281	2355	2430	2506	2584	2662	2742	2822	2904	2988	3073	3159	3247	3337
31	2209	2282	2356	2432	2508	2585	2663	2743	2824	2906	2989	3074	3160	3248	3338
32	2210	2283	2358	2433	2509	2586	2665	2744	2825	2907	2991	3075	3162	3250	3340
33	2211	2285	2359	2434	2510	2588	2666	2746	2826	2908	2992	3077	3163	3251	3341
34	2213	2286	2360	2435	2512	2589	2667	2747	2828	2910	2993	3078	3165	3253	3343
35	2214	2287	2361	2437	2513	2590	2669	2748	2829	2911	2995	3080	3166	3254	3344
36	2215	2288	2362	2438	2514	2591	2670	2750	2830	2913	2996	3081	3168	3256	3346
37	2216	2290	2364	2439	2515	2593	2671	2751	2832	2914	2998	3083	3169	3257	3347
38	2217	2291	2365	2440	2517	2594	2673	2752	2833	2915	2999	3084	3171	3259	3349
39	2219	2292	2366	2442	2518	2595	2674	2754	2834	2917	3000	3085	3172	3260	3350
40	2220	2293	2368	2443	2519	2597	2675	2755	2836	2918	3002	3087	3173	3262	3352
41	2221	2295	2369	2444	2521	2598	2676	2756	2837	2919	3003	3088	3175	3263	3353
42	2222	2296	2370	2445	2522	2599	2678	2758	2839	2921	3005	3090	3176	3265	3355
43	2224	2297	2371	2447	2523	2601	2679	2759	2840	2922	3006	3091	3178	3266	3356
44	2225	2298	2373	2448	2524	2602	2680	2760	2841	2924	3007	3093	3179	3268	3358
45	2226	2299	2374	2449	2526	2603	2682	2762	2843	2925	3009	3094	3181	3269	3359
46	2227	2301	2375	2451	2527	2604	2683	2763	2844	2926	3010	3095	3182	3271	3361
47	2228	2302	2376	2452	2528	2606	2684	2764	2845	2928	3012	3097	3184	3272	3362
48	2230	2303	2378	2453	2530	2607	2686	2766	2847	2929	3013	3098	3185	3274	3364
49	2231	2304	2379	2454	2531	2608	2687	2767	2848	2931	3014	3100	3187	3275	3365
50	2232	2306	2380	2456	2532	2610	2688	2768	2849	2932	3016	3101	3188	3277	3367
51	2233	2307	2381	2457	2533	2611	2690	2770	2851	2933	3017	3103	3190	3278	3368
52	2235	2308	2383	2458	2535	2612	2691	2771	2852	2935	3019	3104	3191	3280	3370
53	2236	2309	2384	2459	2536	2614	2692	2772	2854	2936	3020	3105	3192	3281	3371
54	2237	2311	2385	2461	2537	2615	2694	2774	2855	2937	3021	3107	3194	3283	3373
55	2238	2312	2386	2462	2538	2616	2695	2775	2856	2939	3023	3108	3195	3284	3374
56	2239	2313	2388	2463	2540	2617	2696	2776	2858	2940	3024	3110	3197	3286	3376
57	2241	2314	2389	2464	2541	2619	2698	2778	2859	2942	3026	3111	3198	3287	3378
58	2242	2316	2390	2466	2542	2620	2699	2779	2860	2943	3027	3113	3200	3289	3379
59	2243	2317	2391	2467	2544	2621	2700	2780	2862	2944	3029	3114	3201	3290	3381
	34°	35°	36°	37°	38°	39°	40°	41°	42°	43°	44°	45°	46°	47°	48°

MERIDIONAL PARTS

LATITUDE															
	49°	50°	51°	52°	53°	54°	55°	56°	57°	58°	59°	60°	61°	62°	63°
0	3382	3474	3569	3665	3764	3865	3968	4074	4183	4294	4409	4527	4649	4775	4905
1	3384	3476	3570	3667	3765	3866	3970	4076	4184	4296	4411	4529	4651	4777	4907
2	3385	3478	3572	3668	3767	3868	3971	4077	4186	4298	4413	4531	4653	4779	4909
3	3387	3479	3574	3670	3769	3870	3973	4079	4188	4300	4415	4533	4655	4781	4912
4	3388	3481	3575	3672	3770	3871	3975	4081	4190	4302	4417	4535	4657	4784	4914
5	3390	3482	3577	3673	3772	3873	3977	4083	4192	4304	4419	4537	4660	4786	4916
6	3391	3484	3578	3675	3774	3875	3978	4085	4194	4306	4421	4539	4662	4788	4918
7	3393	3485	3580	3677	3775	3877	3980	4086	4195	4308	4423	4541	4664	4790	4920
8	3394	3487	3582	3678	3777	3878	3982	4088	4197	4309	4425	4543	4666	4792	4923
9	3396	3488	3583	3680	3779	3880	3984	4090	4199	4311	4427	4545	4668	4794	4925
10	3397	3490	3585	3681	3780	3882	3985	4092	4201	4313	4429	4547	4670	4796	4927
11	3399	3492	3586	3683	3782	3883	3987	4094	4203	4315	4431	4549	4672	4798	4929
12	3400	3493	3588	3685	3784	3885	3989	4095	4205	4317	4433	4551	4674	4801	4931
13	3402	3495	3590	3686	3785	3887	3991	4097	4207	4319	4434	4553	4676	4803	4934
14	3403	3496	3591	3688	3787	3889	3992	4099	4208	4321	4436	4555	4678	4805	4936
15	3405	3498	3593	3690	3789	3890	3994	4101	4210	4323	4438	4557	4680	4807	4938
16	3407	3499	3594	3691	3790	3892	3996	4103	4212	4325	4440	4559	4682	4809	4940
17	3408	3501	3596	3693	3792	3894	3998	4104	4214	4327	4442	4562	4684	4811	4943
18	3410	3503	3598	3695	3794	3895	3999	4106	4216	4328	4444	4564	4687	4814	4945
19	3411	3504	3599	3696	3795	3897	4001	4108	4218	4330	4446	4566	4689	4816	4947
20	3413	3506	3601	3698	3797	3899	4003	4110	4220	4332	4448	4568	4691	4818	4949
21	3414	3507	3602	3699	3799	3901	4005	4112	4221	4334	4450	4570	4693	4820	4951
22	3416	3509	3604	3701	3800	3902	4006	4113	4223	4336	4452	4572	4695	4822	4954
23	3417	3510	3606	3703	3802	3904	4008	4115	4225	4338	4454	4574	4697	4824	4956
24	3419	3512	3607	3704	3804	3906	4010	4117	4227	4340	4456	4576	4699	4826	4958
25	3420	3514	3609	3706	3806	3907	4012	4119	4229	4342	4458	4578	4701	4829	4960
26	3422	3515	3610	3708	3807	3909	4014	4121	4231	4344	4460	4580	4703	4831	4963
27	3423	3517	3612	3709	3809	3911	4015	4122	4232	4346	4462	4582	4705	4833	4965
28	3425	3518	3614	3711	3811	3913	4017	4124	4234	4347	4464	4584	4707	4835	4967
29	3427	3520	3615	3713	3812	3914	4019	4126	4236	4349	4466	4586	4710	4837	4969
30	3428	3521	3617	3714	3814	3916	4021	4128	4238	4351	4468	4588	4712	4839	4972
31	3430	3523	3618	3716	3816	3918	4022	4130	4240	4353	4470	4590	4714	4842	4974
32	3431	3525	3620	3717	3817	3919	4024	4132	4242	4355	4472	4592	4716	4844	4976
33	3433	3526	3622	3719	3819	3921	4026	4133	4244	4357	4474	4594	4718	4846	4978
34	3434	3528	3623	3721	3821	3923	4028	4135	4246	4359	4476	4596	4720	4848	4981
35	3436	3529	3625	3722	3822	3925	4029	4137	4247	4361	4478	4598	4722	4850	4983
36	3437	3531	3626	3724	3824	3926	4031	4139	4249	4363	4480	4600	4724	4852	4985
37	3439	3532	3628	3726	3826	3928	4033	4141	4251	4365	4482	4602	4726	4855	4987
38	3440	3534	3630	3727	3827	3930	4035	4142	4253	4367	4484	4604	4728	4857	4990
39	3442	3536	3631	3729	3829	3932	4037	4144	4255	4369	4486	4606	4731	4859	4992
40	3443	3537	3633	3731	3831	3933	4038	4146	4257	4370	4488	4608	4733	4861	4994
41	3445	3539	3634	3732	3832	3935	4040	4148	4259	4372	4490	4610	4735	4863	4996
42	3447	3540	3636	3734	3834	3937	4042	4150	4260	4374	4492	4612	4737	4865	4999
43	3448	3542	3638	3736	3836	3938	4044	4152	4262	4376	4494	4614	4739	4868	5001
44	3450	3543	3639	3737	3838	3940	4045	4153	4264	4378	4495	4616	4741	4870	5003
45	3451	3545	3641	3739	3839	3942	4047	4155	4266	4380	4497	4618	4743	4872	5005
46	3453	3547	3643	3741	3841	3944	4049	4157	4268	4382	4499	4620	4745	4874	5008
47	3454	3548	3644	3742	3843	3945	4051	4159	4270	4384	4501	4623	4747	4876	5010
48	3456	3550	3646	3744	3844	3947	4052	4161	4272	4386	4503	4625	4750	4879	5012
49	3457	3551	3647	3746	3846	3949	4054	4162	4274	4388	4505	4627	4752	4881	5014
50	3459	3553	3649	3747	3848	3951	4056	4164	4275	4390	4507	4629	4754	4883	5017
51	3460	3555	3651	3748	3849	3952	4058	4166	4277	4392	4509	4631	4756	4885	5019
52	3462	3556	3652	3750	3851	3954	4060	4168	4279	4394	4511	4633	4758	4887	5021
53	3464	3558	3654	3752	3853	3956	4061	4170	4281	4396	4513	4635	4760	4890	5023
54	3465	3559	3655	3754	3854	3958	4063	4172	4283	4398	4515	4637	4762	4892	5026
55	3467	3561	3657	3755	3856	3959	4065	4173	4285	4399	4517	4639	4764	4894	5028
56	3468	3562	3659	3757	3858	3961	4067	4175	4287	4401	4519	4641	4766	4896	5030
57	3470	3564	3660	3759	3860	3963	4069	4177	4289	4403	4521	4643	4769	4898	5033
58	3471	3566	3662	3760	3861	3964	4070	4179	4291	4405	4523	4645	4771	4901	5035
59	3473	3567	3664	3762	3863	3966	4072	4181	4292	4407	4525	4647	4773	4903	5037
	49°	50°	51°	52°	53°	54°	55°	56°	57°	58°	59°	60°	61°	62°	63°

MERIDIONAL PARTS

LATITUDE

	64°	65°	66°	67°	68°	69°	70°	71°	72°	73°	74°	75°	76°	77°	78°
0	5039	5179	5324	5474	5631	5795	5966	6146	6335	6534	6746	6970	7210	7467	7745
1	5042	5181	5326	5477	5633	5797	5969	6149	6338	6538	6749	6974	7214	7472	7749
2	5044	5184	5328	5479	5636	5800	5972	6152	6341	6541	6753	6978	7218	7476	7754
3	5046	5186	5331	5482	5639	5803	5975	6155	6345	6545	6757	6982	7222	7481	7759
4	5049	5188	5333	5484	5642	5806	5978	6158	6348	6548	6760	6986	7227	7485	7764
5	5051	5191	5336	5487	5644	5809	5981	6161	6351	6552	6764	6990	7231	7490	7769
6	5053	5193	5338	5489	5647	5811	5984	6164	6354	6555	6768	6994	7235	7494	7774
7	5055	5195	5341	5492	5650	5814	5986	6167	6358	6558	6771	6997	7239	7498	7778
8	5058	5198	5343	5495	5652	5817	5989	6170	6361	6562	6775	7001	7243	7503	7783
9	5060	5200	5346	5497	5655	5820	5992	6173	6364	6565	6779	7005	7247	7507	7788
10	5062	5203	5348	5500	5658	5823	5995	6177	6367	6569	6782	7009	7252	7512	7793
11	5065	5205	5351	5502	5660	5825	5998	6180	6371	6572	6786	7013	7256	7516	7798
12	5067	5207	5353	5505	5663	5828	6001	6183	6374	6576	6790	7017	7260	7521	7803
13	5069	5210	5356	5507	5666	5831	6004	6186	6377	6579	6793	7021	7264	7525	7808
14	5071	5212	5358	5510	5668	5834	6007	6189	6380	6583	6797	7025	7268	7530	7813
15	5074	5214	5361	5513	5671	5837	6010	6192	6384	6586	6801	7029	7273	7535	7817
16	5076	5217	5363	5515	5674	5840	6013	6195	6387	6590	6804	7033	7277	7539	7822
17	5078	5219	5366	5518	5676	5843	6016	6198	6390	6593	6808	7037	7281	7544	7827
18	5081	5222	5368	5520	5679	5845	6019	6201	6394	6597	6812	7041	7285	7548	7832
19	5083	5224	5371	5523	5682	5848	6022	6205	6397	6600	6815	7045	7289	7553	7837
20	5085	5226	5373	5526	5685	5851	6025	6208	6400	6603	6819	7048	7294	7557	7842
21	5088	5229	5376	5528	5687	5854	6028	6211	6403	6607	6823	7052	7298	7562	7847
22	5090	5231	5378	5531	5690	5856	6031	6214	6407	6610	6826	7056	7302	7566	7852
23	5092	5234	5380	5533	5693	5859	6034	6217	6410	6614	6830	7060	7306	7571	7857
24	5095	5236	5383	5536	5695	5862	6037	6220	6413	6617	6834	7064	7311	7576	7862
25	5097	5238	5385	5539	5698	5865	6040	6223	6417	6621	6838	7068	7315	7580	7867
26	5099	5241	5388	5541	5701	5868	6043	6226	6420	6624	6841	7072	7319	7585	7872
27	5102	5243	5390	5544	5704	5871	6046	6230	6423	6628	6845	7076	7323	7589	7877
28	5104	5246	5393	5546	5706	5874	6049	6233	6427	6631	6849	7080	7328	7594	7882
29	5106	5248	5395	5549	5709	5876	6052	6236	6430	6635	6853	7084	7332	7599	7887
30	5108	5250	5398	5552	5712	5879	6055	6239	6433	6639	6856	7088	7336	7603	7892
31	5111	5253	5401	5554	5715	5882	6058	6242	6437	6642	6860	7092	7341	7608	7897
32	5113	5255	5403	5557	5717	5885	6061	6245	6440	6646	6864	7096	7345	7612	7902
33	5115	5258	5406	5559	5720	5888	6064	6249	6443	6649	6868	7100	7349	7617	7907
34	5118	5260	5408	5562	5723	5891	6067	6252	6447	6653	6871	7104	7353	7622	7912
35	5120	5263	5411	5565	5725	5894	6070	6255	6450	6656	6875	7108	7357	7626	7917
36	5122	5265	5413	5567	5728	5896	6073	6258	6453	6660	6879	7112	7362	7631	7922
37	5125	5267	5416	5570	5731	5899	6076	6261	6457	6663	6883	7116	7366	7636	7927
38	5127	5270	5418	5573	5734	5902	6079	6264	6460	6667	6886	7120	7371	7640	7932
39	5129	5272	5421	5575	5736	5905	6082	6268	6463	6670	6890	7124	7375	7645	7937
40	5132	5275	5423	5578	5739	5908	6085	6271	6467	6674	6894	7128	7379	7650	7942
41	5134	5277	5426	5580	5742	5911	6088	6274	6470	6677	6898	7132	7384	7654	7948
42	5136	5280	5428	5583	5745	5914	6091	6277	6473	6681	6901	7136	7388	7659	7953
43	5139	5282	5431	5586	5747	5917	6094	6280	6477	6685	6905	7140	7392	7664	7958
44	5141	5284	5433	5588	5750	5919	6097	6283	6480	6688	6909	7145	7397	7668	7963
45	5143	5287	5436	5591	5753	5922	6100	6287	6483	6692	6913	7149	7401	7673	7968
46	5146	5289	5438	5594	5756	5925	6103	6290	6487	6695	6917	7153	7406	7678	7973
47	5148	5292	5441	5596	5758	5928	6106	6293	6490	6699	6920	7157	7410	7683	7978
48	5151	5294	5443	5599	5761	5931	6109	6296	6494	6702	6924	7161	7414	7688	7983
49	5153	5297	5446	5602	5764	5934	6112	6299	6497	6706	6928	7165	7419	7692	7989
50	5155	5299	5448	5604	5767	5937	6115	6303	6500	6710	6932	7169	7423	7697	7994
51	5158	5301	5451	5607	5770	5940	6118	6306	6504	6713	6936	7173	7427	7702	7999
52	5160	5304	5454	5610	5772	5943	6121	6309	6507	6717	6940	7177	7432	7706	8004
53	5162	5306	5456	5612	5775	5946	6124	6312	6511	6720	6943	7181	7436	7711	8009
54	5165	5309	5459	5615	5778	5948	6127	6315	6514	6724	6947	7185	7441	7716	8014
55	5167	5311	5461	5617	5781	5951	6130	6319	6517	6728	6951	7189	7445	7721	8020
56	5169	5314	5464	5620	5783	5954	6133	6322	6521	6731	6955	7194	7449	7725	8025
57	5172	5316	5466	5623	5786	5957	6136	6325	6524	6735	6959	7198	7454	7730	8030
58	5174	5319	5469	5625	5789	5960	6140	6328	6528	6738	6963	7202	7458	7735	8035
59	5176	5321	5471	5628	5792	5963	6143	6332	6531	6742	6966	7206	7463	7740	8040
	64°	65°	66°	67°	68°	69°	70°	71°	72°	73°	74°	75°	76°	77°	78°

**FOR FINDING THE DISTANCE OF AN OBJECT,
BY TWO BEARINGS AND THE DISTANCE RUN BETWEEN THEM.**

Diff. between the Course and the Bearing.	Difference between the Course and the 1st Bearing.																
	Points.																
	Points.	2	2½	3	3½	4	4½	5	5½	6	6½	7	7½	8	8½	9	9½
3½	1'00																
4	1'00																
4½	0'81	1'23															
5	0'69	1'00	1'45														
5½	0'60	0'85	1'17	1'66													
6	0'54	0'74	1'00	1'35	1'85												
6½	0'49	0'67	0'88	1'14	1'50	2'02											
7	0'46	0'61	0'79	1'00	1'27	1'64	2'17										
7½	0'43	0'57	0'72	0'90	1'11	1'39	1'77	2'30									
8	0'41	0'53	0'67	0'82	1'00	1'22	1'50	1'87	2'41								
8½	0'40	0'51	0'63	0'76	0'92	1'09	1'31	1'58	1'96	2'50							
9	0'39	0'49	0'60	0'72	0'85	1'00	1'18	1'39	1'66	2'03	2'56						
9½	0'38	0'48	0'58	0'69	0'80	0'93	1'08	1'25	1'46	1'72	2'08	2'60					
10	0'38	0'47	0'57	0'66	0'76	0'88	1'00	1'14	1'31	1'51	1'76	2'11	2'61				
10½	0'38	0'47	0'56	0'65	0'74	0'84	0'94	1'06	1'19	1'35	1'55	1'79	2'12	2'60			
11	0'39	0'47	0'56	0'64	0'72	0'81	0'90	1'00	1'11	1'24	1'39	1'57	1'80	2'11	2'56		
11½	0'40	0'48	0'56	0'63	0'71	0'79	0'87	0'95	1'05	1'15	1'27	1'41	1'58	1'79	2'08	2'50	
12	0'41	0'49	0'57	0'64	0'71	0'78	0'85	0'92	1'00	1'08	1'18	1'29	1'41	1'57	1'76	2'03	2'41
12½	0'43	0'51	0'58	0'65	0'71	0'77	0'83	0'90	0'97	1'03	1'11	1'20	1'29	1'41	1'55	1'72	1'96

TABLE 8

539

TRUE DEPRESSION OR DISTANCE OF THE SEA HORIZON											
Height	Dep.	Square	Height	Dep.	Square	Height	Dep.	Square	Dep.	Square	
1-1 st	1'	1	3293 ⁿ	61'	3721	12966 ⁿ	121'	14641	181'	32761	
3-5	2	4	3403	62	3844	13183	122	14884	182	33124	
8-0	3	9	3513	63	3969	13397	123	15129	183	33489	
14-2	4	16	3624	64	4096	13615	124	15376	184	33856	
22-1	5	25	3740	65	4225	13836	125	15625	185	34225	
31-9	6	36	3855	66	4356	14061	126	15876	186	34596	
43-3	7	49	3974	67	4489	14282	127	16129	187	34969	
56-6	8	64	4093	68	4624	14502	128	16384	188	35344	
71-7	9	81	4213	69	4761	14737	129	16641	189	35721	
88-6	10	100	4337	70	4900	14970	130	16900	190	36100	
107	11	121	4461	71	5041	15197	131	17161	191	36481	
127	12	144	4587	72	5184	15429	132	17424	192	36864	
149	13	169	4716	73	5329	15664	133	17689	193	37249	
173	14	196	4846	74	5476	15901	134	17956	194	37636	
199	15	225	4976	75	5625	16139	135	18225	195	38025	
226	16	256	5112	76	5776	16380	136	18496	196	38416	
256	17	289	5249	77	5929	16622	137	18769	197	38809	
287	18	324	5385	78	6084	16866	138	19044	198	39204	
319	19	361	5524	79	6241	17111	139	19321	199	39601	
364	20	400	5665	80	6400	17362	140	19600	200	40000	
390	21	441	5808	81	6561	17608	141	19881	201	40401	
428	22	484	5952	82	6724	17860	142	20164	202	40804	
468	23	529	6098	83	6889	18111	143	20449	203	41209	
510	24	576	6246	84	7056	18366	144	20736	204	41616	
550	25	625	6394	85	7225	18622	145	21025	205	42025	
598	26	676	6547	86	7396	18878	146	21316	206	42436	
645	27	729	6700	87	7569	19140	147	21609	207	42849	
694	28	784	6855	88	7744	19401	148	21904	208	43264	
744	29	841	7012	89	7921	19664	149	22201	209	43681	
797	30	900	7173	90	8100	19930	150	22500	210	44100	
850	31	961	7332	91	8281	20197	151	22801	211	44521	
906	32	1024	7492	92	8464	20465	152	23104	212	44944	
964	33	1089	7656	93	8649	20736	153	23409	213	45369	
1023	34	1156	7824	94	8836	21008	154	23716	214	45796	
1084	35	1225	7987	95	9025	21282	155	24025	215	46225	
1147	36	1296	8158	96	9216	21558	156	24336	216	46656	
1211	37	1369	8330	97	9409	21836	157	24649	217	47089	
1278	38	1444	8504	98	9604	22115	158	24964	218	47524	
1346	39	1521	8678	99	9801	22397	159	25281	219	47961	
1416	40	1600	8852	100	10000	22680	160	25600	220	48400	
1487	41	1681	9032	101	10201	22964	161	25921	221	48841	
1561	42	1764	9210	102	10404	23251	162	26244	222	49284	
1636	43	1849	9393	103	10609	23540	163	26569	223	49729	
1713	44	1936	9577	104	10816	23830	164	26896	224	50176	
1792	45	2025	9760	105	11025	24121	165	27225	225	50625	
1872	46	2116	9951	106	11236	24415	166	27556	226	51076	
1954	47	2209	10135	107	11449	24711	167	27889	227	51529	
2039	48	2304	10325	108	11664	25008	168	28224	228	51984	
2124	49	2401	10518	109	11881	25307	169	28561	229	52441	
2212	50	2500	10712	110	12100	25608	170	28900	230	52900	
2301	51	2601	10908	111	12321	25911	171	29241	231	53361	
2393	52	2704	11105	112	12544	26215	172	29584	232	53824	
2485	53	2809	11304	113	12769	26521	173	29929	233	54289	
2581	54	2916	11506	114	12996	26829	174	30276	234	54756	
2677	55	3025	11709	115	13225	27139	175	30625	235	55225	
2775	56	3136	11913	116	13456	27451	176	30976	236	55696	
2875	57	3249	12120	117	13689	27764	177	31329	237	56169	
2977	58	3364	12328	118	13924	28079	178	31684	238	56644	
3081	59	3481	12538	119	14161	28396	179	32041	239	57121	
3186	60	3600	12749	120	14400	28715	180	32400	240	57600	

TABLE 9

No of FEET SUBTENDING AN ANGLE OF 1'.	
Dist. in Miles.	Feet.
1	1' 77
2	3' 54
3	5' 31
4	7' 08
5	8' 84
6	10' 61
7	12' 38
8	14' 15
9	15' 92
10	17' 69
11	19' 46
12	21' 23
13	23' 00
14	24' 77
15	26' 53
16	28' 30
17	30' 07
18	31' 84
19	33' 61
20	35' 38
21	37' 15
22	38' 92
23	40' 69
24	42' 46
25	44' 23
26	46' 00
27	47' 76
28	49' 53
29	51' 30
30	53' 07

TABLE 10

541

INDEX TO MARITIME POSITIONS

	COLUMN		COLUMN
Cuba	154, 155	H	
Cumana	163	Hainan Id.	71
Cumberland Ids.	143	Hawaiian Ids.	134
Cyprus	37	Heard Ids.	58
		Hebrides	5
D		Hermut Ids.	134
Danger Id.	121	Hindustan, West coast.	59, 60
Davis Strait	140	" East coast.	60, 61
Delaware	151	Holland	20
Demerara	163	Honduras	160, 161
Denmark	11	Horn, Cape	169
Dominica	158	Hudson's Bay	145
Ducie Id.	117	Hull Id.	121
		Humphrey Id.	121
E		I	
Easter Id.	117	Iceland	139
Ecuador	174	Icy, Cape	182
Egypt	37	India	59-63
Elizabeth Id.	117	Indian Ocean Ids.	55-58
Ellice Ids.	123	" Islands off Madagascar	49
England, South coast	1, 2	Ionian Ids.	29, 30
" West coast	2-4	Ireland, West coast	7, 8
" East coast	7	" North coast	8, 9
		" East coast	9
F		" South coast	9, 10
Faero Ids.	6	Italy, West coast	24, 25
Falkland Ids.	158	" South coast	27
Fernando Noronha	44	" East coast	27, 28
Fiji Ids.	125-127	J	
Flint Ids.	120	Jamaica	155
Flores	91, 92	James Ross Strait	144
" Sea	91	Jan Mayen	139
Florida	152, 158	Japan	76, 78
Formosa	75	Jarvis Id.	120
Fox Id.	143	Java	89, 90
France, North coast	16, 17	" Sea	91
" West coast	18, 19	Juan Fernandez	117
" South coast	22	K	
Frans Joseph Land	139	Kamchatka	79, 80
Friendly Isles	124	Karamania	36
Fundy, Bay of	149	Keeling Isles	58
		Kerguelen Land	58
G		Kermadec Ids.	124
Galapagos Islands	133	Kuril Isles	79
Gaspar Strait	65	L	
Georgia	152	Labrador	145, 146
Gilbert Isles	123, 124	Laccadives	55
Gilolo	95, 96	Ladrones	135
Grant Land	141	Lancaster Sound	143
Greece	30, 31	Lapland	16
Greenland	140, 141	Liu-kiu Ids.	76
Grenada	158	Louisiade Archipelago	97
Grinnell Land	141	Louisiana	159
Guadeloupe	158	Low Archipelago	117-119
Guatemala	175	Loyalty Ids.	127
Guiana	163, 164	Luzon	82, 84
Gulf of Guinea	43, 44		
" St. Lawrence	147, 148		

INDEX TO MARITIME POSITIONS

M		P	
	COLUMN		COLUMN
Macassar Strait	88	Pacific Ocean, North	133-137
McClintock Channel	142	Islands off West coast of America	133
Madagascar	48, 49	Islands N.W. of Sandwich Ids. ...	134
" Islands North of	49	Islands in Central Pacific	133
Madeira	39	Pacific Ocean, South	117-133
Magnetic Pole	144	Islands off West coast of America	117
Malabar coast	59	Islands North-west of Low }	120
Malacca Strait	63	Archipelago	
Malden Id.	120	Islands N.E. of Solomon I ^s	129
Maldives	56	Palawan	81
Maine	149, 150	Palmerston Id.	122
Marquesas	120	Panama	174
Marshall Ids.	136	" Isthmus	162, 174
Martin Vas	45	Paracel Ids.	71
Martinique	158	Parry Ids.	141
Massachusetts	150, 151	Pechili Gulf	74
Mauritius	58	Pelew Ids.	138
Meiaco Sima Ids.	75	Pearbyn Id.	120
Melbourne	106	Persian Gulf	53, 54
Melville Peninsula	144	Perth, West Australia	103
Mexico, Gulf of	158, 159	Peru	172, 173
" Eastern coast	159, 160	Pescadores Ids.	75
" Western coast	175, 176	Philippine Ids. ...	82-86
Mindanao	85	Phoenix Ids.	121
Mississippi	159	Pitcairn Id.	117
Morocco	39	Pocklington reef	98
Mosquito coast	161	Porto Rico	156
Mozambique	49	Prince Albert Land	142
		" Edward's Id.	143
		" Regent Inlet	142
		" of Wales Land	142
		Russia	10, 11
N		Q	
Nassau Id.	121	Queensland	109, 111
Navigator Ids.	122		
Newfoundland	146, 147		
New Britain	131, 132		
" Brunswick	149		
" Caledonia	128		
" Grenada	162		
" Guinea	97-99		
" Hampshire	150		
" Hebrides	128		
" Ireland and Islands N.E. of ...	131		
" Jersey	151		
" Orkneys	169		
" Shetlands	169		
" South Wales	108, 109		
" York	151		
" Zealand, Middle Id.	113, 114		
" " North Id.	115, 116		
" " Stewart Id.	114		
Nicaragua	174		
Noowook	143		
North Carolina	152		
" Devon	141		
" Somerset	142		
Norway	14, 15		
Nova Scotia	148, 149		
Novaya Zemlya	16		
O		R	
Okhotsk Sea	79	Red Sea, Western shore	51, 52
Oregon	177	" " Eastern shore	52, 53
Orkneys	5	Reirson Id.	121
		Rhode Id.	151
		Rocas	44
		Rodrigue	58
		Russia	11, 12, 16
		S	
		St. Ambrose Id.	117
		" Domingo	155, 156
		" Helena	44
		" Lawrence Gulf	147, 148
		" Lucia	158
		" Paul's, Indian Ocean	58
		" " Rocks, Atlantic	41
		" Thomas	157
		" Vincent	158
		Saghalin Id.	79
		Sala y Gomez	117
		Samoa Ids.	122
		San Salvador	175
		Santa Cruz, West Indies	157
		" " Islands, Pacific	129

TABLE 10

INDEX TO MARITIME POSITIONS

	COLUMN		COLUMN
Sardinia.....	23	Trinidad, South Atlantic.....	45
Scotland, East coast	6, 7	" West Indies	163
" West coast	4	Tripoli, Africa.....	37, 38
Seychelles.....	57	" Syria	36
Shetlands.....	5-6	Tristan d'Acunha.....	45
Siam Gulf.....	68	Tubuai Id.	121
Siberia	80	Tunis.....	38
Singapore.....	63, 67	Turkey }	32, 33, 34,
Smith's Sound	140, 141		36, 37
Society Ids.	119, 120		
Socotra	51		
Solomon Ids.....	129, 130	U	
South Atlantic, Ids. in	{ 44, 45, 168, 169	Union Ids.....	121
" Australia	104, 105	United States, Western	{ 176, 177 179-182
" Carolina	153	" " Eastern	149-153
" Georgia.....	168	" " Gulf of Mexico	158, 159
Southampton Id.	143	" " California	176
Spain, North coast	19, 20	" " Alaska.....	179-182
" South coast	20		
" East coast.....	21	V	
Spitzbergen	139	Vancouver Id.	176, 177
Starbuck Id.....	120	Venezuela.....	162, 163
Sulu Sea	86, 87	Venice	28
Sumatra, West coast	64	Victoria, Australia	106
" North-east coast	67	" Land	142
Sumba Id.....	93	Virginia	152
Sunda Strait.....	65	Volcano Ids.	135
Suwarrow Id.	120	Vostock Ids.....	120
Sweden	13, 14		
Sydney	108	W	
Syria.....	36, 37	West Australia.....	100-103
		" Indies	153-163
T		Windward Ids.....	158
Tartary.....	78, 79	Wollaston Land	142
Tasmania	107, 108		
Tema Reef	121	Y	
Texas	159	Yucatan	160
Tierra del Fuego.....	169, 170		
Timor	93		
Tohago	163		
Tonquin Gulf	70		
Torres Straits	112, 113		

MARITIME POSITIONS

(d)	Places	Lat. N	Lon. W	(4)	Places	Lat. N	Lon. W
Coast of Wales	Great Hangman Hill, 1160f....	51° 13'	3° 59'	Coast of Scotland	Southernness	54° 52' 4	3° 35' 5
	Bristol, \square , Cathedral.....	51 26 8	2 35 5		Ros. I., Fl. 175f.	54 46	4 5
	Newport, \square , Usk lt. F 39f.	51 32 4	2 59 7		Burrow Hd.	54 41	4 23
	Cardiff, \square , Custom ho.	51 28 6	3 10 0		Mull of Galloway, lt. Int. 325f.	54 38 1	4 51 2
	Nash Pt., 2 lts. N 85° W, F 182f.	51 24 0	3 33 0		Port Patrick, \square , lt. F 38f.	54 50 3	5 6 7
	Mumbles, lt. F 114f.	51 34 0	3 58 2		Corsewall Pt., lt. R 112f.	55 05	5 9 5
	Swansea, \square , pier lt. F 35f., 8f.	51 37 0	3 56 0		Lough Ryan, \square , lt. F 46f.	54 58 5	5 17
	Worms Hd., 1, 164f.	51 34	4 20		Strauraer, \square , Church.....	54 54 5	5 2 0
	Pembrey, \square , lt. F 35f., 10f.	51 40 7	4 15 0		Ayr, \square , 3 lt. S 84° E 830f., } F 53f., F 8. }	55 28	4 38
	Ca'dy I., $\frac{3}{4}$ 1 $\frac{1}{2}$ m., S pt., lt. F 1210f.	51 37 9	4 41 0	Coast of Scotland	SCOTLAND, West Coast.		
	St. Govan's Hd., 142f.	51 35 8	4 55 5		Ailsa Cr. ig, 1098f., lt. Fl. 60f.	55 15 2	5 7 0
	St. Ann's lts. N 41° W 610f., } 2F 192f., 159f. }	51 41 0	5 10 5		Pladda, lts. 2F 130f., 77f.	55 25 6	5 7 0
	Millford, \square , Ch.	51 42 7	5 1 5		Ardrossan, \square , lt. Fl. 25f.	55 38 7	4 50 5
	Pembroke Dk. yd., NW corner	51 41 8	4 57 2		Irvine, \square , Ch.	55 36 8	4 39 7
	Smalls lts., NS 2c., lt. Int. 125f.	51 43 3	5 40 0		Cunbrg., lt. F 115f.	55 43	4 57 8
	Grasholm I., $\frac{3}{4}$ 3c., sum. 146f.	51 43 9	5 28 7		Greenock, \square , spire	55 56 9	4 45 2
	Ramsey I., NS 1 $\frac{1}{2}$ m., sum. 444f.	51 51 7	5 20 7		Port Glasgow, \square , basin	55 56 2	4 41
	South Bishop rk., lt. R 144f.	51 51 4	5 24 5		Glasgow, new bridge	55 51 9	4 16
	St. David's Cath.	51 52 9	5 16 0		— OBSERVATORY	55 52 7	4 17 7
	Strumble Hd.	52 1 7	5 3 5		Campbelton, \square , lt. F 18f.	55 25 0	5 35 5
	Preceilly Top, 1754f.	51 56 8	4 46 2		Mull of Cantire, lt. F 297f.	55 18	5 48
	Cardigan I., $\frac{3}{4}$ 4c., sum. 195f.	52 7 9	4 47 5		Ben Tuirck, 1516°.	55 34	5 34
	— Steeple	52 5 2	4 39 5		Maol Na Ho, Dun Ard.	55 35	6 18
	Aberystwith, \square , lt. F, Castle	52 24 9	4 5 2		Rhyons of Isla. lt. on Ocr-a } I. Fl. 150f. }	55 40	6 31
	Cader Idris, 3549f.	52 42 0	3 54 5		Colonsay I., $\frac{3}{4}$ 6m., N pt.	56 8	6 9
	Snowdon, 3580f.	53 4 1	4 4 5		Ohan, \square , Church	56 24 5	5 28
	Bardsey I., $\frac{3}{4}$ 1 $\frac{1}{2}$ m., lt. Occ. } 129f. }	52 45 0	4 48 0		Lismore I., $\frac{3}{4}$ 9m., lt. F 103f.	56 27 5	5 36
	Caernarvon, \square , lt. F 50f.	53 8 5	4 24 7		Fort William	56 48	5 5
	S. Sack lt. R 1 $\frac{1}{2}$ m. 197f.	53 18 3	4 42 0		Ben Nevis, 4368f.	56 48	5 0
	Holyhead, \square , lt. F 20f., bell	53 20 0	4 37 0		Dubh Arnach rk.	56 8	6 38
	Skerries, $\frac{3}{4}$ 1 $\frac{1}{2}$ m., lts. Int. 117f.	53 25 3	4 36 5		Iona I., $\frac{3}{4}$ 3 m., W pt.	56 18 7	6 26 7
	Pt. Lynus, lt. Occ. 128f.	53 25 0	4 17 2		I. of Mull, Caliacall Pt.	56 36 4	6 19
Coast of England, W. Coast	Beaumaris, \square	53 15 9	4 5 2		Ben More, 3168f.	56 25 5	6 0 7
	Great Ome's Hd., lt. F 325f.	53 20 0	3 51 2		Skerryvore rks., lt. R 150 t.	56 19 4	7 7
	Hoylake, l. F 31f.	53 23 7	3 11 0		Tirey I., $\frac{3}{4}$ 11m., S extr.	56 26	6 55
	Bigston, lt. F 228f.	53 24 1	3 4 7		Dubh Sgeir rk.	56 31 5	7 2 7
	Leasowe, lt. F 94f.	53 24 9	3 7 7		Coll. I., $\frac{3}{4}$ 10m., N & E pt., } rks. }	56 41 5	6 27
	Black rk., lt. R 77f.	53 26 7	3 2 7		Muke Id., Innerah l't.	56 50	6 16 5
	Liverpool, \square , St. Paul's Ch.	53 24 6	2 59 5		Rum I., NS 7m., S pt.	56 56 2	6 19 5
	— Observatory, $\frac{3}{4}$ 1 ^a	53 24 8	3 0 0		— W pt.	57 05	6 27 2
	Crosby, lt. F 95f.	53 31 4	3 3 5		Canna I., $\frac{3}{4}$ 4m., W pt.	57 3	6 36 5
	Formby SE mark	53 32 3	3 4 0		Skye I., Neist Pt.	57 25 2	6 47 2
	Rosell sea mark.	53 55 2	3 3 0		— Dunvegan lld.	57 30 8	6 43
	Wyre, lt. F 30f., bell.....	53 57 3	3 1 7		Fladdachuan Islet, N end.....	57 44 8	6 26 5
	Fleetwood, \square , lt. F 90f. } NW extr. }	53 55 6	3 1 0		Skeir Gratick	57 47 1	6 28
	Launcester, Castle	54 3 0	2 48 2		Ru Hunish	57 42 5	6 21
	Walney I., $\frac{3}{4}$ 7m., S pt., lt. } R 70f. }	54 2 9	3 10 5		Ru Rea	57 51 6	5 48 7
	Black Comb, 1919f.	54 15 5	3 19 5		Ru C'oygach	58 6 5	5 26
	S. pt., Calf of Man.	54 3 2	4 50 0		Ru Stoer	58 16	5 22
	Charleton, lt. F 22f.	54 4 4	4 39 0		Hunda I., [1 $\frac{1}{2}$ m.], 400f. sum....	58 23 0	5 11 7
	Douglas, lt. F 104f.	54 9 0	4 28 0		Bulgie I., [1 $\frac{1}{2}$ m.], 146f.	58 32 7	5 7
	N. pt., Ayre Pt., lt. R 106f.	54 25 0	4 22 0		C. Wrath lt. R 400f.	58 37 5	4 59 7
	Peel, lt. F 27f.	54 13 6	4 42 0		Far-out Hd.	58 36 2	4 45 0
	St. Bees Hd., lt. Occ. 333f.	54 30 8	3 38 0		Roan I., $\frac{3}{4}$ 1 $\frac{1}{2}$ m., mid.	58 33 3	4 19 2
	Whitehaven, \square , lt. R 52f.	54 33 2	3 35 7		Strathly Hd.	58 36 0	4 9 5
	Harrington, \square , pier lt. F } 44f., 7f. }	54 36 7	3 34 2		Thurso	58 33	3 31
	Workington, \square , lt. F 42f. } at 7f. }	54 38 9	3 34 5		Holburn Hd.	58 35	3 31
	Maryport, \square , S pier, F 52f.	54 43 0	3 30 5		Dunnet Hd., lt. F 346f.	58 40 4	3 21 2
	Carlisle, Cathedral.	54 53 8	2 56 0		Duncansby lld.	58 39	3 1
	Annan, Church	54 59 2	3 15 5		Portland Skerries, $\frac{3}{4}$ 1 $\frac{1}{2}$ m., } lts. N pt., 2F 140f., 170f. }	58 41 2	2 55 0

MARITIME POSITIONS

MARITIME POSITIONS							
(5) Places		Lat. N	Lon. W	(6) Places		Lat. N	Lon. W
Hebrides.							
Barra Hd., lt. In ^r . 683f.	56°47'1	7°39'2		Fetlar I., $\frac{1}{4}$ 6m., E pt.	60 35'2	0°46'0	
Barra I., N pt. of Fiary	57 4	7 26'7		Balta I., NS $\frac{1}{4}$ m., S pt.	60 44'4	0 47'7	
Eris Kay I., NS 3m., S end ...	57 3	7 17'5		N. extr. outer Stack rk.	60 51'5	0 52'5	
S. Uist I., NS 17m., E pt., }	57 18	7 11'5		Gloup Holm, 3c., sum.	60 44'2	1 6'5	
Ushinish, lt. Occ. 176f.	57 18	7 11'5		Uya, or NE pt.	60 37	1 26	
— Ru ard Vula, W pt.	57 14'5	7 27'5		Roenness Hill, 1476f. W end...	60 32	1 27	
Monach I., EW 4m., lt. Fl 150f.	57 31'6	7 41'7		Ossa Skerry, rks. $\frac{1}{2}$ 4c.	60 33'0	1 35'5	
Huskier Is., N Loch, 120f.	57 42'3	7 40'7		Esha Ness Skerry	60 28'5	1 37'2	
N. Uist I., EW 15m., W pt.	57 36'2	7 33		Fuglow Skerry	60 20'4	1 45'0	
Berneray I., $\frac{1}{2}$ 3m., N pt.	57 44	7 11'5		Ve Skerries, $\frac{1}{2}$ 1m., mid.	60 22'5	1 49	
Pabbay I., EW 2m., S pt.	57 45'3	7 14'5		Skelda Ness	60 8'8	1 28'0	
Scalpay, Glas I. EW $\frac{1}{2}$ m., }	57 51'4	6 38'2		Fitfull Hd., 929f.	59 54	1 24	
lt. F 130f.	57 51'4	6 38'2		Foula I., $\frac{1}{4}$ 3m., $\frac{1}{4}$ sum. 1369f.	60 8'5	2 5'5	
Shiant Is., 1m., NW one, Wend	57 54'5	6 23		Faero Islands.			
Stornaway, lt. R 56f.	58 11'5	6 22'2		Monk rk., 30f.	61 23	6 45'7	
Chicken Hd.	58 10'8	6 15		Suderoe I., $\frac{1}{4}$ 5 l., S pt.	61 26'5	6 48'5	
Tiupan Hd.	58 15'7	6 8		Grt. Diamond	61 43	6 49	
Butt of Lewis, lt. F 170f.	58 30'8	6 15'7		Myggenocsl., EW 4m., W }	62 8	7 37	
Gallon Hd.	58 14'6	7 1'5		extr.			
Scarpa I., W pt.	58 17	7 10		Fugloe I., NS $\frac{1}{2}$ m., E pt.	62 20	6 13	
Rona I., SE sum. 360f.	59 7'0	5 48'5		Nalsoe I., $\frac{1}{4}$ 5m., S pt.	61 58'5	6 39	
Sulisker I., S sum	59 5'4	6 8'7		Thorsbavn, lt. F 35f.	62 2'5	6 45'2	
Flannan Is., Rodorheim.	58 17	7 39		Haldervig Church	62 18'3	7 2	
St. Kilda, pk. 1220f.	57 49'0	8 34'7		SCOTLAND,			
Rockal [2c.], (a rk. N73°E, }	57 36'3	13 41'5		East Coast.			
1'7m.)				Noss Hd., 577f., lt. R 175f. ..	58 28'6	3 3	
Orkneys.				Ord of Caithness, needle	58 10'2	2 31'0	
Old Hd.	58 44'3	2 55'5		Tain, \square $\frac{1}{2}$ spire.	57 48'7	4 3'2	
Kirkness	58 48'2	2 54'5		Tarbetness, lt. Int. 175f.	57 51'9	3 46'5	
Grimness Hd.	58 49'4	2 52'2		Cromarty, \square spire	57 40'7	4 0'0	
Burra Ness	58 51'4	2 51'0		Cromarty Pt., lt. F 60f.	57 41'0	4 2'0	
Rosness	58 52'5	2 49'5		Fort George	57 35'1	4 4'5	
Mull Hd.	58 58'6	2 42'0		Chanonry Pt., lt. F 40f.	57 34'5	4 5'5	
Kirkwall, pier lt. F 31f.	58 59'2	2 57'5		Inverness, \square jail	57 28'6	4 13'5	
Brough of Bira, $\frac{1}{2}$ m.	59 8'2	3 20'0		Burgh Hd.	57 42'1	3 30'0	
Stromness, \square $\frac{1}{2}$ Church	58 57'8	3 17'5		Corsevea Skerries, lt. R 160f	57 43'4	3 20'2	
Copinska I., $\frac{1}{2}$ 1m., mid.	58 54	2 40		Cullen, Castle hill	57 41'4	2 49'5	
Auskery I.	59 2	2 34		Ranff. \square $\frac{1}{2}$ N pier, lt. F 28f.	57 40'3	2 31	
Stron-a I., $\frac{1}{4}$ 7m., Lamb Hd.	59 4'9	2 32'0		Troup Hd., pt.	57 41'7	2 17'2	
Sanday I., $\frac{1}{2}$ 11m., Treaness	59 13	2 28'5		Kinnaird's Hd., lt. F 120f.	57 41'9	2 0'2	
Siart lt. F 80f.	59 16'7	2 22'5		Fraserburgh, 2 lts. F 20f., 35f.	57 41'5	2 0'0	
N. Ronaldsha I., $\frac{1}{2}$ 3m., lt. }	59 23'4	2 23'7		Rattray Pt.	57 37	1 49	
F 140f.				Peterhead, S \square $\frac{1}{2}$, Keith Incl.	57 30'1	1 46'0	
— Stromness, or S pt.	59 20	2 26		Buchanness, lt. Fl. 130f.	57 28'2	1 46'5	
Runebrake shl.	59 21	2 37		Aberdeen, \square $\frac{1}{2}$ OBSERVATORY	57 8'9	2 5'7	
Moul Hd.	59 23'0	2 53		Girdleness, 2 lts. F 125f.	57 8'5	2 4	
Noup Hd.	59 20'0	3 4'0		Stonehaven, \square $\frac{1}{2}$ 2 lts. F 24f.	56 58'0	2 12'7	
Sacnoy Hd.	59 12'0	3 4'2		Montrose, \square $\frac{1}{2}$ Scurdy Ness.	56 42	2 27	
Stour Roray	58 52'4	3 25'5		lt. Int 124f.	56 37	2 29	
S. pt., or Brinn.s	58 46'4	3 13'5		Red Hd., 255f.	56 33'7	2 35'0	
Shetlands.				Arbroath, \square Abbey	56 33'7	2 35'0	
Fair I., $\frac{1}{2}$ 2m., h. T. pk. 711f.	59 33	1 37'7		Buddonness, 2 lts. N49°W }	56 28'1	2 45'0	
Sumburgh Hd., lt. F 300f.	59 51'3	1 17'0		1122f., F 103f., 61f.			
Mousa I., $\frac{1}{4}$ 1 $\frac{1}{2}$ m., sum.	60 0	1 11		Port-on-Craig, 2 lts. S88°E }	56 27	2 49	
Bard Hd.	60 6'1	1 4'5		1321f., F 80f., 30f.			
Lerwick, \square , fort	60 9'4	1 8'7		Dundee, \square lts. N80°W 390f., }	56 27'6	2 57'7	
Noss Hd., 557f.	60 8'3	1 0'5		2 F 25f.			
Halsey I., $\frac{1}{2}$ 5m., S sum. 376f.	60 20	1 0		Bell rk., lt. R 93f.	56 26'0	2 23'0	
Out Skerries, lt. R 145f.	60 25'4	0 44'5		St. Andrews, \square , Ch.	56 20'4	2 47'5	
Burra Voc Ness	60 29'5	1 2'0		Fifeness, fl. st.	56 16'7	2 35'0	
				Muy I., $\frac{1}{4}$ 1m., lt. Fl. 240f.	56 11'1	2 33'2	
				Leith, \square , pier lts. F	55 58'9	3 10'5	
				Edinburgh, Ons. Blackford ...	55 55'5	3 11'6	

TABLE 10

547

MARITIME POSITIONS

(7)	Places	Lat. N	Lon.	(8)	Places	Lat. N	Lon. W
			West				
	Inch Keith lt. R 220f.	56° 2'0	3° 8'0		Hungry Hill, 181f.	51° 41'	9° 47'5
	N. Berwick, Church	56 34	2 43'2		Bantry, Ch.	51 40'8	9 27'2
	Bass rock	56 47	2 38'2		Roanearragh L, lt. F 55f.	51 39'2	9 44'7
	Dunbar, \square , Church	55 59'9	2 31'0		Calf rk.	51 34	10 16
					Bull rk., lt. Fl. 271f.	51 35'5	10 18
	ENGLAND.				Cod's Head.	51 39'7	10 6'2
	East Coast.				Scariff L, summit.	51 43'6	10 15'5
	St. Abb's Hd., lt. Fl. 224f. ...	55 55	2 8		Bolus Hd.	51 47	10 20'7
	Eyemouth, Church	55 52'3	2 5'5		Skelligs, lt. F 175f.	51 46'2	10 32'7
	Berwick, \square , spire	55 45'8	1 59'0		Bray Hd.	51 53	10 26
	Holy I., Castle	55 40'2	1 47'0		Valentia, \square , Cromwell's } Fort, lt. F 54f. }	51 56	10 19'2
	Farn Is., 2 lts. N36°W 560f., } R 30°, 87f., Fl. 45f. }	55 37'0	1 39'2		Great Foze rk.	52 1'2	10 41'2
	Cheviot hill, 2658f.	55 29	2 9		Tearaght rk., lt. Fl. 275f.	52 4'5	10 40
	N. Sunderland Pt., mill.	55 34'7	1 38'2		Grt. Blasket, $\frac{1}{2}$ 3m, N pt.	52 6'7	10 31'2
	Coquet I., lt. F 83f.	55 20'1	1 32'0		Brandon Hill, 3126f.	52 14	10 15
	Blyth, \square , 2 lts. F.	55 7'5	1 30'0		Tralee Lt. Saphire I., lt. } F 56f. }	52 16'2	9 52'7
	Tynemouth, lt. R 154f., Castle	55 1'3	1 25'0		R. Shannon, \square , Kerry Hd. ...	52 25'3	9 56'5
	N. Shields, \square , Ch.	55 0'7	1 26'7		Tarbert, lt. F 58f.	52 35'5	9 21'7
	Newcastle, bridge, N end	54 58'7	1 35'5		Limerick, \square , Cathedral.	52 40	8 37'5
	Sunderland, \square , Church.	54 54'5	1 21'5		Kilcradan, lt. F 133f.	52 34'8	9 42'5
	Hartlepool, \square , Church	54 41'8	1 10'7		Loop Hd., lt. Occ. 277f.	52 33'6	9 56
	Seaton, \square , 2 lts., high lt. F 89f.	54 40'3	1 12'2		Ballard Pt., tower	52 44	9 37
	Tees River, entrance	54 37'1	1 8'7		Hugs Hd.	52 57	9 28
	Sockton, Church	54 34'0	1 18'7		Arran Is., Eeragh I., lt. R } 115f. }	53 9	9 51'5
	Redcar, Church	54 36'9	1 3'5		— Inisheer I., lt. F 110f. ...	53 2'7	9 31'5
	Whitby, \square , 2 lts. F 240f.	54 28'7	0 34'2		Black Hd.	53 9	9 16
	Scarborough, \square , lt. F 58f. ...	54 17'0	0 23'5		Galway, \square , Mutton I., lt. } F 33f. }	53 15'2	9 3'2
	Flamborough Head, lt. R ^W } 214f. }	54 7'0	0 5'0		Skird rks, 1m. Skirdmore ...	53 15'3	10 0
	Bridlington Quay, Mill, \square ...	54 5'2	0 11'7		Slyne Hd., 2 lts. S18°E 415f., } R ^W 115f., F 104f. }	53 24'0	10 14'0
	Hull, \square , citadel	53 44'6	0 20'0		Inishark Hd.	53 36	10 18
	Killingholme, 3 lts. F 68f., outer	53 38'7	0 12		Clare I., N pt., lt. F 340f. ...	53 49'5	9 59'5
			East		Inishgort, lt. F 36f.	53 49'5	9 40'2
	Spurn Is., N66°W, Occ. & F } 93f., 54f. }	53 34'7	0 7'2		Westport	53 48	9 31
	Inner Dowsing, beacon	53 18'4	0 33'2		Newport, \square	53 53	9 33
	Smith's Knoll, $\frac{1}{2}$ 7m., 4, S pt.	52 48	2 14		Bills rk.	53 53	10 12'7
	Hunstanton Pt., lt. Occ. 109f.	52 57	0 29'7		Achil Hd., 2222f., pt.	53 58'5	10 15'2
	Cromer, lt. R 274f.	52 55'5	1 10'0		Black rk., lt. R 283f.	54 4'2	10 19'2
	Hasborough, lt. F 136f.	52 49'2	1 32'2		Eagle I., 2 lts. N49°E 395f., } F 220f. }	54 17	10 5'5
	Winterton, lt. F 110f.	52 43'0	1 41'5		Erris Hd.	54 18'5	10 0
	Yarmouth, \square , spire	52 36'8	1 43'7		Stag rks, Nst.	54 22	9 47'7
	Lowestoft, 2 lts. N28W 2490f. }	52 29'2	1 45'5		Downpatrick Hd.	55 19'6	9 20'7
	Rev. and F 123f., 40f. ... }	52 19'7	1 40'7		Killala, \square	54 11	9 13
	Southwold, Church.	52 9'2	1 36'0		Ballina, \square , spire	54 6'6	9 9'5
	Alborough, steeple.	52 4'8	1 34'5		Sligo Black rk., lt. F 79f.	54 18	8 37
	Orfordness, lt. Int. 91f.	52 5'7	1 32'2		Innis Murray I., W end	51 25'7	8 40
	Orford, steeple	51 50'3	1 19'2		Ballyshannon, \square , Ch.	54 30'2	8 11'7
	Landguard Fort.	51 55'8	1 16'7		Donegal, \square ...	54 39'5	8 7
	Harwich, \square , 2 lts. F N62°W } 680f., 45f., 27f. }	51 51'8	1 17'2		St. John's Pt., Killbegs, lt. } F 98f. }	54 34'1	8 27'5
	Walton, tower	51 35	1 3		Rathlin O Burne Is., lt. F 116f.	54 32'7	8 50
	Maplin, SE pt., Occ. 36f., bell				Dawros Hd., pt.	54 49'6	8 34'0
			West		Aran I., Riarawros lt. R 233f.	55 0'9	8 33'7
	IRELAND.				Stag rks.	55 4'6	8 29'0
	West Coast.				Bloody Foreland Hill, 1059f.	55 8'2	8 15'7
	Cape Clear, I., $\frac{1}{2}$ 3m., SW point	51 25'3	9 31				
	Fastnet rk., 92f., lt. R 148f. ...	51 23'3	9 36'2		North Coast.		
	Crookhaven, \square , N entr. lt. F 67f.	51 28'6	9 42'7		Tory I., $\frac{1}{2}$ 2'5m., lt. on N }	55 16'5	8 15
	Mizen Hd.	51 47	9 49'5		& W pt. Fl. 130. }		
	Sheep Hd.	51 32'5	9 51'2		Horn Hd., E sum. 824f.	55 12'5	7 57'2
	Bearhaven, \square , Bear I., sum. }	51 37'5	9 52'2		Melmore Pt., tower	55 15'2	7 47'2
	887f. }						

MARITIME POSITIONS

(11) Places		Lat N	Lon. E	(12) Places		Lat N	Lon. E
Altona, Observatory		53°32'7	9°56'5	Stettin		53°25'1	14°34'0
Hamburg, OBSERVATORY		53 33'1	9 58'5	Colberg, fort		54 10'8	15 35
DENMARK.				Jershöft, lt. R 165f.		54 32'5	16 33'0
Horn Pt., rf., outer shl. 1		55 35	7 40	Hela, lt. R 120f.		54 36'1	18 49'2
Hantsholmen Pt., lt. R 218f.		57 6'8	8 36'2	Rixhöft, lt. F 231f.		54 49'9	18 20'5
Harshals Nist		57 35	9 56	Neufahrwasser, lt. F 78f.		54 24'2	18 40'2
The Skaw, pt., l, lt. F 144f.		57 43'8	10 38'5	Danzig, Observatory		54 21'3	18 41'2
Hirtsholmen, lt. F, Fl. 95f.		57 29'2	10 37'5	Pillau, □, lt. F 96f.		54 38'4	19 54'0
Fladstrand, Church		57 27'0	10 33'7	Königsberg, Observatory		54 42'8	20 30'2
Niiningen, ls., 2 F 66f., bell ..		57 18	11 54	Brüster Ort, lt. R 164f.		54 57'6	19 59'2
Læsø I., 8 10m., Byrum Ch.		57 15'4	11 0'2	Memel, □, lt. F 98f.		55 42	21 6'2
Anholt I., E pt., lt. Fl. 133f.		56 44'3	11 39'2	RUSSIA.			
Hasselø, lt. F 118f.		56 11'7	11 43	Libau, □, Pilot's Tower, lt. }			
Aalborg		57 2'7	9 55	F, Fl. 103f.		56 30'9	21 0
Fornæs, lt. Fl. 69f.		56 26'7	10 57'5	Windau, Church		57 23'9	21 34'0
Aarhus, Cath.		56 9'5	10 13'0	Lyser Ort, lt. F 118f.		57 34	21 43
Thundø I., lt. F 100f.		55 56'9	10 27'0	Domesness, lt. F, Fl. 64f.		57 48	22 39
Bangø, lt., S pt., F 39f.		55 17'7	9 48'0	Runo I., lt. F 210f.		57 48	23 15
Apenrade		55 2'6	9 25'2	Riga, □, Cathedral		56 57'0	24 6'5
As-enæ, Church		55 16'1	9 53'7	Pernau, Germ. Church		58 23'2	24 30
Flen-burg		54 46'9	9 26'2	Arensberg		58 15'1	22 30
Siøllands rf., N and W pt.		56 5	11 15	Swalfer Ort, lt. Osell S pt., }			
Kyholm		55 56'0	10 40'7	Rev. 114f.		57 54'6	22 4
Reefness, lt. F 79f.		55 44'7	10 52'5	Filsand, W pt. of grt. Id., }			
Sprogø, lt. R 134f.		55 20	10 58	F 136f.		58 23	21 50
Nyeborg, Ch.		55 18'7	10 47'7	Dager Ort, lt. 5m. Ed. of pt., }			
Fakkelberg, lt. S pt. Lange- }				F, Fl. 334f.		58 55	22 13
land, F 129f.		54 44'4	10 42'0	Winkova		59 12	22 18
Spotsbiorg, lt. Fl. 123f.		55 58'6	11 52'0	Odensholm, lt. Fl. 115f.		59 18'3	23 23'0
Nakkehead, 2 lts. N83°W, F }				Parker Ort, lt. F 147f.		59 23'5	24 3
147f., 98f.		56 7'2	12 21'0	Sourop, lt. F 135f.		59 27'9	24 24
Elsineur, Kronborg, lt. F, Fl. }				Nargen I., lt. N pt., R 126f.		59 36'4	24 32'0
110f.		56 2'2	12 37'5	Revel, St. Olaus Church		59 26'6	24 47
COPENHAGEN, □, University, }				Wolf beacon		59 35	24 48
OBSERVATORY		55 41'2	12 31'7	Kokskar, lt. F 106f.		59 42'0	25 3
Stevens Cape, lt. Fl. 209f.		55 17	12 27	Ekholm, lt. F, Fl. 103f.		59 41	25 49
Moen I., E pt., lt. F 82f.		54 57	12 33	Stoneskar beacon		59 49'5	20 21
Gørdser point, lt. F 64f.		54 33'8	11 56'0	Rolskar I., lt. Fl. 65f.		59 58'2	26 42'0
Trindelen, shl.		54 30'5	12 4	Little Tiouters, W pt.		59 50'0	26 53'0
Eartholms, or Christiansø, lt. }				Great Tiouters, E sum		59 51'0	27 14'5
N pt., Fl. 94f.		55 19	15 12	Hogland, 2 6m., N. pt. 2 lts. }			
Bornholm, N pt.		55 17'7	14 46	S' by W' 0 6m., F 384f., 33f. }		60 6'3	26 58'5
— S pt.		54 59	15 5	lower			
— Rønne, 2 lts., F 76f., 29f.		55 6	14 42	Laven-kar I., N pt.		60 2'3	27 51'0
PRUSSIA				Peni I., E pt.		60 1'1	28 5'0
in the Baltic.				Seskar I., NW pt., lt. Fl. 97f.		60 2'1	28 23'5
Kiel, OBSERVATORY		54 20'5	10 8'7	C. Kolpanpia, Church		59 50'9	28 34'7
Fermom I., Marien, lt. R 94f.		54 29'7	11 14'2	Dolgoi Noos Pt.		59 54'8	29 0'5
Staberhuk I.		54 24	11 19	Tolboukin, lt. Rev. 95f.		60 2'6	29 33'0
Lubeck, St. Mary's Church ...		53 52'1	10 41'5	Kronstadt, □, St. Andrew Ch.		59 59'7	29 46
Wismar, St. Mary's Church ...		53 53'5	11 27'7	St. PETERSBURG, Acad. of }			
Warnemunde, lt. F 59f.		54 10'7	12 5'7	Science, OBSERVATORY ... }		59 56'5	30 18'2
Rostock		54 5'5	12 9'0	POULKOVA, OBSERVATORY ...		59 46'3	30 19'7
Dars Hd., pt., 2 lts. F & R }				Sürs Pt., lt. F 117f.		60 11'0	29 3
108f. & 41f.		54 28'6	12 30'5	Björko I., S pt., tower		60 15'7	28 43'2
Stralsund		54 18'3	13 5'5	Grekova rk., beacon		60 11'6	28 42'5
Arkona, lt. F 200f.		54 40'9	13 26'2	Wiborg		60 42'7	28 46
Bergen, Church		54 25'5	13 28'0	Aspo beacon		60 17'7	27 13
E. pt. of Rugen I.		54 21	13 48	Nerva tower		60 14'8	27 58'5
Greifswald, lt. Rev. 154f.		54 15'1	13 55'7	Sommars I., lt. Rev. 89f.		60 12'4	27 39'5
Swinemünde, lt. F 207f.		53 55'0	14 18'0	Lippu I., beacon		60 14'3	27 30
				Frederickshamm		60 34	27 12
				Lovisa, □		60 27'6	26 16
				Orrengrund, beac. 103f.		60 16'6	26 27'2
				Grt. Pellingö, or Glosholm ...		60 11'2	25 50

TABLE 10

MARITIME POSITIONS

(15) Places		Lat. N	Lon. E	(16) Places	Lat. N	Lon. E
NORWAY	Flekkeø I., \square , rks. to S	58° 2'	7° 57'	LAPLAND.		
	Ryvingen I., lt. F. Fl. 129f.	57 58° 0	7 29° 5	Sværholt Klubb	70° 59'	26° 41'
	Naze, lt. F. Fl. 163f.	57 58 8	7 32	Nord Kyn	71 6 8	27 41
	Listersteen, lt. Fl. 128f.	58 6	6 34	Vardo I.	70 23	31 7
	Jedderns, rf. W pt.	58 46	5 24	Rybatschi I., C. Nomeiski ..	69 58	32 0
	Tungnes, lt. F 29f.	59 2	5 35	Kola, town	68 52 5	33 1
	Hvidings, lt. Occ. 149f.	59 3	5 24	— R. Kildin I., E pt.	69 19	33 30
	Skudesnæs, lt. F 75f.	59 8	5 18	RUSSIA.		
	Hoievarde, lt. F 65f.	59 19	5 19	Sviatoi Noss., lt. F 298f.	68 9 0	39 49 0
	Udsire, 2 lts. N 8° W, 255f. F ..	59 18 3	4 53 5	C. Orlov, lt. F 222f.	67 11 5	41 22 2
	Sor Hango rk., lt. F, Fl. 72f.	59 25 2	5 15 2	Sosnovets, lt. F 139f.	66 29 5	40 43
	Bummeløe, S pt.	59 35	5 11	Tetina, vill., Chap.	66 39	38 17 5
	Fugløe	60 1	4 59	Kouzomen, vill., mid.	66 17 2	36 53 5
	Lervig, lt. F 47f.	59 47	5 33	C. Touria	66 33	34 28
	Odde, Church	60 4	6 33 2	Kandalaks, Monastery	67 10	32 32
	Kors fiord, l. entr.	60 8	4 57	Kyem, Church	64 56 5	34 38 7
	Bergen, \square	60 24	5 18	Onega, St. Michael Church ...	63 53 6	38 8 5
	Blomøe I.	60 32	4 46	Jighinsk I., N pt., lt. F 140f ..	65 12 3	36 51 5
	Udvær Is., W pt.	62 2	4 28	Arkhangel, \square , Trinity Ch.	64 32 1	40 33 5
	Aspo I., NW pt.	61 13	4 44	Moudinga I., lt. Dvina R. F 130f.	64 55 8	40 16 2
	V. ragrud	61 17	4 27	C. Kerets	65 19 9	39 45
	Senning skar rk.	61 39	4 35	C. Voronov	66 31 1	42 19 7
	Stadiland, NW pt.	62 11	5 8	Mezen, Epiphany Ch.	65 50 3	44 17 0
	Svinøe	62 20	5 17	C. Kanushin, near brook	67 11 5	43 48 7
	Rundo, lt. F 158f.	62 24 6	5 35 5	C. Kanin Noss	68 39 2	43 32 5
	Aalesund, Church	62 28 2	6 9	Kolguyev I., NS 50m., N pt.	69 30	49 20
	Lepsorev, lt. F 23f.	62 35 5	6 16 5	C. Russian	68 55	54 40
	Molde, Church	62 44 3	7 10	C. Mediansk	68 58	59 10
	Kvitholm, lt. F, Fl. 128f.	63 1	7 14	Waigatch I., Balvanski Pt.	70 29	58 58
	Christiansund, lt. F 65f.	63 7	7 39	Samoyedes Peninsula, C. } Vengani	70 45	66 16
	Nightingale rks., outer	63 23	7 8	— Beli Ostrov I., C. Ivanoff...	73 24	71 35
	Grip, lt.	63 14	7 37	NOVAYA ZEMLYA.		
	Hav flue, rk.	62 51	6 11	C. Menchikoff	70 45	57 42
	Munk Holm, lt. F 38f.	63 27	10 24	North Moose Cape	72 13	51 50
	Trondhiem, Cathedral	63 25 8	10 23 7	Suchoi Noss	73 41	53 30
	Titter lld.	63 40	8 19	C. Speedwell	74 57	55 35
	Vigten Is., Wextr rks.	61 46	10 24	C. Nassau	76 20	61 39
	— NW extr. rks.	65 2	10 37	Orange Is.	77 2	67 43
	Prestøe, lt. F 39f.	64 47 4	11 8	C. Bismarck	76 19	68 56
	Lekøe, sum.	65 5	11 37	Matotchkin Strait, E entr.	73 8	56 30
	Hailhornet, pk.	65 5	12 9	Gessen Point	72 10	55 34
	Holibraken rk.	65 24	11 0	FRANCE,		
	Torgbatten Pk.	65 24	12 7	North Coast.		
	Sola I., sum.	65 40	11 45	Gravelines lt. F 95f.	51 0 3	2 6 7
	Svingleboen rk.	65 38	11 17	Calais, \square , F, sf., bell, lt. Fl. } (electric) 190f.	50 57 6	1 51 2
	Skal svee, rk.	65 59	11 21	C. Grisnez, lt. Fl. (electric) 226f.	50 52 2	1 35 2
	Træn Is., Soholm, lt. Fl. 118f.	66 26	12 0	Boulogne, \square 2, Column	50 44 5	1 37 2
	Hestmandø Pk.	66 32	12 50	Pt. Alpreck, lt. F, Fl. 161f.	50 41 9	1 34 0
	Kunna, sum.	66 57	13 32	Etaples, \square	50 32 9	1 38 7
	Lofoten lds., Skomvær, lt. Fl. } 159f.	67 24 2	11 54	Pt. de Touquet, 2 lts. F 174f.	50 31 7	1 35 7
	Lofoten Pt.	67 49 5	12 50	Pt. de Berck lt. Occ. 115f.	50 24 0	1 33 7
	Skraaven, sum. 600f.	68 9	14 44	Abbeville, Ch. of Notre Dame	50 7 1	1 50 0
	Trano I., N pt.	68 11 3	15 39	St. Valery sur Somme, \square	50 11 4	1 38 0
	W. Vago I., N pt.	68 20 5	15 59	Cayeux, lt. F, Fl. 92f.	50 11 7	1 31 0
	Lango I., W pt., rks. off.	68 37	14 14	Tréport, \square , lt. F 44f., sf.	50 3 9	1 22 2
	Andøe, N pt.	69 20	16 8	Dieppe, \square , W jetty, lt. F 43f., 70f.	49 56 0	1 5 2
	Tromsøe, Observatory	69 39 2	18 57 0	C. Ailly, lt. R 305f.	49 55 1	0 57 7
	Hvaløe, NW pt.	70 14 6	19 16			
	Hammerfest, Meridian pillar ..	70 40 1	25 40 5			
	Vandø, N pt.	70 17 6	19 36			
	Arnø, NE pt.	70 13	20 49			
	Sorøen I., W pt.	70 39	21 55			
	— N pt., or Tarhalsen ...	70 53	23 19			
	Rolfso Is., N pt., lt. F 141f.	71 6	23 59			
	Knivskierodden Pt.	71 11 0	25 40 0			
	NORTH CAPE	71 10 3	25 46 0			

MARITIME POSITIONS

(17)	Places	Lat. N	Lon.	(18)	Places	Lat. N	Lon. W
FRANCE, N. W. Coast @	St. Valéry en Caux, \square , F. Fl. 43f.	49°52'4	East 0°42'7	Morlaix, \square , lt. F 285f.	48°40'	3°53'	
	Fecamp, \square , Mt. de la Vierge, } F 374f. }	49 46'1	0 22'2	St. Pol de Léon, \square , Cath.	48 41'0	3 59'0	
	C. de la Heve, 2 lts. N19°E } 207f., F 396f. }	49 30'7	0 4'2	I. de Bas, EW 3m., lt., W } side, R ^r 223f. }	48 44'8	4 1'5	
	Havre, \square , lt. N jetty, bell....	49 29'3	0 6'7	I. Vierge, lt. F. Fl. 108f.	48 38'4	4 34'0	
	Pt. du Hoc, lt. F 39f.	49 28'7	0 11'5	Aberwrach, W lt. F ^r 59f.	48 36'9	4 34'5	
	PARIS OBSERVATORY	48 50'2	2 20'2	West Coast.			
	Quillebeuf, lt. F 33f.	49 28'4	0 31'7	Ushant, $\frac{3}{4}$ 4m., lt. Fl. (elc- tric) 272f. }	48 28'5	5 4	
	Honfleur, \square , lt. F 92f.	49 26	0 14	Kermorvan, lt. F 72f.	48 21'7	4 48	
	Month of the Orne, Church ...	49 16'6	0 15'2	Pt. St. Matthew, lt. R 177f. ...	48 19'8	4 46'2	
	Port Corseules, \square , lt. F 30f.	49 20'3	0 27'2	Brest, Observatory	48 23'6	4 29'2	
	Cæn, Abbey	49 11'2	0 21'0	I. de Sein, lt. F, Fl. 148f.	48 2'7	4 52'0	
	Pt. de Ver, lt. F, Fl. 138f.	49 20'5	0 31'0	Outer, or Wst. rk.	48 3	5 15	
	Arentan	49 18'4	1 14'5	Audierne, Church	48 1'4	4 32'5	
	St. Marcouf Is., $\frac{3}{4}$ 3m., lt. } Occ. 56f. }	49 29'9	1 8'7	Penmarc'h rks., lt. R 134f. ...	47 47'9	4 23	
	La Hougue, \square , lt. F 36f.	49 34'3	1 16'2	Glenan I., Penfiet I., lt. F, Fl. } 118f. }	47 44	3 57'0	
	Reville Redoubt, lt. F 36f.	49 36'4	1 13'7	Quimper Riv., Benodet, Ch....	47 52'6	4 6'7	
	C. Barfleur, lt. R 236f.	49 41'8	1 15'7	I'Orient, tower	47 44'7	3 21'0	
	Palée I., fort, lt. F 85f.	49 40'3	1 34'7	Port Louis, Church	47 42'5	3 21'0	
	Cherbourg, \square , Ch.	49 38'6	1 37'2	I. de Groix, $\frac{3}{4}$ 4m., lt. F } 193f. }	47 38'9	3 30'5	
	C. La Hague, I, lt. F 154f.	49 43'4	1 57'0	Port Haliguen, lt. E jetty, } F 39f. }	47 29'2	3 6'0	
Channel Is. @	Alderney I., $\frac{3}{4}$ 3m., St. Anne Ch.	49 42'9	2 12'2	Teignouse, lt. F, Fl. 59f.	47 27'5	3 2'5	
	Pierre au Vrac, rk.	49 41'6	2 17'0	Port Navalo, pt., lt. F 72f.	47 32'9	2 55'0	
	Caskets, T. lt. Fl. 120f., bell...	49 43'4	2 22'5	Peulan Pt., lt. F 68f.	47 31'0	2 30'0	
	Guernsey, Jerbourg tow. 390f.	49 25'3	2 33'0	Belle Isle, $\frac{3}{4}$ 10m., lt. Goul- far Bay, R 276f. }	47 18'7	3 13'5	
	Pleimmont, SW pt., guard ho.	49 25'3	2 41'0	— Port de Palais, lt. F 30f. ...	47 20'9	3 9'0	
	— St. Pierre, lt., S jetty, F 46f.	49 27'0	2 32'0	Hoedic I., $\frac{3}{4}$ 14m.	47 20'5	2 52'0	
	Herm I., NS $\frac{1}{4}$ m., mil.	49 28'0	2 27'7	I. Four rk., lt. R 79f.	47 17'9	2 38'0	
	Sercq I., $\frac{3}{4}$ 3m., Telegraph	49 25'5	2 22'7	Vannes, St. Peter's	47 39'5	2 45'2	
	Islet S, or Etat de Sercq	49 23'6	2 23'0	Guérande, Ch., 177f.	47 19'7	2 25'5	
	Jersey, St. Pierre, Ch.	49 12'5	2 11'7	Croisic, Church	47 17'7	2 30'7	
	— St. Helier's \square	49 11'3	2 7'0	Aiguillon tow., (on with the tour de Commerce, N32°E) } Port St. Nazaire, Mole, lt. } Occ. 26f. }	47 14'6	2 15'7	
	— C. Granoz, ruin	49 15'2	2 15'5	Port St. Nazaire, Mole, lt. } Occ. 26f. }	47 16'3	2 11'7	
	— NE pt., or Pt. de la Coupe	49 15'9	2 2'3	Paimbœuf, Church	47 17'3	2 2'0	
	— SE pt., Seymour tower ...	49 9'4	2 1'1	Nantes, Cathedral	47 13'1	1 33'0	
	Roches Douvres, EW 2m. rk., } mid. }	49 6'5	2 49	I. le Pilier I., lt. F, Fl. 105f. ...	47 2'6	2 21'5	
	Baronnie rks., EW 2m.	49 1	2 48	Noirmoustier I., S pt.	46 53'8	2 8'7	
	Chausey Is., [6m.], Grt. I., lt. } F, Fl. 121f. }	48 52'2	1 49'2	I. d'Yeu, $\frac{3}{4}$ 54m., St. Sau- veur Church	46 42'4	2 19'7	
	Minquiers rks., $\frac{3}{4}$ 5 l., NW } breakers }	48 59	2 19	— Lt. NW part, F 177f.	46 43'1	2 22'7	
	Maitresse Id.	48 58'3	2 3'7	St. Gilles sur Vie, Church ...	46 41'7	1 56'0	
	FRANCE, N. W. Coast @	St. Germain	49 14'2	1 35'7	Sables d'Olonne, Church	46 29'8	1 47'0
C. Carteret, I., lt. R 262f.		49 22'4	1 48'2	La Chaume, lt. F 105f.	46 29'7	1 47'5	
Coutances, Cath., 302f.		49 2'9	1 26'5	Rochebonne, W, or La Con- grée	46 13	2 29	
Granville, \square , C. Libou, lt. } F 154f. }		48 50'1	1 36'7	Pt. de Grouin du Cou, lt. } F 92f. }	46 20'8	1 28'0	
Mt. St. Michel		48 38'2	1 30'5	Pt. de l'Aiguillon, lt. F 43f. ...	46 16'1	1 12'5	
Canalle, Church		48 40'7	1 50'7	I. Rhe, $\frac{3}{4}$ 14m., Baleines, lt. } on N pt. Fl. 166f. }	46 14'7	1 33'5	
Herpin rk.		48 43	1 50	— Port St. Martin, lt. F 56f.	46 12'4	1 21'7	
St. Malo, \square , Church		48 39'0	2 1'5	— S pt., de Chauveau, lt. F 59f.	46 8'0	1 16'2	
La Conchée rk.		48 41	2 3	Rochelle, 2 lts. F 79f., 46f.	46 9'4	1 9'2	
C. Frehel, T, sum., lt. R 259f.		48 41'1	2 19'0	Oleron I., $\frac{3}{4}$ 16m., N pt., } Chassiron, lt. F 164f. }	46 2'8	1 24'5	
Grand Léon rk.		48 45'0	2 39'7	Aix I., lt. Fl. 66f.	46 0'6	1 10'5	
St. Briève, Cathedral		48 30'9	2 45'7	Rochefort, Hospital	45 56'6	0 57'7	
Horaine rk., beacon		48 53'6	2 55'0				
Heaux de Brehat, lt. F 148f.		48 54'5	3 5'0				
Treguier, Cathedral		48 47'3	3 13'7				
Seven Is., $\frac{3}{4}$ 4m., lt. F, Fl. 181f.		48 52'8	3 30				
Triagoz, shl., EW 4m., W extr.		48 53	3 44				

553

(19)	Places	Lat. N	Lon. W	(20)	Places	Lat. N	Lon. W
	Pt. de la Coubre, lt. F 121f.	45° 41'5	1° 15'2		Mt. Nossa Señora del alba, } 1670f.	42° 10'	8° 43'
	Cordonn. lt. (Riv. Gironde) } Rev. 194f.	45 35 2	1 10 2		Mt. Peneda, 4542f.	41 58	8 21
	Pte. de Grave, lt. Occ. 85f.	45 34 1	1 3 5		PORTUGAL.		
	Bordeaux, St. André 44 50 3	0 34 5			R. Mino, Pt. Picos, lt. F 56f.	41 52	8 52
	— OBSERVATORY 44 50 3	0 31 2			Viana, □, 2 lts. F 107f.	41 41	8 50
	Ba-sind'Arcachon, C Ferret, } lt. F 167f.	44 38 7	1 15 0		Mt. Destrello de Malhada, } 3602f.	40 53	8 11
	Bayonne, Cath. 43 29 5	1 28 5			Oporto, □ ¹² , Fort St. Joas } da Foz.	41 8 8	8 40 5
	Pt. St. Martin de Biarritz, } lt. Fl. 210f.	43 29 6	1 33 0		Aveiro, New Bar, □ ²¹ 40 39		8 44
	St. Jean de Luz, Church 43 23 3	1 39 7			Mt. Caramullo, 3274f. 40 32 5		8 12 5
	Socoa, lt. F 115f. 43 23 7	1 41 0			Mount Busaco, 1795f. 40 23		8 22
	SPAIN,				Coimbra, University 40 12 5		8 25 5
	North Coast.				C. Mondego, lt. F 302f. 40 11		8 55
	Fuenterabia, Ch. 43 21 7	1 47 2			Figueira, □ ¹⁹ , lt. F 36f. 40 9		8 51 5
	C. Higuiera, lt. R 197f. 43 23 7	1 48			Nazareth, 39 36		9 5 2
	Port Passage, □, C. La Plata, } lt. F 484f.	43 19 7	1 57 2		Burlings, lt. R 365f. 39 25 0		9 30 5
	C. Machichaco, 1, lt. F, Fl. } 268f.	43 27 0	2 50		C. Carvoeiro, pt., lt. F 180f. 39 21 8		9 24 2
	C. Villano, 1, A. 43 27	2 58			Monte Junto, 2185f. 39 11		9 3
	Bilbao, St. Nicholas Church. 43 15 8	2 54			Mafra 38 56		9 19
	Portugalete, □ 43 20 2	3 3			C. Roca, lt. R* 596f. 38 47		9 30
	Mt. Serantes 43 21	3 5			Mt. Cintra, sum. 1600f. 38 46		9 26 5
	Santona, □, Caballo Pt., lt. } F 85f.	43 28 0	3 27		Da Guña, lt. F 167f. 38 41 8		9 27
	C. Ajo, pt. 43 31 4	3 36			St. Julian, fort, lt. F 128f. 38 40 4		9 19 5
	Santander, □, mole 43 27 9	3 48 7			Lisbon, □, MARINE OBS., □ 38 42 2		9 8 5
	C. Mavor, E pt., lt. R 298f. 43 30	3 48			ROYAL OBSERVATORY 38 42 5		9 11 2
	C. Oyambre 43 25	4 21			C. Espichel, 1, A, lt. Fl. 535f. 38 24 9		9 13
	C. Prieto 43 28 7	4 51 5			Setubal, □ 38 32		8 53
	Pt. Samos, lt. F, Fl 370f. 43 30 7	5 7 2			C. Sines, 1, lt. F 130f. 37 57 5		8 53
	C. Lasres 43 34 2	5 18 2			Monchique Mtns., sum Foia, } 2959f.	37 18	8 34
	Gijon, lt. F 167f. 43 35 5	5 38			C. St. Vincent, 1, lt. R } 221f.	37 1	8 57 7
	C. Peñas, 1, lt. R 343f. 43 42 0	5 49 5			Sagra's Pt., Semaphore 36 59 7		8 55
	C. Busta, A, 1, lt. F, Fl. 307f. 43 36	6 27 5			Lagos, Piedade Pt. 37 4 7		8 38 2
	Tapia I., lt. F, Fl. 77f. 43 35 5	6 55 2			C. Carvoeiro, tower 37 5 2		8 24 7
	Rivadeo, □, I. Pancha, lt. } F 79f.	43 34 7	7 2		C. Sta. Maria, 1, lt. F 109f. 36 58 5		7 49 7
	Mondigo Mt., 1890f. 43 32	7 8			Mt. Figo, 1365f. 37 6		7 48 7
	San Ciprian, lt. F 121f. 43 43	7 25 7			SPAIN,		
	Mt. Faro, 1790f. 43 43	7 35			South Coast.		
	Port Barquero, □, La Estaca, } lt. R 306f.	43 47 2	7 41 5		R. Guadiana, □ ¹⁰ , Canela I., } 2 lts. F 109f., 43f.	37 11 5	7 24
	Port Vivero, □, town 43 40 5	7 36			Palos 37 13 5		6 53
	C. Ortegal, A, 1, tow. (S } 1' 4 of pt.) 43 46	7 54 7			R. Guadalquivir, San Lucar } Lookout 36 46 2		6 21
	C. Prior, 1, lt. F 416f. 43 34 1	8 18 5			Rota, pier 36 36 6		6 21 5
	Monte Venoso, 785f. 43 29	8 19			CADIZ, □, Observatory 36 32 0		6 17 2
	Ferrol, □, mole 43 28 5	8 14 2			— S FERNANDO 36 27 7		6 12 5
	Coruña, □, lt. F, Fl. 332f. 43 22 5	8 24 5			St. Sebastian, lt. F, Fl. 1		

SPAIN, N. Carol. 6

MARITIME POSITIONS

(21)	Places	Lat. N	Lon.	(22)	Places	Lat. N	Lon. E
SPAIN. E. Coast	SPAIN.				FRANCE.		
	Torre Nueva	36° 12' 3	West 5° 19' 7	FRANCE, S. Coast	St. Pedro de Roda, fort.....	42° 19' 0	3° 10'
	C. Sardinia, tower	36 18 7	5 16		C. Sernella	42 21 0	3 13
	Doncella, lt. F, Fl. 69f.	36 25	5 9		C. Bearn, lt. F 751f.	42 31 0	3 7 5
	Sierra Bermeja, Mt., 4728f. ...	36 29	5 13		Port Vendres, lt. Fl. 98f.	42 31 3	3 7 0
	Fuengirol, Castle.....	36 33	4 37		Perpignan	42 43	2 53
	Sierra de Mijas	36 38	4 40		La Nouvelle, lt. F 50f.	43 0 8	3 4 0
	Malaga, \square , mole, lt. F, Fl. } 125f.	36 43	4 24		Narbonne, Cathedral.....	43 11 1	3 0 2
	Velaz Malaga, ∇ n, lt. F 41f.	36 43	4 7		Fort Brecon, lt. SE bast., F 59f.	43 15 5	3 30 0
	C. Sacratif, Δ , 1, lt. F, Fl. } 320f.	36 42	3 28		Aigle, Mt., lt. R 413f.	43 17 9	3 30 2
	Adra, fort, lt. F 55f.	36 44	3 1		Cette, \square , Ft. Louis, lt. F 105f.	43 23 8	3 42 2
	Alboran I., lt. F 115f.	38 58	3 2		Montpellier	43 37	3 53
	Pt. Salincl, lt. F, Fl 105f.	36 41 2	2 42		Aigues Mortes, lt. F 33f.	43 32 0	4 8 0
	Almoria, Citadel.....	36 50 3	2 28 6		W. Mo. of Rhone, Camargue, } 2 lts. F 125f., 38f.	43 20 7	4 41 0
	C. de Gata, lt. R 194f.	36 43	2 11 2		P. de Bouc, \square , 2 lts. ent. F } 49f., 95f.	43 23 6	4 59 2
	Port Genoves, 1, Castle	36 45	2 6 2		C. Couronne	43 19	5 3
	Pt. Mesa, lt. F, Fl. 725f.	36 56	1 54 5		Marseille, St. Jean Ft., F 30f.	43 17 7	5 21 7
	Port Aguilas, Castle	37 23 4	1 34 5		— OBSERVATORY	43 18 3	5 23 7
	C. de Cope, 823f.	37 25 3	1 28		Planner I., lt. Fl. 207f.	43 11 9	5 14 0
	C. Tinosa, Δ , 1, lt. F 480f.	37 32	1 7		Mt. St. Michael, Semaph., 13411.	43 13	5 22
	Cartagena, Escambrera I., } lt. F 223f.	37 33 5	0 58		I. Rion, EW 1m., tower	43 10	5 23
	C. de Pal s, lt. R 263f.	37 37 5	0 41		Cassia, \square , Port, 2 lts. F 92f., } 31f.	43 12 8	5 32 0
	C. Cervera	38 0	0 40		Cassidaigne \square	43 8 7	5 33 0
	I. Plana, E. ex r. of rks. $\frac{2}{3}$ } 1, F, Fl. 90f.	38 10	0 28		Ciotat Port, lt. F 40f.	43 10 3	5 36 7
	Alicante, Castle, (lt. F 26f.)....	38 20 3	0 28 7		Bandol, Church	43 8 2	5 45 5
	Mt. Roldan, gup.....	38 36	East 0 12		C. Sicie, Semaphore	43 3 2	5 51 0
	C. Nao, E pt.	38 43	0 14		Toulou, \square , Observatory	43 7 5	5 56 0
	C. St. Antonio, lt. R 571f.	38 43 5	0 12		Grd. Rileau, lt. F 112f.	43 1	6 8
	Mongó, Mt., 2497f.	38 48	0 8		Porquerolles I., $\frac{2}{3}$ 4m., S pt., } lt. F, Fl. 262f.	42 59 0	6 12 5
	C. Callera, tow., lt. F 91f.	39 11	West 0 12 7		Port Cros I., $\frac{2}{3}$ 2 1/2 m., Fort } Vigie	42 59 9	6 24 2
	Valencia, lt. F 39f., mole	39 26 8	0 19		Titan I., $\frac{2}{3}$ 4 1/2 m., NE part, } lt. F 246f.	43 2 8	6 30 7
	C. Canet, tower	39 43 0	0 9		C. Camarat, lt. R 426f.	43 12 0	6 40 7
	C. Oropesa, lt. F, Fl 74f.	40 4	0 9		St. Tropez	43 14	6 34
	Peñíscola tow.	40 23 0	0 25		Frejus, ∇	43 25	6 46
	Columbretes Is., lt. F 262f.	39 54	0 42		C. Roux, 1, ∇ , sum. 1600f.	43 28	6 55
	Port Alfaques, Pt. de la Baña	40 33 5	0 39		Cannes, S tower	43 32 9	7 1 0
	Ebro R., S passage	40 41 0	0 53		Lenin Is., EW 2m., S extr. rks.	43 30	7 3
	C. Rock, tower	40 49 0	0 45		C. Garoupe, lt. F 338f.	43 33 8	7 8
	C. Tortosa, Buda, lt. Rev. } 174f.	40 42 4	0 54		Antibes, \square , herb. lt. F, Fl. 49f.	43 35 1	7 7 7
	C. Salou, pt., lt. F, Fl. 139f.	41 3 0	1 10		St. Laurent du Var	43 40 7	7 11 0
	Tarragona, lt. F 54f.	41 7	1 15		Nice, St. Francis Church	43 42 0	7 17 0
	Barcelona, \square , mole lt. F, } Fl. 43f.	41 22 6	2 11		— OBSERVATORY, Mont-gros....	43 43 3	7 18
	Mt. Jui, fort	41 21 8	2 10		Villa Franca, \square	43 42	7 18
	Ma'aro	41 32 4	2 27		C. Ferrat, lt. Rev. 229f.	43 40 0	7 19 5
	C. Tosa, tower	41 43 2	2 58		Monaco	43 43 0	7 27 0
	Pt. Molno	41 49 6	3 8				
	C. St. Sebastian, Δ sum., lt. } F, Fl. 548f.	41 53	3 12				
	Medas Is., $\frac{2}{3}$ 1m., S & E extr.	42 3 2	3 14				
	La Escala	42 7	3 8				
	C. Norfeo, Δ , 1, E pt.	42 14	3 17				
	Cadaqués, \square , Church	42 17	3 17				
	C. de Creux, lt. F, Fl. } 285f.	42 19 2	3 19				
ICIZIA	BALZARIC ISLES.			ICIZIA	Formentera I., $\frac{2}{3}$ 3m., SE pt., } lt. F 450f.	38 39	1 35
					— S pt., or Pt. Anguila, 1	38 38	1 23
					Iviza, Port St. Antonio, \square , } Conejera I., lt. Rev. 289f.	38 59 4	1 13 0
					— Grosa Pt., lt. Int. 180f.	39 5	1 36
					Iviza, \square , Castle	38 54 3	1 26 7
					Cabrera I., $\frac{2}{3}$ 3 1/2 m., 564f., Pt. } Ansiola, lt. Rev. 404f.	39 7 2	2 55

MARITIME POSITIONS

(23)		Places	Lat. N	Lon. E	(24)		Places	Lat. N	Lon. E	
Majorca		Majorca, C. Sallua, l, $\frac{1}{2}$, lt. } F 50f.	39° 16'	3° 4'	C. of Genoa		Calvi, Pt. Rivellata, lt. F 289f.	42° 35'2"	8° 43'5"	
		C. Blanco, l, lt. F 292f.	39 22	2 47			C. Rosso, W pt.	42 14'3"	8 32'5"	
		Palma, mole, lt. F 35f.	39 34'1"	2 38'5"			Sanguinaires Is., $\frac{1}{2}$ lm., lt. } F, Fl. 321f.	41 52'8"	8 35'7"	
		C. Cala Figuera, T, lt. F 115f.	39 28	2 32			Ajaccio, Cathedral.	41 55'0"	8 41'7"	
		Dragonera I., $\frac{1}{2}$ 2m., lt. F, } Fl. 1180f.	39 35	2 19			C. Muro, SW pt.	41 44'5"	8 39'5"	
		Mt. Galatzo, 33f3f.	39 39	2 31			C. Campo Moro, \square , tower	41 38'5"	8 48'5"	
		C. Formenton, l, lt. R 592f.	39 58	3 13			Pt. Senetese, h, extr.	41 34'0"	8 47'0"	
		C. Pera, l, lt. F, Fl. 241f.	39 43	3 28'5"			C. Feno, lt. F 63f.	41 23'8"	9 5'7"	
							Bonifacio, \square , lt. F 95f.	41 23'8"	9 9'2"	
							Pertusato, lt. R 325f.	41 22'2"	9 11'2"	
Minorca		Minorca, C. Dartach, l, T, } lt. F, Fl. 71f.	39 55	3 49'5"	C. of Genoa		Port. Sta. Manza, \square , Pt. Ca- } picciolo, tower	41 25'1"	9 15'7"	
		C. Bajoli, l, tow. 256f.	40 1	3 48			Porto Vecchio, \square , Chiappe Pt., } lt. F, Fl. 217f.	41 36	9 22	
		C. Cavalleria, h, l, lt. F 309f.	40 5'8"	4 5'5"			E. extr. Fiorentina, tower.	42 17'0"	9 33'7"	
		Mahon, \square , lt. F 73f.	39 52'5"	4 18'0"			Bastia, \square , Dragon bastion, } lt. F 82f.	42 41'8"	9 27'0"	
		Ayre I., EW $\frac{1}{2}$ in., lt. Rev. 171f.	39 48	4 17			Monte Stello, 4532f.	42 47'5"	9 25'0"	
SARDINIA.										
SARDINIA		Razzoli I., lt. F 232f.	41 18'3"	9 20'7"	G. of Genoa		ITALY. West Coast.			
		C. della Testa, T, lt. F, Fl. 220f.	41 15	9 9'2"			C. St. Martin.	43 43	7 33	
		Port Torres, \square , lt. F 47f.	40 50'2"	8 24'7"			Ventimiglia Pt.	43 45	7 43	
		A-luara I., $\frac{1}{2}$ 10m., 1239f.	41 5'8"	8 18'2"			Mt. Graude, 3100f.	43 50	7 37	
		C. Falcone, tow. 610f.	40 57'3"	8 12'2"			C. del Armi.	43 49	7 54	
		C. Argentera, sum.	40 43'7"	8 9'0"			Port Maurizio, mole bd.	43 53'2"	7 59'0"	
		C. Caccia, T, P. Conte, \square , sum.	40 33'5"	8 10'2"			C. de la Mele, h	43 58	8 11	
		Alghero, Cathedral	40 33'5"	8 19'2"			Gallinara I., tower.	44 2'1"	8 13	
		C. Marargiu, rk.	40 19'7"	8 23'5"			Finale, Church	44 9'9"	8 19'0"	
		C. Mannu, tow. on N pt.	40 2'5"	8 24'0"			Noli, Conv. St. Francisco	44 11'9"	8 22'7"	
		Mal di ventre, rks. $\frac{1}{2}$ 3m., mid.	39 59	8 18			Vado, Fort St. Lorenzo	44 15'5"	8 24'5"	
		Coscio di Donna, rk. [$\frac{1}{2}$ c.]	39 52'8"	8 17'2"			Savona, \square 12, Citadel.	44 18'4"	8 27'7"	
		C. St. Marco, tower	39 51'2"	8 26'5"			Polla rk.	44 25'0"	8 46'0"	
		C. Frasca	39 46	8 27			Genoa, \square 3 lts., Int. 340f., } F 92f., F 69f.	44 24	8 54'0"	
		Oristano, grt. tower	39 54'3"	8 31'7"			Pt. Chiappa, sum.	44 20'0"	9 10'5"	
		Mt. Arcueto (or finger of } Oristano), 2713f.	39 35'7"	8 33'5"			C. Porto Fino, fort.	44 18'2"	9 14'2"	
		C. Pecora, pt., tow.	39 27'1"	8 25'2"			Sestri di Levante, fort.	44 16'4"	9 25'5"	
		St. Pietro I., NS $\frac{1}{2}$ m., 702f.	39 9'7"	8 17'7"			Port Veneri, \square , N entr.	44 3'2"	9 52'7"	
		St. Antioco I., NS 9m., S } sum. 781f.	38 58'3"	8 26'0"			Tino I., lt. Fl. (electric) 384f.	44 1	9 51'0"	
		Toro rk., T, 500f.	38 51'6"	8 25'2"			Spezzia, \square , Castle	44 6'3"	9 52'2"	
		C. Teulada, l, T, sum. 725f.	38 51'9"	8 39'2"			Monte Aluissimo, 5213f.	44 3	10 14	
		Port Malfatano, \square , tow.	38 53'1"	8 48'7"			Viareggio, Sanità	43 51'8"	10 15'7"	
		C. Spartivento, lt. F 264f.	38 52'5"	8 52'5"			Arno R., mouth, fort.	43 40'8"	10 16'7"	
		Cagliari, $\frac{1}{2}$ St. Pancras Ch.	39 13'2"	9 7'7"			Pisa, leaning tow.	43 43'5"	10 24'0"	
		Cavoli I. (off C. Carbonara), tow.	39 6'1"	9 31'5"			Florence, Duomo	43 46'6"	11 15'5"	
		C. Ferrato, l, 80f. pt.	39 17'5"	9 40'0"			Malora, shoul, lt. F 60f.	43 32'6"	10 12'7"	
		Mt. Seven Brothers, 3186f.	39 18'5"	9 26'5"			Leghorn, \square , lt. R 154f.	43 32'7"	10 17'7"	
		C. Bellavista, lt. F 541f.	39 55'8"	9 43'5"			Gorgona I., NS $\frac{1}{2}$ m., h, mid.	43 25'8"	9 53'5"	
		Mt. Gennargentu, 6102f.	40 1	9 19			Val di Vetro rf., $\frac{1}{2}$ 3m., W pt.	43 18'2"	10 21'7"	
		C. Comino, pt.	40 31'4"	9 50'5"			Castagnetto, fort.	43 10'7"	10 32'7"	
		Limbarru, pk. 4331f.	40 51'0"	9 11'0"			C. Buia, tower	42 59'7"	10 29'7"	
		Tavolara I., $\frac{1}{2}$ $3\frac{1}{2}$ m., E pt.	40 54'8"	9 45'0"			Piombino, paluce	42 55'7"	10 31'7"	
		C. Figari, sum.	40 59'9"	9 39'7"			C. Troja, tower	42 48'1"	10 44'5"	
		Rock	41 16'9"	9 29'0"			Castiglione, fort.	42 46'0"	10 53'0"	
		Caprera I., NS 5m., sum.	41 12'9"	9 29'0"			R. Ombrone, mouth	42 39	11 0'5"	
		Madalena I., old fort.	41 13'4"	9 24'0"			Formiche, $\frac{1}{2}$ 2m., N one 32f.	42 34'6"	10 53	
CORSICA.										
C. Corso, Giraglia I., lt. R } 269f.			43 1'8"	9 24'2"			Talamone	42 32'3"	11 8	
		St. Fiorenza, centre of town.	42 41'0"	9 18'0"			St. Stefano, centre of town.	42 26'4"	11 7'2"	
		Pt. Perallo	42 44'1"	9 13'4"			Mt. Argentario, telegraph.	42 23'2"	11 10'5"	
							Capraia I., $\frac{1}{2}$ 4m., fort.	43 3'2"	9 50'5"	
								Palmajola I., NS $\frac{1}{2}$ m., lt. } F, Fl. 334f.	42 51'9"	10 28'7"
								Elba, N extr., or C. Vira.	42 52'6"	10 24'7"

MARITIME POSITIONS

(21)	Places	Lat. N	Lon.	(22)	Places	Lat. N	Lon. E
SPAIN.				FRANCE.			
			West				
Torre Nueva	36° 12' 3"	5° 19' 7"		St. Pedro de Roda, fort.....	42° 19' 0"	3° 10'	
C. Sardinia, tower	36 18 7	5 16		C. Sernella	42 21 0	3 13	
Doncella, lt. F, Fl. 59f.	36 25	5 9		C. Bearn, lt. F 751f.	42 31 0	3 7 5	
Sierra Bermeja, Mt., 4728f. ...	36 29	5 13		Port Vendres, lt. Fl. 98f.	42 31 3	3 7 0	
Fuengirol, Castle	36 33	4 37		Perpignan	42 43	2 53	
Sierra de Mijas	36 38	4 40		La Nouvelle, lt. F 50f.	43 0 8	3 4 0	
Malaga, \square , mole, lt. F, Fl. } 125f.	36 43	4 24		Narbonne, Cathedral	43 11 1	3 0 2	
Velaz Malaga, $\$$ N, lt. F 411.	36 43	4 7		Fort Brescon, lt. SE bast., F 59f.	43 15 5	3 30 0	
C. Sacratif, Δ , 1, lt. F, Fl. } 320f.	36 42	3 28		Agde, Mt., lt. R 413f.	43 17 9	3 30 2	
Adra, fort, lt. F 55f.	36 44	3 1		Cette, \square , Ft. Louis, lt. F 105f.	43 23 8	3 42 2	
Alboran I., lt. F 115f.	38 58	3 2		Montpellier	43 37	3 53	
Pt. Sabinel, lt. F, Fl 105f.	36 41 2	2 42		Aigues Mortes, lt. F 33f.	43 32 0	4 8 0	
Almeria, Citadel	36 50 3	2 28 6		W. Mo. of Rhone, Camargue, } 2 lts. F 125f., 38f.	43 20 7	4 41 0	
C. de Gata, lt. R 194f.	36 43	2 11 2		P. de Bouc, \square , 2 lts. eut. F } 49f., 95f.	43 23 6	4 59 2	
Port Genoves, 2, Castle	36 45	2 6 2		C. Couronne	43 19	5 3	
Pt. Mesa, lt. F, Fl. 725f.	36 56	1 54 5		Marseille, St. Jean Ft., F 30f.	43 17 7	5 21 7	
Port Aguilas, Castle	37 23 4	1 34 5		— OBSERVATORY	43 18 3	5 23 7	
C. de Cope, 823f.	37 25 3	1 28		Planer I., lt. Fl. 207f.	43 11 9	5 14 0	
C. Timos, Δ , 1, lt. F 480f.	37 32	1 7		Mt. St. Michael, Semaph., 13411.	43 13	5 22	
Cartagena, Escombrera I., } lt. F. 223f.	37 33 5	0 58		I. Riou, E.W. 1m., tower	43 10	5 23	
C. de Pal s, lt. R 263f.	37 37 5	0 41		Cassis, \square , Port, 2 lts. F 92f., } 31f.	43 12 8	5 32 0	
C. Cervera	38 0	0 40		Cassidaigne \square	43 8 7	5 33 0	
I. Plana, E. ex. r. of rks. $\$$ } 1, F, Fl. 90f.	38 10	0 28		Ciorat Port, lt. F 40f.	43 10 3	5 36 7	
Alicante, Castle, (lt. F 26f.) ...	38 20 3	0 28 7		Banol, Church	43 8 2	5 45 5	
Mt. Roldan, gap	38 36	0 12	East	C. Scie, Semaphore	43 3 2	5 51 0	
			West	Toulou, \square , Observatory	43 7 5	5 56 0	
C. Nao, E pt.	38 43	0 14		Grd. Ribeau, lt. F 112f.	43 1	6 8	
C. St. Antonio, lt. R 571f. ...	38 48 5	0 12		Porquerolles I., $\$$ 4m., S pt., } lt. F, Fl. 262f.	42 59 0	6 12 5	
Mongó, Mt., 2497f.	38 48	0 8		Port Crois I., $\$$ 2 $\frac{1}{2}$ m., Fort } Vigie	42 59 9	6 24 2	
			Fast	Titan I., $\$$ 4 $\frac{1}{2}$ m., NE part, } lt. F 246f.	43 2 8	6 30 7	
C. Cullera, tow., lt. F 91f.	39 11	0 12 7		C. Camarat, lt. R 426f.	43 12 0	6 40 7	
Valencia, lt. F 39f., mole	39 26 8	0 19		St. Tropez	43 14	6 34	
C. Canet, tower	39 43 0	0 9		Frejus, $\$$	43 25	6 46	
				C. Roux, 1, $\$$, sum. 1600f.	43 28	6 55	
C. Oropesa, lt. F, Fl 74f.	40 4	0 9		Cannes, S tower	43 32 9	7 1 0	
Pefiscola tow.	40 23 0	0 25		Lenin Is., E.W. 2m., S extr. rks.	43 30	7 3	
Columbretes Is., lt. F 262f. ...	39 54	0 42		C. Garoupe, lt. F 338f.	43 33 8	7 8	
Port Alfauque, Pt. de la Baña ..	40 33 5	0 39		Antibes, \square , 10, harb. lt. F, Fl. 49f.	43 35 1	7 7 7	
Ebro R., S passage	40 41 0	0 53		St. Laurent du Var	43 40 7	7 11 0	
C. Rock, tower	40 49 0	0 45		Nice, St. Francis Church	43 42 0	7 17 0	
C. Tortosa, Buda, lt. Rev. } 174f.	40 42 4	0 54		— OBSERVATORY, Mont-gros... ..	43 43 3	7 18	
C. Salou, pt., lt. F, Fl. 139f.	41 3 0	1 10		Villa Franca, \square	43 42	7 18	
Tarragona, lt. F 54f.	41 7	1 15		C. Ferrat, lt. Rev. 229f.	43 40 0	7 19 5	
Barcelona, \square , mole lt. F, } Fl. 43f.	41 22 6	2 11		Monaco	43 43 0	7 27 0	
Mt. Jui, fort	41 21 8	2 10					
Ma'aro	41 32 4	2 27					
C. Tosi, tower	41 43 2	2 58					
Pt. Mol no	41 49 6	3 8					
C. St. Sebastian, Δ sum., lt. } F, Fl. 548f.	41 53	3 12					
Medas Is., $\$$ 1m., S & E extr.	42 3 2	3 14					
La Escala	42 7	3 8					
C. Norfeo, Δ , 1, E pt.	42 14	3 17					
Cadaqués, \square , Church	42 17	3 17					
C. de Creux, lt. F, Fl. } 285f.	42 19 2	3 19					

TABLE 10

MARITIME POSITIONS							
(23)	Places	Lat. N	Lon. E	(24)	Places	Lat. N	Lon. E
Majorca	Majorca, C. Salinas, l, $\frac{1}{2}$, lt. } F 50f.	39° 16'	3° 4'	Corseica	Calvi, Pt. Rivellata, lt. F 289f.	42° 35' 2	8° 43' 5
	C. Bianco, l, lt. F 292f.	39 22	2 47		C. Rosso, W pt.	42 14' 3	8 32' 5
	Palma, mole, lt. F 35f.	39 34' 1	2 38' 5		Sanguinaires Is., $\frac{1}{2}$ 1m., lt. } F, Fl. 321f.	41 52' 8	8 35' 7
	C. Cala Figuera, T. lt. F 115f.	39 28	2 32		Ajaccio, Cathedral	41 55' 0	8 41' 7
	Dragonera I., $\frac{1}{2}$ 2m., lt. F, } Fl. 1180f.	39 35	2 19		C. Muro, SW pt.	41 44' 5	8 39' 5
	Mt. Galatzo, 33f3f.	39 39	2 31		C. Campo Moro, $\frac{1}{2}$, tower ...	41 38' 5	8 48' 5
	C. Formenton, l, lt. R 592f.	39 58	3 13		Pt. Seneccio, h, extr.	41 34' 0	8 47' 0
	C. Pera, l, lt. F, Fl. 241f. ...	39 43	3 28' 5		C. Feno, lt. F 63f.	41 23' 8	9 5' 7
Minorca	Minorca, C. Dartach, l, T, } lt. F, Fl. 71f.	39 55	3 49' 5	G. of Genoa	Bonifacio, $\frac{1}{2}$, lt. F 95f.	41 23' 8	9 9' 2
	C. Bajoli, l, tow. 256f.	40 1	3 48		Pertusato, lt. R 325f.	41 22' 2	9 11' 2
	C. Cavalleria, h, l, lt. F 309f.	40 5' 8	4 5' 5		Port. Sta. Manza, $\frac{1}{2}$, Pt. Ca- picciolo, tower	41 25' 1	9 15' 7
	Mahon, lt. F 73f.	39 52' 5	4 18' 0		Porto Vecchio, $\frac{1}{2}$, Chiappe Pt., lt. F, Fl. 217f.	41 36	9 22
	Ayre L, EW $\frac{1}{2}$ in., lt. Rev. 171f	39 48	4 17		E. extr. Fiorentina, tower....	42 17' 0	9 33' 7
SARDINIA.							
SARDINIA	Razzoli I., lt. F 232f.	41 18' 3	9 20' 7	G. of Genoa	ITALY. West Coast.		
	C. della Testa, T, lt. F, Fl. 220f.	41 15	9 9' 2		C. St. Martin	43 43	7 33
	Port Torres, $\frac{1}{2}$, lt. F 47f.	40 50' 2	8 24' 7		Ventimiglia Pt.	43 45	7 43
	A. inara I., $\frac{1}{2}$ 10m., 1239f. ...	41 5' 8	8 18' 2		Mt. Graude, 3100f.	43 50	7 37
	C. Falcone, tow. 610f.	40 57' 3	8 12' 2		C. del Armi.	43 49	7 54
	C. Argentera, sum.	40 43' 7	8 9' 0		Port Maurizio, mole hd.	43 53' 2	7 59' 0
	C. Caccia, T, P. Conte, $\frac{1}{2}$, sum.	40 33' 5	8 10' 2		C. de la Mele, h	43 58	8 11
	Alghero, Cathedral	40 33' 5	8 19' 2		Gallinara I., tower	44 2' 1	8 13
	C. Marargiu, rk.	40 19' 7	8 23' 5		Finale, Church	44 9' 9	8 19' 0
	C. Mannu, tow. on N pt.	40 2' 5	8 24' 0		Noli, Conv. St. Francisco	44 11' 9	8 22' 7
	Mal di ventre, rks. $\frac{1}{2}$ 3m., mid.	39 59	8 18		Vado, Fort St. Lorenzo	44 15' 5	8 24' 5
	Coscio di Donna, rk. [$\frac{1}{2}$ c.] ...	39 52' 8	8 17' 2		Savona, $\frac{1}{2}$, Citadel.	44 18' 4	8 27' 7
	C. St. Marco, tower	39 51' 2	8 26' 5		Polla rk.	44 25' 0	8 46' 0
	C. Frasca	39 46	8 27		Genoa, $\frac{1}{2}$ 3 lts., Int. 340f., F 92f., F 69f.	44 24	8 54' 0
	Oristano, grt. tower	39 54' 3	8 31' 7		Pt. Chiapa, sum.	44 20' 0	9 10' 5
	Mt. Arcueto (or finger of } Oristano), 2713f.	39 35' 7	8 33' 5		C. Porto Fino, fort.	44 18' 2	9 14' 2
	C. Pecora, pt., tow.	39 27' 1	8 25' 2		Sestri di Levante, fort	44 16' 4	9 25' 5
	St. Pietro I., NS $\frac{1}{2}$ m., 702f.	39 9' 7	8 17' 7		Port Venere, $\frac{1}{2}$, N entr.	44 3' 2	9 52' 7
	St. Antioch I., NS 9m., S } sum. 781f.	38 58' 3	8 26' 0		Tino I., l, Fl. (electric) 384f.	44 1	9 51' 0
	Toro rk., T, 500f.	38 51' 6	8 25' 2		Spezzia, $\frac{1}{2}$, Castle	44 6' 3	9 52' 2
	C. Teulada, l, T, sum. 725f.	38 51' 9	8 39' 2		Monte Altissimo, 5213f.	44 3	10 14
	Port Maltatano, $\frac{1}{2}$, tow.	38 53' 1	8 48' 7		Viareggio, Sanità	43 51' 8	10 15' 7
	C. Spartivento, lt. F 264f.	38 52' 5	8 52' 5		Arno R., mouth, fort.	43 40' 8	10 16' 7
	Cagliari, $\frac{1}{2}$, St. Pancras Ch.	39 13' 2	9 7' 7		Pisa, leaning tow.	43 43' 5	10 24' 0
	Cavoli I. (off C. Carbonara), tow.	39 6' 1	9 31' 5		Florence, Duomo	43 46' 6	11 15' 5
	C. Ferrato, l, 80f. pt.	39 17' 5	9 40' 0		Malora, shoal, lt. F 60f.	43 32' 6	10 12' 7
	Mt. Seven Brothers, 3186f.	39 18' 5	9 26' 5		Leghorn, $\frac{1}{2}$, lt. R. 154f.	43 32' 7	10 17' 7
	C. Bellavista, lt. F 541f.	39 55' 8	9 43' 5		Gorgona I., NS $\frac{1}{2}$ m., h, mid.	43 25' 8	9 53' 5
	Mt. Gennargentu, 6102f.	40 1	9 19		Val di Vetro rf., $\frac{1}{2}$ 3m., W pt.	43 18' 2	10 21' 7
	C. Comino, pt.	40 31' 4	9 50' 5		Castagnetto, fort.	43 10' 7	10 32' 7
	Limbarra, pk. 4331f.	40 51' 0	9 11' 0		C. Buia, tower	42 59' 7	10 29' 7
	Tavolara I., $\frac{1}{2}$ 3 $\frac{1}{2}$ m., E pt. ...	40 54' 8	9 45' 0		Piombrino, palace	42 55' 7	10 31' 7
	C. Figari, sum.	40 59' 9	9 39' 7		C. Troja, tower	42 48' 1	10 44' 5
	Rock	41 16' 9	9 29' 0		Castiglione, fort.	42 46' 0	10 53' 0
	Caprera I., NS 5m., sum.	41 12' 9	9 29' 0		R. Ombrone, mouth	42 39	11 0' 5
	Madalena I., old fort.	41 13' 4	9 24' 0		Formiche, $\frac{1}{2}$ 2m., N one 32f.	42 34' 6	10 53
CORSIKA.							
C. Corso, Giraglia I., lt. R } 269f.		43 1' 8	9 24' 2		Talamone	42 32' 3	11 8
St. Fiorenza, centre of town...	42 41' 0	9 18' 0	St. Stefano, centre of town ...		42 26' 4	11 7' 2	
Pt. Perallo	42 44' 1	9 13' 4	Mt. Argentario, telegraph.		42 23' 2	11 10' 5	
	Capraia I., $\frac{1}{2}$ 4m., fort.	43 3' 2	9 50' 5		Palma Jola I., NS $\frac{1}{2}$ m., lt. } F, Fl. 334f.	42 51' 9	10 28' 7
	Elba, N extr., or C. Vita	42 52' 6	10 24' 7				

MARITIME POSITIONS

(25)	Places	Lat. N	Lon. E	(26)	Places	Lat. N	Lon. E	
Elba and Is. adjacent	Elba, Porto Ferrajo, \square , lt. F, }	42° 48' 3"	10° 20' 5"	Lipari Is. @	Vulcano I., 1601f., lt. F, Fl. ...	38° 22' 1"	14° 59' 0"	
	Stella fort, 200f.				Felicudi I., 2598f., Church ...	38° 34' 1"	14° 34' 2"	
	— W. extr., or Pt. Mortigliano	42° 46' 2"	10° 6' 2"		Alicudi I., summit, 2172f.	38° 32' 7"	14° 21' 1"	
	— Port Longone, Citad. Ch.	42° 45' 8"	10° 24' 2"		Ustica I., $\frac{1}{2}$ 3m., Uomo- }	38° 42' 5"	13° 11' 7"	
	— Mt. Calamità	42° 43' 8"	10° 23' 7"		Morto pt., lt. F, Fl. 328f. }			
	Pianosa I., NS 3m., $\frac{1}{2}$ lt. Rev. }	42° 35'						
	140f.							
	Africa rk., or W. Formiche, 6f.	42° 21' 5"	10° 3' 7"		SICILY.			
	Montecristo I., $\frac{1}{2}$ 3m., 2076f.	42° 20' 3"	10° 18' 5"		Faro I., lt. F, Fl. 147f.	38° 15' 8"	15° 39' 7"	
	Giglio I., $\frac{1}{2}$ 5m., S pt.	42° 19' 2"	10° 55' 1"		Messina, \square , lt. F, Fl. 134f. ...	38° 11' 2"	15° 35' 2"	
Gianuti I., $\frac{1}{2}$ 2m., S pt.	42° 14' 2"	11° 6' 5"	Scaletta, fort	38° 1' 7"	15° 27' 7"			
Formica di Burano	42° 23' 0"	11° 13' 5"	Trizzi Tower	37° 34' 4"	15° 11' 2"			
ITALY, W. Coast @	Civita Vecchia, \square , lt. F, Fl. 121f.	42° 5' 7"	11° 4' 7"	Mt. Etna, 10,874f.	37° 45'	15° 0' 2"		
	C. Linaro, rf. [$\frac{1}{2}$ m.]	42° 2'	11° 50'	Catania, Sciara Biscari, lt. F, }	37° 29'	15° 6'		
	Tiber, R. Fiumicino, 2 lts. F.	41° 46'	12° 13' 5"	Fl. 98f.				
	Rome, St. Peter's, dome	41° 54' 2"	12° 27' 2"	C. Sta. Croce, lt. F 91f.	37° 14' 5"	15° 16'		
	— OBSERVATORY	41° 53' 9"	12° 28' 7"	Augusta Port, \square , lt. F, Fl. 88f.	37° 12' 8"	15° 14'		
	Port Anzio, \square , lt. F, Fl. 92f.	41° 26' 9"	12° 37' 5"	C. Panagia, pt.	37° 6' 5"	15° 17' 0"		
	Monte Circello, lt. F 125f.	41° 13' 4"	13° 4' 5"	Syracuse, \square , w. r., lt. F 82f.	37° 3' 0"	15° 18' 5"		
	Terracina, lt. F 26f.	41° 17'	13° 15' 7"	C. Morro di Porco, lt. Fl. 108f.	37° 0' 0"	15° 21'		
	Gaeta, lt. F, Fl., St. Ca- }	41° 12' 4"	13° 34' 7"	Avola	36° 55' 2"	15° 8' 0"		
	therine tow., 237f.			Passaro I., NS 1m., lt. F, Fl. }	36° 41' 2"	15° 9' 7"		
Mola, watering pl.	41° 15' 0"	13° 36' 0"	137f.					
Castel Volturno	41° 2' 5"	13° 57' 0"	— S. extr., or Correnti I.	36° 38' 5"	15° 5' 2"			
Parmarola I., NS 1 $\frac{1}{2}$ m., N pt.	40° 56' 7"	12° 51' 5"	C. Scalambri, lt. F 121f.	36° 47'	14° 29' 7"			
Ponza I., $\frac{1}{2}$ 4m., (lt. F 200f.)	40° 54' 0"	12° 58' 2"	Terra Nuova, Col.	37° 2' 9"	14° 15' 0"			
Zannone I., EW 1m., lt. F, }	40° 58' 2"	13° 37'		Licata, Castle, lt. F 32f.	37° 6' 0"	13° 57' 0"		
Fl. 3-f.				Rossello, lt. F, Fl. 324f.	37° 17' 5"	13° 27' 7"		
Butte, rks.	40° 50' 4"	13° 6' 2"	Girgenti, \square , Mole lt., 3 lts. F	37° 17'	13° 32' 5"			
Vandotena I., $\frac{1}{2}$ 1 $\frac{1}{2}$ m., T, }	40° 47' 5"	13° 26' 0"		C. Bianco, 90f., (shl. $\frac{1}{2}$ m. S), }	37° 23' 2"	13° 17'		
Fort St. Nicola				tower				
Ischia I., $\frac{1}{2}$ 5 $\frac{1}{2}$ m., Castle, E pt.	40° 43' 9"	13° 57' 7"	C. St. Marco, fort, tow.	37° 29' 5"	13° 2'			
Procida I., NS 2m., N pt., }	40° 46' 2"	14° 1' 0"		C. Granitola, lt. F 123f.	37° 35' 7"	12° 40' 2"		
lt. F 76f.				Mazzara, Cathedral	37° 29' 2"	12° 35' 7"		
Baia, Castle	40° 48' 7"	14° 5' 0"	Marsala, lt. F, Fl. 65f.	37° 47' 4"	12° 27'			
C. Misano, pt., lt. F, Fl. 292f.	40° 46' 5"	14° 5' 2"	Trapani, \square , Columbara, lt. }	38° 0' 7"	12° 30' 2"			
Pozzuoli, Church	40° 49' 2"	14° 7' 2"	F, Fl. 134f.					
Naples, Obs. Capo di Monte...	40° 51' 8"	14° 14' 7"	St. Julian, Castle	38° 22' 7"	12° 36'			
—, mole lt. F, Fl. 161f.	40° 50' 3"	14° 15' 7"	Marittimo I., NS 3m., 237' 6f., }	37° 55' 7"	12° 37'			
Torre del Greco, W extr.	40° 47' 2"	14° 21' 7"	N pt., Castle					
Mt. Vesuvius, 3900f.	40° 49'	14° 26'	Levanzo I., $\frac{1}{2}$ 3m., N pt., T, tow.	38° 1' 6"	12° 21' 0"			
Castellum, lt. F, Fl. 105f.	40° 41' 5"	14° 28' 2"	Favignana I., EW 5m., St. }	37° 55' 7"	12° 19' 2"			
S. S. S. Fort St. Anton.	40° 37' 6"	14° 22' 5"	Cath. Castle, 1249f.					
Pt. Campanella, lt. Int. 85f.	40° 34' 0"	14° 19' 5"	Porcelli Is., $\frac{1}{2}$ 3m., T	38° 4' 5"	12° 27' 0"			
Capri I., EW 3m., S or }	40° 32' 0"	14° 11' 7"		Formiche, lt. F 85f.	37° 59'	12° 26'		
Carena Pt., lt. F, Fl. 238f. }				C. St. Vito, lt. F, Fl. 142f. ...	38° 11' 1"	12° 44' 2"		
Mt. St. Angelo, 4680f.	40° 39'	14° 31'	Castel a Mare, Petrol Pt.	38° 2' 5"	12° 54'			
Galli rks., tower	40° 34' 0"	14° 26' 5"	C. di Gallo (1692f.), lt. F 148f.	38° 13' 5"	13° 10' 2"			
Salerno, 2 lts. F 28f., 13f.	40° 39'	14° 45'	PALERMO, Observatory ...	38° 6' 7"	13° 21' 5"			
C. Licosa	40° 14'	14° 53'	C. Zaffarana, lt. F 111f.	38° 6' 5"	13° 32' 5"			
C. Palunro, lt. F 675f.	40° 0'	15° 18'	Termini, fort, lt. F 30f.	37° 59' 5"	13° 4' 2"			
Policastro	40° 1'	15° 33'	Cetali, Cathedral	38° 2' 2"	14° 1' 7"			
Dino I., EW 3c., tower	39° 48' 0"	15° 48' 7"	Car-nia, Castle	37° 59'	14° 27'			
Cirella I., tower	39° 37'	15° 50'	C. Orlando, 1, Castle	38° 9' 8"	14° 45' 0"			
Mt. Cocuzza	39° 16'	16° 16'	C. Calava	38° 12' 5"	14° 54'			
St. Eufemia	39° 3'	16° 15'	Milazzo, lt. F 288f.	38° 16' 1"	15° 14' 0"			
C. Vaticano, lt. F, Fl. 354f. ...	38° 37' 2"	15° 50'	Skerki Bank, 2	37° 45' 5"	10° 49' 7"			
Gioja	38° 24'	15° 56'	Keiths rf., T.	37° 48' 6"	10° 56' 6"			
Seylla	38° 14' 5"	15° 45' 0"	Pautellaria I., S. Leonardo, }	36° 50'	11° 57'			
Reggio Church, lt. F 72f.	38° 7'	15° 39'	windmill.					
Stromboli, 3030f.	38° 48' 2"	15° 13' 7"	— sum. 2730f.	36° 46' 8"	12° 0' 5"			
Panaria I., N pt.	38° 38' 7"	15° 4' 5"	Grahams sh., 13f.	37° 9'	12° 43'			
Secca di Capo	38° 37' 2"	14° 54' 5"	Linosa I., $\frac{1}{2}$ 1 $\frac{1}{2}$ m., landg. oove	35° 51' 8"	12° 52' 0"			
Sulina I., Salvatore M., 3125f.	38° 33' 2"	14° 50' 7"	Lampion I., $\frac{1}{2}$ 3m.	35° 32' 8"	12° 20' 0"			
Lipari I., summit, 1978f.	38° 29'	14° 56'	Lampedusa I., EW 6m., T, }	35° 29' 2"	12° 35' 2"			
			\square , Castle					

TABLE 10

557

MARITIME POSITIONS

(27) Places		Lat. N	Lon. E	(28) Places		Lat. N	Lon. E
Malta & Italy, South Coast	MALTA.			Pesaro, lt. F 30f.	43° 55' 3	12° 54' 7	
	Valetta, \square , Palace.....	35° 53' 8	14° 31' 2	Rimini, lt. F 67f.	44 4 3	12 35	
	SPENCER'S MONUMENT	35 53 0	14 30 7	Ravenna, tower.....	44 25	12 12 5	
	St. Elmo, lt. F 167f.	35 54 1	14 31 5	Goro, \square , W mo. of the Po ...	44 48	12 23	
	SE extr., Pt. Dellamara, } (rf. 1 $\frac{1}{2}$ m.), lt. R 151f. }	35 49 2	14 34	Chioggia, \square , Cathedral	45 12 9	12 17 0	
	Gozo I., $\frac{1}{2}$ 9m., NW pt., or C. Demitri, lt. Rev. 400f. }	36 4 2	14 13 2	Port Malamocco, \square , N mole .	45 20	12 20 7	
				S. Nicolo, Port Lido, \square , } fort, lt. 9f. }	45 26	12 23 5	
				Venice, St. Mark	45 26	12 20 5	
				Venice, Istituto di Mar. Mer	45 26 2	12 20 5	
				Piave Vecchia, lt. F 146f.	45 28 6	12 33 4	
Italy, South Coast	ITALY.			R. Tagliamento, fort mouth...	45 38 2	13 6 2	
	C. delle Armi, tow., lt. F 312f.	37 57 1	15 41 2	Port Buzio, lt. Rev. 11f.	45 43	13 15	
	C. S. artivento, F. Fl. 210f. ...	37 55 5	16 3	Grado, Ch. (lt. F)	45 40 6	13 23 2	
	Bruzano C.	38 2	16 8 2	Monfalcone, Church	45 48 3	13 32 2	
	Marina de Monasteraci	38 26	16 34 5	Trieste, \square , lt. Fl Sta Teresa } mole hd. 110f. }	45 38 8	13 46 2	
	C. Rizzuto, pt.	38 53 5	17 5 5	Capo d'Istria, Church.....	45 32 7	13 44 2	
	C. Colonne, lt. F 183f.	39 1 5	17 12 2	Pirano, St. G. Church	45 31 6	13 34 2	
	Cotrone, lt. F 30f.	39 5 6	17 8 5	Salvore Pt., Pt. Bassania, lt. } F 112f. }	45 29 5	13 29 5	
	Pt. Alice, tower	39 24	17 8	Citta nuova, \square , Church	45 18 8	13 33 7	
	Pt. del Trionto, tower	39 37	16 46	Parenzo, Church.....	45 13 6	13 35 7	
Adriatic, E. Coast &	Roseto.....	39 59	16 35 7	Rovigno, \square , Pelago I., lt. 42f.	45 2 2	13 36 7	
	Taranto, \square , Citadel	40 28 2	17 14	POLA, \square , OBSERVATORY	44 51 8	13 50 7	
	C. St. Vito, lt. F, Fl. 150f.	40 24 5	17 12 5	C. Promonore, Porer rk. (lt. } F 111f., (rk. SSE 1 $\frac{1}{2}$ m.) }	44 45 2	13 53 5	
	Port Cesareo, tower	40 15 6	17 53 7	Albana, Church	45 5 1	14 7 7	
	Gallipoli, St. Andrea I., $\frac{1}{2}$ } $\frac{1}{2}$ m., mid. (N pt., lt. F, Fl. } 149f.)	40 2 7	17 57 2	Fianona, Church	45 8 2	14 11 0	
				Fiume, clock tower.....	45 19 6	14 26 7	
				Porto Re, Di Oastro Pt., lt. F, } Fl. 54f. }	45 16 7	14 34 2	
	ADRIATIC.			Segna, mole, lt. F 27f.	44 59 6	14 54 0	
	C. St. Maria di Luca, lt. F, } Fl. 316f. }	39 47 7	18 22 5	Carlopaço, mole.....	44 31 7	15 4 7	
	Gauliano	39 51	18 20	Nona, Cathedral.....	41 14 6	15 11 2	
Adriatic, W. Coast &	C. O ranto, Telegr. (E pt. of } Italy)	40 8 6	18 29 7	Zara, lt. F 17	44 6 8	15 12 0	
	Port Otranto, \square , lt. F 197f.	40 6	18 31	Zara Vecchia	43 56 3	15 26 7	
	Brindisi, \square , Telegr., lt. F } 106f. }	40 39 3	17 5 2	Galiola rk.	44 43 5	14 11 0	
	Torre della Testa	40 41 4	17 52 5	Unie Bay, Islet, [2c.].....	44 38	14 14	
	Monopoli, Telegr., lt. F 50f.	40 57 1	17 18 2	Sansogo I., $\frac{1}{2}$ 2m., 350f. sum	44 30 9	14 18 2	
	Bari, St. Cataldo, lt. F, Fl. } 49f. }	41 8 3	16 51	Grivizza I., [$\frac{1}{2}$ m.]	44 24	14 33	
	Molfetta, tow., lt. F, Fl. 65f.	41 13	16 36 0	Sette Bocche Chan., N or } Bonastra Pt. }	44 12 3	14 49 0	
	Barletta, \square , (lt. F), 69f.	41 20	16 18 7	Mt. Vela Strazza, 1070f	43 59	15 2	
	Manfredonia, lt. F, Fl. 65f.	41 37 7	15 55 5	Zuri I., $\frac{1}{2}$ 7m., E pt., Mas- } sarina I. }	43 37 5	15 44	
	Mt. Nero, 3336f.	41 43	15 41	Sebenico, Castel Vecchia, lt. } F 18f. }	43 44 2	15 53 7	
	Vic'e, Sta Croce, lt. F	41 53 3	16 11 2	Zirona piccola, I. sum.....	43 27	16 4	
	Teomoli, tower	42 0 2	15 0	Trau, St. John's Church	43 30 9	16 15 2	
	Tremiti Is., $\frac{1}{2}$ 3m., Semaphore	42 7 3	15 30 5	Spalato, Boticeia pt., lt. F, } Fl. 35f. }	43 30 4	16 26 7	
	Pianosa I., I, EW 4c., E pt.	42 13 5	15 45 2	Makaraka, lt. F	43 17 5	17 10	
	Pelagosa Is., 2, $\frac{1}{2}$ 1m., lt. F, Fl.	42 24	16 16	Solta I., $\frac{1}{2}$ 10m., SE pt.	43 19	16 23	
	Pt. Penna, tower	42 10 4	14 43 0	Brazza I., EW 7 l. St. Vito, } sig. st. mid. }	43 16 7	16 37 5	
	Ortona, Ch., lt. F 39f.	42 19 7	14 24 5	Lessina I., EW 12 l., Pokon- } jido I., lt. F 76f. }	43 9	16 27	
	Mt. Brancastello, 7697f.	42 27	13 39	Lissa I., EW 9m., Port St. } Georgio, St. Francis Ch., } 2 lts. F 72f., 14f. }	43 3 4	16 10 2	
	Montepagano, 1046f.	42 40 5	13 59 5	Busi I., $\frac{1}{2}$ 2 $\frac{1}{2}$ m., sig. st.	42 58	16 2	
	Guilianova	42 45	13 59	St. Andrea in Pelago, $\frac{1}{2}$ 1 $\frac{1}{2}$ m., } 1000f., $\frac{1}{2}$ }	43 1 7	15 45 7	
	Colonella, sum. 1096f.	42 52	13 54	Pomo rk., [2c.], 1	43 5 5	15 27 7	
	Grottamare, Church	42 59 8	13 52 2	Proisdo I., EW 1m., (off W } pt. of do.)	42 59	16 37	
	Pedaso, Church	43 6 4	13 53 0				
	Fermo, Cath., 1197f.	43 9 5	13 43 5				
	Loretto, Ch., 565f.	43 26 3	13 37				
	Mount Conero, Telegr.	43 33 3	13 36 5				
	Ancona, lt. N mole, 34f.	43 37 7	13 30 5				
	Sinigaglia, lt. F 45f.	43 43 7	13 13 5				
	Fano, lt. F 58f.	43 51 3	13 0 7				

MARITIME POSITIONS

(29)	Places	Lat. N	Lon. E	(30)	Places	Lat. N	Lon. E
Adriatic, E. Coast @	Curzola I., EW 8 l., Fort St. } Biaggio	42° 57' 4	17° 8' 0	Ionian Is.	Cephalonia, St. George, Cas- tle, 1030f.	38° 8' 5	20° 34' 0
	Glavat I., lt. F, Fl. 121f.	42 46	17 9		— Sum., or Mt. Elato, 5218f.	38 8' 5	20 41 0
	Cazza I., $\frac{3}{4}$ 2m., sig. st.	42 46 0	16 31 0		— S pt., or C. Monda	38 3' 6	20 48
	Curzola I., $\frac{3}{4}$ 1m.	42 45	16 43		Zante, N pt., or C. Skinari ...	37 56' 2	20 42' 2
	Lagosta I., EW 7m., St. } George Chap., lt. F 342f. }	42 43 0	16 53 0		— Mt. Vachronis, 2724f.	37 48' 8	20 42' 7
	Lagostinarks, EW 3 $\frac{1}{2}$ m., Esum.	42 45' 8	17 9' 0		— S pt., C. Marathia	37 39	20 50
	Meleda I., $\frac{4}{5}$ 7 l., W pt.	42 47	17 18		— Ieraki Pt.	37 42' 5	20 59' 2
	— Port Palazzo, ruin.	42 46' 8	17 21' 7		— Mt. Scopo, 1621f.	37 45	20 56' 2
	Ragusa, ruin, fort, W bast.	42 38' 9	18 7' 0		Krio Nero, lt. F 93f.	37 48' 2	20 54' 5
	Markana Is., grp., $\frac{4}{5}$ 2m., sum.	42 34' 3	18 12' 0	GREECE.			
	Molonta I., sum.	42 29' 9	18 23' 5	Dragomesti Bay, Astoko	38 32	21 5	
	Pt Ostro, lt. F, Fl. 263f.	42 23' 4	18 31' 7	Oxia I., pk., 1411f.	38 18' 7	21 7	
	Kattaro, Sanità	42 25' 4	18 46' 5	Messalonghi	38 21' 9	21 25' 7	
	Veternach, 3960f.	42 19	18 52	Pt. Bakari	38 17	21 31	
	Budua, Greek Church	42 16' 5	18 50' 5	Roumelia, Castle	38 19' 5	21 46' 2	
	Antivari, Volovica Pt., lt. F ...	42 5' 3	19 4' 5	Lepanto, Castle	38 23' 8	21 49' 0	
	Meuders Pt., lt. F 33f.	41 57	19 9' 5	Corinth, Acropolis	37 53' 5	22 52	
	Dulcigno, la Cala beach ...	41 55	19 12' 5	Morea Castle, centre	38 18' 5	21 47' 0	
	C. Rodoni, 400f., lt. Fl.	41 35	19 27' 2	Patras, w', lt. F, Fl. 65f.	38 15' 1	21 43' 5	
	C. Pali, sum.	41 24' 7	19 24' 2	C. Papas, ruined fort	38 12' 7	21 23' 5	
	Durazzo, mole, lt. F 52f.	41 18' 2	19 27' 2	Montague rks., 2, $\frac{3}{4}$ 1m., wf.	37 55	21 0	
	C. Laghi, tower	41 10' 2	19 25' 5	Konoupoli Pt.	38 6	21 23	
Albania	Avlona, or Valona, ruin, w. } Custom house.	40 27' 2	19 26' 7	C. Giavanza, ruin	37 56' 8	21 8' 5	
	Saseno I., $\frac{4}{5}$ 2m., sum. 1000f.	40 29' 2	19 14' 2	Kastro Tornese, 795f.	37 53' 7	21 8' 7	
	C. Linguetta, 1, 2290f.	40 26' 7	19 17' 7	C. Katakelo, Is.	37 38	21 19' 0	
	Mt. Cica, 6300f.	40 15	19 35	Stamphaus Is., $\frac{4}{5}$ 2 $\frac{1}{2}$ m., T. } I, lt. F 127f.	37 15' 3	21 0' 2	
	Port Palermo, ruin, fort	40 2' 9	19 48' 2	C. Kunello	37 10	21 34	
	C. Kiephali	39 54' 3	19 55' 5	Proti I., NS 2m., sum. 605f.	37 3' 4	21 33' 5	
	Tignoso, lt. F 100f.	39 47' 2	19 58' 5	Sphaghia I., $\frac{4}{5}$ 2 $\frac{1}{2}$ m., S pt. ...	36 54' 5	21 40' 5	
	Port Gomenitza, ruin, Dogana..	39 29' 7	20 17' 1	Navarino, Pylos I., lt. F 116f.	36 54	21 41	
	Parga, w. Madonna I.	39 16' 4	20 25	Mt. St. Nicolo, 1542f.	36 53' 0	21 42' 0	
	Mt. Zarothema, 3000f.	39 11' 2	20 38	Modon	36 48' 4	21 42' 5	
Ionian Is. @	Preveza, Fort Giorgio	38 56' 7	20 46' 2	Sajienza I., NS 5m., sum. 740f.	36 46' 6	21 42' 2	
	Vonizza	38 55	20 53' 7	Cabrera I., $\frac{4}{5}$ 5m., S extr. ...	36 41' 7	21 47	
	IONIAN ISLES.				C. Gaillo	36 42' 9	21 52' 7
	Fano I., $\frac{3}{4}$ 3 $\frac{1}{2}$ m., 1339f., lt. F. } Fl. 340f.	39 51	19 27	Venetico I., NS 1 $\frac{1}{2}$ m. (Ants.) SSE 2m. sum 570f.	36 41' 7	21 53' 7	
	Merlera, NS 2m., sum.	39 53' 2	19 36	Koron, w' N 2m., f. Livi- dia Pt.	36 47' 5	21 58' 5	
	Samothraki I., $\frac{4}{5}$ 2 $\frac{1}{2}$ m., N pt.	39 46' 7	19 31' 5	Kalamata, highest ruin	37 2' 6	22 7' 2	
	Corfu, Citadel, lt. F 240f. ... @	39 37' 0	19 56' 7	C. Kitries	36 54' 7	22 8' 0	
	— C. Drasti	39 47' 6	19 41' 5	Mt. Makrino, 7900f.	36 56' 5	22 22' 2	
	— Mt. St. Giorgio, 1288f.	39 36	19 48' 0	Linjeni, ruin	36 40' 6	22 13	
	— C. Bianco, pt.	39 21' 2	20 7' 7	C. Grosso, 1, h, sum.	36 28' 6	22 22' 2	
Cephalonia I.	— Vido I., Fort Alexander ...	39 38' 2	19 56' 5	C. Matapan, 1, h, lt. F, Fl. } 133f.	36 22' 5	22 29' 2	
	Paxo I., $\frac{4}{5}$ 4 $\frac{1}{2}$ m., NW pt. } Laka, lt. F 416f.	39 14' 4	20 8' 5	C. Stavri	36 36' 2	22 32' 5	
	— Port Gajo, ruin.	39 12	20 13	Marathonisi	36 44' 6	22 35' 0	
	Aniupaxo I., $\frac{4}{5}$ 2m., E pt.	39 8' 7	20 14' 0	Eurotas R., mouth	36 48' 2	22 41	
	Sta. Maura, lt. F mole, 54f. ...	38 50' 5	20 43	C. Xyli, (pk. 1040f. N 1' 5), pt	36 39' 0	22 49' 5	
	— Se-ola rk., 114f.	38 41' 5	20 33' 5	Servi I., NS 3 $\frac{1}{2}$ m., S and E pt.	36 27' 0	22 59' 5	
	— Mt. Stavrota, 3700f.	38 41' 6	20 38' 5	C. St. Angelo, h, 1, pt.	36 26' 0	23 12' 0	
	— S extr., C. Ducato, 1, 200f.	38 33' 5	20 33' 7	Cerigo I., N. pt., C. Spathi, } lt. F, Fl. 362f.	36 23' 0	22 57' 2	
	Ithaca, N pt.	38 30' 0	20 40' 0	— Fort St. Nikolo	36 13' 1	23 5' 0	
	— Vathy, Port, ruin, Lazaretto	38 22' 1	20 43' 5	— S extr.	36 7' 7	22 59' 7	
	— SE pt., or Iganni Pt.	38 19	20 46' 7	Ovo I., NS 8c., 550f., T	36 5' 5	23 0' 0	
Cephalonia, N extr.	38 28' 5	20 34' 0	Nautilus rk., [3m.]	35 56	23 13		
	— C. Aterra, pt.	38 21' 5	20 25	Por I., $\frac{4}{5}$ $\frac{3}{4}$ m., 410f.	35 58' 5	23 15	
	— Guarosiana I., lt. F 112f. ...	38 8' 4	20 26' 5	Cerigotto I., $\frac{4}{5}$ 6m., sum. 1230f.	35 50' 1	23 18' 0	
	— Port Argostoli, C.S.Theo- doras	38 11' 6	20 29				

TABLE 10

MARITIME POSITIONS

(31) Places		Lat. N	Lon. E	(32) Places		Lat. N	Lon. E
Crete, East Coast	Mt. Krithina, 2600f.	36°28'2	23° 8'2	Naxos I., 18m., Mt. Zia, } SE-d of mid., 3290f. }	37° 1'8	25°31'2	
	Karavi I., rk., T	36 46 1	23 36 5	— N pt., or C. Stauro	37 12 5	25 33 0	
	Falconera I., 1/2 1/2m., h, sum.	36 50 9	23 53 7	Paros I., 12m., 2530f., } C. Koraka, lt. F. Fl. 193f. }	37 9	25 14	
	Belo Poulo I., 1/2 1/2m., T, sum.	36 54 9	23 27 7	Boidi, or Buey rk., T	37 14 5	25 56 7	
	Spezia I., 1/2 4 1/2m., sum. 812f.	37 15 3	23 8 7	Antiparos, NS 7m. S pt.	36 56 0	25 5 0	
	Trikeri I., NS 1m., N sum.	37 16 2	23 17 0	Strongylo I., 1/2 1 1/2m., S pt.	36 56 2	24 57 5	
	Napoli di Romania	37 33 6	22 48 0	Stapodia, 1/2 1 1/2m.	37 25	25 35	
	Hydra, 1/2 11m., sum. 1939f.	37 19 5	23 28 0	Myconi I., 1/2 8m., E sum. } 1150f. }	37 27 5	25 27 2	
	Stavronisi I., EW 1/2m.	37 15	23 27	Rhenca, NS 4 1/2m., S pt.	37 22 0	25 14 0	
	St. George d' Arbora I., 1/2 1/2 } 3m., sum. SE part, 1085f. }	37 28 0	23 56 0	La Nata, rk., (rk. W 1/2m.)	37 21 7	25 4 0	
	Poros I., EW 5m., 1/2 1/2, W } pt., lt. F 96f. }	37 32	23 26	Syra I., NS 9m., 1415f.	37 28 9	24 55 7	
	Methana, Mt. Khelona, 9429f.	37 36	23 22	— Gaidaro, lt. R 224f.	37 25 5	24 59 0	
	Epina I., 1/2 8m., Mt. St. } E ias, on S part, 1752f. }	37 41 9	23 30 0	Jura I., 1/2 5m., W pt.	37 36 2	24 39 5	
	Kalamaki, E. ent. canal	37 55	23 0	Tinos I., 1/2 15m., 2340f.	37 35 0	25 14 5	
	Ledsina I., or Eleusis, tow.	38 2 4	23 32 2	Andros I., 1/2 22m., Mt. Ku- } vari, W side, mid., 3200f. }	37 50 1	24 50 5	
	C. Themistocles, lt. F. 51f.	37 5	23 28	— C. Fassa, lt. F. Fl. 708f.	37 57 6	24 41 7	
	Piræus, 2 lta. F	37 56 2	23 38 0	Kuloyeri rks., NS 2m.	38 10	25 17	
	Athens, Parthenon	37 58 1	23 43 7	Negropont, Euripo, lt. F 39f.	38 9 7	23 36 5	
	— OBSERVATORY	37 58 3	23 44	— C. Doro, islet off, 93f.	38 28 4	24 36 5	
	C. Colonna, temple, 269f.	37 38 8	24 1 7	— C. Kumi	38 39	24 9 7	
	Port Mandri, 1/2 1/2, pk.	37 44 3	24 3 7	— Mt. Delphi, 5730f.	38 37 4	23 50 7	
	Macroni I., 1/2 7m., S pt.	37 38 5	24 6 7	G. of Volo, C. Kavoulia, lt. F 85f.	39 6	23 4	
	Port Raphti, 1/2 1/2, St. Nicolao ...	37 53 0	24 1 0	Volo, fort	39 24 0	22 56 5	
	C. Marathon	38 7 1	24 3 7				
	Petalies, or Split Is., sum.	37 59 5	24 16 2				
ARCHIPELAGO.							
Archipelago @	Zea I., 1/2 10m., Mt. St. Elias ...	37 37 3	24 21 7	Skyro I., 1/2 6 1/2, rf. N end, } Mt. Kokhilas, 2665f. }	38 49 7	24 36 5	
	— Port St. Nicolao, 1/2 1/2, lt. } F Fl. 108f. }	37 40	24 19	Skyro Poulo, [1m.], 617f.	38 50	24 22	
	Theronia I., 1/2 10m., sum. 966f.	37 22 5	24 26 2	Skantzura I., NS 1 l., mont.	39 5	24 6	
	Piperi I., EW 1/2m., sum.	37 18 2	24 32 0	Adelphi Is., 1/2 1 1/2m., 521f.	39 5 8	23 59	
	Serpho Poulo Is., EW 1 1/2m., } mid. }	37 15	24 36	Khelidromi, 1/2 4 l., N sum. } 1590f. }	39 10	23 53	
	Serpho I., 1/2 7 1/2m., sum. 1585f.	37 10	24 30	Skopelos I., 1/2 11m., sum. 2148f.	39 8 8	23 40 2	
	S. phanto I., 1/2 9m., N pt.	37 2 7	24 38 5	Skinthos I., 1/2 6m., 1/2, Mt. } Stavros, 1448f. }	39 11 4	23 28 2	
	Anti Milo, NS 2m. sum.	36 48	24 15	Pelago, NS 2 l., sum. 1050f.	39 20 4	24 3	
	Ananes rks., 1/2 1/2m.	36 33	24 9	Peathoura I., lt. Fl. 129f.	39 30	24 10 7	
	Milo, EW 11m., Mt. St. } Elias, on SW part, 2480f. }	36 40 5	24 23 2	Mt. Pelion, 5310f.	39 26 5	23 3	
	— Port, 1/2 W pt., Pt. Vani ...	36 45 3	24 22 7	Ossa, Mt., 6407f.	39 48 0	22 42 0	
	Argentiera I., NS 5m.	36 49 3	24 33 5				
	Polino I., 1/2 3 1/2m., sum.	36 46	24 39	TURKEY.			
	Peignes rks.	36 38	24 35	Mt. Olympus, 9764f.	40 4 7	22 22 0	
	Policandro I., 1/2 2 l. sum.	36 37 1	24 55 2	Salonika, 1/2	40 37 8	22 57 2	
	Sikyno I., 1/2 7m., sum.	36 40	25 6	C. Kassandra, lt. Fl. 72f.	39 57 2	23 22 0	
	Nio I., 1/2 8m., sum.	36 42 7	25 21 0	C. Pailluri, 1/2	39 55	23 44 7	
	Amorgo Poulo I., NS 2m.	36 36 9	25 42 7	C. Drapano, 880f.	39 56 5	23 56 2	
	Santorin I., NS 8m., Mt. St. } Elias, on SE part	36 22 0	25 28 7	Mt. Athos, sum. 6349f.	40 9 5	24 20 0	
	Christiana I., (Askunias), 1/2 } 1m. }	36 15	25 13	Pilaf Tepe, 6143f.	40 53 5	24 5 2	
	Anapli I., 1/2 7m., sum.	36 23	25 47	Kavala B., lt. F 148f.	40 55	24 25	
	Hermionisi I.	36 32	26 10	Thaso I., NS 14m., sum. 3428f.	40 41 7	24 42 7	
	Stampalia I., or Astrop. ilaia, } 1/2 4 l., SW sum. }	36 32 2	26 19 7	C. Fenar, lt. F 72f.	40 56 7	25 8 5	
	Levita I., EW 4m., E pt.	37 0 0	26 32 0	Marona, hill, 2174f.	40 52 7	25 32 5	
	Zinari I., 1/2 2m., W pt.	36 58 7	26 17 7	C. Makri, w', 1/2 1m.	40 49 5	25 45 0	
	Amorgo I., 1/2 18m., sum. } near mid., 2175f. }	36 50 7	25 55 7	Dédéagatch, lt. Rev. 115f.	40 50	25 55	
	Karo I., EW 4m., mid.	36 53	25 40	Enos	40 42 0	26 5 0	
	Skipos I., 1/2 2 1/2m., SE pt.	36 51 0	25 33 0	Xeros I., NS 1/2m.	40 36 5	26 44 0	
	Iletraia I., 1/2 4m., sum.	36 49 7	25 27 5				
Lemnos Is.				Samothraki, 1/2 12m., 5248f.	40 27 0	25 35 5	
				— W pt., C. Akrotiri, 1/2	40 28 2	25 27 0	
				Zurafa rk.	40 27 5	25 50 5	
				Strati I., 1/2 5 1/2m., 973f.	39 31 0	25 1 7	
				Lemnos, 1/2 7 l., W pt., or C. } Mountzeplios, 1410f. }	39 58 7	25 2 0	
				— Moudros, 1/2	39 52 0	25 16 2	

MARITIME POSITIONS

(25)	Places	Lat. N	Lon. E	(34)	Places	Lat. N	Lon. E	
Sea of Marmara	Lemnos, S pt., or C. Irene ...	39° 46' 6"	25° 21' 5"	Sea of Azov	Mt. Tchataridag, SW sum.....	44° 44' 0"	34° 17' 2"	
	— N and E pt., C. Plaka ...	40 1 7	25 27 0		C. Megaron	44 46 7	35 7	
	Imbros, $\frac{1}{2}$ 51. sum. 1959f.	40 10 6	25 49 0		O. K-atlamà, sum.....	44 57 0	35 22	
	— W pt., or Pt. Anfiaka ...	40 7 2	25 40 0		C. Theodosia	45 0	35 26	
	Dardanelles, Asia Castle, lt. F 50f.	40 9 0	26 24 5		C. Chaouda, S pt., lt. F Fl. 120f.	44 59 5	35 50	
	Gallipoli, lt. Rev. 120f.	40 24 0	26 41		C. Takli, lt.	45 5 9	36 27	
	Koutalai L., Roun rk., lt. F 49f.	40 31 0	27 28 5		Kertch, \square , Church.....	45 21 2	36 29 5	
	Marmara I., Fanar Adasi, lt. F. Fl. 134f.	40 38	27 45		Yenikaleh, lt. Fl. 409f.	45 23 1	36 39 2	
	Pasha harb., \square , Liman	40 29 5	27 36 2		C. Kazantip, sum.	45 28 0	35 54 0	
	Rodosto	40 59 7	27 31 0		Arabat, E bast.	45 17 9	35 29 5	
	Erekli, lt. F 184f.	40 58 5	27 58 0		Ghenitcheb, lt. F 81f.	46 11 0	34 52	
	CONSTANTINOPLE, St. SOPHIA	41 0 3	28 59 0		Berdiansk, lt. F 165f.	46 46	36 48 2	
	Bosporus Seraglio pt., lt. F, Fl. 117f.	41 0	29 1		C. Biel-sarai, lt. F 73f.	46 52 5	37 20 7	
	Roumili, lt. F 190f.	41 14	29 7 2		Mariupol, Church	47 5 3	37 35 5	
	Fanar Bournou, lt. F 83f.	40 57 7	29 2 2		Taganrog, lt. F 161f.	47 12 2	38 57	
	Proti I., [1m.] Vill. E side ..	40 54 0	29 3 5		Azov, Cathedral	47 7 0	39 26 5	
	Dil Burnu, lt. F 40f.	40 44 5	29 30 7		Long nos., s.	46 48	38 35	
	Lmid	40 45 7	29 55		Gheisk, lt. F 34f.	46 43	38 17	
	C. Boe Burnu, 1050f.	40 32	28 47		Black Sea	Taman	45 13 0	36 44
	Gemlik or Kios	40 26	29 9 5			Anapa, lt. F 98f.	44 54 1	37 18 5
	Kalolimno I., NS 4m. N sum.	40 34	28 32			Ghelenjik, \square , fort	44 33 4	38 3 2
BLACK SEA.				High Summit, 4m. inland		43 17	40 16	
Black Sea	Kilios, tow.....	41 10 8	29 37	Soukoum, fort, lt. Rev. 121f.		42 59 3	40 59 7	
	C. Karabournu, N pt. lt. Fl. 302f.	41 21 7	28 41 2	C. Batoum, Mosque, lt. F 65f.		41 39 4	41 37 0	
	C. Kouri	41 52 7	28 3 0	Rezo		41 3 0	40 31 5	
	Cizopol	42 26 3	27 43 7	Tr. Lizonde, \square , lt. Fl. 105f.		41 1 0	39 46 0	
	Bourgas, Minaret	42 30 3	27 30 7	C. Ieros, T, N pt., lt. Fl. 98f.		41 7 7	39 26 0	
	Akhiole, Mosque	42 34 0	27 40 5	Triboli		41 1 0	38 49	
	C. Emeneh, E pt., lt. Fl. 207f.	42 42	27 55 7	Keresoun		40 57 2	38 24	
	Varna, Mosque, mid.....	43 12 0	27 56 5	C. Yazon, l, rks		41 8 5	37 41 5	
	C. Kaliagri, ruin	43 22 1	28 29 7	Eunich, S. Mosque.....		41 7 7	37 17 7	
	C. Shabler lt. F 120f.	43 32 7	28 37 7	Samsoun, N lt. F 56f.		41 19	36 21 2	
	Kustenjah, C., lt. F 68f.	44 10 5	28 41 0	C. Kizil Kirmak, W. mo. riv.		41 44	35 58	
	Portitski Mouth	44 40 5	29 1 7	Sinope, Castle, lt. F 544f.		42 1 2	35 12 5	
	Danube R., Sulina mo. lt. F 70f.	45 9 3	29 40 5	C. Intjeh, lt. F, Fl. 92f.		42 6	34 58	
	Serpent's I., w, lt. R 194f.	45 15 5	30 14 2	C. Kerempch, lt. Fl. 262f.		42 1	33 17 2	
	Tsaregradskoe mo. 2 lts. F 52f.	46 4 8	30 29 7	Amastir, E extr, lt. Fl. 312f.		41 45 3	32 24 5	
	Akerman, Church	46 11 9	30 20 2	C. Baba, lt. F 657f.		41 18	31 26	
	C. Fontane, lt. F 200f.	46 22 8	30 45 5	Kephken Ada-si I., lt. F 98f.		41 14	30 17 5	
	Odessa, \square , Reidovi mole, lt. F, Fl. 63f.	46 30	30 46	ASIA MINOR.				
	— OBSERVATORY	46 28 5	30 45 5	Rabbit Is., l, $\frac{1}{4}$ 2m. W extr.	39 55 5	26 37		
	Berezan I., $\frac{1}{4}$ 1m., fort	46 35 6	31 23	Tenedos I., $\frac{1}{4}$ 6m., rf. NW-d., sum.	39 50 2	26 5		
	Kinbourn lt. v. 2 vert.	46 35 4	31 29 2	C. Baba, fort	39 28 2	26 4 5		
	Otechukov, Church	46 36 4	31 32 2	Mt. Ida, 5750f.	39 42 0	26 50 5		
	Nicolayev, \square , Observatory ..	46 58 2	31 58 0	Airanyti	39 35 5	27 2 5		
	Kherson, Cathedral	46 37 7	32 38 0	Mityleni, $\frac{1}{4}$ 13 l., E pt., C. Agia Maria	39 0 7	26 37 7		
	Tendra I., l, $\frac{1}{4}$ 8m. N end, beac.	46 21 7	31 32 0	— Mt. Olympus, 3079f.	39 4 2	26 22 0		
	— lt. Rev. 96f. bell	46 18 9	31 30 2	— Caloni, \square , Isl.	39 4 7	26 5 5		
	Armiansk, Church	46 7	33 43	— W. pt. C. Sigri, lt. Rev. 180f	39 13	25 51		
	C. Jarkan, lt. F 117f.	45 20 7	32 29 7	SMYRNA, MILL ON DARAGAZ } Pt.	38 26 5	27 9 7		
	Eupatoria pt. lt. F, Fl. 52f.	45 9 7	33 15	Vourla Scala, fountain	38 21 7	26 47 5		
	C. Khersonese, l, lt. Rev. 116f.	44 35	33 22 2	C. Karabournou, pt.	38 39 9	26 22 7		
	Sevastopol, \square , Church	44 37 9	33 29 5	Scio, NS 27m., N sum. 4157f.	38 33 7	26 1 2		
	C. Saritch, pt.	44 23	33 44	Veneticio I., off S pt. of Scio, T	38 8 0	26 2 0		
	C. A-todor, lt. F 315f.	42 25 3	34 7 7	Psara I., $\frac{1}{4}$ 5m., S pt.	38 32	25 35		
				Antipsara, W pt.	38 32	25 31		
				C. Blanco	38 16 6	26 14 7		
				C. Koraka, T	38 6 5	26 36 7		
				Sighajik, \square	38 12 0	26 48 2		

TABLE 10

MARITIME POSITIONS

(35) Places		Lat. N	Lon. E	(36) Places		Lat. N	Lon. E
Aegean M ^{or}	Scala Nuova, lt. F 98f.	37° 51' 5	27° 16' 5	C. Stavros	35° 25' 6	24° 59'	
	Samsun Dag, 4130f.	37 39 8	27 9 0	Megalo Kastron, □, (lt. F 53f.)	35 20 6	25 9	
	C. Monodendri, ruin	37 21 3	27 13 0	Standia I., summit, 870f.	35 27	25 14 2	
	Wreck rk. 21f.	37 9 0	27 17 7	C. St. John, □, SW 2½m.	35 20 5	25 47	
	Budroom, □, Castle	37 2 0	27 27 5	Yanisades Is., N pt., Paxi- mada	35 23	26 11 5	
	Port Giova	37 3 5	28 22	C. Sidero, lt. Rev. 138f.	35 19	26 19 7	
	C. Krio, W pt.	36 41 0	27 23 5	C. Salomon, or Plaka	35 9 2	26 19 5	
	Iujah Pt.	36 39 4	27 42 7	C. Zakro	35 5 2	26 17 2	
	Symi I., grp. NS 9m. S islet, Trompetto	36 30 7	27 54 2	Kupho Nisi, S pt.	34 54 7	26 8 7	
	C. Aloupo	36 33 0	28 1 0	Gaidaro Nisi, W pt.	34 52 3	25 41 3	
Candia	ARCHIPELAGO.			C. Littinos	34 54 7	24 45	
	Samos, Mt. Kerki, 4725f.	37 43 8	26 38 5	Mt. Ida, 8060f.	35 13 3	24 47 0	
	— Vathi □, port. lt. F 260f.	37 47	26 58	Paxinadia Is., W end, 1160f.	35 0	24 35	
	— S pt., or C. Colonna	37 38 3	26 52 7	Sphakia	35 12	24 8 7	
	Furni Is., NS 11m., S extr. rk. 1	37 28 4	26 31 2	Gavdo I., ½ 5m., lt. Rev. } 1181f.	34 50	24 4	
	Nikaria, ½ 22m. W pt., or C. Papan, lt. F, Fl.	37 31 2	25 59 5	Gavdo Pulo, ½ 1½m., 440f. ...	34 55 2	24 0 5	
	Mt. Melissa, 3390f.	37 32 2	26 4 7	KARAMANIA.			
	Gaidaro, EW 4m. sum. 720f.	37 28 1	26 58 7	Marmorice, □, Castle	36 51 1	28 19 0	
	Arki, ½ 4m. N pt.	37 24 9	26 44 5	— Cape, lt. F 131f.	36 43 9	28 20 7	
	Patmos, NS 7m. Prasso Islet... — Scala, □, pier	37 16 0	26 34 7	Karghatch, □, watering place	36 51 5	28 30 7	
Archipelago @	Lipso, ½ 4½m. SW pt.	37 18 2	26 44 2	Linosa I., 327f., sum	36 46 5	28 29 0	
	Lero, ½ 8m., Mt. Klidi, 1060f.	37 10 7	26 51 5	C. Suvelah	36 35 2	28 54 0	
	Kalimno, ½ 10m. Mt. Para- siva, 2250f.	36 58 8	27 0 0	Makry, □, theatre	36 38 1	29 9 7	
	Saphonidi, ½ ½m. sum.	36 53 0	26 56 7	Highest sum., 5930f.	36 31 8	29 14 2	
	Kos, ½ 24m. W pt.	36 43 1	26 56 5	C. Seven Capes, W pt. T	36 21	29 12	
	Madona I. sum., lt. F, Fl.	36 30 5	26 57 5	Volos I., T	36 13	29 25	
	Nisero, EW 4½m. sum. 2270f.	36 35 5	27 11 0	Port Vathy, □, sarcophagus... Port Sevedo, □, tank	36 11 5	29 39	
	— W islet off, ½ 1m., N pt.	36 35 6	27 3 5	C. Roxo, Hipsili I., T	36 6	29 40	
	Piskopi, ½ 8½m., sum. 2097f.	36 26 1	27 21 0	Kakava I., ½ 4m. □, W pt.	36 9 6	29 52	
	Karki, EW 5m., SW pt.	36 12 2	27 33 2	Phineka Prom. A, T, S pt. ...	36 14 5	30 9	
Koromania	Rhodes, □, □, lt. Rev. 82f.	36 26 9	28 16 2	Khelidonia Is. NS 2m., S islet	36 9 5	30 26 2	
	— W pt., C. Mon litho	36 8 7	27 43 2	Grambousa I., ½ 1m., w } NE part	36 13 5	30 30	
	— S pt. C. Prasso Nisi	35 52 4	27 47 0	Yanar. volc.	36 24	30 30	
	Khina Id., rk.	35 51 2	27 56 0	Mt. Takhtalu, 7800f.	36 31 7	30 28	
	Scarpanto I., NS 27m. S pt. ...	35 23 5	27 10	C. A ova, 1, w W-d.	36 35 4	30 38	
	Saria [2m.] mid., 1853f.	35 51	27 14	Adalia, □, lt. F 131f.	36 52 2	30 47	
	Caxo I., EW 12m. SW pt.	35 19	26 50	Esly Adalia, theatre, w, b, ...	36 45 6	31 26	
	Stakida, 2 Is., [2m.] N one ...	35 53	26 51	C. Karabournu	36 38 0	31 43	
	Unia Nisia	35 50	26 29	Aluya, □, SE pt.	36 31 5	32 1	
	Kamila Nisi	35 51	26 14	C. Anamour, 1	36 0 8	32 49	
Candia @	Sofrana Is.	36 4 5	26 25	Chelindreh, □, w	36 9	33 22	
	Tria Nisia, Is.	36 18	26 45	C. Cavaliere, 1, S pt. (w N-d.)	36 7 5	33 43 7	
	Sirina I., 1087f.	36 20 8	26 41 2	Provençal I., ½ 2m., w } Castle, sum.	36 11 1	33 48	
	Adelphi Is., N one	36 25	26 38 5	Pt. Lissan al Kabbeh, 1, shl. 1 off, lt. F 49f.	36 14 3	33 59	
	Ovo I., 170f.	35 36	25 35 5	Lamas Riv., T, w'	36 33 8	34 17 7	
	Candia.			C. Karadash, lt. F 131f.	36 32 4	35 21	
	C. Krio	35 13 4	25 34 7	Ayas, tower on I.	36 46 1	35 48	
	Pondikonisi, 730f.	35 34 7	23 28	SYRIA.			
	Agr'a Grabusa, N point	35 38 6	23 34	Alexandretta, 2 Is. F 49f.	36 35 5	36 9 7	
	N extr., C. Spada, A, 1, sum.	35 41	23 43 7	Ras el Khanzir	36 19 2	33 46	
	Khania, □, lt. F 85f.	35 30 8	24 1	Antioch	36 12	36 8	
Candia @	C. Tripiti	35 36 1	24 7 7	Ras el Bazit	35 52	35 47 5	
	Sada, □, lt. F 82f.	35 28	24 9 3	Ras Ibn Hani, lt. Fl. 45f.	35 35 4	35 42 5	
	Rhitymno, lt. F 49f.	35 22	24 29 2	Latakiyah, □, w, lt. F 49f. ...	35 30 7	35 45 5	
				Ruad I., lt. Fl. 92f.	34 51 7	35 51	
Candia @				Tripoli, Ramkine I., lt. F 67f.	34 30	35 45	
				Ras Beirut, lt. Fl. 125f.	33 54 2	35 28	

MARITIME POSITIONS

(37) Places		Lat. N	Lon. E	(38) Places		Lat. N	Lon. E
Syria	Damascus, Madinet-el-Arsh...	33°30'6"	36°18'5"	Lebida, Citadel	32°38'7"	14°16'5"	
	Mt. Hormon, sum. 9053f.	33 25 5	35 51	Ras al Tajourah, E pt.	32 53 5	13 23 7	
	Saida, Jemireh, 2 lts. F 62f.	33 34 5	35 21 5	Tripoli, \square , lt. R 115f.	32 54 4	13 11 2	
	Sur, 2 lts. F 68f.	33 16 7	35 11 2	Port Zouaga	32 48 5	12 27 7	
	Acra, lt. F 46f.	32 55 5	35 4	Zorah	32 55	12 4	
	C. Carmel Cont. lt. F, Fl. 490f.	32 49 8	34 58	TUNIS.			
	Jaffa, lt. Rev 69f.	32 27	34 44	Al Biban bank, Zera spit	33 26 5	11 20	
	JERUSALEM, Kubbet es Sak- rah, or Dome of the rock }	31 46 5	35 14 7	Jerba I., Houmt-souk, lt. F ...	33 53 5	10 51	
	Ascalon, ruins	31 39 0	34 32 7	Rabes Dzara pier	33 54	10 7	
	El Ariah, fort.	31 6 5	33 48 0	Surkenis B. Nather Tr.	34 12	10 3 5	
CYPRUS.				Jebel Thelj, NE sum	34 25	9 52	
Cyprus	C. Arnant	35 6 8	32 16 2	Sphax, lt. F 38f.	34 44	10 46 2	
	C. Cormachiti	35 24 7	32 55 7	Kerkenah Is., $\frac{1}{2}$ 9l., 4 Ras }	34 36 7	11 3 2	
	Kyrenia, lt. F 68f.	35 20	33 18 7	Sinub	34 49	11 18 5	
	N and E extr., C. St. Andrea	35 42 2	34 36 5	— NE extr., Gzira Kebir	34 51 5	11 45	
	Famagousta, lt. F 49f.	35 7 7	33 57 2	— Banks Eastern buoy lt.	34 51 5	11 10	
	C. Grego	34 56 5	34 6 5	Kadijah, tower, 50f.	35 14	11 10	
	Larnaca, lt. F 42f.	34 55 2	33 37 7	Mehudiah, Castle	35 30 4	11 5	
	C. Chiti, l. tow.	34 49 9	33 36 2	Kuriah Is., lt. F 98f.	35 48 5	11 3	
	Limassol, lt. F 25f.	34 40 2	33 17	Monastir, fort Ghadir	35 45 4	10 50 7	
	C. Gatto, l.	34 33 7	33 2	Soussa, lt. F	35 49	10 39	
Tunis	C. Bianco, A	34 38 2	32 42 2	Jebel Zaghwane, 4078f.	36 21 5	10 7 2	
	C. Papho	34 44 8	32 23 7	Hammanet Castle	36 23 3	10 37 2	
	EGYPT.			Ras Mahmur	36 27 5	10 49	
	Port Said, lt. Fl. 175f.	31 15 7	32 19 2	Kalibia, lt. F 269f.	36 49 7	11 8	
	Nile, Rosetta mouth	31 30 5	30 19 5	Ras al Aswad (b/k. Hd.)	36 58	11 7	
	— Damietta mouth, Kawa }	31 33	31 52	C. Bon. 1290f., lt. Int. 412f.	37 5	11 2 7	
	Burun	31 24	31 48	Zembra, $\frac{1}{2}$, 2 $\frac{1}{2}$ m. sum. 1324f.	37 7 4	10 48 5	
	Damietta, Engl. Cons.	31 31	31 51	Jebel Israa, 2536f.	36 36	10 20 5	
	— lt. Rev. 180f.	30 21	31 15 5	Tunis, Goleta, \square , lt. F 39f.	36 48 5	10 15 2	
	Cairo, tow. of Janissaries	29 58 6	31 7 5	C. Carthage, lt. R 482f.	36 52 4	10 18 2	
Egypt	Great Pyramid, sum. (487f.) now 460f.	29 58 6	31 7 5	Piana I., EW 1m., lt. F 65f.	37 10 8	10 20 2	
	Aboukir, B., Nelson I.	31 21 4	30 6	Cani, rka, $\frac{1}{2}$ 2m. lt. F 129f.	37 21 2	10 8 0	
	ALEXANDRIA, \square , lt. R 180f.	31 11 7	29 51 7	Benzert, fort, lt. F 46f.	37 17	9 53	
	Arab's tower	30 59 7	29 34 7	C. Il Guerra	37 19 9	9 52 2	
	Ras al Kanais, pt.	31 15 4	27 52	Fratelli, rka, $\frac{1}{2}$, West Rock ...	37 17 9	9 24 2	
	Marsa Mutroo, \square , w. Pt. La- beit	31 22 9	27 15 5	Galita I., $\frac{1}{2}$ 3m. pk. Monte }	37 31 3	8 56 2	
	Ishailah rks., E one, 58f.	31 31 3	26 38 7	Sorelle, rka, Avenger reef ...	37 23 7	8 37 5	
	Ras Haleimah	31 37 5	26 0	ALGERES.			
	TRIPOLI.			Taharca. N tow.	36 58 0	8 45 5	
	Ras al Milhr	31 53 2	25 5 7	La Cala, \square , lt. F 55f.	36 54 0	8 27 5	
Tripoli	Tebbruk, \square , Saracen gate	32 5	23 59 2	Bona, North jetty Pt., lt. F 63f.	36 54 5	7 47	
	Bomba, or Bhurdah I.	32 22 6	23 13 7	C. de Garde, lt. F, Fl. 469f.	36 58 0	7 48 5	
	Ras al Tyn, sum.	32 37 7	23 7 8	Ferro I	37 5	7 20	
	Dernah, lt. Rev. 92f.	32 46 0	22 46	Ras Hadid, or C. de Fer, lt. }	37 5 1	7 11	
	Pt. Zawawi (Ras al Hilil)	32 57	22 8	Rev. 218f.	37 5 1	7 11	
	Marsa Sousa, \square , Arsenal	32 54 9	21 56 5	Philippeville, 2 lts. F	36 52 8	6 53 0	
	Ras Sem	32 57	21 42 2	Srigina I., lt. F 180f.	36 56 3	6 53	
	Tolmeitah, pt. of the Kothon ..	32 43 1	20 53 2	Coilo, lt. F 33f.	37 1	6 36 5	
	Benghazi, lt. Rev. 72f.	32 6 8	20 2 7	C. Bugaroni, (Peak 3579f.) }	37 5	6 29	
	Gharah I.	30 47 5	19 54	lt. F 564f. on cape	36 57	6 14	
Algeria	Marsa Boureigah, ruin	30 25	19 35 5	Marsa Zeitoun	36 50 0	5 44 7	
	Bouskeifa I.	30 17 5	19 9	Jidjelli, 2 lts. F	36 50 0	5 44 7	
	Ras Ben Gahouah, ruin	30 46 3	18 14	Mt. Babur, 6200f.	36 32 5	5 27	
	Marsa Zafrun, Port Chebek ...	31 12 6	16 36	Bougie, pier end, lt. F 23f.	36 44 5	5 4 2	
	C. Misratah, Ras Torug, lt. }	32 22 4	15 13 2	C. Carbon, lt. R 722f.	36 46	5 6 3	
	Fl. 138f.	32 22 4	15 13 2	Pisan, rks, $\frac{1}{2}$ 1m., w., W pt.	36 49 8	4 59 5	
	Marsa Ougrah, Ras al Tabiah	32 33 5	14 26 2	Mt. Azafoun, 4360f.	36 50	4 25	
				C. Bengut, lt. F 208f.	36 55	3 53 2	
				C. Tedlès	36 55	4 9	
				Dellys, pier, lt. F 33f.	36 55 5	3 55	
				C. Matifou, lt. Fl. 242f.	36 48 9	3 14	

TABLE 10

563

MARITIME POSITIONS

(39)	Places	Lat. N	Lon.	(40)	Places	Lat. N	Lon. W
Algiers	Algiers, Marine I., lt. R 115f....	36° 47' 3"	3° 3' East	Canaries	Grand Canary, NS 25m., } NW pt.....	28° 9' 6"	15° 43' 2"
	— OBSERVATORY	36 47 8	3 2 2		— Palmas, mole head, lt. F 25f.	28 7 0	15 25
	C. Caxine, lt. Rev. 210f.	36 49	2 56 5		— Maspalomas pt., lt. F 190f.	27 43 8	15 34
	Sherschel, [I], fort lt., F 121f.	36 36 8	2 11		— Isleta, $\frac{1}{2}$ 2m., lt. F, Fl. 817f.	28 11 0	15 25 5
	C. Tenez, lt. R 292f.	36 31	1 18		Tenerife I., N pt., Anaga rk....	28 36 6	16 8 5
	Palomos I., rk. $\frac{1}{2}$ 85f.	36 26 3	0 55 7		— Sta. Cruz, Brit. Consul. w'''	28 28 2	16 14 7
	Mostaghanem, lt. F 115f.	35 56 3	0 4 5 West		— S pt. or Pt. Rasca.....	28 0 0	16 41 2
	Arzen I., lt. F 66f.	35 52 5	0 17 7		— Peak, 12, 172f.	28 16 5	16 39 0
	C. Ferrat, 1, $\frac{1}{2}$, lesser sum.	35 54 3	0 23 5		— W extr., l	28 20 5	16 55
	Pt. Abuja, 2050f., pt.	35 53	0 29		— Orotava, port.....	28 25 2	16 32 0
Morocco	Oran Mursa el Kebir, lt. F } 121f. }	35 44 3	0 41 7	Gomera, EW 14m., W pt.....	28 6 5	17 20 5	
	C. Faicon, $\frac{1}{2}$, 8, lt. Rev. 340f....	35 46 4	0 47 2	— Sum. 1440f.	28 6 7	17 13 5	
	Habibas Is., $\frac{1}{2}$ 3m. w. sum.	35 43	1 8	Lierro, or Ferro, $\frac{1}{2}$ 15m. N } extr..... }	27 50 5	17 55	
	lt. F 340f. }			— W extr., Orchilla pt. (or Meridian of Ferro) }	27 42 5	18 10	
MOROCCO.				Palma, Cumpida Pt., lt. R 207f.	28 50	17 47	
Zafarine Is., EW $\frac{1}{2}$ m. W } ext. sum. 441f., lt. F }	35 11 0	2 25 7	— S pt. or Fuencaliente.....	28 26 7	17 49 7		
Melilla, [I]	35 18 3	2 57 0	— Sta. Cruz, fort San Miguel	28 40 5	17 44 5		
C. Tres Forcas, N pt. mid.....	35 27	2 59	Azores.				
Alboran I., $\frac{1}{2}$ 1m., lt. F 115f.	35 58	3 2	Corvo, $\frac{1}{2}$ 4m., $\frac{1}{2}$, N pt.....	39 43 5	31 7 2		
C. Quillates.....	35 16 5	3 45 5	Flores, NS 9m., N extr.....	39 31 6	31 13 0		
Mostaza	35 9 7	4 26 5	— Sta. Cruz, fort	39 27 0	31 8 0		
Tetuan, Custom-ho.	35 37	5 18	Fayal, $\frac{1}{2}$ 11m., W pt.	38 35 6	28 50 5		
Centa, lt. R 590f.....	35 53 6	5 17	— Horta, Sta. Cruz, castle, } lt. F 28f. }	38 31 7	28 38 5		
Tangier, Battery, lt. F 58f.....	35 47 2	5 48 2	Pico, $\frac{1}{2}$ 25m., Pk. 8400f. ? ...	38 28 0	28 25 0		
ATLANTIC OCEAN.				— E pt.	38 24 7	28 3 0	
Madeira.				St. George, $\frac{1}{2}$ 29m., S and E pt..... }	38 32 5	27 46 7	
Porto Santo, $\frac{1}{2}$ 7m., 1660f.	33 5 0	16 19 5	— N and W pt. outer rk.	38 45 2	28 20 2		
Styx, rks. NW of P. Santo, 12	33 11	16 24	Graciosa, $\frac{1}{2}$ 7m., W. pt.	39 4 2	28 4 7		
Desertas, $\frac{1}{2}$ 12m. sum. 1610f.	32 31 3	10 30 7	— Praya, castle	39 3 2	27 58 5		
— S. or Agulha pt.	32 23	16 27	Tercera, EW 16m. Praya	38 43 7	27 4 2		
Madeira, l. W. 30m., E pt., } lt. F, Fl. 343f. }	32 43 4	16 39 5	— Angra, Custom ho.	38 38 9	27 13 7		
FUNCHAI, BRIT. CONS. [I]	32 38 3	16 54 5	— Sum. 3495f.	38 43 5	27 20 5		
— PONTINHA, lt. F 112f.....	32 37 7	16 55	St. Miguel, F, E or Arnel } pt., F, Fl. 219f. }	37 49	25 8 2		
Pico Ruivo, 6100f.....	32 45 0	16 57 0	— Delgada, lt. F 20f., Cust- om-ho. quay	37 44 2	25 40 7		
West, or Pargo pt.	32 48	17 17	— West pt. or Pt. Ferraria, } lt. bad	37 51 7	25 52 2		
Salvages, 2 grps., $\frac{1}{2}$ 15m. } NE breaker..... }	30 8 6	15 49 7	St. Mary I., $\frac{1}{2}$ 9m., town	36 56 6	25 9 5		
Great Salvage, $\frac{1}{2}$ 1 $\frac{1}{2}$ m., W sum.	30 7 5	15 51 2	— mid., sum. 1660f.	36 58 5	25 6 2		
Great Piton, $\frac{1}{2}$ 3m., sum.....	30 1 0	16 0 2	Formigas, NS $\frac{1}{2}$ m., 60f....	37 16 2	24 47 5		
Canaries.				Dollabarats shl. [1c.], 11f. 8 ...	37 13 7	24 44 5	
Aleganza, $\frac{1}{2}$ 2 $\frac{1}{2}$ m., 939f., } Pt. Delgado, lt. R 57f. }	29 24	13 29	Cape Verdes.				
Clara, $\frac{1}{2}$ 1m., N pt.	29 18 0	13 32 2	St. Antonio, $\frac{1}{2}$ 22m. N pt., } lt. F 23f. }	17 12 0	25 5 7		
Graciosa, $\frac{1}{2}$ 5m. w. SW pt....	29 12 7	13 32 7	— West pt.....	17 4 0	25 22 5		
East rock, [3c.]	29 16 4	13 20 0	— Sum. 7400f.	17 4	25 17		
Lanzarote, $\frac{1}{2}$ 32m., NW pt....	29 2 7	13 48 0	— Tarafal B. wat. place	16 57 2	25 19 0		
— S pt.	28 50 0	13 47 0	— South pt.	16 54 7	25 18 5		
— Arcicif, (Port Naos, [I]) } fort Gabriel, 2 lta. F 47 } & 35f. }	28 57 0	13 32 5	— NE, Bull pt., lt. F, Fl. 543f.	17 7	24 59 0		
Lobos I., $\frac{1}{2}$ 2m., N pt., lt. } F 93f. }	28 45 5	13 48 5	St. Vincent, EW 16m., S pt....	16 47 0	24 59 0		
Fuerteventura, $\frac{1}{2}$ 53m., NW pt.	28 42	14 1	— PORTO GRANDE, [I], Bird } I., lt. F 306f. }	16 54 7	25 0 7		
— Port Cabras	28 29	13 51 7	— FLAGSTAFF OF TELE- GRAPH OFFICE	16 53 3	24 59 5		
— S pt. or Pt. Jandia, l, lt. } Rev. 108f. }	28 3 0	14 32	St. Lucia, $\frac{1}{2}$ 7m., N pt.....	16 49 0	24 47 0		
			— Village, ruins, SW side, w.	16 45 0	24 45 5		
			Branca, $\frac{1}{2}$ 3m., N pt.....	16 41 0	24 41 5		

865

MARITIME POSITIONS

(43) Places		Lat. N	Lon.	(44) Places		Lat.	Lon.																																																																			
Is. de Los. EW 6m., w', r, } Crawford Id., Engrl. Estab. } — W one, Tainara I., 8 l. } T, & E, W pt. } Sallahtok Pt. } Yellaboi I., EW 2m., ♀, W cliff } C. Sierra Leone, lt. F.F.I. 75f. [5]. } Freetown, N battery } False C. Sierra. L. } C. Shilling, l., ♀, sum over ... } Bananas Is., 4 th 5m., w, } Gov. ho. } Maitain Is., EW 5m., out-rk. } Shls. of St. Ann, NW patch: s, } Turtle Is., l, N Id., [3m.] } Sherboro I., W pt., or C. St. } Ann, ♀ } R. Shebar, E entr., or Mana Pt. } R. Gallinas, Kamasoun I. } [1m.], W elbow } C. Mount Riv., town. } C. Mount, w, pk., 1060f. } C. Mearado, 8 l. ♀, w, lt. } F 240f. } Mourovia, Govt. ho. } Marshall, Agent's ho. } Grand Bassa, Amer. Agent's ho. } Tabocannee rk. } Trade Town } Mt. Tobacco, 830f. } Custos, factory } R. Sanguin, r, b, Pt. Sanguin } Bloorbarra pt. } Setra Kroo. } King William Town, Europ. } factories } Coley rk 1 }		9°27'4	13°48'5	Porto Novo (no port) Badagry, shore hut Lagos, entr. [4m.] bar 3 f., lt. F 70f. } Oddy Sand beach R. Benin, bar 1st. NW pt. R. Forcados, entr. S pt. R. Quorra, or Niger, E pt. C. Formosa, l, ♀ (no distinct } cape) } New Calebar R., entr. 1st., W pt. } Bonny R., entr. 1st., E pt., } T, r, rough corner. } Old Calebar, Tom Shot's Pt. Mt. Cameroons, 13760f. Cape Cameroons. Rumby Mountains, sum. Qua Mount, 25 l. Ambas B., Mondoleh I. [4m.] } A, ♀, w, S pt. } Suellata pt. (rf. 3m. off) The Mitre, 3940f., S sum. C. St. John, ♀ Corico I., l, ♀ C. Es ciras Gaboon R., r, w, Libreville, lt. F } King George Town }	6°23'	2°35'	6°24'2	2°53'2	6°24	3°27	6°20	4°31'7	5°46'0	5°4	5°22'0	5°19'2	4°17	6°4	4°15	6°11	4°23	7°1	4°23	7°8	4°36	8°19	4°13	9°12	3°55	9°30	4°57	9°18	5°15	8°51	3°58'7	9°12'5	3°51	9°35	1°20	9°57	1°9'7	9°22	0°55'9	9°20	0°38	9°21	0°23	9°26	0°8	9°44	3°48	8°43	3°35	8°47	3°13	8°43	3°46'0	8°47'5	1°43	7°23	1°39'5	7°26'5	1°21'1	7°17'5	0°14'7	6°33	0°20'5	6°43	0°0'5	6°30	1°24'3	5°38'2	1°28'6	5°36'7
Gulf of Guinea.				ISLANDS IN SOUTH ATLANTIC.																																																																						
C. Palmas, lt. F Tafon pt. Kadahlboo bluff Oval Mountain, 1315f King George Town C. Lahou Head of the Bottomless Pit, 100 } Assini R., entr. bar, 1st. } Apollonia (abandoned). Axim, Dutch fort C. Threc Pis., 8, 2m., lt. F 75f. } Dix Cove, f, fort } Elmina, Dutch fort C. Coast Castle, lt. F on Fort } William, 192f. } Accra, Fort James, [1, 0, h. } F 50f. } Camel's Hump, 1200f. }		4°22'1	7°44'2	Ascension, EW 7½m., Fort } Thornton, lt. F [5] } — Green Mtn., 2820f. } — Cross Hill, 850f. on with } Gr. Mt., S 71° E }		7°55	14°25	7°57	14°21	7°55'7	14°25'0	15°57	5°40'5	15°55'4	5°42'5	3°52	32°28	3°50'4	32°25'5	3°51'5	33°49																																																					
R. Volta, W pt., l, entr. C. St. Paul, l (no distinct } cape), ♀ }		5°46'0	0°41'2	St. Helena, 4 th 9m., Diana's } pk. 2700f. } — OBSERVATORY, f 1° G.M.T. }		15°57	5°40'5	15°55'4	5°42'5	3°52	32°28	3°50'4	32°25'5	3°51'5	33°49																																																											
Jella Coffee. Quitta Danish, r, SE bast. Little Popo, w, l, NW shed. Gr. Popo (bar. 8). Whydah, fl. st.		5°52	1°0	Fernando Noronha, Is., 4 th } 6m., S and W. extr. pt. .. }		3°52	32°28	3°50'4	32°25'5	3°51'5	33°49																																																															

West

MARITIME POSITIONS

(45)	Places	Lat. S	Lon.	(46)	Places	Lat. S	Lon. E.
	Trinidad I., $\frac{3}{4}$ 4m., 2020f. S. pt.	20° 31'	West 20° 19'		Mercury I. [3m.]	25° 46'	15° 0'
	Martin Vaa. 3 Is., NS $1\frac{1}{2}$ m. ...	20 28	28 51		Angra Pequena, F, W N 10m., SW or Pedestal Pt. }	26 38.4	15 8
	Tris'an d'A Cunha, [6m.] }	37 2.7	12 18.5		Seal I. [1m.], w. }	26 34	15 14
	Waterfall, N side				Possession I., $\frac{2}{3}$ 3m., rfs. off, w., 8 pt. }	26 58	15 13
	Inaccessible Is., 16 L., \sim , L. w, W one	37 17	12 36		Archod rk., 100f.	27 20	15 19
	Nightingale I. [2m.]	37 27	12 29		Orange R., \sim , bar,	28 38	16 28
	Gough's I. [5m.], 4385f., N pt. }	40 19	9 44		C. Volta, w,	28 44	16 32
					Koussie R.	29 40	17 10
	AFRICA, West Coast.				CAPE COLONY.		
	Nazareth R., Fetish town, W entr. }	0 37	East 9 1		Olifant's R., or Elephant's R. .	31 38	18 12
	C. Lopez, l, T, F	0 36.0	8 43		C. Doukin	31 54.2	18 19
	C. St. Catherine, [F]	1 51	9 6		C. Descead, l, h	32 18	18 23
	Settee R., a high F	2 23	9 26		Berg R., entr. (w' 5m. up) ...	32 45	18 13
	Mayumba B., F, Matooti Pt.	3 22.7	10 38		Britannia rk.	32 38	17 41
	Loango R., entr.	4 39.5	11 45		St. Helena B., Pt. St. Martin, l	32 40	17 59
	Black Pt., B., [F], w', Sandy Pt., l	4 49	11 46		Pt. Paternoster, or W pt.	32 42.2	17 54.7
	Lendana Pt., lt. F 111f.	5 11	12 8		Sunken rock ?	32 51	17 46
	Kabenda Pt., lt. F 50f.	5 32	12 11		Saldanha B., F, r, w, Ship rk., at N pt. }	33 1.7	17 54
	Congo R., F., Pt. Padron	6 8	12 13		— Houfjes B., B, Hout. pt.	33 0.1	17 58.0
	— S. entr., or Shark's Pt, T, } S, 2c. }	6 4.6	12 17		— Schapen I., w', W pt.	33 4.2	18 1.0
	Foreland bluff, lt. F 78f.	7 15	12 53		Dassen I., $\frac{1}{2}$ 2m., l, \sim , w., S 2m., cent. }	33 26.2	18 6.7
	Ambria, F., lt. F	7 52	13 8		Bock Pt.	33 33.8	18 19
	Dandé Pt. and riv.	8 28	13 19		Robben I., $\frac{1}{2}$ 1 $\frac{1}{2}$ m., lt. F 154f.	33 49.2	18 22
	C. Lagoetas, rka., lt. F, Fl. 210f.	8 46.1	13 17.5		Table B., Green Pt., lt. F } 65 ft. B. }	33 54.2	18 24.5
	St. Paul de Loando, B, B. } d. st. B. }	8 48.3	13 13		Devil's Peak, 3270f.	33 57.2	18 26.7
	Palmainrinhas Pt., lt. F, Fl. 57f.	9 4	13 0		CAPE OBSERVATORY, F 1 $\frac{1}{2}$ G.M.T. 11 $\frac{1}{2}$ 46" 5" }	33 56.0	18 28.7
	C. Leda, h, F, pt.	9 46	13 17		Cape of Good Hope, lt. Rev. 816f. }	34 21.2	18 29.5
	C. St. Bras, B, F.	10 1	13 22		Bellow's rk.	34 23	18 29.7
	Nova Redonda, r, w, l,	11 12	13 54		Simon's B., Dk. yd.	34 11.3	18 26.0
	Quicombo B., S 1m. out, } w, S pt. }	11 20	13 48		C. Hangklip	34 23.2	18 49.5
	St. Philip de Benguela, F, w, } St. Philip's Bonnet, lt. F 394f. }	12 33.9	13 18		Danger Pt., l, rks. 2m. bluff ..	34 37.8	19 17.7
	Logito R., w' r	11 58.5	13 46		Quoin Pt.	34 46.8	19 38.5
	Lobito, B, F, w., pt.	12 20	13 32		C. Agulhas, S. extr. of Africa, lt. F 128f. }	34 49.7	20 0.7
	Salinas Pt., l, F at pt., lt. F, B	12 53	12 59		Pt. Struys, S 3m.	34 41.4	20 14.2
	Elephant B., B, R, F w., Monks, or Friars, rks. } 12 or 14f. }	13 14	12 42.7		C. Infanta, S pt., Sebastian B.	34 28.4	20 51
	C. St. Mary, T, w.	13 25	12 33		C. Barracouta	34 26.4	21 18.4
	Little Fish B., Ponta do Giraul, lt. F 64f.	15 9	12 12		C. Vacca	34 19.7	21 55
	C. Negro, 200f., l pt., Diaz's Pillar	15 40.7	11 58		Flesh Pt.	34 17.7	21 57.0
	Port Alexander, B, F w.	15 46	12 0		C. St. Blaize, lt. F 240f.	34 11.2	22 9.5
	Great Fish B., w, P, Tiger Pt., T, S, 2c. }	16 30.2	11 46		Knysna R., B, entr. l	34 5	23 37
	Nourse R. (temporary)	17 25	11 54		Plettenburg B., w, r, F, S pt. or Seal C. }	34 6.5	23 25
	C. Frío	18 23	12 2		C. St. Francis, rf, B, T, lt. Fl. 118f.	34 11.6	24 50
	C. Cross (or Sierra)	21 50	13 57		C. Recife, l, lt. Rev. 93f. (rf. 4m.)	34 1.7	25 42.2
	Mt. Colquhoun, 17 or 18 l.	22 32	-		Algoa B., Port Elizabeth, lt. F 225f. }	33 57.7	25 37.7
	Walvich B., B, F w., factory, lt. F 24f.	22 57	14 30		Bird Is., $\frac{1}{4}$ 3m., E pt. lt. F 80f.	33 50.5	26 17.2
	Port Sandwich, or d'Ilheo, B, F F	23 30	14 25		Pt. Padron	33 46.5	26 28
	William's Bird I. [2c.], rf. SW 5m., \sim , l, }	24 37.4	14 32		Kowie R., entr. Port Alfred, lt. F 40f. }	33 36	26 54.2
					Grt. Fish Pt.	33 31.4	27 7
					— R., entr.	33 29.6	27 8.5
					Keiskama, lt., entr. W pt.	33 16.7	27 29.5
					Cove rks., centre	33 5.1	27 49.2
					Buffalo R., East London, F 45f.	33 1.7	27 55.0
					C Morgan	32 42.1	28 24.7
					Hole in the Wall	32 3.2	29 1.0

West Coast of Africa

Cape Colony

TABLE 10

567

MARITIME POSITIONS

(47)	Places	Lat. S	Lon. E	(48)	Places	Lat. S	Lon. E
Kafferland	Rame Head.....	31° 48' 4	29° 14' 5	Mozambique	Pomba Bay, \square , N pt., entr., T	12° 55' 8	40° 31' 2
	St. John's R. entr.....	31 34' 5	29 28' 7		Arimba Head	12 38' 2	40 39' 0
	C. Natal	29 53' 0	31 2' 2		Ibo I., $\frac{1}{2}$ 5m., Ibo Bluff, lt. }	12 20' 0	40 38' 5
	Port Natal, \square , bar δ , S pt. }				F 51f.		
	of bay, lt. Rev. 282f. }	29 53	31 4		Mahato I., $\frac{1}{4}$ 2m., N and E pt.	11 58' 2	40 36' 2
	Fisher's R.	29 16' 3	31 33		I. dos Mattoes, [$\frac{1}{2}$ m.], rfs. }	11 49	40 37
	Dunford Pt.	29 0' 2	21 51' 5		2m. out	11 28' 5	40 40' 7
	C. St. Lucia	28 32' 5	32 27' 5		Fungu Namegao, E. pt. of reef	11 28' 5	40 40' 7
	St. Lucia R., enr.	28 26' 0	32 26' 5		Tambuzi I., EW 2m., rfs. }	11 21' 3	40 41
	C. Vidal	28 9' 6	32 38' 0		2m., w'.....	11 18' 5	40 22' 5
Goldown's Blind river	26 55	32 53	Mazimba, fort.....	11 18' 5	40 22' 5		
AFRICA,				MADAGASCAR.			
East Coast.							
Delagoa B., C. Collato, 260f.	26 4' 0	32 58	S extr., C. St. Mary	25 38' 9	45 5' 0		
— C. Inyack, N pt. of St. }			Star bk., SW part, π	25 39	45 21		
Mary I., 265f. }	25 58' 0	33 0	Star reefs, NS 3 l., T W, S one	25 25	44 16		
Port Melville, Elephant I., }			Leven I., [$\frac{1}{2}$ m.], centre	25 12' 5	44 16' 0		
w SW side, Gibbon B. pt. }	25 58	32 54' 2	Barracouta I., [$\frac{1}{2}$ m.].....	25 3' 0	44 5' 5		
English R., Keuten pt., lt. }			St. Augustine B., Tent rk.	23 35' 4	43 43' 7		
F 134f. }	25 58' 8	32 36	Noss Veh, or Sandy I.	23 38' 4	43 36		
Innampura R., entr.	25 11' 6	33 31' 5	Murderer's Bay, N pt.	22 12' 5	43 16' 0		
Pt. Zavora R.	24 28' 5	35 12' 5	Murder I., rf. 2m., SW	22 5' 3	43 13' 5		
C. Corrient s, 11 l., small rk., }			C. St. Vincent	21 52' 5	43 18' 5		
15f. }	24 5' 5	35 30' 5	Mouronilava, w, r, γ	20 18' 3	44 17' 5		
Barrow Hill, Burra, lt. F }			Barrou Is., l, ϕ , S danger ..	18 41	44 1		
80f. }	23 45' 5	35 32' 2	— Smyth's islet, on rf. $\frac{1}{2}$ }	18 18' 1	43 44' 7		
Innamban B., \square , town.....	23 49' 5	35 3' 5	Coffin I., l, (δ 2 l.).....	17 29' 0	43 45' 2		
C. Lady Grey, 95f.	22 55	35 36' 5	NW extr., C. St. Andrew.....	16 11' 4	44 29		
C. St. Sebastian, 10 l., pt. }			Chesterfield bk. [$\frac{1}{2}$ m.], γ	16 17	43 53		
225'..... }	22 6	35 29	Boyanna B., W or Table C....	15 59' 0	45 16		
Bazarouta Is., N pt., or C. }			Bemba ooka B., \square , r, E or }	15 42' 9	46 18' 5		
Bazarouta, 390f. }	21 31' 0	35 28' 0	Majunga Pt.	15 42' 0	45 55' 7		
Inverarity sh., Mi-adjuano ...	20 42	35 10	Makumba I.	15 11' 7	46 57' 5		
Chiuanan I. [5m.], l, ϕ , }			Majambo B., \square , entr. W pt....	14 3' 3	47 24' 5		
Singune, lt. F 36f. }	20 38' 2	34 53' 5	Nareenda B., \square , entr. W pt....	14 36' 9	47 41' 0		
Sofala R., bar. 12f. fort.....	20 10' 7	34 43	Luza R., bar δ , \square , entr.....	14 30' 7	47 33' 2		
Pungue R., Beira, lt. red	19 50' 2	34 50' 5	Saucasee I., NS $\frac{1}{2}$ m., N pt....	14 15' 0	47 47' 2		
Zambesi R., Kongoni R.	18 53	36 11' 7	McCluer Pt.	13 53' 5	47 45		
Kiliman R., bar sf., l, ϕ , }			Eranda I., NS 2m., N pt.	13 28' 2	48 13' 0		
Pt. Tagalane, lt. F 52f. }	18 1' 4	36 57	Pa-sandava B., Ninpin I., }	13 28' 2	48 27' 7		
Acorn rk.	17 37	38 13' 5	lt. F 184f.	13 30' 4	48 0		
Primeira Is., Casuarina, or }			Passage I., [$\frac{1}{2}$ m.]	14 6	48 18		
Raza I., $\frac{1}{2}$ W, w, b	17 6' 5	39 4	Dalrymple B., \square , r, ϕ , b, entr.	13 12' 2	48 16' 7		
Mt. Cockburn.....	16 29	38 56	Martahoulah Pk.	12 49' 5	48 37' 0		
Angoche Is., Wst., or Moma }			Noss Beh I., NS 13m., N pt....	12 27' 7	48 43' 7		
bk. [1m.]..... }	16 47	39 32	Minow I., N. pt.	12 16' 7	48 39' 2		
— Mafamede I., l, ϕ , rfs., cent.	16 20' 5	40 2	C. St. Sebastian (ls. 5m. }	12 3' 3	49 9' 5		
— R., Custom ho.	16 13	39 56' 5	off), pt.	11 57' 5	49 17' 0		
St. Antonio, R., S pt., rf. }			Woody I., [$\frac{1}{2}$ m.]	12 34' 5	49 9		
[2m.]..... }	15 57	40 9	Port Liverpool, \square , entr. N pt.	12 13' 8	49 21' 5		
Huddart's sh.	15 47	40 26	N extr., C. Amber.....	12 35' 0	49 37' 7		
Moginkwah R., Funco pt.	15 32	40 29	Amber Mountain	12 44' 2	49 45' 0		
Port Mocamba, N pt., entr., }			British Sound, \square , entr., Cla-				
T, \square , pk., ab. 2000f. }	15 8	40 35	renee Id.				
Mozambique, \square , Sebastian	15 0' 7	40 44' 7	C. Lowry				
Fort fl. staff, lt. F. green 42f. }			Porte Looké, \square , Bathurst Pt				
Mt. Pao	14 50	40 25					
Mount Meza, 1095f.	14 43	40 38					
Titangonya I., $\frac{1}{2}$ 2m., S pt....	14 51' 0	40 50' 0					
C. Melamo	14 25' 0	40 50					
Penda sh., E estr.	14 15' 0	40 50' 0					
Loguno Peak.....	14 21' 0	40 35					
Sorisa Pt.	13 32' 8	40 35' 2					
Mauchané Ft.	12 58	40 36					

MARITIME POSITIONS						
(49)	Places	Lat. S	Lon. E	(50)	Places	Lat. Lon. E
Madagascar, E. Coast	Port Leven, \square , Linga rk.....	12°46'5	49°53'2	East Coast of Africa	Quiloa, Ukyera reef, E extr ...	South 8°53'5 39°39'
	Noshe Barracouta, [1m.].....	12 48	49 55		Songa I., $\frac{1}{2}$, $\frac{1}{2}$ m., SE pt.....	8 32'5 39 31
	Andrava B., Berry Hd.....	12 56'5	49 54'5		Mafia I., $\frac{1}{2}$ 9 l., W. or Kis- mani pt.....	7 56'5 39 35'7
	Manambattoo Vill., $\frac{1}{2}$, Vohemar Pt.	13 14' 49 56'5 13 23'5 50 12			Panna Pt. extr.	7 20 39 34'2
	Mananhar, Table Hill	14 39'7	50 13'7		Iatham's I., [2c.], l. sd. mid.	6 54'2 39 56
	C. East, outer l.	15 15'5	50 29'5		Zanzibar I., $\frac{1}{2}$, 16 l., $\frac{1}{2}$, S pt. or Kizinkaz, w., lt.	6 28'5 39 30'0
	Durnford Nosa, pt.....	16 0'0	50 9'5		— ENGLISH CONSULATE — N pt., or Nungwe Pt., lt.	6 9'7 39 11'2
	Port Choiseul, town	15 27'3	49 50'2		Rev. 105f.	5 43 39 18
	C. Ballones, pt.	16 14'0	49 52'0		Mazeewy I. and rfs., [1m.]...	5 30'0 39 6'0
	Tangiang, \square , fl. st.	16 42'5	49 44'2		Tungaty, Mt., 15 l., S pk Pemba I., NS 13 l., l., $\frac{1}{2}$, S or Said pt.	5 22'3 38 52'0 5 29'3 39 39
	St. Mary's I., $\frac{1}{2}$ 11 l., N. pt. — I. Madame, or Quail I., on } W side, Establ., lt. F 31f. }	16 40'5 50 2'7 17 0'0 49 52'0			— North-East pt.	4 54'2 39 51'5
	Fenerive, town	17 23'0	49 26'2		— Port Chak chak, \square , Mo- sal I., [1m.], SW. pt.....	5 15'7 39 37'5
	Foule Pt. Vill., r, l.	17 40'4	49 33'2		Waseen Peaks, 15 l., mid one	4 30 39 20
	Prune I., vis. 5l., $\frac{1}{2}$ Tamatave Pt., l.	18 4 49 30 18 10 49 27			Mombaza, l., $\frac{1}{2}$, w, r, P, fort.	4 4'0 39 41'0
	Fong Is., small, S one	18 26'5	49 23'7		Melinda (leopard rf. 3m.) off), Pillar	3 12'8 40 18'2
	Vaïomandri	19 17'2	49 2		Ras Gomany, N pt.	3 0'0 40 17'7
	Mahanuru, town	19 54'0	48 50'2		Ozy Pt., (Riv. $\frac{1}{2}$ 5m.; rf. 4m.)	2 37'5 40 38'5
	Fanantara, town	20 51'2	48 31'2		Lamo B., \square , W pt., or R s Kattow	2 18'7 40 56'7
	Rangasava, town	20 58'2	48 30'7		— Town	2 15'7 40 56'2
	Footak, town	24 4'0	47 30		Patta B., \square , rk.....	2 14'0 41 1'2
	Manambattoo (South), town ..	24 17'2	47 23'0		Patta, town	2 9'2 41 7'5
	Loodatoo, town	24 36'7	47 15'5		Kwyhoo I., Sat. of Juha, or Dundas Is., pk. 155f.	2 0'0 41 18'2
	St. Luce, N islet.....	24 44'7	47 12'2		Simmambaya, Settlein.	1 45'5 41 32'0
	Pt. Ytapere, extr.	24 59'7	47 5'7		Mt. Gibbons	1 12'2 41 28
	Fort Dauphin, fl. st.	25 1'3	47 0'2		Port Durnford, \square , Foot Pt., N. entr.	1 13'2 41 54'2
	Islands off Madagascar.				Tola I., huts	1 0'0 42 3'5
	Europa I., [1 l.], $\frac{1}{2}$, 65f.	22 22'5	40 24'2		Port Kiama, Doubt rk., mid entr.	0 40'2 42 20'0
	Basas da Inda, [2 l.], T, S pt. St. Juan da Nova, [2m.] } l, s, r	21 31 39 41 17 3'5 42 47			Ki-mayo I., $\frac{1}{2}$ 3m., N pt.	0 36'8 42 22'0
	Mayotta, NS 71, Pamanzi I., lt F.....	12 46 45 15			Juba R., bar, P, entr.	0 14'5 42 39'2
	Johanna, NS 8 l., pk., E part — Town, w, r, P.....	12 15 44 27'1 12 11'0 44 22			North	
	Numachao Mohillah	12 25 43 42			Brava, town	1 6'8 44 3
	Comoro, NS 12 l., T, $\frac{1}{2}$ } NW, SE pt.	11 54 43 33			Murka, town	1 44'1 44 51
	— North-east pt.....	11 19'5 43 39			Magadoxa, town, P,	2 1'8 45 24'7
	Geyser sh., SW elbow	12 25 46 25			Murot hill	2 41'3 46 17'2
	Borneo shl.	12 14 46 12			Ras Asuad, l, l, pt.	4 34'2 48 6'0
	Glorioso I. and rfs. [4 l.], l, $\frac{1}{2}$, T, Isle du Lise, W pt.	11 30'2 47 22			Ras Awath	5 32'8 48 40'0
	Assumption I., $\frac{1}{2}$ 2 l., l, $\frac{1}{2}$, hummock on SE pt., 60f. Aldabra Is., EW 8 l., \square ? $\frac{1}{2}$ } F, W pt., 70f.	9 46 46 30'5 9 22'5 46 12'2			Ras al Khyle	7 43'5 49 45'7
	Cosmoledo Is., [3 l.], lag., no entr., F, [$\frac{1}{2}$] S; — SW, or Menai I., $\frac{1}{2}$, $\frac{1}{2}$, 40f.	9 41 47 31			Ras Mabbere, 1' N, s w, pt. E extr. of Africa, Ras Ha- foon, 800f., $\frac{1}{2}$ S, w, r, E pt.	10 26'8 51 22'0
	Astove, small, l, centre.....	10 6'5 47 45'7			Hor Hadeea, (boats)	10 34 51 10
					Ras Banna ($\frac{1}{2}$ 11m.)	11 9 51 10
					C. Guardafui (NE extr. Afric.)	11 50'0 51 16
	African Coast continued.				Gulf of Aden.	
	Lindy R., w, r, fort	9 59'5 39 43'7			Abd'l Koory, $\frac{1}{2}$ 7l., h. w, W pt	12 13'5 52 3
	Mohinga B. Vill.	9 44'4 39 44			Salt's white rks. or Kal Fa- roon [1m.], 282f., mid....	12 26 52 8
	Kiawere Hr., \square , Rushingi Vill	9 25'6 39 37'5			Brothers, 2, $\frac{1}{2}$, 4l. E, or Durji	12 7 53 16
	Pagoda, Pt.	9 17 39 33'2			Socotra, EW 70m., W extr. pt.	12 33 53 15'7
	Quila, \square , fort	8 57'0 39 31'2			— NW extr., Ras Bedoo, 800f.	12 39 53 21'7
					— Gollonsier, vill., w, r, b.....	12 41'5 53 26'7
					— Tamareed, r. w, Mosque...	12 39'0 53 59
					— E pt., Ras R'dresser, l.	12 34 54 27'7

56

MARITIME POSITIONS

(51) Places		Lat. N	Lon. E	(52) Places		Lat. N	Lon. E
Socotra	Socotra, Wadde Fellingk, w, reservoir	12° 28'	54° 13' 7"	Ras Benass, T E, 8 SE, pt., l	23° 56'	35° 47'	
	— SW pt., Ras Kattaunie, sum. over, 1465f.	12 22 5	53 29 7	Jebel Wady Lehuma, via, 100m.	24 12	35 0	
	Ras Ahleib, l, 800f. T	12 0	50 45	Wady Jumaul l., 2 2 1/2 m., l mid	24 39	35 8	
	Ras Feluk, l, 800f. T	11 57	50 38	Dadalus shl. (Abd'l Kheesan), T, lt. F 61f.	24 56	35 52	
	Meyet, or Burnt l., h, w, l, S side, 2, 430 f.	11 14	47 16	Kosair, town	26 6	34 16 1/2	
	Berberch Sandy pt., lt. F 49f.	10 25	44 59	The Brothers, 2 Is., 2 1/2 1/2 m., T, N Islet, lt. F 71f.	25 18 8	34 50 1/2	
	Zayla, r, P	11 21	43 29	Jaffatin l., Sereea pk.	27 12	33 58 1/2	
	Cape Obokh, lt. F 64f.	11 57	43 17	Shadwan l., 2 7/8 m., 700f., T, SE pt., lt. Fl. 120f.	27 27	34 2 1/2	
	Ras Bir (w' W 4m.), lt. F	11 58	43 22	Jubal l., [2 1/2 m.], T E, sum...	27 38 7	33 48	
	High Brothers, 5, 2 1/2 4m., rks., large one.....	12 29	42 23	Ashrafi Is., lt. F 125f.	27 47 3	33 42 1/2	
				Ras Ghaib, lt. F 165f.	28 20 9	33 6 1/2	
				Ras Zafarana, lt. F 83f.	29 6 5	32 39 1/2	
				Mt. Agrib. (Gharib), 5740f.	28 6 7	32 54	
				Suez, PORT IBRAHIM, S MOLE HD.....	29 56 2	32 33 1/2	
				Toor, harb., 2, w'''	28 13 7	33 37	
Red Sea, W. Coast	Jebel Searjan. volc., sum.	12 29	43 17	Mount Sinai, 7450f.	28 32	33 58 1/2	
	Dumeirah l., [1/2 m.], h, pk.	12 43	43 7 5	Ras Mohammed, l, 90f., peninsula	27 45 2	34 13 1/2	
	Asab, lt. F	13 0 5	42 44	Akunah, fort, w	29 28	35 1	
	Ras B'ilul, sum.	13 14	42 32 5	Tirahn Is., 2 3/4 m., pk., 700f.	27 55 2	34 34	
	Mohablahak Is., 3, 2 1/2 2m., SW. Flar, 40f.	13 25	42 32 5				
	Rakhmat l., 282f.	13 40 2	42 12				
	Jebel Ahayil l., 150f.	13 54	41 58				
	Barn rock, 10f.	13 59 5	41 51 5				
	Eid town.....	13 57	41 38				
	Kurdumiyat l., 180f., [2m.], h, volc.	14 7	41 39				
	Hanfulah B., Daramsas l., 25f. W. reef	14 44 5	40 51 5				
	Shumna l., lt. F 59f.	15 32	39 59 5				
	Howakel l., 2 1/2 7 m., sum., 720f.	15 9	40 14 5				
	Massowah l., [1/2 m.], w, r, b, 2, lt. F 47f.	15 38	39 28				
	Dahalak bank, SE extr., Mojeidi, [1 1/2 m.], h	15 31	40 50				
	— N extr., Harmil l., 2 5m., l, 2, E pt.	16 32	40 12				
Red Sea, E. Coast	Dahalak Kebir, 2 1/2 10 l.	15 37	40 0				
	Difnein l., 30f.	16 36 5	39 18 7				
	Towers, hill	17 38	38 43				
	Khor Nowaret, 2, r, Sha-tireh l.	18 15 2	38 19 5				
	Ras Asis.....	18 26 5	38 7 7				
	Low Sandy Is., 2 1/2 12 l., E extr., Eddom Sheikh l.	18 37	38 50 5				
	Trinkitat Harbour.....	18 41	37 44				
	Barrmusa Kebir l., [3m.], w	19 13 5	38 10				
	Sawakin, 2, w, r	19 7	37 20				
	Omm el Kurush bk., [1m.], l, sand	20 51	37 26				
	Chimney Hill	20 28 5	37 48				
	Mahammed Ghoul.....	20 54	37 9				
	Ras Raweyyah, rks., 3m., E pt.	21 3	37 19				
	Reef, 2 3m., S pt.	22 0	37 0				
	South Peak, 6900f.	21 53	36 29				
Gulf of Suez	Merza Halaib, 2, w, b, P, entr.	22 15	36 38				
	S el Is., 3, l, w, E one	22 47	36 12				
	St. John's, or Seberget l., small, 700f., T	23 36 3	36 9				

Red Sea, W. Coast

MARITIME POSITIONS						
(53) Places		Lat. N	Lon. E	(54) Places		Lat. N Lon. E
Red Sea	Zehayir I., large one, [3m.], } S. sum. 734f.	15° 2'	42° 10' 2"	Schenas, town	24° 45'	56° 29'
	Hodeidah	14 47	42 56	Dibbah, town	25 38	56 17
	Ras Zebeed, w' 1m. N.	14 7	43 45	Shām Peak, 6750f.	25 58.7	56 14.5
	Avocet rock, 8	14 22	42 41.7	C. Mussendom Peak, 875f.	26 21.9	56 32
	Jebel Zukur I., 2047f., 2½ } 10m., A, High islet, 216f. }	14 5.2	42 45.2	Great Quoin, 540f.	26 30	56 31
	— Tongue I., 166f.	13 53.4	42 42.2	Ras Sheikh Maand... ..	26 15.4	56 13.2
	Harnish Is., 1335f., NS 6 l., }	13 47.2	42 47	Shām, fort, r, w', P'	26 1.4	56 5.5
	Haycock I.	13 38.2	42 35.5	Ras el Khaymah, r.	25 48	55 57
	— SW rocks, 22f.	13 19	43 14.0	Shargah, w, 3,	25 22	55 24
	Mocha, Pier end	12 41	43 27	Abūthabi fort.	24 29	54 21.7
Arabia, S. Coast	Bab el Mandeb, pk.	12 39	43 26	Sir Benī Yās, N pt.	24 21.5	52 38
	Perim I., [4½m.], 11, lt. R } 249f. on summit	12 39	43 26	Rug Zakkum shl. [3]	24 48.5	53 46
				Ras Luffan	25 54	51 33
				Sir Abū Neyr, NS 2½m., N } pt. 240f.	25 15	54 13.5
				Zirkuh I., 540f., S pt.	24 52	53 5.2
				Girneyr I., 190f.	24 56	52 52
				Dās I., [1½m.], S pt., 145f. ...	25 9	52 53
				Arzench, 200f.	24 46	52 34
				Dalmeh, 244f.	24 33	52 19
				Deyni, 9f.	24 57	52 24
Persian Gulf, S. Coast	Ras Marshigh, lt. F 244f.	12 45	45 3	Shirāao I., 40f.	25 2	52 14
	Sugra, w', r, Castle	13 21.5	45 40	Halul, 180f.	25 40	52 26
	Howtha, w', r, F.	13 25	46 45	Ras Rekken	26 11	51 13
	A barn-like pk., 5284f.	14 4	47 32	Shah Allum shl. [2½]	26 25.5	52 31
	Ras Khelb, l, sandy, no point	14 2	48 40	Bahrain I., Manauah, town, r, w	26 14	50 35
	Makalleh	14 31	49 7	Maharag I., N pt.	26 18	50 38
	Jebel Dhebah, a table land ...	14 41	49 26	Rennie shl. [2½]	27 3.5	50 42
	Shahah, Sultan's resid., r, w, ...	14 43.7	49 35	Al Krān, 5f.	27 43	49 50
	C. Bogashu	14 49	50 4	Herguz, 3f.	27 56	49 42
	Palinurus shl. 2½fm. 2½ 2m., }	14 53	50 39	Araby, 3f., sandy	27 47	50 11
Persian Gulf, N. Coast	— T 8 pt.	15 39	52 16	Farsē, 10f., sandy	27 59	50 10
	C. Fartak, 26 l., l.	16 38	53 3	Ras al Ghar	28 11	48 39
	Ishubat Ali	16 55	53 52	Ras Mushāb, A	28 49	48 47
	Ras el Ahmar	16 58	54 42	Garú I.	29 4	48 31
	C. Merbat, l, rky., f, w,	17 3	55 2	Kūbbr I.	29 20	48 8
	Jebel Kinkeri, 1800f.	17 14	55 18	Ras al Arth	29 23	48 0
	Ras Nūs, 20 l., S pt., l.	17 27.2	55 35.7	Kuweit, N end town, 11,	29 23	48 21
	Kuria Muria Is., EW 45m., }	17 29.6	55 51.2	Feylecheh I., ¾ 7m.	30 32	47 51.5
	Wone, Haski, ¾ 1½m., pk. f }	17 32.7	56 2.2	Basrah Custom Hou-e	30 8	49 6
	— Soda, ¾ 3m., pk., 1310f., }	17 29.2	56 19	Ras Tanūb, l.	29 58	50 10
Gulf of Oman	— Helānes, EW 7m., NE }	17 53	56 20			
	bluff, 1645f., w,	18 58.5	57 46.0			
	— Kibliyāh, EW 2m., pk., }	20 7.6	58 33			
	550f., w, ½ W 3m.	20 43.5	58 52			
	Ras Sherbedāt, l, w 4m., W...	21 27.5	59 21.5			
	C. Isolette, vis. 16 l., pt.	22 14.4	59 49			
	Mazeira I., ¾ 13 l., 600f., }	22 33	59 48			
	S pt.					
	— N pt., or Ras Jel					
	Ras Jibah					
PERSIAN GULF.						
Gulf of Oman	Ras Abu Daud	23 19.2	58 55.5	Khargú I., NS 4m., l, w, N pt.	29 20	50 22
	Maskat, r, w, f, Fisher's rk. 11	23 37.7	58 36.0	Kharg I., ¾ 5m., w', fort. NE 11	29 15.4	50 20.7
	— Saddlehill, 1340f.	23 35.1	58 35	Abu-Shahr, 11, w, r. Resi- } dency	20 59.1	50 50
	Jeziret Jun, 107f.	22 50.5	57 58.5	Asses' Fars, 5m. inland, 2500f.	28 29	51 12
	Clive Shoal, sf.	22 51	57 57.2	Hummocks of Dreng, S one. }	28 4	51 37
	Jebel Kostasg, a bluff of the }	23 14.2	56 16	3270f.		
	Jebel Akhtar			Ras Mutaf, S pt.	27 41	51 45
	Birkeh	23 42.7	57 54.2	Konguin	27 49.5	52 4
	Suwik, fort and town	23 51.5	57 26	Barn Hill, 4660f.	28 48	52 14
	Sohar, town and fort	24 21.5	56 46	Ras Nabend, l.	27 23	52 35
Persian Gulf, N. Coast				Sheykh Shāyāh, 120f., l, ¾ }	26 48	53 24
				14m., w, P, E pt.		
				Hinderabi I., EW 4m., l, 100f.	26 41	53 40
				Sumberrun Shl., [6]	26 33	53 44
				Gays, 120f., ¾ 8m., l, ¾, 7, }	26 31	54 3.5
				r, w, P, E pt.		
				Frúr I., 465f., NS 4m., N pt.	26 19	54 30.5
				Ras Bostaneh, l, pt.	26 30	54 37
				Frúr Shl. [½m.], 4	26 26	54 32.5
				Nabyú Frúr I., [1m.], 120f.	26 7	54 26.5
Persian Gulf, S. Coast				Seri I., 50f. [3m.], S pt.	25 53	54 33
				Bumusa I. [3m.], 360f., peak	25 53	55 3

571

(55)	Places	Lat. N	Lon. E	(56)	Places	Lat.	Lon. E
<i>Pernau Gulf, N. Coast</i>	Jest. Nabu Tumb [1m.]	26° 14' 7"	55° 9'	<i>Maldive Is.</i>	North		
	Jest. Tumb [3m.], 165f., w...	26 15 7	55 18 7		Maldiva Is., 19 Atolls, or groups, l, t, ll, f, p' }		
	Baidûh Chapel.	26 39 2	55 16 2		N extr., Heawandoo Pholo Atoll, # 4 l., ☐, w', N pt., Turacoon I. }	7° 6'	72° 53'
	Henjar I., # 5m., S pt.....	26 36	55 52		Heawandoo I., [1m.], f, on SW side, w, }	6 57·5	72 54
	Kesm, fort	26 57·5	56 17		Tilla, and Milla, don Atolla, E extr. }	5 51	73 27
	Larek I., # 5½m., # ½m., N pt. l.	26 53·1	56 21·7		— N Id., Keelah, [2m.], f ... }	6 59	73 12
	Hormuz I., EW 4m., fort, N pt.	27 5·8	56 27·5		— S extr. }	5 39	73 15
	Bander Abbas, Sheikh's hous: ☐, f }	27 10·5	56 17		Malcolm Atoll, # 5 l., rf. Mah-koondoo I., [1m.], w' at NE extr. }	6 24·5	72 40
	Kûhî Mubârak, rk.....	25 42·2	57 28		Powell's Is., 2, # 2m., N one Paddipholo Atoll, # 7 l., E pt. }	5 59	72 54
	C. Jashak, l, sandy pt., Tomb R us Tagin, l }	25 38·3	57 45·7		Cardova I., # 1½m., f, w' ... Horsburgh Atoll, # 10m., entr. S, f, E extr. Id., w }	4 58	73 26
	Ras Maidani l, (shl. 3m.)	25 23·7	59 6·5		A lagoon rf., EW 6m., N pt... Malé Atoll, NS 33m., E extr. — King's I., fl str, N side.... South Malé Atoll, # 7 l., S extr. }	4 27	73 42
	Ras Gurdim, l., (rk., SE 3m.) ..	25 19	60 7·2		To-doo I., [1m.], w'	4 10	73 29
	Ras Mutakkaddim	25 16·5	60 27·7		Ari Atoll, NS 16 l., f, N, l. at S pt. w'	3 48	73 25
	Chahbar, f, t, w', Telegraph ..	25 16·7	60 37·2		Pha-lee-doo Atoll, EW 10 l., E extr. }	4 26	72 58
	Ras Fasta	25 3	61 25·2		Molouque Atoll, # 8 l., S extr. — Do. Id., on N side entr. ☐, w, b, f	3 30	72 50
	Gwatar, vill.	25 8·9	61 30·2		Nilandoo Atolls, 2, ll, NS 13 l., ld. at S entr., f, w', on W side entr. ☐	3 27	73 44
	Ras Jiynni	25 0·5	61 42·2		Collomandoo Atoll, EW 10 l., Karn-doo-doo I., w', ☐, Adou Matte Atoll, # 9 l., N and E pt. Id. }	2 45·5	73 23
	Guadar Telegraph	25 7·3	62 19·2		— S extr., Id., (entr. ☐, f 3m., # 0)	2 57	73 33
	Ras Shahid	25 12	62 58·7	<i>Maldive Is.</i>	Suadiva Atoll, NS 15 l., W side, entr. to ☐, 10	2 40	72 54
<i>Mukran Coast</i>	Pasni Telegraph	25 15·9	63 28		Phoowa Moloku I., w', N pt. S extr., Addoo Atoll, EW 3 l., w, b, t, Gung I., ☐, E pt. }	2 20	72 55
	Astaluh I., EW 3m., (rk.), 2n. S)	25 6·2	63 49		Almirante & Seychelles.	2 7	73 35
	Ornarar, Telegraph	25 11·9	64 36·5		W extr., L Boudouse, small, f, Marie Louise I., small, f, (rf. off, z)	1 46·5	73 22
	Ras Malan	25 18	65 12·2		I. Etolle, [1½m.], l, ✱	0 28	72 56
	Sunmiyani, f, w, Jam's ho. ...	25 25·5	66 35		S extr., I. De Neuf, small, ✱ Poivre Is., two, [1m.], rfs, NE pt. }	South	
	Ras Muwari, or C. Monze, shl. 3m. }	24 50	66 39·5		Isle de Roches, (bks. 4 l.), North beach	0 16·5	73 23
					St Joseph Is., E pt.	0 41·5	73 6
					D'Arros I., NE pt.		
<i>Laccative Is.</i>	INDIAN OCEAN. Islands.						
	Laccativas, l, f, f.						
	Bassas de Pedro bk., # 22l., T, N pt., # }	13 37	72 32				
	— ff., NS 6m., T, S dry sand (Cherbaniani)	12 16	71 52				
	Byramgore, ff., NS 13m., S part Betra-par, rf., NS 7m., Id., [1m.], N extr., l. }	11 48	71 50				
	Peremul-par, rf., # 7m., T, Id. NE	11 35	72 11				
	Ancutta, [3½m.], P, f, mid....	11 9	72 0				
	Tingaro	10 51	72 10				
	Pittie, [2c.], sand						

Laccadive Is.

MARITIME POSITIONS

MARITIME POSITIONS							
(57) Places		Lat. S	Lon. E	(58) Places		Lat. S	Lon. E
Almirante Is.	Eagle, or Remire I., [$\frac{1}{2}$ m.], l, *, rfs. 2m., w., NE pt. }	5° 6'4	53° 19'	Great Chagos bk., N extr., s. .	5° 39'	72° 1'	
	African Is., small, l, * W. }	4 52'5	53 23'7	— NW extr., Eagle Is., $\frac{1}{2}$ m., 5m., l, *, N pt. }	6 10'5	71 18	
	w., North I. }	4 52'5	53 23'7	— W entr., Danger L. [$\frac{1}{2}$ m.]	6 23	71 13	
	I. Platte, [$\frac{1}{2}$ m.], rfs. 3m.	5 52	55 22	Egmont, or Six Is., $\frac{1}{2}$ 6m., T, SE Id., * }	6 40	71 22	
	La Perle rft., Centre }	6 1	55 17'5	Pitt's bk., $\frac{1}{2}$ 10 L, T, } N pt., 15 }	6 49	71 10	
	Mahé I., $\frac{1}{2}$ 13 l., *, Port }	4 37'2	55 27'5	— West extr., 15 }	7 2	71 4	
	Victoria, Hodoul Jetty ... }	4 37	55 31	A Reef, NS 2 l. }	7 11	72 36	
	— lt. F 37f. on S reef }	4 37	55 31	Ganges' bk., $\frac{1}{2}$ 4m., W extr., }	7 22	71 2	
	Silhouette I., [3m.], l, *, }	4 27'0	55 16'7	Diego Garcia NS 13m., l. SE, *, F, *, Mid I., E entr.... }	7 13'5	72 23'7	
	N pt. }	4 27'0	55 16'7	— South pt. }	7 26'0	72 23'2	
Seychelle Archipelago	Recif I., [$\frac{1}{2}$ m.], 150f., ~, mid.	4 34'8	55 50	Islands in Southern Indian Ocean.			
	E extr., Frigate I., [$\frac{1}{2}$ m.], }	4 35'2	56 1'2	MAURITIUS, PORT LOUIS. }			
	550f., P. rft. SW, mid. }	4 17'4	55 44'2	Martello Twr., Ft. George }	20 8'6	57 29'0	
	Pra-lin I., 12 l., * N, W pt....	4 16	55 47'7	— Round I., [1m.], 1049f. ...	19 50'5	57 47'5	
	Curieuse I., EW 2m., w, *, mid.	3 48'2	55 40	— Peter Botte, 2600f. }	20 11'3	57 33'5	
	Denis I., NS 3m., l, *, lt. F }	3 42'7	55 12'5	— Grand Port, Fouquet Id., }	20 23'5	57 46'7	
	60f. }	3 42'7	55 12'5	lt. F 108f. }			
	N extr., Bird I., [2m.], l, *, }	3 42'7	55 12'5	Bourbon I., $\frac{1}{2}$ 141 St. Denis, }	20 51'5	55 27'5	
	~, *, mid. }	3 42'7	55 12'5	2 lts., F, vert., 85f. }	20 53'2	55 36'5	
	French Shoal, [5 or 6m.], }	3 58	54 42	— Pt. of Bel Air, lt., F 148f.	21 22'5	55 39	
Chagos Archipelago.	s, mid. }	6 24	60 4	Rodrigue, EW 15m., v.s. 141., }	19 40'4	63 26'2	
	Roquepis, l, sandy, rfs. }	7 0'5	52 45'2	rfs., 5 l. to SW-d., Point Venus }			
	Alphonse, l, *, SE pt. }	7 6	56 17	Keeling Is., *, l, N Id., [$\frac{1}{2}$ m.]	11 50	96 51	
	Coetivy I., l, sandy, $\frac{1}{2}$ 8m., }	10 21'5	56 32	— S grp., Borneo Coral Is., }	12 12'6	96 54	
	*, * NW, w, *, F, N pt.... }	9 12	60 21	SE, NS 8m., S pt. }	12 5'4	96 33'0	
	Agalegas, I. and reefs, $\frac{1}{2}$ }	10 7	51 10'2	— Direction I., [$\frac{1}{2}$ m.], SW pt	10 25'3	105 43	
	6 l., *, NW pt. }	9 55	50 15	Christmas I., EW 3 l., vis. 12 l., *, l NW, Flying- fish cove }			
	Sava de Malha bk. 5 fms. w. c.	9 19	50 43'5	Enderby's land, pt. uncertain...	67 30	44 0	
	John de Nova, or Farquhar Is., $\frac{1}{2}$ 8 l., w, *, Grande Porte }	9 14	51 2'5	Bouvet's I. }	54 20	5 24	
	McLeod, or Marq. of Huntly bk., [2 l.], 15 }	9 39'5	51 18	Thompson's I. }	53 56	5 30	
Chagos Group	St. Pierre, [$\frac{1}{2}$ m.], l, *, NW pt.	15 51'6	54 27'7	Prince Edward's I., 2 [5 l.], }	46 34	37 56	
	Providence I., [2m.], w, F, l, }	16 48'9	59 31'5	and [3 l.], l, *, West I. }	46 52	37 53'5	
	Village }	16 26'5	59 37'5	Crozet's Is., Hog I., l, l, }	46 10	50 28	
	Umsinto bk. coral 11 fms. ... }	16 15'0	59 36'5	*, (a rft. SE 9 m.) }			
	Tromelin, [1m.], l, or Sable I., 8, N pt. }	5 15	71 42'7	Kerguelen's land, $\frac{1}{2}$ 32 l., }	48 40	69 4	
	Cargados Carajos reefs, $\frac{1}{2}$ }	5 27	71 46	Christmas Harb., SE, b S }	48 27	68 48'5	
	9 l., l, T E, F, S extr., }	5 15	71 37	side, N pt., or C. François...	49 15'5	68 38	
	Coco I., * }	5 33	72 13	— Bligh's Cap., l, *, 230f....	49 43'5	70 5	
	— Baleine shl., rft., [$\frac{1}{2}$ m.]....	6 5	72 43	— C. St. Louis }	49 11	70 33'5	
	— Establishment }	5 40	72 16	— C. Challenger }	53 1'5	72 31	
Chagos Group	Albatross I., [$\frac{1}{2}$ m.], o }			— E extr., C. Sandwich }			
	Speakers' bk., $\frac{1}{2}$ 8 l., T, l, }			Heard or McDonald Is., $\frac{1}{2}$ }			
	NE pt. }			50m. Meyer rk., NW extr. }			
	Blenheim rft., $\frac{1}{2}$ 6m., T, N pt.			St. Paul's, $\frac{1}{2}$ 3m., 860f., * }			
	Salomon Is., $\frac{1}{2}$ 53m., SE, N }			E, r, Ninepin rk. on E side, (w' $\frac{1}{2}$ m.) }	38 42'7	77 34'7	
	Id., E of entr., or l. de Passe }			Ams'erdam [4m.], w, sum. }	37 50'7	77 31'5	
	— SW, or Boddam I. }						
	Peros Banhos, 27 Is., $\frac{1}{2}$ 6 l., }						
	l, SE, I. de Passe, E side, entr., mid. }						
	— Diamond I., [$\frac{1}{2}$ m.], establ.						
— S extr., Foquet I., l, * ... }							

573

Hindustan, W. Coast ⊕

Mulubar Const. Co.

Ceylon

Coromandel Coast

TABLE 10

578

MARITIME POSITIONS

(63) Places		Lat. N	Lon. E	(64) Places		Lat.	Lon. E.
Nicobar Isles	Little Andaman, NS 7 l., } $\frac{1}{2}$ S bay, (P, w N pt.)... } S. Sentinel, [1m.], 6 l., $\frac{1}{2}$ } Flat Rock, [30 yds.], 8f. (on } Invisible Bk.)..... } Volcano or Barren I., 1158f... } Narcondam, T, 2330f. }	10° 33'5	92° 28'5	S. W. Coast of Sumatra	Pulo Wal $\frac{3}{4}$ l., vis. 12 l., } T S, S pt. } Buru I., or Malora lt. F 62f. } Po. Nancy, (bay S, w, b, $\frac{1}{2}$), } N pt. } Pulo Brass, A. N. lt. Rev. 525f. } Golden or Queen's Moun- } tain, 8280f. } Achen Hd., or King's Pt., h, l } Rajah Passage } Rigas Bay } Bubu Bay } Analabu, w, r, b } C. Felix, l, T } Susu, Po. Kio } Goonung Loo e, 12,140f. }	North 5° 46'5	95° 21'
	Kar Nicobar I., Sawi B. }	9 14'2	92 45'7		Tampat Tuan lt. }	3 15	97 10
	Batti Malv, or Quoin, } [1½m.], $\frac{1}{2}$, w, 150f. }	8 49'7	92 51		Teunon Road..... }	2 46	97 37
	Chaura, [1½m.], $\frac{1}{2}$, 343f. }	8 27	93 2'2		Sinkel. pt. } Cocos Is., 2, l, $\frac{1}{2}$ }	2 16'8	97 44'7
	Teresa, $\frac{3}{4}$ l., $\frac{1}{2}$, 897f, } 8 pt. }	8 12	93 11		Pulo Simalla, $\frac{3}{4}$ l., N pt. } — South pt. }	3 0	95 18
	Tilangchong, EW 4 l., $\frac{1}{2}$, } Maharani Pk., 1058f. }	8 29'7	93 37		Flat Is., 2, (small), S pt. } Banjak Is., Middle Is., Po } Sorong Alu..... }	2 57	95 47
	Kamorta I., 238f., Naukauri } Hr., Naval Pt. }	8 2	93 32		Pulo Lakotta, l, $\frac{1}{2}$ }	2 19	96 22
	Kachal I., 835f. pk. }	7 57	93 23		Pulo Babi }	2 3	96 35
	Meroc, small, l }	7 30'7	93 31'7		Pulo Nias, $\frac{3}{4}$ l., 22 l., W pt., } Tanjung Letang }	1 58	97 21
	Little Nicobar, $\frac{3}{4}$ l., $\frac{1}{2}$, } Mt. Deoban, 1428f. }	7 20	93 40'7		Nako Is., Asu..... }	1 51'5	97 59
	Grt. Nicobar, 2105f., Kon- } dul I., 400f. }	7 13	93 42		Tapanuli B., l., Siboga ... }	1 41	97 27'2
	— Pygmalion Pt. }	6 45	93 49'5		Pulo Dua..... }	1 24	97 1
					Tanjung Road }	0 33	97 50
					Natal B., 33, Natal }	0 54	97 11
STRAIT OF MALACCA.					Ayer Bangies, Po. Parka... }	0 51	98 45'7
Strait of Malacca.	Pulo Pera, vis. 7 l., $\frac{1}{2}$, T ... }	5 42	98 56'7		Po. Pinie, Batu Belobang, } $\frac{3}{4}$ l. }	0 33'5	98 9
	Penang I., NS 4 l., sum. 2713f. }	5 25	100 14		Mt. Ophir, 9472 f. }	0 8	98 55'5
	— George Town, [2], [2], } fort Cornwallis, lt. Rev. } 107f. }	5 24'5	100 20'2		Tanah Massa I., N pt. }	0 39	98 32
	Saddle L., [½m.]..... }	5 13	100 10		Po. Bojo, lt. Fl. 361f. }	0 55	98 55
	Pulo Dinding, $\frac{3}{4}$ l., h, $\frac{1}{2}$, } w E, Port Pancore, lt. F. }	4 13'3	100 34'2		— West I. }	1 55	99 12
	Salangor fort, lt. F. }	3 20	101 12		Sipora I., Hurlock Bay }	2 2	99 33
	Sumbelan, or 9 Is., $\frac{3}{4}$ 7m., } vis. 7 l., $\frac{1}{2}$, white rk. }	4 2	100 30		— S pt., C. Marlborough ... }	2 24	99 49
	Jara I., [½m.], T, $\frac{1}{2}$ }	4 0	100 9		N. Pagi I., N pt. }	2 32	100 0
	Parcelar hill }	2 52	101 25		— SW pt., or Pt. Batu }	2 49	99 57
	Round, or S. Arroa, h, $\frac{1}{2}$, } (rks. off)..... }	2 49	100 35		S. Pagi I., 8 pt. Sibaru I. }	3 20	100 25
	C. Rachado, l, $\frac{1}{2}$, lt. F 446f. }	2 24	101 51		Trieste I., Po. Mega, } [1½m.], l, $\frac{1}{2}$ }	4 0	101 1
	Malacca, St. Paul hill, lt. } F 180f. }	2 12	102 15		Engano I., $\frac{3}{4}$ l., P, W } pt., Komang }	5 21	102 5
	Water Is., h, $\frac{1}{2}$, large or S, w }	2 4	102 19		— South pt., Kenemci }	5 31	102 9'5
	Mt. Moar, h, $\frac{1}{2}$ }	1 59	102 40		Priaman, fl. st. }	0 38	100 6
	Mt. Formosa, (bk. WSW 2 l.) }	1 49	102 54		Palang I., lt. Rev. 180f. ... }	0 57	100 7
	Po. Pisang, $\frac{1}{2}$, lt. Fl. 325f. ... }	1 27	103 15		Pulo Baringin }	1 55'5	100 39
	SINGAPORE, [2], FULLERTON } BATTERY..... }	1 17'2	103 51'2		Indrapura Pt., l, $\frac{1}{2}$ }	2 10	100 50
	Pt. Romania, (Is., 3m. out) ... }	1 22	104 16		Moko Moko }	2 34	101 8
	Barbukit hill, 645f. }	1 24	104 11		Benculen, lt. F }	3 47	102 16
	Pedra Branca, T, NW, 3 } S. Horsburgh, lt. Fl. 101f. }	1 20	104 24'6		— Po. Tikus, lt. F 44f }	3 50	102 11
	Bintang hill, 1260f. }	1 5	104 26		Mana Pt. }	4 31	102 54'5
	— Black rk. }	1 14'5	104 34		Kawur or Sambat }	4 50	103 24
WEST COAST SUMATRA.				Sumatra	Pulo Pisang, [1½m.], lt. }	5 7	103 49'5
Po. Rondo, (Tepurong), 426f. }		6 3'5	95 7'7				

MARITIME POSITIONS

(65)	Places	Lat. S	Lon. E	(66)	Places	Lat.	Lon. E
	Kroe Road, w. r.	5°11'	103°56'		Shoal-water I., lt. F 200f.	South 3°19'2"	107°13'2"
	Bangkunat B., rky. S pt. ...	5 35	104 14		Vansittart shls., NS 3 l., } S pt. }	3 10	107 6
	Little Fortune I., [1m.], l. }	5 57	104 24		Saddle I., Klamhau, 266f.	3 2	107 11
	X }				Table I., Goesik, 116f.	2 59	107 17
STRAIT OF SUNDA							
Straits of Sunda	Flat Pt., lt. Fl. 213f.	5 55	104 33.5	Straits of Geyser	Pulo Leat, 2 1/2 6m., Alceste } (wrecked there), lt. F 39f. }	2 49	107 1.2
	Lambuan I., 2 1/2 7m., W end ...	5 47.5	104 47		Long I., EW 10m., W pt.	2 52	107 21
	Keyser's Pk., 7412f.	5 26	104 40		Billiton, Po. Selio, to SW } [4m.], S pt. 242f. }	3 15.5	107 32
	Kalambayang Harb., [w. r.], }	5 46.2	105 2.2		— S point, Kalumpang, (stil.) } 1m. out) }	3 16.4	107 59.5
	Klapa I. }				— Shoals on E side E. } Protet }	3 3	108 31
	Pulo Lagundi, [w.], mid. N }	5 50	105 17.2		— Burung Mandi Pt.	2 45.3	108 16.7
	side }				— North-west I., Longwas, } lt. I 200f. }	2 32.3	107 38
	Telok Betung, lt. F 48f.	5 28	105 15.7		Carabee shl., rks.	3 34.2	107 41
	Rajah Basa, w. r. pk., 4233f.	5 47.5	105 39		Canning's rk., [1c.], 2, T, 8 ...	2 23	107 15.5
	Hog Pt.	5 55	105 43		Gaspar I., [1 1/2 m.], 812f.	2 25	107 5
	Java Head	6 47	105 11	Tree I., [1m.], 40f., 2 or 3 1/2 }	2 28	106 59	
	Mew B., w. r., SE of Mew }	6 45	105 15	Warren Hastings rf.	2 22	106 56.5	
	I., P, }			B. lidere rk., 10f.	2 12	107 2.5	
	Prince's I., 2 1/2 4 l., N and }	6 31	105 15	Stard rf., 2, 8 ...	2 12	106 46	
	E pt., 1450f. }			Magdalen shl., [1c.], 2, T, cri.	2 2	107 0.5	
	Krakatoa, [k.], 2657f.	6 9	105 27	Newland shl., 2, 8, T /	1 52	107 1.5	
	Sea rks., Gap rk.	5 59	105 23	Palmer shl.	1 58	106 24	
	Sebooko, 2 1/2 3m., 1398f., N pt.	5 51.5	105 32	Seyern shl., [3m.], 10f.	1 37.6	106 31.5	
	Thwart the Way, or Sangian }			Deva rfs.	1 10.2	106 46.2	
	I., 2 1/2 2 1/2 m., l. (rks. 2m. }	5 58	105 49.7	Vega shl., [1c.], sf., T 8 ...	1 7.5	106 37.5	
NW), pk. 503f. }							
Banda Strait	Anjer, w. r., (lt. SW-d), fl. st	6 3.2	105 55	Carinata Strait	Shoe I., Kebatu, 346f.	3 47.7	108 4
	St. Nicolas Pt.	5 52.5	106 2		Discovery, West bk., [1m.], ld.	3 39	108 45.5
	North Id., small, vis. 7 l.	5 42	105 50		— East bk., [1 1/2 m.], ld., 2 1/2 }	3 35	109 11
	Thousand Is., Northern- }	5 24.5	106 28		Osterley shls., [6 l.], N one ...	3 17.7	108 38.2
	most Dua I. }				Cirencester bk., [1/2 m.], ...	3 16.2	108 59.2
	— Peblakan, or W. Id.	5 28.5	106 23		Montaran Is., EW 12 l., NE }	2 30.7	108 55.2
	Arnemuiden rk., [1/2 m.], 10f.	5 13	106 44.2		extr. or Catherina rf. }		
	North Watcher, small, X, }	5 12.5	106 27		W. grp., Nangka I., pk. 549f. ...	2 30	108 33
	(Omega shl., E' b S' 1/2 m., }				Ontario rf., [1/2 m.], T, 8 (a)	1 59.5	108 39.5
	8 T), lt. R. 159f. }				coral rf. W 3m., s)		
Banda Strait	Two Brothers, X, 1/2 10, N one...	5 9.5	106 6	Is. N.W. of Banda	Serutu, EW 2 l., 1575f., w. }	1 43	108 41.2
	Lynn shl., [1c.], d, T	5 12	106 12		W end. }		
	Brouwers shla., 2 rfs., [1/2 m.]...	5 4.7	106 16		Carinata, [3 1/2 l.], w, b, l. k. }	1 36	108 54.5
	Shalibunder shl., E lim.	5 7	105 59		3378f. }		
	STRAIT OF SUNDA TO SINGAPORE				Penebaungan, 2 1/2 l., 2, w', }	1 24	109 15
	Tree I., N pt.	3 46	105 54		pk. 1722f. }		
	Lucipara I., [1m.], X, w', }	3 13	106 13		Greig Shoals, N. Greig.	0 52.5	108 32.5
	(rf. SSE, 2m.) }				Greig shls., Gwalia	1 5.7	108 34.5
	First Point, l, level, X	3 0	106 3		Pulo Toty	0 54.5	105 46
	Blanca, S extr., Dapur I. 120f.	3 8	106 31		Pulo Duncan	0 58	105 39
— Parnesang hill, 1608f.	2 35	105 56	Po. Tudju, or Seven Is., 2 1/2 }	1 8	105 14		
— Nangka Is., 3, great one, }	2 23	105 45.5	8m., X, NW one }				
w, b, N pt. 285f. }			Pulo Varella, (Is. [3m.]), 450f.	0 48	104 24		
— Monopin Hill, 1456f.	2 1	105 11	Pulo Taya, [3m.], 630f.	0 43.6	104 54.2		
— Kalian Pt., lt. F 170f.	2 5	105 8	Po. Sinkop, 8 pt. C. Bulu.	0 38	104 22		
— Frederic Hendric rks.	1 58	104 58	Alang Kalem, [2m.], 1	0 24	104 57		
— North or Mengkudu Pt., islet	1 29.3	105 53.5	Linga I., 1/2 sum. 3921f.	0 11	104 32.5		
— Goonung, or Mt. Marass, }	1 52	105 52	East Domino, [1m.]	0 6	104 58		
E sum., 2300f. }							
— E extr., Berikat Pt., 660f.	2 34	106 51	Pollox rk., 2	0 12.5	104 44.5		
— Entrance Pt., (SE extr. of }	3 2	106 54	Terobi, 112f.	0 42.4	104 47		
Lepa), Murong }			Frederick rk., [3c.], 2, 8, 8, ...	0 38.5	105 10.7		
Fairlie rk., [1c.], sf., T	3 27	107 1	Pulo Panjang, EW 4m., }	1 1	104 51.2		
Sand I., [1 l.], 8 all round ...	3 30	107 10	390f., E pt. }				

TABLE 10

577

MARITIME POSITIONS

(67) Places		Lat.	Lon. E	(68) Places		Lat. N	Lon. E
Sumatra, N.E. Coast	Batacarang Pt.	South 2° 0'	104° 51'	Natunas	Great Natuna, NS 40m., N pt.	4° 16'	108° 11'
	Jabong Pt.	0 56	104 23		—Mt. Ranay, on E side, 1890f.	4 1	108 19
	C. Baroe	0 1	103 48.5		Miculle rf.	4 4	108 25
	Rhio Str., Garras I., W side } entr., lt. F 121f. }	North 0 46	104 21		Selouan I., [1 l.], S sum.	4 8	107 49
	— Pulo San, lt. F 108f.	1 4	104 10		Low pyramidal rks., 25f.	4 3	107 21
	Gt. Carimon, S pk., 1474f. ...	1 5	103 19		Success breakers, [2m.]	4 23	107 53
	Little Carimon, $\frac{3}{4}$ 3m., $\frac{3}{4}$, } T NE, N pk., 1063f. }	1 8	103 22		Semione, or Saddle I.	4 31	107 42
	Bucalise I., NE pt.	1 34	102 23		N. Natunas, $\frac{3}{4}$, N islet	4 51	108 2
	Pulo Roopat, N pt., T	2 6	101 39		Blair Harbour, \square	2 38	103 47
	Reccan R., Lalang Besar I. ...	2 10	100 34		Pulo Varela, rk., $\frac{3}{4}$, rf. 2m.	3 19	103 38
	N. and S. Brothers, $\frac{3}{4}$ 5m., } $\frac{3}{4}$, N one }	3 24	98 46		Howard shl., T	4 17	103 38
	Buttoo Barra R.	3 13	99 34		Pulo Brala, 10 l., rks., N 5 l.	4 49	103 39
	Pulo Varella, S l., $\frac{3}{4}$, b, P. ...	3 47	99 30		Pulo Capas	5 13	103 14
	Delhi R.	3 46	98 41		Tringano R., w. r., bar	5 21	103 6
	Prauhlah Pt. (rf. 3m.)	4 53	97 52		Great Redang I., pk.	5 50	103 1
	Diamond Pt., l. $\frac{3}{4}$	5 16	97 30		Pulo Lantinga	5 50	102 52
	Pedir Pt., or Batoo Pedir ...	5 29.5	95 55.2		Printiaa Is., outer one	5 55	102 44
	Pt. Pedro	5 39	95 27.2		Pulo Loxin, small, 7f.	7 21	102 0
					Kalantan R., bar, w'	6 12	102 19
					E. Patani Pt.	6 58	101 17
Entrance of China Sea				Gulf of Siam	Koh Krah, grp., large one ...	8 25	100 44
	CHINA SEA.				Carnon Pt.	8 56	99 49
	Pulo Tingy, $\frac{3}{4}$ w, w, sum. 2046f.	2 18	104 8.5		S. mini I., [2 l. ?], 2000f. sum.	9 33	100 1
	Pulo Aor, $\frac{3}{4}$ 2 $\frac{1}{2}$ m., 1805f. ...	2 28	104 31		How Lung, Mt., 7m. in- land, 4326f. }	11 38	99 33
	Pulo Pemangil, 1507f.	2 36	104 19		Koh Tarkut (Po. Chin ?) } (peaks, 1815f., $\frac{3}{4}$ 5m.) ... }	12 12	99 59
	Pulo Tio-nan NS 10m., 3444f., } N pt., $\frac{3}{4}$ b, w, P, }	2 55	104 10		Bangkok R., lt. F 44f.	13 29	100 35
	St. Barbe, [3m.], $\frac{3}{4}$, w, 752f.	0 8.1	107 13.5		Bangkok, Brit. Factory	13 44.6	100 28.2
	Direction I., sum. 639f.	0 14.3	108 2		Siam, now Ayuthia, mid.	14 22	100 36
	Pulo Dattoo, h, SE pt.	0 8.2	108 36.2		Koh-si-chang I., NS 4m., } w', N pt. }	13 11	100 47
	Gre-n Id., centre	0 44.7	107 19		Koh Leum I., [3m.], 445f.	12 57.5	100 38
	St. Esprit Is., $\frac{3}{4}$ 4 l., 817f.	0 37.5	107 1		C. Liant	12 35	100 57
	Wellstead rk., s	0 32.4	107 53		Chalan I., [1c.], 40f., T, $\frac{3}{4}$...	12 28	100 57
	Ellen shl., rks., [3c.], sf.	0 41.2	107 31.2		Cawsbuff Mt.	12 31	103 4
	St. Julian, summit 537f.	0 55.7	106 43.5		Junk Rock Pt.	12 8	102 47
	Tambelan Is., $\frac{3}{4}$ 6 l., f., } Great, summit 1300f. }	1 10	107 32.2		Kurovie rk.	11 7	102 45
	— Gap rk.	1 12.5	107 34.5		Samit Pt.	10 52	103 7
	Europe shl., R., [1m.], s	1 11.3	107 25.5		Bumba town	10 35	104 10
	Camel I., summit 574f.	1 11.7	106 53		Teeksia R., mouth	10 6	104 54
	Saddle I., summit 307f.	1 19.3	107 2.2		Cambodia Pt.	8 35	104 42
	Barren I., summit 80f.	1 31.7	106 25.5		Po. Way, 2 ls., $\frac{3}{4}$ 1m., 250f. ...	9 55	102 52
Natunas	Victory I., summit 285f., 8 l. $\frac{3}{4}$	1 34.7	106 18.5	Cochin China	Pu'o Panjang Is., EW 3m., } 550f., w, b, f., great one ... }	9 18	103 27
	Acasta rk., sf., T	1 39	106 19		Pulo Oby, $\frac{3}{4}$ 2 $\frac{1}{2}$ m., w, 1046f. ...	8 25	104 48
	White rk., h 110f.	2 18	105 35		Saigon, City	10 46.7	106 42
	Repon, 695f.	2 21.6	105 53		C. St. JAMES, 3 3m., lt F 482f.	10 19.8	107 5
	Pulo Domar, 270f., $\frac{3}{4}$ T	2 44.5	105 23		Britto shl., [1 $\frac{1}{2}$ m.], 4, T	10 29	107 49.5
	Djimaja, $\frac{3}{4}$ 5 l., S pt.	2 48	105 43		Pt. Kega, $\frac{3}{4}$, (Mt. Taicou, } h $\frac{3}{4}$) }	10 42	108 0
	Tokong Belauer, Pillar rk. ...	3 27	106 16		Ceicer de Terra, l, $\frac{3}{4}$, 3 3m.	11 14	108 48
	Pulo Selei, 480f.	3 12	106 30		C. Padaran, h, 1, T, lt. Pl. ...	11 23	109 1
					False C. Varela, (Camranh } Harb., \square), h }	11 44	109 13
	St. Pierre Is., 2	8 51.7	108 39		Pyramid I., h	12 17	109 20
	S. Haycock I.	2 17	108 54		Nhutrang B., \square , w, b, riv., } bar, rf., Tree I., pk. 1640f. }	12 13	109 16
	Sirihassan Id., Koi Hd., 765f.	2 33	108 59.5		Three Kings, rks., T, Hone- Coke harb., \square , w, 15f. ... }	12 34	109 27
	Kepalou	2 39.5	109 10		C. Varela, or Pagoda C., h, } T, pt. }	12 55	109 26
	West I., 865f., N end	2 43.5	108 35		Perforated rk., rks.	12 58	109 25.5
	Soubi I., N end, 200f.	3 3	108 51		Conical Mountn., 1870f.	13 11	109 10
	Jackson rfs., E extr.	2 56	107 56		Phuyen Harb., \square , Nest I. ...	13 23	109 15
	Low I., [1 l.], N end	3 1	107 48				
	N. Haycock I., h, rf., S-d ...	3 16	107 34				
	Elphinstone rk., [1m.], 70f. ...	3 23	107 51				
	S extr., Sededap I., h.	3 33	108 3				

TABLE 10

MARITIME POSITIONS

(69)	Places	Lat. N	Lon. E	(70)	Places	Lat. N	Lon. E
Cochin	Commons Harb., \square , Gainta Hd.	13° 31'	109° 16'	Islands in the China Sea	Pennsylvania	9° 59'	115° 11'
	Pulo Camldr, $\frac{1}{4}$ 3m., 6 l.	13 37	109 19		— Another do.	9 5	115 17
	Quinhone Harb., \square , C. San- ho, A, 1	13 45	109 16		Half Moon shl., $\frac{1}{4}$ 3m., } 8 pt.	8 52	116 15.5
	Charlotte Bk., [3m.], $\frac{1}{4}$ T ...	7 7.3	107 37		Royal Captain shl., $\frac{1}{4}$ 3m., } NE Investigator	9 1	116 39
	Browers, $\frac{1}{4}$ 3m., E onc. A, $\frac{1}{4}$...	8 37	106 9		Pennsylvania	9 12	116 30
	Pulo Condore Is., [31.], \square , } w. r., 1954f., lt. F 696f.	8 40	106 41		Bombay shl., $\frac{1}{4}$ W pt., T ...	9 26	116 56
	Royal Bishop, $\frac{1}{4}$ 32m., \square	9 40	108 14		Sabina shl.	9 42	116 38
	Id. Catwick, summit 56f.	9 59.5	107 4		Pennsylvania, shls., [4 L.], } mid.	9 49	116 47
	Great Catwick, $\frac{1}{4}$ 3m., 196f.	10 29	108 55		Islands and Shoals N.W. of Borneo	Pennsylvania	10 0
	Yasun shl., $\frac{1}{4}$ 3m., 196f.	10 16	109 2.2	Ganges		10 18	115 5
Pulo Sapatu, $\frac{1}{4}$ 3m., 346f.	9 58.4	109 6	Loai-ta I. and rfs., S. I., $\frac{1}{4}$...	10 40.5		114 25.5	
Holland bk., $\frac{1}{4}$ T, centre ...	10 39	108 43	— Cay, W end	10 44		114 21	
Pulo Criver de Mer, $\frac{1}{4}$ 34m., } r., highest peak 360f.	10 32	108 56	Soubie rf., d., centre	10 55		114 7	
Vanguard shl., E and W 71. s	7 28	109 43	Thitu I. and rfs., W end ...	11 2		114 11.5	
Grainier shl., $\frac{1}{4}$ 3m., 110 29.5	7 47.8	110 29.5	Trident shl., N end, d.	11 31		114 39.5	
Prince of Wales bk., $\frac{1}{4}$ S part	8 3	110 30	North Danger, a $\frac{1}{4}$ 2 islands, } 10 to 15f.	11 28		114 21	
Prince Consort bk., $\frac{1}{4}$ S part	7 46	109 55	Brown, s.	10 30		116 39	
Rifelman bk., $\frac{1}{4}$ S part, { SW end, NE "	7 31.5	111 32	Brown, shl.	10 35		116 58	
Amboyana Cay, centre	7 51.8	112 55.5	Brown, shl., [3 L.], $\frac{1}{4}$ a } flat, mid.	10 43	117 20		
Owen shl., [2m.], crl., $\frac{1}{4}$...	8 8	112 0	Cochin China	North Pennsylvania	10 52	116 55	
Sprattly or Storm I., 8f.	8 38	111 55.2		Carnaic shl., $\frac{1}{4}$ 3m., 117 26	10 6	117 26	
Ladd rf.	8 40.3	111 39		Auckland, $\frac{1}{4}$ T	10 20	117 20	
London rfs., W reef—cay... @	8 51.9	112 15.5		Fairy Queen, $\frac{1}{4}$ 3m., 117 39	10 34	117 39	
— central rf., d.	8 55	112 21		Seahorse or Routh bk., $\frac{1}{4}$ } 9m., $\frac{1}{4}$ 3m., 117 47	10 50	117 47	
— East rf., E extr.	8 49.5	112 38.2		Templar bk., NS 4m., $\frac{1}{4}$...	11 7	117 21	
— Cuarteron rf., d.	8 51	112 50		Cochin China continued from (69).			
Fiery Cross rf., $\frac{1}{4}$ 15m., I. } or NW Investigator, } SW bank, beacon	9 35	112 54.5		Buffalo I., or rk., T, 98f.	14 9	109 16	
Laconia breakers, South	5 3	112 42		Turtle I., small, l.	14 22	109 10	
— shl., Seahorse breakers ...	5 31	112 33		Tamquan R., bar	14 35.5	109 2	
— Friendship shl., [3 L.], } $\frac{1}{4}$ N pt.	5 58	112 31	G. of Tuquin	C. Batangan	15 16	108 54	
Louisa shl., [3m.], rks., T mid.	6 20	113 18		Pulo Canton, vis. 9 l., rf. SE, w	15 23	109 6	
Royal Charlotte shl., } [14m.], rks.	6 57	113 35		Qui-Quik, $\frac{1}{4}$ W, C. Bantam...	15 25	108 47	
Swallow shl., [4m.], rks. at }	7 23	113 50		Collao Cham, False, Honong, } Collao Cham I., $\frac{1}{4}$ 3m., A, } $\frac{1}{4}$ W, summit 1230f.	15 49	109 39	
E pt.	7 23	113 50		C. Turon	15 57	108 30	
South Viper shl. ?	7 30	113 0		Turon Bay, $\frac{1}{4}$ W, r. Turon I	16 7	108 19	
North Viper shl. ?	8 0	115 25		C. Choumay, West C.	16 5	108 12	
Ardaier shl., $\frac{1}{4}$ 3m., 114 10	7 37	114 10	R. Hue Fo, bar $\frac{1}{4}$ fort, W } entr.	16 33	107 38		
— Gloucester shl.	7 50	114 14	Tiger I., [1m.], 230f.	17 9	107 19		
SW Shra	8 0	114 50	S. Watcher, 272f.	17 55	106 39		
Investigator, $\frac{1}{4}$ W, EW 51., } W pt.	8 5	114 35	Hon Tseu, Goat I., 475f.	18 6	106 26		
Cay Marino ?	8 30	114 20	Hon Mat, Eastern I., 144f. ...	18 49	105 58		
S. Cornwallis shl. ?	8 52	114 12	Vinh, fort at entr. Ngan } Ka R.	18 47	105 43		
Pearson shl., rks., NS 3m.	8 56	113 44	Lacht Kuen Harbour.....	19 4.5	105 41		
Ganges	9 25	114 10	Hon Mè I.	19 20.5	105 57.5		
Sin Cona I.	9 42	114 22	Thanh-hoa town	19 48	105 45		
Discovery, Great rf., NS } 7m., d., N end	10 7.5	113 53	Song Ka River, Ninh Lacht } Custom Ho.	20 8.5	106 14		
— Small rf., d.	10 1	114 2	— Fort Ba Lacht	20 19	106 27		
Western or Flora Temple... @	10 15	113 37.5	Nightingale I., Batchlong vi. ...	20 7	107 41		
Tizard Bank, Itu Aba I. ... @	10 22.5	114 21.5	Hon Dau, lt. F 148f.	20 40	106 47		
— Nam Yit I.	10 12	114 22	Norway Is., S rk.	20 37	107 8		
— Eldad rf.	10 23	114 42	Laitao I., 8 pt.	20 43.5	107 25		
— Gaven rf.	10 13	114 13	Kua Doi or Bamoun	20 58.5	107 30.5		

TABLE 10

MARITIME POSITIONS

(71) Places		Lat. N	Lon. E	(72) Places		Lat. N	Lon. E
G. of Tongkin	Gautau Is., E cape	21° 2'	107° 50'	Haipong I., $\frac{1}{2}$ 3m., S part. }	21° 54'	114° 0'	
	Loshushan I., 804f.	21 14	107 55.5	Asses' Ears			
	C Paklong	21 29.5	108 11	Great Lema, $\frac{1}{2}$ 6m., w, E pt.	22 5	114 19	
	Long Moun R., Onloi Pt.	21 36	108 43.5	Lantau pk., 3050f.	22 16	113 58	
	Pakhoi Kwantau Pt., 374f. ...	21 27	109 2	Macao, Guia fort, lt. Rev. 339f.	22 11.4	113 38	
	Guie Chaw I., pk. 279f.	21 1	109 6.5	Canton, English factory	23 6.9	113 15.0	
	Lui Chew, C. Cami	20 13	109 55	Hong Kong, $\frac{1}{2}$ 9m., Vic- toria, N side, Cath. [N] }	22 16.9	114 9.5	
	Hainan I., $\frac{1}{2}$ 53 L. Hong pi Kok	20 0	109 49	C. Collinson, lt. F 200f.	22 15.7	114 15	
	Double hill pt., Pingmar	19 55	109 17	Mira Bay, [E], rk. mid. entr.	22 27.5	114 25.5	
	Chappa B., Hiongpo tort.	19 43	109 12	A high summit, 2810f.	22 31	114 32	
Hainan I.	Bluff Pt., 190f.	19 21	108 41	Single L., [3c.], T	22 24	114 40	
	South-west pt., Inkohai	18 32	108 41	Mendoza I., [1m.], T, 480f.	22 31	114 50	
	Rutton L. 256f.	18 20	108 57.5	Fokai Pt., sum. N 1m., 670 f. }	22 34	114 54	
	Great Cape, 1740f.	18 18	109 12	Pedro Blanco, k. T	22 18.5	115 7	
	Yu-lin-kan B., [E], entr. to inner harb. }	18 13	109 33	Whale rk., small, T	22 30.5	115 0	
	C. Bastion, 863f.	18 9	109 36	Che lang piah Pt., T	22 39	115 34	
	Liong-soy Pt.	18 22.5	110 3	Si-ki rk., 80f., T	22 42	115 45	
	Tien fung rk., rks., [W, T] ...	18 26	110 8	Cup-chi Pt., 210f., rks. S 2m.	22 48	116 4.5	
	Tinhosa Is., NS $2\frac{1}{2}$ m., 1609f., T E, N sum., (w.) }	18 42	110 28.2	Breaker Pt., l. rky., lt. Occ. } 132f. }	22 56	116 28	
	False Tinhosa, 150f.	18 50.5	110 34	Tonglao fort	22 59.5	116 31.5	
Paracel Is.	High Mountain, 3 pks., 2040f.	19 2	110 23	C. of Good Hope, lt. Int. 171f.	23 14.5	116 48.5	
	Mt. Toncon, 1229f.	19 40	111 1	Swatau lt. F. Fl. 200f.	23 19.9	116 45.5	
	Mofou Pt.	20 1	110 55	Namoa I., EW 12m., 1934f.	23 26	117 4.5	
	NE pt., or Hainan Head	20 10	110 41	Lamock Is., $\frac{1}{2}$ 8m., Boat rk.	23 11.4	117 14	
	Hoihau, W fort	20 3.2	110 19.5	Table Hill, 1767f.	23 39	117 9	
	Taya Is., 648f., [W, N one] ...	19 58.8	111 16	Chelsieu rks., [1m.], 20f.	23 29	117 15	
	Triton I., $\frac{1}{2}$ 4m., N part 20f.	15 47	111 14	Brothers, 2, $\frac{1}{2}$ 2m., S one Tonsang Harb., [E], entr., pagoda. }	23 32.5	117 42	
	Bombay shl., $\frac{1}{2}$ 4 L., rks., T, mid. }	16 3	112 32	South-east I., [1m.]	23 47	117 43	
	Discovery rf., $\frac{1}{2}$ 5 L., T, E extr.	16 14	111 54	S Merope shl., $\frac{1}{2}$ 5m., l. S pt., T	24 6	118 6	
	Crescent Chain, 6 ls., l. EW, Observation Bk. }	16 36	111 44	Chapel I., l., lt. F. Fl. 227f.	24 10.3	118 13.5	
CHINA, SOUTH AND EAST COAST.	North shl., $\frac{1}{2}$ 2 l., T, E pt.	17 3	111 36	Chauchat rks., l. E extr.	24 21	118 9	
	E extr., Dido	16 49	112 54	Amoy, [E], Kulangsea Semph.	24 26.8	118 4.0	
	Lincoln I., [1 m.], rfs. 1 m., l. w. }	16 40	112 44	Qumoy I., $\frac{1}{2}$ 10m., S pt.	24 24	118 19	
	Amphitrite Is., 2 grps., $\frac{1}{2}$ 3 l., l. Tree I. }	16 58	112 17	Dodd I., [1c.], lt. Occ. 147f.	24 26.1	118 29.2	
	Macclesfield shl., coral, EW 23 l., s to w, supposed growing, W extr. }	15 41	113 43	West Peak, a Mk., 1714f.	24 40	118 20	
	Scarborough shl., 8 rk. 10f. ...	15 5	117 49	Hoo-e-tow Pt., 80f.	24 31	118 33	
	St. Esprit shl., 7	19 33	113 2	Chinmo, (South), Pagoda I.	24 38	118 40	
	Helen shl., 4	19 12	113 54	Mt. Keu-sau, pagoda, 760f. ...	24 43	118 38	
	Pratas shl., [7 l.], rks., 8, ld. at W part, 40f. }	20 42	116 42.5	Chung-chi Pt., 400f., (rks. off)	24 46	118 46	
				Chin chu, [E], Passage I.	24 50	118 49	
CHINA, S.E. Coast				Pyramid Pt., (rks. off)	24 52	118 57.2	
				Meichow I., $\frac{1}{2}$ 5m., S pt.	25 1	119 6	
				— Sorrel rk., [1m.], 60f.	25 2	119 9	
				Ockau Is., $\frac{1}{2}$ 2m., lt. Rev. 286f.	24 58.8	119 26	
				Ping-hai	25 11	119 16	
				Loutzee rk., [1m.], (rks. off)	25 7	119 22	
				Lam-yit I., $\frac{1}{2}$ 8m., peak	25 12	119 33	
				Yit ls., $\frac{1}{2}$ E extr., Reef I. ...	25 18	119 45	
				Chimney I., EW 2m., N pt.	25 23	119 43	
				South reef, [1m.]	25 23	119 50	
CHINA, S.E. Coast				Turnabout I., [1m.], lt. F 257f.	25 26	119 57	
				Hae-tan I., NS 17m., pk. on NE side, 1420f. }	25 36	119 49	
				Kwing I., [2m.], (off NE part of Hae-tan), E pt. }	25 36	119 55	
				White Dogs, grp., $\frac{1}{2}$ 4m., Middle Dog, lt. F. Fl. 257f.	25 58	120 1	
				Sea Dog rk., small, T E	26 5	119 59	
				River Min., Temple Pt.	26 8.4	119 37.7	
				Ting-hae	26 18	119 48	

MARITIME POSITIONS							
(73)	Places	Lat. N	Lon. E	(74)	Places	Lat. N	Lon. E
	Matsou I., $\frac{1}{2}$ 3m., S pt.	26° 9'	119° 56'		Fisherman's Is., Monte Video, } $\frac{1}{2}$ 3m., T, 996f., ϕ	30° 8'	122° 46' 7"
	Chang-chi I., $\frac{1}{2}$ 3 $\frac{1}{2}$ m., 1330f.	26 14	120 0		Steep I., lt. Fl. 243f.	30 12	122 36
	Laræ rk.	26 16	120 12		Lakon Is. 313f., [1m.], T ...	30 26	122 56
	Alligator rk., small, 40f.	26 9	120 24 5		Beehive rk., T, 46f.	30 22	122 41
	Tung-ying Is., $\frac{1}{2}$ 3m., T 8, } sum. 853f.	26 23	120 29 7		Tai-san I., EW 8m., Pen- } nell Pt.	30 25	122 16
	Double Peak I., $\frac{1}{2}$ 3 $\frac{1}{2}$ m., } w, pk. 1190f.	26 36	120 9 7		Childers rk., T	30 37	122 50 5
	Pih-seang Is., [5m.], N Id.	26 42	120 20 5		Barren Is., [1m.], rky., T, } 150f.	30 45	123 8 5
	A dangerous rk., 88.	26 52 2	120 33 2		Saddle Grp., $\frac{1}{2}$ 13m., E } Sad., S pt., T, 692f.	30 42	122 49
	Fut-wan I., $\frac{1}{2}$ 4m., w' NE, } W-d. sum. 1700f.	26 56	120 21		— N Saddle, EW 2m., T, } N pt., lt. Rev. 273f.	30 51 5	122 40
	Tao Is., [2 l.], E one, sum. } 618f.	26 59	120 42		Rugged Is., EW 10m., SW } Horn, 50f.	30 36	121 57 2
	Seven Stars, rks., [2m.]	27 4	120 49		Gutzlaff I., [1m.], lt. F 270f.	30 48 5	122 10
	Cleft rk.	27 6	120 47		Yang-tse Kiang, beac. 33f.	30 51	121 52
	Nam-quan, [2], Bate I.	27 9 2	120 24 2		Aria-tne rks., [1c]	31 9	122 14 7
	Pih-quan Pk., 5m. inland.	27 18 5	120 27		Amberst rks., [1c], 26f.	31 11	122 22
	Castellated rk.	27 20	120 57		Wusung, fort, lt. F 50f.	31 23	121 30
	Nam-ki I., grp., $\frac{1}{2}$ 7m., w, } 740f., ϕ	27 26 5	121 2 5		SHANGHAI, BRIT. CONSULATE	31 14 7	121 29 0
	Pih-ki-shan Is., EW 4m., Coin I.	27 37 4	121 11 2		Nankin, city, porcelain to ...	32 2	118 49
	Quoin	27 50	121 13		Hankow, Boancker I., lt. F ...	30 33	114 30
	Wan-chu-fu, city	28 1	120 36		Sha-wei-shan, rk., lt. F 229f.	31 25	122 14
	Pe-shan Is., [2m.], E one.	28 5 5	121 30		Tung Ming I., $\frac{1}{2}$ 10 l., } E pt.	31 28	121 51
	S. Foreland I., [1m.]	28 16	121 42		A shi, pt., NNE 6l.	31 44	121 57
	Chik-hok I., [1m.], 1, 760f.	28 22 4	121 42		A shi, $\frac{1}{2}$ 5m., ϕ	32 0	122 0
	N. Foreland I., [1m.]	28 33	121 37		Is. in G. of Whang-ho, } outer	33 0	120 40
	Taichow Is., $\frac{1}{2}$ 8m., S pt., } or Fingers	28 23	121 53		Whang-ho, or Yellow R. ...	34 2	120 10
	— Shang-tai, grt. one, $\frac{1}{2}$ w, } N pt.	28 30	121 52		Hae-chow, city	34 35	119 30
	— North Id., [and rfs., 1m.] ...	28 32	121 54		Tower Pt.	36 21	119 33
	Square I.	28 35	121 47		Kyau-chau Harb., NE hill ...	36 3	120 14
	Tung-chuh, or Bella Vista, } $\frac{1}{2}$ 2m., sum. 700f.	28 42 2	121 54		Ka-tih-neau I.	36 11	120 57
	Hai-mun, S of entr. of R.	28 40	121 26		Surveyors I.	36 16	121 24
	Taichow, citadel.	28 50	121 50		Urh Taou, or Staunton I.	36 45 7	122 16 2
	Fall I., [1m.]	28 51	122 13		Shan Tung prom., lt. F 220f.	37 24	122 42 5
	Hirshan Is., $\frac{1}{2}$ 5m., F, S or } Saddle I., 320f., w.	28 56	122 17		Alceste I., small, Fks. off ...	37 27	122 40 5
	Eight feet rk., (N of do.)	28 59	121 53		Wei-hai-wei Harb., [2], N } pt., entr., Lungung I.	37 32	122 10
	Triple I., [2c. ?]	29 3	121 55		Che-tow C., [2] SE-d.	37 36	121 26 2
	C. Conway	29 10	122 4		Chung-shan I., S extr., $\frac{1}{2}$ } 7m., 8 pt.	37 55	120 45
	Montague I., $\frac{1}{2}$ 4m., 740f., } E pt.	29 13	121 55		Miautan Is., Ta-Hi Shan, W pt.	37 58	120 36
	Sheepoo	29 26	122 11		Howki I., lt. Fl. 328f.	38 4	120 39
	Kwee-shan Is., [6m.], grt. } one, sum 400f.	29 22	122 13 5		N extr., Siao-kin-Tao, [1m.] ...	38 21	120 51
	— Patahecock I., [3c.], A.	29 27	122 15		Hwang-ching-tao I., EW 2m.		

CHINA E. Coast

CHINA, E. Coast

CHINA, N. E. Court

Gulfs of Pechili and Liawlung

TABLE 10

MARITIME POSITIONS

(75)	Places	Lat. N	Lon. E	(76)	Places	Lat. N	Lon. E
	Round I., small, 200f.	38° 40'	122° 12'		Kerama Is., W one, High } I., 916f.	26° 10'	127° 15'
	Rock, like a junk, Shi-siau ...	38 56	122 45		Great Liu-kiu, Okinawa, } # 191., Nafakiang, Ab- bey Pt.	26 13	127 41
	Hai yun-tau I., 8 pk. 1370f. ...	39 3	123 10		- C. Yakimu Pt., (rf. 4-8m.)	26 4	127 41
					- E extr., C. Sidmouth, l. off	26 47	128 21
					- N extr., C. Hope, Heto ...	26 51	122 17
					- Kiu, Herbert I., # 24m., entr., Port Oouting or Melville, (ft., sum. 354f.)	26 42	128 2
					- Sugarloaf, 8 l., 575f.	26 43	127 49.5
					Montgomery Is., # 51., # } N pt.	27 5	128 2.5
					Yori-sima, 413f.	27 2	128 26.5
					Yerabu-sima, pk. 687f.	27 21.5	128 35
					Kakirouma I., 2207f., C. }	27 38	128 55.5
					Ohotabu	27 52	128 14
					Sulphur I., Iwo-simas, 541f. ...	27 52.5	128 53
					- C. Sarafana	28 00	129 9
					Iwo-sima, C. Kataki	28 17	129 19
					Amami oo Sima, Ylomi	28 31	129 42
					- Iono Misaki	28 17.5	129 59
					Kikai ga sima, pk. 864f.	28 44.5	129 47
					Sandon rks., 30f.	28 48	129 2
					Yoko sima, 1700f.		

(79)	Places	Lat. N	Lon. E	(80)	Places	Lat. N	Lon. E
Saghalin Island	C. Siourkum	50° 6'	140° 43'	Kamchatka	C. Shipunski	53° 6'	160° 4'
	Castries B., lt. F 262f.	51 25 5	140 55		Kronotsky, pk., 10,810f.	54 47	160 37
	Amur R., Nikolaevsk Cathedral ..	53 8 1	140 43		C. Kronotsky	54 54	162 35
	Saghalin I., C. Jonquiere, } lt. F 360f.	50 53	142 7		Kluchevski, volc., 16,131f. ...	56 8	160 48
	Tcharkaïkove-ossa Pt.	48 46	141 50		C. Kamchatka	56 0	163 15
	Kosounai Road	47 58 7	142 13 7		Behring I., $\frac{1}{2}$ 16 l., NW pt.	55 17	165 42
	Monneron I., Totomusiri I., } 1400f.	46 14	141 11		— South pt.	54 43	166 42
	C. Notoro, lt. F 135f.	45 54	142 2		Copper, or Medni I., 8 pt.	54 33	168 11
	Kam-n Opornosti, 20f.	45 4 5	142 10		C. Stolbovoi, A, 1	56 40	163 25
	Karsakovsk Road, lt. F.	46 40	142 44		C. Ozernoi	57 37	163 15
	C. Siretoko	46 1	143 26		Karaghinsky I., $\frac{1}{2}$ 20 l., N pt. ...	59 13	164 38
	C. Tonin	46 50	143 27		— South pt.	58 28	163 27
	Robben I., 48f.	48 32	144 45		C. Olutorsky	59 57	170 19
	Tichmenev	49 13	143 9		C. Navarin, A	62 16	178 56
	C. Patence	48 42	144 55 5	Asia, E. Coast	NORTH-EAST COAST OF ASIA.		
	C. Delisle de la Croyere	51 1	143 47		Bay of Archangel Gabriel, } NE pt., or C. King	62 28	179 14
	C. Loevenstern	54 3	143 15		C. St. Thaddeus	62 42	179 30
	C. Elizabeth	54 24	142 47		R. Anadyr, C. Alexandra	64 42	177 22
	C. Maria	54 17	142 18		Kresta Gulf, C. Meechken ...	65 29	181 15
	C. Gulovaicheff	53 25	141 53		C. Behring	65 0	184 6
Okhotsk Sea	C. Khanbaroff	53 30	141 3		C. Tehnokotski	64 17	187 46
	R. ineeke I.	54 18	139 52		Plover Hd.	64 21	186 40
	Shantar Is., EW 20 l., E one, } I Procoffieff, [4m.], E pt. }	55 2	138 27		Arakam L. E pt.	64 46	187 54
	R. Onoda, mouth	54 44	135 24		Metchignie B., entr., pt. L ...	65 31	187 51
	St. Jonas I., [1m.], ϕ , 1200f. ...	56 25	143 18		C. Krléongoune	65 29	189 0
	Port Aian	56 25 5	138 21		St. Lawrence B., E pt. entr. ...	65 37	189 11
	Okhotsk	59 22	143 14		East Cape, SE extr., 2521f. ...	66 3	190 16
	C. Bligan	58 40	151 37		N. Coast		
	C. Piaglin	59 13	156 15		C. Serdze Kamen (Behring, } 1728)	67 0	188 6
	Ghujinsk, lt. F.	61 53	160 37		Jinretlen (Nordenskiöld, } 1879-80)	67 7	186 26
	Penjinsk	62 30	162 56		Burney, or Koliutchin I., 8 pt	67 27	185 55
Kuri Is.	Yetorup I., $\frac{1}{2}$ 43 l., 8 pt., } C. Rickard	44 25	146 56		Herald I., 900f.	71 19	184 43
	— N pt., C. Vries	45 40	148 45		Kellett land, or Wrangell I., }	70 58	182 20
	Urup I., $\frac{1}{2}$ 17 l., SW pt.	45 37	149 32		C. Hawaii	71 7	181 18
	Pyramid rk., off N and E pt. ...	46 19	150 27		C. North of Cook, 105f.	69 4	179 31
	Broughton I., [1 l.], A, ϕ	46 44	150 28		C. Jakan	69 40	176 34
	Simu-ir I., $\frac{1}{2}$ 10 l., S pt., or } C. Rollin (Sianuni)	46 49	151 37		C. Shelskoi	70 2	171 10
	Broughton B.	47 13	151 56		Bear Is., E or Column I.	70 38	162 20
	Rashua I., [pk.], (rks. SW-d.) ..	47 51	152 47		— West one	70 50	160 35
	Matua I., Saryche Pk.	48 6	153 12		De Long Is., Jeannette I.	76 45	159 0
	Raikoke I., [1 l.], sum.	48 16	153 15		— Bennett I., C. Emma	76 40	149 0
	Musir Is., S.						

C. Ongon	58	0	157	50
Bolshebetk, ent. R.	52	45	156	14
C. Lopaika	50	53	156	46
Mt. Vlutchin, 7060f.	52	42	158	22
Avatcha B., \boxtimes , E entr., lt. }	52	52.5	158	47.0
— F 526f.				
St. Peter and St. Paul, Ch.	53	1.0	158	43.5

TABLE 10

MARITIME POSITIONS

(81)	Places	Lat. N	Lon. E	(82)	Places	Lat. N	Lon. E
EASTERN ARCHIPELAGO.							
Pontianak R., Pa d'ang I. ...	0° 2'	109° 10'		Nangaloo Is., [1 l.], NE pt....	11° 25'	120° 10'	
Bangkai Pt.	0 19	108 56		Yloe I., [3 l.], S pt., rock off	11 16	119 42	
Setu d'ang I.	0 21	108 45		Linicapan, NW pt.	11 28	119 43	
Burog Is., Lamukutan, N pk.	0 48	108 42		Tres Reyes rks., [½ m.]	11 34	120 6	
Sambar R., Fort Sorg.	1 11	103 58		Delian I., [1 m.]	11 51	120 19	
Tanjong Api, l. ½, 8 2m., w' ...	1 57.5	109 19		Tara I., ¼ 3m., 730f., N pt....	12 20	221 21	
Tanjong Dato, A.	2 5	109 40.5		Bu-uanga I., ¼ 12 l., N pt. ...	12 20	119 53	
Marundam I., small, 120f.	2 3.5	109 6.5		Colocoto rks., [1 m.]	12 28	120 2	
Tanjong Sipang, ark. (rks. 5m.)	1 48	110 21		Culion I., ¼ 7 l., Culion	11 54	120 0	
Tajong Po, lt. F 490f.	1 44	110 32.5		Philippine Islands.			
Sarawak R., New fort.	1 33	110 21		Hunter Rock.	12 41	120 11	
Sirik Pt., l. lt. F.	2 46	111 21		Merope shl., [2m.]	12 40	120 15	
Mt. Biliungan, 1500f.	3 48	113 47		Apo shl., ¼ 2 l. ? Is. ½, l	12 44	120 24	
Tanjong Barram, 4 r. off ? ...	4 36	113 58		Apo I.			
Mt. Mula, 4000f.	4 7	115 14		Falmouth Bank, NS 2 l., N pt.	11 54	120 58	
Bruni, or Borneo, city palace	4 52.2	114 54.2		Panagatan shl., EW 3m., 3f....	11 52	121 16	
Marao I., E pt.	5 0.4	115 4		Semirara Is., N pt., [5m.], ½	12 7	121 20	
Labuan I., Ram-ay Pt.	5 16.5	115 15		— S pt., or Pirato I., ½ o. l	11 58	121 22	
I'ulo Tega, S, N d 3 l. N end	5 44	115 38.5		w, (a lake), SE pt.			
Castle Pk., 1500f.	5 47	116 5		Kiniluban, [1 l.], remble. }	11 26	120 46	
I'ulo Gaya, ¼ 4m., lt. F.	6 0	116 3		— spire on W extr.			
Samarang Bk., 5 ...	5 36	114 53		Manigian I.	11 36.5	121 40	
Vernon Bk., 3 Fury rks.	5 44	115 2.5		Pointed bank.	11 21	121 40	
Saracen Bk., SW extr.	6 6	115 18		Manamoc I. and rfs., [2 l.], pk.	11 18	120 42	
Mangaloon I., small, 88 ...	6 11	115 35		Cuyos I.			
Ambong B., ½ ...	6 18	116 19		— Grt. or Cayo I., Town...○	10 51	121 1	
Kini Bau, Min., 13,700f.	6 7	116 33		— E extr. or Tagauayan ...○	10 58	121 13	
Matanani Is., [5m.], W pt.	6 42	116 16		— S extr., Imalagan, 303f.○	10 45	121 4.5	
N. Furious shl., 7 ...	7 1	116 17		— SW extr., islet, P'aya, 90f.○	10 48	120 36.5	
N extr., Samjanmango Pt., }				Sombrero rks., [10 yds.] ...○	10 43	121 33	
Kalampuanian I., off ... }	7 4	116 43		White rks., 24f.	10 26	121 2	
Belambangan I., ¼ 5 l., 2 }				Ambolon I., S end, (shl.) }	12 11	121 1	
SE, 440f., Kalutan I. ... }	7 13	116 49		SE d)			
Banguey I., ¼ 7 l. NW, }				Port Mangar'm Town.	12 21	121 5	
pk., 1876f. }	7 17.5	117 5.7		Pt. Lumintau.	12 31	120 54	
— E side, Bancowan I., S pk. }	7 12.5	117 18.5		Sablayan Pt.	12 50	120 45	
Mang-i Is., ¼ 3 l., (rfs. }				Mamburao R.	13 15	120 33.5	
WSW 31.), S' l. }	7 32	117 16		C. Calavite.	13 26	120 17.5	
— N one, Salingsingan I. }	7 34	117 16		Paluan B., vill., w.	13 23.5	120 29.2	
Balabac I., NS 7 l., 1900f., }				Mt. Calavite, 3000f.	13 28.7	120 24	
S pt., or C. Melville. }	7 49	116 59		Pt. Escarceo.	13 21.6	120 59.2	
Calandorag B., lt. F 119f. ... }	8 0	117 2.7		Silonay I.	13 27	121 13	
Palawan, ¼ 80 l., S extr., }				Pt. Dumali, (sum. ¼ 3m.) ...	13 6	121 34	
or Pt. Buliluyan. }	8 20	117 10		Pt. Dayagan.	12 38	121 32	
Bulanhan hill, N end of }				Pt. Pandan.	12 17.5	121 23	
range, 3,500f. }	8 40	117 24		Libagao I., [2m.], 410f.	12 12	121 25	
Albion head.	9 17	117 58		Ilin I., Pt. Ilin.	12 9	121 6	
York breakers, [½ m.], 1 foot	9 53	118 8					
Table Pt.	10 0	118 38		Golo I., SE end.	13 38.5	120 25.5	
Ulugan B., NW head.	10 8	118 45		Labang I., ¼ 4 l., A, N pt....	13 52	120 5.5	
— Watering B.	10 10	118 48		— Loco Bay.	13 43.8	120 16.7	
High I., off Port Barton, }				Calraa, or Goat I., lt. Fl.	13 54	120 2	
1050f. }	10 31	119 4					
Malampaya Id., Pancoh.	10 52	119 23		C. Santiago, (Minerva rk. }			
Tapiutan I., (Rugg. Is.), N pt.	11 14	119 15		ESE 5m.) }	13 46	120 40	
Cabuli I., [1m.], 560f.	11 26	119 29		Fortune I., [1m.], 450f.	14 4	120 29	
Dumaran I., ¼ 5 l., E pt., }				Friar, 120f. off Pt. Limbones	14 18	120 37.5	
Pirate Hd. }	10 35	120 0		Cavite, lt. F 30f.	14 29.5	120 54.5	
Carlandagan I., NS 3m., E pt.	10 39	120 15		MANILA CATHEDRAL.	14 35.5	120 58	
Barbacan, Stockade.	10 21	119 23		Orani.	14 48	120 33	
Port Royalist, lt. F 43f.	9 44	118 43		Corregidor I., lt. Fl. 639f. ...	14 23.3	120 34	
Detached I., East I., [1m.], l.	8 53	118 15		Pt. Luzon, or Hornos.	14 25.5	120 28	
Kanaran I., [½ m.], 800f.	11 14	120 16		Port Subec, Grande I.	14 47	120 13	
				Pt. Capones, large I. off. A, ½ c	14 55.5	120 0.5	
				Yba, town.	15 20	119 58	

TABLE 10

MARITIME POSITIONS

(83)	Places	Lat. N	Lon. E	(84)	Places	Lat. N	Lon. E	
Luzon, W. Coast	Masingloc, town.....	15° 33'	119° 57'	Luzon, E. Coast	Yligan Pt.	18° 20' 5"	122° 18'	
	Hermana mayor I., summit ...	15 48	119 47.2		Mt. Dos Cuernos, 4008f.	17 30	122 6	
	Pt. Caiman, rf. SW	15 55	119 46		Tumango Port, N pt. entr. ○	16 43	122 14	
	Tambobo Pt.	16 05	119 43.5		C. St. Ildefonso	16 5	121 46	
	Bolinao, Tel. Station.....	16 24	119 56		Port Lampon	14 43	121 34	
	Port Sual, lt. F 79f.	16 6	120 7.5		Polillo I., $\frac{1}{2}$ 7 l., Banla	} ○	15 5 122 6	
	Dagupan R., lt. F 29f.	16 5	120 19.5		Pt., (Is. SE-d.)			
	Pt. San Fernando, lt. F 29f.	16 37.5	120 17.5		— South point	14 43	122 4	
	Pt. Darigayos.....	16 51	120 20.0		Jomalie I., [3 l.], E pt. ...	14 35	122 17	
	Port Santiago.....	17 18	120 27		Maulamat I.	14 30	122 19	
	Pt. Dile	17 34	120 21		Cabelete I., [4m.], S pt. ...	14 15	121 50	
	Mt. Bulagao, 3629f.	17 38.5	120 31		Alabat I., [3 l.], 4, N pt. ...	14 14	121 55	
	Pinget I., S pt.	17 40	120 22		Jesus Pt.	14 22	122 26	
	Culili Pt.	18 5	120 28.7		Samur I.	14 31	122 43	
	C. Bojeador, l. β 2m.	18 30	120 34.5		Matandumaten, l. Is.	14 17	123 5	
	Pt. Mayraira	18 40	120 52		San Miguel B., Canton	} ○	14 4 123 5	
	Caraballo Hill.....	18 31.5	120 54		I., W of entr. [1m.] ...			
	Cabucungan Pt.	18 38.2	121 6		I. Batavanan, $\frac{1}{2}$ 3m., N pt....	14 9	123 17	
	Aparri, town, $\frac{1}{2}$ to	18 21.3	121 37		Sisiran Port, $\frac{1}{2}$ Basi	13 55	123 36	
	C. Engano, Hermanos Is.	18 35.5	122 6.5		Palumbanes I., EW 3m., W pt.	14 5	124 4	
Babuyan Is.	Dedicas rks., $\frac{1}{2}$ pkd.	19 3	122 9.5	Luzon S. Coast	Catanduanes I., $\frac{1}{2}$ 13 l.,	} ○	14 8 124 13	
	Guinapac rks., $\frac{1}{2}$ T, $\frac{1}{2}$ W ...	18 58	122 4		shl. N of, [1 l.], tot pt. ...			
	Camiguin I., $\frac{1}{2}$ 4 l., (Port	} 18 55	} 121 48		— S. or Taguntun Pt.	13 31	124 9	
	S Pio Quinto, $\frac{1}{2}$ W, w),				Volcano of Isaro	13 39	123 21	
	volc., vis. 20 l., Font l....	} 18 52	} 121 16		Volcano of Albay, 8274f.....	13 16	123 41	
	Fuga, or New Babuyan,				Rapurapu I., [3 l.], Unguy Pt.	13 11	124 10	
	EW 5 l., Port Musa, $\frac{1}{2}$,	} 19 9	} 121 13		Pt. Montugan, rfs. 3m.	13 8.5	124 13.7	
	at W End				Volcano of Bulusan	12 47	124 2	
	Dalupiri, vis. 11 l., $\frac{1}{2}$ rks.	} 19 22	} 121 22		St. Bernardino I., [2c.], $\frac{1}{2}$ o.	} 12 46	} 124 15	
	S-d., N pt.				I. E and W, 150f.			
Batan Is.	Calayan, [3 l.], $\frac{1}{2}$ T, rf.,	} 19 30	} 121 39		S extr. of Luzon, Calintan I.	12 31	124 5	
	NW pt.				Los Naranjos Is., [2 l.],	} 12 22	} 124 0	
	Wyllie rks., 2, $\frac{1}{2}$ 2m., N	} 19 31	} 122 1		Raza I.			
	part				Capul, $\frac{1}{2}$ 7m., N pt.	12 29	124 8	
	Claro Babuyan, [5 l.], $\frac{1}{2}$	} 20 1	} 122 18		Port Sorsogon, $\frac{1}{2}$ town	13 0	123 59	
	volc. E end.....				Ticao I., $\frac{1}{2}$ 5 l., N pt., S	} 12 43	} 123 36	
	Balintang, or Richmond Is.,	} 20 17	} 121 53		Miguel I.			
	3, [1 l.], $\frac{1}{2}$ A. 1, T, 80, N				— Port San Jacinto, on E	} 12 32.3	} 123 45.5	
	one, vis. 8 l.	} 20 19	} 121 49		side, $\frac{1}{2}$ w, r			
	Sabtan I., NS 5m., S pt.				Masbate I., Bugui Pt.	12 36	123 15	
Busue Is.	Ibugos, NS 2m., S pt.	} 20 21	} 121 48		— Jintotolo I.	11 51	123 7.5	
	Dequez, (Goat Is.), [$\frac{1}{2}$ m.],				— Port Barreras, on N side,	} 12 33	} 123 24	
	W. pt.	} 20 28.5	} 120 1.2		$\frac{1}{2}$, N pt. entr.			
	Batan, or Monmouth, $\frac{1}{2}$				Burias I., Busin lt. F.....	13 8	122 58	
	9m., r, w', N sum. 3806f.	} 20 27.5	} 121 59.0		Cabeza de Bondo, 1250f.	13 12	122 35	
	— San Domingo, Cathedral ..				Marinduque I., $\frac{1}{2}$ 8 l., Mar-	} 13 12	} 122 2	
	Diogo, (Grafton I.), [$\frac{1}{2}$ m.],	} 20 41.5	} 121 57		langa Pt.			
	848f.				— St. Andre, pt. 751f., $\frac{1}{2}$...	13 33	121 52	
	Ibayat, (Orange I.), $\frac{1}{2}$ 8m.,	} 20 47.3	} 121 52.7		Pagvilao I., $\frac{1}{2}$ 1 l., S Pt.	13 53	121 45	
	r, $\frac{1}{2}$ W, N sum., or Sta.				Pt. Locoloco	13 39	121 25	
	Rosa, 680f.	} 20 54	} 121 57		Mt. Labo, sum. 3363f.	13 40	121 18	

MARITIME POSITIONS

(85) Places		Lat. N	Lon. E	(86) Places		Lat. N	Lon. E
Samar Strait	Silayan I., $\frac{1}{2}$ 51, pk 6424f., } Pt. Cavit.....	12° 16'	122° 38' 7	Mindanao	Pt. Cavit	9° 17' 5	126° 14'
	Crosta del Gallo I., [1m.], S	12 11 5	122 42 5		Catel. town	7 48	126 22
	Samar I., $\frac{1}{2}$ 42 I., Batag I., } NS 5m., N pt.	12 43	125 5		Pt. Pusan	7 14	126 25
	— Port Palapa, Calapan I.	12 37	125 0		C. St. Augustin, or Pan- } dagitan	6 14	126 6
	— Borongan, town	11 42	125 25		Palmas I.	5 30	126 28
	— S and E extr. I.	10 54	125 52		Davao R., lt. F 27f.	7 1	125 36
	— Manican I., [1 I.], S pt.	10 58	125 38		E Sirangani I., NS 4 I., w', } b, hill, S end	5 24	125 25
	Canduy I., lt. F 33f.	11 26	124 53		Pt. Tinaka, vis 12 I., T	5 35	125 16
	Parasan Pt.	11 44	124 46		Glan Masila R., lt. F 33f.	5 45	125 15
	Sibugay I., N end, [1 I.]	12 0	124 27		Volcano, 3600f.	5 45	125 25
Leyte	I. de la Mesa, [1 I.], Bagu } pul I.	11 53 5	124 17 5	Mindanao	Leno Bay	6 45	124 00
	B. Ilian, $\frac{1}{2}$ 7 I., Tincanuan I.	11 41	124 20		Mindanao, R. entr.	7 16	124 11
	Carnosa I., small, S pt.	11 30	124 6		Pollock Cove, $\frac{1}{2}$ w. P., fori	7 21	124 11 5
	I. del Gato, rk.	11 27	124 1		Bongo I., $\frac{1}{2}$ 5m., SW pt.	7 18	123 59
	Tagapula, $\frac{1}{2}$ 6m., E pt.	12 5	124 15		Tiguma	7 46 5	123 25
	Leyte I., $\frac{1}{2}$ 37 I., } Girantaungan islet	11 35	124 16		Pt. Flecha	7 22	123 22
	Port Palompon, town	11 2	124 24		Oluntanga I., S pt.	7 16 7	122 48 5
	Camotes Is., NW one, Tulang	10 44	124 18		Cocos I., small, 690f.	6 44	122 14
	Ylongos, town	10 23	124 44		Sea Crus Is., 2, E one	6 52 5	122 3 2
	South pt., Leyte I.	10 0	125 2		Samboanga, w, r, Gov. Ho. } lt. F 33f.	6 55	122 4 5
Zebu	Limasana I., S end	9 54	125 4	Sulu Sea	Cudera Port	6 57 5	121 57 5
	Panaon I., 2313f., 8 pt.	9 55	125 16 5		Sibuco B.	7 20	122 4
	Bohol, EW 15 I., Namanuco Pt.	9 47	124 36		Pt. Balangonan, >	7 47	122 5 5
	— West point, or Pt. Duljo ...	9 45	123 42		Murcielagos I.	8 7 5	122 26
	Zebu, $\frac{1}{2}$ 35 I., Taffon Pt.	9 25	123 19		Pt. Sindangan	8 11	122 39
	— Zebu town, $\frac{1}{2}$ fort, lt. F 42f.	10 17 5	123 54		Pt. Blanca	8 32	123 4 5
	— NE, or Butalique Pt.	11 17	124 4		Aliquay I., l, $\frac{1}{2}$, T S.	8 45	123 13
	Doon Is., SW I.	11 2	123 36		Silino I., l, $\frac{1}{2}$, T S.	8 51	123 24
	Calangaman I., at E extr. } of a rf.	11 7	124 15		Pt. Tabud, lt. F 43f.	8 42	123 22
					Misamis town	8 9	123 47 5
Negros	Siquijor, $\frac{1}{2}$ 7 I., Pt. Minalutan	9 10	123 42	Sulu Sea	Pt. Suluanang	8 38	124 29 5
	Negros I., $\frac{1}{2}$ 38 I., Siaton Pt. ...	9 2	122 59		Cagayan, anchorage	8 30	124 40
	— Pt. Sojoton, T	9 59	122 27		Pt. Bagacay	8 59	124 49
	— North Pt., Ylason I.	11 2	123 11		Camiguin I., [4 I.], 5338f.	9 11	124 44
	Panay $\frac{1}{2}$ 32 I., 8 pt., A, I., } Juraojarao islet	10 24	121 57 5		Sulu Sea.		
	S. Jose de Buenavista	10 44 5	121 55		Sultana Bank, $\frac{1}{2}$	9 59	121 22
	Nalupapt rf.	11 13	121 59		Cagayanes Is., 3, l, $\frac{1}{2}$, (rf. } N end)	9 47	121 20
	Maniglin	11 37	121 40		Calusa, [3c.], $\frac{1}{2}$, $\frac{1}{2}$	9 36	121 6
	Pt. Pucio, 620f.	11 46	121 50		Anuling I.	9 44	121 25
	Borocay I., 436f., N pt.	11 59	121 54		Cavelli I., 124f., [$\frac{1}{2}$], NE } extr.	9 14 2	120 52 2
Panay	Pontud, [1 $\frac{1}{2}$ m.]	11 50	122 15	Sulu Sea	— Reefs, SW extr.	9 10 5	120 45 7
	Port Butan, $\frac{1}{2}$	11 36	122 30		Jessie Beazley rf.	9 2 5	119 48
	Olutaya Islet	11 38	122 50		Toob Bavaha, shl., $\frac{1}{2}$ 7 I., } rk. S extr.	8 49	119 55 5
	Zapato Mayor	11 45 5	123 2		— Shl., SW-d, S rk.	8 43 5	119 51
	Jintotolo I., [1 I.], 120f.	11 50	123 8 5		St. Michael's I., Manuk } Manukan, 32f.	7 42 6	118 28
	Pt. Bulacane	11 37	123 9 5		— Bancawang, 123f.	7 44 8	118 33
	Gigantes Is., [2 I.], Vaidajon	11 38	123 22		— Bancoran, 140f.	7 56 6	118 41
	Culebra Islet	11 22	123 14		Cugayan Sulu Is., 2, large } one, A, $\frac{1}{2}$, rk. at entr. } of circ. basin	6 59 1	118 29
	Baliguian Islet	11 12	123 20		— Keenapoussan I.	7 11 3	118 26
	Ilo Ilo Fort, lt. F 21f.	10 42	122 36		— S extr., Mulegee Is., T, 2, ..	6 53	118 24 2
Surigao Is.	Suluan, [1 I.]	10 46	125 58	Sulu Sea	Mambahanan	6 34	118 31 5
	Malhon I., [4 I.], E pt.	10 43	125 49		Talantam bk., S	5 42	119 27
	Dinatag I., Pt. Desolation ...	10 28	125 38		Pearl Bank, ent.	5 48	119 39
	Gibuson I., N pt.	10 28	125 28		Tawi Tawi, Bongola, $\frac{1}{2}$	5 3	119 47 5
	Siargao I., Sapao Pt., 620f.	10 4	126 3 5		Manuc Manca, S pt.	4 47 2	119 50 5
	P. Sibunga, entr., $\frac{1}{2}$	9 41	126 1				
	Bilau Pt., N pt. Mindanao	9 49	125 26				
	P. Surigao, $\frac{1}{2}$, town	9 47	125 31 7				

587

Sulu Archipelago

Borneo, N.E.

Borneo, E. Coast

1

MARITIME POSITIONS

(89) Places		Lat.	Lon. E	(90) Places		Lat. S	Lon. E
Celebes, N. Coast	C. Rivers, via. 30 L. Slime } islets, 80f., ♀, ~	North 1°20'4"	120°44'5"	Hoorn Is., EW 4m., rk. } W-d., Payung Dekat..... }		5°47'7"	106°28'
	Pienjan I.	1 19	121 3	BATAVIA, OBSERVATORY ♀ 0°, G.M.T. 7° 7' 14.5" ... }		6 7 6	106 48.5
	C. Kandie, or Dako	1 20	121 25	— Edam I., lt. F 183f.		5 57.5	106 50.5
	Josina rfs., Bongk'e I.	1 5	122 57	Karawang Pt., ♀		5 56.3	107 0.2
	Mr. Sopotan, 5994f.	1 7	124 45	Tanj. Sedari, ♀ NW lim.....		5 58.5	107 21
	Manado, Fort Amsterdam ...	1 30	124 46.5	Sedari rf., [3m.], ♀, S		5 56	107 25
	Mt. Klobat, 6694f.	1 28	125 2	Pamanukan Pt.		6 12	107 46
	Tona Manado I., [3m.], 2737f.	1 39	124 42	Injarimayn Pt., ♀, ♀, E extr.		6 14	108 18
	— Nuia I., [14m.], 76f.	1 47	124 47	Boompjes Is., lt. R 191f.		5 56	108 22.5
	Talisse I., ♀ 6m., 1168f., N pt.	1 54	125 6	Cheribon, lt. F 46f.		6 43	108 34.2
	Banka, ♀ 7m., E pt.	1 48	125 11	— Pk., 10,075f.		6 54	108 24.2
	C. Coffin	1 41	125 10	Tegal, lt. F 49f.		6 51	109 8
	Limbe I., ♀ 3 l. N pt.	1 33	125 17	Pekalongan, lt. F 50f.		6 51.5	109 41.2
	Kema, w, r, fort.	1 22	125 5	Mt. Selamat, (vol.), 11,224f....		7 14.5	109 13
	Belang Town	0 56	124 47	Bapang sh., [2m.], s.		6 34.5	109 50
Celebes, E. Coast	C. Flesko, Kalapa I.	0 26	124 27	Mt. Sumbing, 10,945f.		7 23	110 4
	Gorontalo R., r, w, lt. F 95f...	0 30	122 58	Sumarang, lt. Fl. 107L		6 57	110 24.5
	Parigio	0 47	120 9	Japara, Po. Panjeng		6 34.6	110 37
	C. Tellogonda	0 58	120 34	Mandjika I., lt. F 280f.		6 23	110 54.7
	Una Una I., N pt.	0 9	121 35	Laut, Juana, lt. F 49f.		6 41.5	111 9
	C. Apie	0 47	121 36	Leran Pt.		6 38	111 27.5
	Grt. Waleah I., N end	0 13	122 12	Aur Aur Pt.		6 46	111 56.7
	C. Talalo, A, E pt.	0 46	123 27	Panka Pt., l. fl. st.		6 53	112 34
	Toko B., Once Malubu Pt. ○	1 58	121 33	Sourabaya, citadel, lt. F 42f...		7 13.5	112 44
	Peling I., E pt.	1 17	123 31	Madura, EW 29 l., NW pt., }		6 54.3	112 49
	Bangkula I., S end	1 57	123 5	— C. Modang		6 58.5	114 7
	Nederburgh Pt., 8 5m.	2 53	122 17	— East pt., Lapa Pt.		7 2	113 54
	Low Ambeli I.	3 6	122 33	— Samenep B., fort.		6 58	114 26
	Labengki I., [8m.], E pt.	3 27	122 28	Pajangan I., [1m.]		7 5.3	114 16
	Maui I., [3 l.], A, NE pt. ...	3 35	123 12	Ho: I., or Sapudi, ♀ 9m, }		7 6	114 47.7
Celebes, Gulf of Boni	Pt. Nipa Nipa, N extr.	3 54	122 39	W pt., lt. F 192f.		7 37.5	112 55
	Kendarie B., Woweala Pt. ...	4 0	122 38	Po. Kamali		7 43.5	113 41.2
	Wawoni I., [5 l.], E pt.	4 5	123 11	Pasuruan, lt. F 52f.		7 35	114 2.2
	Bouton I., ♀ 27 l., N pt.	4 23	123 4	C. Sedano		7 49	114 28
	— East pt., l.	5 13	123 15	Karang Maas, Meinders rk., }		7 0.5	114 26
	— South pt.	5 42	122 48	lt. F 56f.		8 3.7	114 15.5
	— Bouton town, fort, r, P. ...	5 28	122 37	Mt. Merapi		8 12.8	114 23
	South I., 8 pt.	5 43	122 30	BARJUWANGIS, Ft. UTAKCHT lt. F		8 42.5	114 36
	Kabaena I., [5 l.], pk. 4000f.	5 19	121 55	Tanj. Soloka, E pt. of Java ...		8 46.7	114 31.5
	Mengkoka B. Tahoa	4 3	121 40	South pt. of Java, Ba nenan ...			
	Herayu	2 40	120 42	Nusa Barung I., EW 9m., }		8 27.5	113 25.2
	Palapa B.	2 55	120 13	l., ♀, Kamal Pt.		8 6.5	112 55.2
	C. Djeneo	3 18	120 29	Semiru, Mr., 12,140f.		7 45.7	112 35.5
	C. Patiro	4 38	120 27	Arjund. Mt., 10,320f.		8 27	112 42.5
	Boni, city, 5m. inland	4 32	120 18.5	Sempo I., EW 5m., S pt.		8 22	111 43.5
	Salangketa Pt.	4 50	120 22	Segoro Wedi B., Klappa I. ...		8 24	111 42.5
Java S. Coast	Boni rk.	5 15	120 32	Skul rk.		8 15	111 5
	C. Laras, or Biera	5 35	120 28	Pa-hitan B., E pt., entr.		7 46.6	109 2
	Saroniang	5 39	120 30	Kembangan I., ♀ 14m., in- let of Tylatiap, lt. R 653f.		7 44	107 50
	Salayur I., ♀ 13 l., N pt.	5 45	120 29	C. Sanchang		7 23	106 24
	Whale rf., s.	6 7	120 19	C. Genteng		7 11	106 24
	Bulekombo, ww., fl. st.	5 31.5	120 12	Zand Bay, ♀ 12, Panchur Pt. Po. Tinjil, or Trouwers I., }		6 58.3	105 46.2
	Mansfield sh., 4, Bolloh	5 45	120 12	♀ 4m., W pt.		7 0	105 33
	Mt. Lambo Batang	5 21	119 56	Kelapa, or Breakers I., EW 3m., rka. W pt.		6 49	105 16
	C. Bulu Bulu	5 42	119 45	C. Sangian Sira, (rka. SE), T., 1575f. sum.		6 45.3	105 12.7
	Java.			Java Hd., First pt., lt. Fl. 260f.			
	Button, Toppers I.	5 54.2	105 55.8				
	Pulo Babi, EW 3m., W pt. ...	5 48.7	106 15				
	Bantam, fl. st.	6 1.7	106 8.7				
	Mt. Karang, 5833f.	6 14.5	106 0.7				
	Pontang Pt.	5 56.3	106 16				

MARITIME POSITIONS

(91)	Places	Lat. S	Lon. E	(92)	Places	Lat. S	Lon. E	
Java Sea to Flores Sea	Java Sea to Flores Sea.				Token Besi Is., Kaka Rf., South rk.	6° 7'	124° 16'	
	Woerden Castle, rk., or Panamanukan, (shl. s. ½ 3 in.)	6° 1'5"	107° 52'5"		— N limit, Wangy Wangy, vis. 7 l., sum.	5 18	123 35	
	Pulo Rackit, Boompjes, [½ m.], lt. R 91f.	5 56	108 22'5"		— St. Matthew's Is., ¼ 5 l., l. SE pt.	5 27	124 21	
	Karimun, Java Is., EW 13 l., ¼, b, W extr., or Katang rk.	5 48'3"	110 8		Veldthoen I., [5m.], l, ¼, Moro Maho, centre.	6 7	124 37	
	— Karimun I., ¼ 5m., SW pt., fl. st.	5 53'5"	110 26'2"		Bali to Flores.			
	Hastings rk., s.	6 5'5"	112 30	Bali	Bali, ¼ 33 l., ¼, Mt. Agung, 10,500f.	8 21	115 31	
	Bavean I., ¼ 12m., 2000f., w. r., N pt., Mantegi ...	5 43	112 41			Budung B., Bukit pt.	8 49	115 5
	— Sankapura Bay.	5 51'5"	112 39			Beliling, lt. F 58f.	8 6	115 5
	Arrogant rk., [½ m.], T.	5 12	112 57			C. Pasir.	8 6'5"	114 25'5"
	Grt. Solombo, ¼ 6m., ¼, flat hill, 620f.	5 33	114 27		Lombok	Lombok, ¼ 23 l., Mt. Rin-juni, 11,810f.	8 25'	116 27
	Little Solombo, [3m.], l, ¼ 118f.	5 27	114 26			— Labuan-Tering B.	8 44	116 3
	Arends, [3m.], N end.	5 2	114 33'5"			— Pandaman pt. (C. Banko)	8 44	115 49
	Karang Takat grp., ¼ 4 l., rks., W pt.	7 0	114 55	Sumbawa		Sumbawa, EW 51 l., SW pt., Tafelberg.	9 0'5"	116 44
	Kangeang, ¼ 9 l., Ketapang B. Pandjag., EW 3 l., E pt., (rks. off)	6 50	115 17				— Sumbawa, town.	8 28
	Urk, [2m.], l, ¼, Id.	7 4'6"	115 11'5"			Flat l., Malang [1 l.], E end	8 8	117 25
	P. Maurits' rf.	6 19	115 29			Gulf of Saleh, Rakit l., pk. ...	8 38	117 58
	Belliqueux rf. 4).	6 31	116 0			Setonda l., W pk.	8 6	117 44
	Turkey, Polo or Anak Kangeang Is., and shls., N l., Ara han.	6 31	115 44		Mt. Tambora, 9070f., volcano	8 14	117 58	
	Sakala or Hastings l., l.	6 57	116 15		Joro Batu Pt.	8 14	118 29	
	Paternoster Is., Pulo Ter-gah, NW, Paposa, (rks. 2 l.)	7 30	117 10'5"		Bima Bay, E. fort.	8 27	118 43	
	NE Paternoster Bankawang	6 38	118 21		Sangeang l., 6180f., pk.	8 11	119 4'5"	
	Postilion Is., ¼ 12 l., l, ¼, T, N island, Jailamu...	6 33	118 47		Sapoh Pt.	8 45	119 8	
	— E. l., Puman Tawan.	6 50	119 11		Gili Banta l., [2 l.], T, pk. ...	8 25	119 16	
	— Lamarus l., small.	7 18'5"	118 6		L. euwenkop pt. ...	8 51	118 51	
	Drill shl., Taka Renataya, [4m.], T, ¼, lt. F, Fl. 68f. }	6 7	118 57'5"		Komodo, or Mangarei, NS }	8 45	119 22	
				7 l., ¼, ¼, Schoor-teen ... }				
				Flores, Timor, and Sumba Islands.				
				Flores, EW 67 l., Alligator B.	8 48	119 50		
				Terang and Bari Bays, Bari...	8 20	120 11		
				Potta Rd., Potta.	8 18	120 42		
				Giliting.	8 35	122 16		
				Tower l., EW 1 l., 1200f.	8 53	120 14		
				Ende B., ¼, Aloso Pt.	8 52	121 39		
				Lobetobie, volcano, 7120f.	8 35	122 48		
				Flores Head, or Iron Cape ...	8 3	122 47		
				Larantuka Road.	8 18	123 1		
				Kambing, S entr. Flores Str.	8 39	122 51		
				Adonara, ¼ 12 l., town.	8 14	123 9		
				Solor, ¼ 9 l., S pt., islets off.	8 36	122 52		
				Komba l., vol., 1800f.	7 47	123 31		
				Lomblen, ¼ 12 l., E pt.	8 14	123 54		
				— Mt. Lannarap, 5880f.	8 31	123 25		
				Pantar, ¼ Babi l., off SW pt.	8 25	123 52		
				— North East pt.	8 10	124 14		
				Onbay, EW 17 l., Dalolo.	8 12	124 23		
				— Ea t pt., Leisumbu.	8 18	125 10		
				Timor, ¼ 85 l., SW or Oy-}	10 23	123 29		
				sina Pt.				
				Koepang, ft. Concordia, lt. F 47f	10 9'9"	123 35		
				Weig: Pt.	9 33	123 40		
				Sutranha, ¼ 18.	9 20	124 5		
				Gula l., small.	9 14	124 0		
				Lifou, r, w.	9 10	124 25		
				Atapapa, lt.	8 59	124 50		
Java Sea to Flores Sea								
Java Sea to Flores Sea								
					</			

MARITIME POSITIONS

(93) Places		Lat. S	Lon. E	(94) Places		Lat. S	Lon. E
Timor	Dilhi, town, r, Custom ho., lt. F	8°33'	125°36'2	Ki I.	Grt. Ki I., 15 l., 1, 1, 1	5°17'	133° 9'
	E pt., 1/2 1/2, Po. Jackie, or 1	8 26	127 20		3000f., C. Borang	5 42	132 57
	Nusa Besie, sum. 350f.	9 6	126 12		— Nuja	6 3	132 53
	Kalaeko, town	10 5	124 18		— Madua Pt.	5 28	132 42
	Noy Mini B., 1/2	10 22	123 25		Little Ki I., Rumadan I.	5 34.7	132 45.7
	Semao, 1/2 5 l., 8 pt.	10 52	123 5		— Ki Doulan, vill., T, w, r, 1	5 40	131 58
	Botti, 1/2 14 l., via 12 l., Cy- } rus B. on SE side, w, r }	10 58	122 55		b, (1/2 3m. N), pi r ...	5 25	132 0
	— Pulo D-na, off S pt.	10 48	122 41		Nusa Tello I., Fadd I.	4 46	131 52
	Pulo Dau, 1/2 4m., 1, 1, N end	10 34	121 41		— Koor I., 8 pt.	4 47	131 44
	Saru, EW 7 l., W C. Mesara...	10 27	122 0	Banda Is.	Matabella Is., 2 groups, 1, 1	4 31	131 38
Sumba	— East pt., l., (rks. off)	10 37	121 31		grt., Kasiwoi, S pt.	4 9	131 23
	Banjoan, EW 7m., SW pt., l	10 49	121 16		Manovolko I., Sera	4 1	131 14
	Dana, or New I., [1 l.] }	9 42	119 0		Suruaki-Wisaleat	3 59	131 26
	8 part, 120f.	9 25	119 45		Goram I., [3 l.], NE pt.	4 33	129 38
	Sumba or Sandalwood I., 1/2 }	9 37	120 12		Banda Is., 5, W, or Po. }	4 18	129 40
	24 l., C. Lambuya, (rks.) }	10 12	120 51		Rhan	4 32	129 53
	Palmedo Road	10 23	120 29.7		— NW one, or Swanji	4 36	130 2
	Paddaway B., 1/2, [5m] 1/2, }				— Banda, 1/2 6m., Fort Nassau		
	r, 1/2, Arif town anchg. }				— East one, Ruzengain		
	E point, C. Mandayeli			Boro	Bouro I., 1/2 27 l., Palpatu }	3 6	126 1
Banda Sea.					Pt., T	3 15	126 2
Sawutty Is.	Cambing, or Passage I., 1/2 }	8 18	125 35		— Mt. Tumahu, 8530f.	3 22.8	127 6.5
	4 l., A. S pk., 3273f.	8 2	125 45		Cajeli B., r, w', b, Fort }	3 21	127 16
	Bali I., sum.	7 53	126 24		Defence	3 54	126 37
	Wetta, 1/2 19 l., San town, }	6 39	126 36		East point, or Pt. l'ela	3 52	127 17
	on SE side, 1/2	5 28	127 29		South pt., or Baton P kka ...	3 20.5	127 40
	Gunong Api, volc., 1378f.	8 6.7	127 8.5		Amblaw I., [2 l.], NE pt. ...	3 12	127 38
	Lucipara, 5 Is., N Id.	7 42	127 20		Manipa I., A, (rk. 1 1/2m. W), }	3 1	127 51
	Kissa I., 803f., Pura landing	8 10.2	127 40.5		R pt., Lubu		
	Roma, [3 l.], A, Uwakekee ...			Ceram	Kelang, A, 1 W, W pt.	3 33	127 55
	Letti I., Serwaru, Church ...				Bano, A, 1, SW pt.	2 57	129 12
Timor Is.	Moa, 1/2 6 l., 1/2 K, Buffalo }	8 14	128 13		Ceram, 1/2 59 l., Pt. Secal	2 48	129 29
	Pk., 4100f.	8 11	128 48		— Sawaa Harb.	2 52	129 42
	Lakor, [3 l.], l, E end	8 11	128 39		Wahaay Harb., vill., w''' , }	3 0	130 24
	Luang, [1 l.], A, 1'	7 9	128 40		r, b, fort	2 55	130 35
	Seratan, [5 l.], W pt., Eto O	7 2	129 7		Pasahai Pt.	3 22	130 35
	Damma Is., NS 5l., 8117f. }	6 52	129 28		Lama Pt.	3 21	130 48
	Kulewate Harbour	6 17	130 0		Leuwarden sh., [2m.], T, rka	3 37	130 59
	Tau, [3 l.], 2030f., 1/2 Lajani O	5 33	130 18		Waru B., 1/2, w, r, Baru ...	3 51	130 47
	Nila, [3 l.], 3898f. sum.	7 50	129 33		Po. Parang, or Leuwarden I., }	3 3	130 52
	Seru, 2 Is., [3 l.], W. I.	8 11	129 51.5		8 pt.	3 57	131 12
Aru Is.	Bird I., or Po. Mano, 880f. ...			Sula Is.	Po. Madurang, small	1 54	123 45
	Wetan, 1/2 E, 160f.				Great Keffing I., E pt.	1 52	124 1
	Baba, w, P., 8 pt. 3000f.				Ceram Laut, Gesser I.	1 57	124 27
	Masella, 8 pt. 839f.				— Kon	1 50	126 25
	Tenimber Is., 1/2; Timor Laut, }				Amboina I., 1/2 11 l., SW, }	1 58	125 30
	1/2 34 l., S end, Jernata }				or Alang Pt., T	2 24	126 6
	Selaru, Woody I., small				Amboina City, Port Victoria...		
	Oillett, village, 413f.				Noessaniva Pt., T ...		
	Larat, 1/2 6 l., Lamdesar				Haruku I., 1/2 8m., SW pt. }		
	Vordate, 1/2 2 l., 1/2, Sobiani...				Islet		
Aru Is.	Sera I., Aha			Sula Is.	Saparua I., 1/2 11m., fort		
	Mulu I., Nuskalbur				Nusa Laut, 1/2 7m., Nalabia B.		
	Arru Is., NS 35 l., 1/2, 1/2, r }				Bowakan		
	P, S extr., Enau I., 100f. }				Hammond's I., [3 l.], S pt. ...		
	— SW limit, Bayn				Taliabu, EW 18 l., Lekitobi...		
	— Po. Babi, small				Mangola, 16 l., EW 1/2 Lisa- }		
	— NW extr., Wassir				matula I., 1164f.		
	— C. Watale Juhong				Vesuvius B., 1/2		
	— Dobbo Harb., 1/2 pt.				Sula Besi, NS 10 l., S and }		
	Tjando Is., N lim.				E pt., Ipa		

TABLE 10

MARITIME POSITIONS

(95)	Places	Lat.	Lon. E	(96)	Places	Lat.	Lon. E
Pitt Passage	Oby Latta, [2 l.], S pt., 2400f.	South 1° 29'	127° 16'	Is. to N.W. and N. of Gilolo	Tifori, sum. 587f.	N. rth 1° 0'	126° 8'
	Gomomo, 850f., W pt.	1 52	127 33		Mayo, N pt. 1280f.	1 21	126 21 7
	Po. Gasé, [5m.], T, rka. SE, } 8 pt.	1 39	128 22		Biarro, sum.	2 7	125 25
	Tapa l., NW pt.	1 12	127 17		Roang, vol., 2330f.	2 18	125 22
	Bisa, E pt.	1 16	127 37		Siao, pk., 5924f.	2 44	125 23
	Obv Major, 4, 19 l., SE pt., Wai	1 44	128 0		Mskalébé l., 394f.	2 42	125 12
	Lookisong l., 4, 3 l., N pt.	1 32	128 8		Nennung Is., South I○	3 2	125 41
	Kekik l., 4	1 30	128 37		Kalama, [North l., N extr. ...	3 15	125 27
	Lawin l., 4	1 29	128 42		Sangir, 4, 8 l., Taruna B., } w, r	3 33	125 28
	Po. Pisang, via. 11 l.	1 24	128 53		— North pt., Salima	3 45	125 27
	Grosvenor shl., [4m.], sf	1 19	129 26		Louisa shl.	4 0	125 18
	Bu Is., 4, P. Esplee○	1 10	129 25		Haycock Is., Kabalusa	4 15	125 19
	Grand Canary, w, E pt., } NW pt.	1 45	129 37		— Meares, South pt.	4 39	125 26
	Mysole, EW 14 l., Lungu.....	1 53	129 42		Anda l.	4 34	125 38
	Hasil l., S pt.	1 11	128 28		Ariaga l.	4 44	126 28 5
Gilolo.				Charruca shl.	4 45	125 38	
Gilolo Passage	Gilolo, 4, 67 l., SE, or Co- } conut Pt.	0 56	128 27	Iphigenia rka., South rk.	4 15	125 45 5	
	Weda Is., [3 l.], E lim.○	0 40	128 39	Nanusa Is., Merampi Pk., } 666f.	4 46	127 7	
	Iyoi, [5m.], S pt.	0 3	129 34	Talauer Is., NS 15 l., N pt., } Mamaga	4 34	126 48	
	Gelv. 4, 7 l., Port Fou, ou } SW side, 4, w, r	0 6	129 21	— Nusa l.	4 18	126 43	
	— North-West pt.	0 2	129 15	— Salitabu l., 4, 5 l., S } pt.	3 48 5	126 42	
	Shampee Is., 3 or 4, NS 3 l. ...	0 30	128 43	— Kaburuan, 4, 3 l., S } pt.	3 45	126 49	
	Canton Packet shl., sf.	0 35	128 55	Northumberland shl., [3m.] ...	3 39 5	126 51	
	Catherine Is., 3, l.	0 41	129 5	Eye l., [4m.]	0 22	129 56	
	Ardassier Islet	0 45	129 0	Syang, [3m.], l, w, SW } pt. l.	0 18	129 55	
	Aurora bk., sf.	0 43	129 23	Wyang, or Vayag Is., 4, } 6 l., NW extr., Laborde } Islet	0 13	130 3	
	Weda, 4	0 18	127 52	— SE extr., Labishe l., } [1m.], (rka. SE)	0 5	130 15	
	Dilegisa Pt.	0 15	128 31	E-n, or Ine Is., EW 4m., } E pt.	0 8	130 19	
	Po. Moar, 4, l, 4	0 7	128 55	Ormsby shl., T N, N pt. ...	0 44	130 2	
	Wossa, village, w, r, b	0 35 5	128 34	Budd l., l, 4○	0 27	130 51	
	Pt. Monat	1 1	128 28	Aiu Is., about 20 small, l, } 4, rfa. T, Wirisoi	0 41	131 9	
Pt. Waigamele, (rka. 1 l.) ...	1 9	128 38	Aiu Baba, [3m.]	0 21	131 7		
Pt. Salaway, (rka. 1 l.)	1 33	128 43	Asia Is., 3, l, SW and small- } est	1 0	131 15		
Watering-place, N of Galela } Tiabu	1 51	127 52	Po Manuaran, [2m.], l S, } w	0 2	130 57		
Gilolo, E. Coast	Bisoa Pt.○	2 13	127 55	South			
	Rau, [2 l.], mid.	2 23	128 11	Buccleuch shl., [3m.], 4, 4, ...	0 16	131 30	
	Morty, 4, 21 l., N pt., (rf.), }	2 44	128 20	Waigiu, EW 22 l., SE pt., }	0 21	131 12 0	
	T	1 57	128 13	or Pt. Pigot	0		
	— South-West pt., Lints l. ...	2 19	127 44	— Boni l., [3m.], 4 SW-d., }	0 17	131 8	
	Toekara, N pt.	1 6	127 22	N pt.	0		
	Talabu Pt.	1 7	127 27	— Offak Harbour, 4, w, l }	0 18	130 43	
	Dyilolo, town	0 48 0	127 21	entr.	0 5	130 12	
	Ternate, 4, 6m., sum. 5180f., }	0 40	127 25	— NW pt., C. Forrest	0 1	130 24	
	Fort Orange, on E side... }	0 33	127 22	Buttons, [1m.]	0 2	130 9	
	Tidore, [2 l.], sum. 5900f.	0 27	127 24	Ruib, NS 6m., pk.	0 2	130 4	
	Potubakker l., [2m.], 1160f. ...	0 12	126 53	Gag l., [7m.], N pt.	0 20	129 55	
	Metir, [3 l.], sum. 2800f.	0 20	127 23	Pigeon l., 4, ~, W pt.	0 39 7	130 34 7	
	Wolf Pk.	0 17	126 59	Batantia, EW 15 l., W pt. }	0 54	130 25	
	Makyan, [5 m.], sum. 4166f. ...	0 29	127 3	C. Mabo	0 49 5	130 54 7	
Is. on West Coast of Gilolo	Larta-Latta Is., Japi	0 54	127 34	— Marchesa Bay, Toe Pt. ...	0 58	130 38	
	Grt. Tawally, 4, 7 l., SW } pt. Id.	0 44	127 25	Salawatti, 10 l., Dady Pt.			

MARITIME POSITIONS

(97)	Places	Lat. S	Lon. E	(98)	Places	Lat. S	Lon. E
NEW GUINEA.							
New Guinea, S. & W. Coast	Brebes Pt., or C. Wilson ...○	0° 40'	131° 57'	New Guinea, North Coast and Outlying Islands	Ouessant I., small	11° 8' 6"	151° 15' 5"
	Threshold Pt.○	0 47	131 27		Teste I., (Wari), East I.	10 58	151 5 2
	C. Spencer, or Foul Pt., (rfs. 2m.).....}	0 52	131 15		Moresby I., Fairfax Pk., 1740f.	10 36 8	151 0 5
	Selé Pt.	1 27	130 57		CHINA ST., SAMARI I. MISSION	10 36 8	150 39 7
	W. Brother, or Pinkin I.	1 47	131 6		Lydia I., (Nuakata), pk., 1010f.	10 16	151 0 5
	Sabra Pt.	2 2	131 57		Possession B.	10 34 6	150 42 2
	Pisangs Is., Po. Sabuda. SW pt.....}	2 39 5	131 38		East Cape, Anchor I., E pt....	10 13 2	100 53 7
	Mac Cluer's Inlet, Head, or E lim. of the bay	2 10	133 46		D'Entrecasteaux Is., S pt., C. Ventenat, (Is. S-d.) ...	10 10 7	151 13 5
	Tatingar Pt.	2 48	132 1		Welle I., [2 l.], E part, (rfs.)	9 37	151 3
	C. Sapey, (sum. 3020f.), W pt. (Balk)	3 41	132 42		Goodenough I., pk., 7000f. ...	9 21 5	150 14
	C. Kaffura	4 7	132 55		C. Vogel, Glen I.	9 45	150 4
	Po. Adi, or Wessels, $\frac{1}{2}$ 8 l., W pt. $\frac{1}{2}$	4 9	133 20 5		C. Nelson	8 59	149 20
	Bird I., [3m.] (Vogel)	4 21	133 36		L. Riche, Mitre rk.	7 59	148 9 5
	Lamansiere Hill, NW sum. 2460f.}	3 44	134 7		Pocklington shl., EW 10 l., rks., 8 E rk.}	10 45 4	155 51 7
	Triton B., Fort Dabus	3 47	134 7		Laughlan Is., 9, EW 5m., 4 $\frac{1}{2}$ f, low E rk.}	9 19	153 40
	Lakabia Mt., 4564f.	4 10	134 45		Cannac rk., $\frac{1}{2}$ f, high	9 18	153 28
	Charles Louis Mts., 9510f. ...	4 9	136 15		Woodlark Is., $\frac{1}{2}$ 13 l., P', North point	9 3 5	152 47
	C. Baru, via 10 l.	4 12	134 45		— West Rock	9 16	152 13
	Viakke Pt.	4 27	135 10		Yanaba, Sharp I.○	9 29	152 40
	Wamuka R., mouth	4 40	136 15		Jouvenoy I., [2m.]	8 45	151 45
	C. Steenboom.....	4 50	136 29		Jurien I., [1 l.], mid.	8 39	151 22
	Snowy Mountains, sum. 14,000f.}	4 13	137 7		Lagrandière I., [2 l.], E pt. ...	8 52	151 8
	Dounga Strait, E pt.	7 22	138 34		Trobriand Is., C. Denis	8 24	151 4
	C. Valsche, (W pt. of Frde- rick Henry I., $\frac{1}{2}$ 36 l.) ...}	8 22	137 40		Lusauya Is., & rfs., EW, & others W-d, unexplored, NE ext., North I.}	8 23	150 48
	New Guinea, S. Coast	St. Bartholomew I.	8 17		139 28	C. Cretin, Cretin Is.	6 43
Deliverance I., small, rfs. ...○		9 35	141 47	C. King William	6 2	147 37	
Mt. Cornwallis, vis. 9 l.		9 25	142 31	Mount Disraeli, 11,000f.....	5 58	146 29	
Bristow I., [5m.], 4 $\frac{1}{2}$ SE pt.}		9 9	143 14	C. Rigny	5 29	145 58	
Fly River, Tree I.		8 41	143 36	Rich I., [1 l.], A.....	4 49	146 13	
Aird Hill, 1260f.		7 28	144 20	Dampier I., $\frac{1}{2}$ 5 l., ab 5000f.	4 40	145 58	
Blackwood, Pt., 4 $\frac{1}{2}$ f		7 52	144 28	Vulcan I., [2 l.], conical, 4000f.	4 5	145 2	
Mt. Yule, 10,046f.		8 14 5	146 46	C. della Torre	3 51	144 31	
C. Possession		8 36	146 22	Lesson I., [2m.], A, conical ...	3 33	144 48	
Port Moresby, Jane I.		9 25 5	147 7	Blosseville I., [1m.], 1100f. ...	3 36	144 34	
C. Hood		10 7	147 42	Garnot I., [3m.], conical	3 30	144 35	
C. Rodney, SE pt.		10 12	148 22	Jacquinot I., [3m.], $\frac{1}{2}$ f	3 24	144 24	
Dufaure I., [1 l.], sum.		10 29	149 48	Deblois I., [$\frac{1}{2}$ l.]	3 21	144 9	
South Cape, Suau		10 43 5	150 14 2	Roi-sy I., [1 l.], $\frac{1}{2}$ f, N pt....	3 12	144 3	
Louisiade Islands.		Adale I., [2c.], 4 [$\frac{1}{2}$ f.], W ...	11 29	154 26 5	Victoria Bay, D'Urville I.	3 16 4	143 29
	Rossel I., EW 7 l., 4 $\frac{1}{2}$ f, lo	11 23 3	154 17 7	D'Urville I., [3 l.], pk. near W end	3 17	143 30	
	W. C. Deliverance	11 30 6	153 26	Gilbert I., [4m.], 4 E pt., (rf.)	3 13	143 17	
	Sudest I., Mt. Rim 2645f. ...	10 54	152 58	Bertrand I., 1 $\frac{1}{2}$ W, $\frac{1}{2}$ f	3 10	143 10	
	Fox, or Renard Is. ? [4 l.], W pt.}	10 41	152 55	Torricelli Mountns, W sum. }	3 21	142 12	
	St. Aignan I., EW 10 l., E pt., C. Henry	10 40 5	152 23	4 l. inland			
	Deboyne Is., [2 l. f.], N pt. ...	10 40 5	152 6	Eyries Mt., very A, W sum. }	2 50	141 15	
	Bonvouloir Is., E extr.	10 25	152 3	3 l. inland	2 40	140 51	
	Laeine Is., [2 l.], Dawson I.}	10 23	151 25 5	Humboldt B., Obsn. I.	2 36	140 42 3	
				Cyclops Mt., vis. 20 l., E sum.	2 31	140 30	

MARITIME POSITIONS

(99) Places		Lat. S	Lon. E	(100) Places		Lat. S	Lon. E
New Guinea, Gerdoin Bay	C. D'Urville, 4° , (riv. W-d. ?)	1° 24'	137° 47'	North Coast	Crocodile Is., North I.	11° 41'	135° 9'
	Kurudu I., E pt.	1 48	137 2		C. Stewart, rky.	11 57	134 46
	Jappen I., Ansum Harbour ...	1 44	135 49		Liverpool R., Haul-round I. ...	11 54	134 45
	Nau I.	2 19	136 19		Pt. Cuthbert, (shls. 3 l. out.)	11 43 5	133 51
	Terschelling Is., E pt.	2 55	135 54		Goulburn Is., North I., $\frac{1}{2}$ l.	11 28	133 30
	Haerlem Is., [4 l.], W one ...	3 5	135 52		7m., N pt.		
	Pt. Pinxter, W pt.	3 24	135 46		Pt. Brodgen, rky.	11 31	133 6 5
	Hoog, South pt.	2 51 5	135 5		De Courcy Hd.	11 21	132 57
	Angermus I., E pt.	2 38	135 3		Mac Cluer I., $\frac{1}{2}$ 2m., N pt. ...	11 4	133 1
	Meosani I.	1 57	134 8		New Year I., small, w.	10 55	133 45
	Job I.	2 33	134 24		Money sh., [5m.], t.	10 21 5	132 45 7
	C. Oran Swari	1 22	134 17		Crocker I., NS 7 l., N pt., } C. Croker, (rks NW-d.) }	10 58	132 37
	Mefur I., 164f.	1 15	134 53		Orontes rf., [1m.], t.	11 4	132 6
	Mysory Is., $\frac{1}{2}$ 20 l., A, E pt.	1 10	136 45		Pt. Smith, [rks. 1m.], t.	11 8	133 9
	— Mt. Schooten, Kaiori, 1640f.	0 47	135 37		Port Essington, Gov. Hd.	11 22	132 9 2
	— W pt., C. Saavedra	0 38	135 19		Vashon Hd., (shl. 2m.), N } pt.	11 7	132 0
	Mioskaroar I.	0 18	135 3		C. Don, 130f.	11 18	131 46
	Arfak Mountains, 9157f.	1 11	133 59	Melville I., Van Diemen Gulf	Burford I., [1m.], t.	11 31	131 56
	Port Dorel, Manawari I.	0 54	134 7		Greenhill I., NS 5m., Webb } Pt., (rf. off)	11 39	132 47
	C. Mamori	0 48	134 8		Field I., [4m.], t. (off mo.) } of S. Alligator R.), W pt. }	12 5	132 21
	C. Maiami	0 29	133 12		C. Hotham, shl. NE-d.	12 3	131 18
	C. Good Hope	0 19	132 21		Vernon Is., [3 l.], S side of } Clarence Strt., W pt.	12 3	131 0
	Mt. Diceras, 8m. inland	0 32	132 17		Melville I., $\frac{1}{2}$ 25 l., E pt.	11 28	131 34
	Misapu Is., Amsterdam I. ...	0 19	132 9 0		— Pt. Jahleel	11 9	131 18 4
					— N and W pt., C. Van De } men, l. sandy, (shl. 5m.) }	11 8	130 20
					Bathurst I., Brace Pt.	11 18	130 16
					— C. Helvetius	11 41	129 58
					— S extr., C. Fourcroy	11 51	129 57
Gulf of Carpentaria	AUSTRALIA, North Coast.			North-West Coast	North-West Coast.		
	Duythen Pt.	12 34	141 41		PORT DARWIN, PALMERS } TON, E extr. of Cable H. } Port Paterson, E. Raft Pt., } on E side } Paterson's B., Quail I., w" } Pt. Blaze, } Peron Is., $\frac{1}{2}$ 5 l., N pk. } C. Ford, (rks. 2m.) } Port Keats, E. Tree Pt. } C. Hay, (shls. $\frac{1}{2}$ 5 l.) } Pt. Pearce, 85f., (a rf. off) } Cambridge G., Laerosse I., } $\frac{1}{2}$ 4m., W pt., 600f. } — Wyndham } C. Dussejour, (rk. off), sum } over } Mt. Casuarina, 800f. } Lesueur I., (and rks. 1 l.) } C. Londonderry, (Stewart } Is., 20f., and rks. 3m.) }	12 28 4	130 50 5
	Pera Hd., l. 1	12 59	141 40			12 37	130 33 7
	C. Kwerwer	13 58	141 34			12 31	130 26 7
	Van Diemen's Inlet, w. entr.	16 58	141 1			12 51	130 11
	Norman R., Kimberly Tel. Stn.	17 26 6	140 56			13 9	130 2
	Albert R., Kangaroo Pt.	17 35 1	139 49 5			13 28	129 55
	Wellely Is., N extr., rocky islet	16 18	139 26			14 1 5	129 38
	— Pisonia I., small	16 29	139 56			14 3	129 32 2
	— E extr., Bountiful Is., 2, } $\frac{1}{2}$ 3m., E pt.	16 39	139 59			14 26	129 21 5
	— Sweers I., $\frac{1}{2}$ 5m., $\frac{1}{2}$ w, } f, b, S pt., Inspection } Hill, 105f.	17 8 2	139 41			14 43	128 17
	Sir Ed. Pellew's Is., $\frac{1}{2}$ 12 l., } N extr., a rk.	15 29	137 4			15 28	128 3 2
	— Vanderlin I., $\frac{1}{2}$ 6 l., N } pt., or C. Vanderlin ...	15 34	137 8			14 42	128 13
	— West I., NE pt.	15 32	136 46			14 23	127 39
	Maria I., $\frac{1}{2}$ 7m., N pt.	14 50	135 54			13 48	127 15 5
	Groote Eylandt, NS 12 l., } SE pt., (an I. S 5m.) ...	14 16	136 58			13 42	126 54 7
	— Central Hill, vis. 10 l.	13 57	136 41			13 46	126 45 2
	North-East Is., [7m.], E extr.	13 39	137 1			13 43 2	126 25
	Bickerton I., [4 l.], sum.	13 45	136 15			13 52	126 11
	Woodah I., $\frac{1}{2}$ 4 l., S pt.	13 34	136 13			13 44	126 13 5
	Nicols I., [3m.], t.	13 27	136 19			13 32	125 48
	C. Shield	13 20	136 23			13 55	125 44
	C. Grey	13 0	136 42				
	Mt. Caledon	12 53	136 33				
	Mt. Alexander	12 39	136 44				
	C. Arnhem	12 16 5	137 0				
	Bumby Is., NE pt.	11 46 5	136 42				
	C. Wilberforce	11 53	136 35				
	Truant I., small	11 39	136 48				
	Wessel's Is., C. Wessel, 180f.	10 59	136 45				
	Arnhem B., entr., Malli- } son's I., W pt.	12 11	136 6				
	Brown's Strait, Pt. Dale	11 36	136 5				

MARITIME POSITIONS

(101)	Places	Lat. S	Lon. E	(102)	Places	Lat. S	Lon. E
North-West Coast	Admiralty Gulf, Port Warrender, Crystal Hd.	14° 28'	125° 58'	AUSTRALIA, North-West Coast	C. Borda	16° 40'	122° 43'
	C. Voltaire, flat hill, (1½ m. inland)	14 13	125 41.5		Beagle B., N Hd.	16 50	122 32
	Condillae I., small	14 6	125 38		Laopede Is., W one, [and rks. 3 l.], 15f., sand	16 50	122 8
	Montalivet Is., W extr. shl.	14 14	125 6		C. Beakerville	17 9	122 16.5
	Maret Is., (rfs. W 2 l.), N pt.	14 23	124 57		Pt. Coulomb, rf. 1m.	17 21	122 10
	Lamarck I.	14 45	125 2		C. Boileau, sandy	17 38	122 10
	C. Pond, islet off	14 45	125 9		Pt. Ganthiesume	17 58	122 11
	Pt. Hardy	14 58	125 2		C. Villaret, 150f.	18 19	122 4.5
	Port Nelson, E., Careening B. beach	15 6	125 1		C. Latouche Treville, 250f.	18 28	121 51.5
	Prince Regent's R., Mt. Trafalgar, sum.	15 16	125 4		C. Bossut, Casurina rf.	18 43	121 37
	Port George IV., 3', v', b. rfs., Augustus I., Adieu Pt.	15 13.5	124 34		C. Jaubert, 45f.	18 58	121 36.5
	Colbert I.	14 51	124 42		Mt. Blaise, 60f.	19 59.5	119 3.5
	Freycinet grp., W island	15 0	124 32		Amphinome shls., outer S.	19 43	119 19
	White rock islet	15 4	124 19		Bedut L., 20f., rf. SW, } [½ m.]	19 35	119 6
Buccoener Archipelago	Red I.	15 13	124 13.3	Turtle I., 35f., [½ m.], rf. F ...	19 54	118 55	
	Champagny Is., 3' 7m., } Degers do. sum.	15 19	124 10	Port Headland, Hunt Pt.	20 18.2	118 35.7	
	Adele I., [rfs 4m.], 8f., 0.	15 32	123 14	C. Thonia, rf. N.	20 20.5	118 13	
	Beagle bk., [S 5m.], 15f.	15 19	123 30		Géographie shls., 2. NW one, } [½ m.]	20 16	117 55.5
	Pt. Hall, sum.	15 40	124 21		Depuch I., w.w., 514f.	20 38.4	117 44.5
	Doubtful B., Raft Pt., w.	16 3.5	124 26		Port Walcott, (Tien Twin Hr.), Cosack, lt. F 97f. on Jarman I.	20 39.1	117 13.2
	Cockell's Is., [2 l.], W pt.	15 46	124 4		Port Robinson, Dixon I.	20 38	117 3.2
	Mac Leay Is., N extr. reef.	15 54	123 39		Legendre I., 55f., 4 8m., } NW pt.	20 21	116 51
	Caffarelli I., 3' 2½ m., mid.	16 3	123 18		Dampier's Archipelago, 3' 10 l., Rosemary I., [3m.], } W sum. 250f.	20 29	116 36
	Brue rk.	15 57	123 4		Hampton Hr., Channel I.	20 39.8	116 42
	Hidden I., W pt.	16 14	123 27		C. Preston	20 50	116 12.5
	High I., [3m.], 290f.	20 20	123 20		Montebello Is., NS 4 l., lo. } Ritchie rf.	20 18	115 23
	Port Osborne, [½ m.], v. w.	16 39	123 30		— Tremouille Is., 0. w. b. } 11 g islet, 21f.	20 28	115 35
	King's Sound, Pt. Torment ...	17 0	123 35		— Tryal rks., NS 4m., N extr.	20 35	115 27
— Derby	17 20	123 39	Barrow I., 3' 4 l., F, (rf 16m. from S end), C. Dupuy		20 40	115 27	
— Fitzroy R. mo., Escape Pt.	17 24.4	123 34	Fortescue R., mouth		20 59.8	116 6	
— Pt. Cunningham, NW art.	16 41.5	123 7	Rusily I., 21f.	21 18.5	114 59.5		
Skeleton Pt., w'	16 31	123 0	Ashburton R., (Onslow), } mouth	21 40.7	114 56.2		
Swan Pt., v'	16 21	123 1.7	N Muiron I., pk. 70f.	21 37	114 23		
C. Leveque, 83f., (an islet off)	16 22	122 55.5	NW Cape	21 46.5	114 10		
Islands and Shoals N.W. of Australia	Rowley shls., Impérieuse shl. NS 3 l., N. Sandy I., 8f.	17 32	118 51	West Coast.			
	— Clarke's rf., or Minstrel shl., N Sandy I., 8f. ...	17 16	119 21	Exmouth Gulf, B. of Rest. } N pt.	22 15	114 7.2	
	— Mermaid shl., [3 l.], passage on E side	17 5	119 38		Pt. Cloates	22 43	113 41
	Scott Is., a lagoon, NS 6 l., } T W, I. sand and cri., } Sandy I., 8f.	14 3	121 49		C. Farquhar, sand, l.	23 35	113 39.5
	Seringapatam rf., EW 5m., } sf., T, N pt.	13 34	122 3		C. Cuvier, 400f., 1. rock off	24 13	113 23
	Browse I., [1m.], 4. 20f.	14 7	123 33.5		Bernier I., 3' 4 l., Koks } Id. off N pt.	24 44	113 10
	D'Arctagan shoal, 10	13 16	120 38		Dorre I., 3' 6 l., 1. T. (Dampier's rf. 8 4m.), 8 pt., or C. St. Crieg	25 17	113 4
	Corona shoal, 5	12 26	118 40		Gascoyne Rd., Gascoyne R., } beacon	24 53.5	113 39.5
	Dry sand, 10f., (Ship Cartier, 1800)	12 32	123 38				
	Hiberna rf., 1810	12 0	123 24				
	Ashmore shl., Middle I.	12 15	123 4				
	Troubadour (1843), s.	9 44	128 28				
	Coral bank, v'	9 57	129 27				
	Lynedoch, shl. [½ m.], 7	9 54	130 40				

TABLE 10

MARITIME POSITIONS

(103) Places		Lat. S	Lon. E	(104) Places		Lat. S	Lon. E
West Coast	Shark B., Dirk Hartogs I., ¾ 13 l., 1, N pt., or C. Inscription, W extr. of Australia	25° 29' 4	112° 58'	Pt. Hood, (Doubtful Is., 3m. E-d.)	34° 24'	119° 34'	
	— Cape Peron, 66f.	25 30 5	113 30	East Mt. Barron, vis. 14 l. ...	33 57	119 19	
	— Baba B.	26 40 5	113 40	Seals' Is., (rks. N), l.	34 6	120 28	
	St ep Pt.	26 8 5	113 8 5	Rocky islets	34 5	120 53	
	Gantheaume B. Red Pt.	27 42	114 10 5	Esperance B., W pt., Ob- serv. I., small	33 56	121 46	
	Houtman rks., ¾ 16 l., ¾, w w o, b, r, North I., [1 ½ m.]	28 18	113 35	C. Le Grand, (islets off)	34 1	122 4	
	— Wallabi grp. Evening rf., (Middle Channel S of do.), S pt.	28 33	113 41	Lucky B.	34 0	122 14	
	— North-East rf., [½ m.]	28 25	113 50	West grp., SWat I., [2m.] ...	34 3	121 31	
	— Easter grp., [3 l.], (Zee- wyk Chan. S of do.), Rat I. N pt.	28 42 5	113 47 5	SW, or outer danger	34 21	121 41	
	— Snapper bk., [2m.], ¾	28 42	114 1	Mondrain I., NS ¾ m., vis. 10 l., S, S sum.	34 10	122 14	
	— Pelsart grp. EW 4 l., SW part, Wreck Pt. ...	28 59	113 58	S extr. of Archip., Termina- tion I., [1m.], vis. 9 l. ...	34 30	121 58	
	Mt. Fairfax, 603f.	28 45 4	114 41 7	Twin rks., [rfs. 2m., T]	34 24	122 12	
	Wizard Pt., 640f.	28 29 7	114 47 0	Draper's I., [½ m.]	34 13	122 30	
	Champion B., (Geraldton), Moore Pt., lt. R 110f.	28 47 1	114 35	Twin pks., vis. 9 l., (pks.) ¾ 2m.	34 1	122 47	
	Port Dongara, or Denison, lt. F. Leander Pt. beacon	29 17 1	114 55 2	A break at times, SW one ...	34 18	122 53	
	Mt. Peron, (3 l. inland)	30 7	115 9	Douglas Is., [1m.]	34 10	123 6	
	Mt. Lesueur, (do.)	30 13	115 10	Middle I., ¾ 4m., b, w o, SW sum.	34 8	123 8	
	C. Leichenhault	31 18	115 30	C. Arid., rky., SE pt.	34 1	123 13	
	Rottenest I., ¾ 5 ½ m., lt.] R 211f.	32 0 3	115 30 2	C. Pasley, sum. 1 ½ m. inland...	33 56	123 28	
	FREEMANTLE, SCOTT'S JETTY	32 3 3	115 44 5	Pt. Malcolm, l, sandy (rk.) ¾ 3m.), rk.	33 48	123 42	
	Swan B., Perth, Gov. House ...	31 57 4	115 51 7	SE Isles. [1 l.], mid.	34 20	123 28	
	Garden I., ¾ 5 ½ m., NW pt. ...	32 8 9	115 39 5	Pollock rf., [1m.], S, T	34 34	123 30	
	Coventry rk.	32 22	115 30	Round I., small	34 5	123 50	
	Peel	32 27	115 44	Eastern grp., NS 3 l., S extr.	33 52	124 4	
	C. Bouvard	32 34	115 40	Pt. Culver, 1	32 55	124 30 5	
	Koomabanah B. w, lt. F 117 ...	33 19	115 39	Pt. Dover	32 31 5	125 31	
	Busselton, lt. F 63f.	33 38	115 21	Low sandy pt.	32 22	126 28	
	Naturaliste, rf., [½ m.], sf. ...	33 15	114 55	Hd. of Grt. Australian bight...	31 29	131 10	
	C. Naturaliste	33 32	114 58	Nuyts rfs., outer detached ...	32 9	132 7	
	Geographie rk.	34 20	114 54	Fowler B., Port Eyre Tele- graph Office	31 59 7	132 26 7	
South Coast.				Pt. Bell, l.	32 13	133 8 2	
South Coast ⊕	C. Leeuwin, (rks. 2 l. out) ...	34 21	115 6	Purdies Is., ¾ 5m., w o, f o, S l., 83f.	32 17	133 14 2	
	Low Black Pt.	34 25	115 29	Smoky R., Laura B.	32 14 5	133 49	
	Pt. D'Entrecasteaux, 1, vis. l 10 l., (ld., l, rk., ¾ 3m. S) l	34 52	116 1	Is. of St. Francis, NS 2 l., w o, f o, Hart l., 65f.	32 39	133 8 5	
	White topped rks.	35 4	116 13	Yatala rf.	32 39	132 35	
	C. Chatham, vis 10 l., (islets S)	35 2	116 28	Pt. Brown	32 33	133 51	
	Pt. Nuyts, vis. 8 l.	35 5	116 38	Streaky B., Port Blanche	32 48	134 13 2	
	W Cape Howe, 1	35 9	117 40	Olive I., [1 ½ m.], 82f., rfs. N...	32 44	133 58	
	Eclipse Is., [1 l.]	35 12	117 53	C. Bauer, 1, W pt.	32 44	134 4	
	Maude rf., 680	35 13	117 56	Pt. Westall, 1	32 55	134 3 5	
	Bald Hd., vis. 12 l., S pt.	35 7	118 1	C. Radstock, 1	33 12 5	134 20	
	Braksea I., lt. F 384f.	35 4	118 3	Pt. Weyland, 1, Venus Hr. ...	33 15	134 37 5	
	King George's Sound, w, b, Princess Harb., [2], New Govt. buildings	35 2 2	117 54	Waldegrave I., 120f., W extr.	33 36	134 46	
	Mt. Gardner, sum.	35 0	118 8	Waterloo B., SE pt.	33 39 3	134 52 5	
	Bald I., ¾ 3m., (rk. 8 lm.) ...	34 55	118 27	Flinders I., ¾ 7m., N pt. 205f.	33 41	134 31	
	Sealer's ledge	35 10	118 27	Ward's Is., 162f.	33 45	134 16 5	
	Haul off rk.	34 43	118 40	Pearson's Is., NS 2 l., 2 pks., S l. 460f.	34 00	134 14	
	C. Knoh, sum.	34 31	119 14	Pt. Drummond, 1	34 9	135 14	
				Coffin's B., Pt. Sir Isaac	34 26	135 12	
				— Port Douglas, Coffin Hd. Station	34 37	135 28 2	
				Greenly Is., [1 l.], pk. 753f. ...	34 39	134 47	
				Whidbey Is., [2 l.], W grp., 862f., 4 honimocks, S extr. }	34 47	135 1 5	

MARITIME POSITIONS

(105) Places		Lat. S	Lon. E	(106) Places		Lat. S	Lon. E
Spencer Gulf @	Rocky Isl., small, l.....	34° 49'	134° 43'	Coast of Victoria @	Glencelg R., entrance	38° 37'	140° 59' 5
	Stuart rf.....	34 49 5	135 22		C. Bridgewater, l., 441f.	38 22	141 24
	C. Wiles, l.....	34 57	135 41		C. Nelson, l., lt. F 250f.	38 26	141 33
	Liguanea l., $\frac{1}{2}$ 2m. rf. S-d	35 0	135 37		Portland B., Laurence rk.	38 24 6	141 40 5
	C. Catastrophe, S pt. l.....	35 59	136 0		Percy l. [lm.], l., 153f.	38 25 2	142 0 5
	William's l. [1m.]	35 17	135 58 5		P. Fairy, (Bellast), Griffith } l., lt. F, Fl. 41f.	38 23 8	142 15
	Neptune Is., l., S l., 120f.	35 20 5	136 7		Lady B., (Warrnambool), } Middle l., (lts. F 100f. and 87f.)	38 24 3	142 28 5
	Gambier's Is., Spt., peaked rks	35 12	136 30		C. Otway, A., l., lt. R 300f.	38 51 7	143 31
	Dangerous rf.....	34 49	136 12 5		Apollo Bay, A., lt. F	38 45 7	143 41
	C. Donnington	34 43 5	135 59 5		Loatit Bay, Mt. Saint George, 657f.	38 33 9	143 57
	Port Lincoln, \square , w. Church.....	34 43 3	135 51 5		PORT PHILLIP, MELBOURNE, NEW OBSERVATORY	37 49 9	144 58 5
	Pt. Bolingbroke, l., l.....	34 33	136 4		— Pt. Lonsdale, lt. F 54f.	38 17 7	144 37
	Sir Jos. Banks grp., S extr. } Stickney l., 100f.	34 41	136 16 5		C. Schank, lt. F, Fl. 328f.	38 29 7	144 53 2
	— Winceby l., 33f., N pt.	34 29 2	136 17 5		Phillip l., $\frac{1}{4}$ 10m., $\frac{1}{2}$ W pt., Pt. Grant	38 31 6	145 7
	South B., Shipping place	34 23	135 55 5		C. Liptrap, l., pt.	38 55	145 56
	Franklin Harbour	33 44	136 57 2		Glauie Is., NS 3m., 456f., S pt.	39 7	146 15 5
	Pt. Lowly, lt. Fl 57f.	33 0	137 47 2		Clift l.	39 10	146 20
	Port Augusta, d. st	32 29 7	137 45 7		S pt. of Australia, Wilson's Promontory, l., lt. F 342f.	39 8	146 25 5
	Mt. Brown, ab. 3174f.	32 30 7	138 1		Mt. Wilson, 2350f.	39 3 5	146 24 5
	Germeia, lt. on pier F	33 2	137 59 2	Bass Strait.			
St. Vincent Gulf @	Port Pirie, jetty	33 10 5	138 1	Furneaux Is. @	King l., NS 35m., N pt. } C. Wickham lt. F 280f.	39 35 6	143 57
	Port Broughton, jetty	33 36	137 55 2		— S Pt., l., C. Stokes	40 10	143 56
	Pt. Riley, l.....	33 53	137 56		— Harbinger rks., 2, $\frac{1}{2}$ 2m., l. n. outer, or SW rk.	39 34	143 52
	Wallaroo, pier, lt. F 23f	33 55 5	137 37 2		— New Year Is., w, NW rk.	39 40	143 49
	Tipara B., (Moonta), lt.	34 3	137 34		— Carrie Hr., lt. Fl. 150f.	39 56	143 51
	Pt. Pearce, Wardang l.	34 30	137 19 5		Reid rks., [3m.], NW, 25f.	40 15	144 10
	Port Victoria, Waaraltee, lt. F	33 29 2	137 29		Bell rf., 1m., S end	40 24	144 5
	Port Minlacowie	34 51	137 27 7		Black Pyramid, 240f.	40 28	144 21
	Port Turlon, jetty	34 56 5	137 21		Redondo, rk., l., 1130f.	39 14	146 23 5
	Cornay Pt., A, lt. F 98f.	34 54	137 0 5		Monocor Is., small, E extr.	39 14	146 34
	C. Spencer, Sst. of 3 pts., 258f.	35 18 5	136 53		Crocodile rk.	39 21 5	146 30 5
	Althorpe Is., lt. Fl. 350f.	35 23	136 51 5		Curtis l., [2m.], 1060f., (Sugar loaf, S 3m.)	39 28 5	146 39
	Port Moorowie	35 7	137 31 5		Devil Tower, ~, 350f.	39 23	146 47
	Troubridge, lt. R 81f	35 7 5	137 49 7		Hogan l., [1 $\frac{1}{2}$ m.], 430f.	39 13	147 1
	Edithburgh, lt. F	35 5 5	137 45		Judgment rk.	39 30	147 10
	Port Vincent, Surveyor Pt.	34 47	137 51 7		Pyramid, 300f.	39 49	147 16
	Port Alfred, Kooley Wurta ...	34 37 4	137 53 2		Kent Is., 3, $\frac{1}{2}$ 6 $\frac{1}{2}$ m., Deal l., w., b, lt. R 957f.	39 30	147 19
	Androsan, lt. F.....	34 26	137 55 5		Wright rk., small, 300f.	39 35	147 32
	Port Wakefield, lt. F.....	34 12	138 8 7		Endeavour R., Beagle R., and Craggy l., $\frac{1}{4}$ 8m., S pt., or Craggy l.	39 41	147 42
S. Australia @	PORT ADELAIDE, SNAPPER Pt.	34 46 8	138 30 7	Furneaux Is. @	Sisters, 2, $\frac{1}{2}$ 7m., NE one, sum. 636f.	39 39	147 59 8
	Adelaide, town hall	34 56 2	138 35 7		Flinders l., $\frac{1}{4}$ 36m., W pt., or C. Frankland, ...	39 52	147 46
	Mt. Lofty, 2330f.	34 59 2	138 42 5		— Streleski pks., 2, at S part, 2550f.	40 12	148 6
	Glencelg, lt. F 29f.	34 59	138 30 5		— Babel Is., off E side, sum.	39 58	148 21 5
	Port Noarlunga, jetty	35 9 6	138 28		Hummock l., $\frac{1}{2}$ 6m., Low Furneaux Is. off S pt. ...	40 7	147 44 5
	Port Willunga, S jetty	35 16 4	138 27 5				
	C. Jervis, A, lt. F	35 37	138 6				
	Kangaroo l., EW 28 l., N } pt., Pt. Marsden	35 34 5	137 38				
	C. Borda, lt. R 510f.	35 45 7	136 35 2				
	— SW extr., C. Conedie, 95f.	36 4 5	136 42 2				
	— Pelorus rk., 40f.	36 7 3	137 31 5				
	— C. Willoughby, lt. R 247f.	35 51	138 8				

TABLE 10

MARITIME POSITIONS							
(107) Places		Lat. S	Lon. E	(108) Places		Lat. S	Lon. E
Banks Strait	Goose I., [1½ m.], w, S pt., l. F 100f.	40° 19'	147° 48'	Tasmania, North Coast	C Portland	40° 44'	147° 57' 7
	Barren I., EW 23m., Mt. Manro, on NW part, 2300f.	40 22 4	148 7 5		Waterhouse I., ½ 2½ m., w, w } SE s, N pt.	40 46	147 38
	Preservation I., pk.	40 29	148 4		Ninth I., small	40 50	147 17 7
	Clarke I., ½ 8m., S pt.	40 35	148 10		Mt. Arthur, 5 l. inland, 4300f. Tenth I., small	41 16	147 17
	Look-out rk., (SW of do) ...	40 33	148 7 5		Port Dalrymple, [w], Low Hd., lt. R 142f.	40 56 2	147 0
	Moriarty bk., SE pt.	40 36	148 17		Flinders Pt.	41 4	146 44
TASMANIA.					Emu Bay, NW, or Black- man Pt.	41 3	145 57
West Coast	C. Grim, 1, blk.	40 40	144 40 7	Tasmania, North Coast	Valentine Pk., 7 l. inland, 4000f.	41 22	145 45
	West Pt., sandy	40 57	144 38		Table Cape, lt. F 390f.	40 56 7	145 45 7
	Mt. Norfolk.	41 28	144 57		Rocky Cape, sum. 2m. in- land, 1000f., (a rk. 2m.) ..	40 53	145 31
	Mt. Heemskerk, vis. 10 l.	41 54	145 10		Circular Hd., 1, 485f. N pt.	40 43	145 17
	Macquarie Harb., [w], bar sf., w, w, f, entr. L.	42 11 6	145 13 5		Walker I., NS 3m., N pt.	40 35	144 55
	C. Sorrell, l. rky. pt.	42 11	145 10		Three Hummock I., ½ 7m., w, SW side.	40 26 5	144 51 0
	Pt. Hibbe, ½ 2m.	42 38	145 15		Hunter I., NS 13m., 300f., w, w, f, E, N pt.	40 24	144 48
	Rocky Pt., a rf.	43 0	145 30		North black rk.	40 29	144 39
	Mt. de Witt, vis. 12 l.	43 10	145 50		Albatross I., [1m.], 125f. sum.	40 22	144 39 7
	Port Davey, [w], b, pyra- midal rk., entr.	43 20	145 55	AUSTRALIA, East Coast.			
	Sugarloaf rks.	43 25	145 56		C. Wellington	39 4	146 29
	South-west C., 1000f., 1	43 35	146 1		Corn r Inlet, [w], entr. S pt. ...	38 47	146 28
	South C.	43 39	146 53		— Alberton, town	38 40	146 42
	Mastsuyker Is., ½ 7m., SW, or Needle rk.	43 41	146 11		Is. to SE-d., ½ 5m., E. or Cliffy I., lt. F 180f.	38 57	146 42
	Mewstone, A, rugged, N Pedra Blanca, (Eddystone 1m. E), [w]	43 44 5	146 23		Gabo I., [1½ m.], lt. F 179f.	37 34 2	149 55
	Sidmouth rk., [w]	43 47 5	147 7		C. Howe, l, T, islet close off	37 30 2	149 58 7
	Rurick rk.	43 59	147 42		C. Green, pt., lt. F 144f.	37 15 5	150 3
	Recherche B., 2 [w], w, b, S port	43 34	146 54		Two-fold B., Eden, [w], b, w, Red Pt., lt. F 125f.	37 4	149 54 7
	Huon R., Swan Port, [w], w, ... Acton R.	43 14	147 5		Mt. Dromedary, 2706f. Montague I., [2m.], w, W, rky., lt. F, Fl. 250f.	36 18 7	150 1 2
	Bruny, Id., ½ 9 l., S pt., or Tasman's Hd., 1	43 31	147 19 2		Pt. Upright, 1	35 38 7	150 19 5
	— SW pt., or C. Bruny, lt. R 335f.	43 28 7	147 8		Ulladulla, Warden Head, lt. F C. St. George, lt. alt. 224f. ...	35 22 2	150 30 2
	— Fluted Cape	43 22	147 24		Jervis B., Corranbean	35 3	150 40 7
	HOBARTON, [w], FORT MUL- GRAVE	42 53 4	147 20 5		Kiama, lt. F	34 40 5	150 52 2
	Storm B., C. Raoul	43 13	147 47		Wollongong, lt. F 56f.	34 25 5	150 55
	Port Arthur, [w], w, F, Se- maphore	43 9 1	147 50 7		Botany Bay, w, w, N pt. entr., C. Banks, 180f.	34 0 5	151 15
	C. Pillar, 1, Tasman's I., off do, vis. 12 l.	43 14	148 2		Port Jackson, [w], lt. elec- tric, R 344f.	33 51 2	151 17 2
	Hippolite rk., 70f.	43 6	148 2		SYDNEY, FORT MACQUARIE* Observatory	33 51 5	151 13 0
	Maria I., NS 4 l., Oyster B., w, w, W side, w, w } — Pyramid, off S pt.	42 40	148 2		Broken B., [w], Baranja Hd., lt. F 370f.	33 34 7	151 20
	— Sum. at N end, 3500f.	42 37	148 7 5		Catherine Hill B., Coaling jetty	33 9 4	151 38 2
	C. Bougainville	42 30	148 0		Newcastle, Nobby Hd., lt. 115f. Pt. Stephen's, T, lt. R 126f.	32 55 2	151 48 2
	Schouten's I., ½ 6m., S islet off C. Degerando	42 21	148 18		Broughton Is., E pt.	32 37 5	152 21
	C. Degerando	42 16	148 17		Sugarloaf Pt., lt. Rev. 258f. ...	32 26 5	152 33
	St. Patrick's Head	41 34	148 18		C. Hawke, pk., 777f.	32 13	152 35
	Eddystone Pt., lt. F, Fl. 133f. do., 1730f.	40 59	148 20		Three Brothers, 1700f., N one Port Macquarie, entr.	31 40	152 47
	Mt. Cameron, (8 l. inland of do.), 1730f.	40 59	147 56		Smoky C.	31 25	152 57
	Black rf., [1½ m.],	40 50	148 16			30 56	153 6
	Swan Is., [3m.], 90f.; w, lt. at E pt., R 100f.	40 44	148 8				

* Garden Id., the usual place of observation. lies 2° 43' E. of Fort Macquarie.

MARITIME POSITIONS

(109)	Places	Lat. S	Lon. E	(110)	Places	Lat. S	Lon. E
N. Solitary L.		29°55'5	153°24'	Cumberland Is., Bailey I., } 120f.		21° 3'	149° 34'
Clarence R., entr., lt. F.		29 26	153 24	— Shaw's Pk., N part of I., } [4m.]. 1324f.		20 28	149 6
C. Byron, E pt. of Australia		28 37-6	153 39	— Kenedy Sd., Brush L., 62f.		20 29	149 4
Mt. Warning 28 23-1	153 17			Dent I., lt. Rev. 120f.		20 22	148 57
Fingal Pt., lt. F 80f.	28 11-2	153 34		Whitsunday I., pk. 1426f.		20 16	148 58-5
Pt. Lookout, 260f.	27 26	153 33		Hayman I., N pt., 844f.		20 2	148 54
O. Mookroo, N part of Id., } (rks. 4-4m.), lt. R 382f. }	27 2-3	153 28		Port Molle S' Id., 223f.		20 19	148 52
Brisbane R., Lytton I., lts.	27 24-7	153 10		Mt. Dryander, 2690f.		20 15	148 34-5
Mt. Arthur, 1620f.	26 17-5	152 50		Gloucester Head, 1555f.		19 58	148 27
Double I., pt., lt. R 815f.	25 56	153 12		Port Denison, Obay. Pt., W } side of Stone L.		20 2-2	148 16-5
Grt. Sandy I., 4 23 I., E } pt., or Indian Head ... }	25 0	153 22		Nares rk., 26f.		19 46-4	148 22
— N and E pt., Sandy Cape, } w 7m., lt. R 400f. }	24 42-5	153 12-5		Holborne I., [1m.], 360f.		19 43-6	148 22
— Shls. off N pt., Break- } sea Spit, T }	24 25	153 12		Mt. Abbott, 2410f.		20 5-5	147 44-5
Maryborough R., Woody I., } pk., lt. F 215f. }	25 18	152 58-5		C. Upstart, (sum. 1510f.), } NW pt., (w 4 1m.) ... }		19 42-2	147 45
Burnett R., lt. F 37f.	24 45	152 24-5		C. Bowling Green, lt R 70f.		19 19-5	147 26
				C. Cleveland, lt R 206f.		19 11-2	147 1
				TOWNVILLE PILOT FLAG- } STAFF }		19 15-5	146 50-0
North East Coast.				Mt. Eliot, 3980f.		19 29	146 58-5
Bustard Hd., lt. F, Fl. 330f.	24 1-5	151 46		Magnetic L., [5m.], 1628f.		19 8-5	146 49-5
Lady Elliott I., lt. Fl. 60f.	24 6-5	152 45-5		— Bay rk., lt. F 96f.		19 7-2	146 45-5
Mask-Head Islet, 4, 50f.	23 32	151 45		Palm Is., b, w, large one, 4 } 8m., 1890f., SE pt. }		18 45-5	146 42
Capricorn grp., 4, NW L., } (rfs. E), 4, 50f. }	23 16	151 44		Hinchinbrook I., Pt. Hil- } lock, 270f. }		18 25	146 23
— North rf., lt. F, Fl. 72f.	23 10-8	151 56		— Mt. Bowen, 3650f.		18 20-7	146 17-2
Port Curtis, (Gladstone) H. } Facing I., 4, 8m., Gat- } combe Hd., lt. F 66f. }	23 53	151 22-7		— C. Sandwich, rks. 2m.		18 13-5	146 20
C. Capricorn, lts. R and F.	23 29-5	151 14		Cardwell 18 14-5		146 3	
Keppel Is., Barren I., 548f.	23 9-5	151 5		Rockingham B., Gould I., } [2m.], w 3" W, sum. 1375f. }		18 9-5	146 11-5
Rockhampton 23 24	150 32			Dunk I., 4 3m.		17 57	146 11
Atherton 23 7-5	150 42			Double Pt., rks. SE 5m.		17 39-3	146 10-5
Flat I., 175f. 22 44	151 0			Flyingfish Pt., lts F 17 30-2		146 6-2	
C. Manifold, islet, 260f.	22 41	150 52		Frankland Is., 4 4m., Sand } E L., 220f. }		17 13-7	146 7
Port Bowen, H., w, Olan. } rk. }	22 31-7	150 47		Fitz Roy I., [2m.], w, b, } NE pk., 860f., 4 W }		16 55-7	146 1
C. Townshend, N extr., 500f.	22 12	150 30		C. Grafton, 1273f.		16 52	145 57
High Double Mt., 2345f.	22 32-7	150 18-5		Cairns Landing-place, lts. F ...		16 55-7	145 48
Thiraty Bd., Pier Hd., 334f.	22 6-5	150 3		Green I., [and rfs. 3m.], 90f.		16 46	146 0
Turn I., 280f. 21 59	149 49			Port Douglas, lt. Rev. 82f.		16 29-3	145 29
St. Lawrence Creek, (St. } Lawrence), S. Red Bluff. }	22 17	149 37		Low Is., lt. R 65f.		16 23	145 35
Northumberland Is., E one, } or High Pk., 718f. }	21 57	150 42		Snapper I., [14m.], w., SE } pt., 350f. }		16 17-7	145 31
Percy Is., 4 7 I., lt. F, Fl. } 180f. }	21 39	150 14		Archer Pt., lt. F 220f.		15 36	145 2
— Beverly Is., 4, Hull I., 272f.	21 27-5	149 53		C. Tribulation 16 4-4		145 30	
— Pradhos I., 4 2m., 1074f.	21 19	149 42		ENDEAVOUR R., COOKTOWN } Pilot Station, lt. F 570f. }		15 27-5	145 15-2
West Hill I., 983f. 21 49-4	149 30-7			Turtle rf., [3m.], 2, N pt.		15 24	145 27
C. Palmerston, (w 4 10m.) ...	21 31-5	149 31		C. Bedford, 818f., 1, (shl. } 1m.) }		15 16-5	145 23
Pioneer R., (MacKay), Flat- } top I., lt. F 174f. }	21 9-5	149 16		C. Flattery, 2 pks., 863f., pt.		14 59	145 23
Slade Pt. 21 3	149 15			Lizard I., [3m.], 1167f.		14 40	145 30
C. Hillsborough, 1, 996f.	20 54	149 3		Eagle I., [1m.], 4 4, (shl. } 8-d.) }		14 42	145 24-7
Sir Jas. Smith's grp., Linné } Pk., 926f. }	20 40	149 12		Lookout Pt. 14 50		145 15-7	
Repulse Is., N. I. pk., 265f.	20 35-7	148 54		Coles' Is., 4 4, NE ext.		14 33	144 57
C. Conway, pk. 1637f.	20 31	148 54-5		Howick's grp., 4, SE sum.		14 32-4	145 1-5
Cumberland Is., 4 26 I., 4, } S and E end, Snare Pk., } 300f. }	21 5-7	149 56-7		Noble I., [1m.], rky., A.		14 30-5	144 48-5
				C. Bowen 14 31		144 42-5	
				Pt. Barrow, rky. 14 28-5		144 42	

Coast of Queensland

N.E. Coast of Queensland

MARITIME POSITIONS.

(111) Places		Lat. S	Lon. E	(112) Places		Lat. S	Lon. E
<i>N.E. Coast of Queensland</i>	C. Melville, (shl. $\frac{1}{2}$ 2 $\frac{1}{2}$ m.) ...	14° 10'	144° 33' 5	Fly entrance, $\frac{1}{2}$ m., [4 m.]	10° 1'	144° 3'	
	Pipon Is., [2 m.], $\frac{1}{2}$ $\frac{1}{2}$, N pt.	14 6 5	144 34	Cumberland entrance	9 52 5	144 8	
	Clack's I., small, $\frac{1}{2}$ rk., $\frac{1}{2}$...	14 4 7	144 17 5	Murray Is., [4 m.], grt. one, } $\frac{1}{2}$ pk. 700f.	9 55	144 1	
	Flinders grp., $\frac{1}{2}$ 2 l., 994f., } N pt. C. Flinders	14 8	144 16 2	Flinders' entr., $\frac{1}{2}$ 4 m., S pt., } T	9 35	144 10	
	Jane's Tableland, abt. 1000f.	14 29	144 10	Islands and Shoals Eastward of Australia.			
	A dry sand, [1 $\frac{1}{2}$ m.]	14 8	144 2 5	Ball's Pyramid, 1810f.	31 45	159 15 2	
	Low Woody I., [1 m.]	13 40	143 43	Lord Howe I., 2834f., w'	31 31 5	159 5	
	C. Sidmouth	13 25	143 37 2	Seringapatam and Eliza- beth I., mid.	29 56	159 4	
	C. D. rection, rf. 2m.	12 51	143 34	Middleton I.	29 28	159 4	
	C. Weymouth, Restoration I., $\frac{1}{2}$ pk. 446f., W pt., $\frac{1}{2}$ } $\frac{1}{2}$, $\frac{1}{2}$	12 37 5	143 27 5	A rock	24 0	160 15	
	Fair Cape, rf. 2m.	12 25	143 17	Capel bk., $\frac{1}{2}$	25 15	159 18	
	Forbes Is. sum. 340f.	12 16	143 24	Ferriers' bk., $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$	23 23	155 32	
	C. Grenville, E pt.	11 57 5	143 13 2	Cato bk., $\frac{1}{2}$	23 14	155 33	
	Conical Hill	11 50 3	143 18 7	Wreck rf., (Porpoise and Cato, 1803), EW 7 l., Eastern extremity, Bird Island, $\frac{1}{2}$	22 10	155 28	
	Sir Ch. Hardy's Is., [8 m.], w. $\frac{1}{2}$, N one, 320f.	11 54 7	143 28 5	Sir James Beaumarez bks., [3 leagues], SW Cay	21 51	153 30	
	Cockburn rf., Cockburn I., 300f.	11 50 3	143 18 7	Frederick, shoal, (ship, 1812)	21 1	154 23	
	Bird Is., l, $\frac{1}{2}$, West I.	11 46	143 4 7	Kenn rf., $\frac{1}{2}$ 9 miles, low, T, $\frac{1}{2}$	21 15	155 49	
	Orfordness, Pudding-pan Hill, 403f.	11 19 7	142 48	Booby shoal, NW extreme ...	20 57	158 31	
	Cairncross I., $\frac{1}{2}$, 93f.	11 14 5	142 55	Mid. Bellona	21 24 3	158 52	
	Busby I.	11 15 5	142 53 5	Bellona shl., NW	20 47 7	158 27 2	
	Arnold I., $\frac{1}{2}$, 30f.	11 0 3	142 59 2	Bellona shl., S	21 47 3	159 34	
	Shadwell Pt., 245f.	11 0	142 44	Ball's rks.	21 0	160 36	
	Z Reef, beacon	12 49 3	142 43	Bampton shl., [17 leagues], South-West part, Avon Islands, 2, [2 miles], l, $\frac{1}{2}$ } Bampton I., 17f.	19 33	158 16	
	Grt. Albany Is., Ulrica Pt. ...	10 45	142 37 2	Reward I., 20f.	19 8	158 30	
	Mount Adolphus Is., Mt. Adolphus, 548f.	10 38	142 39 2	Mellish Cays, [4 l.], mid.	19 13 5	158 55 7	
	North Brother	10 42 3	142 40	Libou shoal, [15 l.], E lim. ?	17 25	155 53	
	N. extr. of Australia. C. York I., small, rky., 283f., l ...	10 41 2	142 31 5	Tergrose Islets, 2, rfs., W pt.	17 10	152 12	
	C. YORK, SEXTANT BE.	10 41 7	142 32 7	Coringa shl., Id. 10f., rfs., Chilcott I.	17 43	150 42	
	Barrier Reefs.			Bougainville shls., 2, $\frac{1}{2}$, NS 6 l., N pt. ?	16 50	149 57	
<i>Barrier Reefs</i>	S limit of Grt. Barrier rfs., } Swain's rfs.	22 23 2	152 36	Bougainville shls., 2, $\frac{1}{2}$, NS 6 l., N pt. ?	15 31	147 7	
	Hixson Cay	22 20	152 41	Osprey shl., $\frac{1}{2}$ 10 m., S pt. ...	13 50	146 34	
	NE lim.	21 5	152 52	Torres Straits.			
	Flinders rfs., S extr.	17 55	148 31	Possession I., $\frac{1}{2}$ 3 m., rky., } $\frac{1}{2}$ $\frac{1}{2}$, w. $\frac{1}{2}$, centre	10 5	142 19	
	Herald's Surprise	17 20	148 28	Double I., [4 m.], 218f., N sum.	10 27	142 26	
	Endeavour opening	15 42	145 48 5	Prince of Wales' I., 5 l., } Heath I.	10 35 7	142 11	
	Lark Pass	15 7	145 45	— S pt., or C. Cornwall	10 46	142 10	
	First Three mile opening, } N pt. of rf., T	13 26 5	144 0	Wallis Is., shl., N one, 60f. ...	10 51	142 1	
	Second Three-mile opening, (rf. in mid.), pt. to E-d., T	13 5	143 54	Thursday I., Vivien Pt., fl. st.	10 35	142 12	
	Cook entr., (1770), Provi- dential Chan.	12 39	143 49	Goode I., lt. F 345f.	10 33 7	142 8 2	
	Southern, small, [1 m.]	12 40 5	143 50 5	Booby I., [4 m.], 30f., $\frac{1}{2}$, } $\frac{1}{2}$, r, w. $\frac{1}{2}$, "Post Office" } Proudfoot shl., $\frac{1}{2}$ li. ves. occ.	10 36	141 54 0	
	Northern, small, [1 m.]	12 25	143 48	Eastern Fields, [7 l.], E end, $\frac{1}{2}$	10 5	145 45	
	Black rks., N pt.	12 12 5	143 55	Boot rf., NS 4 l., (shls.) } SE-d and SW-d, N pt.	9 58	144 40	
	Yule's rf., [1 l.], E edge, T ...	11 58	143 58	Portlock rf., N limit	9 28	144 53	
	Nimrod's entr., [3c.]	12 6	143 47				
	Stead's entr., [4 m.]	11 55	143 49				
	Grt. Detached rf., NS 4 l., E extr.	11 44 5	144 6				
	— South-east pt.	11 51	144 5				
	Raine I., $\frac{1}{2}$ 1 $\frac{1}{2}$ m., (entrance), $\frac{1}{2}$, w. $\frac{1}{2}$, beac. 60f.	11 36	144 1 2				
	Pandora entr., [2 m.]	11 26 5	144 0				
	Olinda entr.	11 14 5	144 5				
	Yales' opening, II, [1 m.], (current l)	10 23	143 55 5				

MARITIME POSITIONS

(113) Places		Lat. S	Lon. E	(114) Places		Lat. S	Lon. E
<i>Torres Straits, Eastern Entrances</i>	East Cay.....	9° 21'	144° 12'	<i>Stewart I.</i>	West Cape	45° 54'	166° 26'
	Anchor Cay, (S lim. of Bligh's enr.)	9 22	144 6		Chalky I., (S centr. of Dark Cloud inlet), N pt.	45 59	166 35.7
	Bramble Cay, sandbk., 12f., (Bk. rks. $\frac{1}{2}$ 3m.) ...	9 8	143 51		Puysegur Pt., lt. Fl. 180f.	46 10	166 38
	Darley I., or Erooh, (at W edge of rfs., $\frac{1}{2}$ 11m.), ww., P., hill 610f.	9 35.3	143 45		Sandhill Pt.	46 16	167 22
	Nepson I.	9 34	143 39		Solander Id., [1m.], 1100f.	46 36	166 55
	Stephen's I., l, $\frac{1}{2}$...	9 31	143 32		Black rk. Pt.	46 41.5	167 53.7
	Pearce Cay	9 30	143 16		Mt. Anglem. 3200f.	46 45	167 57
	Dalrymple I.	9 37	143 18		Codfish I., $\frac{1}{2}$ 3m., NW rocks	46 46	167 37.7
	Rennell I., village	9 46	143 15		Ernest I., W head of Mason B	46 57	167 42
	Yorke Is., 2, W Id., village ...	9 45	143 25		Wedge I., $\frac{1}{2}$ 1m., cent.	47 13.5	167 21.5
	Arden I.	9 53	143 9		SW Cape.	47 17	167 30
	Aured I., village	9 58	143 16.5		Port Pegasus, cove abreast Anchorage island	47 11.7	167 41.7
	Half-way I. and rfs., $\frac{1}{2}$ 4m., NW pt.	10 6	143 17		Wrcek If., [$\frac{1}{2}$ m.]	47 6	168 18
	Cocoa-Nut I., 2, [4m.], E pt.	10 4	143 6.5		Port Adventure, Entrance } I., E pt.	47 4.7	168 14.2
	Dove I.	10 0	143 1		Paterson Inlet, Glory Cove, hd.	46 58.5	168 10.7
	Dungeness rf., S pt.	10 4.5	142 56.5	<i>Middle I., South and East Coasts</i>	North Trap, $\frac{1}{2}$ 2 $\frac{1}{2}$ m., 3f., E pt.	47 22.2	166 55.2
	Dungeness I., EW 4m., W pt.	9 52	142 53		South Trap, If., NS 2m., S pt.	47 33	167 53
	Warrior I., [1 $\frac{1}{2}$ m.], at S pt. of Warrior rf.	9 48	142 57		Snarea, [1], 470f., $\frac{1}{2}$ W Id.	48 7	166 29
	Turtle-backed I., 268f., $\frac{1}{2}$ Long I., $\frac{1}{2}$ 4m., $\frac{1}{2}$ rfs., E-d, W pt.	9 54	142 45.5		Centre I., lt. F 263f.	46 28	167 52
	Gable I., Brothers, hills, h ...	9 45	142 37		Awarua, Bluff Hr., Starling Pt., lt. F 30f.	46 37	168 23
	Poll rk.	10 16	142 49		Raspuke I., (group $\frac{1}{2}$ 10m.), N pt.	46 45	168 33
	Harvey rks.	10 19	142 40		Slope Pt.	46 41	169 3
	Mt. Ernest, 807f.	10 15.5	142 28.2		Nugget Pt., lt. F 250f.	46 27.2	169 51
	North Possession I.	10 5.2	142 19		Saddle Hill	45 55	170 22
	Banks I., Mt. Augustus, } 1310f.	10 10	142 19		C. Saunders, lt. Rev. 210f.	45 53	170 46
	Mulgrave I., peak, 686f.	10 8	142 8.2		Taeri I., [$\frac{1}{2}$ m.], mo. of T. riv.	46 4	170 15
	Duncan Is., Whale I., N pk. ...	10 15.5	142 3.7		(Mago Harb., Tairua Hd., lt. F Whalers' Home Pt., Merangi, lt. F 170f.	45 47	170 45
	Jervis I., [2 l.], 525f.	9 58	142 10		C. Wanbrow, Oamaru, lt. F ...	45 7	171 1
	Cook Reef	10 23	141 33		Waitangi R., mo.	44 55	171 12
	Alert Reef, [$\frac{1}{2}$ m.]	9 52	140 38		Timaru, lt. F 85f.	44 23	171 18
					Banks' Peninsula, Akaroa Harb., W head, lt. Fl. 270f.	43 54	173 0
					— East point	43 46	173 9
					Port Cooper, Lytt. Cust. ho.	43 36.7	172 44.2
					Christchurch	43 32	172 37
					Table Id.	43 4	173 5
					Huranni R.	42 55	173 18
<i>West Coast, Middle Island</i>	NEW ZEALAND.				Kaikora Penins., E pt.	42 26	173 44
	Farewell Spit, bush end pt., lt. Rev. 180f.	40 33.3	173 2		Kaikora Range, sum. 9700f.	42 1	173 41
	C. Farewell	40 30	172 42		Ben More, 4360f.	41 55	174 2
	Mount Olympus, 5400f.	40 52	172 35		C. Campbell, lt. R 155f.	41 44	174 18.2
	Rocks Pt.	40 58	172 4.5		Wairau R., lt. F 38f.	41 30	174 5
	C. Foulwind, lt. B 190f.	41 45.5	171 28.7		Port Underwood, E head	41 21	174 8
	Grey R., lts. F.	42 26	171 13	<i>Middle I., N. Coast</i>	Brothers, lt. Fl. 238f.	41 6	174 27
	Hokitika R., lt. F 122f.	42 42	170 59		C. Jackson	41 0	174 20
	Abut Hd., extr.	43 7	170 17		Stephen's I., [1m.]	40 40	174 1
	Mt. Cook, 13,349f.	43 33.5	170 12.2		D'Urville I., Port Hardy, E arm, Wooding Pt. ...	40 46.6	173 55
	Cascade Pt., N extr.	44 0	168 24		— Greville Harb., S head ...	40 50	173 48
	Milford So., Freshwater basin	44 49.3	167 55.7		Current Basin, Cross Pt.	40 56.3	173 52.2
	Pembroke Pk., 6710f.	44 35	167 54		Nelson, lt. F 60f.	41 15.6	173 17
	George Sound, Anchorage Cove, N side	44 55.3	167 26.7		Astrolabe rd., Adele I., NE pt.	40 58.9	173 5.2
	Thompson Sound, Deas Cove, hd.	45 11.7	166 58.2		Separation Pt.	47 173 2	
	Breaksea Id., NE pt.	45 34.7	166 38.7		Clifton, anchorage	40 50	172 52
	Five Fingers Pt., Dusky B. ...	45 44.2	166 28				

* Positions marked thus are provisional.

MARITIME POSITIONS

(115) Places		Lat. S	Lon. E	(116) Places		Lat. S	Lon. E
North I., East Coast	Kapiti I., $\frac{1}{2}$ sm. sum. 1780f.	40°52'	174°55'	N.E. Coast	C. Tewara, or Bream Hd. ...	35°52'	174°37'
	Mana I., (off Porirua Harb.), $\frac{1}{2}$ sm. sum. NW pt. ...	41 58	174 48		Wangari Harb., \square , Passage I.	35 51	174 31.5
	C. Terawiti, extr.	41 17.2	174 38.7		Tutukaka Harb., N head	35 38	174 34.0
	Port Nicholson, \square , East or Pencarrow Hd., lt. F 420f.	41 22.0	174 52.0		Poor Knights' Is., N one, 630f.	35 29	174 45
	WELLINGTON, PIPITEA Pt. ...	41 16.5	174 47		Wangaruru Harb., Grove Pt.	35 23.3	174 22.7
	— MOUNT COOK, OBSERVATORY	41 18	174 47		Waimangaroa pt., lt. F on wharf.	35 19	174 8
	Taourakira Hd., extr.	41 26	174 56		C. Brett, (W hd. of B. of Is)	35 10	174 21
	C. Palliser, extr.	41 37.5	175 17		Port Russel, wharf, lt. F 20f.	35 16	174 8
	Flat Rock, extr.	41 15	175 58.5		C. Wiwiki	35 9	174 10.7
	Castle Pt., extr.	40 54.5	176 14.2		Cavalli Is., great, NE extr. ...	35 0	173 58
	C. Turnagain, E extr.	40 29.5	176 38.5		Stephenson I., NW pt.	34 58	173 47.5
	C. Kidnappers, extr.	39 38	177 8		Wangaroa Harb., Peach I. ...	35 17	175 46.7
	Ahuriri Road (Napier) Bluff } lt. F 160f.	39 28.7	176 57		Flat Hd., (E. hd. of Doubtless B.)	34 55	173 35
	Mahia Peninsula, Table Cape	39 6	178 1		Mongonui Harb., White's Pt.	35 0.3	173 33.5
	Portland I., S extr., lt. R 300f.	39 18	177 53		C. Karakara, extr.	34 47.3	173 25.7
	Poverty B., Gisborne lt. F.	38 41	178 3		Parenga-renga Harb., coal pt.	34 30.7	173 17
	Ariel rks., centre, δ	38 44	178 18.5		North Cape, islet	34 25	173 4.5
	Gable end Foreland, white gab.	38 32	178 18		C. Reinga	34 26	172 41
	Tolago B., Motu Huka islet... *	38 20.8	178 21.2		C. Maria Van Diemen, islet } lt. Rev. 330f.	34 28.5	172 38.7
	Open B., N pt.	37 58	178 23		Three Kings, 995f., NE one, NE pt.	34 6.3	172 9.7
	Mt. Hikurangi, 5535f. *	37 53	178 3	W. Coast ; New Zealand, North I.	Reef Pt., W. ent. of Ahaipara B.	35 11	173 5
New Zealand	East Cape islet, 420f.	37 40	178 36		Herekino, S pt.	35 18.2	173 11
	Matakawa Pt.	37 32	178 21		Hokianga R., entr. fl. st.	35 32.1	173 23
	C. Runaway, extr.	37 31	178 1		Monganui Bluff, 2040f., bluff	35 46.3	173 34.7
	Waikana Pt.	37 38	177 46		Kaipara Harb., \square , shls. 1 l. out, N. entr. lt. F 1278f. ...	36 24.3	174 7
	Mt. Edgecumbe, E sum. 2375f.	38 6	176 45		Manukau Harb., \square , South Hd., lt. F 385f.	37 3	174 33.7
	White I., 863f.	37 30	177 12		Waikato R., Maratai Vill.	37 24.3	174 47.2
	Tauranga Harb., \square , Mt. Mongonui, entr., E side ...	37 36.4	176 11		Whaingaroa Harb., S entr. pt.	37 46.5	174 53.7
	Motiti I., $\frac{1}{2}$ sm., N pt.	37 35	176 25		Karehoa Mt., 2370f. *	37 50	174 51
	Mayor I., [2m.], 1110f.	37 16	176 15		Gannet Id., summit, 70f.	37 57	174 35
	Tairua R.	36 59	175 54		Aotea Harb., entr., N hd.	37 59	174 49
	Mercury B., Oyster R. mo. ...	36 49	175 48		Ka Whia Harb., \square , S hd. ...	38 4.9	174 49
	Alderman Is., [4m.], E or outer	36 56	176 7		Albatross Pt., N extr.	38 6.2	174 43.5
	Red Mercury I., [1 $\frac{1}{2}$ m.], E pt.	36 37	175 59		Ternua Pt.	38 23	174 40
	Great Mercury I., $\frac{1}{4}$ sm., N pt.	36 34	175 49		Mokau R., entr.	38 42.5	174 38.7
	Richard's Is.	36 35	175 58		Raleigh, lt. F.	39 0	174 15
	Cavir I., [1 $\frac{1}{2}$ m.], sum.	36 26	175 21		New Plymouth, lt. F 100f. ...	39 3.6	174 2
	Channel I. (Tahoupo), 370f. ...	36 26	175 21	S.E. Coast. New Zealand, North I.	C. Egmont, extr., lt. F 103f. ...	39 17	173 46
	C. Colville	36 28	175 22		Mt. Egmont, 8270f.	39 18	174 5
	Coromandel Harbour, \square , Juhuia I.	36 48.6	175 25.5		Patea R., Carlyle, lt. F 150f.	39 47	174 31
	Riv. Thames, Grahamstown, } lt. F.	37 8	175 33		Waitotara Pt.	39 52	174 44
	Panhehe spit, lt. F 50f.	36 54	175 12		R. Wanganui, N or Castle } cliff, lt. F 65f.	39 57	175 1
	Bean rocks, lt. F 50f.	36 50	174 52		R. Manawatu, N k. F 44f. ...	40 27.2	175 14.7
	Auckland, \square , Dépôt Pt. ... @	36 50.1	174 49.7				
	Tiri Tiri I., lt. F 300f. on SE pt.	36 38	174 56				
	Kawau B., Fish Pt., E entr.	36 27.0	174 48.5				
	Great Barrier I., 2330, $\frac{1}{2}$ 71., } S pt. C. Barrier	36 22	175 33				
	— Port FitzRoy, W pt. of E side	36 12.0	175 22.5				
	— Wellington Hd.	36 10	175 18				
	— Id. off N end, N or Aigulles Pt.	36 2	175 27				
	Horn rk.	36 15	175 13				
	Simpson rk.	36 1	175 9				
	Mokou Hinou Is., $\frac{1}{2}$ 1 $\frac{1}{2}$ m., } lt. F 385f.	35 57	175 9				
	Rodney Pt.	36 17	174 51				
	Bream Tail	36 3	174 37				
	Moro Tiri Is., EW 5m., E pt.	35 54	174 49				

* Positions marked thus are provisional.

MARITIME POSITIONS

(117) Places		Lat. S	Lon.	(118) Places		Lat. S	Lon. W
SOUTH PACIFIC OCEAN.							
Auckland Islands.			East				
Bishop and Clerk	55° 18'	158° 56'		Serie I. (<i>Pukoraka</i>), $\frac{1}{4}$ 7m., }	18° 22'	136° 58'	
Macquarrie I., NS 12 L, N pt.	54 40	158 56		SE pt.			
Judge and Clerk	54 19	159 10		Narcissus, or Clerke I. } O	17 18	138 19	
Campbell I. [3 L.], 1867f., }				(<i>Totakoto</i>), E end			
South harb., Shoal pt. ... }	52 33 4	169 8-7		Presipriatic I. (<i>Fakaini</i>), }	15 58	140 8	
Auckland Is., NS 81, S.C. 2000f.	50 56	166 4		$\frac{1}{2}$ 4m., centre			
West extreme	50 50	165 57		Arakteeheoff I. (<i>Angatu</i>), }	15 51	140 50	
Disappointment L., [1 L.]	50 37	166 0		$\frac{1}{2}$ 5m. centre			
C. Bennet	50 51	166 15		Crescent I. (<i>Timoa</i>), $\frac{1}{4}$ 3m., }	23 20 5	134 29	
Sarah's Bosom, Terror Cove...	50 32 5	166 12 5		S pt.			
Bristow Is., 3	50 26	166 18		Portland reef	23 41	134 30	
Antipodes I., Depôt, 1320f.	49 39	178 50		Gambier Is. (<i>Manga Reva</i>), }	23 7 5	135 07	
Bounty Is., EW 3½m., 290f.	47 43	179 0		$\frac{1}{2}$ 6 l., rfs., E, w, Flg. of. }			
				1315f.			
Chatham Islands.			West	Lord Hood I. (<i>Marutan</i>) }	21 31	135 38	
Chatham Is., Whare-Kauri, }	44 20	176 17		[4 l.], W pt.			
$\frac{1}{4}$ 20 l., S. isl., Tarakoi- }				Maria I. (<i>Moerenhut</i>) [4m.] ...	22 0	136 12	
koi's Pyramid, 566f. }				Acton Is., 3 [5 l.] (<i>Mata-</i>	21 25	136 25	
— Rangiauria, Pitt I., $\frac{1}{2}$ 7m., }	44 14	176 11		<i>rei Vavao</i> , Melbourne I.) }			
$\frac{1}{2}$ 2m.), 791f. }				Carysfort I. (<i>Tureia</i> , Papa-	20 45	138 30	
— Great I., $\frac{1}{2}$ 13 l., S pt. }	44 8 5	176 35		<i>kana</i>), $\frac{1}{4}$ 7m., NE pt. ... }			
Pt. Evêque				Barrow I. (<i>Vuna Vana</i>), }	20 45	139 10	
— Port Waitangi, w, Pt. }	43 57	176 31		N pt.			
Hanson				Marone or Cadmus I.	23 8	137 8	
— E extr., Wakura I. (rf. }	43 44	176 10		Cockburn I. (<i>Fangataufa</i>) }	22 12	138 42	
2m.), E pt. }				[4m.], lag. NE pt.			
— Berrier rk., 150f., [2m.], }	43 58	175 48		Osnaburgh, or Matilda I. }	21 50	138 47	
W pt. }				(<i>Muraoa</i>), $\frac{1}{2}$ 5 l., P, P, P. }			
— North-west reef, extr. pt. ... }	43 31	176 53		E pt.			
				Bligh's Lagoon I. (<i>Tema-</i>	21 38	140 40	
Islands off Coast of South America.				<i>tangi</i>), $\frac{1}{4}$ 2 l., N pt. ... }			
Juan Fernandez I., 3000f., }	33 37 6	78 53		Cook Lagoon I. (<i>Vahitahi</i>), }	18 42	138 50	
$\frac{1}{2}$ 4 l., Cumberland B. Fort }				$\frac{1}{2}$ 3m., P, P, N pt.			
— S. pt., Sta. Clara I., EW 2m. }	33 45	79 2		Thrum Cap (<i>Ahiaki</i>) [$\frac{1}{2}$ m.], }	18 30	139 14	
Masafuera I., 6023f. }	33 45 5	80 45		NW pt.			
St. Ambrose I., 1512f., W }	26 21	79 59		Bow I. (<i>Hoa</i>), $\frac{1}{4}$ 8 l., E, }	18 3 6	140 59 2	
rock (St. Felix, 472f.) ... }				w, lag. Morai on E side }			
Sala y Gomez, rks. [$\frac{1}{2}$ m.], }	26 27 7	105 28		of entr.			
via, 15m. }				— South pt.	18 16	140 41	
Easter I., $\frac{1}{2}$ 4 l., 1767f., }	27 10	109 26		Moller I. (<i>Amanu</i>), $\frac{1}{2}$ 5 l., }	17 40	140 39	
Perouse Pt., Cook's Bay ... }				P, P, N pt.			
Ducie I., $\frac{1}{2}$ 2m., 14f., NE pt. }	24 40 3	124 48		Resolution I., 2 Is. (<i>Tauerie</i>), }	17 23	141 30	
Elizabeth I., $\frac{1}{4}$ 5m., NE pt. ... }	24 21 3	128 19		[4m.], S pt.			
Pitcairn I., $\frac{1}{4}$ 2m., 1000f., }	25 3 6	130 8		Goud Hope I. (<i>Rekareka</i>) }	16 51	141 55	
Adamstown				[2 l.], S pt.			
Oeno I. [2½m.], N pt. }	24 1 3	130 41		Barclay de Tolly I. (<i>Raroia</i>), }	16 13	142 31	
				$\frac{1}{2}$ 6 l., S pt.			
Low Archipelago.				Wolkowsky I. (<i>Takume</i>), $\frac{1}{2}$ }	15 44	142 9	
Disappointment Is., 2, }	14 12	141 12		13m., lag. l., N pt. P, P ... }			
Wytoche I., SE pt. }				Whitsunday I. (<i>Pinahi</i>) }	19 24	138 43	
— Tetapoto, Ototohoo L. }	14 6	141 24		[½m.], NW pt.			
Clermont Tonnerre I. (<i>Reoo</i>), }	18 34	136 20		Queen Charlotte I. (<i>Nuku-</i>	19 17	138 49	
or Minerva, $\frac{1}{4}$ 10m., SE pt. }				<i>tavake</i>), EW 3m., 1, P, P. }			
				E pt.			
				Egmont I. (<i>Vairatea</i> , <i>Puka-</i>	19 18	139 18	
				<i>ranga</i>), $\frac{1}{2}$ 4 m., T, P, P. }			
				Byam Martin I. (<i>Ahenui</i>), }	19 37	140 25	
				[4m.], lag., b, N pt.			
				Gloucester I. (<i>Paraoa</i>), EW }	19 8	140 40	
				3m., NE pt.			
				Cumberland I. (<i>Manuhangi</i>), }	19 12	141 16	
				$\frac{1}{2}$ 2½m. SE pt.			
				Leaving L. or Pr. Wm. Henry }	18 46	141 45	
				(<i>Nengo-Nengo</i>), EW 5m., }			
				NE pt.			

MARITIME POSITIONS

(119)	Places	Lat. S	Lon. W	(120)	Places	Lat. S	Lon. W	
Low Archipelago	D. of Gloucester Is., 2, E, or Margaret I. (<i>Nukutipi</i>)	20° 42'	143° 5'	Society Is.	O aheite I., Papeete Harb., E. w Motu-uta Is., Its. F.	17° 31' 6"	149° 34'	
	Ann Anurunga, W Id.	20 38	143 19		Murca, or Eimeo, Mt. Tohivea, perforated pk., 3975f.	17 32' 5"	149 48 7	
	St. Paul's I. (<i>Kerekere-tue</i>), $\frac{1}{2}$ 4 l., N pt.	19 52	145 0		Tetuaroa I., EW 5m., SE pt.	17 2	149 32	
	Two Groups I., $\frac{1}{2}$ 8 l. (<i>Marokau</i> and <i>Raohere</i>), S pt.	18 18	142 12		Tapamano I., or Sir C. Saunders (<i>Muniki</i>), pk.	17 38' 7"	150 37	
	Melville I. (<i>Hikueru</i>), NW pt.	17 35	142 41		Huabene I., 2231f. Owharree harb.	16 42' 5"	151 1' 5"	
	Tekokoto [3m.], E. pt.	17 20	142 37		Ulitea, or Raiatea I., NS 14m., Uturoa harb., E	16 43	151 26	
	Furneaux I. (<i>Marutea</i>), EW 7 l., W pt.	16 54	143 20		Regent pt., or Tahaa, Tautu I.	16 33' 7"	151 30' 5"	
	Nihiru I., NS 3 l., N pt.	16 41	142 53		Bola bola I., NS 8m., sum.	16 30	151 45	
	Holt, or Yermaloff I. (<i>Taenga</i>), EW 5 l., Pass.	16 20	143 11		— Oteavanua, E. w, f, ho.	16 30	151 42	
	Philip's I., or Koutousoff (<i>Makemo</i>), $\frac{1}{2}$ 11 l., W pt.	16 26	143 58	Tubai I., [5m.], N pt. ?	16 11	151 48		
	Sacken I. (<i>Katua</i>), W pt.	16 22	144 28	Marua, or Maupiti I., 800f.	16 26' 5"	152 12		
	Romanzoff I. (<i>Tikei</i>), [3m.]	14 56	144 33	Howe I., Mopelia (<i>Mopihá</i>)	16 52	154 0		
	K. George's I., Tioka, Pyramid	14 27	145 0	Scilly Is., [2 l.], l. rls., f, P, E	16 31	154 43		
	— Ura I., $\frac{1}{2}$ 4 l., S pt.	14 44	145 14	B. lingshausen I.	15 48	154 25		
	Waterlandt, or Wilson's I. (<i>Manihi</i>), $\frac{1}{2}$ 4 l., E pt.	14 23	145 50	Marquesas.	Marquesas, w, r, b, E extr., Ariane rk., 15f.	10 21	138 25	
	Peacock I. (<i>Ahi</i>), $\frac{1}{2}$ 4 l., W pt.	14 33	146 24		Magdalena I. (<i>Fatu-hiva</i>), NS 8m., 3150f., Hanavave H'	10 27' 1"	138 39	
	Bird I. (<i>Reitoru</i>), N pt.	17 48	143 7		St. Pedro I. (<i>Motane</i>), 1640f., SE pt. rk.	10 1	138 48	
	Croker I. (<i>Huraki</i>), N pt.	17 29	143 31		Sta. Christina (<i>Tau-ata</i>), ab. 3280f., Resolution B, E side	9 56' 3"	139 7	
	Adventure I. (<i>Motutunga</i>), NW Pass.	17 3	144 25		Dominica I., 3530f. (<i>Hiva-Oa</i>), Perigot B. (<i>Panmanu</i>)	9 44' 8"	138 52' 7"	
	Raeffsky I., or Seagull grp., S & W one, Clute I. (<i>Hiti</i>)	16 42	144 9		Hood I. (<i>Fatu-huku</i>), [4m.], ab. 1180f., 1, w, P.	9 26' 5"	138 55	
	Tchitchagoff I. (<i>Tahanea</i>), NW pt.	16 46	144 58		Washington I. (<i>Ua-huka</i>), [31.], ab. 2805f., Hannay B. (<i>Motu-Haana</i>)	8 56	139 32	
	Miloradovitch I. (<i>Faaiti</i>), NW pt.	16 42	145 22		Adam I. (<i>Ua-pa</i>), 4042f., Hakahe-tau B.	9 21	140 4' 2"	
	Wittgenstein I. (<i>Fakarua</i>), $\frac{1}{2}$ 10 l., f, f, f SW Rotova Pyramid	16 2	145 36		Nukahiva, [6 l.], ab. 3800f., head of Anna Maria B.	8 55' 3"	140 47'	
	Greig I. (<i>Niau</i>), [5m.], N. pt.	16 7	146 23		Hergests rks. (<i>Motu-iti</i>), 130f.	8 41' 7"	140 36	
	Chain I. (<i>Anaa</i>), Tunhora pass.	17 20	145 30	Islands North-west of Low Archipelago.	Ma-se (<i>Eiao</i>), ab. 2000f., pk.	8 1	140 40' 5"	
	Raraka, EW 5 l., entrance	16 4	144 59		Coral R., [& sh. 2 l.]	7 53	140 22	
	Kanehi I., $\frac{1}{2}$ 14m., S pt.	15 56	145 11		Islands N. W. of Low Archipelago	Starbuck I., [1 l.], f, f, f, 15f., W. pt.	5 37	155 56
	Tiaro King's I., N pt.	15 46	144 37			Malden I., [3 l.], w, l', [f] 30f., W pt. Settlement	4 3	155 1
	Carlschoff I. (<i>Aratika</i>), W pt.	15 33	145 34			Jarvis I., 40f. [2m.], l, w, f, l, s.	0 23	159 54
	Rurick Is. (<i>Arutua</i>), $\frac{1}{2}$ 8 pt.	15 26	146 44			Caroline Is., numerous, small, 18f. l, f, f, T, South island Settlement	10 0	150 14' 5"
	Hagemeister I. (<i>Apaluki</i>), NE pt.	15 18	146 15			Vostok I., [3m.], ab. 80f., rls., f, lag., l, Boat pass.	10 6	152 23
	Elisabeth I. (<i>Toau</i>), E pt., Otani	15 55	145 50			Flint I., 50f. l, f Settlement	11 26	151 48
	Aura I. (<i>Kaukura</i>), W pt.	15 40	146 51			Sawarrow Is., 4, small, P, 15f.	13 13	163 13
	Dean, or Vlieg-n I. (<i>Nairaa</i>), $\frac{1}{2}$ 15 l., N Avatika, W pt.	14 46	147 50			Pearhyn I., $\frac{1}{2}$ 4 l., l, lag., f, f, f, P, 50f., W pass.	9 0	158 3' 5"
	Krusenstern I. (<i>Tikehu</i>), Tuheiva pass.	14 58	148 14					
	Aurora I. (<i>Makutea</i>), 230f. N pt.	15 48	148 13					
	Lazareff I. (<i>Mataiva</i> , <i>Mali</i>), [5m.], f, f, P, W pt.	14 54	148 40					
Society Islands.								
Maitea I., $\frac{1}{2}$ 7 m., P, 1597f.	17 53	148 5						
OTAKEITE I. (<i>Tahiti</i>), $\frac{1}{2}$ 12 l., Pt. VENUS, lt. F 82f.	17 29' 2"	149 29						
— Sammit, Orohena, 7321f.	17 37	149 28						

(121)	Places	Lat. S	Lon. W	(122)	Places	Lat. S	Lon. W	
Union Group	Reirson I., 60f. (<i>Rohakanga</i>), Church [2m.], l, ♀, P ...	10° 2'	161° 55'	Cook Is.	Cook Islands.			
	Humphrey I., 65f., Church (<i>Mowahiki</i>)	10 23'5	160 59		Mangaia I., [2 l.], ab, 650f. rfs. 30.	21° 55'	157° 56'	
	Bernardo, or Danger Is., 3, small, 3 125f., Puka Puka	10 52'8	165 51'5		Rarotoonga I., [3 l.], 2920f. ♀, l, r, P, NW pt.	21 14	159 45	
	Tema Reef, 3	11 7	165 35		Parry, or Mauki I., 120f., [2m.], l, ♀, 8 pt.	20 7	157 22	
	Nassau, or Ranger I., small, l, ♀, b, P, 70f.	11 33'3	165 27		Mitiéro I., 92f., NS 4m., l, [♀], Tombon W coast.	19 49	157 43	
	Union Islands.				Vatuu I. (<i>Aitu</i>), 394f., [5m.], ♀, l, SW Peak.	19 59	157 43	
	Gente Hermosa, 20f. [1½m.], or Swain's I., ♀ ♀, l, l, 10	11 10	170 52		Fenua itii (<i>Tukatea</i>), 50f., [1m.], l, ♀ ♀, l, W, w, o, E, centre.	19 49	158 16	
	Duke of Clarence I., (<i>Nukunono</i>), NS 7m., lag. l, ♀ ♀, SE l.	9 13	171 44'7		Hervey Is., 2, (<i>Mannui</i> , S, <i>Auota</i> , N), 60f., 2 2 l. l, rfs. 3m., ♀ ♀, ♀, N l.	19 11	158 49	
	Duke of York I. (<i>Outifu</i>), 2 4m., lag. l, ♀ ♀, l, l, P, ♀ ♀, 8 l., 'rees.	8 39'7	172 28		Whytootackie I. (<i>Aitutaki</i>), [8 rf. 2 3 l.], 360 l., N pt.	18 57'5	159 49	
	Bowditch I., 80f. (<i>Fika'a'o</i>), 2 7m., lag. l, ♀ ♀, l, w 8 pt.	9 28	171 9'2	Navigator's or Samoa Is.	Navigator Islands.			
Phoenix Islands	Phoenix Islands.				Palmerston Is., NS 4m., l, ♀ ♀, ♀, w, l, centre.	18 3	163 10	
	Mary or Cantoa I., 15f., West Entrance	2 8'9	171 42'5		Beveridge, Middleton, or Nicholson sh., H., NS 3 l., 2, (entr. 2), SW pt.	20 2	167 49	
	Hull Is., 5, EW 5m., l, 3, lag., ♀ ♀, w, W pt.	4 30	172 13'2		Savage I. (<i>Niue</i>), NS 11m., ♀ ♀, T, P, NW pt.	19 0	169 50	
	Snidney I., 15f., W pt., l, w ...	4 27'4	171 16		Antiope reef	18 14	168 20	
	Phoenix [2m.], 20f., l, sand, T, North point	3 42'5	170 42'5		Navigator Islands.			
	Birnie I., 6f., & rfs. [2m.], 2, l, ♀, centre.	3 35	171 33		Rose I., 33f., and rf. 1½m., l, lag., ♀, ...	14 32	168 11	
	Enderbury I., 23f., 2 3m., ♀, Pier on W side.	3 8'5	171 10		Manua I., 4 6m., 2500f., l, ♀ ♀, l, l, Tau village ...	14 14'2	169 32	
	Gardner, or Kemin I., 40f., l, lag. l, ♀, ♀, centre.	4 37'7	174 39'2		Ofu I., EW 3m., ♀, West I. Tutuila, 9 l., Hubner B. ...	14 11'5	169 39'5	
	M'Kean I., [½m.], 25f., ♀, l, l	3 35'2	174 16		— L off N, or Coxcomb Pt., Vatia	14 15'8	170 41'5	
	Rapa Island, &c.				— West cape I., lt. F	14 21	170 52	
Tubuai or Austral Islands	Four Crown, or Bass Is., 4, small, 346f. (<i>Morotiri</i>)	27 55'5	143 28'5		— Pang-o-Pango harb., [w, b, r, tower rk. W of entr.] ...	14 17'7	170 40	
	Rapa, or Oparo I., 2172f., P, w, [w], Aburei Bay, entr	27 35'7	144 17'2		Upolu, 4 16 l., 3200f., Nuu-lua islet off SE pt., 120f. ...	14 2	171 22'2	
	Osborne, or Nielson rf., 15f. East pt.	27 1'6	146 1'7		— Fangafoa B., Eids pt.	13 54'2	171 29'7	
	Maria Theresa reef?	37 0	151 13		— Apia harb., [w, w, f, 2 lts. F., 13 & 197f.	13 49'7	171 44'5	
	L'Orne bank	27 42	157 44		— Tofua Mount, Crater, [1m.], 3200f.	13 51	172 55'2	
	Haymet rocks?	27 11	160 13		— W extr. Manono I., 400f., [1m.], ♀, l, E, ♀, ...	13 50	172 4	
	Tubuai or Austral Islands.				— Safatu harb., [w] Village pt.	13 56'5	171 47'7	
	Vavitoa I. (<i>Ravivao</i>), NE pt. Tubuai I. [2 l.], vis. 10 l., [w, ♀ ♀, ♀ ♀, v, b, l']	23 50	147 40		Apolima I., [½m.], 472f., T, ♀ ♀ ...	13 49'2	172 6	
	Anchorage	23 22	149 36		Savaii I., 4 14 l., 5400f., ♀, w, r, E pt. rf.	13 42'3	172 8'5	
	Ruu tó I. (<i>Oheteroa</i>), NS 4m., ab. 1300f., South pt.	22 30	151 20		— N pt. (Matautu harb., W d., ♀ ♀, w, t, b) ...	13 28	172 21'2	
Tubuai Is.	Rimitara I., [3m.], 315f.	22 45	152 45		— South pt., Tanga	13 48'6	172 32	
	Hull I., [1 l.], ab. 66f., (8 ½) ○	21 49	154 43		— West pt., Fialalupo	13 31	172 48	

TABLE 10

605

MARITIME POSITIONS

(123) Places		Lat.	Lon.	(124) Places		Lat.	Lon.
Islands and Banks west of Samoa Is.	Verraders, or Boscawen, (<i>Niua-tabou-tabou</i>). { & rks., ab. 6m.], ab. 2000f., r	South 15° 52'	West 173° 50'	Hall I., (<i>Maiua</i>), $\frac{1}{4}$ 9m., $\frac{1}{2}$ W, 1 $\frac{1}{2}$ W, 2 $\frac{1}{2}$ R, 3 $\frac{1}{2}$ B, House on N pt.	North 1° 0' 5'	East 173° 1'	
	Good Hope I. (<i>Niu-afu</i>), 550f., P, [3 $\frac{1}{2}$ m.], NW end, vill.	15 34	175 41	Cook I., (<i>Tarawa</i>), $\frac{1}{4}$ 7 l., $\frac{1}{2}$ SW pt., Bitita	1 20 5	172 55 5	
	Zephyr reef	16 0 3	177 6	Charlotte I. (<i>Apaiung</i>), $\frac{1}{4}$ 6 l., lag. entr. SE, T, $\frac{1}{2}$ F, Lone Tree I. (<i>Ika</i>)	1 46 3	172 57	
	Wallis Is., 197f. (<i>Uea</i>). 9 $\frac{1}{2}$, 8 S, $\frac{1}{2}$ b, r, Maa Mission	13 20 7	176 10	Mathews' I., (<i>Maraki</i>), NS 5m., lag., 1 $\frac{1}{2}$ N pt.	2 1 5	173 17	
	Horne Is., 2, Alofa, $\frac{1}{4}$ K, Pk. 1200f.	14 21 4	177 56 2	Pitt I., 3 Is., $\frac{1}{2}$ F, (<i>Makin</i>), N pt. Touching I., $\frac{1}{2}$ lag., 1 W, 1, (<i>Taraturu</i>), South entr.	3 20	172 58	
	— Fotuna, Mt. Schouten, 2500f., Sigave B.	14 16	178 10		3 4 5	172 44 7	
	Bayonnaise bk., 18.	12 8	179 43	Ocean I., (<i>Paanopa</i>), { 4m., vis. 8 l., $\frac{1}{2}$ T, $\frac{1}{2}$ P, Pleasant I., (<i>Naura</i>), 100f. { 5m., $\frac{1}{2}$ T, $\frac{1}{2}$ R, P, }	South 0 52	169 35	
	Field Bank.	12 17	174 44		0 33	166 55	
	Robbie Bank.	11 3	176 53				
	Isabella Bank.	12 27	177 17				
	Tascarora Bank.	11 49	178 14				
Ellice Islands	Ellice Islands.		East	Kermadec Islands, &c.		West	
	Sophia I. (<i>Nurakitu</i>), vis. 16m.	10 46	179 31	Raoul, or Sunday Is., 1627f. mid	29 15 5	177 55	
	Rose Bank.	11 3	179 50	Havre rk.	31 18	178 59	
	Mitchell grp., (<i>Nukulaiai</i> , Fangawa I.	9 22	179 50	Espérance rk., small, 577f. \odot	31 26	178 55	
	Ellice, 2 Is., (<i>Fanafuti</i>), NS 14m., $\frac{1}{2}$ T, lag. $\frac{1}{2}$ b, $\frac{1}{2}$ W, N pass.	8 25 3	179 7 5	Macaulay I.	30 15	178 32	
	De Peyster Is., (<i>Nukufetau</i>), $\frac{1}{4}$ 9m., $\frac{1}{2}$ lag. entr. NW, 16 inside, 8 pt.	8 4	178 29	Curtis Is., 2, ab. 500f.	30 35	178 36	
	Tracy I., (<i>Oaitupu</i>), [3m.], $\frac{1}{2}$ S pt.	7 30	178 41	N Minerva I., N elbow.	23 37	178 50	
	Netherland I., (<i>Nui</i>), NS 4m., vis. 4 l., P, South I. Fantapu	7 15 7	177 10	S Minerva I., mid.	23 56	179 5	
	Lynx, or Speiden I. (<i>Nuitao</i>), small, no lagoon, Church	6 6	177 20	Wolverine shoal.	25 30	179 4	
	Hudson I., (<i>Nunomana</i>), NS 1 $\frac{1}{2}$ m., 50f., $\frac{1}{2}$ lag. no lagoon	6 18	176 20	Pylstaart I., [1m.], 700f., T, $\frac{1}{2}$ P, P.	22 20	176 12 5	
Gilbert Archipelago	St. Augustine I., (<i>Nunomea</i>), 2 Is., $\frac{1}{4}$ 2 l., $\frac{1}{2}$ T, La-kina I.	5 39	176 6	Pelorus reef 12 8.	22 51	176 25	
	Gilbert Islands.			Friendly Islands.			
	Aroral, or Hurd I., (<i>Tamoa</i>) ...	2 39	176 52	Cattow I., small.	21 30 5	174 53	
	Rotcher I., (<i>Tamana</i>)	2 33	175 55	Eoa I., NS 4 l., ab. 600f., 1 N, mid.	21 24	174 51	
	Clerk I., (<i>Onoatou</i>), N pt.	1 52	175 30	Tongatābou I., $\frac{1}{4}$ 7 l., l, w, r, b, P, Van Dieman pt. ...	21 4	175 22	
	Peru I., Francis Is., South pt.	1 27	175 59	— N side, Niukalofo. It. F ...	21 8 0	175 11 7	
	Nukunau, Byron Is., S pt. ...	1 24	176 31	Reef, (H.M.S. North Star) ...	20 50	174 30	
	Taputeuea I., $\frac{1}{4}$ 10 l., Pea-cock anchorage, $\frac{1}{2}$ T, (<i>Utiroa</i>), w, b, P, ...	1 12	174 43	Honga Hapai, (S & West of 2 Is.), [1m.], 200f., $\frac{1}{2}$ R, 1 $\frac{1}{2}$ Annamuka I., (<i>Namuka</i>), l, [1 l.], lag., l, $\frac{1}{2}$ B ...	20 36	175 21	
	Sydenham, (<i>Nonoti</i>), $\frac{1}{4}$ 7 l., lag. 1 $\frac{1}{2}$ S pt. village	0 48 5	174 28	Hapai Is., EW 16 l., S, or Fonua-ika	20 15	174 46	
	Hopper I., (<i>Apamama</i>), $\frac{1}{4}$ 10m., $\frac{1}{2}$ W, $\frac{1}{2}$ b, 2 $\frac{1}{2}$ R, Sth. pass.	North 0 21	173 51 2	Falcon I., volcano (now a shoal) Lefouka I., $\frac{1}{4}$ 5m., Mission Star. NW side, l.	20 8	174 42	
Gilbert Archipelago	Henderville I. (<i>Aranuka</i>), EW 7m., S pt.	0 8	173 37 5	Haano I., $\frac{1}{4}$ 4m., E pt., Moui-tea	20 18 7	175 25	
	Woodle I., (<i>Kuria</i>), $\frac{1}{4}$ 8m., $\frac{1}{2}$ T, (r, $\frac{1}{4}$ 3m.), 2 $\frac{1}{2}$ W, b, N pt. of reef	0 19	173 22	N Id., or Ofo-langa, [1m.] ...	19 48 2	174 20	
				Kao I., [1 l.], pyr., 3030f., 1 Tufua I., [5m.], ab. 1890f., 1 Coral rf., (Sir E. Home)	19 41	174 14	
				Latte I., [1 l.], ab. 1790f. ...	19 36	174 26	
				Vavu I., (<i>Hafuluha</i>), $\frac{1}{4}$ 4 l., 600f., W pt., (Port Refuge to SE d., 2 $\frac{1}{2}$ R, 2 $\frac{1}{2}$ W) ...	19 42	175 0	
				— Port Valdez, Sandy pt.	19 45	175 3	
				Toku I., [2m.], 82f.	19 2	174 44	
				Amargura I., (<i>Fanualei</i>), l, $\frac{1}{2}$ P, 1230f.	18 49	174 37	
					18 39 0	174 37	
					18 38 3	174 1	

MARITIME POSITIONS

(123)	Places	L at S	Lon. W	(126)	Places	Lat. S	Lon.
Fiji Islands.				West			
Ono Is., peak 370f.	20°40'	178°42'		Nanuku reef, <i>Nanuku Levu</i> } at S extreme, 70f.	16°43'	179°26'5	
— Simonoff (<i>Tuvana-i-</i> <i>thole</i>), 95f.	21 2	178 48		Nuku-Mbasanga I., 70f., small	16 18	179 147	
Beregis reef (<i>Vasata Ono</i>)	20 44	178 51		Ngele Levu rf., EW 10m., } Ngele I., 60f.	16 53	179 87	
Vatou, or Turtle I., [2m.] } 209f. $\frac{1}{2}$ f., rf. SE, w. $\frac{1}{2}$ f. }	19 49'4	178 13		Va-tanua I., small, 90f., mid.	15 57	179 24	
Nuku Singea rf., [2m.], 3f. }	19 14'2	178 20'7		Badd reef, Thombia I., 590f., } pk.	16 27'5	179 39'7	
Ongea I., (3 Is. & rf., $\frac{1}{2}$ }	19 12'5	178 25		Thikombia I., (Farewell), } Nat. of the Is., $\frac{1}{2}$ 3m., } rfs., Is., <i>Nanuku Vatu</i> , 480f. }	15 45	179 53'5	
Fulanga I., (<i>Ongea Ndriki</i>) } 300f., $\frac{1}{4}$ 5m., $\frac{1}{2}$, 260f. }	19 7'5	178 32		East			
Namaka I., E pt., 260f.	18 51	178 35		Tiviuni I., 4040f., $\frac{1}{2}$ 8 l., }	17 1	179 56	
Mothe I., 590f., peak	18 39	178 30		South Cape.....	16 32'5	179 59'7	
Kambara I., 470f., NS 3m., }	18 9'5	178 56'5		Rambe I., 1550f., C. Georgia	16 6	180 6'5	
S pt.	18 43'5	179 5		Vanua Levu I., $\frac{1}{2}$ 33 l., }	16 48'7	179 18	
Tavunasithi, 300f., small	18 22	179 16		2428f., E, or Undu Pt., }	17 1	178 44'7	
Vanua Vatu I., [2m.], A, }	18 38	179 31'5		<i>Nu Pota</i> }	16 49	178 19	
$\frac{1}{2}$, P., 310f., peak	18 57	179 48		— Savu Savu Pt.	16 42	178 55'5	
Tova I., <i>Nu Vatu</i> , [3m.], }	18 36'3	178 45		— S extr., Vuya Pt.	16 10	179 5	
N pass.	18 32'5	178 27'5		— Yendua I., pk., 6412 W }	18 31	179 58'5	
Totoya I., [6m.], 1184f., peak				N pt. of reef	19 10	179 45	
Olorua I., 250f., peak	18 26'5	178 20'5		— N extr. of rf. lining N }	17 14	179 26	
Thakaan I., <i>Lakuleka</i> reef, }	18 12'3	178 42'2		coast, 3m. off Kia I., 780f. }	17 38	179 17	
[3m.], NE pt.	18 21'3	178 13'7		Moala I., [& rfs., $\frac{1}{2}$ 4 l., }	17 47'5	179 25	
(<i>Onesta</i> Passage.)	17 58	178 25'5		ab. 1535f., $\frac{1}{2}$ f., (rf. 3m.), }	18 0	179 17'2	
Onesta, 160f., l., [& rfs. }	17 55	178 21		N pt. of reef	18 14'2	179 19	
EW 8m.], E islet	17 58	179 2		Matuku I., 1256f., [& rf. }	17 36	179 1	
Lakemba I., $\frac{1}{4}$ 3m., ab. }	17 47	178 40		NS 4m.], Matuku harb. }	17 28	178 58'5	
720f., $\frac{1}{2}$ peak	17 43	179 16'5		Goro I., (<i>Koro</i>), NS 9m., }	17 22'5	178 47	
Bukatatanoa or Argo reefs, }	17 42'5	178 48		1710f., $\frac{1}{2}$ NW, N pt.	17 40'7	178 51'0	
SE extreme	17 31	178 42'7		Horse-shoe I., (<i>Thackau-</i>	18 10'2	178 31'5	
— North extreme	17 25'5	179 31'5		momo), [1m.], $\frac{1}{2}$ N pt.	18 8	178 42	
Reid reef, Reid haven	17 14'3	179 30'7		Nairai I., NS 4m., (rfs. }	18 8	178 26	
(Lakemba Passage, N-d. of do.)	17 12'7	178 39		4m.), Needle Pk., 1078f. }	17 53	177 15	
Naiiau I., $\frac{1}{4}$ 5m., 580f., sum....	17 9'5	179 0'2		Ngau I., pk., 2345f. EW }	17 51	177 57'5	
Hawkins rf., <i>Thakau Lase</i> }	17 1	179 16		8m., (rfs. S, W).....	17 40'5	177 7	
<i>marawa</i> , rks. 3f.	16 58	178 46'5		Mumbolithe I., small, S pt. ...	17 17	177 9	
Gordon rf., [2m.], <i>Thakau</i> }	16 46	179 7		Mbatiki I., (<i>Daveta Naka</i> }	17 9	176 54	
<i>Tambu</i> , N pt.				<i>Suvu</i>), [1 l.], rf.	17 5'5	177 16	
Thithia, 540f., NE pass., }				Wakaia I., NS 4m., 595f., E pt. }	16 43	177 31'5	
NS 4m., $\frac{1}{2}$ f., SW pt., }				M. kongai I., NS 3m., rfs., }			
(rf. W 3m.)				S pt.			
Tavutha I., $\frac{1}{4}$ 4m., S pt., }				(Mokungai Passage.)			
(rfs. $\frac{1}{2}$), 800f.				Vatu e thake, or Passage I., }			
Katafanga I., 180f., small, }				small, 304f.			
rfs. pk.				OVALAU I., $\frac{1}{2}$ 8m., 2089f. }			
Mango I., 670f., [4m.], SW lt.				LEVUKA, SITE of SCHOOL-			
Vatu Vara I., 1030f., NS }				HOUSE, (Its. F 240 & 193f.)			
4m., pk.				Viti Levou, EW 29 l., }			
Ythata I., 840f., [& rf. EW }				4000f., $\frac{1}{2}$, Rewa roads, }			
5m.], Boat pass.				Nukulau I.			
Exploring Is., & rfs., $\frac{1}{2}$ 8 l., }				— Nasalai reef, lt. Fl. 45f. }			
E reef, Nuku Thikombia }				— Suva harb., $\frac{1}{2}$ w, h, $\frac{1}{2}$ o, }			
Cairn, 6f.				Suva pier, (Its. F 320 & }			
— Munia, 950f. pk.				125f.)			
— Vanua Mbalavu, 930f., }				— West extr., Navula Pt. ...			
Black Swan pt.				— Munai Vatu Pk., 4000f. ...			
Naitamba I., $\frac{1}{4}$ 5m., sum. }				Mananutha grp., Hudson's }			
610f.				Is., Mana I.			
Look-out rf., EW 6m., E pt....				— Waia I., $\frac{1}{2}$ 5m., sum., 1874f. }			
Wailangilala I., 70f., small, }				Yasawa group, west extr. of }			
Ship pass.				the Is., Wiwa I., [2m.], }			
				(chl. S)			
				— Naviti, 740f., pk.			
				— Timboor I.			

Fiji Is., Eastern Archipelago

Fiji Is., Western Archipelago

TABLE 10

60°

MARITIME POSITIONS

(127)	Places	Lat. S	Lon. E	(128)	Places	Lat. S	Lon. E
Fiji Is.	Round I., (<i>Leva Kalou</i>), } 500f., small, (1 W-d.) ... }	16°40'	177°46'	New Caledonia.	New Caledonia, ¾ 63 l., }	22°15'5	167° 3'5
	Vatu Leile I., 110f., ¼ 8m., }	18 31	177 37		5360f., E pt., Nau I. }	22 2	166 52'5
	l, ½, 1 N. W pt. }	18 36	177 48		C. Coronation (Unia)	20 17'2	164 29'0
	Thakau Lekleka or Flying }	18 23	178 8'2		Balade harb., ½ ½, (rfs. 2 l.), Id. }	19 18'5	163 57
	Fish shl. }	18 31'3	177 59		NW extr., Tia I., (shl.) }	20 22'5	163 49
	Mbenga I., [5m.], ½ W, }	18 53	178 29'7		Yandé I., peak 1000f. }	20 45	164 22
	pk. 1430f. }	18 58'5	178 22		C. Deverd., (shl. 3 l.) }	22 1	165 57
	— S pt. of rf. round lagoon ... }	18 38	178 32'2		Port St. Vincent, ½, ½, ½, }	22 16'2	166 27'2
	Ono I., [5m.], ½ pk. 1110f. }	18 41'3	178 31'5		¾ ¾m., ½ f., Entr., (rfs. }	22 29	166 29
	Kandavu, Mt. Challenger, }	19 5	178 11'2		¾ ¾m.), Tenia I. }	19 31	163 35
	2180f., ¾ 9 l., ½ ½, }	19 8	177 57		D'Entrecasteaux rfs., SW }	18 40	162 46
	(½ ½m.) }	15 32	175 20		pt., Boat pass. }	17 54	162 56
	N. Astrolabe reef, Solo I., }	12 29'3	177 7'5		Huon Is., Bond reef, [½m.], }	21 0	161 46
	lt. FL 96f. }	12 21	177 50		l, ½, (rfs. 3 l.), N extreme, }		
	Great Astrolabe reef, N pt. }	11 47	173 13		Three rocks 20f. }		
— N'galoa harb., N'galoa. }	12 11	172 5					
— Denham I., W extreme ... }	11 55	170 10					
Hammond reef	11 36	169 40					
Rotumah I., 900f., ¾ 3 l., }	12 21	168 43					
¾ ¾, ½, P., Oinafa. }	21 45	174 37'7					
Eagleson reef	22 20	171 20					
Charlotte bk., W. }	22 24	172 5					
Pandora rf. }	23 14	170 5					
Mitre I., (<i>Futaka</i>), [1m.], }	22 38	168 56'7					
vis. 4 l., ½, P. }	22 2	168 39					
Cherry I., (<i>Anuda</i>), [3m.] ... }	29 3'7	167 58					
Tucupia, [3m.], 3000f., T, }							
¾ ¾, P. }							
Conway rf., [2c.], 6f., T }							
Mathew rk., [½m.], volcanic, }							
465f., ½, ... }							
Hunter I., [½m.], 974f., ½ ... }							
Brilliant shoal							
Walpole I., [1½m.], 229f., }							
¾, ½, P., S pt. }							
Durand I., [½m.], 880f., T, 8... }							
NORFOLK I., 1039f., Sydney }							
B., flag staff							
Loyalty Islands.				New Hebrides.			
Maré or Britannia Is., 8 pt...	21 40	168 1'2		Aneityum I., EW 31. 2788f., }	20 15'3	169 44'7	
— E pt., C. Coster.....	21 24	168 7'5		¾ ¾, b, P., P. Inyeu }	19 31	170 11	
— Tandine B., ¾	21 32	167 50		Erronan I., (<i>Futuna</i>), }	19 31'3	169 27'5	
Boucher I., 90f. [4m.], ½, }	21 5'5	167 49		[1 l.], 1931f., NW pt. }	19 32'4	169 24'5	
mid. }	21 1	167 24		Tanna I., ¾ 8 l., ½ ½, r, P., }	19 16	169 37	
Chabrol I., E pt., C. Pine.....	20 45	167 8		Port Resolution, ½ }	18 47'5	168 58	
— Wreck Bay	21 9'5	167 18'5		— Volcano, 4m. inland, 980f. }	17 33'3	168 16'7	
— SE pt., C. de Flotte	20 43	166 36		Imner I., small, l, P. 140f. ... }	17 3'1	168 24'5	
Uvea or Halgan I., [6 l.] }	20 28	166 30		Kromango, Dillon Bay, on }	17 16	168 28	
— Oidiy I., Bishop Id. }	20 22	166 14		W side, w }	16 47'5	168 10	
Beaupré Is., [2 l.], l, ½, NE }	19 50	165 56		Sandwich I. (<i>Efate</i>), ¾ 10 l., }	16 30'5	168 21	
Id. }	18 35	164 22		¾ ¾, Havannah har- }	16 14	167 54'7	
Astrolabe rfs., 2, ¾ 10 l., }	22 42'5	167 28'5		bour. }	15 40	168 8	
½, East reef	23 1	167 2		Three hill I., (<i>Mai</i>), 2171f. }	14 58	168 2	
Petrie reef, 20f., ¾				(rf. E pt., B) }	15 19	167 43	
l of Pines, [3 l.], lag., ¾ W., }				Monument rock, 397f., [1 l.], }	16 25'5	167 47'5	
¾ ¾, P., Alemene I. }				(ls W-d.) }	15 58'5	167 10'7	
SE elbow of ½				Ap I., 2800f., [6 l.], Dia- }	15 43	167 15	
				mond B., (<i>Onamavit</i>) ... }	15 38	166 46'5	
				Lopevi I., 4755f., pk. }	14 38	166 39	
				Ambrym I., 4380f., EW 6 l., }	15 1'3	167 5'5	
				Dip Pt. }			
				Pentecost I., (<i>Arugh</i>), NS }			
				11 l., 2000f., Steep Cliff B. }			
				Aurora I., (<i>Muino</i>), NS 11 l., }			
				2000f., ¾, w, b, Laika rere }			
				Lapers I., (<i>Aoba</i>), 4000f., }			
				Duin Dui			
				Mallicollo I., ¾ 18 l., Port }			
				Sandwich, ½ }			
				— Espiègle B. }			
				St Bartho omew I., (<i>Malo</i>), }			
				EW 3 l., ialet SE pt. }			
				Espiritu Santo I., ¾ 22 l., }			
				EW pt., or C. Lisburne ... }			
				— North pt., or C. Cum- }			
				berland			
				Port Olry			
				Pic de l'Etoile, (Star I.), }			
				(<i>Merakaka</i>), 2900f., [1 m.], }			
				pk., ¾, P. }			

MARITIME POSITIONS

(129) Places		Lat. S	Lon. E	(130) Places		Lat. S	Lon. E
Banks Is.	Claire I., (<i>Merig</i>), small, 200f.	14° 17'	167° 48'	Gower I., [4 l.], 4, 7, 8	7° 56'	160° 28'	
	Vanna Lava, 3120f., P. Pat-	13 48	167 30.5	pt.	8 19	160 9	
	teson. Nusa Pt.	14 17	167 25	Ramos Is.	9 50.5	160 48.7	
	Santa Maria, (<i>Gewa</i>), 2300f.	13 32	167 20	Guadalcanal I., 26 l.	9 59	160 35	
	Lakova B.	13 15	166 33	Marau sound, Ferguson I.	9 45	160 0	
Santa Cruz Is.	Bligh I., (<i>Ureparapara</i>),			— South pt., C. Henslow	9 41.8	159 39.5	
	2440f., peak			— Mt. Lammas, A, 8000f.	9 49	159 47	
	Torres Is., (<i>Ababa</i>). Tegua			— North extr., C. Espérance	9 14	159 41	
	I., 600f., Hayter B.			Florida I., 1500f., Mboli hr.,	9 35	160 17	
				Tree I.	8 53.5	160 1	
Santa Cruz Islands.				Buena Vista I., 1050f., pt.	9 5	159 3	
Solomon Is.	Vanikoro I., La Pérouse. 4 $\frac{1}{2}$	11 37	166 51.5	Russell Is., 1600f., Pavuvu	9 1	158 40	
	14m., sum. 3031f.	11 40.4	166 55.0	Pt.			
	— Ocili harb., on E side, 2 $\frac{1}{2}$	11 20	166 30	Murray I. (<i>Barakoi</i>) [1m.],			
	Tonpoua I., (or Edgecumbe),	10 41	166 8	1000f.	8 30.5	159 32	
	Basilisk hr.	10 53	165 52.5	St. George I., 4 $\frac{1}{2}$ l., N,			
Solomon Is.	Sta. Cruz I., (<i>Ndeni</i>), 1800f.	10 24.3	165 46.7	Astrolabe Creek, 2 $\frac{1}{2}$ w,			
	4 $\frac{1}{2}$ 8 l., E pt., C. Byron....	10 17.5	166 18.5	r., F, P., 8 cove			
	— 8 pt., C. Mendana	10 6.2	165 41.7	Isabel I., 4 $\frac{1}{2}$ 40 l., S pt.,	8 36	159 44.5	
	Volcano I., (<i>Tinakula</i>)....			2050f., C. Prieto (Vi-			
	Swallow group (<i>Matema Pu-</i>			tora I.)	8 14	159 26	
Solomon Is.	nasi), 180f.			— Mt. Marecot, 3900f.	7 25.5	158 18.5	
	— Anologo, 120f.			— Port Praslin	7 19	158 6	
	Goldfinch shoal			— C. Comfort, (rfa. 2 l.)			
	Duff or Wilson group, NW			New Georgia I., (<i>Narow</i>),			
	extreme			EW 14 l., Ia. (W d.), S	8 48	158 15	
Solomon Islands.				pt., or C. Pitt, <i>Garukai</i>			
Ida. N.E. of Solomon Is.	— Disappointment I., 1200f. ...	9 57	167 0	Rendova I., 2500f., C. Pleas-	8 45	157 24.5	
	— SE extr., Bass Is., 200f.	10 1	167 5	ant			
				— Rendova harbour	8 23.5	157 19	
				— Kolikars Inlet	8 10.3	157 17.5	
Solomon Is.	Stewart Is., 150l., 5 on a rf.,	8 21.5	162 42.5	Eddystone rk., (<i>Narova</i>),			
	[2 l.], 1, 7, 7, 1, 1, <i>Nikaima</i>			1100f., P., (chis. 1, 1	8 16.1	156 29.5	
	Rondeor, or Candelaria rfa.,	6 13	159 13	3m.), harb. on W coast...			
	rock, 10f.			Guizo I., 4 $\frac{1}{2}$	8 57	156 50	
	Ontung Java, or Lord			Vella Lavella, C. Middleton,	7 38	156 20	
Solomon Is.	Howe's Is., (<i>Levenauoa</i>),			3000f.			
	SW ext., Tonkousa I....			Choiseul I., 1800f., 4 $\frac{1}{2}$ 33 l.	7 29	157 49	
	Frindsbury rf.			E pt., C. Labée	7 7	156 40	
	Tasman's Is., Numanno S pt			— Bambatani	6 40	156 34	
	Mortlock, or Marqueen			— Kangopassa			
Solomon Is.	Is., EW 7 l., centre			— Choiseul B., Redman I.,	6 43.3	156 24.5	
	Nine Is. of Carteret, 60f.,			(shl. 2 l.)			
	4 $\frac{1}{2}$ ab. 10 l., Green I.			Shortland Is., 676f. [6 l.],	7 8	155 52.7	
	Trading station			SE pt., C. Stephens			
				Treasury Is., (<i>Mono</i>), [3 l.],	7 24	155 34	
Solomon Is.	Sta. Catalina I., 320f., (<i>Yo-</i>	10 54	162 26.5	1, 7, Blanche harb., Wat-			
	riki), pt.			son I.			
	St. Anna I., (<i>U-ah</i>). [4m.],			Bougainville I., 4 $\frac{1}{2}$ 44 l., C.	6 42.5	155 58	
	520f., 7, 7, Port Mary ...			Friendship, E end			
	St. Christoval I., (<i>Robata</i>),			— C. Le Cras, (Id., [2 l.])?	6 0	155 20	
Solomon Is.	4 $\frac{1}{2}$ 25 l., 7, E pt., or C.			Gazelle harbour	6 35	155 5	
	Survile			— Mt. Balbi, 10,171f., 5 l.,	5 56	154 54	
	— Makira harbour			inland			
	— NE pt., C. Recherche			— C. l'Averdi	5 30	155 1	
	Three Sisters, 4 $\frac{1}{2}$ 3 l., 250f.			— Buka I., 7, 7, N Cape	5 0	154 35	
Solomon Is.	N one, (<i>Alita</i>)			— Summit of Buka I., 1306f.	5 16	154 33	
	Contrariété I., (<i>Ulausa</i>), NS			— Queen Carola harbour	5 10	154 29	
	7m., 1200f., pk.			Indispensable rf., S pt.	13 2	160 31	
	Ugi I., 676f., Selwyn B.			— NW pt.	12 15	159 59.7	
	Maleita I., (<i>Mala</i>), 4 $\frac{1}{2}$ 34 l.,			Rennell I., 400f., 4 $\frac{1}{2}$ 12 l.,	11 52	160 40	
Solomon Is.	8 pt., or C. Zélé			SE pt.			
	— Mt. Kolovrat, 4275f.			Bellona I., 400f., [3 l.], SE			
	— Alit Bay			pt.			
	— NW pt., C. Astrolabe,						
	Mallu harbour						

TABLE 10

609

MARITIME POSITIONS							
(131) Places		Lat. S	Lon. E	(132) Places		Lat. S	Lon. E
New Ireland and New Britain.				Rooke I., $\frac{1}{2}$ 7 l., A, $\frac{1}{2}$, } Dampier Strait, Luther } Anchorage, C. King } — Tupinier I., [1 l.], A, < }		5°28'3"	147°46'7"
Islands N.E. of New Ireland.	Sable reef	3°33'	154°36'	Lottin I., [4m.], upw. of 5000f.	5 18	147 36	
	Fead Is., or Abgarria, $\frac{1}{4}$ 9 l., } l., $\frac{1}{2}$, S, or Goodman I. }	3 24	154 43	Long I., NS 5 l., Réaumur }	5 16	147 6	
	Lyra sh., $\frac{1}{4}$ 4 l., $\frac{1}{2}$ or 5, } centre	1 53	153 28	Pk. at N end, 2000f. }	4 54	149 5	
	Sir Charles Hardy, or Veres }	4 30	154 13	Mérite I., 2150f., EW 4m., mid.	4 32	149 4	
	Is., 330f., [6 l.], E pt. ... }	4 3	153 45	North I., small, hot spring, }	4 16	149 16	
	St. John I., 450f., [3 l.], }	4 16	148 10	shoal, 5m. NW	3 57	147 58	
	$\frac{1}{2}$ 1, $\frac{1}{2}$, E pt. }	3 32	153 30	Gipps I., hot springs	3 15	148 16	
	Kaan Is., [1 l.], (rky. Isl. }	3 8	152 39	Victoria reef	3 18	147 40	
	2 l., centre	2 50	152 43	Albert reef	3 20	146 50	
	Gerret Denys I., [5 l.], 1600f., }	2 36	152 1	Sherburne rf., EW 4 l., rka. }	2 55	146 49	
	(highest of these islands). }	1 40	150 30	20f., SE part	2 51	145 54	
$\frac{1}{2}$ 1, P, mid. }	1 40	149 40	Circular rf., [1 l.], T, (a }				
San Francisco I., 650f. }			lag. NW)				
Gardner I., and Fisher's I., }			Sydney sh., rks. }				
(3 ls. E-d., a sh. W-d ?) }			Elizabeth I., [2m.], l, $\frac{1}{2}$, }				
NS 10 l., ab. 1600f., N pt. }			[1] NE, P				
Fisher I. }			Purdy Is., $\frac{1}{2}$, 3 ls., P., (Mole, }				
Squally I., [3 l.], l, $\frac{1}{2}$, }			Mouse, & Bat), Bat I. ... }				
(small Id. S-d., $\frac{1}{2}$ o)							
Mathias' I., [8 l.], A, vis. }							
45m., (Tombara), sum. }							
Cape Santa Maria							
— Holy Haven, S side							
New Ireland, W pt., C. Teschke }							
— Port Carteret, $\frac{1}{2}$ o, Cocoa- }							
nut I., 800f., NE pt., }							
w., w N, $\frac{1}{2}$, $\frac{1}{2}$							
— Port Praslin, $\frac{1}{2}$ o, SE corn., w }							
— C. St. George							
Sandwich I., [4 l.], pk. 600f. }							
Mansoleum I., Byron Strait, }							
656f. }							
New Hanover, 1640f., $\frac{1}{2}$ }							
13 l., N pt., or C. Salomon }							
Sweet							
— W pt., C. Queen Charlott }							
Portland Is., EW 7m., 4 l. }							
large L. }							
Duke of York I., [3 l.], w, }							
f., Port Hunter, N side, }							
Mitchell Pt. }							
Father and Son reefs, Father }							
reef							
New Britain, $\frac{1}{2}$ 85 l., }							
Blanche B., Matupi I. ... }							
— Father Pk., vol., 4000f. ... }							
— C. Palliser							
— SE pt., C. Orford, l., SE extr. }							
— C. Quoy (pk. $\frac{1}{2}$ 3m.)							
— Pt. Beechey							
— Port Montague, $\frac{1}{2}$, w, }							
r, Pt. Roebuck							
— South Cape, rky. islet ... }							
— C. Ann							
— C. Gloucester							
Duportail Is., sum							
Willames I., NS 5 l., S pt. ... }							
Whirlwind reef, centre							

TABLE 10

MARITIME POSITIONS

(135) Places		Lat. N	Lon.	(136) Places		Lat. N	Lon. E
Bonin Is.	Pearl & Hermes rf., SE I.	27° 47' 8"	175° 51' West	Detached Is. and Reefs	Grampus Is. (Sebastian Lobo?) E.D.	25° 10'	146° 40'
	Midway I., SW pt. of Sand I., 57f.	28 12	177 22		Marcus I., 60f.	21 14	154 0
	Cure I., (Ocean, Stavers), 4, Sand Island, 20f.	28 25 7	178 29 7		Wake, or Haleyon I., [3m.], 4, lag., 4, f. o., w. o., f. 8f.	19 11	166 31
	Bonin and Volcano Islands.		East		Gaspar Rico, or Cornwallis, (Tsang), vis. 5m., Scylla rks., NS 21.	14 50	169 5
	Bonin Is., N 3 14 l., N, or Parry's grp., 4, 3 l., Nrk.	27 45	142 7		Marshall Islands.		
	Kater I., [4 rks. 1 1/2 m.], N rk.	27 31	142 12		Bikar, or Dawson Is., [4 l.], 9f. S I.	12 14	170 15
	Peel I., NS 5m., SW islet.	27 2	142 10		Button, or Kutusov Is. (Uitrik), N I.	11 18	169 54
	— Port Lloyd, E. w., b. r., f. Kyosé.	27 5 6	142 11 5		— S grp., Taka Is., S pt.	11 3	169 46
	Bailey Is., Ane Tima	28 33	142 9		Krusenstern, Tindle & Watts Ailuk, Is., 4, 5 l., Kapeniur I.	10 27	170 0
	Rock, I.	29 37	141 58		Count Heiden, or Lekieh Is., 4, 8 l., S pass. 14f.	9 49	169 22
Islands South of Japan	Rosario (or Disappointment) I., 148f., [1m.], rky., 1, 4, 6.	27 16	140 51	East chain, Ratak Is.	Jemo I., or Steep to	10 6	169 42
	Volcano Is., S, Sulphur I., 4, 5m., 644f.	24 48	141 20		New Year I., (Mudi), NS 3m., 1, 4, 4.	10 18	170 55
	— N Id., San Alessandro, 2534f.	25 24	141 18		Chatham Is., N grp., Romanzoff, (Oldia), Port Noel, E islet.	9 28	170 17
	— S Id., San Augustin o, 3039f.	24 18	141 28		— S grp., Erikub, 4, 8 l., S extr., (Arik)	8 55	170 8
	Forfana (late Arzobispo) I.	25 43	140 43 5		Calvert Is., 4, 10 l., NW one, (Kaven)	8 51	170 49
	Rock, 7f.	24 2	137 59		— South extreme	8 30	171 10
	Rica de Oro rk., or Lot's Wife, 466f.	29 45	140 22		Inoetson Is., (Aurh), 4, 4 l., NE pt.	8 21	171 2
	Rasa I., 4, 5m., 4, 220f.	24 30	131 22		Arrowsmith Is., (Majuro), 4, 6 l., Caroline I., W. pt.	7 10	171 13
	Borodino Is., 2, NS 4 l., 4, Sandy, R, N one, 40f.	26 2	131 20		Arho Atoll, Ine I.	6 53	171 43
	Parece Vela (Bishop Douglas Nautilus), a rk 12f., in a lag., [1 l.], 4, 4.	20 28	136 13		Mulgrave Is., [6 l. ?], small, rfs., 10, Port Rhin.	6 14	171 46
Mariana Is., or Ladrões	Ladrones.			West chain, Ralik Is.	Keats shoal, 2.	5 55	173 38
	Santa Rosa shoal.	12 30	144 15		Boston, or Elbon Is., Jurij I.	4 36 5	168 41 5
	Guam, or Guahan I., 4, 9 l., Cocoa I.	13 13	144 38		Bonham Is., (Jalut), 4, 8 l., SE pass.	5 55 5	169 43
	— San Luis de Apra, E. w. r., fort.	13 25 8	144 39 5		Hunter I., [2m.], (Kili)	5 42	169 9
	— North pt., Ft. Ritidian.	13 39	144 51		Baring Is., Namorik.	5 35	168 5
	Rota I., 4, 4 l., about 800f.	14 7 5	145 13		Elmore, or Odia Is., 4, 7 l., South Pass.	7 15	168 48
	Aguijan I., [1 l.], centre.	14 51	145 31		Musquillo Is., 4, 12 l., rfs., 10, W pt. Namu I.	8 14	168 3
	Tinian I., NS 4 l., 10 N, Anson's R. at SW part, 4, w, r, Anson Bay.	14 59 4	145 36 2		Lib I., 14f.	8 19	167 28
	Saipan I., 4, 4 l., ab. 1200f., 4, w, r, (rf. W-d.), N pt.	15 17 5	145 46 5		Mentschikoff Is., 4, 20 l., Ebodon I.	9 22	166 53
	Biri I., or Farallon de Medinilla, 4, 2m., ab. 50f. rks.	16 0	146 0		Line I., W pass.	8 58	166 27
	Anatxan I., 4, 4, 4, f, E pt.	16 20	145 41		Uja, or Catharina Is., NW I.	9 21	165 36
	Sariguan I.	16 40 5	145 46		Schurz Is., 4, 5 l., Wotho I., 14f.	10 10	166 6
	Zealandia bank (Piedras de Torres) 4.	16 52	145 49		Rongelab, or Pescadores Is., 14f., P. o. South I.	11 15	167 0
	Guguan I., NS 2m., E pt.	17 18 5	145 51 5		Rongerik Is., 4, 18 l., Boek I.	11 24	167 35
	Alamagan I., 2316f., E part.	17 35	145 52		Ailinginae Is., Knox I.	11 4	166 36
	Pagan I., W end. 1000f.	18 3 5	145 53		Bikini or Eschholts Is., 4, 7 l., NW extr.	11 42	165 25
	Agrigan I., P., W end.	18 50	145 37				
	Assumption I., [3m.], 2848f., 4 W, 4, 4.	19 45	145 29 0				
	Urracas, 3 rks.	20 0	145 21				
	Farallon de Pajaros, 1089f. ...	20 32	144 54				

MARITIME POSITIONS

(137)	Places	Lat. N	Lon. E	(138)	Places	Lat. N	Lon. E
	Eniwetok, or Brown's group. [8 l.], $\frac{1}{2}$ $\frac{1}{2}$ o. lag. P. o.	11° 31'	162° 5'		Suk I., or Pulusuk I., NS. 2m., l. $\frac{1}{2}$	6° 40'	149° 21'
	West Point				Lanthe and Nile Shoals. [$\frac{1}{2}$ m.], sf., P.D.	15 53 5 32	145 39 145 42
	— SE islet, or Parry	11 21	162 25		Pikelot Coquille, [$\frac{1}{2}$ m.], on a rf., $\frac{1}{2}$ $\frac{1}{2}$ P. o.	8 9	147 42
	Arecifoa, or Providence Is., rf., $\frac{1}{2}$ o. P., Uyelang I., 14f. }	9 42	161 1		Fau I., West rf. $\frac{1}{2}$ 5m., islet in middle, $\frac{1}{2}$	8 3	146 50
	Greenwich Is., (<i>Kapinga</i> - <i>marangi</i>)	1 4	154 45		Satawal (Tucker) I., [1m.], P	7 22	147 6
	Indiana reef	3 20	160 18		Swede Is., (Lamoirek), 6, $\frac{1}{2}$ $\frac{1}{2}$ 2 l., S & E islet	7 27	146 31
	Two Is. (reported 1877)	0 0	146 0		— Elato Is., NS 21, N pt.	7 30	146 19
	Caroline Islands.				Olimarao Is., $\frac{1}{2}$ 2m., N islet ..	7 43	145 56
	Ualan I. (Strong I.), $\frac{1}{2}$ 8m., Coquille Harb. on NW side, $\frac{1}{2}$ w. r. NE islet ..	5 21 3	163 0 7		Farauk p Is., 3, [2m.], lag., S pt.	8 35	144 36
	— Mt Crozer, ab. 2155f.	5 19	163 2 5		Ifalik Is. (Wilson), [2m.], lag., SW extr.	7 14	144 30
	Pingelap, or MacAskill Is., 3, [2m.], Tugula I.	6 14 5	160 52		Ulio Is. (Thirteen Is.), EW 6m., E, or Raur I. (th 15 E, [SE), N pt	7 21 5	143 57 5
	Duperrey Is. & rf., $\frac{1}{2}$ 3m., or Mokil I., S pt.	6 39	159 53		Iaripik (Kama), 2 Is., $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ m., E pt.	6 40	143 11
	Seniavina Is., 3grps., $\frac{1}{2}$ 13l., Ponapi I., EW 5 l., $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ P., Tolocolme Pk., 2861f.	6 53	158 12		Sorol, Philip Is., S.E. I.	8 6	140 24
	Andama Is., $\frac{1}{2}$ 3 l., rfa., S pt.	6 44	157 54		Feys, or Tromelin I., [1m.], l. $\frac{1}{2}$, no lag., $\frac{1}{2}$ o. l., 80f.	9 46	140 35
	Pakin, or Pagenema Is., Kapenuar I.	7 6	157 43		Uluthi Is. (Mackenzie), $\frac{1}{2}$ $\frac{1}{2}$ 7 l., lag. l. $\frac{1}{2}$, N extr., Mogmog I.	10 6	139 46
	Ngatik Is., EW 3 l., l. $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ l. P., E pt.	5 48	157 31 5		— S extr., Pugelug I.	9 46	139 41
	Bordelaise I., S. Augustin I., 107f., [$\frac{1}{2}$ m.], $\frac{1}{2}$ (8 NW, rf. SE 3 l.)	7 37	155 9		Yap I., 1150f., NS 31., $\frac{1}{2}$ (rf.) S-d., Tomil B., lt. F., 25f.	9 25	138 6
	Monteverde Is., Nukunor, E pt., $\frac{1}{2}$ 2 l., lag.	3 52	155 0		Hunter's reef.	9 58	138 23
	Mortlock Is., $\frac{1}{2}$ 6 l., $\frac{1}{2}$ L., Nukunor I., EW 7m., lag. Port Chamisso, $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ ww., Entr.	5 20	153 58		Matelotas Is. (Ngoli), $\frac{1}{2}$ 9 l., l. $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ S l.	8 15	137 35
	— Etal Is., NS 4m., N pt.	5 37	153 42		— North I., 150f.	8 35	137 40
	— Ta, or Sotoang grp., S pt.	5 17	153 48		Pelew Islands, &c.		
	Namoluk Is., 100f., (<i>Tai</i> - <i>nowe</i>), 3, $\frac{1}{2}$ 3m., l.	5 55	153 16		Palao or Pelew Is., $\frac{1}{2}$ 29 l., $\frac{1}{2}$ P. (rfa. NW-d.), Korror H'	7 19	134 32
	Lospal I.	6 53	152 43		— Kajangle I., [2m.], (rf.) $\frac{1}{2}$ 4 l.)	8 3	134 38
	D'Urville I., 3 islets on a rf., l. $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$	6 59	152 34		— Baobeltoab, N extr., reef — Angaur I., 4m., w. l., S pt.	7 47 6 50	134 33 134 10
	Truk Is. (<i>Hogota</i>), $\frac{1}{2}$ 15 l., P., S islet	6 57	151 58		Pulo Marière, Warren Hastings I., NS 2m., via. 4 l., $\frac{1}{2}$	4 19	132 28
	— Tis I., [$\frac{1}{2}$ m.], rfa., $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ N, $\frac{1}{2}$ NW, N pt. ...	7 18 5	151 48 5		Pulo Anna, or Current I., [$\frac{1}{2}$ m.], l. $\frac{1}{2}$ (rf. W., 1m.), via. 10m.	4 38	132 2
	Mourileu grp., $\frac{1}{2}$ 7 l., E isle Namolipifan grp., $\frac{1}{2}$ 5 l., lag. [8, Namune islet ...	8 42 8 25	152 26 151 49		Sonsorol Is., or St. Andrew, 2, small, l. $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ via. 12m.	5 20	132 16
	Lutke I., or East Fau, [$\frac{1}{2}$ m.], rfa., $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$	8 33	151 26		Nevil I., or Lord North, $\frac{1}{2}$ $\frac{1}{2}$ 1 $\frac{1}{2}$ m., l. $\frac{1}{2}$ (rf. E)	3 2	131 5
	Namonuito grp., EW 15 l., E islet, Pisaras	8 34	150 32		Helen, or Carteret sh., $\frac{1}{2}$ $\frac{1}{2}$ 5 l., rks. 4f., N pt. islet, 2 $\frac{1}{2}$	3 0	131 52
	— N extr., or Magur islet.	8 59 7	150 14 5		St. David's, or Freewill Is., 4, $\frac{1}{2}$ 5 l., l. $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ mid., via. 18m.	0 57	131 21
	— W extr., or Ulu islet	8 36	149 47				
	Martyr's Is., NS 7m., $\frac{1}{2}$ $\frac{1}{2}$ P., N isld., Ollap	7 37	149 31				
	— S Id. Tamatam, (W Id.) Fanadik)	7 32	149 30				
	Enderby Is. 2, $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ (a bk. $\frac{1}{2}$ $\frac{1}{2}$ 2 l.), (NW one, Alet; SE one, Pozost)	7 20	149 17				

TABLE 10

MARITIME POSITIONS						
(139)	Places	Lat. N	Lon.	(140)	Places	Lat. N Lon. W
Fraser Joseph Land	ARCTIC ARCHIPELAGO.			Greenland, East Coast	W. pt., or Staalburgbuk	65 30' 24° 30'
	FRANK JOSEPH LAND, Wilson I., C. Hansa	80° 23'	East 59° 32'		Sneefeldsyökel, 4696f.	64 48 23 43
	C. Flora. Jackson wintered (1895-6)	79 55	49 40		Reikiavik, Holmenshaven.....	64 8-6 21 53
	C. Mary Harmsworth	80 28	42 0		C. Reikianaes, lt. F 1800f.....	63 49 22 40
	Frederick Jackson I. Nansen wintered (1895-6)	81 13	55 45		Mt. Heckla, 5364f.	63 58 19 38
	C. Germania, 1200f	81 58	57 45		Oster Yökel, 5964f.....	63 36 19 33
	Hridtland	81 38	63 0		Westmanoerne Is., S pt.....	63 24 20 15
	Nansen's farthest (1895)	86 5	96 30		Greenland.	
	Fram's farthest (1895)	85 57	66 0		C. Bismarck	76 47 18 30
	Capt. Cagni's farthest (1900) ..	86 34	64 30		Shannon I., ½ 8 l., S pt., } or C. Philip Brooke.....	74 55 17 33
	C. Grant	80 0	47 40		P. ndulum Is., 2, ½ 5 l., 3000f }	74 38 18 30
	Gillis Land (1707)	81 30	56 0		C. Borlase Warren	74 14 19 23
	King Charles Is., East extr. ○	79 0	32 40		C. Hold with Hope of Hud- son, 3000f.	73 26 20 29
	— Swedish Foreland, N extr. ○	78 50	26 40		Bontekoe, EW 3 l., SE pt. ...	73 29 20 40
	Spitsbergen.				C. Parry	72 22 22 2
	Snoerenberg, ½, 13 sd.....	79 43	11 15		Trall I., C. Young	72 16 21 52
	Hackluyt's Headland	79 47	11 5		Canning I., C. Wardlaw ...	71 47 22 0
	Cloven Cliff	79 45	11 45		Liv rpool I., NS 23 l., S pt. ...	70 26 21 55
	Moffen I., [2m], 1, N pt.	80 1	14 42		— Church Mt., 2967f.	71 4 21 37
Vertegen Hook, 7	80 4	16 25	Rathbone I., E pt.	70 40 21 15		
Treurenberg B., Heckla Cove, ½ }	79 55 3	16 57	C. Brewster, 1	70 11 22 0		
Hinlopen St. Hyperite I. ...	79 42	19 0	C. Tupinier	68 42 25 5		
North Cape	80 32	20 14	King Christian IX. Land, } Leifs I., 2300f.	65 55 35 30		
Walden I., ½ 1½ m., b., NW pt.	80 36	20 0	Holdsæden I.	65 3 39 5		
Little Table I., [½ m.], 750f....	80 48	20 22	C. Moltke	63 36 40 22		
Charles XII. I.	80 43	25 12	C. Adelaer	61 49 42 0		
Parry's farthest (July 1827)...	82 40	19 0	C. Farewell, vis. 30 l.	59 49 43 54		
Spitzbergen	C. Leigh Smith	80 11	28 7	C. Desolation	60 44 48 6	
	C. Molen	79 15	25 0	Fredericksaah Church.....	61 59 49 44	
	Ryk Yse Is., E. pt.	77 50	26 0	Lichtenfels	63 3 50 47	
	Thousand Is., High rk.	77 2	21 20	Godthaab	64 10 51 46	
	Stor Fiord, Fox Ness.....	78 3	19 2	Holsteinburg	66 56 53 42	
	Hope I., ½ 9m., W pt.	76 37	25 30	Whalefish Is., Kronprind- sens I., ½, ½ st.	68 58-9 53 14-0	
	S. Cape, or Look-out	76 27	16 50	Disco I., ½ Issunguak Pt.....	69 39 51 55	
	Hornsunds Pl., 4560f	76 51	16 18	— North pt., Igloipait	70 19 54 36	
	Bel Sd., Separation Pt.	77 38	14 50	— Godhavn	60 13-9 53 42	
	Ice Sound, pt. S side, entr. ○	78 7	14 7	Waygat, or Hare I., [5m.] ...	70 27 54 45	
	Charles I., S., or Saddle Pt. ○	78 13	12 30	Black Head	71 38 55 50	
	Fair Foreland	78 58	10 35	Sanderson's Hope	72 42 56 15	
	Cape Mitra	79 5	11 29	Upernivik	72 46-9 56 2-7	
	Bear, or Chérie I., 1200f. } South H.	74 22	29 18	C. Shackleton, 1400f.....	73 44 56 40	
	JAN MAYEN I., C. Northeast, or Young's Foreland.	71 8	7 50	Devil's Thumb, 1300f.	74 20 56 47	
	— Mt. Beerenberg, 5836f. ...	71 4	8 10	Red Head	74 58 57 15	
	— C. South	70 49	9 8	Sabine's Is., SW one	75 25 58 50	
	Iceland.			C. York, Immagen	75 55 66 33	
	Portland I.	63 23	19 6	C. Dudley Digges, 1, 800f. ...	76 8 68 43	
Hvalsöak rk.	64 40	13 12	North Star B. (Saunders) wintered 1849)	76 32 68 45		
E. extreme, or Ft. Geirhuk ..	65 5	13 26	Cary's Is., Southern	76 40 72 41		
C. Langanæs	66 23	14 30	C. Parry	77 26 71 8		
C. Revsnig	66 33	16 9	Hackluyt I. (Agpaguak), W pt.	77 19 72 30		
Grimsey I., ½ 4m., N pt.....	66 34	18 1	C. Alexander	78 11 73 21		
Mevenkiint	67 9	18 34	Port Foulke	78 18 73 0		
North C.	66 28	22 26	Rensselaer B. (Kane wintered 1853-4-5)	78 37 70 53		
Iceland				Davis Strait	M'Gary I.	79 16 65 0
					C. Calhoun	80 6 67 23
					C. Constitution	80 33 66 30
					Jou Island	81 22 63 31

MARITIME POSITIONS						
(141)	Places	Lat. N	Lon. W	(142)	Places	Lat. N Lon. W
Arctic Sea	Thank-God Hr., Hall's Rest.....	81° 37'	61° 37'	Prince of Wales Strait	Banks Land.	
	C. Bryant	82 23	54 46		C. McClure	74° 33' 120° 50'
	Mt. Hooker	82 30	50 41		— Bay of Mercy (Investi- gator abandoned 1858).....	74 14 118 15
	C. Britannia, 2050f.	82 44	49 00		Prince Alfred, C.....	74 7 124 0
	C. Beaumont	82 48	50 30		— C. Kellett	71 55 125 28
	Markham I., C. Neumayer ...	83 1	48 0		— Nelson Head.....	71 2 122 24
	Lockwood I., Lockwood's } farthest (1882)	83 25	40 45		— Princess Royal Is. } (McClure wintered 1850-1) }	72 45 117 44
	C. Robert Lincoln	83 32	39 35			
	Grant and Grinnell Land.				Prince Albert Land.	
	C. Alfred Ernest	82 14	85 55	Dease Strait	Prince of Wales Str., Peel Pt.	73 20 113 54
Smith's Sound	C. Columbia	83 7	70 23		Ramsay I. (Colinson win- tered 1851-2)	71 36 119 5
	C. Joseph Henry	82 49	63 36		C. Wollaston	71 3 118 9
	Markham's farthest (1876) }	83 20 5	63 7		C. Baring	70 0 117 0
	C. Sheridan (Sir G. Nares } wintered 1875-6)	82 26	61 21		C. Bick (Rae's farthest 1951)	70 9 116 0
	C. Union	82 15	61 8		Wollaston and Victoria Land.	
	Discovery Harbour	81 43	64 46		C. Lady Franklin	68 33 113 10
	C. Beird	81 32	64 32		Cambridge B. (Collinson } wintered 1852-3)	69 5 105 10
	C. McClintock	79 58	70 50		Point Back	68 55 103 16
	C. Louis Napoleon.....	79 38	72 19		Lind I., South pt.	68 37 102 5
	C. Sabine	78 43	74 15		Gateshead I.	70 25 100 38
Lancaster Sound	C. Isabella	78 16	75 33	Victoria Strait	King William Land.	
	Clarence Head	76 41	77 48		Victoria Strait (Erebus and } Terror abandoned 1848) }	69 49 98 49
	Cobourg Is., East L., Prin- } cess Charlotte Monument }	75 39	77 45		C. Felix	69 55 97 55
	North Devon.				Pt. Franklin	69 28 99 10
	C. Horsburgh.....	74 55	79 3		C. Crozier	69 4 100 4
	C. Osborn	74 24	81 42		C. Herschel.....	68 42 98 2
	C. Warrender.....	74 28	81 51		Mount Matheson.....	68 45 95 7
	C. Bullen	74 22	85 0		Prince of Wales Land.	
	C. Hurd, 1	74 32	90 3		Cape Swinburne	71 12 99 00
	C. Riley	74 40	91 48	McClintock Channel	Pt. Allen Young.....	72 10 101 55
Barrow Strait	Beechey I. (Franklin win- tered 1845-6)	74 43	91 45		Minto Head.....	73 4 102 40
	Baring B. (Belcher wintered } 1853-4)	75 40	91 52		Parker I.	74 14 100 35
	N. Cornwall, Mt. Greenwich	77 36	94 41		Palmerston Pt., 600f.....	74 7 97 44
	Parry Islands.				Cape McClure	72 50 96 36
	Cornwallis I., C. Hotham.....	74 38	93 34		North Somerset.	
	— Assistance B.	74 37	94 16		C. Rennel	74 7 93 14
	Griffith I., $\frac{1}{2}$ 8 l., 8 pt.	74 28	95 20		Leopold Is., N one, 1, E pt.	74 3 89 53
	Lowther I., $\frac{1}{2}$ 9 l., 8 pt.	74 26	97 40		Port Leopold (James Ross } wintered 1848-9)	73 50 90 12
	Bathurst I., C. Cockburn, A ..	75 3	100 23		Batty Bay	73 13 91 8
	— Lyall Pt.	76 39	104 58	Prince Regent Inlet	Fury Pt. (H.M.S. Fury } abandoned Aug. 1825; Sir J. Ross wintered 1832-3) }	72 40 5 91 53
Barrow Strait	— Sherard Osborn I., N pt.	76 47	100 0		C. Garry.....	72 23 93 17
	Byam Martin I., C. Gillman....	75 0	104 8		Bellot Strait, Pt. Kennedy } (McClintock windt. 1858-9) }	72 2 94 14
	Melville I., $\frac{1}{2}$ 44 l., Win- ter Harb. (Sir E. Parry } wintered 1819-20)	74 47 2	110 48 2		Cookburn Island.	
	— W extreme, C. Russell	75 14	117 40		C. Kuter	71 54 89 59
	— N extreme, Markham I.	77 00	109 43		Sherer's Mt.	73 2 89 20
	Eglinton I., C. Nares	75 34	119 30			
	Prince Patrick I., Land's End	76 16	124 6			
	Polynia Is., Ireland's Eye.....	77 49	115 30			

TABLE 10

MARITIME POSITIONS

(143) Places		Lat. N	Lon. W	(144) Places		Lat. N	Lon. W
Lancaster Sound	Port Bowen (Parry wintered 1824-5), Stony I. } ⊕	73° 13' 6"	88° 54' 7"	Arctic Sea	Return reef C	70° 25'	148° 30'
	C. York ⊕	73 50	86 40		Flaxman I., 50f., N side	70 11	145 50
	C. Crawford ⊕	73 53	83 50		Camden B. (Collinson wintered 1853-4)..... }	70 8	145 29
	C. Charles York	73 50	82 0		Pt. Manning	70 7	143 40
	C. Hay	73 52	79 50		Herschel I., S pt.	69 34	138 54
	Possession Mt., 2200f.	73 22	77 35		Mt. Cupola	68 45	137 53
	C. Walter Bathurst	73 28	76 36		Mackenzie R., Shoalwater B.	68 49	136 27
	C. Graham Moore	72 56	76 10		Pelly Is., [1 l.]	69 32	135 33
	C. Bowen	72 21	74 45		Pul en I.	69 45	134 20
	C. Adair	71 32	71 29		Warren Pt.	69 47	131 35
	Agnes' Monument, 1, 40f. ⊕	70 33	68 15		C. Dalhousie	70 16	129 10
	Cape Raper	69 44	67 30		C. Bathurst	70 36	127 30
Davis' Strait	C. Kater	69 12	66 53		C. Parry, NE pt.	70 6	123 35
	Cumberland Island.				Keats Pt.	60 49	122 0
	C. Searle	67 13	62 22		Sir S. Clerk's I., SE pt.	69 33	118 0
	Cape Dier of Davis	66 48	61 15		C. Bexley	69 0	115 52
	Mt. Raleigh, A.	66 34	62 18	Coronation Gulf	C. Krusenstern	68 28	113 54
	C. Walsingham	66 4	61 15		Copernicus R., mouth, E side	67 48 5	115 31
	C. Mercy of Davis	64 51	63 43		C. Flinders	68 14	109 14
	Cumberland Id., Njudluk Harbour }	65 7	64 25		Back's Western River	66 28	107 49
	— Kingaita Fiord, Union Hr.	66 23	66 25		Turnagain Pt.	68 39	108 35
	Kingawa Fiord	67 16	68 0		C. Alexander	68 55	106 19
	— Harrison Pt.	64 57	66 5		Melbourne I., EW 6 l., E pt.	68 29	104 50
	Hall I., Mt. Warwick ⊕	62 33	64 0		White Bear Pt.	68 9	103 30
	Frobisher B., Jordan R.	63 45	68 55		O'Reilly I., [4 l.], NW pt. ...	68 12	99 24
	Resolution I., $\frac{1}{2}$ 13 l., E pt., or C. Warwick }	61 40	64 30		Cape Gedde	68 31	98 5
	— S pt., or Hutton's Headland, or C. Best }	61 21	65 0		Pt. Ogile	68 17	96 15
	Lower Savage I.	61 35	66 7	James Ross Strait	Cockburn B., mouth of Great Fish or Back River }	67 13	95 24
Hudson Strait	Saddleback I.	62 11	67 43		Castor and Pollux R. (Dease and Simpson 1839, Rae 1854)..... }	68 32	94 0
	Upper Savage I., $\frac{1}{2}$ 3 l., E pt. ⊕	62 33	70 0		Stanley Island.....	68 44	94 50
	North Bluff	62 32	70 25		Hull Bay	69 20	93 42
	Fox Land.				Boothia Isthmus, Josephine B.	69 39	94 40
	King Charles Cape..... ⊕	64 22	77 50		MAGNETIC POLE (1851)	70 5	96 47
	Queen's C.	64 45	78 12		C. Nikolas	70 25	97 0
	C. Weston	65 35	78 12		C. Hobson	71 26	95 55
	C. Dorchester.....	66 21	78 0		Murchison Promontory, Northern pt. of America. }	72 0	94 37
	Pt. Peregrine (Fox's farthest, 1631) }	66 40	76 50		Elizabeth Harbour	70 38	91 46
	Southampton Island.				Victoria Harb. (Ross abandoned the Victoria 1831-2) }	70 9 3	91 25
	Southampton Is., $\frac{1}{2}$ 83 l., N pt., or C. Frigid. }	65 59	85 30	Boothia Gulf	Felix Harb., M'Diarmid I., (Ross wintered 1829-30) }	69 59 7	91 50
	— E extr., or Seahorse Pt.	63 35	80 7		Pelly Bay, Parker Peak.....	68 25	89 36
Fox Channel	— C. Kendall.....	63 42	87 15		C. Chapman	69 15	89 0
	Tom I., [4 l.], S pt.	63 10	87 0		Rae Isthmus, C. Simpson.....	67 20	87 2
	Coats I., C. Pembroke ⊕	63 0	81 20		Cape Richardson	68 50	85 15
	— S extr., or C. Southampton }	62 10	83 45		C. Englefield, Fury and Hecla Strait }	69 51	85 30
	NORTH AMERICA.				C. Haslowell, (N head of do.)	69 57 5	85 26
	Pt. Barrow, (Noowook)	71 23	156 22		Igloodik I., EW 9m., (Parry wintered 1822-3), E pt. }	69 21	81 31
	Port Moore (Maguire wintered 1852-4), MAGNETIC OBSERVATORY. } ⊕	71 21 4	156 16		Arlagnuk.....	69 12	81 30
	Tangent Point	71 10	154 46		Ooglit Is.....	68 58	81 4
	C. Halket	70 49	152 15		Ooglit I., [2m.], l.	68 24	81 38
	Pt. Beechey	70 24	149 37		C. Jermain	67 47	82 0
					C. Penrhyn	67 25	81 25
Southampton I.					Winter I., $\frac{1}{2}$ 10m., l. S pt., or C. Fisher (Parry wintered 1821-2) }	66 11 4	83 10 0

MARITIME POSITIONS							
(145) Places		Lat. N	Lon. W	(146) Places		Lat. N	Lon. W
Rose's Welcome	Baffin I., $\frac{3}{4}$ 7m., SE pt.	65° 40'	83° 29'	Aillik Harb., C. Mokkovik ...	55° 13' 5"	59° 18' 2"	
	Repulse B., head Fort Hope...	66 33	86 56	Webeck Harb., Harbour rocks	54 54' 5"	58 17'	
	Wager R., S cape of entr.	65 13	87 28	White Bear Is., Middle I., 190f.	54 28	56 55	
	HUDSON'S BAY.			Hamilton Inlet, Rigoulette ...	54 10 8	58 25' 2"	
	Chesterfield Inlet, Wagg I. ...	63 21	91 14	— Goose B., Rabbit I.	53 23	60 9	
	— Head of inlet	64 0	95 50	Cape Porcupine, 343f.	53 56	57 8	
	Marble I., E part	62 41	90 30	Outer Gannet I., 104f.	54 0' 3"	56 31' 5"	
	Whale Cove	62 10	92 50	Cartwright's Hb., Caribou Castle	53 42' 6"	56 59' 7"	
	C. Esquimaux	61 8	94 0	Greedy Harb.	53 48	56 25' 7"	
	Churchill Battery Beacon ...	58 46	91 10	Indian Tickle, Indian Id., 360f.	53 34' 2"	55 59' 5"	
James Bay	C. Churchill	58 52	93 14	Roundhill I., 174f.	53 26	55 36	
	York, factory, r., f.	57 2	92 26	Occasional Harb. Obs.	52 40	55 44' 2"	
	C. Tatnam	57 22	91 10	C. St. Francis, 115f.	52 33' 5"	55 41' 5"	
	Seymour Fort	55 58	89 12	C. St. Lewis, St. Lewis rk.	52 21' 7"	55 37' 2"	
	C. Lookout	55 23	85 13	Battle Is., Double L., 130f.	52 15	55 33	
	C. Henrietta Maria	55 9	82 45	Table Head	52 6	55 41	
	Albany Fort	52 12	81 50	Belle Isle, $\frac{1}{2}$ 9m., lt. F 470f.	51 53	55 22' 2"	
	Moose Fort	51 13	80 40	Chateau B., Castle I., S pt. ...	51 58	55 50	
	Rupert's House	51 23	78 29	Amour Pt., lt. F 153f.	51 27' 5"	56 51	
	East Main Fort	52 10	78 32	Greenly I., lt. Rev. 100f.	51 22' 7"	57 10' 5"	
Hudson's Strait	North Bear I.	54 27	81 6	Bradore hills, sum. 1264f.	51 34	57 12	
	Agoomaka I., $\frac{1}{4}$ 17 l., S pt. ...	52 49	81 0	Old Fort I., [1 $\frac{1}{2}$ m.]	51 22	57 47	
	South Cub	53 57	79 42	Shag rks.	51 10	58 18	
	Long I., $\frac{1}{2}$ 6 l., S pt.	55 0	78 48	Eagle Harb., E side, entr.	51 0	58 41	
	Richmond B., entr.	56 14	77 15	Grt. Mecatina I., $\frac{1}{4}$ 3 $\frac{1}{2}$ m., }	50 44	58 53	
	South Belchers, centre	55 55	80 48	— SE pt.			
	King George's Is., centre ...	57 30	80 10	Murr Is. and rks., [1 l.], }	50 42	58 50	
	Sleepers, N part	58 18	80 40	E extr.			
	Brothers, East Bro.	58 37	80 0	Little Mecatina I., $\frac{1}{2}$ 6m., }	50 31	59 21	
	Ottawa Is., NE I.	59 55	79 38	S pt.			
Labrador	C. Dufferin	58 46	79 11	St. Mary rks., [2m.], S pt. ...	50 13	59 45	
	Smith I.	60 50	79 7	South Maker's ledge	50 9	59 57	
	Mansfield I., $\frac{1}{2}$ 19 l., }	61 33	80 20	C. Whittle, (rks. $\frac{1}{2}$ 3m.)	50 11	60 8	
	South pt.	62 37	79 52	NEWFOUNDLAND.			
	— North pt.	62 37	79 52	Quirpon I., N pt., or C. }	51 38' 8"	55 25	
	C. Woostenholme	62 37	77 26	Bauld, I., lt. Alt. 141f. ...	50 42' 2"	55 35' 5"	
	Diggs Is., W extreme	62 34	78 5	Bell I., (S end)	50 0	55 21	
	Nottingham I., $\frac{1}{4}$ 14 l., }	63 6	77 50	C. St. John, Gull I., lt. Occ. }	50 0	55 21	
	S pt., (8 sh. 7m.)	63 22	76 30	525f.			
	Salisbury I., $\frac{1}{4}$ 9 l., SE pt.	64 4	77 50	Toulinguet Is., lt. Rev. 335f. ...	49 41' 3"	54 47' 5"	
Labrador	Mills I., N pt.	62 47	74 0	Seldom-come-by Harbour, }	49 35	54 10' 7"	
	Charles I., C. Moses Oates ...	62 47	74 0	Cann I., lt. F 85f.	49 35' 7"	53 45' 0"	
	C. Weggs, Island	62 31	74 0	Offer Wadham, lt. F 100f.	49 45' 5"	53 10' 7"	
	Stupart Bay	61 33	71 33	Funk I., 46f.	49 10' 5"	53 21' 5"	
	C. Hope's Advance	61 17	70 2	C. Freels, Stinking I., lt. Occ.	49 4' 3"	53 32' 5"	
	Green I.	60 8	67 52	Greenspond I., 85f.	48 42' 0"	53 4' 5"	
	Akpatok I., E end	60 10	66 36	C. Bonavista, lt. Rev. 150f. ...	48 30' 2"	53 2' 2"	
	Koksoak R., The Wort, 165f. ...	58 29	68 7	Catalina Harb., Green I., }	48 16' 9"	53 23' 6"	
	Fort Chimo	58 8	68 18	lt. F 92f.	48 30' 2"	53 2' 2"	
	LABRADOR.			Bonaventure Head	48 16' 9"	53 23' 6"	
C. Chidleigh, 1500f.	60 33	64 15	New Perlican, Bloody Pt.	47 55' 1"	53 21' 5"		
Button Is., NS 3 l., via. 7 l., }	60 51	64 39	Baccalieu I., lt. Fl. 380f.	48 9	52 47' 5"		
NE pt.	59 50	64 2	Harbour Grace, (lt. F 40f. on beach)	47 41' 4"	53 12' 5"		
Eclipse Harb., Mt. Bache, 2150f.	59 3	63 52	C. St. Francis, lt. F 123f.	47 48' 5"	52 47' 0"		
Nashvak B., H. B. Co. Post ...	58 16	62 40	ST. JOHN'S (CHAINROCK BATTERY)	47 34' 0"	52 40' 7"		
Hebron Mission Station	56 53	61 19	C. Race, lt. Rev. 180f.	46 39' 4"	53 4' 3"		
Mt. Thoresby, 2773f., Port }	56 32' 9"	61 40' 7"	C. Pine, lt. F 314f.	46 37' 1"	53 31' 7"		
Manvers, w, b.	55 27' 1"	60 12' 5"	Trepassy Harb., (Shingle neck)	46 43' 3"	53 22' 2"		
Nain			C. St. Mary, lt. Rev. 300f. ...	46 49' 5"	54 11' 5"		
Hopedale Harb. Obs.			Placentia Harb., lt. F 180f.	47 14	54 1		
			Burin Harb., lt. Rev. 430f.	47 0' 4"	55 8' 7"		
			Laun, Gt. Laun R. C. Church	46 56' 5"	55 32' 0"		

617

[illegible]

MARITIME POSITIONS

(149)	Places	Lat. N	Lon. W	(150)	Places	Lat. N	Lon. W
Nova Scotia	Margaret's B., [2], Shut-in I.	44° 34'	63° 54'	Maine	Owl's Head, lt. F 103f.	44° 6'	69° 3'
	Tancook I.	44 29	64 6		Mt. Desert rk. lt. F 75f.	43 58	68 8
	Malaguash Harb., [2]. Cross I., [1 1/2 m.], h., 2 lts. Vert. dist. 34f.	44 20	64 7		Cash's Ledge, 7 T, 1 [1 m.]	42 56	68 51
	C. L. Have, 1, 107f., (Black rk. 1m.)	44 12	64 18		1 Haute, 2 5m., Saddleback ledge, 10 E-d., lt. F 51f.	44 1	68 44
	Coffin I., lt. R 65f.	44 2	64 38		Matinicus I and rks., [4 m.], lt. on rk., F 90f.	43 47	68 51
	Little Hope I., [2c.], 21f.	43 49	64 45		White Head, 1, lt. F 79f.	43 59	69 7
	Gull rk., lt. F 56f.	43 39	65 6		Monhegan I., [1m.], T, lt. R 175f.	43 46	69 19
	Shelburne Harbour, [2]. McNut's I., SE pt., 1, r, w, 2 lts. F vert. 120f. and 65f.	43 37.5	65 16		Pemaquid Pt., lt. F 75f.	43 50	69 30
	Brazil rk., [3 vds.], 2f.	43 28	65 25		Burnt Island, lt. F 61f.	43 49	69 38
	C. Sable, (SE pt. of small l., 1, 2. W end advancing 1m. in 4 years), 1, 8 3m., lt. R 53f.	43 23	65 37		Seguin I., lt. F 180f.	43 41.6	69 46
	Blonde rk., small, 8	43 20	65 57		Cash's ledge, 2, [1 m.]	42 50	69 4
	Seal I., [2m.], S pt., 8 1 1/2 m., 2, lt. F 98f.	43 24	66 1		Portland, [2], City Hall	43 39.2	70 15.2
	Tusket Is. Pubnico Harb., [2] r, w, b, entr.	43 37	65 52		— lt. W entr., F 101f.	43 37	70 12
	C. Fourchu, A., 2, lt. R 117f.	43 47	66 9		C. Elizabeth, 2 lts., [300 yds.], F, Fl. and F 143f.	43 33.6	70 11.5
Lurcher rk., 8, small, 2f.	43 52	66 25	New Hampshire	Wood I., entr. Saco Harb., lt. F, Fl. 63f.	43 27	70 19	
C. St. Mary	44 7	66 11		Agamenticus Hills	43 13	70 41	
Bryer's I., 2 4m., lt. F 92f.	44 16	66 22		C. Porpoise, Goat I., SW part, lt. F 38f.	43 21	70 26	
Annapolis Harb., [2], Pt. Prim, lt. F 76f.	44 42	65 47		Bald Head	43 13	70 34.5	
Black rk., pt., lt. F 45f.	45 10	64 46		Boon I., [2m.], 1, lt. F 135f.	43 7	70 29	
Haute I., w, 2, lt. Int. 363f.	45 15.1	65 1		York Harb., [2]	43 9	70 39	
C. Chignecto, A., T	45 19	64 57		Whale's Back, lt. F, Fl. 65f.	43 4	70 42	
C. Enragé, lt. F 120f.	45 36	64 47		Portsmouth, Fort Constitution, lt. F 70f.	43 3.5	70 43	
Quaco, lt. R 110f.	45 19.5	65 32		Is. of Shoals, [3 m.], S or White I., lt. R 87f.	42 58	70 37	
Quaco ledge, [1 l.]	45 14	65 20		Newbury Port, [2], bar sf., 2 leading lts. F on N pt. of Plumb I., movable	42 48.5	70 49.0	
C. Spencer	45 12	65 55		Ipswich Bay, lt. F, Fl. 50f.	42 41	70 46	
St. John's, [2], Partridge I., lt. F 119f.	45 14.1	66 3.5		Annisquam Harb., [2], lt. F 50f.	42 39.8	70 41	
C. L. preau, lt. F 80f.	45 3.7	66 28		C. Ann, lts. NS, on Thatcher I., 2 lts. F 165f. (Salvage N-d., 2m.)	42 38.4	70 34.7	
Wolf Is., 2 3/4 m., 1 T, 100f.	44 59.5	66 41		C. Ann Harb., [2], lt. on Ten-Pound I., F 49f.	42 36	70 40	
Northst.	45 4	66 49		Salem, [2], City Hall	42 31.5	70 54.0	
Etang, harb., [2], tower S pt.	45 4	66 49		Baker's I., [2m.], 2 lts. F 87, 50f.	42 32.2	70 47.5	
St. Andrew's, [2], N pt., lt. F 42f.	45 4.3	67 3		Marblehead, lt. F 43f.	42 30.2	70 50	
Campobello I., N pt., lt. F 64f.	44 58	66 54		St. George's shls., EW 7 l., SW, or shl. part, 1.	41 43	67 47	
UNITED STATES.							
Maine	Quoddy Hd., lt. F 133f.	44 49	66 57	Massachusetts	Little George's, [2]	41 15	68 0
	Old Proprietor shl., [2c.], [2]	44 30	66 37		Boston, [2], Cambridge Obs.	42 22.8	71 7.7
	Grand Manan, 2 1/4 m., w, r, [2] W, 8, NE pt.	44 46	66 43		— N side, main outer entr., lt. R 111f.	42 19.7	70 53.7
	Gannet rk., lt. Fl. int. 66f.	44 31	66 47		Plymouth, [2], Gurnet lts., 2 F 93f.	42 0.2	70 36.2
	Libby I., off Machias B.	44 32.5	67 22		Barnstable, [2] 1/2, bar., lt. F 33f.	41 43.2	70 16.5
	Machias Seal Is., 2 lts. F 66f. and 54f.	44 30	67 6		Billingsgate I., lt. F 52f.	41 51.6	70 4.5
	Nash's I., entr. Pleasant R., lt. F 47f.	44 28	67 45		Race Pt., lt. F, Fl. 51f.	42 3.7	70 15
	Petit Manan, S pt., lt. F, Fl. 125f. (8 2 to 5m.)	44 28	67 52		C. Cod, high, or Truro, lt. F 195f.	42 2.4	70 4
	Baker's I., lt. Fl. 105f.	44 13.5	68 12		Nausset, 3 lts. F 93f.	41 51.6	69 57.2
	Castine, lt. F 130f.	44 23	68 49		Chatham Harb., 2 lts. F 80f., S one	41 40.3	69 57.2
					Monomy Pt., lt. F 41f.	41 33.6	70 0.0

MARITIME POSITIONS							
(153) Places		Lat. N	Lon. W	(154) Places		Lat. N	Lon. W
Florida	Carysfort rf., lt. R 106f.....	25° 13'	80° 32'7	Samana, or Attwood's Cay. }	23° 55'	73° 49'	
	Tavanier Cay, § 1 l.	25 0	80 30	*, T, W pt..... }			
	Lower Matacumba l., § 3m. }	24 49	80 44'5	Plana Cays, EW 10m., l, §, }	22 35	73 38	
	W pt. (w st N) }			T, hill, W pt., §, l, w st ... }			
	Sombrero Cay, lt. F 144f.....	24 37'5	81 6'7	Mariguana l., rf. EW 10 l. }	22 23	72 55	
	Sand Cay, lt. F, Fl. 110f.....	24 27	81 52'7	l, §, T, §, Centre hill, 110f. }			
	Cay West, NW pass., lt. F 50f....	24 37	81 54	Hogsty rf., EW 5m., T, §, }	21 40'5	73 50'7	
	— CAY WEST, U.S. NAVAL }	24 33'4	81 48'5	NW Cay }			
	STOREHOUSE }			Gr. Inagua, § 15l., l, §, lt. R 120f }	20 56	73 41	
	Tortugas, EW 9m., shls. W }	24 38	82 53	— Man of War B, W side, well }	21 4	73 39	
Bahama Is.	4l., *, Wpt., Fort Jefferson, lt. F 65f., (§ 6m.) }			Little Inagua, EW 3 l., N pt....	21 33	73 0	
				Cuicoo bk., § 22 l., S rk.....	21 3	71 45	
				— West Caicos, § 7m., S pt....	21 37	72 30	
				— East Harbour, wat. pl.	21 31	71 32	
				Turk's Is., § 6 l., N extr., }	21 31	71 8	
				lt. Fl. 108f. }			
				— Hawk's Nest, w st §, §, §, §, }	21 26'3	71 10'5	
				Endymion rk., l, f. }	21 7	71 18	
				Square Handkerchief, EW }	21 6'5	70 29	
				30m., NE breaker }			
Bahama Is. and Banks	— "South-east" Pt. (so call- ed), [§] W, w }	26 28	78 40	Silver bk., § 15 l., Cay. }	20 18	69 58	
	Gr. Abaco l., § 23 l., lt. }	25 51'5	77 11'2	SW rk..... }			
	near S pt., R 160f. }	26 20	76 59	— North rks.	20 53	69 55	
	— East Pt.	26 31	76 58	— Eastern edge, R, T	20 35	69 22	
	Elbow Cays, §, lt. F 123f.....	26 2	79 5	Bajo Navidad, § 7 l., N pt. W, T }	20 13	68 52	
	Great Bahama Bk., § 110 l. }						
	Gr. Isaac rk., [3m.], 40f. }	25 41	79 20				
	Bemini Is., [7m.], l, §, SW }	25 34'5	79 19				
	pt. w }	24 56	79 9'0				
	Gun Cay, lt. R 80f.	22 45	78 8				
Bahama Is. and Banks	Orange Cays, Id., [3m.], 13f. }	22 22'8	77 35'5	Cuba, § 217 l., E pt., C. }	20 15'2	74 9	
	*, §, f }	22 10	77 20	Mayai, lt. F 128f., 4 rf. 1m. }	20 21	74 28'5	
	Cay Guinchos.....	21 42	75 45	Barracoa, fort.....	20 41	74 53	
	Lobos Cay, T, lt. F 146f.....	22 1	75 11'5	C. Moa, Cay, §'.....	21 5	75 36'5	
	Diamond Pt., § T	22 11'5	75 44'2	Pt. Lucracia, lt. R 112f.....	21 6	75 50	
	St. Domingo Cay, 15f., l § }	23 0	75 44	Port Naranjo, §, W pt., l, 1	21 17	76 25	
	Cay Verde, 72f.....	23 41	75 19	Port Maternillos, lt. R 176f. ...	21 40	77 8'7	
	Gr. Ragged l., beac. hill 115f.	22 51	74 51	l. Guajaba, § 10m., W pt. ...	21 55	77 36'	
	Water Cay, [1½m.]	23 56'5	80 28	Cay Confitas	22 12	77 39	
	Long l., § 19 l., l, §, T, N pt. }	23 35	75 48	Cayo Romano, 2 Is., § 16 l., }	22 27	78 19	
Bahama Is. and Banks	— South pt.	25 9	76 9	NW pt. }	22 19	77 48	
	Cay Sal bank, N. Elbow, lt. F 96f.	25 35	76 9	Minerva Cay, [1m.]	23 41'7	80 25'0	
	Exuma l., § 8 l., entr. harh. }	24 38	76 9	Cay Sal, bk., § 20 l., l, Cay }	23 56'5	80 28	
	Eleuthera l., § 22 l., §, T, S pt. }	25 9	76 9	Sal, [1m.], w, §, N pt. }	24 2	79 51	
	— NE, or Palmetto Pt.	25 35	76 44	— Elbow Cay, lt. F 96f.....	23 29	79 32	
	— Npt., hill, (shls. E and W 3 l.) }	25 30	76 55	— Dog rks., § 5m., E pt.....	23 12	80 21	
	Eug and Royal Is., West l. ...	25 5'6	77 22'2	— Anguilla Is., § 7m., w st . }	23 12	80 30	
	New Providence l., EW 5 l., }	25 7	77 36	S pt.	23 14'2	81 8'7	
	Nassau, § 11, lt. F 68f. }	24 3	77 11	Nicolas rf., Medano l., 8-d. ...	23 3	81 37	
	— E pt., Goulding Cay, w SW }	25 4	77 57	Bahia de Cadiz, lt. R 175f. ...	23 1'9	81 45	
Bahama Is. and Banks	Green Cay, [2m.], w }	24 8	75 17	Bahama Is. and Banks	Piedras Cay, lt. F, Fl.	23 9'4	82 21'5
	Andros l., § 32 l., Mastic Pt. ...	25 4	75 17		Matanzas Bay, §, S Severmo }	22 57	82 22
	Berry Is., NS 9 l., T, w, r, }	25 32'5	77 42		Castle }	23 0	83 11'7
	E lim., or Frozen Cay }	25 49'7	77 54		Pan de Matanzas, 1277f.	22 48	83 24
	Great Stirrup Cays, r, lt. F 81f.	24 36	75 59		HAVANA, §, MORRO lt. R 144f.	22 9	84 48
	Little Salvador, § 5m., W pt. }	24 41	75 46		Managua Paps, 2, EW 2m., }	21 53	84 57'2
	St. Salvador, § 14 l., NW pt. }	24 8	75 17		732f., W one }		
	— East pt. (Columbus's landfall)	23 50	75 8		Port Mariel, §, entr.	23 3	82 44
	Concepcion [and rks. 2 l.], §, }	24 6	74 26		Bahia Honda, § Cerro Morillo }	23 0	83 11'7
	l, §, T, Id. W pt. }				Pan de Guajabon, 2532f.....	22 48	83 24
Bahama Is. and Banks	Watling's l., § 5 l., Dixon }	23 37	74 50	Bahama Is. and Banks	Colorados rfs., rks., §, T, W pt. }	22 9	84 48
	Hill, lt. Fl. 165f. }	22 6	74 28		W extr., C. St. Antonio, l, }		
	Rum Cay, EW 3 l., w st , S pt. }	22 6	74 28		§, T, rky., (chl. § 7m., w), }		
	Mira por vos, § 3 l., §, NE rk. }	22 6	74 20'5		lt. R 128f. }		
	Crooked l., § 14 l., §, §, w st . }	22 6	74 20'5		C. Corrientes, l, sand, §	21 45'5	84 31
	S pt., Castle l., lt. F 123f. }	22 6	74 20'5		Pt. Piedras }	22 2	83 50'5
	— Bird Rock, lt. R 120f.....	22 50'5	74 23		Cays of San Felipe, SW part. }	21 55	83 32
					T, 1½m. }		

TABLE 10

621

MARITIME POSITIONS

(155) Places		Lat. N	Lon. W	(156) Places		Lat. N	Lon. W
Cuba S. Coast O	I. of Pines, EW 16 l., S pt.	21° 24' 4"	82° 56'	Town of Savana la Mar, fort	19° 3'	69° 22'	
	Rosario Channel, 1, S ent.	21 37	81 55	C. Samaná, rugged, A, 1 > ...	19 18	69 8	
	Jardines, W, E extr.	21 39	81 2	Port Plata, lt. R 137f.	19 47	70 38	
	Cay de Piedras, lt. F 27f.	21 58	81 3	Old C. Français, >	19 40	69 52	
	Placer de Xagua, [3m.], 1 ...	21 37	80 35	Pt. Isabelle	19 57	71 1	
	Bitavano	22 43	82 18	Monte Christi B., &, F, w.	19 53	71 40	
	Xagua B., [3m.], lt. F, FL 82f. ...	22 1	80 30	C. Haytien Harb., [3m.], w, f, } turret d'Estaing }	19 46.7	72 11.7	
	Trinidad, mole	21 42	79 59	Acul, [3m.], [3m.], 7 l., E pt., l ...	19 45	72 22	
	Cayo Blanco, 20f.	21 36.6	79 53.5	Tortuga I., [3m.], 7 l., E pt., l ...	20 1	72 34	
	Manzanillo	20 20	77 10	St. Nicolas' Mole, [3m.], w, Fort } St. George }	19 49.5	73 22.2	
Caymans	C. de Cruz, rf. 2m., T, lt. F, FL 114f.	19 49.9	77 45.5	Cape Fou	19 44	73 29	
	Tarquino Pk., 8,400f.	19 56	76 45	Gonaives, [3m.], Pt. Verrier	19 25.7	72 42.7	
	SANTIAGO DE CUBA, [3m.], r, w, lt. F, FL 228f., Morro Castle }	19 57.4	75 52.2	St. Marcos Pt., A, 1	19 2	72 50	
	— BLANCA BATTERY	20 00.3	75 50.5	Gonaive I., [3m.], 10 l., F, W pt.	18 55.4	73 18.2	
	Guantanamo, or Cumberland Harb., [3m.], E head }	19 55	75 11	Port-au-Prince, r, w, Fort } Alexander, lt. F 46f. }	18 33.2	72 20	
	Cayman Brack, [3m.], 3 l., F, E pt.	19 45.2	79 44	Rochelois shl., [1 l.], [3m.], 3f.	18 39	73 13	
	Litt. Cayman, [3m.], 7m., l, 3 f.	19 42	79 58	Caymites, &, 8 [3m.], 500f. NE pt.	18 39	73 40	
	E end			C. Dame Marie, W pt., (w } SE 2m.) }	18 36	74 27	
	Grt. Cayman, EW 6 l., l, } F, F, &, &, r, town, } Fort George }	19 17.7	81 23.5	C. Tiberon, A, >, T, w, b } in bay }	18 22	74 28	
	— East pt., F, 8 lm.	19 19	81 7	La Hotte mountain, 7,400f.	18 23	74 3	
Jamaica	— East pt., F, 8 lm.	19 19	81 7	Navasa I., [2m.], 300f., T, &, } &, F, mid. N side }	18 25	75 2	
	JAMAICA.			Formigas shl., [3m.], 2 l., 2, N pt.	18 35	75 45	
	Jamaica, [3m.], 43 l., E pt., or Pt. } Morant, lt. R 115f. }	17 55.1	76 11.7	Pt. Gravois	18 1	73 56	
	Port Antonio, 2 [3m.], w, fort, lt. F 54f.	18 11.3	76 27	I. Vache, [3 l.], T S, NW pt.	18 6	73 43	
	St. Ann's B., [3m.], Long wharf, w Falmouth Harb., [3m.], bar, fort	18 26.4	77 13.7	Aux Cayes	18 12	73 46	
	Montego B., fort	18 29.4	77 56.5	C. Jaquenet, [3m.], Wharf	18 13.5	72 33	
	Lucia Harb., &, fort, E entr.	18 28	73 10.7	Mountain, 8900f.	18 21	72 0	
	Pedro Pt.	18 28	78 14	C. False	17 45	71 40	
	N. Negril, N pt.	18 21.4	78 22	Beata I., NS 4m., l, F, & } NW, NW pt., 80f. }	17 36.7	71 32	
	Dolphin Hd., pk., 1820f.	18 23	78 11	Fraysle rk., 50f.	17 37	71 41	
Pedro Bank and Is. S.W.ward	S. Negril Pt.	18 16.8	78 23.5	Alta Vela, A, T, 500f.	17 28	71 40	
	Savannah la Mar, fort, shl. 2m.	18 12.3	78 8.7	C. Mongon	17 50	71 14	
	Pedro Bluff, 220f.	17 51	77 45.2	Pt. Avarena	18 7	71 0	
	Alligator rf. [3m.], W pt.	17 48.5	77 33.5	Pt. Caldera, or Salinas	18 12	70 36	
	Portland Pt., SE pt.	17 43	77 10	Pt. Nisso	18 13	70 0	
	Old Harbour, [3m.], Careening L. PORT ROYAL, [3m.], F. CHARLES	17 53.5	77 5.5	St. Domingo, City, [3m.], Consulate, lt. R 111f.	18 28.2	69 52	
	Yallah's Pt., (hill 2400f., [3m.])	17 56.0	76 50.7	I. Saona, EW 4 l., F, Cana Pt.	18 4	68 32	
	Port Morant, [3m.], Leith Hall...	17 52	76 33.5				
		17 53	76 21				
St. Domingo	Morant Cay, [3m.], 1 l., &, 8, } 2 1/2m., & NW, NE Cay, F, 7f. }	17 25	75 59	Mona I., EW 6m., (&, w, } W end, 5, rfa. 2m.), 175f., } C. San Juan }	18 3	67 51	
	Pedro Bk., EW 31 l., SW rock	16 48	78 13	Desecho I., [1m.], T, F, vis. 121	18 22.7	67 29.2	
	— NW edge, &	17 36	78 52				
	— Portland rk., E edge, 32f. } [3c.], 15f., &, &, E }	17 6	77 26				
	Razo Nuevo, EW 5 l., NE pt.	15 53	78 34				
	Swan Is., 2, 4 1/2m., l, 60f., (W } ome, F, w, F, E pt., &, l, } [3m.], 15f., &, &, E }	17 25	83 56				
Porto Rico	ST. DOMINGO.			PORTO RICO.			
	St. Domingo, EW 190 l., Ept., } C. Engano, (shl. N 3m.) ... }	18 33.8	68 18.7	Aguila Pt., lt. R 128f.	17 58	67 15	
	C. Rafael, Mt. Redonda, 2m. inland	19 1	68 55	Suolas 2 l. off W coast, Bajo } Gallardo, [3] }	18 0	67 21	
				B of Mayaguez, lt. F	18 13	67 10	
				Aguadilla B., lt. Fl., r, w, [3m.], ...	18 28.5	67 11	
				Porto Rico, [3m.], MORRO, } lt. R 174f. }	18 28.9	66 7.5	
				NE extr., or C. Juan, (rks.), } lt. F, Fl. 266f. }	18 23	65 36	
				Anvil, 3700f.	18 19	65 47	
				SE pt., C. Mala Pasqua	17 59	65 49	
				Cazo de Muertos I., [1m.], } (& W 1), S rk., lt. F, Fl. } 297f. }	17 53	66 34	

MARITIME POSITIONS							
(157) Places		Lat. N	Lon. W	(158) Places		Lat. N	Lon. W
Virgin Islands	Port Ponce, lt. Fl. 39f.	17° 58'	66° 40'	Guadeloupe	Guadeloupe, Vieux Fort, pt....	15° 57'	61° 42'
	Pt. Guanica	17 56	66 57		— Basse Terre, Fort Irôis @	16 05	61 45?
	CARIBBEAN ISLANDS.				— Soufrière, volc. 5500f.....	16 5	61 39
	Culebra, or l'Passage I., $\frac{3}{4}$ 7m., (SE. w, r, b), Culebrita I., lt. F 305f.	18 19	65 14		Désirade, $\frac{3}{4}$ 7m., N pt.	16 21.4	60 58.7
	St. Thomas I., $\frac{3}{4}$ 4 l., SE, [N]. r, lt. F 93f., E entr., FORT CHRISTIAN.....	18 20.4	64 55.7		Petite Terre, lt. F 108f.....	16 10 5	61 6
	Frenchman's Cap, 195f.	18 14	64 51		Marie Galante, $\frac{3}{4}$ 10m., w W, Grand Bourg, lt. F. 46f.....	15 54	61 19
	St. John's I., EW 3 l., Ham Hd	18 18.1	64 42		Dominica, $\frac{3}{4}$ 9 l., A, S, 1m., 4747f., N pt.	15 38	61 26
	Norran I., 440f., Man of War H., on W side. [N] Npt.	18 20	64 37		— Roseau, town, lt. F.	15 17.4	61 23
	Tortola, $\frac{3}{4}$ 10m., ab. 1780f. Town, [N] w, r, Fort Burr Pt.	18 25.1	64 36.5		— South pt., A, S. st.	15 13	61 22
	Ginger I., [1m.] 500f., 1 ...	18 24	64 28		Martinique	Aves I. [3c.], 10f., w ? & W...	15 42
Virgin Gorda, $\frac{3}{4}$ 3 l., pk. 1370f., East pt.	18 31	64 18.5	Martinique, $\frac{3}{4}$ 11 l., Mt. Pelée, 4428f.	14 48		61 10	
Anegada, $\frac{3}{4}$ 3 l., $\frac{1}{2}$ 3. (rf SE 3 l.), W pt., w, 30f.	18 45	64 24.7	— St. PIERRE St. MARTIN. Battery, lta. 2 F.	14 43.9		61 11?	
Sta. Cruz, $\frac{3}{4}$ 7 l., 1184f. w, } S. E pt.	17 45	64 34	— Fort Royal, [N] lt. F 131f.. — South pt. islet	14 36		61 4?	
— Christiansted, [N] LANG'S OBSERVATORY, Transit pier, lt. F.	17 44.7	64 41.2	— Caravel rk., 96f., @, @ ...	14 48.5		60 53	
Sombrero, [3m.], l, r, w, r, 37f., @, lt. E 150f. } @	18 35.6	63 27.7	St. Lucia, NS 10 l., 4000f., N pt. — Port Castries, [N] Vigie, lt. F 300f.	14 5		60 57	
Dog I., [& rks. 2 $\frac{1}{2}$ m.], W rk.	18 16.7	63 15.5	— W pt., 2 Sagarloaves, 66f., x, vis. 16 l.	14 1.5		61 1	
Anguilla, $\frac{3}{4}$ 14m., 213f., w, Cust. ho.	18 13.2	63 4.2	St. Vincent I., NS 5 l., 3000f.. — Kingston, Fort Charlotte, lt. F 640f.	13 23		61 11	
St. Martin I., EW 8m., w, r, b. sum. 1361f.	18 5	63 3.9	Bequia I., $\frac{3}{4}$ 2 l., $\frac{1}{2}$ W, w, Admiralty Bay, r, b, N pt. }	13 9		61 13?	
— Fort Marigot, lt. F 66f. @	18 4.1	63 5.5	Grenada, $\frac{3}{4}$ 5 l., 2749f., (S.) 2m.), S pt.	13 5		61 12	
S. Bartholomew, $\frac{3}{4}$ 5m., N pk. 992f.	17 54.3	62 48.5	Windward Is.	— St. George, [N], [N], fort, lt. F	11 59	61 42	
Saba [3m.], A, T, 2820f.	17 38	63 14		Barbados, $\frac{3}{4}$ 6 l., 1104f., E pt., lt., [N]	12 3	61 45	
St. Eustatius, $\frac{3}{4}$ 4m., A, 1950f., Fort fl. st.	17 29.2	62 59		— RICKETTS BATTERY	13 9.9	59 25.5	
St. Christopher, $\frac{3}{4}$ 6 l., w, r, Mt. Misery. 4313f.	17 22	62 48		— BRIDGETOWN, Eagr's Wharf	13 5.7	59 37.2	
— St. George's Ch., lt. F 37f.	17 18	62 43		GULF OF MEXICO.			
Nevis, [2l.], w, r. 3595f. sum.	17 12	62 33		C. Sable, fort	25 7	81 5	
— Charleston, SW pt., w	17 8.8	62 36		C. Romano, l, @, (bk. SW 9m., S f.)	25 51	81 42	
Barbuda, $\frac{3}{4}$ 14m., vis. 6 l., w, r, & SW pt.; S & E pt., S l., 200f.	17 33	61 43		Sanialhel I., [N] ¹² , r, w, b, lt. F, Fl., 98f.	26 27	82 1	
— River fort, SW side	17 35.8	61 49.5		Tampa B., Egmont Cay at entr., lt. F 86f.	27 36.1	82 46	
ANTIGUA, $\frac{3}{4}$ 12m. (8N), 1330f. }	17 6.2	61 50.5		Anclote Cays, lt. Fl. 100f.	28 10	82 52	
St. JOHN'S CATHEDRAL [N] — English Harb., [N], w, [N], Duckyd., flagstaff	17 00	61 45.7	Florida	Cedar Cays, Dépot Cay, (shl.) $\frac{3}{4}$ 7m.), lt. F, Fl. 75f. ... }	29 6	83 4	
— Boggy's Pk., 1339f.	17 2	61 51		St. Mark's, lt. E entr. F 85f.. Dog I., [6m.], $\frac{1}{2}$ 3 E, l., W...	29 4	84 10.5	
Redondo, @, 600f., & n } @	16 55.5	62 18.7		St. George I. (Harb. [N] ¹⁰), C. St. George, lt. F 73f.	29 46.3	84 38.2	
W, T	16 55.5	62 18.7		— C. St. George, lt. F 73f.	29 35.3	85 3	
Montserrat, $\frac{3}{4}$ 3 l., 3000f., w, T, N pt.	16 49.3	62 11.7		C. St. Blas, l, (shl. $\frac{1}{2}$ 4m.), lt. Fl. 198f.	29 40	85 21	
— Plymouth, w, l., lt. F 56f.	16 42.2	62 13		Panacola B., [N] Fort Bar- rancus, lt. Fl. 210f.	30 20.8	87 19	
Guadeloupe, [12 l.], 4870f. N pt.	16 31	61 26.8		Mobile, [N] lt. E entr., R 33f.	30 13.6	88 07	
				— Choctaw Pt., lt. F 47f.	30 40	88 0	

623

(139)	Places	Lat. N	Lon. W	(140)	Places	Lat. N	Lon. W
Louisiana	Ship I., $\frac{1}{2}$ 7 m., $\frac{1}{2}$ w N, } mid.; W pt., lt. F 54f. ... }	30° 12' 6"	88° 58'	Yucatan	Celestun, lt. F 95f.	20° 53'	90° 24'
	Car I., EW 5 m., $\frac{1}{2}$ w, W pt., } lt. F. }	30 13 7	89 10		Pt. Palmas, $\frac{1}{2}$...	21 2	90 15
	Chanteleur Is., $\frac{1}{2}$ 4, $\frac{1}{2}$ w, b, l. } SW, lt. N pt., F 58f. }	30 3	88 53		Sisal, $\frac{1}{2}$ w, b, fort, lt. } F 60f. }	21 10 1	90 2 7
	Mississippi Riv., NE pass., } Frank's I. }	29 11 5	89 0		Sisal rk., [$\frac{1}{2}$ m.], sf., (Snake and Madagascar shls. } NW-d 7 l.) }	21 21	90 10
	— South Pass, lt. Fl. 108f. ...	29 1	89 10		Progreso, lt. F 57f.	21 16	89 36
	— SW Pass, lt. F 128f.	28 58 5	89 23 5		Lagartos, R. San Felipe ...	21 34	88 18
	New Orleans, City Hall	29 57 7	90 6 7		C. Catoche, l, $\frac{1}{2}$ (N pt. of Jolbos I., $\frac{1}{2}$ 6 l.) }	21 36	87 6
	Timbaler I., $\frac{1}{2}$ 7 m., lt. F, } Fl. 111f. }	29 3	90 21		Contoy I., $\frac{1}{2}$ 4 m., l, $\frac{1}{2}$ w, N pt.	21 32	86 49
	Ship I., shoal, lt. R 115f.	28 55	91 5		Mugeris I., $\frac{1}{2}$ 5 m., 80f., $\frac{1}{2}$ w, b, 8 pt., Stone turret. ... }	21 12 7	86 40 5
	South west reef, lt. F 56f. ...	29 23	91 30		Coxumel I., $\frac{1}{2}$ 8 l., 70f., $\frac{1}{2}$ w, N pt. }	20 35 5	86 44 7
	Sabine Pass, Texas Pt., bar sf., mound, lt. Fl. 85f. ... }	29 43	93 51		Ascension B., Noja spit.	19 37	87 27
	Bolivar Pt., lt. F 117f.	29 22	94 45 7		Arcas, [3 m.], rks., $\frac{1}{2}$ w, Cay	20 12 6	91 59 7
	Galveston I., $\frac{1}{2}$ 7 l., l, 3 $\frac{1}{2}$ mid., NE pt. }	29 21	94 45 7		Obispo, shls., 2, $\frac{1}{2}$ 5 m., $\frac{1}{2}$ l, N one, beac. buoy }	20 28 5	92 13
	San Luis Harb., bar sf., town Montagorda Bay, bar sf., lt. F 91f. }	29 4	95 6		Triangles, 3 ls., $\frac{1}{2}$ 7 m., l, rk., $\frac{1}{2}$ w, b, E one ... }	20 54 9	92 13
	Aransas Pass, sf., lt. F 59f. ...	27 51 5	97 3		English tank, [5]	21 47	91 56
Texas	Santiago, Barra de, sf., lt. F 60f. }	26 6	97 10	In g.c. in Gulf of Mexico	Bazo Nuevo, [2c.], sf., l, 8, beac. 35f. }	21 50 5	92 5
	Rio Grande, or Bravo del Noite, U.S. Observatory }	25 57 4	97 7 2		Cay Arenas, Sandy I., [3 m.], l, $\frac{1}{2}$ beac. 20f., N pt. }	22 8	91 23
					Alacranes, $\frac{1}{2}$ 5 l., rks., 8, Whale rock. }	22 35	89 49
					— Port, [2], Perez I., [4c.], huts. }	22 23 6	89 42 2
MEXICO.				HONDURAS.			
Veracruz	Rio Fernando, or Tigre ...	25 23	97 20	British Honduras	Chinchorro bk., or Northern Triangles, 8 l., Great Cay, } N pt. }	18 37	87 20
	Barra de Santander, sf.	23 48	98 43		Ambergris I., or Cay, E or Reef Pt., 8 2 m. }	18 6	87 50
	Barra del Ciega ...	22 38	97 52		— S pt.	18 23	87 23
	Cerro del Mecate, 10 m. in- land. }	22 47	98 3		Lt. ho. reef, $\frac{1}{2}$ 10 l., SE pt., } Half Moon Cay, $\frac{1}{2}$ l., F 8f. }	17 12	87 33
	Tampico, bar sf., 8, fl. st., lt. Fl. 141f. }	22 16	97 49		Turneffe, rfs., $\frac{1}{2}$ 10 l., Mau- ger Cay, 3 lts. F 53f., 49f. }	17 36	87 46
	C. Roxo ...	21 35	97 22		Glover rf., $\frac{1}{2}$ 5 l., 8 pt.	16 41	87 53
	Lobos I., [$\frac{1}{2}$ m.], 35f., $\frac{1}{2}$, w, F, (rf. N 2 m.) ... }	21 23	97 13		Belize, [2], Fort St. George, $\frac{1}{2}$, lt. F 43f. }	17 29 3	88 12
	Tuspan shl., islets, $\frac{1}{2}$ 7 ...	21 1	97 10		Dolphin Hd., 5 m. inland ...	17 17	88 24
	Mexico, city, St. Augustine ...						

Vera Cruz

MARITIME POSITIONS							
(161) Places		Lat. N	Lon. W	(162) Places		Lat. N	Lon. W
Honduras	Rattan Is. Port Royal Harb., [w', George Cay, NW pt.]	16° 24' 3	86° 19' 2	Chiriqui	Chiriqui, lag., [], Chica } Mola riv.	8° 59' 0	81° 55' 7
	Barbarete L. S 1 l. E	16 26	86 9		Valiente Pk., 729f.	9 10 5	81 55
	Bonacca L. ½ 3 l., [] NW and SE, ½, ½, F, sum. 1200f.	16 28	85 55		Racudo L., ½ 2½ m., l, ½, w W pt.	9 6 4	81 34 5
	Misteriosa bk., ½ 8 l. N, S pt. N }	18 44	84 2		High pk., 5251f., (½ 6m. of Buppan bluff)	8 42 7	81 30 0
	Swan Is., 2, EW 4m., W } one, ½, w', F, E pt. }	17 25	83 53		Castle Choco, 6342f., 5 l. inland	8 37	80 52
	Poyas Pk., 3700f., 12m. inland	15 44	84 56		ISTHMIUS OF PANAMA.		
	C. Camaron, projecting, l.	16 0	85 3		Chagre, w riv., rr., San } Lorenzo, fort	9 19 7	79 59 5
	Black R., bar 8, w', b	15 57	84 56		Aspinwall, or Colon, lt. F 60f.	9 22 2	79 54 7
	Patook R.	15 49	84 18		Porto Bello, rr., [], Fort } St. Jeronymo	9 32 5	79 38 5
	Caratasca lag., entr. sf., E pt. }	15 23 7	83 43		Isthmus of Panama.	Farallon Sucio, rk	9 39
False Cape, ½, 8 shl.	15 13	83 22	Pt. Manzanilla, ½, l.	9 39		79 32	
C. Gracias a Dios, l, ½, w., b. }	14 59	83 11	Pt. San Blas, l, (rf. 2m.) ...	9 35		78 58	
Bank off C. Gracias, N part.	16 48	82 10	Mandinga, ½'	9 30		78 58	
— East exit, N	15 32	80 56	Muletas Archipelago, E pt. ...	9 37		78 38	
Caxones, or Hobbies, ½ 4l., E pt. }	16 3	83 6	Pt. Musquitos	9 8		77 56	
Cay Gorda, [2m.], ½, (SE-d. } 2 l)	15 52	82 24	Pine I., [1m.], ½, ½, NE pt. ...	9 1 5		77 46	
Alargate rf., ½ 10m., E pt.	15 7	82 20	C. Tiburón, l, ½, rky., (½ 13 W)	8 41		77 21 5	
Moquito Cays, ½ 60f., (w W } 5m., ½ S 2), SE part. }	14 20	82 44	New Grenada	Pt. Caribana, (shl. ½ 5m.) ...		8 38	76 53
Rosalind bk., SE shl. part. } l, [5m.]	16 8	80 17		l. Fuerte, [1½m.], ½, ½, ½, } Cispata Harb., [], East pt. Zapote		9 24	76 10 7
Serranilla bk., Cays, EW } 25m. S, beacon Cay, 8f. }	15 48	79 51		Santiago de Tolú, E entr.	9 31	75 38	
Serrana bk., ½ 6 l., ½ SW } Cay, 32f. }	14 16	80 24		San Bernardo Is., [3 l.], l, ½, } Nst. one	9 48	75 53	
Quira Sueño bk., rf., NS 8 l., S pt. }	14 8	81 9		Tortuga shls., 2, outer, [] ...	10 3	75 57	
Roncador Cay, ½ 6m., 7f., ½, } w, S pt. l	13 31	80 2		Rosario Is., [2 l.], Wst. one. ...	10 11	75 51	
Old Providence and Catalina } Is., [rfs. 5 l.], w' W, b, r, } ½ ½ W, sum. 1190f. }	13 21	81 23		Cartagena, [], Dome.	10 25 6	75 34 0	
St. Andrew's I., ½ 8m., 50f., } w', r, SW cove	12 31 7	81 44		— Entrance, fort, lt. F 60f. ...	10 19	75 35 2	
Courtown bk., ½ 7m., SW } Cay, ½ w. }	12 24	81 29		Pt. Canoa, l, ½, over, (rks.) } S W-d. 3m. sf.)	10 34	75 33	
Albuquerque Cays, [4m.], ½ W }	12 10	81 54		Pt. Galera, l	10 47	75 26	
Off-lying Islands and Cays	Brangman's Bluff, ½ 2 S, w, l. }	14 3	83 22	Port Sabanita, [], lt. F, FL 98f.	11 0	74 58	
	Rio Grande, bar sf.	12 54	83 32	Magdalena Riv., bar, l, b, w, } C. Augusta	11 6	74 51	
	P. arl Lagoon, entr., N pt., (shl.)	12 21	83 38	Sta. Maria, [], Morro, lt. F 328f. ⊕	11 15	74 14 7	
	Blew fids. [1½], (shifting } bar), r, W pt. of bluff. }	11 59 3	83 41	C. Aguja, l, ½, T, (rks. 8c.)	11 20	74 12	
	Little Corn I., l, ½, [1½m.], } W pk. }	12 17 0	82 36	C. San Juan de Guis.	11 21	74 0	
	Great Corn I., ½ 2½ m., ½, ½, } w, b, r, ½ ½ SW pt., sum. }	12 9 2	82 59 7	Hacha, 8, lt. F 90f.	11 33	72 55	
	Pajaro I., small, 155f.	11 31	83 43	C. Vela, (islet 2c. off, 8c.), E pt.	12 10	72 12	
	San Juan de Nicaragua, } (called Grey-town, 1848), } [], w' up riv., b, r ... }	10 55	83 43	Bahia Honda, ½', 8 shl. in } mid. entr., E pt. }	12 19	71 46	
	Pt. Arenas	10 56 7	83 43 2	Pt. Gallinas, (shl. 2m.)	12 25	71 42	
	Mt. Cartago, 11, 100f.	10 2	83 48	Druid shl., [], T E	12 30	71 39	
Moquito Coast	Pt. Blanco, Grape Cay, E } of do., (w W 1m.), lt. F 60f. }	10 0 0	83 2 5	Pt. Espada	12 4	71 8	
	Carreta Pt., w W 2m.	9 38	82 40	Zapara Castle	11 1	71 38	
	Boca del Toro, [], fort, w' } ½ 1m., r., b	9 20 5	82 15 2	Maracaybo, [1½], bar, entr., } (shifts)	11 2	71 39	
	Blanco Pk., 11, 740f.	9 17	83 4	— Town, 20m. up the lake, rf.	10 41	71 42	
	Shepherd's Harb., [], Cay, } ½ 2½ m., White hut ... }	9 14 4	82 20 7	Pt. Arenas	11 7	70 55	
	Zapadilla Cays, ½ 3m., E pt. ...	9 15	82 2	Coro	11 24	69 44	
				Pt. Cardon, l	11 36	70 18	
				C. San Roman	12 11	70 5	
				Pt. Manzanilla	11 31	69 20	
				VENEZUELA.			
Costa Rica			Monjes, 8c., N rks.	12 29	70 57		
			Oruba I., ½ 5 l., Port Ca- } ballos, lt. F 40f. }	12 29	70 7		
			Caracao I., ½ 12 l., Mount } S. Christoffel, 1200f. }	12 19	69 9		

621

Coast of Venezuela

Trinidad

MARITIME POSITIONS

(165) Places		Lat. S	Lon. W	(166) Places		Lat. S	Lon. W
N. Coast	Manoel Luiz shl., [1 l.], } T. $\beta\beta_0$, W rk. }	0° 51'	44° 17'	E. Coast	Anchoras Is., [1 l.], E one ... C. Frio, (l. $\frac{1}{2}$ 2 $\frac{1}{2}$ m., $\frac{1}{2}$ 4). } 8 pt., lt. Fl. 300f. }	22° 40' 5	41° 45'
	Silva shl.	0 32	44 19		C. Negro, l. $\frac{1}{2}$ 3 m., pt.	22 57	42 39
	I. St. Anna, [7 m.], (rfs. $\frac{1}{2}$ } 4 l.), $\frac{1}{2}$ l. R 190 f. }	2 16	43 38		Maricas Is., $\frac{1}{2}$ 1 l. $\frac{1}{2}$ 8. Sat.	23 1	42 54
	Lançoes Grande, W pt.	2 21	43 22		Raza I., [$\frac{1}{2}$ m.], lt. R 315f.	23 3 7	43 8 7
	Barra Velha, B. Paranalhyba, lt. F.	2 50	41 44		Rio Janeiro, [4], fort Villa- gagnon, [4], lt. F 59f. }	22 54 8	43 9 5
	Jericoacoará w, f, E sand hill	2 47	40 28		Rio Janeiro, OBSERVATORY ...	22 54 4	43 10 2
	Almufedas, vill., Steeple in f	2 56	39 48		Gabia Mt.	22 59	43 17
	Mt. McLancias, isolated sand hill	3 12	39 18		Pt. Guaratiba, hill	23 3 6	43 3 2
	Ceara, Church tower.	3 43	38 32 5		Marambaya I., EW 8 l., T S, } W pt., (E entr. of Ilha Grande B. w. b.), hill 2066f. }	23 4 4	43 59
	Pt. Macoripe, lt. F 85f.	3 42	38 27		Lage rk., 18f.	23 6 6	43 49 7
Brazil	Jaguaripe R., bar, $\beta\beta_0$, w, N pt., lt. F.	4 25	37 45	Brazil	I. Grande, EW 6 l., [4] N, E. pt., or Pt. Castellhanos }	23 9 7	44 5 2
	Araçati, town	4 31	37 48		Ubatuba Ch.	23 25 9	45 3 7
	Morro Tibão, red sand hill ...	4 49	37 18		Pt. Cairuçu, E sum. of mt.	23 18 2	44 35
	Pt. do Mel, $\frac{1}{2}$ l. (shls.), N pt.	4 55	36 53		Porcos Is., [rks. 4 m.], $\frac{1}{2}$ l. S hill	23 32 9	45 3 2
	Pt. Tubarão, N sand hill	5 2	36 28		Basios Is., [2 m.], SE one	23 44 5	44 59
	Urcas, shls., A, T N, N edge...	4 50	36 16		St. Sebastian, [4], w, r, b, } town }	23 47	45 21
	C. St. Roque, l. 1	5 30	35 16		St. Sebastian I., $\frac{1}{2}$ 5 l., via, 15 l., S pt.	23 57	45 15
	Rio Grande do Norte, [4], Circular Fort on ledge, } (w $\frac{1}{2}$ m.), lt. F 43f. }	5 45	35 11		Mont de Trigo, A, $\frac{1}{2}$	23 51	45 45
	Parahybad Norte Riv., [4] 1 $\frac{1}{2}$, Pedra Secca, lt. R 52f. }	6 56	34 49		Moela, lt. F 334f.	24 2	46 13
	Fort Cabedello, f	6 57 8	34 50		Santos Harb., [4], r, w' 7 m., up river, b, Arsenal }	23 55 8	46 19
E. Coast	C. Branco, sand, 1, (2 f at pt ?)	7 8	34 48	S. E. Coast	Pt. Taipu	24 1	46 24
	Pt. de Guia, E extr. of S. Amer.	7 26	34 47		Alcatrazes Is., rks., 8 5 m., sum. }	24 6	45 40
	Olinda Pt., lt. Oce.	8 1	34 50		Lage de Santos, rk. 7f.	24 18	46 11
	PERNAMBUCO, [4] 1 $\frac{1}{2}$, bar, w', f, b, Fort Picao, lt. R. }	8 3 4	34 52		Queimada, Is., 2, $\frac{1}{2}$ 10 m., large or outer one }	24 28	46 40
	C. St. Agostinho, $\frac{1}{2}$ l., Ch. sum.	8 20	34 56		Iguape R.	24 37	47 22
	Mt. Sellada, S pk.	8 25	35 11		Bom Abrigo L., [1 $\frac{1}{2}$ m.], A, $\frac{1}{2}$, lt. Fl. 504f. ($\frac{1}{2}$ E, Cananea, [4], bar 5). }	25 7	47 52
	St. Aleixo I., [2c.], w	8 56	35 0		Mt. Cardoso	24 59	48 6
	Tamandaré, [4], fort	8 43 4	35 5		Figueira L., [$\frac{1}{2}$ m.], 160f., $\frac{1}{2}$ 4 T	25 22	48 3
	Macao f, w, fort, ($\frac{1}{2}$ l. R } 208f. }	9 39	35 39		Paranaguá B., [4], town	25 31	48 28
	R. St. Francisco, S, or Samoco Pt., l., $\frac{1}{2}$ l., β 1 $\frac{1}{2}$ m., lt. F 59f.	10 29	36 24		I. do Mel, $\frac{1}{2}$ 3 m., lt. F } 262f. }	25 33	48 18
E. Coast	Itabayana Mts., sum.	10 47	37 23	S. E. Coast	Coral I., [1 m.], 64f., $\frac{1}{2}$ 2 m.,	25 47	48 22
	Tres Irmaos, 3 mts., 2 l. in- land, SE hill	11 16	37 17		R. Guaratuba, pt., hill	25 33	48 36
	Mt. Maserandupio, 10 m. inland	12 24	38 4		St. Francisco I., $\frac{1}{2}$ 6 l., A, } $\frac{1}{2}$ C. Joao Dias, lt. F 309f. }	26 10	48 33
	BAHIA, [4], C. St. AN- TONIO, lt. R 140f. }	13 0 7	38 32		Tamboretas Is., [1 l.], $\frac{1}{2}$ l., S one	26 21	48 32
	Morro St. Paulo, lt. R 27f.	13 23	38 52		Itapacoroya Pt., N part.	26 47	48 47
	Quamannu B., Pt. de Muta	13 52	38 56		Pt. Bombas	27 8	48 29
	Os Ilheos, rks., large one	14 47	39 0		Arvoredo L., $\frac{1}{2}$ 2 m., $\frac{1}{2}$ l., F, Fl. 292f. }	27 18	48 22
	St. George, town, fort	14 49 4	39 1		Anhatirim, w N 2 m., f, } b, fort, fl. st., lt. F 125f. }	27 25 5	48 34 5
	Porto Seguro, [4], f, Cathedral	16 26 8	39 0		St. Catherine I., $\frac{1}{2}$ 10 l., [4], NW-d.), N pt. }	27 22 5	48 25 7
	Abrolhos Is., [1 $\frac{1}{2}$ m.], $\frac{1}{2}$ W 8 m., St. Barbara, lt. Rev. } 189f. }	17 58	38 41		— Nostra Senhora de Desterro	27 35 4	48 32
E. Coast	Sta. Cruz, Ch.	16 17 3	39 0 2	S. E. Coast	Pt. dos Naufragados, lt. Rev. } 149f. }	27 49	48 32
	Rio Doce, W pt., entr.	19 37	39 46		Pt. Pinheira	27 54	48 35
	Espiritu Santo B., w', f, b, Sta. Luzia, lt. F 66f. }	20 19	40 16		Batuba Pt., lt. F 69f.	28 16	48 40
	Guarapari, Ch.	20 43 9	40 27		Lagos, (City Im. W-d.) bar ...	28 28 5	48 48
	Calvada Islet, 4 m. out. l. W ...	20 44	40 21		C. Sta. Marta	28 39	48 50
	C. St. Thomé, l. (bks. 15 m.) off, lt. Fl. 157f.	22 2	41 0		Rio Grande do Sul, entr. s. w, f, E pt. tower, lt. F, Fl. 101f. }	32 7	52 7
	St. Ann Is., 3, $\frac{1}{2}$ 4 m., w, b, sum. grt.	22 25	41 41				

TABLE 10

627

MARITIME POSITIONS

(167)		Places	Lat. S	Lon. W	(168)		Places	Lat. S	Lon. W
R. Plate	URUGUAY.								
	C. Polonio, lt. F 137f.	34°25'	53°47'	Watchman C, l. (shl. 2 l. s.)...	48°21'	66°20'			
	Ranger rk., small. 880.	34 30	53 51	Bellaco rk., or Eddystone, 6f...	48 29	66 12			
	C. St. Mary, († N-d. m.), lt. }	34 40	54 9	C. Curioso, l. striped	49 11	67 37			
	Rev. 132f.	34 40	54 9	Wood's Mr., via. 11 l.	49 137	67 45			
	I. Lobos, [1m.], (rfs. E. d. 3m.)	35 1	54 52	Pt. St. Julian, [D], Sholl Pt...	49 153	67 41?			
	Maldonado, tower, w.	34 53.5	54 57.7	C. Francisco de Paulo, l.	49 42	67 37			
	Flores I., [1m.], lt. R ^o 106f. ...	34 57	55 55	Port Sta. Cruz, bar rif., Mt. }	50 9	68 22			
	MONTE VIDEO, RAT I.	34 53.5	56 14	Entrance, on Side, l. 350f. }	50 54	69 8			
	Colonia, lt. Rev. 110f.	34 28	57 51.7	Coy Inlet	50 54	69 8			
Buena Ayres	ARGENTINA.								
	Buenos Ayres, Custom }	34 36.5	58 22.2	C. Fairweather, ab. 300f.	51 32.1	68 55.5			
	HOUSE, lt. F	34 36.5	58 22.2	Port Gallegos, [D], Obsn. }	51 33.3	68 59.2			
	Santiago, pier head, lt. F	34 48	57 53.5	Cape Virgins	52 20.2	68 21.7			
	C. St. Antonio, N pt., or Pt. Rasa	36 19	56 45	FALKLAND ISLANDS.					
	Pt. Medano, (shl. 6m.), S sum.	36 59	56 41	Jason Is., $\frac{3}{4}$ 9 l., 3 l., W Cay...	50 58.5	61 27.7			
	Mar Chiquito, (entr. impract.)	37 47	57 22	Grand Jason, $\frac{3}{4}$ 4m., 1210f...	51 3.2	61 3			
	C. Corrientes, h. l. 120f., E. um.	38 5	57 29	White rk.	51 17	60 52			
	Pt. Mogotes, h. l. 104f., 3 2m.	38 5.7	57 31.2	New I., NS 5m., [D] $\frac{1}{4}$ NW pt.	51 42	61 17			
	Gueguen R., l.	38 36	58 40	Bird I., EW $\frac{1}{2}$ m., 410f.	52 11	60 54			
Patagonia, E. Coast	Sierra Venana, 3500f.	38 11.7	61 56.5	West Falkland, $\frac{3}{4}$ 25 l., Port }	52 11	60 41.2			
	Rahia Blanca, Mt. Hermosa, }	38 59	61 39	Stephens, entr. E pt. }	52 15.2	60 38			
	lt. F 168f.	38 59	61 39	C. Meredith, S extr. 290f.	52 13	60 21.7			
	Fort Argentino	38 43.8	62 15	Albemarle rk. 150f.	52 0.7	60 13.2			
	R. Colorados, bar rf.	39 52	62 4	C. Tamar, 150f., N cliff. sum...	51 17	59 29			
	Union B., 17f., Indian Hd. }	39 57.5	62 7.2	Port Egmont, Cove, ruins	51 21	60 3			
	45f., l. ϕ , w, b.	39 57.5	62 7.2	Wreck I., EW 3m., W extr.	51 10	60 14			
	San Blas Harb., [D] w', b', r. }	40 30.4	62 8	Port San Carlos, [D], w, b, }	51 27.2	59 7.2			
	r. Main Pt. 35f., W entr. }	41 3	62 48	Fanning Hd., SW sum.	51 10	59 2.5			
	R. Negro, bar rf. ? South }	40 49	64 54	East Falkland, $\frac{3}{4}$ 27 l., Port }	51 23.7	58 19			
Sandwich Is.	Barranca, r. b, lt. F 143f. }	41 41	65 12	Salvador, [D], Shag I., entr. }	51 25.2	57 50.5			
	Port St. Antonio, [D], w, b, E }	42 14	64 25	C. Carysfort, NE cliff	51 32	58 7			
	hd., or Villariño Pt., (bk. }	42 13	63 48	Extr. C. Pembroke, lt. F 110f.	51 40.7	57 42			
	4m. S), hum 40f.	42 46	63 37	Port Louis [D], Settle., fl. st. }	51 41.2	57 51			
	Sierra de Sn. Antonio, 1700f...	42 53	64 8	Lively I., NS 7m., SE pt., (rks.)	52 4.7	58 25			
	Port San Josef, w, b, W head, pt.	42 58	64 20	Sea Lion Is. and rks. EW }	52 25	59 8.5			
	Valdez Penins., Pt. Norte, 3 lm.	42 58	64 20	11m., W extr.	52 22.3	59 47.7			
	Pt. Delgada, 200f., SE cliff ...	42 58	64 20	George I., $\frac{3}{4}$ 7m., rks. W }	52 55.7	59 12.7			
	Nuevo G., E, or Nuevo Hd. }	44 25	65 8	2m. SW pt.					
	l. 200f., T. (w', b)	44 32	65 22	Beauchene I., [1½m.], 200f., }					
W Ed., Niuas Pt. 240f., }	44 55	65 31	(rk. $\frac{3}{4}$ 5m.?), S pt. }						
Sandwich Is.	rks. 2m., E cliff	45 1	65 29	SOUTH ATLANTIC ISLANDS.					
	Salaberría r., $\frac{3}{4}$ 8m., N and }	45 0	65 40	South Georgia, $\frac{3}{4}$ 30 l., C. }	53 59	37 28			
	E pt.	45 10	65 53	North, pt., or C. Buller... }	54 4	38 14			
	Port St. Elena, w, b, S Head	45 6	65 56	Wallis I., EW 4m., W pt.	54 37	37 3			
	C. Two Bays	45 13	66 30	Annenkov I., [2m.], pk.	55 2	36 2			
	Arce I., [1m.], SE sum.	45 34	67 20	Mokke Harbour, Obsn. spot...	54 30.9	36 5.7			
	The Oven, or Prince Regent }	47 6	65 51	Clerks' rks., $\frac{3}{4}$ 2 l., S extr. }	55 4	34 38			
	haven, [D], entr.	47 12	65 44	Shag rks.	53 48	42 45			
	Medrano rks.	47 45	65 55.5	Marquis de Traverse Is., h. }	56 18	27 29			
	Tova I., $\frac{3}{4}$ 4m., (Cove $\frac{3}{4}$ }	47 55	65 42	N one, Zavodovski, [3m.]}	56 41	28 10			
	l., b', w)			W one, or Lienkov, [2m.]} ..	57 10	26 45			
C. Aristazabal, (rks. off)			Candlemas Is., EW 6m., h. }	57 52	26 24				
Salamanca Pk., 700f.			volc., E one	58 27	26 44				
C. Three Pts., ab. 2000f., 30 }			Saunders' I., $\frac{3}{4}$ 6m., sum.	59 0	26 18				
1m., NE pitch			Montague I., [3 l.], Cape	59 26	27 13				
C. Blanco, l. rugged, (shls. }			Bristol I., [3 l.], E pt.	60 49	44 20				
2 l.), NE sum., (S Cove, }			Southern Thule Is., [3 l.], E pt.						
w, b'')			E extreme of group, rk.						
Port Desire, w', b', ruins									
Sea Bear B., ϕ , b, w at pt. }									
Penguin I.									
Sirius rk.									
Monte Video, ab. 300f.									

MARITIME POSITIONS

(169) Places		Lat. S	Lon.	(170) Places		Lat. S	Lon. W
<i>New Orkneys</i>	Laurie I., EW 7 l., E pt., C. } Dundas, 559f. }	60° 54'	West 44° 20'	<i>Tierra del Fuego</i>	Diego Ramirez Is., NS 5m., } 587f. }	56° 31'	68° 43' 2
	Murry Is., 1410f. 8 one	61 2	44 30		York Minster	55 25	70 3
	Saddle I., [4m.], W pk., 1643f.	60 43	45 10		C. Castlereagh, (Stewart Hr. } NE-d)	54 56 5	71 29
	Coronation I., 4, 12 l., E sum. } 5397f. }	60 46	45 53		Townshend Harb., 4, " islet, N	54 42 3	71 55 7
	— NW pt., or Pt. Penguin ...	60 33	46 40		Tower rks., 2, [1 1/2 m.], S & Est.	54 37	73 3
	Despair rk.	60 36	47 12		C. Noir, (8 2m.), 600f., 8 pt....	54 30	73 6
	Inaccessible Is., [4m.], 337f.	60 40	47 38		C. Gloucester, W pt.	54 5	73 30
	Cornwallis I., [2m.]	61 4	54 28		C. Inman, (rk. 4-2m.)	53 19	74 19 5
	Elephant I., 4, 9 l., E sum.	61 6	54 45		Dislocation Harb., 4, (w 4) ...	52 54	74 37
	— Rocks, NW-d., outer	61 0	55 40		C. Desendo, 4, (rky. 1. 2m. off)	52 44	74 45
	O'Brien I., [1m.]	61 32	55 52		C. Pillar, N cliff.	52 43	74 42
	Rocks	61 43	56 50	SOUTH AMERICA.			
	Bridgeman I., [2m.], 600f. } volcano	62 10	56 40	West Coast.			
	King George I., 4, 13 l., } E pt., or C. M. ville ... }	62 2	57 30	CHILE.			
	Ridley I., [2m.]	61 48	58 0	<i>Magellan Strait</i>	C. Virgins	52 20 2	68 21 7
	Livingston I., 4, 10 l., NW } pt., C. Shirreff	62 28	60 28		Dungeness Pt.	52 24	68 25 7
<i>New S. Shetland</i>	Deception I., NS 10m., Port } Foster, 4, Mt. Pond ... }	62 55 6	60 30		C. Possession, Refuge Beacon	52 18 3	68 56 7
	Smith I., EW 7 l., Mt. Fos- } ter, 6600f. }	63 2	62 47		Direction Hill Beacon, 224f. ...	52 22	69 30
	William rk.	63 17	63 0		SANDY POINT, BOAT-HO. 1. F 26f.	53 9 9	70 54
	C. Possession	63 45	61 50		PORT FAMINE, TENT N SIDE } BAY	53 38 2	70 56 5
	Astrolabe I., EW 4m., mid.	63 16	58 20		C. Froward, (Sext. of America)	53 54 6	71 18 5
	Joinville I., EW 15 l., S pt., } or C. Purvis	63 39	55 48		Port Gallant, Cross Id.	53 42	71 59 7
	C. Seymour	64 13	56 32		Mt. Sarmiento, 7330f., 2 pks. ...	54 28	70 52 5
	Mt. Haddington	64 12	58 2		Mt. Buckland, ab. 4000f.	54 26	70 23 7
	Biscoe Is., Pitt I., mid.	65 20	65 38		Port Angosto, Hoy Pt.	53 13 5	73 22 5
	— Adelaide I., 4, mid.	67 15	68 15	<i>Patagonian Inner Channel</i>	Tuesday B., Cascade Pt. ...	52 50 2	74 29 5
<i>Antarctic Ocean</i>	Alexander I., N pt.	68 51	73 10		Port Churruca, Diaz I., 60f.	53 1 4	73 56
	St. Peter I.	68 57	90 46		Port Tamar, Mouatt Id.	52 56 5	73 46 5
	ANTARCTIC OCEAN.		East		Sholl B., Obs. spot.	52 44 5	73 53
	Sir Jas. C. Ross' furthest	78 4	161 0		Otter B., Obs. Pt.	52 22 5	73 40
	Mt. Erebus, 12,400f.	77 33	166 58		Fortune B., Low L.	52 15 8	73 41
	Mt. Sabine	71 42	169 55		Isthmus B., Obs. Pt.	52 9 6	73 36 5
	Bullenby Is.	66 44	163 11		Columbine Cove, islet	51 53 3	73 41 5
	Adelie Land, Geology Pt.	66 35	140 10		Mayne Harb., head of Str. ...	51 18 5	74 4
	TIERRA DEL FUEGO.		West		Puerto Bueno, Obs. Rock	50 59 4	74 11 7
	Pt. Catherine, l.	52 33	68 46		Port Grappler, Obs. Pt.	49 25 3	74 17 5
<i>Tierra del Fuego</i>	C. St. Sebastian, l., 190f., N sum.	53 19	68 10	<i>W. Coast Patagonia</i>	Eden Harb., cove, (staff)	49 7 5	74 25 2
	C. Peñas, SE cliff	53 51 5	67 33		Halt B., Obs. I.	48 54 3	74 21
	C. San Diego, l., l., E pt.	54 41	65 7		Island Harb., Obs. I.	48 36	74 36 2
	Staten I., C. St. John	54 42 3	63 43 5		Guanaco Is., S. Pedro I., } 410f. }	47 44	74 52 5
	— Vancouver, C. Kendall	54 49 8	64 6		Westminster Hall, [1m.], 1120f.	52 38	74 22
	C. St. Bartholomew	54 54	66 46		Evangelists, Sug. loaf, 360f. ...	52 24	75 4
	Good Success B., 4, w, b, S hd.	54 49	65 13		C. Victory, or Narborough pt.	52 16	74 55
	C. Good Success A., l., rks. close	54 55	65 22		Diana Pk.	52 8	74 48 5
	Ushuwa, Beagle Channel, } Mission Station	54 49 4	68 18 5		C. Isabel, 4, l., (pk. 2m. E), pt.	51 50	75 11
	New I., 4, 8m., 80. Pt. Waller	55 11	66 33		Cambridge I., C. St. Lucia ...	51 30	75 22
<i>W. Coast Patagonia</i>	Barneveldt Is., [2 1/2 m.], cent. ...	55 49	66 48 5		Scout rks., 10f.	50 49	75 40
	C. Horn, ab. 1891f.	55 59	67 16		Madre de Dios Archip., W } cliff, l. }	50 36	75 32
	Hermit I., EW 14m., West C. ...	55 50	67 55		C. Three Pts., Rugged Hd., } 2000f., (rks. 2m.) }	50 1 4	75 23
	— St. Martin Cove, 4, w, b, w	55 51	67 34		Port Henry, 4, w, b, W head	50 0	75 20 5
	Orange B., 4, Pyramid I.	55 31 4	68 5 5		Mt. Corso I., SW sum., (shls. } 5m.), 1420f. }	49 46 4	75 32 5
	False C. Horn	55 43	68 3		C. Montague, extr. of rocky spit	49 11 5	75 50
	Ildefonso Is., 4, 5m., 100f., mid.	55 50	69 18				

MARITIME POSITIONS

(171)	Places	Lat. S	Lon. W	(172)	Places	Lat. S	Lon. W
	Parallel Pk., 2m. inland, 2800f.	48° 46'	75° 31'		Horeon B., (♂, ♀, F, b), Hd., (rks. 1½m.)	32° 42' 5"	71° 30' 7"
	Dundee rk., 45f.	48 55	75 37.5		Papado B., Gobernador Mt.	32 31	71 28.7
	Port Sta. Barbara, W head	48 2	75 25		Pichidanque B., ♂, Locos I.	32 7.9	71 32.7
	Guianeco Is., Byron I., W pt.	47 46	75 20		Mt. Talinay, 2300f.	30 51	71 38.7
	C. Machado, ♂, (rks. 2m.)	47 26.5	74 29		Pt. Lengua de Vaca, (B. E-d. ♂)	30 14	71 38.7
	Purcell I., [2m.], ♂, SW rk.	46 55	74 39		Herradura de Coquimbo, ♀, w. b., SW corner	29 58.7	71 22.7
	Port Otway, S entr., sum.	46 49.5	75 16		Coquimbo, ♀, w., ♂, r., (L Sig- nal-hill), Tortuga Pt., lt.	29 57	71 21
	C. Tres Montes, 1, 1300f., pt.	46 59	75 26		F. Fl. 98f.		
	C. Raper, rk. close	46 49	75 37.5		Pajeros Islets, 2, 2½ 3m., N & W one	29 33	71 35.
	C. Gallegos, T	46 35	75 35		Chaneral I., [2m.]	29 1	71 37
	San Estevan, port, w., ♂, entr.	46 18	75 9		Huasco Port, ♂, w., pier lt.	28 25	71 16
	Hellyer rk., [1m.]	46 4	75 11.5		Herradura Pt., ♂, l., w.	28 6	71 13
	C. Taytao, 2850f., 1, 8 1m., W pt.	45 53	75 5.5		Copiapo, ♂, w., r., b., land pl.	27 19.5	70 59
	Huamblin I., 700f., NS 3 l., ♂, W hd.	44 49	75 12		Morro Pt.	27 7	70 59
	Ypun, or Narborough I., 2½ 9m., (Scotchwell Harb., SE, b, w), S, or John Pt.	44 40.7	74 45.7		Port Caldera, W hd., lt. F, Fl. 121f.	27 3	70 53
	Port Low, ♀, w., b, F, Hua- canec I., 2½ 2m., S pt.	43 48.5	73 59.5		Flamenco, port. S head	26 54	70 45
	Huafu I., 2½ 13m., ♂, ♀, NW pt., 800f., (rks. 3m.)	43 36	74 46		Ballena Pt., rks.	25 49	70 48
	Chiloe I., NS 3 l., W pt., C Quilan, ♂	43 17	74 23		Grande Pt., ♂, E, W sum. 1572f.	25 7	70 31
	— Corona Hd., lt. F, Fl. 224f.	41 47	73 52		Paposo vill., w, b, White Hd.	25 2	70 30
	— C. Matalqui	42 11	74 11		Jara Hd., 1, w N	23 53	70 33
	Huechucneuv Hd.	41 46	74 0		Antofagasta, Custom ho., lt. F 30f.	23 39	70 25
	C. recobado Volc., 7500f.	43 11.3	72 45.7		Mt. Moreno, (Jorge, old), 4160f., ♂	23 28.5	70 35.2
	Chayapirin Volc., 8000f., sum.	42 48	72 31.5		— Constitution R.I., [♂], w. b.	23 26.7	70 37.5
	C. Queal, T	41 3	73 57.7		Leading bluff, islet off	23 1	70 32
	Pt. Guiera, W pt., lt. F, Fl. 180f.	40 2	73 43.7		Mt. Mexillones, 2560f., (3m.) inland	23 65	70 32
	Gonzales Hd., N pitch	39 51	73 26.7		Cobija B., w, r, fl. st., l.	22 34	70 18
	Fort Corral	39 52.9	73 26		— Pk., 3330f.	22 32	70 15
	Valdivia, ♀, Niebla bluff, lt. F 121f.	39 52	73 24		C. St. Francisco, or Paquiqui	21 56	70 12
	Mocha I., 2½ 7m., (rks. 3m., ♂, ♀ and ♂, l., r., b, w), sum., 1250f.	38 23	73 55.7		Arena Pt., l, ♂ 16	21 39	70 10
	Tucapel Hd., (R. Leibu, E-d.)	37 36	73 38.7		R. Loa, l., w., and Gulley	21 28	70 3
	Lota Point, lt. R 180f.	37 5	73 11		Chipana B., ♂, tail of pt., l.	21 23.0	70 8
	Sta. Maria I., NS 6in., l, ♂, (rks. 4-11, w, b, r), lt. Fl. 258f.	36 59	73 32		Lobo, or Blanco Pt., l, 1, ...	21 5	70 13
	Arauco, fort	37 15	73 19		Carrasco Mt., 5521f.	20 58.5	70 7
	Paps of Bio Bio, 800f., SW sum.	36 48	73 11.7		Grueso Pt., l, 1, l, ...	20 23	70 13
	Concepcion, ♀, City, mid. at river	36 49.5	73 2.2		Iquique, w, Id., lt. F, Fl. 98f.	20 12.5	70 11.5
	Talcahuano, w. r, b., Quiri- quina I., lt. R 213f.	36 36	73 3		Pichalo Pt., projecting	19 37	70 16
	Pt. Carranza, rks.	35 37	72 38.7		Pisagua, Gulley and R., l., w.	19 34	70 14
	Riv. Maule, Church rk., (bar 1½m.), ♂	35 19.7	72 26.2		C. Lobos	18 45	70 24
	Bucalemo Hd., (Rapel sh., 4 2m.)	33 52	71 49.7		ARICA, w, r, f, IRON CHURCH (Inglezia Matrix)	18 28.7	70 20
	Algarroba Pt.	33 26	71 42.7				
	Caramilla Pt., rk.	33 6	71 44.7				
	Bell of Quillota, 6200f., 7 l. inland	32 57.2	71 6.2				
	Aconcagua, 28,080f., 25 l. in- land	32 38.5	69 57.7				
	VALPARAISO, ♀, ♀, EXCHANGE CUPOLA	33 2.1	71 38.5				
	PORT ST. ANTONIO, SITE OF	33 1.9	71 38.5				

TABLE 10

MARITIME POSITIONS

(175) Places		Lat N	Lon. W	(176) Places		Lat N	Lon. W
Neurayus	C. Velas	10°21'5	85°53'	Rocky Bluff, 408f.	31°20'	113°40'	
	Culebra, \square , entr. S, Vir- d res Is.	10 35	85 43'2	Colorado R., Port Isabel beacon	31 46	114 42	
	St. Elena Pt.	10 53'5	85 58	San Felipe Pt., 940f.	31 2	114 49'5	
	Salinas B., Salinas Is., [3c.] ..	11 28	85 43'5	Guardia I., $\frac{1}{2}$ 13 I., Pt. }	29 33'1	113 35'2	
San Salvador	Port St. Juan, S bluff, lt. F 490f.	11 15'2	85 53'5	Refugio	28 25	112 51	
	C. Desolado	11 59	86 42	Sta. Teresa B., N pt.	27 26	111 53	
	Realejo, \square , r, b, Cardon I., $\frac{1}{2}$ }	12 27'9	87 12'7	I. Tortuga, [2m.], 1016f.	27 3	111 56	
	Volcan Viejo, 5670f.	12 41	87 1'5	Sta. Inez Pt.	26 53'5	111 57'5	
Guatemala	Pt. Consegüina, (Volcano, }	12 58'5	87 35	Ildefonso I., [1m.], 387f.	26 37	111 26	
	2830f., $\frac{1}{2}$ 31.)	13 17'1	87 47	La Giganta Pk., 5794f.	26 6	111 35	
	G. of Conchagua, or Fonseca, Port de la Union, \square , w, r, }	13 25'5	88 18	Loreto	26 0'5	111 20'5	
	Chicarense Pt.	13 28'8	89 19'2	Carmen I., 1572f., $\frac{1}{2}$ 4 I., }	25 59'5	111 7	
Mexico, W. Coast	S. Miguel, vol., 7134f.	13 30	89 48	Salinas B.	25 42	110 47	
	LISENTAD, l., r, PIER Hd. lt. F }	13 34'4	89 50'7	Catalina I., [7m.], 1548f., pt...	25 16	110 43	
	Pt. Remedios, l., $\frac{1}{2}$, (r, $\frac{1}{2}$ 3m.)			Sta. Cruz I., [3m.], pk., 1500f	24 54'5	110 38'7	
	Acajutla, vill., $\frac{1}{2}$ n, l., lt. F..			San José I., $\frac{1}{2}$ 6 I., 2077f., }	24 24'2	110 20'5	
NORTH AMERICA.	San Jose de Guatemala, }	13 55'3	90 49'7	Espiritu Santo I., $\frac{1}{2}$ 4 I., }	24 10	110 20	
	Custom ho., lt. F	14 29	90 53'5	Lupona Pt.	24 8	109 47	
	Acuteuango Volcano, 12,890f.	15 8'5	92 7	La Paz	24 4	109 49	
	Mount Tacana, 14,000f.			Cerralbo I., $\frac{1}{2}$ 5 I., 2477f., }	23 3'5	109 41'7	
MEXICO. West Coast.	Tonalá Bar.	15 59	93 58	Montana rock.	22 53	109 53	
	St. Franc. de Tehuantepec, bar	16 13	94 45	Pt. Arenas	24 38'3	112 8'7	
	Salina Cruz, Morro, 244f.	16 9'8	95 12'5	C St. Lazaro, Mt. 1300f.	24 47	112 17'5	
	Port Guatulo, rky. islets.	15 44'4	96 8'2	San Juanico Pt.	26 2	112 17'5	
Mexico, W. Coast	Galera Point	15 57'6	97 41'5	Pt. Abreojos	26 42	113 33	
	Acapulco, \square , w, r, Fort St. }	16 50'8	99 55'7	I. Asuncion, 100f.	27 6	114 17'7	
	Diego, \square	17 16	101 4'5	Port St. Bartholomew, N hd.	27 39'8	114 52	
	Pt. Tequerpa	17 31'5	101 27	I. Cerros, 3955f., NS 8 I., }	28 1'3	115 11	
Mexico, W. Coast	Morro Petatlan, 640f.	17 38'0	101 3'3	Morro Redondo	28 18	115 36	
	Port Sihuatenejo, NW bight.	17 40'3	101 40	Is. San Benito, W one, 650f.	28 55	114 32	
	Istapa, or Isla Grande B.	17 55'5	102 12	Playa Maria B.	29 48	115 47'7	
	Mangrove bluff, 35f.	18 24	103 11	I. San Geronimo, [1 I.], 172f. @	30 22	115 59	
Mexico, W. Coast	Tejupan Papa, 5660f.	19 25	103 33	St. Quintin, \square , Sextant Pt.	30 57	116 19'5	
	Colima Volcano, 12,000f.	19 3'2	104 19'7	C. Colnett, SW pt., 400f.	31 51	117 37'2	
	Manzanilla B., $\frac{1}{2}$ w, village	19 11	104 43	Todos Santos Bay, Ensen-	32 23'9	117 14	
	Port Navidad, S head, 705f.	19 23'5	105 3	eda Pt., 370f.			
Mexico, W. Coast	Pt. Farallones, (rks. off)	20 24	105 42'5	Coronados rks., $\frac{1}{2}$ 5m., Sisl. }			
	C. Corrientes, flat, $\frac{1}{2}$, 506f.	20 45	105 51				
	Corventa rk., 25f.	21 43	106 41				
	Tres Marias Is., S Juanito, 150f.	21 26	104 58'5				
Mexico, W. Coast	Mt. St. Juan, 7550f., 5 l. inland	21 32'5	105 19				
	San Blas, w, r, Arsenal.	21 52	105 53'5				
	Isabel I., w, h., pk. 280f.	22 47'5	106 2				
	Chamatia R., Went. pt.	23 11'7	106 27'2				
Mexico, W. Coast	Mazatlan, w, Cust. ho.						
	Culiacan R., Altata Railway }	24 37'7	107 56				
	Station	25 26	109 24'2				
	I. St. Ignacio, [1m.], l. 465f.	26 16'3	109 17'2				
Mexico, W. Coast	Estero de Ajiabampo, bar ...	26 40	109 40'7				
	Pt. Rosa	27 21	110 38				
	Lobos I., [5 l.], 75f., SW pt.	27 55'4	110 55				
	Guaymas, \square , w, w, fort	27 50'5	110 54'7				
Mexico, W. Coast	C. Haro, lt. F, Fl. 346f.	28 1	111 5				
	Tetas de Cabra, 1633f.	27 58	111 24				
	I. St. Pedro Nalasco, 1071f.	28 51	112 36				
	Tiburón I., [9 l.], Willard }	30 16	112 52				
Mexico, W. Coast	Pt., 345f.						
	C. Tep ea						

MARITIME POSITIONS

(177) Places		Lat. N	Lon. W	(178) Places		Lat. N	Lon. W
Upper California	St. Barbara, lt. F 180f.	34° 23' 7"	120° 43' 2"	Queen Charlotte Sound	Texada, Marshall Pt.	49° 48' 0"	124° 40'
	Pt. Concepcion, lt. R. 135f.	34 26 8	120 28		Jervis Inlet, Hardy I., SW end ..	49 43 7	124 14 7
	Pt. Arguilla	34 35	120 39		Mystery Rock	49 54 8	124 46
	San Luis Obispo, Whaler I.	35 9 5	120 45		Hernando I. 8 pt.	49 58	124 56 2
	Pt. Pinos, T, lt. F 91f.	35 37 9	121 56		Mittenlatch I., 200f.	49 57	125 15
	Monterey, w, w, f, b, fort	36 36 4	121 53		Valdes I., C. Mudge	50 07	125 10 4
	Pt. Ano Nuevo	37 6 7	122 20		Thurlow I., Knox B.	50 24 2	125 39
	Farallones rks., [lm.], pk., } lt. Fl. 360f.	37 41 8	123 0		Port Neville, Robber's Nob.	50 31 1	126 43
	St. FRANCISCO, Fort Pt., lt. } F 124f., S side, entr.	37 48 5	122 28 7		Port Harvey, tide pole islet ..	50 34	126 16 7
	Mt. Bolbones, 3765f., 10 l. ind.	37 52 9	121 54 5		Wells pass, Tracey Hb, Starrk ..	50 51	126 53 2
	Pt. de los Reyes, lt. Fl. 296f.	37 59 6	123 1 2		Blunden Harb., Byrnes I.	50 54 4	127 19
	C. Bodega, (Rosa. Stor. w)	38 17 7	123 4 5		Slingsby Chan., Dalkeith Pt.	51 47 7	127 40
	Pt. Arena, lt. F 156f.	38 57 5	123 44 2		C. Caution	51 96	127 48
	C. Mendocino, lt. Fl. 423f.	40 26 3	124 24 5	Vancouver I., N.E. Coast	Port San Juan, pinnacle rk., } N side of Bay	48 33 5	124 27 5
Oregon	Humboldt B., lt. F 53f.	40 46	124 13 2		Sooke Inlet, Secretary I.	48 19 6	123 42 7
	Crescent City, Pt. St. George, } lt. Fl. 80f.	41 44 6	124 18		Race I., lt. Fl. 118f.	48 17 7	123 32 2
	C. Orford, lt. F 256f.	42 50 1	124 33 7		ESQUIMALT H., [w, r, b.], } DUNTEE HEAD	48 25 8	123 26 7
	C. Gregory, Empire City, } lt. F, Fl. 75f.	43 20 6	124 23 2		Victoria Harb., Laurel Pt.	48 25 4	123 23
	C. Perpetua	44 18	124 6 7		Nanaimo Hb., Dr. Benson's ho.	49 10 2	123 56 6
	Yaquina Hd., lt. F 61f.	44 40 6	124 4 7		Nanooec Harb., entrance rk.	49 15 7	124 8
	C. Look-out	45 20	124 0 7		Baynes Sd., Henry B., Beak Pt.	49 36 5	124 51 2
	Columbia R., Fort Astoria } — C. Disappointment, lt. F } 232f.	46 11	123 50 7		Seymour Narrows, Plumper } B., W pt.	50 10 0	125 22 5
	Shoalwater B., Toke Pt., lt. } F. Fl. 85f.	46 43	124 4 5		Albert B., Cormorant I., bluff ..	50 35 0	126 57 5
	Gray's Harb., [w, bar, Pt. } Brown	46 56 2	124 8		Beaver Harb., shell islet	50 42 6	127 25
	Pt. Grenville	47 18 3	124 16 5		P. Alexander, Goldias Chn., } islet in centre of the port ..	50 50 8	127 40
	Destruction I., rf. W 2 1/2 in.	47 40 5	124 28 5		Bull Hb., Hope I., N pt. Ind. Is.	50 54 8	127 56
	Flattery rks.	48 10 3	124 46	Vancouver I., S.W. Coast	C. Scott, 500f., sum. of cape.	50 46 7	128 26 7
	C. Flattery, Tatouch I., lt. } F 162f.	48 23 2	124 44 7		Triangle I., 680f., Scott Is., W pt.	50 51 9	129 6 5
Washington	Neeah B., Wyadda I., SW pt.	48 22 5	124 36 2		C. Russell, 8	50 41	128 23 5
	New Dungeness Pt., lt. F 100f.	48 11	123 6		C. Palmerston, 8	50 36 5	128 19
	Port Discovery	48 5 5	122 54 5		Quatsino Sd., ent., mt. 1275f., 8 ..	50 27 5	128 3 7
	Whidbey I., Admiralty Hd., } lt. F 119f.	48 9 4	122 39 5		— Observatory rk., N harb.	50 29 4	128 3 7
	Admiralty Inlet, Foul- } weather Bluff	47 56 3	122 37 2		— Observ. I., Koprino Harb.	50 30	127 52 2
	— Seattle Town	47 36	122 21		— Kitten I., Hecate Cove	50 32 4	127 36 2
	— Hood Canal, Union City	47 21	123 7		— Reef Pt.	50 21 3	128 0
	Puget Sound, Nisqually	47 7	122 40		Clerke reefs, W extreme	50 12 3	127 55
	— Olympia Town	47 3	122 55		C. Cook, or Woody Pt., } Solander I.	50 6 5	127 57 2
	Smith, or Blunt I., lt. Fl. 90f.	48 19	122 51 5		Nasparti Inlet, Head beach.	50 11 3	127 38
	Mount Baker, 10,694f.	48 49	121 46		Sullivan reefs	50 4 5	127 41
	Semiamoo Bay	49 0	122 45 5		Lookout I., 8, W extreme	50 00	127 26 5
	BRITISH COLUMBIA.				Ninety-eight-foot Island	49 47 7	127 21 7
	Roberts Pt., W side	49 0	123 5 5		Kynquod Sound, Shingle Pt., } ent. of Narrowgut Creek.	49 59 9	127 9 5
Strait of Georgia	Fraser River, lt. F 52f.	49 37	123 17 0		Thirty-foot Island	49 55 2	127 16
	— Garry Pt.	49 7 1	123 12 0	Vancouver I., S.W. Coast	Totchu Pt., 8	49 51 2	127 9 5
	— New Westm., Milit. Barr.	49 13	122 54 5		Esperanza Inlet, Obscr. rk., } Queen's Cove	49 52 7	127 0
	Burrard Inlet, Atkinson Pt., } lt. Rev. 119f.	49 20	123 16		Nuchatlits In., Port Lang- } ford, Colwood I.	49 47 3	126 57
	— City of Vancouver, Cana- } dian and Pacific Railway } Wharf	49 17	123 6		Ferrer Pt.	49 44 7	126 59 7
	Bowen I., Roger Curtis C.	49 20 3	123 26 2		Rajo Pt., rf. 3m.	49 37 5	126 50 7
	Howe Sound, Plumper Cove.	49 24 6	123 29 2		Nootka Sound, Friendly Cove ..	49 35 5	126 37 5
	Texada I., Pt. Upwood	49 29 7	124 8 7		Festevan Pt., 8 extr., rf. 2m.	40 22 1	126 32 5
					Hesquiat Harb., Boat Cove, } leading Mt. 2726f.	49 27 5	126 25 5
					Refuge Cove, vil. on W side.	49 20 8	126 16 7
					Flores I., summit 3000f.	49 18 2	126 9
					Sea Otter rk., 6f.	49 11 5	126 8 5
					Clayoquot Sound, Obs. I., } Hecate B.	49 15 4	125 56 2

TABLE 10

MARITIME POSITIONS

	(179) Places	Lat. N	Lon. W		(180) Places	Lat. N	Lon.
Hecate Strait	Gowlland rks., 10 to 15f.	49° 36'	125° 51' 7"	Alaska	C. Douglas, E pt.	58° 54'	West 153° 17'
	Barclay Sound, Obs. I., Al-berni Can., Stamp Harb. }	49 13 8	124 50 0		Barren Is., [5 l.], A, E pt.	58 58	151 50
	— Observ. I., Island Harb.	48 54 7	125 17		Pt. Banks 58 38	152 12	
	— Danger rk.	48 49 2	125 18 5		Kadiak I., # 27 l., E pt., C. Greville, or Tolstoy, rks. }	57 37	152 0
	— Cape Beale, lt. FL 166f. ...	48 47 4	125 13		— St. Paul Harb.	57 47 5	152 19 7
	Virgin rks., 50f.	51 17	128 13		— Trinity Is., SW pt.	56 23	154 40
	Pearl rks., 15f.	51 22	128 2		Chirikoff I., [3 l.], N pt.	55 56	155 34
	Dalkeith Pt.	51 4 7	127 40		Shumagin Is., Nagai I., Sanborn Harb.	55 8 1	159 58 2
	Safety Cove 51 31 7	127 56 5			Sannakh I., sum. 1850f.	54 25 3	162 44
	Goldstream Harb. 51 43 3	128 0 5			Unimak Pass, Ugamak I., S pt.	54 12	164 57
	Namu Harb. 51 51 7	127 52 5			Unalashka, # 23 l., Iliu-liuk Pt., # church } 53 50 2	166 30 7	
	Loughlin Harb. 52 8 6	128 10 2			Bogosloff I., [2 m.], # pk. 344f.	53 57 5	167 58
	Kynumpt Harb. 51 12 3	128 11 5			Umnak I., Vaevidoff, vol. 8000f.	53 15	168 29
	C. Swaine 52 18	128 32			Yunaska I., # 5 l., sum. 2864f.	52 36	170 47
	Carter Bay 52 49 7	128 24 5			Amukhta I., [2 l.], 3738f.	52 28	171 17
	Holmes Bay 53 16 4	129 5 2			Siguam I., # 5 m., 2098f. SW pt.	52 17 5	172 36
	Stewart Anchorage 53 52 5	130 5 2			Amlia I., EW 12 l., # o (rk) # 5 m., Suchikoff B.	52 2 2	173 22 5
	Alpha Bay 53 52	130 17 5			Atka I., # 20 l., vol., 4988f., Nagai B.	52 10 6	174 15
	C. Ibbetson 54 1	130 36			Sitchin I., [2 l.], A, vol., 5083f.	52 5	176 8
	Duncan Bay, Observatory Pt.	54 20 2	130 27 5	Aleutian Islands	Kanaga I., # 9 l., N pt.	51 56	177 5
Queen Charlotte Is.	P. Simpson Fort.	54 33 5	130 26 2		Tanaga I., EW 11 l., (w in Bay, W d.), NW pk. 7108f.	51 53	178 9
	Queen Charlotte's Is., # 55 l., S pt. C. St. James, (rks. # 1000f.)	51 55	131 2		Gareloi, or Burning I., or Volcano, [2 l.], 5334f.	51 47 5	178 52 5
	— C. Henry 52 55 5	132 21			Amatignak I., 1921f., West pt.	51 18	179 12
	— Skidegate I., Anchor Cov. 53 12 5	132 14 2			I. of Seven Mountains, Semisopochnoi, 3122f. [3 F]	51 56	East 179 37 5
	— Hippa I., [1 l.], village.	53 33	132 58		Anchitika I., # 11 l., Constantine Harbour 51 23 6	179 10 2	
	— Frederick I.	53 59	133 9		Kyska I., NS 8 l., Kyska Harbour 51 59 1	177 29 2	
	— Pt. North 54 15	132 56			Bouldyr I., [1 l.], (rks. E 6 l.), mid. 1145f.	52 34	175 45
	UNITED STATES.				Agattu, [4 l.], sum. 52 25	173 10	
	Alaska.				Semichli, 2 Is., # 2 l., Alaid I., 818f.	52 45	173 52
	Port Stewart, #, Sst. islet.	55 38 3	131 47		Atta, EW 15 l., 3084f., W pt., C. Wrangel 52 58	172 27	
	C. Chacon 54 41	132 1			— Chichogoff Harb.	52 55 7	173 11 5
	C. Mazon 54 40	132 41			Pribeloff Is., St. Paul I., EW 8 l., NE pt., (rf. E 2 l.)	57 15 2	West 170 7
	Forrester's I., NS 4 m., Spt. (rks.) 54 48	133 35			— St. George I., # 4 l., E pt.	56 36 7	169 27 5
	C. Addington 55 27	133 52			I. Amak, [1 l.], rk. NW-d.	55 27	163 3
	Port Protection, #, Pt. Baker 56 20 5	133 39			Port Moller, #, tongue, S pt.	55 56	160 35
	Coronation Is., [3 l.], S pt.	55 50	134 12		C. Strogonov, (I. off)	56 52	158 42
	Hazy Is.	55 54	134 32		Bristol B., C. Constantine, (bks. S-d. 4 l.)	58 25	158 44
	C. Ommanney 56 10	134 37			— Nagnek R., Suworoff vill.	58 40	157 3
	Sitka, #, Arsenal, lt. F 57 2 9	135 19 7			Hagenmeister I., # 6 l., S pt.	58 34	160 50
	C. Edgecumbe, 2855f.	57 0	135 49		C. Newenham 58 41	162 5	
	C. Cross, rks.	57 56	136 31		C. Avinoff, Anogognmute 59 39	163 45	
	C. Spencer, rks.	58 13	136 35		Nunivak I., EW 23 l., N pt., C. Etolin.	60 27	166 5
	C. Fairweather 58 51	137 50		Behring Sea, Coast of Alaska	I. St. Mathew, # 10 l., 1500f., SE pt., C. Upright.	60 18	172 4
Sitka Archipelago	Mt. Fairweather, 15,500f.	58 58	137 27		— Hall I., 1500f., [2 l.], N pt.	60 32	172 40
	Port Mulgrave, #, Pt. Turner 59 33 0	139 43 0					
	Pt. Manby 59 45	140 17					
	Mt. St. Elias, 19,500f.	60 20	140 58				
	C. Suckling 60 1	144 15					
	Kaya I., # 5 l., S pt., } 59 52	144 50					
	C. Hammond 60 21 2	146 50 2					
	Port Etches, #, Phipps Pt.	59 46	148 0				
	Montague I., S pt. C. Clear.	59 56	148 30				
	C. Puget 59 11	150 52					
	Pt. Gore 59 9	151 42					
	C. Elizabeth, E pt.	59 49	151 47				
	Anchor Pt., S hd.	60 3	153 0				
	Iliamna Pk., 12,066f., vol.	61 4	150 9				
	Pt. Campbell 61 4	150 9					
	Mt. St. Augustine, (Id. [3 l.]), } 59 22	153 30					
	sum.						

MARITIME POSITIONS

(181) Places		Lat. N	Lon. W	(182) Places		Lat. N	Lon. W
Belting's Strait	I. St. Lawrence, $\frac{1}{2}$ 30 l., NE pt.	63°15'	168°38'	Arctic Ocean	C. Prince of Wales (extreme W pt. of America)	65°33'	167°59'
	— West pt., C. Sansachno	63 26	171 50		Fairway rock	65 39	168 43
	C. Romantsof, 70f.	61 52	166 10		Diomedes Is., 2, N on a, or Ratmanoff I., [5m.], S pt.	65 47	169 4
	Mouth of Yukon R.	62 20	164 20		Kotzebue Sound, C. Espe- nberg, E pt.	66 33	163 28
	I. Stuart, [3 l.]	63 23	162 37		— Chamisso L., 231f., w E summit	66 13·2	161 46
	St. Michael, fort	63 26	161 24		C. Krusenstern, l, sandy	67 11	163 37
	C. Darby	64 17	162 45		Pt. Hope, l	68 20	166 45
	Sledge I., [2m.], Aziak	64 30	166 8		C. Lisbarne, 849f.	68 52	166 6
	Pt. Rodney	64 39	166 18		Icy Cape (shoals)	70 20	161 46
	King I., [1 l.], N pt., 700f. ...	65 0	168 1		Pt. Barrow, Noowook	71 23	156 22
	Port Clarence, $\frac{1}{2}$ w, Pt. ...	65 16·7	166 48				
	Spencer						

TABLE 11.

PLACES AT WHICH DOCKS, WET OR DRY, OR SLIPS, MAY BE FOUND,
REPAIRS MADE, COALS OBTAINED, &c.

London	Williamshaven	Barcelona	Dix Cove	Nagasaki	Savannah
Chatham	Hamburg	Marseille	Elmira	Hiogo	Pennacola
Sheerness	Kisineur	Port Clotat	C. Coast ?	Kobe	Mobile
Dund	Copenhagen	Toulon	Whidah	Osaka	New Orleans
Dover	Kiel	Port Mahon	Princes L.	Yedo	Nassau
Shorham ?	Stettin	Cagliari	Lagos	Hakodadi	Havana
Portsmouth	Dantsig	Caprera I.	Fernando Po		Santiago de Cuba
Southampton	Memel	Genoa	Congo	Labuan	Cienfuegos
Topsham	Riga	Spezia	Loanda	Manilla	Port Royal
Dartmouth	O-cashawan	Leghorn	Ascension ?	Macassar	Port au Prince
Devonport	Kronstadt	Civita Vecchia	St. Helena	Batavia	Porto Rico
Palmouth	Stockholm	Naples	Cape Town	Samarang	St. Thomas
Pennance	Ciurcrona	Messina	Simon's B.	Sourabaya	Sta. Cruz
Bristol	Malmö	Catania	Port Elizabeth	Amboina	Antigua
Newport	Gottenburg	Syracuse	East London	Ternate	Martinique
Cardiff	Christiansund	Marsala	Natal	Swan R.	St. Lucia ?
Swansea	Christiania	Palermo	Comoro Is. ?	King G.'s Sound	Barbados
Hartlepool	Christiansand	Taranto	Mozambique	Adelaide	Grenada
Pembroke	Bergen	Bari	Reunion	Port Phillip	Vera Cruz
Holyhead	Trondheim	Ancona	Mauritius	Port Western	Belize
Liverpool	Arolhaug	Venice	Mahé	Hobart	Porto Belle
Barrow	Dun. Yerkue	Trieste	Zanzibar	Port Jackson	Curaçao
Whitehaven	Calais	Foia	Aden	Newcastle	Caracas
Greenock	Dieppe	Plume	Muscat	Brisbane	Port Spain
Glasgow	Havre	Corfu	Basrah	Maryborough	Demerara
Stornoway	Trouville	Patras	Karachi	Townsville	Campeche
Lerwick ?	Honfleur	Salamis	Bombay	Nelson	Surinam
Inverness ?	Caen	Piræus	Colombo	Wellington	Cayenne ?
Aberdeen	Cherbourg	Syria	Trincomalee	Auckland	
Graugemouth	St. Pierre	Constantinople	Negapatam	Otago	Par ?
Dundee	St. Helier's	Rostoff	Pondicherry	Lyttelton	Marshall ?
Leith	Granville	Odeum	Madras	Napier	Permanbuce
Berwick	Morlaix ?	Nicolaiëff	Ca cutta	Wangarua	Bahia
Tynemouth	Brest	Servatopol	Chittagong		Rio Janeiro
Sunderland	L'Orient	Batoum	Akyab	Noouma	Rio Grande de
Hull	Port de Palais ?	Smyrna	Hangoon	Leruka	Sul
Great Grimsby	Nantes	Suda Bay	Moulmein	Tahiti	Monte Video
King's Lynn	Rochelle	Beirut	Mergui	Honolulu	Buenos Ayres
Ipswich	Rochefort	Alexandria	Port Blair	St. John's	Port Stanley,
Oork	Bordeaux	Port Said	Acheen	Montreal	Falkland Is. ?
Limerick	Lormont	Suez	Toronto	Quebec	
Sligo	Bayonne	Malta	Singapore	Pictou	Coronel
Londonerry	Bilbao	Tunis	Padang	Sydney	Talcahuano
Belfast	Rivades	Algiers	Bangkok	Halifax	Valparaiso
Larne	Ferrol	Palmas	Saigon	Garden	Coquimbo
Drogheda	Vigo	Teneriffe	Canton	St. John's,	Cañera
Dublin	Figueira	Flora	Whampoa	New Brk.	Antofagasta
Kingstown	Oporto	St. Michael's	Hong Kong	Portland	Iquique
Dundalk	Lisbon	St. Vincent	Swatou	Portsmouth	Callao
Carriockfergus	Huelva	Bermuda	Amoy	Boston	Payta
Wexford	Cádiz	Senegal	Fu-chau	New London	Gua; aquil
Ostend	Gibraltar	Goree	Shanghai	Philadelph	Panama
Antwerp	Valencia	Bathurst	Ningpo	Philadelphia	Acapulco
Rotterdam		Sierra Leone	Taku	Baltimore	Maxatlan
Flushing		Quetta	New-chang	Norfolk	Guaymas
Harlingen			Vladivostok	Charleston	St. Francisco
Ghent					Portland
Delft					Requimault
Amsterdam					

[illegible]

THE NAVIGABLE MERCATORIAL DISTANCES IN NAUTICAL MILES BETWEEN EUROPE AND THE PRINCIPAL PORTS OF THE WEST COAST OF AFRICA.

[illegible]

641

THE NAVIGABLE MERCATORIAL DISTANCES IN NAUTICAL MILES BETWEEN CAPE HORN AND THE PRINCIPAL PORTS OF THE WEST COAST OF SOUTH AMERICA.

IMPORTANT DISTANCES.

[illegible]

THE PRINCIPAL PORTS OF THE PACIFIC OCEAN TO EUROPE, VIA LAT. 62° S., AND STRAIT OF MAGELLAN.

* The passage made by O. Horn adds 100 m. to these distances

[illegible]

643

GIBRALTAR AND PORTS IN THE ATLANTIC AND WESTERN HEMISPHERE.

[illegible]

THE NAVIGABLE DISTANCES IN NAUTICAL MILES BETWEEN PORTS IN THE BRITISH ISLES AND NORTH SEA,
BAL TIC AND NORWEGIAN PORTS.

[illegible]

BY NAIGER WILHELM CANAL

[illegible]

TIME SIGNALS, 1902*

It will be noticed that many countries have now adopted a uniform time system. Great Britain, Belgium, Netherlands, Spain, and Portugal have adopted Greenwich mean time as a standard.

In Ireland the mean time of the Observatory at Dublin is the standard, 25^m 22^s slow of G.M.T. Austria-Hungary, Denmark, Germany, Italy, Norway and Sweden, and the British Colony of Malta have adopted the Meridian of 15° E. from Greenwich as a standard, or 1 hour fast of G.M.T. This is known as Mid European time. France and Algeria use the Meridian of Paris, 9^m 21^s fast of G.M.T.

Cape Colony has adopted the Meridian of 22½° E. as a standard, or 1½ hours fast of G.M.T. This is known as Cape Colony mean time. Egypt and Natal have adopted Meridian of 30° E., or 2^h fast of G.M.T.

Japan has adopted as a standard the Meridian of 135° East from Greenwich, or 9 hours fast of G.M.T. This is known as Japan mean time. Straits Settlements, Mer. of Ft. Fullerton, Singapore, 6^h 55^m 25^s fast of G.M.T.

In the Colony of West Australia and Philippine Islands, the standard time of the Meridian of 120° E. of Greenwich, or 8 hours fast of G.M.T., has been established.

In the Colony of South Australia the standard time of the Meridian of 122° 30' E. of Greenwich, or 9 hours 30 min. fast of G.M.T., has been established.

In the Colonies of Queensland, New South Wales, Victoria, and Tasmania the standard time of the Meridian of 150° E., or 10 hours fast of G.M.T. has been established.

New Zealand has adopted as a standard the Meridian of 172½° E. from Greenwich, or 11½ hours fast of G.M.T. This is known as New Zealand mean time.

In the United States of America, at the Atlantic ports and Cuba, the standard time of the Meridian of 75° W. of Greenwich, or 5 hours slow of G.M.T. has been established. At Pacific ports and British Columbia the standard time is that of the Meridian of 120° W., or 8 hours slow of G.M.T.*

Lat.	Long.	Place	Signal adopted	Situation of Time Signal	Time of Signal being made		Greenwich Time of Preparatory Signal
					Greenwich Mean Time	Local Mean Time	
51 28 39 N.	0 0 0	Greenwich	Ball	Royal Observatory	1 00 00	1 00 00	12 55 00
51 26 45 N.	0 44 45 E.	Sheerness	Ball	Garrison Flagstaff	1 00 00	1 2 59	12 57 30
51 13 17 N.	1 24 22 E.	Deal	Ball	Telegraph Tower	1 00 00	1 05 37	12 55 00
51 7 15 N.	1 19 40 E.	Dover	Gun	Drop Battery	0 00 00	0 05 19	12 57 00
50 48 0 N.	1 6 18 W.	Portsmouth	Ball	Duck Yd. Semaphore	1 00 00	0 55 35	12 55 00
50 8 45 N.	5 2 45 W.	Falmouth	Ball	Pendennis Castle	1 00 00	0 39 49	—
50 53 39 N.	1 24 5 W.	Southampton	Ball	South Castle	1 00 00	0 54 24	12 55 00
50 22 0 N.	4 10 20 W.	Devonport	Ball	Mount Wise	1 00 00	0 43 19	12 55 00
51 36 55 N.	3 55 35 W.	Swansea	Gun	On old Eastern Pier	1 00 00	0 43 19	—
53 24 4 N.	3 0 36 W.	Liverpool	Gun	Birkenhead, Mersey Dock	1 00 00	0 44 18	—
56 27 56 N.	2 58 45 W.	Dundee	Gun	—	1 00 00	0 48 05	—
55 57 23 N.	3 10 54 W.	Edinburgh	Ball	Nelson's Monument	1 00 00	0 47 16	12 55 00
—	—	—	—	—	—	—	12 57 00
55 0 32 N.	1 27 28 W.	North Shields	Gun	Edinburgh Castle	1 00 00	0 47 16	—
—	—	—	Gun	Near Albert Edward Dock	1 00 00	0 54 10	—
51 53 53 N.	8 27 17 W.	Cork	Gun	Victoria Quay	1 00 00	0 26 11	—
51 51 9 N.	8 16 37 W.	Queenstown	Gun	Near Military Hosp.	1 00 00	0 26 53	—
53 20 46 N.	6 15 30 W.	Dublin	Ball	Docks Board Building	1 00 00	0 34 58	—
24 49 11 N.	66 58 00 E.	Karachi	Ball	Merewether Pier	20 32 8	1 00 00	20 27 8
18 55 51 N.	72 50 33 E.	Bombay†	Ball	Bombay Castle	20 08 44	1 00 00	20 03 44
18 57 13 N.	72 50 46 E.	"	Ball	Clock Tower, Docks	15 00 00	7 51 16	14 55 00
6 50 34 N.	79 50 34 E.	Colombo	Sema.	Master Attendant's	22 54 1	4 15 00†	22 49 1
16 46 0 N.	96 10 0 E.	Rangoon	Ball	Sailors' Home	17 35 20	0 00 00	17 30 20
13 5 47 N.	80 17 37 E.	Madras.	Sema.	Master Attendant's Office	19 39 00	1 00 00	—
22 33 25 N.	88 20 12 E.	Calcutta	Ball	Fort William	19 06 39	1 00 00	19 01 39
—	—	—	Ball	Port Commissioner's	19 06 39	1 00 00	19 01 39
22 17 44 N.	114 10 8 E.	Hongkong	Ball	Kau'ung Tower	17 23 18	1 00 00	17 18 18
1 17 33 N.	103 50 53 E.	Singapore	Ball	Fl. Comm'g Flagstaff	18 4 35	1 00 00	18 00 00
1 15 45 N.	103 50 00 E.	"	Ball	Pulo Bruni	18 4 35	1 00 00	18 00 00
6 5 48 S.	106 53 07 E.	Batavia.	Dises	Tanjung Priok Basin	16 52 28	0 00 00	16 47 28
—	—	—	Dises	—	18 00 00	1 07 32	17 55 00
7 12 10 S.	112 43 40 E.	Sourabaya	Dises	Kalimas River	16 29 05	0 00 00	16 24 05
15 55 0 S.	5 42 30 W.	St. Helena	Ball	Ladder Hill Flagstaff	1 00 00	0 37 10	12 55 00
—	—	—	Ball	Time Office	1 00 00	0 37 10	12 55 00
5 31 48 N.	0 11 30 W.	Accra	Flag	Telegraph Office	11 00 46	11 00 00	—
8 48 45 S.	13 13 20 E.	Paul de Loanda	Ball	Observatory	0 7 7	1 00 00	0 2 7

* For more detailed and later information on Time Signals see Admiralty List of Time Signals, sold by J. D. Potter, Agent for Admiralty Charts, 145 Minories, E.

† Clock on N.E. Bastion shows Bombay mean time.

‡ Madras mean time, also at 8^h 15^m a.m.

TABLE 13

645

TIME SIGNALS, 1903

Lat.	Long.	Place	Signal adopted	Situation of Time Signal	Time of Signal being made		Greenwich Time of Preparatory Signal
					Greenwich Mean Time	Local Mean Time	
33 54 24 S.	18 25 15 E.	Table Bay *	Ball	At Alfred Docks	h m s	h m s	h m s
			Gun	On Imhoff Battery	0 00 00	1 30 00	—
34 11 35 S.	18 25 58 E.	Simons Bay	Disc	Telegraph Office	0 00 00	1 30 00	23 55 00
33 57 43 S.	25 37 19 E.	Port Elizabeth	Ball	At the Lighthouse	0 00 00	1 30 00	—
33 36 10 S.	26 54 5 E.	Port Alfred	Ball	—	0 00 00	1 30 00	—
33 1 50 S.	27 34 55 E.	East London	Ball	Signal Hill	0 00 00	1 30 00	—
29 52 30 S.	31 3 0 E.	Natal	Ball	North Entrance Point	22 55 59	0 25 59	—
20 10 5 S.	57 29 0 E.	Mauritius	Ball	Signal Mt. Pt. Louis	21 09 47	1 00 00	21 04 47
32 3 12 S.	115 44 15 E.	Freemantle	Ball	Arthur Head	17 0 0	0 42 57	16 57 00
34 51 6 S.	138 28 50 E.	Adelaide†	Ball	At the Semaphore	15 30 00	0 43 55	15 25 00
37 52 7 S.	144 54 47 E.	Port Phillip.	Ball	Gellibrand Point	15 00 00	0 39 39	14 55 00
38 9 00 S.	144 21 00 E.	—	Ball	Telegraph, Geelong	15 00 00	0 37 24	14 55 00
38 16 27 S.	144 39 45 E.	—	Flag	Queenscliff Signals	15 00 00	0 38 39	—
33 51 41 S.	151 12 23 E.	Sydney	Ball	Observatory	15 00 00	1 04 49	14 53 00
32 55 43 S.	151 47 28 E.	Newcastle	Ball	Custom House	15 00 00	1 07 10	14 53 00
27 28 3 S.	153 1 31 E.	Brisbane	Ball	Signal Tower	15 00 00	1 12 06	14 55 00
42 53 22 S.	147 20 28 E.	Hobart.	Ball	Fort Mulgrave	15 00 00	0 49 20	14 50 00
			Gun	Queen's Battery	—	—	—
43 35 42 S.	172 41 50 E.	Lyttelton	Ball	Observatory	13 30 00	1 02 59	13 25 00
41 16 50 S.	174 46 55 E.	Wellington	Ball	Railway Wharf†	12 30 00	0 09 08	—
45 49 0 S.	170 39 0 E.	Otago	Ball	Signal Staff, Port	12 30 00	11 52 36	Once a week
36 50 44 S.	174 45 52 E.	Auckland	Ball	Post Office Flagstaff	12 30 00	0 09 03	12 25 00
47 34 10 N.	52 40 27 W.	St. John's	Gun	Signal Hill	3 30 43?	0 00 00	—
45 15 42 N.	66 3 45 W.	St. John, N.B.	Ball	New Custom House	5 00 00	1 00 00	4 45 00
46 48 23 N.	71 12 17 W.	Quebec.	Ball	At Citadel	6 00 00	1 15 11	5 55 00
45 31 0 N.	73 33 15 W.	Montreal	Ball	Harbour Office	5 00 00	0 5 47	4 55 00
32 19 22 N.	64 49 35 W.	Bermuda‡	Ball	Dockyard Flagstaff	4 19 18	0 00 00	4 14 18
23 08 30 N.	82 20 50 W.	Havana	Ball	Naval Office	5 00 00	11 30 36	4 50 00
14 00 53 N.	81 00 00 W.	St. Lucia	Ball	Harbour Master's Office, Castries	4 04 00	0 00 00	3 59 00
6 48 48 N.	58 9 52 W.	Demerara	Ball	General Post Office	3 52 39	0 00 00	3 47 46
10 39 0 N.	61 30 38 W.	Trinidad	Ball	Observatory Tower	4 06 02?	0 00 00	—
5 49 30 N.	55 8 48 W.	Paramaribo	Disc	Guardship	3 40 35	0 00 00	3 35 35
12 6 45 N.	68 56 44 W.	Curacao	Flag	Guardship	4 35 47	0 00 00	4 30 47
22 54 24 S.	43 10 21 W.	Rio de Janeiro	Drum	Mount Castello	2 52 41	0 00 00	2 47 41
34 52 33 S.	57 54 43 W.	Rio de la Plata	Ball	Dock Engine Ho.	2 51 39?	23 00 00	2 47 39
34 35 50 S.	58 22 15 W.	Buenos Aires	Ball	Hyd. Office	5 16 48	1 23 19	5 14 48
51 13 15 N.	4 24 15 E.	Antwerp	Discs	Hanseatic House	1 00 00	1 17 37	12 55 00
51 26 33 N.	3 35 48 E.	Flushing	Discs	Stone Tower of sluice	23 45 37	0 00 00	23 40 37
51 49 19 N.	4 7 40 E.	Hellevoetsluis	Discs	Marine Establishment	23 43 29	0 00 00	23 38 29
52 22 40 N.	4 54 45 E.	Amsterdam	Discs	Commercial Quay	23 40 21	0 00 00	23 35 21
51 54 39 N.	4 29 47 E.	Rotterdam	Discs	Gate Building	23 42 01	0 00 00	13 37 01
52 57 50 N.	4 46 36 E.	Willemsoord	Discs	Marine Office	23 40 54	0 00 00	23 35 54
53 31 54 N.	8 8 48 E.	Wilhelmshaven‡	Ball	Observatory	23 00 00	11 32 35	20 50 00
			Ball	—	0 00 00	0 32 35	23 57 00
53 32 51 N.	8 34 7 E.	Bremerhaven	Ball	S.W. of Lighthouse	23 00 00	11 34 16	22 50 16
			Ball	—	0 00 00	0 34 16	23 57 00
53 52 24 N.	8 42 30 E.	Cuxhaven	Ball	E. of Lighthouse	23 00 00	11 34 59	22 50 00
			Ball	—	0 00 00	0 34 59	23 57 00
53 32 30 N.	9 58 57 E.	Hamburg	Ball	On the Kaiser Quay	0 00 00	0 39 56	23 50 00
54 19 18 N.	10 9 40 E.	Kiel	Ball	Imperial Wharf	23 00 00	11 40 39	22 50 00
			Gun	Guardship	23 00 00	11 40 39	—
53 54 36 N.	14 15 58 E.	Swinemunde	Ball	S.W. of Lighthouse	22 00 00	10 57 4	21 50 00
			Ball	—	3 00 00	3 57 4	2 50 00
54 24 18 N.	18 40 10 E.	Neufahrwasser	Ball	Lighthouse	23 00 00	1 14 41	22 50 00
56 2 4 N.	19 37 24 E.	Elsinore	Ball	Quarantine House	0 00 00	0 50 30	23 55 00
57 42 34 N.	11 58 0 E.	Gothenburg	Ball	Navigation School	0 00 00	0 47 52	23 55 00
55 40 42 N.	12 35 7 E.	Copenhagen	Ball	Nikolai Tower	0 00 00	0 50 19	23 55 00
55 37 0 N.	13 0 15 E.	Malmö	Ball	School of Navigation	0 00 00	0 52 02	23 55 00
56 09 28 N.	15 35 36 E.	Carlskrona	Ball	Dockyard Tower	0 00 00	1 1 23	23 54 00
59 19 10 N.	18 4 44 E.	Stockholm	Ball	School of Navigation	0 00 00	1 12 19	23 55 00

* Cape Colony mean time.

† Balls dropped at 2nd 00th 00th, standard times, of the Australian Colonies and New Zealand.

‡ Once a week. § On Saturdays only.

¶ At Demerara, on Wednesday and Saturday only.

‡ Balls dropped at 2nd 00th 00th, Mid-European time, throughout Germany and Denmark.

TIME SIGNALS, 1902

Lat.	Long.	Place	Signal adopted	Situation of Time Signal	Time of Signal being made		Greenwich Time of Preparation, Signal
					Greenwich Mean Time	Local Mean Time	
56 56 52 N.	24 05 30 E.	Riga . . .	Ball	Sailors' Home . .	23 23 32	0 59 54	23 18 32
59 59 24 N.	29 45 54 E.	Kronstadt . .	Ball	Marine Telegraph .	22 00 56	0 00 00	21 52 56
59 59 31 N.	30 18 22 E.	St. Petersburg .	Gun	Fort Petri-Paul . .	21 58 41	0 00 00	—
60 9 49 N.	24 57 7 E.	Helsingfors . .	Ball	Observatory . . .	22 20 11	0 00 00	22 16 11
60 26 57 N.	22 17 43 E.	Abo . . .	Ball	Navigating School .	22 30 51	0 00 00	22 24 51
65 1 19 N.	25 30 30 E.	Uleaborg . . .	Ball	Navigating School .	22 17 58	0 00 00	22 12 58
63 25 40 N.	10 22 4 E.	Trondhjem* . .	Ball	Observatory . . .	23 00 00	23 41 28	22 45 00
60 23 53 N.	5 18 35 E.	Bergen* . . .	Ball	Observatory . . .	23 00 00	23 21 13	22 45 00
59 45 44 N.	10 43 33 E.	Christiania* . .	Drum	Observatory . . .	23 00 00	23 42 54	22 55 00
49 38 42 N.	1 37 34 W.	Charbourg . . .	Di c	Marine Observatory .	21 50 39	10 00 00†	21 45 39
48 22 46 N.	4 29 48 W.	Brest . . .	Flag	Observatory . . .	21 50 39	10 00 00†	21 45 39
47 44 45 N.	3 21 15 W.	L'Orient . . .	Ball	Harbour Tower . .	21 50 39	10 00 00†	21 45 39
45 59 10 N.	1 5 50 W.	F u a s . . .	Ball on	Tower . . .	21 50 39	10 00 00†	21 45 39
45 56 10 N.	0 57 35 W.	Rochefort . . .	Ball on	St. Louis Tower . .	21 50 39	10 00 00†	21 45 39
38 42 18 N.	9 8 24 W.	Lisb n . . .	Ball	Naval School . . .	1 36 45	1 00 00	1 31 45
36 27 41 N.	6 12 24 W.	Cadix . . .	Ball	Observatory . . .	1 24 50	1 00 00	1 14 50
43 7 22 N.	5 55 27 E.	Toulon . . .	Ball	Naval Observatory .	21 50 39	10 00 00†	21 40 39
36 47 0 N.	3 3 15 E.	Algier . . .	Cock	Town Hall . . .	—	Cock shows Paris Mean T. r.	—
44 25 10 N.	8 55 21 E.	Genoa† . . .	Gun	Fort Castelletto . .	23 00 00	23 35 41	22 55 00
44 6 55 N.	9 49 33 E.	Spezia . . .	Gun	Laguna Mo'e . . .	23 00 00	23 39 18	—
40 28 20 N.	17 14 10 E.	Taranto . . .	Ball	S. Angelo Castle . .	23 00 00	0 8 57	22 55 00
40 28 8 N.	13 50 45 E.	Pola . . .	Ball	Harbour Castle . .	23 00 00	23 55 23	22 55 00
45 38 56 N.	13 45 30 E.	Trieste . . .	Ball	Lighthouse . . .	23 00 00	23 55 00	22 55 00
45 19 36 N.	14 25 44 E.	Fiume . . .	Ball	Staff, Mole end . .	23 00 00	23 57 43	22 55 00
44 31 49 N.	14 28 6 E.	Lussin Piccolo .	Disco	S.W. Quay . . .	23 00 00	23 57 52	—
35 53 50 N.	14 30 55 E.	Malta . . .	Ball	Palace Valletta . .	23 00 00	23 58 4	22 55 00
40 30 5 N.	14 15 30 E.	Naples . . .	Ball	Custom House . . .	23 00 00	23 58 4	22 55 00
31 11 39 N.	29 53 15 E.	Alexandria† . .	Ball	Vincenzo's Mole . .	23 00 00	23 57 2	22 55 00
31 15 45 N.	32 18 45 E.	Port Said† . .	Ball	Fort Napoleon . . .	22 00 00	23 59 33	21 55 00
46 58 21 N.	31 58 28 E.	Nicosia . . .	Ball	High Light Ho. . .	22 00 00	0 00 00	21 55 00
		(Black Sea)		Observatory . . .	21 52 06	0 00 00	21 47 6
46 29 0 N.	30 45 0 E.	Odessa . . .	Ball	Russian S.N.C. Office	21 57 0	0 00 00	21 52 00
41 31 30 N.	70 40 20 W.	Woods Hole† .	Ball	Water Tower . . .	5 00 00	0 17 19	—
41 29 36 N.	71 19 39 W.	Newport . . .	Ball	Torpedo Station . .	5 00 00	0 14 41	—
40 43 0 N.	74 0 25 W.	New York . . .	Ball	Union Telegraph Office	5 00 00	0 03 58	4 55 00
39 56 45 N.	75 9 10 W.	Philadelphia . .	Ball	Maritime Exchange .	5 00 00	23 59 23	4 50 00
39 17 51 N.	76 36 57 W.	Baltimore . . .	Ball	Baltimore Railway . .	5 00 00	23 53 32	—
38 53 39 N.	77 3 8 W.	Washington . .	Ball	Naval Observatory . .	5 00 00	23 51 47	4 50 00
37 0 0 N.	76 18 25 W.	Hartington Roads	Ball	Hydra Hotel . . .	5 00 00	23 54 46	—
32 4 50 N.	81 5 10 W.	Savannah . . .	Ball	Custom House . . .	5 00 00	23 35 39	—
29 57 8 N.	90 3 50 W.	New Orleans . .	Ball	Sugar House . . .	5 00 00	22 59 43	4 55 00
29 18 0 N.	94 47 30 W.	Galveston . . .	Ball	Levy Building . . .	5 00 00	23 0 0	4 55 00
37 47 40 N.	122 23 35 W.	San Francisco . .	Ball	Tower of Ferry Ho.*	8 00 00	23 50 23	7 55 00
38 5 53 N.	122 16 16 W.	Mare Island . .	Ball	The Observatory** .	8 00 00	23 50 55	7 55 00
49 17 30 N.	123 7 0 W.	Vancouver . . .	Gun	Brockton Point . .	17 00 00	9 00 00	—
33 1 50 N.	71 38 30 W.	Valparaiso . . .	Ball	Naval School . . .	4 46 34	0 00 00	4 41 34
21 18 13 N.	157 51 47 W.	Honolulu . . .	Whistle	Steam Mills . . .	12 00 00	1 28 33	—
14 36 0 N.	120 58 0 E.	Manila . . .	Ball	Meteorological Office	16 00 00	0 3 52	15 55 00
20 51 56 N.	106 39 54 E.	Haifong . . .	Ball	Observatory . . .	13 53 20	21 00 00	13 43 20
23 31 43 N.	116 40 30 E.	Suway . . .	Ball	Harbour Office . . .	16 13 05	0 00 00	—
24 27 25 N.	118 3 33 E.	Amoy . . .	Gun	Kulangshan . . .	16 07 44	0 00 00	16 02 44
31 14 7 N.	121 29 10 E.	Shanghai . . .	Ball	Semaphore . . .	15 54 03	0 00 00	15 49 3
37 33 10 N.	121 25 20 E.	Chi u . . .	Ball	Mast near Tower Hill	15 54 20	1 00 00*	—
34 1 0 N.	135 11 0 E.	Kobe . . .	Ball	On the Bund . . .	15 00 00	0 00 00	—
41 46 35 W.	140 43 50 E.	Hakodate . . .	Flag	Obs. Fl. staff . . .	15 00 00	0 22 55	14 55 00
43 7 0 N.	131 52 44 E.	Vladivostok . .	Ball & Gun	Harbour Office . . .	15 12 29	0 00 00	15 07 20

* On Wednesdays and Saturdays.

† Paris mean time.

‡ Guns fired and balls dropped at 3^h 00^m 00^s Mid-European time, throughout Norway, Austria, and Italy.

§ Throughout Egypt, the official time kept is standard time of the meridian of 30° E.

|| Ball at Port Said dropped also at 2^h a.m. and 4^h p.m., standard time.¶ All time balls on the Atlantic and Gulf of Mexico coasts of the United States are dropped at noon, mean time of the 75th meridian West from Greenwich—equivalent to 3^h 00^m 00^s p.m. Greenwich mean time.

** Balls dropped at noon, mean time of 120th meridian West from Greenwich.

N.B.—When the report of the gun is used allow for time of passage of sound. See p. 126.

TABLE 14.

EPOCHS												
Years									Months			
Year	Epoch	Year	Epoch	Year	Epoch	Year	Epoch	Year	Month	Epoch	Month	Epoch
	d h		d h		d h		d h			d h		d h
1891	20 9	1897	27 6	1903	3 11	1909	9 4		Jan.	0 0	July	3 20
1892L	1 10	1898	8 8	1904L	13 2	1910	19 19		Feb.	1 11	Aug.	5 7
1893	13 5	1899	19 0	1905	24 17	1911	0 22		March	29 11	Sept.	6 18
1894	24 5	1900	0 2	1906	5 19	1912L	11 13		April	1 10	Oct.	7 5
1895	5 0	1901	10 17	1907	16 11	1913	23 4		May	1 21	Nov.	8 17
1896L	15 15	1902	21 8	1908L	27 2	1914	4 7		June	3 8	Dec.	9 4

TABLE 15.

SEMIMENSTRUAL INEQUALITY OF THE TIME OF HIGH WATER, For London, Liverpool, Pembroke, Ramsgate, Sheerness, Portsmouth, Plymouth, and Brest.									
Moon's Transit	Sem. Ineq.	Moon's Transit	Sem. Ineq.	Moon's Transit	Sem. Ineq.	Moon's Transit	Sem. Ineq.	Moon's Transit	Sem. Ineq.
sub.		sub.		sub.		sub.		sub.	
0 ^h 0 ^m	0 ^h 0 ^m	2 ^h 30 ^m	0 ^h 36 ^m	5 ^h 0 ^m	1 ^h 3 ^m	7 ^h 30 ^m	0 ^h 30 ^m	10 ^h 0 ^m	0 ^h 16 ^m
10	0 2	40	0 38	10	1 4	40	0 25	10	0 16
20	0 4	50	0 41	20	1 5	50	0 20	20	0 15
30	0 6	3 0	0 43	30	1 5	8 0	0 15	30	0 15
40	0 8	10	0 45	40	1 5	10	0 10	40	0 14
50	0 11	20	0 47	50	1 4	20	0 5	50	0 12
1 0	0 13	30	0 49	6 0	1 3	30	0 1	11 0	0 11
							add		
10	0 15	40	0 51	10	1 1	40	0 3	10	0 10
20	0 18	50	0 53	20	0 59	50	0 6	20	0 8
30	0 20	4 0	0 55	30	0 56	9 0	0 9	30	0 6
40	0 23	10	0 57	40	0 52	10	0 12	40	0 4
50	0 25	20	0 59	50	0 48	20	0 14	50	0 2
2 0	0 28	30	1 0	7 0	0 44	30	0 15	12 0	0 0
10	0 30	40	1 1	10	0 39	40	0 15		
20	0 33	50	1 2	20	0 35	50	0 16		

TABLE 16.

APPROXIMATE RISE AND FALL OF THE TIDE AT ANY TIME FROM HIGH OR LOW WATER																			
Range of Tide in feet	0 ^h			1 ^h			2 ^h			3 ^h			4 ^h			5 ^h			Range of Tide in feet
	m	m	m	m	m	m	m	m	m	m	m	m	m	m	m	m	m	m	
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	0	0	0	0	1	0	0	0	0	1	1	1	1	1	1	1	1	1	2
4	0	0	0	0	1	0	0	1	1	2	2	2	3	3	3	3	3	3	4
6	0	0	0	0	2	0	0	1	1	2	2	3	4	4	5	5	5	6	6
8	0	0	1	0	2	0	0	1	1	2	2	3	4	4	5	5	6	7	8
10	0	0	1	0	3	0	0	1	1	2	2	3	4	4	5	5	6	7	10
12	0	0	1	0	4	0	0	1	1	2	2	3	4	4	5	5	6	7	12
14	0	0	1	0	4	0	0	1	1	2	2	3	4	4	5	5	6	7	14
16	0	0	1	0	5	0	0	1	1	2	2	3	4	4	5	5	6	7	16
18	0	0	1	0	5	0	0	1	1	2	2	3	4	4	5	5	6	7	18
20	0	0	2	0	6	0	0	1	1	2	2	3	4	4	5	5	6	7	20
22	0	0	2	0	7	0	0	1	1	2	2	3	4	4	5	5	6	7	22
24	0	0	2	0	7	0	0	1	1	2	2	3	4	4	5	5	6	7	24
26	0	0	2	0	8	0	0	1	1	2	2	3	4	4	5	5	6	7	26
28	0	0	2	0	8	0	0	1	1	2	2	3	4	4	5	5	6	7	28
30	0	0	2	0	9	0	0	1	1	2	2	3	4	4	5	5	6	7	30
32	0	0	2	0	10	0	0	1	1	2	2	3	4	4	5	5	6	7	32
34	0	0	3	0	10	0	0	1	1	2	2	3	4	4	5	5	6	7	34
36	0	0	3	0	11	0	0	1	1	2	2	3	4	4	5	5	6	7	36
38	0	0	3	0	11	0	0	1	1	2	2	3	4	4	5	5	6	7	38
40	0	0	3	0	12	0	0	1	1	2	2	3	4	4	5	5	6	7	40
42	0	0	3	0	13	0	0	1	1	2	2	3	4	4	5	5	6	7	42
44	0	0	3	0	13	0	0	1	1	2	2	3	4	4	5	5	6	7	44
46	0	0	3	0	14	0	0	1	1	2	2	3	4	4	5	5	6	7	46
48	0	0	4	0	14	0	0	1	1	2	2	3	4	4	5	5	6	7	48
50	0	0	4	0	15	0	0	1	1	2	2	3	4	4	5	5	6	7	50

TABLE 17.

ARC.					
°	H.M.	'	M.S	"	S.
0	0 0	0	0 0	0	0'00
1	0 0	4	1 0	4	0'07
2	0 0	8	2 0	8	0'13
3	0 12	3	0 12	3	0'20
4	0 16	4	0 16	4	0'27
5	0 20	5	0 20	5	0'33
6	0 24	6	0 24	6	0'40
7	0 28	7	0 28	7	0'47
8	0 32	8	0 32	8	0'53
9	0 36	9	0 36	9	0'60
10	0 40	10	0 40	10	0'67
11	0 44	11	0 44	11	0'73
12	0 48	12	0 48	12	0'80
13	0 52	13	0 52	13	0'87
14	0 56	14	0 56	14	0'93
15	1 0	15	1 0	15	1'00
16	1 4	16	1 4	16	1'07
17	1 8	17	1 8	17	1'13
18	1 12	18	1 12	18	1'20
19	1 16	19	1 16	19	1'27
20	1 20	20	1 20	20	1'33
30	2 0	21	1 24	21	1'40
40	2 40	22	1 28	22	1'47
50	3 20	23	1 32	23	1'53
60	4 0	24	1 36	24	1'60
70	4 40	25	1 40	25	1'67
80	5 20	26	1 44	26	1'73
90	6 0	27	1 48	27	1'80
100	6 40	28	1 52	28	1'87
110	7 20	29	1 56	29	1'93
120	8 0	30	2 0	30	2'00
130	8 40	31	2 4	31	2'07
140	9 20	32	2 8	32	2'13
150	10 0	33	2 12	33	2'20
160	10 40	34	2 16	34	2'27
170	11 20	35	2 20	35	2'33
180	12 0	36	2 24	36	2'40
		37	2 28	37	2'47
		38	2 32	38	2'53
		39	2 36	39	2'60
		40	2 40	40	2'67
		41	2 44	41	2'73
		42	2 48	42	2'80
		43	2 52	43	2'87
		44	2 56	44	2'93
		45	3 0	45	3'00
		46	3 4	46	3'07
		47	3 8	47	3'13
		48	3 12	48	3'20
		49	3 16	49	3'27
		50	3 20	50	3'33
		51	3 24	51	3'40
		52	3 28	52	3'47
		53	3 32	53	3'53
		54	3 36	54	3'60
		55	3 40	55	3'67
		56	3 44	56	3'73
		57	3 48	57	3'80
		58	3 52	58	3'87
		59	3 56	59	3'93

TABLE 18

647

TIME.									
H.	°	M.	'	S.	"	10"	"		
0	0	0	0 0	0	0 0	0'0	0'0		
1	15	1	0 15	1	0 15	0'1	1'5		
2	30	2	0 30	2	0 30	0'2	3'0		
3	45	3	0 45	3	0 45	0'3	4'5		
4	60	4	1 0	4	1 0	0'4	6'0		
5	75	5	1 15	5	1 15	0'5	7'5		
6	90	6	1 30	6	1 30	0'6	9'0		
7	105	7	1 45	7	1 45	0'7	10'5		
8	120	8	2 0	8	2 0	0'8	12'0		
9	135	9	2 15	9	2 15	0'9	13'5		
10	150	10	2 30	10	2 30	1'0	15'0		
11	165	11	2 45	11	2 45				
12	180	12	3 0	12	3 0				
13	195	13	3 15	13	3 15				
14	210	14	3 30	14	3 30				
15	225	15	3 45	15	3 45				
16	240	16	4 0	16	4 0				
17	255	17	4 15	17	4 15				
18	270	18	4 30	18	4 30				
19	285	19	4 45	19	4 45				
20	300	20	5 0	20	5 0				
21	315	21	5 15	21	5 15				
22	330	22	5 30	22	5 30				
23	345	23	5 45	23	5 45				
24	360	24	6 0	24	6 0				
		25	6 15	25	6 15				
		26	6 30	26	6 30				
		27	6 45	27	6 45				
		28	7 0	28	7 0				
		29	7 15	29	7 15				
		30	7 30	30	7 30				
		31	7 45	31	7 45				
		32	8 0	32	8 0				
		33	8 15	33	8 15				
		34	8 30	34	8 30				
		35	8 45	35	8 45				
		36	9 0	36	9 0				
		37	9 15	37	9 15				
		38	9 30	38	9 30				
		39	9 45	39	9 45				
		40	10 0	40	10 0				
		41	10 15	41	10 15				
		42	10 30	42	10 30				
		43	10 45	43	10 45				
		44	11 0	44	11 0				
		45	11 15	45	11 15				
		46	11 30	46	11 30				
		47	11 45	47	11 45				
		48	12 0	48	12 0				
		49	12 15	49	12 15				
		50	12 30	50	12 30				
		51	12 45	51	12 45				
		52	13 0	52	13 0				
		53	13 15	53	13 15				
		54	13 30	54	13 30				
		55	13 45	55	13 45				
		56	14 0	56	14 0				
		57	14 15	57	14 15				
		58	14 30	58	14 30				
		59	14 45	59	14 45				

TABLE 21

FOR REDUCING DAILY AND TWELVE-HOURLY VARIATIONS

Interval 24 ^h	Interval 12 ^h	Variation in 24 ^h or in 12 ^h									
		1'		2'		3'		4'		5'	
		0"	30"	0"	30"	0"	30"	0"	30"	0"	30"
0 ^h 0 ^m	0 ^h 0 ^m	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"
1 0	15	0' 1'2	0' 1'9	0' 2'5	0' 3'1	0' 3'7	0' 4'4	0' 5'0	0' 5'6	0' 6'2	0' 6'9
1 30	30	0' 2'5	0' 3'7	0' 5'0	0' 6'2	0' 7'5	0' 8'7	0' 10'0	0' 11'2	0' 12'5	0' 13'7
2 0	45	0' 3'7	0' 5'6	0' 7'5	0' 9'4	0' 11'2	0' 13'1	0' 15'0	0' 16'9	0' 18'7	0' 20'6
2 30	1 0	0' 5'0	0' 7'5	0' 10'0	0' 12'5	0' 15'0	0' 17'5	0' 20'0	0' 22'5	0' 25'0	0' 27'5
3 0	15	0' 6'2	0' 9'3	0' 12'5	0' 15'6	0' 18'7	0' 21'9	0' 25'0	0' 28'1	0' 31'2	0' 34'4
3 30	30	0' 7'5	0' 11'2	0' 15'0	0' 18'7	0' 22'5	0' 26'2	0' 30'0	0' 33'7	0' 37'5	0' 41'2
4 0	45	0' 8'7	0' 13'1	0' 17'5	0' 21'9	0' 26'2	0' 30'6	0' 35'0	0' 39'4	0' 43'7	0' 48'1
4 30	2 0	0' 10'0	0' 15'0	0' 20'0	0' 25'0	0' 30'0	0' 35'0	0' 40'0	0' 45'0	0' 50'0	0' 55'0
5 0	15	0' 11'2	0' 16'8	0' 22'5	0' 28'1	0' 33'7	0' 39'4	0' 45'0	0' 50'6	0' 56'2	1' 1'9
6 0	30	0' 12'5	0' 18'7	0' 25'0	0' 31'2	0' 37'5	0' 43'7	0' 50'0	0' 56'2	1' 2'5	1' 8'7
6 30	45	0' 13'7	0' 20'6	0' 27'5	0' 34'4	0' 41'2	0' 48'1	0' 55'0	1' 1'9	1' 8'7	1' 15'6
7 0	3 0	0' 15'0	0' 22'5	0' 30'0	0' 37'5	0' 45'0	0' 52'5	1' 0'0	1' 7'5	1' 15'0	1' 22'5
7 30	15	0' 16'2	0' 24'4	0' 32'5	0' 40'6	0' 48'7	0' 56'9	1' 5'0	1' 13'1	1' 21'2	1' 29'4
8 0	30	0' 17'5	0' 26'2	0' 35'0	0' 43'7	0' 52'5	1' 1'2	1' 10'0	1' 18'7	1' 27'5	1' 36'2
8 30	45	0' 18'7	0' 28'1	0' 37'5	0' 46'9	0' 56'2	1' 5'6	1' 15'0	1' 24'4	1' 33'7	1' 43'1
9 0	4 0	0' 20'0	0' 30'0	0' 40'0	0' 50'0	1' 0'0	1' 10'0	1' 20'0	1' 30'0	1' 40'0	1' 50'0
9 30	15	0' 21'2	0' 31'9	0' 42'5	0' 53'1	1' 3'7	1' 14'4	1' 25'0	1' 35'6	1' 46'2	1' 56'9
10 0	30	0' 22'5	0' 33'7	0' 45'0	0' 56'2	1' 7'5	1' 18'7	1' 30'0	1' 41'2	1' 52'5	2' 3'7
10 30	45	0' 23'7	0' 35'6	0' 47'5	0' 59'3	1' 11'2	1' 23'1	1' 35'0	1' 46'9	1' 58'7	2' 10'6
12 0	5 0	0' 25'0	0' 37'5	0' 50'0	1' 2'4	1' 15'0	1' 27'5	1' 40'0	1' 52'5	2' 5'0	2' 17'5
12 30	15	0' 26'2	0' 39'4	0' 52'5	1' 5'6	1' 18'7	1' 31'9	1' 45'0	1' 58'1	2' 11'2	2' 24'4
13 0	30	0' 27'5	0' 41'2	0' 55'0	1' 8'7	1' 22'5	1' 36'2	1' 50'0	2' 3'7	2' 17'5	2' 31'2
13 30	45	0' 28'7	0' 43'1	0' 57'5	1' 11'8	1' 26'2	1' 40'6	1' 55'0	2' 9'4	2' 23'7	2' 38'1
14 0	6 0	0' 30'0	0' 45'0	1' 0'0	1' 15'0	1' 30'0	1' 45'0	2' 0'0	2' 15'0	2' 30'0	2' 45'0
14 30	15	0' 31'2	0' 46'9	1' 2'5	1' 18'1	1' 33'7	1' 49'4	2' 5'0	2' 20'6	2' 36'2	2' 51'9
15 0	30	0' 32'5	0' 48'7	1' 5'0	1' 21'4	1' 37'5	1' 53'7	2' 10'0	2' 26'2	2' 42'5	2' 58'7
15 30	45	0' 33'7	0' 50'6	1' 7'5	1' 24'4	1' 41'2	1' 58'1	2' 15'0	2' 31'9	2' 48'7	3' 5'6
16 0	7 0	0' 35'0	0' 52'5	1' 10'0	1' 27'5	1' 45'0	2' 2'5	2' 20'0	2' 37'5	2' 55'0	3' 12'5
16 30	15	0' 36'2	0' 54'4	1' 12'5	1' 30'6	1' 48'7	2' 6'9	2' 25'0	2' 43'1	3' 1'2	3' 19'4
18 0	30	0' 37'5	0' 56'2	1' 15'0	1' 33'7	1' 52'5	2' 11'2	2' 30'0	2' 48'7	3' 7'5	3' 26'2
18 30	45	0' 38'7	0' 58'1	1' 17'5	1' 36'8	1' 56'2	2' 15'6	2' 35'0	2' 54'4	3' 13'7	3' 33'1
19 0	8 0	0' 40'0	1' 0'0	1' 20'0	1' 40'0	2' 0'0	2' 20'0	2' 40'0	3' 0'0	3' 20'0	3' 40'0
19 30	15	0' 41'2	1' 1'9	1' 22'5	1' 43'1	2' 3'7	2' 24'4	2' 45'0	3' 5'6	3' 26'2	3' 46'9
20 0	30	0' 42'5	1' 3'7	1' 25'0	1' 46'2	2' 7'5	2' 28'7	2' 50'0	3' 11'2	3' 32'5	3' 53'7
20 30	45	0' 43'7	1' 5'6	1' 27'5	1' 49'3	2' 11'2	2' 33'1	2' 55'0	3' 16'9	3' 38'7	4' 0'6
21 0	9 0	0' 45'0	1' 7'5	1' 30'0	1' 52'5	2' 15'0	2' 37'5	3' 0'0	3' 22'5	3' 45'0	4' 7'5
21 30	15	0' 46'2	1' 9'3	1' 32'5	1' 55'6	2' 18'7	2' 41'9	3' 5'0	3' 28'1	3' 51'2	4' 14'4
22 0	30	0' 47'5	1' 11'2	1' 35'0	1' 58'7	2' 22'5	2' 46'2	3' 10'0	3' 33'7	3' 57'5	4' 21'2
22 30	45	0' 48'7	1' 13'1	1' 37'5	2' 1'9	2' 26'2	2' 50'6	3' 15'0	3' 39'4	4' 3'7	4' 28'1
24 0	10 0	0' 50'0	1' 15'0	1' 40'0	2' 5'0	2' 30'0	2' 55'0	3' 20'0	3' 45'0	4' 10'0	4' 35'0
24 30	15	0' 51'2	1' 16'8	1' 42'5	2' 8'1	2' 33'7	2' 59'4	3' 25'0	3' 50'6	4' 16'2	4' 41'9
25 0	30	0' 52'5	1' 18'7	1' 45'0	2' 11'2	2' 37'5	3' 3'7	3' 30'0	3' 56'2	4' 22'5	4' 48'7
25 30	45	0' 53'7	1' 20'6	1' 47'5	2' 14'3	2' 41'2	3' 8'1	3' 35'0	4' 1'9	4' 28'7	4' 55'6
26 0	11 0	0' 55'0	1' 22'5	1' 50'0	2' 17'4	2' 45'0	3' 12'5	3' 40'0	4' 7'5	4' 35'0	5' 2'5
26 30	15	0' 56'2	1' 24'4	1' 52'5	2' 20'6	2' 48'7	3' 16'9	3' 45'0	4' 13'1	4' 41'2	5' 9'4
27 0	30	0' 57'5	1' 26'2	1' 55'0	2' 23'7	2' 52'5	3' 21'2	3' 50'0	4' 18'7	4' 47'5	5' 16'2
27 30	45	0' 58'7	1' 28'1	1' 57'5	2' 26'8	2' 56'2	3' 25'6	3' 55'0	4' 24'4	4' 53'7	5' 23'1
28 0	12 0	1' 0'0	1' 30'0	2' 0'0	2' 30'0	3' 0'0	3' 30'0	4' 0'0	4' 30'0	5' 0'0	5' 30'0
28 30	15	1' 1'2	1' 31'9	2' 2'5	2' 33'1	3' 3'7	3' 34'4	4' 5'0	4' 35'6	5' 6'2	5' 36'9
30 0	30	1' 2'5	1' 33'7	2' 5'0	2' 36'2	3' 7'5	3' 38'7	4' 30'0	4' 41'2	5' 12'5	5' 43'7
30 30	45	1' 3'7	1' 35'6	2' 7'5	2' 39'4	3' 11'2	3' 43'1	4' 15'0	4' 46'9	5' 18'7	5' 50'6
31 0	13 0	1' 5'0	1' 37'5	2' 10'0	2' 42'5	3' 15'0	3' 47'5	4' 20'0	4' 52'5	5' 25'0	5' 57'5
31 30	15	1' 6'2	1' 39'4	2' 12'5	2' 45'6	3' 18'7	3' 51'9	4' 25'0	4' 58'1	5' 31'2	6' 4'4
32 0	30	1' 7'5	1' 41'2	2' 15'0	2' 48'7	3' 22'5	3' 56'2	4' 30'0	5' 3'7	5' 37'5	6' 11'2
32 30	45	1' 8'7	1' 43'1	2' 17'5	2' 51'9	3' 26'2	4' 0'6	4' 35'0	5' 9'4	5' 43'7	6' 18'1
33 0	14 0	1' 10'0	1' 45'0	2' 20'0	2' 55'0	3' 30'0	4' 5'0	4' 40'0	5' 15'0	5' 50'0	6' 25'0
33 30	15	1' 11'2	1' 46'9	2' 22'5	2' 58'1	3' 33'7	4' 9'4	4' 45'0	5' 20'6	5' 56'2	6' 31'9
34 0	30	1' 12'5	1' 48'7	2' 25'0	3' 1'2	3' 37'5	4' 13'7	4' 55'0	5' 26'2	6' 2'5	6' 38'7
34 30	45	1' 13'7	1' 50'6	2' 27'5	3' 4'3	3' 41'2	4' 18'1	4' 50'0	5' 31'9	6' 8'7	6' 45'6
35 0	15 0	1' 15'0	1' 52'5	2' 30'0	3' 7'5	3' 45'0	4' 22'5	5' 0'0	5' 37'5	6' 15'0	6' 52'5

FOR REDUCING DAILY AND TWELVE-HOURLY VARIATIONS

Interval 24 ^h	Interval 12 ^h	Variation in 24 ^h or in 12 ^h									
		6'		7'		8'		9'		10'	
		0''	30''	0''	30''	0''	30''	0''	30''	0''	30''
0 ^h 0'	0 ^h 0'	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"
30	15	0 7.5	0 8.1	0 8.7	0 9.4	0 10	0 10.6	0 11.2	0 11.9	0 12.5	0 13.1
1 0	30	0 15	0 16.2	0 17.5	0 18.7	0 20	0 21.2	0 22.5	0 23.7	0 25	0 26.2
30	45	0 22.5	0 24.4	0 26.2	0 28.1	0 30	0 31.9	0 33.7	0 35.6	0 37.5	0 39.4
2 0	1 0	0 30	0 32.5	0 35	0 37.5	0 40	0 42.5	0 45	0 47.5	0 50	0 52.5
30	15	0 37.5	0 40.6	0 43.7	0 46.9	0 50	0 53.1	0 56.2	0 59.4	1 2.5	1 5.6
3 0	30	0 45	0 48.7	0 52.5	0 56.2	1 0	1 3.7	1 7.5	1 11.2	1 15	1 18.7
30	45	0 52.5	0 56.9	1 1.2	1 5.6	1 10	1 14.4	1 18.7	1 23.1	1 27.5	1 31.9
4 0	2 0	1 0	1 5	1 10	1 15	1 20	1 25	1 30	1 35	1 40	1 45
30	15	1 7.5	1 13.1	1 18.7	1 24.4	1 30	1 35.6	1 41.2	1 46.9	1 52.5	1 58.1
5 0	30	1 15	1 21.2	1 27.5	1 33.7	1 40	1 46.2	1 52.5	1 58.7	2 5	2 11.2
30	45	1 22.5	1 29.4	1 36.2	1 43.1	1 50	1 56.9	2 3.7	2 10.6	2 17.5	2 24.4
6 0	3 0	1 30	1 37.5	1 45	1 52.5	2 0	2 7.5	2 15	2 22.5	2 30	2 37.5
30	15	1 37.5	1 45.6	1 53.7	2 1.9	2 10	2 18.1	2 26.2	2 34.4	2 42.5	2 50.6
7 0	30	1 45	1 53.7	2 2.5	2 11.2	2 20	2 28.7	2 37.5	2 46.2	2 55	3 3.7
30	45	1 52.5	2 1.9	2 11.2	2 20.6	2 30	2 39.4	2 48.7	2 58.1	3 7.5	3 16.9
8 0	4 0	2 0	2 10	2 20	2 30	2 40	2 50	3 0	3 10	3 20	3 30
30	15	2 7.5	2 18.1	2 28.7	2 39.4	2 50	3 0.6	3 11.2	3 21.9	3 32.5	3 43.1
9 0	30	2 15	2 26.2	2 37.5	2 48.7	3 0	3 11.2	3 22.5	3 33.7	3 44	3 56.2
30	45	2 22.5	2 34.4	2 46.2	2 58.1	3 10	3 21.9	3 33.7	3 45.6	3 57.5	4 9.4
10 0	5 0	2 30	2 42.5	2 55	3 7.5	3 20	3 32.5	3 45	3 57.5	4 10	4 22.5
30	15	2 37.5	2 50.6	3 3.7	3 16.9	3 30	3 43.1	3 56.2	4 9.4	4 22.5	4 35.6
11 0	30	2 45	2 58.7	3 12.5	3 26.2	3 40	3 53.7	4 7.5	4 21.2	4 35	4 48.7
30	45	2 52.5	3 6.9	3 21.2	3 35.6	3 50	4 4.4	4 18.7	4 33.1	4 47.5	5 1.9
12 0	6 0	3 0	3 15	3 30	3 45	4 0	4 15	4 30	4 45	5 0	5 15
30	15	3 7.5	3 23.1	3 38.7	3 54.4	4 10	4 25.6	4 41.2	4 56.9	5 12.5	5 28.1
13 0	30	3 15	3 31.2	3 47.5	4 3.7	4 20	4 36.2	4 52.5	5 8.7	5 25	5 41.2
30	45	3 22.5	3 39.4	3 56.2	4 13.1	4 30	4 46.9	5 3.7	5 20.6	5 37.5	5 54.4
14 0	7 0	3 30	3 47.5	4 5	4 22.5	4 40	4 57.5	5 15	5 32.5	5 50	6 7.5
30	15	3 37.5	3 55.6	4 13.7	4 31.9	4 50	5 8.1	5 26.2	5 44.4	6 2.5	6 20.6
15 0	30	3 45	4 3.7	4 22.5	4 41.2	5 0	5 18.7	5 37.5	5 56.2	6 15	6 33.7
30	45	3 52.5	4 11.9	4 31.2	4 50.6	5 10	5 29.4	5 48.7	6 8.1	6 27.5	6 46.9
16 0	8 0	4 0	4 20	4 40	5 0	5 20	5 40	6 0	6 20	6 40	7 0
30	15	4 7.5	4 28.1	4 48.7	5 9.4	5 30	5 50.6	6 11.2	6 31.9	6 52.5	7 13.1
17 0	30	4 15	4 36.2	4 57.5	5 18.7	5 40	6 1.2	6 22.5	6 43.7	7 5	7 26.2
30	45	4 22.5	4 44.4	5 6.2	5 28.1	5 50	6 11.9	6 33.7	6 55.6	7 17.5	7 39.4
18 0	9 0	4 30	4 52.5	5 15	5 37.5	6 0	6 22.5	6 45	7 7.5	7 30	7 52.5
30	15	4 37.5	5 0.6	5 23.7	5 46.9	6 10	6 33.1	6 56.2	7 19.4	7 42.5	8 5.6
19 0	30	4 45	5 8.7	5 32.5	5 56.2	6 20	6 43.7	7 7.5	7 31.2	7 55	8 18.7
30	45	4 52.5	5 16.9	5 41.2	6 5.6	6 30	6 54.4	7 18.7	7 43.1	8 7.5	8 31.9
20 0	10 0	5 0	5 25	5 50	6 15	6 40	7 5	7 30	7 55	8 20	8 45
30	15	5 7.5	5 33.1	5 58.7	6 24.4	6 50	7 15.6	7 41.2	8 7.9	8 32.5	8 58.1
21 0	30	5 15	5 41.2	6 7.5	6 33.7	7 0	7 26.2	7 52.5	8 18.7	8 44	9 11.2
30	45	5 22.5	5 49.4	6 16.2	6 43.1	7 10	7 36.9	8 3.7	8 30.6	8 57.5	9 24.4
22 0	11 0	5 30	5 57.5	6 25	6 52.5	7 20	7 47.5	8 15	8 42.5	9 10	9 37.5
30	15	5 37.5	6 5.6	6 33.7	7 1.9	7 30	7 58.1	8 26.2	8 54.4	9 22.5	9 50.6
23 0	30	5 45	6 13.7	6 42.5	7 11.2	7 40	8 7.7	8 37.5	9 6.2	9 35	10 3.7
30	45	5 52.5	6 21.9	6 51.2	7 20.6	7 50	8 19.4	8 48.7	9 18.1	9 47.5	10 16.9
24 0	12 0	6 0	6 30.5	7 0	7 30	8 0	8 30	9 0	9 30	10 0	10 30
30	15	6 7.5	6 38.1	7 8.7	7 39.4	8 10	8 40.6	9 11.2	9 41.9	10 12.5	10 43.1
25 0	30	6 15	6 46.2	7 17.5	7 48.7	8 20	8 51.2	9 22.5	9 53.7	10 25	10 56.2
30	45	6 22.5	6 54.4	7 26.2	7 58.1	8 30	9 1.9	9 33.7	10 5.6	10 37.5	11 9.4
26 0	13 0	6 30	7 2.5	7 35	8 7.5	8 40	9 12.5	9 45	10 17.5	10 50	11 22.5
30	15	6 37.5	7 10.6	7 43.7	8 16.9	8 50	9 23.1	9 56.2	10 29.4	11 2.5	11 35.6
27 0	30	6 45	7 18.7	7 52.5	8 26.2	9 0	9 33.7	10 7.5	10 41.2	11 15	11 48.7
30	45	6 52.5	7 26.9	8 1.2	8 35.6	9 10	9 44.4	10 18.7	10 53.1	11 27.5	12 1.9
28 0	14 0	7 0	7 35	8 10	8 45	9 20	9 55	10 30	11 5	12 40	13 15
30	15	7 7.5	7 43.1	8 18.7	8 54.4	9 30	10 5.6	10 41.2	11 16.9	12 52.5	13 28.1
29 0	30	7 15	7 51.2	8 27.5	9 3.7	9 40	10 16.2	10 52.5	11 28.7	12 5	13 41.2
30	45	7 22.5	7 59.4	8 36.2	9 13.1	9 50	10 26.9	11 3.7	11 40.6	12 17.5	13 54.4
30 0	15 0	7 30	8 7.5	8 45	9 22.5	10 0	10 37.5	11 15	11 52.5	12 30	13 7.5

TABLE 21

651

FOR REDUCING DAILY AND TWELVE-HOURLY VARIATIONS												
Interval 24 ^h	Interval 12 ^h	Variation in 24 ^h or in 12 ^h										
		11'		12'		13'		14		15'		
		0'	30"	0'	30"	0'	30"	0'	30"	0'	30"	
0 0	0 0	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"	0' 0"
30	15	0 13.7	0 14.4	0 15	0 15.6	0 16.2	0 16.9	0 17.5	0 18.1	0 18.7	0 19.4	
1 0	30	0 27.5	0 28.7	0 30	0 31.2	0 32.5	0 33.7	0 35	0 36.2	0 37.5	0 38.7	
30	45	0 41.2	0 43.1	0 45	0 46.9	0 48.7	0 50.6	0 52.5	0 54.4	0 56.2	0 58.1	
2 0	1 0	0 55	0 57.5	1 0	1 2.5	1 5	1 7.5	1 10	1 12.5	1 15	1 17.5	
30	15	1 8.7	1 11.9	1 15	1 18.1	1 21.2	1 24.4	1 27.5	1 30.6	1 33.7	1 36.9	
3 0	30	1 22.5	1 26.2	1 30	1 33.7	1 37.5	1 41.2	1 45	1 48.7	1 52.5	1 56.2	
30	45	1 36.2	1 40.6	1 45	1 49.4	1 53.7	1 58.1	2 2.5	1 36.9	2 11.2	2 15.6	
4 0	2 0	1 50	1 55	2 0	2 5	2 10	2 15	2 20	2 25	2 30	2 35	
30	15	2 3.7	2 9.4	2 15	2 20.6	2 26.2	2 31.9	2 37.5	2 43.1	2 48.7	2 54.4	
5 0	30	2 17.5	2 23.7	2 30	2 36.2	2 42.5	2 48.7	2 55	3 1.2	3 7.5	3 13.7	
30	45	2 31.2	2 38.1	2 45	2 51.9	2 58.7	3 5.6	3 12.5	3 19.4	3 26.2	3 33.1	
6 0	3 0	2 45	2 52.5	3 0	3 7.5	3 15	3 22.5	3 30	3 37.5	3 45	3 52.5	
30	15	2 58.7	3 6.9	3 15	3 23.1	3 31.2	3 39.4	3 47.5	3 55.6	4 3.7	4 11.9	
7 0	30	3 12.5	3 21.2	3 30	3 38.7	3 47.5	3 56.2	4 5	4 13.7	4 22.5	4 31.2	
30	45	3 26.2	3 35.6	3 45	3 54.4	4 3.7	4 13.1	4 23.5	4 31.9	4 41.2	4 50.6	
8 0	4 0	3 40	3 50	4 0	4 10	4 20	4 30	4 40	4 50	5 0	5 10	
30	15	3 53.7	4 4.4	4 15	4 25.6	4 36.2	4 46.9	4 57.5	5 8.1	5 18.7	5 29.4	
9 0	30	4 7.5	4 18.7	4 30	4 41.2	4 52.5	5 3.7	5 15	5 26.2	5 37.5	5 48.7	
30	45	4 21.2	4 33.1	4 45	4 56.9	5 8.7	5 20.6	5 32.5	5 44.4	5 56.2	6 8.1	
10 0	5 0	4 35	4 47.5	5 0	5 12.5	5 25	5 37.5	5 50	6 2.5	6 15	6 27.5	
30	15	4 48.7	5 1.9	5 15	5 28.1	5 41.2	5 54.4	6 7.5	6 20.6	6 33.7	6 46.9	
11 0	30	5 2.5	5 26.2	5 30	5 43.7	5 57.5	6 11.2	6 25	6 38.7	6 52.5	7 6.2	
30	45	5 16.2	5 40.6	5 45	5 59.4	6 13.7	6 28.1	6 42.5	6 56.9	7 11.2	7 25.6	
12 0	6 0	5 30	5 45	6 0	6 15	6 30	6 45	7 0	7 15	7 30	7 45	
30	15	5 43.7	5 59.4	6 15	6 30.6	6 46.2	7 1.9	7 17.5	7 33.1	7 48.7	8 4.4	
13 0	30	5 57.5	6 13.7	6 30	6 46.2	7 2.5	7 18.7	7 35	7 51.2	8 7.5	8 23.7	
30	45	6 11.2	6 28.1	6 45	7 1.9	7 18.7	7 35.6	7 52.5	8 9.4	8 26.2	8 43.1	
14 0	7 0	6 25	6 42.5	7 0	7 17.5	7 35	7 52.5	8 10	8 27.5	8 45	9 2.5	
30	15	6 38.7	6 56.9	7 15	7 33.1	7 51.2	8 9.4	8 27.5	8 45.6	9 3.7	9 21.9	
15 0	8 0	6 52.5	7 11.2	7 30	7 48.7	8 7.5	8 26.2	8 45	9 3.7	9 22.5	9 41.2	
30	45	7 6.2	7 25.6	7 45	8 4.4	8 23.7	8 43.1	9 2.5	9 21.9	9 41.2	10 0.6	
16 0	8 0	7 20	7 40	8 0	8 20	8 40	9 0	9 20	9 40	10 0	10 20	
30	15	7 33.7	7 54.4	8 15	8 35.6	8 56.2	9 16.9	9 37.5	9 58.1	10 18.7	10 39.4	
17 0	30	7 47.5	8 8.7	8 30	8 51.2	9 12.5	9 33.7	9 55	10 16.2	10 37.5	10 58.7	
30	45	8 1.2	8 23.1	8 45	9 6.9	9 28.7	9 50.6	10 12.5	10 34.4	10 56.2	11 18.1	
18 0	9 0	8 15	8 37.5	9 0	9 22.5	9 45	10 7.5	10 30	10 52.5	11 15	11 37.5	
30	15	8 28.7	8 51.9	9 15	9 38.1	10 1.2	10 24.4	10 47.5	11 10.6	11 33.7	11 56.9	
19 0	30	8 42.5	9 6.2	9 30	9 53.7	10 17.5	10 41.2	11 5	11 28.7	11 52.5	12 16.2	
30	45	8 56.2	9 20.6	9 45	10 9.4	10 33.7	10 58.1	11 23.5	11 46.9	12 11.2	12 35.6	
20 0	10 0	9 10	9 35	10 0	10 25	10 50	11 15	11 40	12 5	12 30	12 55	
30	15	9 23.7	9 49.4	10 15	10 40.6	11 6.2	11 31.9	11 57.5	12 23.1	12 48.7	13 14.4	
21 0	30	9 37.5	10 3.7	10 30	10 56.2	11 22.5	11 48.7	12 15	12 41.2	13 7.5	13 33.7	
30	45	9 51.2	10 18.1	10 45	11 11.9	11 38.7	12 5.6	12 32.5	12 59.4	13 26.2	13 53.1	
22 0	11 0	10 5	10 32.5	11 0	11 27.5	11 55	12 22.5	12 50	13 17.5	13 45	14 12.5	
30	15	10 18.7	10 46.9	11 15	11 43.1	12 11.2	12 39.4	13 7.5	13 35.6	14 3.7	14 31.9	
23 0	30	10 32.5	11 1.2	11 30	11 58.7	12 27.5	12 56.2	13 25	13 53.7	14 22.5	14 51.2	
30	45	10 46.2	11 15.6	11 45	12 14.4	12 43.7	13 13.1	13 42.5	14 11.9	14 41.2	15 10.6	
24 0	12 0	11 0	11 30	12 0	12 30	13 0	13 30	14 0	14 30	15 0	15 30	
30	15	11 13.7	11 44.4	12 15	12 45.6	13 16.2	13 46.9	14 17.5	14 48.1	15 18.7	15 49.4	
25 0	30	11 27.5	11 58.7	12 30	13 1.2	13 32.5	14 3.7	14 35	15 6.2	15 37.5	16 8.7	
30	45	11 41.2	12 13.1	12 45	13 16.9	13 48.7	14 20.6	14 52.5	15 24.4	15 56.2	16 28.1	
26 0	13 0	11 55	12 27.5	13 0	13 32.5	14 5	14 37.5	15 10	15 42.5	16 15	16 47.5	
30	15	12 8.7	12 41.9	13 15	13 48.1	14 21.2	14 54.4	15 27.5	16 0.6	16 33.7	17 6.9	
27 0	30	12 22.5	12 56.2	13 30	14 3.7	14 37.5	15 11.2	15 45	16 18.7	16 52.5	17 26.2	
30	45	12 36.2	13 10.6	13 45	14 19.4	14 53.7	15 28.1	16 2.5	16 36.9	17 11.2	17 45.6	
28 0	14 0	12 50	13 25	14 0	14 35	15 10	15 45	16 20	16 55	17 30	18 5	
30	15	13 3.7	13 39.4	14 15	14 50.6	15 26.2	16 1.9	16 37.5	17 13.1	17 48.7	18 24.4	
29 0	30	13 17.5	13 53.7	14 30	15 6.2	15 42.5	16 18.7	16 55	17 31.2	18 7.5	18 43.7	
30	45	13 31.2	14 8.1	14 45	15 21.9	15 58.7	16 35.6	17 12.5	17 49.4	18 26.2	19 3.1	
30 0	15 0	13 45	14 22.5	15 0	15 37.5	16 15	16 52.5	17 30	18 7.5	18 45	19 22.5	

FOR REDUCING DAILY AND TWELVE-HOURLY VARIATIONS

Interval 24 ^h	Interval 12 ^h	Variation in 24 ^h or in 12 ^h									
		16'		17'		18'		19'		20'	
		0"	30"	0"	30"	0"	30"	0"	30"	0"	30"
0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
30	15	0 20	0 20.6	0 21.2	0 21.9	0 22.5	0 23.1	0 23.7	0 24.4	0 25	0 25.6
1 0	30	0 40	0 41.2	0 42.5	0 43.7	0 45	0 46.2	0 47.5	0 48.7	0 50	0 51.2
30	45	1 0	1 1.9	1 3.7	1 5.6	1 7.5	1 9.4	1 11.2	1 13.1	1 15	1 16.9
2 0	1 0	1 20	1 22.5	1 25	1 27.5	1 30	1 32.5	1 35	1 37.5	1 40	1 42.5
30	15	1 40	1 43.1	1 46.2	1 49.4	1 52.5	1 55.6	1 58.7	2 1.9	2 5	2 8.1
3 0	30	2 0	2 3.7	2 7.5	2 11.2	2 15	2 18.7	2 22.5	2 26.2	2 30	2 33.7
30	45	2 20	2 24.4	2 28.7	2 33.1	2 37.5	2 41.9	2 46.2	2 50.6	2 55	2 59.4
4 0	2 0	2 40	2 45	2 50	2 55	3 0	3 5	3 10	3 15	3 20	3 25
30	15	3 0	3 5.6	3 11.2	3 16.9	3 22.5	3 28.1	3 33.7	3 39.4	3 45	3 50.6
5 0	30	3 20	3 26.2	3 32.5	3 38.7	3 45	3 51.2	3 57.5	4 3.7	4 10	4 16.2
30	45	3 40	3 46.9	3 53.7	4 0.6	4 7.5	4 14.4	4 21.2	4 28.1	4 35	4 41.9
6 0	3 0	4 0	4 7.5	4 15	4 22.5	4 30	4 37.5	4 45	4 52.5	5 0	5 7.5
30	15	4 20	4 28.1	4 36.2	4 44.4	4 52.5	5 0.6	5 8.7	5 16.9	5 25	5 33.1
7 0	30	4 40	4 48.7	4 57.5	5 6.2	5 15	5 23.7	5 32.5	5 41.2	5 50	5 58.7
30	45	5 0	5 9.4	5 18.7	5 28.1	5 37.5	5 46.9	5 56.2	6 5.6	6 15	6 24.4
8 0	4 0	5 20	5 30	5 40	5 50	6 0	6 10	6 20	6 30	6 40	6 50
30	15	5 40	5 50.6	6 1.2	6 11.9	6 22.5	6 33.1	6 43.7	6 54.4	7 5	7 15.6
9 0	30	6 0	6 11.2	6 22.5	6 33.7	6 45	6 56.2	7 7.5	7 18.7	7 30	7 41.2
30	45	6 20	6 31.9	6 43.7	6 55.6	7 7.5	7 19.4	7 31.2	7 43.1	7 55	8 6.9
10 0	5 0	6 40	6 52.5	7 5	7 17.5	7 30	7 42.5	7 55	8 7.5	8 20	8 32.5
30	15	7 0	7 13.1	7 26.2	7 39.4	7 52.5	8 5.6	8 18.7	8 31.9	8 45	8 58.1
11 0	30	7 20	7 33.7	7 47.5	8 11.2	8 15	8 28.7	8 42.5	8 56.2	9 10	9 23.7
30	45	7 40	7 54.4	8 8.7	8 23.1	8 37.5	8 51.9	9 6.2	9 20.6	9 35	9 49.4
12 0	6 0	8 0	8 15	8 30	8 45	9 0	9 15	9 30	9 45	10 0	10 15
30	15	8 20	8 35.6	8 51.2	9 6.9	9 22.5	9 38.1	9 53.7	10 9.4	10 25	10 40.6
13 0	30	8 40	8 56.2	9 12.5	9 28.7	9 45	10 1.2	10 17.5	10 33.7	10 50	11 6.2
30	45	9 0	9 16.9	9 33.7	9 50.6	10 7.5	10 24.4	10 41.2	10 58.1	11 15	11 31.9
14 0	7 0	9 20	9 37.5	9 55	10 12.5	10 30	10 47.5	11 5	11 22.5	11 40	11 57.5
30	15	9 40	9 58.1	10 16.2	10 34.4	10 52.5	11 10.6	11 28.7	11 46.9	12 5	12 23.1
15 0	30	10 0	10 18.7	10 37.5	10 56.2	11 15	11 33.7	11 52.5	12 11.2	12 30	12 48.7
30	45	10 20	10 39.4	10 58.7	11 18.1	11 37.5	11 56.9	12 16.2	12 35.6	12 55	13 14.4
16 0	8 0	10 40	11 0	11 20	11 40	12 0	12 20	12 40	13 0	13 20	13 40
30	15	11 0	11 20.6	11 41.2	12 1.9	12 22.5	12 43.1	13 3.7	13 24.4	13 45	14 5.6
17 0	30	11 20	11 41.2	12 2.5	12 23.7	12 45	13 6.2	13 27.5	13 48.7	14 10	14 31.2
30	45	11 40	12 1.9	12 23.7	12 45.6	13 7.5	13 29.4	13 51.2	14 13.1	14 35	14 56.9
18 0	9 0	12 0	12 22.5	12 45	13 7.5	13 30	13 52.5	14 15	14 37.5	15 0	15 22.5
30	15	12 20	12 43.1	13 6.2	13 29.4	13 52.5	14 15.6	14 38.7	15 1.9	15 25	15 48.1
19 0	70	12 40	13 3.7	13 27.5	13 51.2	14 15	14 38.7	15 2.5	15 26.2	15 50	16 13.7
30	45	13 0	13 24.4	13 48.7	14 13.1	14 37.5	15 1.9	15 26.2	15 50.6	16 15	16 39.4
20 0	10 0	13 20	13 45	14 10	14 35	15 0	15 25	15 50	16 15	16 40	17 5
30	15	13 40	14 5.6	14 31.2	14 56.9	15 22.5	15 48.1	16 13.7	16 39.4	17 5	17 30.6
21 0	30	14 0	14 26.2	14 52.5	15 18.7	15 45	16 11.2	16 37.5	17 3.7	17 30	17 56.2
30	45	14 20	14 46.9	15 13.7	15 40.6	16 7.5	16 34.4	17 1.2	17 28.1	17 55	18 21.9
22 0	11 0	14 40	15 7.5	15 35	16 2.5	16 30	16 57.5	17 25	17 52.5	18 20	18 47.5
30	15	15 0	15 28.1	15 56.2	16 24.4	16 52.5	17 20.6	17 48.7	18 16.9	18 45	19 13.1
23 0	30	15 20	15 48.7	16 17.5	16 46.2	17 15	17 43.7	18 12.5	18 41.2	19 10	19 38.7
30	45	15 40	16 9.4	16 38.7	17 8.1	17 37.5	18 6.9	18 36.2	19 5.6	19 35	20 4.4
24 0	12 0	16 0	16 30	17 0	17 30	18 0	18 30	19 0	19 30	20 0	20 30
30	15	16 20	16 50.6	17 21.2	17 51.9	18 22.5	18 53.1	19 23.7	19 54.4	20 25	20 55.6
25 0	30	16 40	17 11.2	17 42.5	18 13.7	18 45	19 16.2	19 47.5	20 18.7	20 50	21 21.2
30	45	17 0	17 31.9	18 3.7	18 35.6	19 7.5	19 39.4	20 11.2	20 43.1	21 15	21 46.9
26 0	13 0	17 20	17 52.5	18 25	18 57.5	19 30	20 2.5	20 35	21 7.5	21 40	22 12.5
30	15	17 40	18 13.1	18 46.2	19 19.4	19 52.5	20 15.6	20 58.7	21 31.9	22 5	22 38.1
27 0	30	18 0	18 33.7	19 7.5	19 41.2	20 15	20 48.7	21 22.5	21 56.2	22 30	23 3.7
30	45	18 20	18 54.4	19 28.7	20 3.1	20 37.5	21 11.9	21 46.2	22 20.6	22 55	23 29.4
28 0	14 0	18 40	19 15	19 50	20 25	21 0	21 35	22 10	22 45	23 20	23 55
30	15	19 0	19 35.6	20 11.2	20 46.9	21 22.5	21 58.1	22 33.7	23 9.4	23 45	24 20.6
29 0	30	19 20	19 56.2	20 32.5	21 8.7	21 45	22 21.2	22 57	23 33.7	24 15	24 46.2
30	45	19 40	20 16.9	20 53.7	21 30.6	22 7.5	22 44.4	23 21.2	23 58.1	24 35	25 11.9
30 0	16 0	20 0	20 37.5	21 15	21 52.5	22 30	23 7.5	23 45	24 22.5	25 0	25 37.5

TABLE 21

659

FOR REDUCING DAILY AND TWELVE-HOURLY VARIATIONS

Interval 24'	Interval 12'	Variation in 24' or in 12'									
		21'		22'		23'		24'		25'	
		0"	30"	0"	30"	0"	30"	0"	30"	0"	30"
0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
30	15	0 26.2	0 26.9	0 27.5	0 28.1	0 28.7	0 29.4	0 30.0	0 30.6	0 31.2	0 31.9
1 0	30	0 52.5	0 53.7	0 55	0 56.2	0 57.5	0 58.7	1 0	1 1.2	1 2.5	1 3.7
30	45	1 18.7	1 20.6	1 22.5	1 24.4	1 26.2	1 28.1	1 30	1 31.9	1 33.7	1 35.6
2 0	1 0	1 45	1 47.5	1 50	1 52.5	1 55	1 57.5	2 0	2 2.5	2 5	2 7.5
30	15	2 11.2	2 14.4	2 17.5	2 20.6	2 23.7	2 26.9	2 30	2 33.1	2 36.2	2 39.4
3 0	30	2 37.5	2 41.2	2 45	2 48.7	2 52.5	2 56.2	3 0	3 3.7	3 7.5	3 11.2
30	45	3 3.7	3 8.1	3 12.5	3 16.9	3 21.2	3 25.6	3 30	3 34.4	3 38.7	3 43.1
4 0	2 0	3 30	3 35	3 40	3 45	3 50	3 55	4 0	4 5	4 10	4 15
30	15	3 56.2	4 1.9	4 7.5	4 13.1	4 18.7	4 24.4	4 30	4 35.6	4 41.2	4 46.9
5 0	30	4 22.5	4 28.7	4 35	4 41.2	4 47.5	4 53.7	5 0	5 6.2	5 12.5	5 18.7
30	45	4 48.7	4 55.6	5 2.5	5 9.4	5 16.2	5 23.1	5 30	5 36.9	5 43.7	5 50.6
6 0	3 0	5 15	5 22.5	5 30	5 37.5	5 45	5 52.5	6 0	6 7.5	6 15	6 22.5
30	15	5 41.2	5 49.4	5 57.5	6 5.6	6 13.7	6 21.9	6 30	6 38.1	6 46.2	6 54.4
7 0	30	6 7.5	6 16.2	6 25	6 33.7	6 42.5	6 51.2	7 0	7 8.7	7 17.5	7 26.2
30	45	6 33.7	6 43.1	6 52.5	7 1.9	7 11.2	7 20.6	7 30	7 39.4	7 48.7	7 58.1
8 0	4 0	7 0	7 10	7 20	7 30	7 40	7 50	8 0	8 10	8 20	8 30
30	15	7 26.2	7 36.9	7 47.5	7 58.1	8 8.7	8 19.4	8 30	8 40.6	8 51.2	9 1.9
9 0	30	7 52.5	8 3.7	8 15	8 26.2	8 37.5	8 48.7	9 0	9 11.2	9 22.5	9 33.7
30	45	8 18.7	8 30.6	8 42.5	8 54.4	9 6.2	9 18.1	9 30	9 41.9	9 53.7	10 5.6
10 0	5 0	8 45	8 57.5	9 10	9 22.5	9 35	9 47.5	10 0	10 12.5	10 25	10 37.5
30	15	9 11.2	9 24.4	9 37.5	9 50.6	10 3.7	10 16.9	10 30	10 43.1	10 56.2	11 9.4
11 0	30	9 37.5	9 51.2	10 5	10 18.7	10 32.5	10 46.2	11 0	11 13.7	11 27.5	11 41.2
30	45	10 3.7	10 18.1	10 32.5	10 46.9	11 1.2	11 15.6	11 30	11 44.4	11 58.7	12 13.1
12 0	6 0	10 30	10 45	11 0	11 15	11 30	11 45	12 0	12 15	12 30	12 45
30	15	10 56.2	11 11.9	11 27.5	11 43.1	11 58.7	12 14.4	12 30	12 45.6	13 1.2	13 16.9
13 0	30	11 22.5	11 38.7	11 55	12 11.2	12 27.5	12 43.7	13 0	13 16.2	13 32.5	13 48.7
30	45	11 48.7	12 5.6	12 22.5	12 39.4	12 56.2	13 13.1	13 30	13 46.9	14 3.7	14 20.6
14 0	7 0	12 15	12 32.5	12 50	13 7.5	13 25	13 42.5	14 0	14 17.5	14 35	14 52.5
30	15	12 41.2	12 59.4	13 17.5	13 35.6	13 53.7	14 11.9	14 30	14 48.1	15 6.2	15 24.4
15 0	30	13 7.5	13 26.2	13 45	14 3.7	14 22.5	14 41.2	15 0	15 18.7	15 37.5	15 56.2
30	45	13 33.7	13 53.1	14 12.5	14 31.9	14 51.2	15 10.6	15 30	15 49.4	16 8.7	16 27.1
16 0	8 0	14 0	14 20	14 40	15 0	15 20	15 40	16 0	16 20	16 40	17 0
30	15	14 26.2	14 46.9	15 7.5	15 28.1	15 48.7	16 9.4	16 30	16 50.6	17 11.2	17 31.9
17 0	30	15 52.5	15 13.7	15 35	15 56.2	16 7.5	16 38.7	17 0	17 21.2	17 42.5	18 3.7
30	45	15 18.7	15 40.6	16 2.5	16 24.4	16 46.2	17 8.1	17 30	17 51.9	18 13.7	18 35.6
18 0	9 0	15 45	16 7.5	16 30	16 52.5	17 15	17 37.5	18 0	18 22.5	18 45	19 7.5
30	15	16 11.2	16 34.4	16 57.5	17 20.6	17 43.7	18 6.9	18 30	18 53.1	19 16.2	19 39.4
19 0	30	16 37.5	17 1.2	17 25	17 48.7	18 12.5	18 36.2	19 0	19 23.7	19 47.5	20 11.2
30	45	17 3.7	17 28.1	17 52.5	18 16.9	18 41.2	19 5.6	19 30	19 54.4	20 18.7	20 43.1
20 0	10 0	17 30	17 55	18 20	18 45	19 10	19 35	20 0	20 25	20 50	21 15
30	15	17 56.2	18 21.9	18 47.5	19 13.1	19 38.7	20 4.4	20 30	20 55.6	21 21.2	21 46.9
21 0	30	18 22.5	18 48.7	19 15	19 41.2	20 7.5	20 33.7	21 0	21 26.2	21 52.5	22 18.7
30	45	18 48.7	19 15.6	19 42.5	20 9.4	20 36.2	21 3.1	21 30	21 56.9	22 23.7	22 50.6
22 0	11 0	19 15	19 42.5	20 10	20 37.5	21 5	21 32.5	22 0	22 27.5	22 55	23 22.5
30	15	19 41.2	20 9.4	20 37.5	21 5.6	21 33.7	22 1.9	22 30	22 58.1	23 26.2	23 54.4
23 0	30	20 7.5	20 36.2	21 5	21 33.7	22 2.5	22 31.2	23 0	23 28.7	23 57.5	24 26.2
30	45	20 33.7	21 3.1	21 32.5	22 1.9	22 31.2	23 0.6	23 30	23 59.4	24 28.7	24 58.1
24 0	12 0	21 0	21 30	22 0	22 30	23 0	23 30	24 0	24 30	25 0	25 30
30	15	21 26.2	21 56.9	22 27.5	22 58.1	23 28.7	23 59.4	24 30	25 0.6	25 31.2	26 1.9
25 0	30	21 52.5	22 23.7	22 55	23 26.2	23 57.5	24 28.7	25 0	25 31.2	26 2.5	26 33.7
30	45	22 18.7	22 50.6	23 22.5	23 54.4	24 26.2	24 58.1	25 30	26 1.9	26 33.7	27 5.6
26 0	13 0	22 45	23 17.5	23 50	24 22.5	24 55	25 27.5	26 0	26 32.5	27 5	27 37.5
30	15	23 11.2	23 44.4	24 17.5	24 50.6	25 23.7	25 56.9	26 30	27 3.1	27 36.2	28 9.4
27 0	30	23 37.5	24 11.2	24 45	25 18.7	25 52.5	26 26.2	27 0	27 33.7	28 7.5	28 41.2
30	45	24 3.7	24 38.1	25 12.5	25 46.9	26 21.2	26 55.6	27 30	28 4.4	28 38.7	29 13.1
28 0	14 0	24 30	25 5	25 40	26 15	26 50	27 25	28 0	28 35	29 10	29 45
30	15	24 56.2	25 31.9	26 7.5	26 43.1	27 18.7	27 54.4	28 30	29 5.6	29 41.2	30 16.9
29 0	30	25 22.5	25 58	26 35	27 11.2	27 47.5	28 23.7	29 0	29 36.2	30 18.7	30 48.7
30	45	25 48.7	26 25.6	27 2.5	27 39.4	28 16.2	28 53.1	29 30	30 6.9	30 43.7	31 20.6
30 0	15 0	26 15	26 52.5	27 30	28 7.5	28 45	29 22.5	30 0	30 37.5	31 15	31 52.5

FOR REDUCING DAILY AND TWELVE-HOURLY VARIATIONS

Interval 24"	Interval 12"	Variation in 24" or in 12"											
		26		27		28		29		30			
		0"	30'	0"	30"	0"	30"	0"	30"	0"	30"	0"	30"
0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
30	15	0 32.5	0 33.1	0 33.7	0 34.4	0 35	0 35.6	0 36.2	0 36.9	0 37.5	0 38.1	0 38.7	0 39.4
1 0	30	1 5	1 6.2	1 7.5	1 8.7	1 10	1 11.2	1 12.5	1 13.7	1 15	1 16.2	1 17.5	1 18.7
30	45	1 37.5	1 39.4	1 41.2	1 43.1	1 45	1 46.9	1 48.7	1 50.6	1 52.5	1 54.4	1 56.2	1 58.1
2 0	1 0	2 10	2 12.5	2 15	2 17.5	2 20	2 22.5	2 25	2 27.5	2 30	2 32.5	2 34.4	2 36.2
30	15	2 42.5	2 45.6	2 48.7	2 51.9	2 55	2 58.1	3 1	3 4.4	3 7.5	3 10.6	3 13.7	3 16.2
3 0	30	3 15	3 18.7	3 22.5	3 26.2	3 30	3 33.7	3 37.5	3 41.2	3 45	3 48.7	3 52.5	3 56.2
30	45	3 47.5	3 51.9	3 56.2	4 0.6	4 5	4 9.4	4 13.7	4 18.1	4 22.5	4 26.9	4 31.2	4 35.6
4 0	2 0	4 20	4 25.2	4 30	4 35	4 40	4 45	4 50	4 55	5 0	5 5	5 10	5 15
30	15	4 52.5	4 58.1	5 3.7	5 9.4	5 15	5 20.6	5 26.2	5 31.9	5 37.5	5 43.1	5 48.7	5 54.4
5 0	30	5 25	5 31.2	5 37.5	5 43.7	5 50	5 56.2	6 2.5	6 8.7	6 15	6 21.2	6 27.5	6 33.7
30	45	5 57.5	6 4.4	6 11.2	6 18.1	6 25	6 31.9	6 38.7	6 45.6	6 52.5	6 59.4	7 6.2	7 13.1
6 0	3 0	6 30	6 37.5	6 45	6 52.5	7 0	7 7.5	7 15	7 22.5	7 30	7 37.5	7 44.4	7 51.2
30	15	7 2.5	7 10.6	7 18.7	7 26.9	7 35	7 43.1	7 51.2	7 59.4	8 7.5	8 15.6	8 23.7	8 31.9
7 0	30	7 35	7 43.7	7 52.5	8 1.2	8 10	8 18.7	8 27.5	8 36.2	8 45	8 53.7	9 2.5	9 11.2
30	45	8 7.5	8 16.9	8 26.2	8 35.6	8 45	8 54.4	9 3.7	9 13.1	9 22.5	9 31.9	9 41.2	9 50.6
8 0	4 0	8 40	8 50	9 0	9 10	9 20	9 30	9 40	9 50	10 0	10 10	10 20	10 30
30	15	9 12.5	9 23.1	9 33.7	9 44.4	9 55	10 5.6	10 16.2	10 26.9	10 37.5	10 48.1	10 58.7	11 9.4
9 0	30	9 45	9 56.2	10 7.5	10 18.7	10 30	10 41.2	10 52.5	11 3.7	11 15	11 26.2	11 37.5	11 48.7
30	45	10 17.5	10 29.4	10 41.2	10 53.1	11 5	11 16.9	11 28.7	11 40.6	11 52.5	12 4.4	12 16.2	12 28.1
10 0	5 0	10 50	11 2.5	11 15	11 27.5	11 40	11 52.5	12 5	12 17.5	12 30	12 42.5	12 54.4	13 6.2
30	15	11 22.5	11 35.6	11 48.7	12 1.9	12 15	12 28.1	12 41.2	12 54.4	13 7.5	13 20.6	13 33.7	13 46.9
11 0	30	11 55	12 8.7	12 22.5	12 36.2	12 50	13 3.7	13 17.5	13 31.2	13 45	13 58.7	14 12.5	14 26.2
30	45	12 27.5	12 41.9	12 56.2	13 10.6	13 25	13 39.4	13 53.7	14 8.1	14 22.5	14 36.9	14 51.2	15 5.6
12 0	6 0	13 0	13 15	13 30	13 45	14 0	14 15	14 30	14 45	15 0	15 15	15 30	15 45
30	15	13 32.5	13 48.1	14 3.7	14 19.4	14 35	14 50.6	15 6.2	15 21.9	15 37.5	15 53.1	16 8.7	16 24.4
13 0	30	14 5	14 21.2	14 37.5	14 53.7	15 10	15 26.2	15 42.5	15 58.7	16 15	16 31.2	16 47.5	17 3.7
30	45	14 37.5	14 54.4	15 11.2	15 28.1	15 45	16 1.9	16 18.7	16 35.6	16 52.5	17 9.4	17 26.2	17 43.1
14 0	7 0	15 10	15 27.5	15 45	16 2.5	16 20	16 37.5	16 55	17 12.5	17 30	17 47.5	18 5.6	18 23.7
30	15	15 42.5	16 0.6	16 18.7	16 36.9	16 55	17 13.1	17 31.2	17 49.4	18 7.5	18 25.6	18 43.7	19 2.5
15 0	30	16 15	16 33.7	16 52.5	17 11.2	17 30	17 48.7	18 7.5	18 26.2	18 45	19 3.7	19 22.5	19 41.9
30	45	16 47.5	17 6.9	17 26.2	17 45.6	18 5	18 24.4	18 43.7	19 3.1	19 22.5	19 41.9	20 20.6	20 39.4
16 0	8 0	17 20	17 40	18 0	18 20	18 40	19 0	19 20	19 40	20 0	20 20	20 40	21 0
30	15	17 52.5	18 13.1	18 33.7	18 54.4	19 15	19 35.6	19 56.2	20 16.9	20 37.5	20 58.1	21 18.7	21 39.4
17 0	30	18 25	18 46.2	19 7.5	19 28.7	19 50	20 11.2	20 32.5	20 53.7	21 15	21 36.2	21 57.5	22 18.7
30	45	18 57.5	19 19.4	19 41.2	20 3.1	20 25	20 46.9	21 8.7	21 30.6	21 52.5	22 14.4	22 36.2	22 58.1
18 0	9 0	19 30	19 52.5	20 15	20 37.5	21 0	21 22.5	21 45	22 7.5	22 30	22 52.5	23 15	23 37.5
30	15	20 2.5	20 25.6	20 48.7	21 11.9	21 35	21 58.1	22 21.2	22 44.4	23 7.5	23 30.6	23 53.7	24 16.9
19 0	30	20 35	20 58.7	21 22.5	21 46.2	22 10	22 33.7	22 57.5	23 21.2	23 45	24 8.7	24 32.5	24 56.2
30	45	21 7.5	21 31.9	21 56.2	22 20.6	22 45	23 9.4	23 33.7	23 58.1	24 22.5	24 46.9	25 11.2	25 35.6
20 0	10 0	21 40	22 5	22 30	22 55	23 20	23 45	24 10	24 35	25 0	25 25	25 50	26 15
30	15	22 12.5	22 38.1	23 3.7	23 29.4	23 55	24 20.6	24 46.2	25 11.9	25 37.5	26 3.1	26 28.7	26 54.4
21 0	30	22 45	23 11.2	23 37.5	24 3.7	24 30	24 56.2	25 22.5	25 48.7	26 15	26 41.2	27 7.5	27 33.7
30	45	23 17.5	23 44.4	24 11.2	24 38.1	25 5	25 31.9	25 58.7	26 25.6	26 52.5	27 19.4	27 46.2	28 13.1
22 0	11 0	23 50	24 17.5	24 45	25 12.5	25 40	26 7.5	26 35	27 2.5	27 30	27 57.5	28 24.4	28 51.2
30	15	24 22.5	24 50.6	25 18.7	25 46.9	26 15	26 43.1	27 11.2	27 39.4	28 7.5	28 35.6	29 3.7	29 31.9
23 0	30	24 55	25 23.7	25 52.5	26 21.2	26 50	27 18.7	27 47.5	28 16.2	28 45	29 13.7	29 42.5	30 11.2
30	45	25 27.5	25 56.9	26 26.2	26 55.6	27 25	27 54.4	28 23.7	28 53.1	29 22.5	29 51.9	30 21.2	30 50.6
24 0	12 0	26 0	26 30	27 0	27 30	28 0	28 30	29 0	29 30	30 0	30 30	31 0	31 30
30	15	26 32.5	27 3.1	27 33.7	28 4.4	28 35	29 5.6	29 36.2	30 6.9	30 37.5	31 8.1	31 39.4	32 10.6
25 0	30	27 5	27 36.2	28 7.5	28 38.7	29 10	29 41.2	30 12.5	30 43.7	31 15	31 46.2	32 17.5	32 48.7
30	45	27 37.5	28 9.4	28 41.2	29 13.1	29 45	30 16.9	30 48.7	31 20.6	31 52.5	32 24.4	32 56.2	33 8.7
26 0	13 0	28 10	28 42.5	29 15	29 47.5	30 20	30 52.5	31 25	31 57.5	32 30	33 2.5	33 35	33 67.5
30	15	28 42.5	29 5.6	29 48.7	30 21.9	30 55	31 28.1	32 1.2	32 34.4	33 7.5	33 40.6	34 13.7	34 46.9
27 0	30	29 15	29 48.7	30 22.5	30 56.2	31 30	32 3.7	32 37.5	33 11.2	33 45	34 18.7	34 51.2	35 23.7
30	45	29 47.5	30 21.9	30 56.2	31 30.6	32 5	32 39.4	33 13.7	33 48.1	34 22.5	34 56.9	35 31.2	36 5.6
28 0	14 0	30 20	30 55	31 30	32 5	32 40	33 15	33 50	34 25	35 0	35 35	36 10	36 45
30	15	30 52.5	31 28.1	32 3.7	32 39.4	33 15	33 50.6	34 26.2	35 1.9	35 37.5	36 13.1	36 48.7	37 19.4
29 0	30	31 25	32 1.2	32 37.5	33 13.7	33 50	34 26.2	35 2.5	35 38.7	36 15	36 51.2	37 26.2	38 1.9
30	45	31 57.5	32 34.4	33 11.2	33 48.1	34 25	35 1.9	35 38.7	36 15.6	36 52.5	37 29.4	38 5.6	38 31.9
30 0	15 0	32 30	33 7.5	33 45	34 22.5	35 0	35 37.5	36 15	36 52.5	37 30	38 7.5	38 44.4	39 16.9

TABLE 21 A

655

LOGARITHMS FOR REDUCING DAILY VARIATIONS													
Min. or Sec.	Hours, Degrees, or Minutes											Min. or Sec.	
	0	1	2	3	4	5	6	7	8	9	10		11
0		1'3802	1'0792	9031	7781	6812	6021	5351	4771	4260	3802	3388	0
1	3'1584	1'3730	1'0756	9007	7763	6798	6009	5341	4762	4252	3795	3382	1
2	2'8573	1'3660	1'0720	8983	7745	6784	5997	5330	4753	4244	3788	3375	2
3	2'6812	1'3590	1'0685	8959	7728	6769	5985	5320	4744	4236	3780	3368	3
4	2'5563	1'3522	1'0649	8935	7710	6755	5973	5310	4735	4228	3773	3362	4
5	2'4594	1'3454	1'0614	8912	7692	6741	5961	5300	4726	4220	3766	3355	5
6	2'3802	1'3388	1'0580	8888	7674	6726	5949	5289	4717	4212	3759	3349	6
7	2'3133	1'3323	1'0546	8865	7657	6712	5937	5279	4708	4204	3752	3342	7
8	2'2553	1'3259	1'0512	8842	7639	6698	5925	5269	4699	4196	3745	3336	8
9	2'2041	1'3195	1'0478	8819	7622	6684	5913	5259	4690	4188	3737	3329	9
10	2'1584	1'3133	1'0444	8796	7604	6670	5902	5249	4682	4180	3730	3323	10
11	2'1170	1'3071	1'0411	8773	7587	6656	5890	5239	4673	4172	3723	3316	11
12	2'0792	1'3010	1'0378	8751	7570	6642	5878	5229	4664	4164	3716	3310	12
13	2'0444	1'2950	1'0345	8728	7552	6628	5866	5219	4655	4156	3709	3303	13
14	2'0122	1'2891	1'0313	8706	7535	6614	5855	5209	4646	4148	3702	3297	14
15	1'9823	1'2833	1'0280	8683	7518	6600	5843	5199	4638	4141	3695	3291	15
16	1'9542	1'2775	1'0248	8661	7501	6587	5832	5189	4629	4133	3688	3284	16
17	1'9279	1'2719	1'0216	8639	7484	6573	5820	5179	4620	4125	3681	3278	17
18	1'9031	1'2663	1'0185	8617	7467	6559	5809	5169	4611	4117	3674	3271	18
19	1'8796	1'2607	1'0153	8595	7451	6546	5797	5159	4603	4109	3667	3265	19
20	1'8573	1'2553	1'0122	8573	7434	6532	5786	5149	4594	4102	3660	3258	20
21	1'8361	1'2499	1'0091	8552	7417	6518	5774	5139	4585	4094	3653	3252	21
22	1'8159	1'2445	1'0061	8530	7401	6505	5763	5129	4577	4086	3646	3246	22
23	1'7966	1'2393	1'0030	8509	7384	6492	5752	5120	4568	4079	3639	3239	23
24	1'7782	1'2341	1'0000	8487	7368	6478	5740	5110	4559	4071	3632	3233	24
25	1'7604	1'2289	0'9970	8466	7351	6465	5729	5100	4551	4063	3625	3227	25
26	1'7434	1'2239	0'9940	8445	7335	6452	5718	5090	4542	4055	3618	3220	26
27	1'7270	1'2188	0'9910	8424	7318	6438	5706	5081	4534	4048	3611	3214	27
28	1'7112	1'2139	0'9881	8403	7302	6425	5695	5071	4525	4040	3604	3208	28
29	1'6960	1'2090	0'9852	8382	7286	6412	5684	5061	4516	4032	3597	3201	29
30	1'6812	1'2041	0'9823	8361	7270	6398	5673	5051	4508	4025	3590	3195	30
31	1'6670	1'1993	0'9794	8341	7254	6385	5662	5042	4499	4017	3583	3189	31
32	1'6532	1'1946	0'9765	8320	7238	6372	5651	5032	4491	4010	3576	3183	32
33	1'6398	1'1899	0'9737	8300	7222	6359	5640	5023	4482	4002	3570	3176	33
34	1'6269	1'1852	0'9708	8279	7206	6346	5629	5013	4474	3994	3563	3170	34
35	1'6143	1'1806	0'9680	8259	7190	6333	5618	5003	4466	3987	3556	3164	35
36	1'6021	1'1761	0'9652	8239	7174	6320	5607	4994	4457	3979	3549	3157	36
37	1'5902	1'1716	0'9625	8219	7159	6307	5596	4984	4449	3972	3542	3151	37
38	1'5786	1'1671	0'9597	8199	7143	6294	5585	4975	4440	3964	3535	3145	38
39	1'5673	1'1627	0'9570	8179	7128	6282	5574	4965	4432	3957	3529	3139	39
40	1'5563	1'1584	0'9542	8159	7112	6269	5563	4956	4424	3949	3522	3133	40
41	1'5456	1'1540	0'9515	8140	7097	6256	5552	4947	4415	3942	3515	3126	41
42	1'5351	1'1498	0'9488	8120	7081	6243	5541	4937	4407	3934	3508	3120	42
43	1'5249	1'1455	0'9462	8101	7066	6231	5531	4928	4399	3927	3501	3114	43
44	1'5149	1'1413	0'9435	8081	7050	6218	5520	4918	4390	3919	3495	3108	44
45	1'5051	1'1372	0'9408	8062	7035	6205	5509	4909	4382	3912	3488	3102	45
46	1'4956	1'1331	0'9382	8043	7020	6193	5498	4900	4374	3905	3481	3096	46
47	1'4863	1'1290	0'9356	8023	7005	6180	5488	4890	4365	3897	3475	3089	47
48	1'4771	1'1249	0'9330	8004	6990	6168	5477	4881	4357	3890	3468	3083	48
49	1'4682	1'1209	0'9305	7985	6975	6155	5466	4872	4349	3882	3461	3077	49
50	1'4594	1'1170	0'9279	7966	6960	6143	5456	4863	4341	3875	3454	3071	50
51	1'4508	1'1130	0'9254	7947	6945	6131	5445	4853	4333	3868	3448	3065	51
52	1'4424	1'1091	0'9228	7929	6930	6118	5435	4844	4324	3860	3441	3059	52
53	1'4341	1'1053	0'9203	7910	6915	6106	5424	4835	4316	3853	3434	3053	53
54	1'4260	1'1015	0'9178	7891	6900	6094	5414	4826	4308	3846	3428	3047	54
55	1'4180	1'0977	0'9153	7873	6885	6081	5403	4817	4300	3838	3421	3041	55
56	1'4102	1'0940	0'9128	7854	6871	6069	5393	4808	4292	3831	3415	3034	56
57	1'4025	1'0902	0'9104	7836	6856	6057	5382	4798	4284	3824	3408	3028	57
58	1'3949	1'0865	0'9079	7818	6841	6045	5372	4789	4276	3817	3401	3022	58
59	1'3875	1'0828	0'9055	7800	6827	6033	5361	4780	4268	3809	3395	3016	59
60	1'3802	1'0792	0'9031	7781	6812	6021	5351	4771	4260	3802	3388	3010	60
	0	1	2	3	4	5	6	7	8	9	10	11	

Min. or Sec.	Hours, Degrees, or Minutes												Min. or Sec.
	12	13	14	15	16	17	18	19	20	21	22	23	
0	3010	2663	2341	2041	1761	1498	1249	1015	0792	0580	0378	0185	0
1	3004	2657	2336	2036	1756	1493	1245	1011	0788	0576	0375	0182	1
2	2998	2652	2330	2031	1752	1489	1241	1007	0785	0573	0371	0179	2
3	2992	2646	2325	2027	1747	1485	1237	1003	0781	0570	0368	0175	3
4	2986	2640	2320	2022	1743	1481	1233	0999	0777	0566	0365	0172	4
5	2980	2635	2315	2017	1738	1476	1229	0996	0774	0563	0361	0169	5
6	2974	2629	2310	2012	1734	1472	1225	0992	0770	0559	0358	0166	6
7	2968	2624	2305	2008	1729	1468	1221	0988	0767	0556	0355	0163	7
8	2962	2618	2300	2003	1725	1464	1217	0984	0763	0552	0352	0160	8
9	2956	2613	2295	1998	1720	1459	1213	0980	0759	0549	0348	0157	9
10	2950	2607	2289	1993	1716	1455	1209	0977	0756	0546	0345	0153	10
11	2944	2602	2284	1988	1711	1451	1205	0973	0753	0542	0342	0150	11
12	2938	2596	2279	1984	1707	1447	1201	0969	0749	0539	0339	0147	12
13	2933	2591	2274	1979	1702	1443	1197	0965	0745	0535	0335	0144	13
14	2927	2585	2269	1974	1698	1438	1193	0962	0741	0532	0332	0141	14
15	2921	2580	2264	1969	1694	1434	1189	0958	0738	0528	0329	0138	15
16	2915	2574	2259	1965	1689	1430	1185	0954	0734	0525	0326	0135	16
17	2909	2569	2254	1960	1685	1426	1181	0950	0731	0522	0322	0132	17
18	2903	2564	2249	1955	1680	1422	1178	0947	0727	0518	0319	0128	18
19	2897	2558	2244	1950	1676	1417	1174	0943	0724	0515	0316	0125	19
20	2891	2553	2239	1946	1671	1413	1170	0939	0720	0511	0313	0122	20
21	2885	2547	2234	1941	1667	1409	1166	0935	0716	0508	0309	0119	21
22	2880	2542	2229	1936	1662	1405	1162	0932	0713	0505	0306	0116	22
23	2874	2536	2223	1932	1658	1401	1158	0928	0709	0501	0303	0113	23
24	2868	2531	2218	1927	1654	1397	1154	0924	0706	0498	0300	0110	24
25	2862	2526	2213	1922	1649	1392	1150	0920	0702	0495	0296	0107	25
26	2856	2520	2208	1917	1645	1388	1146	0917	0699	0491	0293	0104	26
27	2850	2515	2203	1913	1640	1384	1142	0913	0695	0488	0290	0101	27
28	2845	2510	2198	1908	1636	1380	1138	0909	0692	0484	0287	0098	28
29	2839	2504	2193	1903	1632	1376	1134	0905	0688	0481	0283	0094	29
30	2833	2499	2188	1899	1627	1372	1130	0902	0685	0478	0280	0091	30
31	2827	2493	2183	1894	1623	1368	1126	0898	0681	0474	0277	0088	31
32	2821	2488	2178	1889	1618	1363	1123	0895	0677	0471	0274	0085	32
33	2816	2483	2173	1885	1614	1359	1119	0891	0674	0468	0271	0082	33
34	2810	2477	2168	1880	1610	1355	1115	0887	0670	0464	0267	0079	34
35	2804	2472	2163	1875	1605	1351	1111	0883	0667	0461	0264	0076	35
36	2798	2467	2159	1871	1601	1347	1107	0880	0663	0458	0261	0073	36
37	2793	2461	2154	1866	1597	1343	1103	0876	0660	0454	0258	0070	37
38	2787	2456	2149	1862	1592	1339	1099	0872	0656	0451	0255	0067	38
39	2781	2451	2144	1857	1588	1335	1095	0868	0653	0447	0251	0064	39
40	2775	2445	2139	1852	1584	1331	1091	0865	0649	0444	0248	0061	40
41	2770	2440	2134	1848	1579	1326	1088	0861	0646	0441	0245	0058	41
42	2764	2435	2129	1843	1575	1322	1084	0858	0642	0438	0242	0055	42
43	2758	2430	2124	1838	1571	1318	1080	0854	0639	0434	0239	0052	43
44	2753	2424	2119	1834	1566	1314	1076	0850	0635	0431	0235	0048	44
45	2747	2419	2114	1829	1562	1310	1072	0846	0632	0427	0232	0045	45
46	2741	2414	2109	1825	1558	1306	1068	0843	0628	0424	0229	0042	46
47	2736	2409	2104	1820	1553	1302	1064	0839	0625	0421	0226	0039	47
48	2730	2403	2099	1816	1549	1298	1060	0835	0621	0418	0223	0036	48
49	2724	2398	2095	1811	1545	1294	1057	0832	0618	0414	0220	0033	49
50	2719	2393	2090	1806	1540	1290	1053	0828	0614	0411	0216	0030	50
51	2713	2388	2085	1802	1536	1286	1049	0824	0611	0408	0213	0027	51
52	2707	2382	2080	1797	1532	1282	1045	0821	0608	0404	0210	0024	52
53	2702	2377	2075	1793	1527	1278	1041	0817	0604	0401	0207	0021	53
54	2696	2372	2070	1788	1523	1274	1037	0814	0601	0398	0204	0018	54
55	2690	2367	2065	1784	1519	1270	1034	0810	0597	0394	0201	0015	55
56	2685	2362	2061	1779	1515	1265	1030	0806	0594	0391	0197	0012	56
57	2679	2356	2056	1774	1510	1261	1026	0803	0590	0388	0194	0009	57
58	2674	2351	2051	1770	1506	1257	1022	0799	0587	0384	0191	0006	58
59	2668	2346	2046	1765	1502	1253	1018	0795	0583	0381	0188	0003	59
60	2663	2341	2041	1761	1498	1249	1015	0792	0580	0378	0185	0000	60
	12	13	14	15	16	17	18	19	20	21	22	23	

FOR REDUCING THE MOON'S DECLINATION

M	Difference for 10"												
	10"	20"	30"	40"	50"	60"	70"	80"	90"	100"	110"	120"	130"
1	0' 1"	0' 2"	0' 3"	0' 4"	0' 5"	0' 6"	0' 7"	0' 8"	0' 9"	0' 10"	0' 11"	0' 12"	0' 13"
2	0 2	0 4	0 6	0 8	0 10	0 12	0 14	0 16	0 18	0 20	0 22	0 24	0 26
3	0 3	0 6	0 9	0 12	0 15	0 18	0 21	0 24	0 27	0 30	0 33	0 36	0 39
4	0 4	0 8	0 12	0 16	0 20	0 24	0 28	0 32	0 36	0 40	0 44	0 48	0 52
5	0 5	0 10	0 15	0 20	0 25	0 30	0 35	0 40	0 45	0 50	0 55	1 0	1 5
6	0 6	0 12	0 18	0 24	0 30	0 36	0 42	0 48	0 54	1 0	1 6	1 12	1 18
7	0 7	0 14	0 21	0 28	0 35	0 42	0 49	0 56	1 3	1 10	1 17	1 24	1 31
8	0 8	0 16	0 24	0 32	0 40	0 48	0 56	1 4	1 12	1 20	1 28	1 36	1 44
9	0 9	0 18	0 27	0 36	0 45	0 54	1 3	1 12	1 21	1 30	1 39	1 48	1 57
10	0 10	0 20	0 30	0 40	0 50	1 0	1 10	1 20	1 30	1 40	1 50	2 0	2 10
11	0 11	0 22	0 33	0 44	0 55	1 6	1 17	1 28	1 39	1 50	2 1	2 12	2 23
12	0 12	0 24	0 36	0 48	1 0	1 12	1 24	1 36	1 48	2 0	2 12	2 24	2 36
13	0 13	0 26	0 39	0 52	1 5	1 18	1 31	1 44	1 57	2 10	2 23	2 36	2 49
14	0 14	0 28	0 42	0 56	1 10	1 24	1 38	1 52	2 6	2 20	2 34	2 48	3 2
15	0 15	0 30	0 45	1 0	1 15	1 30	1 45	2 0	2 15	2 30	2 45	3 0	3 15
16	0 16	0 32	0 48	1 4	1 20	1 36	1 52	2 8	2 24	2 40	2 56	3 12	3 28
17	0 17	0 34	0 51	1 8	1 25	1 42	1 59	2 16	2 33	2 50	3 7	3 24	3 41
18	0 18	0 36	0 54	1 12	1 30	1 48	2 6	2 24	2 42	3 0	3 18	3 36	3 54
19	0 19	0 38	0 57	1 16	1 35	1 54	2 13	2 32	2 51	3 10	3 29	3 48	4 7
20	0 20	0 40	1 0	1 20	1 40	2 0	2 20	2 40	3 0	3 20	3 40	4 0	4 20
21	0 21	0 42	1 3	1 24	1 45	2 6	2 27	2 48	3 9	3 30	3 51	4 12	4 33
22	0 22	0 44	1 6	1 28	1 50	2 12	2 34	2 56	3 18	3 40	4 2	4 24	4 46
23	0 23	0 46	1 9	1 32	1 55	2 18	2 41	3 4	3 27	3 50	4 13	4 36	4 59
24	0 24	0 48	1 12	1 36	2 0	2 24	2 48	3 12	3 36	4 0	4 24	4 48	5 12
25	0 25	0 50	1 15	1 40	2 5	2 30	2 55	3 20	3 45	4 10	4 35	5 0	5 25
26	0 26	0 52	1 18	1 44	2 10	2 36	3 2	3 28	3 54	4 20	4 46	5 12	5 38
27	0 27	0 54	1 21	1 48	2 15	2 42	3 9	3 36	4 3	4 30	4 57	5 24	5 51
28	0 28	0 56	1 24	1 52	2 20	2 48	3 16	3 44	4 12	4 40	5 8	5 36	6 4
29	0 29	0 58	1 27	1 56	2 25	2 54	3 23	3 52	4 21	4 50	5 19	5 48	6 17
30	0 30	1 0	1 30	2 0	2 30	3 0	3 30	4 0	4 30	5 0	5 30	6 0	6 30
31	0 31	1 2	1 33	2 4	2 35	3 6	3 37	4 8	4 39	5 10	5 41	6 12	6 43
32	0 32	1 4	1 36	2 8	2 40	3 12	3 44	4 16	4 48	5 20	5 52	6 24	6 56
33	0 33	1 6	1 39	2 12	2 45	3 18	3 51	4 24	4 57	5 30	6 3	6 36	7 9
34	0 34	1 8	1 42	2 16	2 50	3 24	3 58	4 32	5 6	5 40	6 14	6 48	7 22
35	0 35	1 10	1 45	2 20	2 55	3 30	4 5	4 40	5 15	5 50	6 25	7 0	7 35
36	0 36	1 12	1 48	2 24	3 0	3 36	4 12	4 48	5 24	6 0	6 36	7 12	7 48
37	0 37	1 14	1 51	2 28	3 5	3 42	4 19	4 56	5 33	6 10	6 47	7 24	8 1
38	0 38	1 16	1 54	2 32	3 10	3 48	4 26	5 4	5 42	6 20	6 58	7 36	8 14
39	0 39	1 18	1 57	2 36	3 15	3 54	4 33	5 12	5 51	6 30	7 9	7 48	8 27
40	0 40	1 20	2 0	2 40	3 20	4 0	4 40	5 20	6 0	6 40	7 20	8 0	8 40
41	0 41	1 22	2 3	2 44	3 25	4 6	4 47	5 28	6 9	6 50	7 31	8 12	8 53
42	0 42	1 24	2 6	2 48	3 30	4 12	4 54	5 36	6 18	7 0	7 42	8 24	9 6
43	0 43	1 26	2 9	2 52	3 35	4 18	5 1	5 44	6 27	7 10	7 53	8 36	9 19
44	0 44	1 28	2 12	2 56	3 40	4 24	5 8	5 52	6 36	7 20	8 4	8 48	9 32
45	0 45	1 30	2 15	3 0	3 45	4 30	5 15	6 0	6 45	7 30	8 15	9 0	9 45
46	0 46	1 32	2 18	3 4	3 50	4 36	5 22	6 8	6 54	7 40	8 26	9 12	9 58
47	0 47	1 34	2 21	3 8	3 55	4 42	5 29	6 16	7 3	7 50	8 37	9 24	10 11
48	0 48	1 36	2 24	3 12	4 0	4 48	5 36	6 24	7 12	8 0	8 48	9 36	10 24
49	0 49	1 38	2 27	3 16	4 5	4 54	5 43	6 32	7 21	8 10	8 59	9 48	10 37
50	0 50	1 40	2 30	3 20	4 10	5 0	5 50	6 40	7 30	8 20	9 10	10 0	10 50
51	0 51	1 42	2 33	3 24	4 15	5 6	5 57	6 48	7 39	8 30	9 21	10 12	11 3
52	0 52	1 44	2 36	3 28	4 20	5 12	6 4	6 56	7 48	8 40	9 32	10 24	11 16
53	0 53	1 46	2 39	3 32	4 25	5 18	6 11	7 4	7 57	8 50	9 43	10 36	11 29
54	0 54	1 48	2 42	3 36	4 30	5 24	6 18	7 12	8 6	9 0	9 54	10 48	11 42
55	0 55	1 50	2 45	3 40	4 35	5 30	6 25	7 20	8 15	9 10	10 5	11 0	11 55
56	0 56	1 52	2 48	3 44	4 40	5 36	6 32	7 28	8 24	9 20	10 16	11 12	12 8
57	0 57	1 54	2 51	3 48	4 45	5 42	6 39	7 36	8 33	9 30	10 27	11 24	12 21
58	0 58	1 56	2 54	3 52	4 50	5 48	6 46	7 44	8 42	9 40	10 38	11 36	12 34
59	0 59	1 58	2 57	3 56	4 55	5 54	6 53	7 52	8 51	9 50	10 49	11 48	12 47
60	1 0	2 0	3 0	4 0	5 0	6 0	7 0	8 0	9 0	10 0	11 0	12 0	13 0

FOR REDUCING THE MOON'S DECLINATION

M	Difference for 10"											
	140"	150"	160"	170"	1"	2"	3"	4"	5"	6"	7"	8"
1	0' 14"	0' 15"	0' 16"	0' 17"	0' 18"	0' 19"	0' 20"	0' 21"	0' 22"	0' 23"	0' 24"	0' 25"
2	0 28	0 30	0 32	0 34	0 36	0 38	0 40	0 42	0 44	0 46	0 48	0 50
3	0 42	0 45	0 48	0 51	0 53	0 56	0 59	1 02	1 05	1 08	1 11	1 14
4	0 56	1 0	1 4	1 8	0 4	0 8	1 2	1 6	2 0	2 4	2 8	3 2
5	1 10	1 15	1 20	1 25	0 5	1 0	1 5	2 0	2 5	3 0	3 5	4 0
6	1 24	1 30	1 36	1 42	0 6	1 2	1 8	2 4	3 0	3 6	4 2	4 8
7	1 38	1 45	1 52	1 59	0 7	1 4	2 1	2 8	3 5	4 2	4 9	5 6
8	1 52	2 0	2 8	2 16	0 8	1 6	2 4	3 2	4 0	4 8	5 6	6 4
9	2 6	2 15	2 24	2 33	0 9	1 8	2 7	3 6	4 5	5 4	6 3	7 2
10	2 20	2 30	2 40	2 50	1 0	2 0	3 0	4 0	5 0	6 0	7 0	8 0
11	2 34	2 45	2 56	3 7	1 1	2 2	3 3	4 4	5 5	6 6	7 7	8 8
12	2 48	3 0	3 12	3 24	1 2	2 4	3 6	4 8	6 0	7 2	8 4	9 6
13	3 2	3 15	3 28	3 41	1 3	2 6	3 9	5 2	6 5	7 8	9 1	10 4
14	3 16	3 30	3 44	3 58	1 4	2 8	4 2	5 6	7 0	8 4	9 8	11 2
15	3 30	3 45	4 0	4 15	1 5	3 0	4 5	6 0	7 5	9 0	10 5	12 0
16	3 44	4 0	4 16	4 32	1 6	3 2	4 8	6 4	8 0	9 6	11 2	12 8
17	3 58	4 15	4 32	4 49	1 7	3 4	5 1	6 8	8 5	10 2	11 9	13 6
18	4 12	4 30	4 48	5 6	1 8	3 6	5 4	7 2	9 0	10 8	12 6	14 4
19	4 26	4 45	5 4	5 23	1 9	3 8	5 7	7 6	9 5	11 4	13 3	15 2
20	4 40	5 0	5 20	5 40	2 0	4 0	6 0	8 0	10 0	12 0	14 0	16 0
21	4 54	5 15	5 36	5 57	2 1	4 2	6 3	8 4	10 5	12 6	14 7	16 8
22	5 8	5 30	5 52	6 14	2 2	4 4	6 6	8 8	11 0	13 2	15 4	17 6
23	5 22	5 45	6 8	6 31	2 3	4 6	6 9	9 2	11 5	13 8	16 1	18 4
24	5 36	6 0	6 24	6 48	2 4	4 8	7 2	9 6	12 0	14 4	16 8	19 2
25	5 50	6 15	6 40	7 5	2 5	5 0	7 5	10 0	12 5	15 0	17 5	20 0
26	6 4	6 30	6 56	7 22	2 6	5 2	7 8	10 4	13 0	15 6	18 2	20 8
27	6 18	6 45	7 12	7 39	2 7	5 4	8 1	10 8	13 5	16 2	18 9	21 6
28	6 32	7 0	7 28	7 56	2 8	5 6	8 4	11 2	14 0	16 8	19 6	22 4
29	6 46	7 15	7 44	8 13	2 9	5 8	8 7	11 6	14 5	17 4	20 3	23 2
30	7 0	7 30	8 0	8 30	3 0	6 0	9 0	12 0	15 0	18 0	21 0	24 0
31	7 14	7 45	8 16	8 47	3 1	6 2	9 3	12 4	15 5	18 6	21 7	24 8
32	7 28	8 0	8 32	9 4	3 2	6 4	9 6	12 8	16 0	19 2	22 4	25 6
33	7 42	8 15	8 48	9 21	3 3	6 6	9 9	13 2	16 5	19 8	23 1	26 4
34	7 56	8 30	9 4	9 38	3 4	6 8	10 2	13 6	17 0	20 4	23 8	27 2
35	8 10	8 45	9 20	9 55	3 5	7 0	10 5	14 0	17 5	21 0	24 5	28 0
36	8 24	9 0	9 36	10 12	3 6	7 2	10 8	14 4	18 0	21 6	25 2	28 8
37	8 38	9 15	9 52	10 29	3 7	7 4	11 1	14 8	18 5	22 2	25 9	29 6
38	8 52	9 30	10 8	10 46	3 8	7 6	11 4	15 2	19 0	22 8	26 6	30 4
39	9 6	9 45	10 24	11 3	3 9	7 8	11 7	15 6	19 5	23 4	27 3	31 2
40	9 20	10 0	10 40	11 20	4 0	8 0	12 0	16 0	20 0	24 0	28 0	32 0
41	9 34	10 15	10 56	11 37	4 1	8 2	12 3	16 4	20 5	24 6	28 7	32 8
42	9 48	10 30	11 12	11 54	4 2	8 4	12 6	16 8	21 0	25 2	29 4	33 6
43	10 2	10 45	11 28	12 11	4 3	8 6	12 9	17 2	21 5	25 8	30 1	34 4
44	10 16	11 0	11 44	12 28	4 4	8 8	13 2	17 6	22 0	26 4	30 8	35 2
45	10 30	11 15	12 0	12 45	4 5	9 0	13 5	18 0	22 5	27 0	31 5	36 0
46	10 44	11 30	12 16	13 2	4 6	9 2	13 8	18 4	23 0	27 6	32 2	36 8
47	10 58	11 45	12 32	13 19	4 7	9 4	14 1	18 8	23 5	28 2	32 9	37 6
48	11 12	12 0	12 48	13 36	4 8	9 6	14 4	19 2	24 0	28 8	33 6	38 4
49	11 26	12 15	13 4	13 53	4 9	9 8	14 7	19 6	24 5	29 4	34 3	39 2
50	11 40	12 30	13 20	14 10	5 0	10 0	15 0	20 0	25 0	30 0	35 0	40 0
51	11 54	12 45	13 36	14 27	5 1	10 2	15 3	20 4	25 5	30 6	35 7	40 8
52	12 8	13 0	13 52	14 44	5 2	10 4	15 6	20 8	26 0	31 2	36 4	41 6
53	12 22	13 15	14 8	15 1	5 3	10 6	15 9	21 2	26 5	31 8	37 1	42 4
54	12 36	13 30	14 24	15 18	5 4	10 8	16 2	21 6	27 0	32 4	37 8	43 2
55	12 50	13 45	14 40	15 35	5 5	11 0	16 5	22 0	27 5	33 0	38 5	44 0
56	13 4	14 0	14 56	15 52	5 6	11 2	16 8	22 4	28 0	33 6	39 2	44 8
57	13 18	14 15	15 12	16 9	5 7	11 4	17 1	22 8	28 5	34 2	39 9	45 6
58	13 32	14 30	15 28	16 26	5 8	11 6	17 4	23 2	29 0	34 8	40 6	46 4
59	13 46	14 45	15 44	16 43	5 9	11 8	17 7	23 6	29 5	35 4	41 3	47 2
60	14 0	15 0	16 0	17 0	6 0	12 0	18 0	24 0	30 0	36 0	42 0	48 0

TABLE 23

ACCELERATION					
H	M	S	M	S	S Dec.
1	0	9'86	1	0'16	1'00
2	0	19'71	2	0'33	2'00
3	0	29'57	3	0'49	3'01
4	0	39'43	4	0'66	4'01
5	0	49'28	5	0'82	5'01
6	0	59'14	6	0'98	6'02
7	1	9'00	7	1'15	7'02
8	1	18'85	8	1'31	8'02
9	1	28'71	9	1'48	9'02
10	1	38'56	10	1'64	10'03
11	1	48'42	11	1'81	11'03
12	1	58'28	12	1'97	12'03
13	2	8'13	13	2'13	13'04
14	2	17'99	14	2'30	14'04
15	2	27'85	15	2'46	15'04
16	2	37'70	16	2'63	16'04
17	2	47'56	17	2'79	17'05
18	2	57'42	18	2'96	18'05
19	3	7'27	19	3'12	19'05
20	3	17'13	20	3'29	20'05
21	3	26'99	21	3'45	21'06
22	3	36'84	22	3'61	22'06
23	3	46'70	23	3'78	23'06
24	3	56'56	24	3'94	24'07
			25	4'11	25'07
			26	4'27	26'07
			27	4'44	27'07
			28	4'60	28'08
			29	4'76	29'08
			30	4'93	30'08
			31	5'09	31'08
			32	5'26	32'09
			33	5'42	33'09
			34	5'59	34'09
			35	5'75	35'10
			36	5'91	36'10
			37	6'08	37'10
			38	6'24	38'11
			39	6'40	39'11
			40	6'57	40'11
			41	6'74	41'11
			42	6'90	42'12
			43	7'06	43'12
			44	7'23	44'12
			45	7'39	45'12
			46	7'56	46'13
			47	7'72	47'13
			48	7'89	48'13
			49	8'05	49'14
			50	8'21	50'14
			51	8'38	51'14
			52	8'54	52'14
			53	8'71	53'15
			54	8'87	54'15
			55	9'04	55'15
			56	9'20	56'15
			57	9'36	57'16
			58	9'53	58'16
			59	9'69	59'16
			60	9'86	60'16

TABLE 24

659

RETARDATION					
H	M	S	M	S	S Dec.
1	0	9'83	1	0'16	1'00
2	0	19'66	2	0'33	2'00
3	0	29'49	3	0'49	3'01
4	0	39'32	4	0'66	4'01
5	0	49'15	5	0'82	5'01
6	0	58'98	6	0'98	6'02
7	1	8'81	7	1'15	7'02
8	1	18'64	8	1'31	8'02
9	1	28'47	9	1'47	9'02
10	1	38'30	10	1'64	10'03
11	1	48'13	11	1'80	11'03
12	1	57'95	12	1'97	12'03
13	2	7'78	13	2'13	13'04
14	2	17'61	14	2'29	14'04
15	2	27'44	15	2'46	15'04
16	2	37'27	16	2'62	16'04
17	2	47'10	17	2'78	17'05
18	2	56'93	18	2'95	18'05
19	3	6'76	19	3'11	19'05
20	3	16'59	20	3'28	20'05
21	3	26'42	21	3'44	21'06
22	3	36'25	22	3'60	22'06
23	3	46'08	23	3'77	23'06
24	3	55'91	24	3'93	24'07
			25	4'10	25'07
			26	4'26	26'07
			27	4'42	27'07
			28	4'59	28'08
			29	4'75	29'08
			30	4'91	30'08
			31	5'08	31'08
			32	5'24	32'09
			33	5'41	33'09
			34	5'57	34'09
			35	5'73	35'10
			36	5'90	36'10
			37	6'06	37'10
			38	6'23	38'11
			39	6'39	39'11
			40	6'55	40'11
			41	6'72	41'11
			42	6'88	42'12
			43	7'04	43'12
			44	7'21	44'12
			45	7'37	45'12
			46	7'54	46'13
			47	7'70	47'13
			48	7'86	48'13
			49	8'03	49'14
			50	8'19	50'14
			51	8'36	51'14
			52	8'52	52'14
			53	8'68	53'15
			54	8'85	54'15
			55	9'01	55'15
			56	9'17	56'15
			57	9'34	57'16
			58	9'50	58'16
			59	9'67	59'16
			60	9'83	60'16

TABLE 25

FOR FINDING THE EQUATION OF SECOND DIFFERENCES											
TABULAR INTERVAL										Multi- plier.	Logarit.
24 Hours		12 Hours		3 Hours		1 Hour					
0 ^h 12 ^m	23 ^h 48 ^m	0 ^h 0 ^m	11 ^h 54 ^m	0 ^h 1 ^m 5	2 ^h 58 ^m 5	1	50	0041	7.61615		
0 24	23 36	0 12	11 48	0 3	2 57			0082	7.91352		
0 36	23 24	0 18	11 42	0 4.5	2 56.5			0122	8.08591		
0 48	23 12	0 24	11 36	0 6	2 54	2	58	0161	8.20713		
1 0	23 0	0 30	11 30	0 7.5	2 52.5			0200	8.30028		
1 12	22 48	0 36	11 24	0 9	2 51	3	57	0238	8.37566		
1 24	22 36	0 42	11 18	0 10.5	2 49.5			0275	8.43878		
1 36	22 24	0 48	11 12	0 12	2 48	4	56	0311	8.49292		
1 48	22 12	0 54	11 6	0 13.5	2 46.5			0347	8.54017		
2 0	22 0	1 0	11 0	0 15	2 45	5	55	0382	8.58200		
2 12	21 48	1 6	10 54	0 16.5	2 43.5			0416	8.61943		
2 24	21 36	1 12	10 48	0 18	2 42	6	54	0450	8.65321		
2 36	21 24	1 18	10 42	0 19.5	2 40.5			0483	8.68393		
2 48	21 12	1 24	10 36	0 21	2 39	7	53	0515	8.71204		
3 0	21 0	1 30	10 30	0 22.5	2 37.5			0547	8.73789		
3 12	21 48	1 36	10 24	0 24	2 36	8	52	0578	8.76176		
3 24	20 36	1 42	10 18	0 25.5	2 34.5			0608	8.78389		
3 36	20 24	1 48	10 12	0 27	2 33	9	51	0637	8.80448		
3 48	20 12	1 54	10 6	0 28.5	2 31.5			0666	8.82368		
4 0	20 0	2 0	10 0	0 30	2 30	10	50	0694	8.84164		
4 12	19 48	2 6	9 54	0 31.5	2 28.5			0722	8.85846		
4 24	19 36	2 12	9 48	0 33	2 27	11	49	0749	8.87426		
4 36	19 24	2 18	9 42	0 34.5	2 25.5			0775	8.88911		
4 48	19 12	2 24	9 36	0 36	2 24	12	48	0800	8.90309		
5 0	19 0	2 30	9 30	0 37.5	2 22.5			0825	8.91627		
5 12	18 48	2 36	9 24	0 39	2 21	13	47	0849	8.92871		
5 24	18 36	2 42	9 18	0 40.5	2 19.5			0872	8.94045		
5 36	18 24	2 48	9 12	0 42	2 18	14	46	0894	8.95195		
5 48	18 12	2 54	9 6	0 43.5	2 16.5			0916	8.96205		
6 0	18 0	3 0	9 0	0 45	2 15	15	45	0937	8.97197		
6 12	17 48	3 6	8 54	0 46.5	2 13.5			0958	8.98136		
6 24	17 36	3 12	8 48	0 48	2 12	16	44	0978	8.99024		
6 36	17 24	3 18	8 42	0 49.5	2 10.5			0997	8.99864		
6 48	17 12	3 24	8 36	0 51	2 9	17	43	1015	9.00658		
7 0	17 0	3 30	8 30	0 52.5	2 7.5			1033	9.01409		
7 12	16 48	3 36	8 24	0 54	2 6	18	42	1050	9.02119		
7 24	16 36	3 42	8 18	0 55.5	2 4.5			1066	9.02789		
7 36	16 24	3 48	8 12	0 57	2 3	19	41	1082	9.03421		
7 48	16 12	3 54	8 6	0 58.5	2 1.5			1097	9.04016		
8 0	16 0	4 0	8 0	1 0	2 0	20	40	1111	9.04576		
8 12	15 48	4 6	7 54	1 1.5	1 58.5			1125	9.05102		
8 24	15 36	4 12	7 48	1 3	1 57	21	39	1138	9.05595		
8 36	15 24	4 18	7 42	1 4.5	1 55.5			1150	9.06057		
8 48	15 12	4 24	7 36	1 6	1 54	22	38	1161	9.06487		
9 0	15 0	4 30	7 30	1 7.5	1 52.5			1172	9.06888		
9 12	14 48	4 36	7 24	1 9	1 51	23	37	1182	9.07260		
9 24	14 36	4 42	7 18	1 10.5	1 49.5			1191	9.07603		
9 36	14 24	4 48	7 12	1 12	1 48	24	36	1200	9.07918		
9 48	14 12	4 54	7 6	1 13.5	1 46.5			1208	9.08206		
10 0	14 0	5 0	7 0	1 15	1 45	25	35	1215	9.08468		
10 12	13 48	5 6	6 54	1 16.5	1 43.5			1222	9.08703		
10 24	13 36	5 12	6 48	1 18	1 42	26	34	1228	9.08912		
10 36	13 24	5 18	6 42	1 19.5	1 40.5			1233	9.09096		
10 48	13 12	5 24	6 36	1 21	1 39	27	33	1237	9.09255		
11 0	13 0	5 30	6 30	1 22.5	1 37.5			1241	9.09388		
11 12	12 48	5 36	6 24	1 24	1 36	28	32	1244	9.09498		
11 24	12 36	5 42	6 18	1 25.5	1 34.5			1247	9.09582		
11 36	12 24	5 48	6 12	1 27	1 33	29	31	1249	9.09643		
11 48	12 12	5 54	6 6	1 28.5	1 31.5			1250	9.09679		
12 0	12 0	6 0	6 0	1 30	1 30	30	30	1250	9.09691		

APPARENT TIME OF THE SUN'S RISING AND SETTING

DECLINATION, of the same Name as the Latitude

Lat.	0°		2°		4°		6°		8°		9°		10°	
	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.
0°	6 ^h 0 ^m	6 ^h 0 ^m	6 ^h 0 ^m	6 ^h 0 ^m	6 ^h 0 ^m	6 ^h 0 ^m	6 ^h 0 ^m	6 ^h 0 ^m	6 ^h 0 ^m	6 ^h 0 ^m	6 ^h 0 ^m	6 ^h 0 ^m	6 ^h 0 ^m	6 ^h 0 ^m
2	6 0	6 0	6 0	6 0	5 59	6 1	5 59	6 1	5 58	6 2	5 58	6 2	5 57	6 3
4	6 0	6 0	6 0	6 0	5 58	6 2	5 58	6 2	5 57	6 3	5 57	6 3	5 56	6 4
6	6 0	6 0	5 59	6 1	5 58	6 2	5 57	6 3	5 56	6 4	5 55	6 5	5 55	6 5
8	6 0	6 0	5 59	6 1	5 57	6 3	5 56	6 4	5 54	6 6	5 54	6 6	5 53	6 7
10	6 0	6 0	5 58	6 2	5 57	6 3	5 55	6 5	5 53	6 7	5 53	6 7	5 52	6 9
12	6 0	6 0	5 58	6 2	5 56	6 4	5 54	6 6	5 52	6 8	5 51	6 8	5 51	6 10
14	6 0	6 0	5 58	6 2	5 55	6 5	5 53	6 7	5 51	6 9	5 50	6 10	5 48	6 12
16	6 0	6 0	5 58	6 2	5 55	6 5	5 52	6 8	5 50	6 10	5 48	6 12	5 47	6 13
18	6 0	6 0	5 57	6 3	5 54	6 6	5 51	6 9	5 48	6 12	5 47	6 13	5 45	6 15
20	6 0	6 0	5 57	6 3	5 54	6 6	5 51	6 9	5 48	6 12	5 46	6 14	5 44	6 16
21	6 0	6 0	5 57	6 3	5 54	6 6	5 50	6 10	5 47	6 13	5 45	6 15	5 44	6 16
22	6 0	6 0	5 57	6 3	5 53	6 7	5 50	6 10	5 46	6 14	5 45	6 15	5 43	6 17
23	6 0	6 0	5 57	6 3	5 53	6 7	5 49	6 11	5 46	6 14	5 44	6 16	5 42	6 18
24	6 0	6 0	5 56	6 4	5 53	6 7	5 49	6 11	5 45	6 15	5 43	6 17	5 41	6 19
25	6 0	6 0	5 56	6 4	5 52	6 8	5 48	6 12	5 44	6 16	5 42	6 18	5 40	6 20
26	6 0	6 0	5 56	6 4	5 52	6 8	5 48	6 12	5 44	6 16	5 41	6 19	5 39	6 21
27	6 0	6 0	5 56	6 4	5 51	6 9	5 47	6 13	5 43	6 17	5 41	6 19	5 38	6 22
28	6 0	6 0	5 56	6 4	5 51	6 9	5 47	6 13	5 43	6 17	5 40	6 20	5 38	6 22
30	6 0	6 0	5 55	6 5	5 51	6 9	5 46	6 14	5 41	6 19	5 39	6 21	5 37	6 23
31	6 0	6 0	5 55	6 5	5 50	6 10	5 46	6 14	5 41	6 19	5 38	6 22	5 36	6 24
32	6 0	6 0	5 55	6 5	5 50	6 10	5 45	6 15	5 40	6 20	5 37	6 23	5 35	6 25
33	6 0	6 0	5 55	6 5	5 50	6 10	5 44	6 16	5 39	6 21	5 36	6 24	5 34	6 26
34	6 0	6 0	5 55	6 5	5 49	6 11	5 44	6 16	5 38	6 22	5 35	6 25	5 33	6 27
35	6 0	6 0	5 55	6 5	5 49	6 11	5 43	6 17	5 37	6 23	5 35	6 25	5 32	6 28
36	6 0	6 0	5 55	6 5	5 48	6 12	5 42	6 18	5 37	6 23	5 34	6 26	5 31	6 29
37	6 0	6 0	5 55	6 5	5 48	6 12	5 42	6 18	5 36	6 24	5 33	6 27	5 29	6 30
38	6 0	6 0	5 55	6 5	5 47	6 13	5 41	6 19	5 35	6 25	5 32	6 29	5 28	6 32
39	6 0	6 0	5 55	6 5	5 47	6 13	5 40	6 20	5 34	6 26	5 31	6 29	5 27	6 33
40	6 0	6 0	5 54	6 6	5 47	6 13	5 40	6 20	5 33	6 27	5 29	6 31	5 26	6 34
41	6 0	6 0	5 54	6 6	5 46	6 14	5 39	6 21	5 32	6 28	5 28	6 32	5 25	6 35
42	6 0	6 0	5 54	6 6	5 46	6 14	5 38	6 22	5 31	6 29	5 27	6 33	5 23	6 37
43	6 0	6 0	5 53	6 7	5 45	6 15	5 38	6 22	5 30	6 30	5 26	6 34	5 22	6 38
44	6 0	6 0	5 53	6 7	5 45	6 15	5 37	6 23	5 29	6 31	5 25	6 35	5 21	6 39
45	6 0	6 0	5 52	6 8	5 44	6 16	5 36	6 24	5 28	6 32	5 24	6 36	5 19	6 41
46	6 0	6 0	5 52	6 8	5 43	6 17	5 35	6 25	5 27	6 33	5 22	6 38	5 18	6 42
47	6 0	6 0	5 51	6 9	5 43	6 17	5 34	6 26	5 25	6 35	5 21	6 39	5 16	6 44
48	6 0	6 0	5 51	6 9	5 42	6 18	5 33	6 27	5 24	6 36	5 19	6 41	5 15	6 45
49	6 0	6 0	5 51	6 9	5 42	6 18	5 32	6 28	5 23	6 37	5 18	6 42	5 13	6 47
50	6 0	6 0	5 50	6 10	5 41	6 19	5 31	6 29	5 21	6 39	5 16	6 44	5 11	6 49
51	6 0	6 0	5 50	6 10	5 40	6 20	5 30	6 30	5 20	6 40	5 15	6 45	5 10	6 50
52	6 0	6 0	5 50	6 10	5 39	6 21	5 29	6 31	5 19	6 41	5 13	6 47	5 8	6 52
53	6 0	6 0	5 49	6 11	5 39	6 21	5 28	6 32	5 17	6 43	5 11	6 49	5 6	6 54
54	6 0	6 0	5 49	6 11	5 38	6 22	5 27	6 33	5 15	6 45	5 10	6 50	5 4	6 56
55	6 0	6 0	5 49	6 11	5 37	6 23	5 25	6 35	5 14	6 46	5 8	6 52	5 2	6 58
56	6 0	6 0	5 48	6 12	5 36	6 24	5 24	6 36	5 12	6 48	5 6	6 54	4 59	7 1
57	6 0	6 0	5 48	6 12	5 35	6 25	5 23	6 37	5 10	6 50	5 4	6 56	4 57	7 3
58	6 0	6 0	5 47	6 13	5 34	6 26	5 21	6 39	5 8	6 52	5 1	6 59	4 54	7 6
59	6 0	6 0	5 47	6 13	5 33	6 27	5 20	6 40	5 6	6 54	4 59	7 1	4 52	7 8
60	6 0	6 0	5 46	6 14	5 32	6 28	5 18	6 42	5 4	6 56	4 56	7 4	4 49	7 11
61	6 0	6 0	5 46	6 14	5 31	6 29	5 16	6 44	5 1	6 59	4 54	7 6	4 46	7 14
62	6 0	6 0	5 45	6 15	5 30	6 30	5 14	6 46	4 59	7 1	4 51	7 9	4 43	7 17
63	6 0	6 0	5 44	6 16	5 28	6 32	5 12	6 48	4 56	7 4	4 48	7 12	4 39	7 21
64	6 0	6 0	5 44	6 16	5 27	6 33	5 10	6 50	4 53	7 7	4 44	7 16	4 35	7 25
65	6 0	6 0	5 43	6 17	5 26	6 34	5 8	6 52	4 50	7 10	4 41	7 19	4 31	7 29
66	6 0	6 0	5 42	6 18	5 24	6 35	5 5	6 54	4 46	7 13	4 37	7 23	4 27	7 33
67	6 0	6 0	5 42	6 18	5 23	6 36	5 4	6 56	4 44	7 16	4 34	7 26	4 24	7 36
Lat.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.

Latitude and Declination of contrary Names

APPARENT TIMES OF THE SUN'S RISING AND SETTING

DECLINATION, of the same Name as the Latitude

Lat.	11°		12°		13°		14°		15°		16°		17°	
	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.
0°	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m
2	5 59	6 1	5 58	6 1	5 58	6 2	5 58	6 2	5 58	6 2	5 58	6 2	5 58	6 2
4	5 57	6 3	5 57	6 3	5 56	6 4	5 56	6 4	5 56	6 4	5 56	6 4	5 55	6 5
6	5 56	6 4	5 55	6 5	5 55	6 5	5 54	6 6	5 54	6 6	5 53	6 7	5 53	6 7
8	5 54	6 6	5 53	6 8	5 53	6 7	5 52	6 8	5 51	6 9	5 51	6 9	5 50	6 10
10	5 52	6 8	5 52	6 9	5 51	6 9	5 50	6 10	5 49	6 11	5 49	6 12	5 48	6 12
12	5 51	6 9	5 50	6 10	5 49	6 11	5 48	6 12	5 47	6 13	5 46	6 14	5 45	6 15
14	5 50	6 11	5 48	6 12	5 48	6 13	5 46	6 14	5 45	6 15	5 44	6 16	5 43	6 17
16	5 47	6 13	5 46	6 14	5 45	6 15	5 44	6 16	5 42	6 18	5 41	6 19	5 40	6 20
18	5 46	6 14	5 44	6 16	5 43	6 17	5 41	6 19	5 40	6 20	5 39	6 21	5 37	6 23
20	5 44	6 16	5 42	6 18	5 41	6 19	5 39	6 21	5 38	6 22	5 36	6 24	5 34	6 26
21	5 43	6 17	5 41	6 19	5 40	6 20	5 38	6 22	5 36	6 24	5 35	6 25	5 33	6 27
22	5 42	6 18	5 40	6 20	5 39	6 21	5 37	6 23	5 35	6 25	5 33	6 27	5 32	6 28
23	5 41	6 19	5 39	6 21	5 38	6 22	5 36	6 24	5 34	6 26	5 32	6 28	5 30	6 30
24	5 40	6 20	5 38	6 22	5 36	6 24	5 34	6 26	5 33	6 27	5 31	6 29	5 29	6 31
25	5 39	6 21	5 37	6 23	5 35	6 25	5 33	6 27	5 31	6 29	5 29	6 31	5 27	6 33
26	5 38	6 22	5 36	6 24	5 34	6 26	5 32	6 28	5 30	6 30	5 28	6 32	5 26	6 34
27	5 37	6 23	5 35	6 25	5 33	6 27	5 31	6 29	5 29	6 31	5 26	6 34	5 24	6 36
28	5 36	6 24	5 34	6 26	5 32	6 28	5 30	6 30	5 27	6 33	5 25	6 35	5 23	6 37
29	5 35	6 25	5 33	6 27	5 31	6 29	5 28	6 32	5 26	6 34	5 23	6 37	5 21	6 39
30	5 34	6 26	5 32	6 28	5 29	6 31	5 27	6 33	5 24	6 36	5 22	6 38	5 19	6 41
31	5 33	6 27	5 31	6 29	5 28	6 32	5 26	6 34	5 23	6 37	5 20	6 40	5 18	6 42
32	5 32	6 28	5 29	6 31	5 27	6 33	5 24	6 36	5 21	6 39	5 19	6 41	5 16	6 44
33	5 31	6 29	5 28	6 32	5 26	6 34	5 23	6 37	5 20	6 40	5 17	6 43	5 14	6 46
34	5 30	6 30	5 27	6 33	5 24	6 36	5 21	6 39	5 18	6 42	5 15	6 45	5 12	6 48
35	5 29	6 31	5 26	6 34	5 23	6 37	5 20	6 40	5 17	6 43	5 14	6 46	5 11	6 49
36	5 28	6 32	5 24	6 36	5 21	6 39	5 18	6 42	5 15	6 45	5 12	6 48	5 9	6 51
37	5 26	6 34	5 23	6 38	5 20	6 40	5 17	6 43	5 13	6 47	5 10	6 50	5 7	6 53
38	5 25	6 35	5 22	6 39	5 18	6 42	5 15	6 45	5 12	6 48	5 8	6 52	5 5	6 55
39	5 24	6 36	5 20	6 40	5 17	6 43	5 13	6 47	5 10	6 50	5 6	6 54	5 3	6 57
40	5 22	6 38	5 19	6 43	5 15	6 45	5 12	6 48	5 8	6 52	5 4	6 56	5 1	6 59
41	5 21	6 39	5 17	6 44	5 14	6 46	5 10	6 50	5 6	6 54	5 2	6 58	4 58	7 2
42	5 20	6 40	5 16	6 44	5 12	6 48	5 8	6 52	5 4	6 56	5 0	7 0	4 56	7 4
43	5 18	6 42	5 14	6 46	5 10	6 50	5 6	6 54	5 2	6 58	4 58	7 2	4 54	7 6
44	5 17	6 43	5 13	6 47	5 8	6 52	5 4	6 56	5 0	7 0	4 56	7 4	4 51	7 9
45	5 15	6 45	5 11	6 49	5 7	6 53	5 2	6 58	4 58	7 2	4 53	7 7	4 49	7 11
46	5 14	6 46	5 9	6 51	5 5	6 55	5 0	7 0	4 56	7 4	4 51	7 9	4 46	7 14
47	5 12	6 48	5 7	6 53	5 3	6 57	4 58	7 2	4 53	7 7	4 48	7 12	4 43	7 17
48	5 10	6 50	5 5	6 55	5 1	6 59	4 56	7 4	4 51	7 9	4 46	7 14	4 41	7 19
49	5 8	6 52	5 3	6 57	4 58	7 2	4 53	7 7	4 48	7 12	4 43	7 17	4 38	7 22
50	5 6	6 54	5 1	6 59	4 56	7 4	4 51	7 9	4 46	7 14	4 40	7 20	4 35	7 25
51	5 4	6 56	4 59	7 1	4 54	7 6	4 48	7 12	4 43	7 17	4 37	7 23	4 31	7 29
52	5 2	6 58	4 57	7 3	4 51	7 9	4 46	7 14	4 40	7 20	4 34	7 26	4 28	7 32
53	5 0	7 0	4 54	7 6	4 49	7 11	4 43	7 17	4 37	7 23	4 31	7 29	4 24	7 36
54	4 58	7 2	4 52	7 8	4 46	7 14	4 40	7 20	4 33	7 27	4 27	7 33	4 20	7 40
55	4 56	7 4	4 49	7 11	4 43	7 17	4 37	7 23	4 30	7 30	4 23	7 37	4 16	7 44
56	4 53	7 7	4 47	7 13	4 40	7 20	4 33	7 27	4 26	7 34	4 19	7 41	4 12	7 48
57	4 50	7 10	4 44	7 16	4 37	7 23	4 30	7 30	4 23	7 37	4 15	7 45	4 8	7 52
58	4 47	7 13	4 40	7 20	4 33	7 27	4 26	7 34	4 18	7 42	4 11	7 49	4 3	7 57
59	4 44	7 16	4 37	7 23	4 30	7 30	4 22	7 38	4 14	7 46	4 6	7 54	3 58	8 2
60	4 41	7 19	4 34	7 26	4 26	7 34	4 18	7 42	4 9	7 51	4 1	7 59	3 52	8 8
61	4 38	7 22	4 30	7 30	4 22	7 38	4 13	7 47	4 4	7 56	3 55	8 5	3 46	8 14
62	4 34	7 26	4 26	7 34	4 17	7 43	4 8	7 52	3 59	8 1	3 49	8 11	3 40	8 20
63	4 30	7 30	4 21	7 39	4 12	7 48	4 3	7 57	3 53	8 7	3 43	8 17	3 33	8 27
64	4 26	7 34	4 17	7 43	4 7	7 53	3 57	8 3	3 47	8 13	3 36	8 24	3 25	8 35
65	4 23	7 39	4 12	7 48	4 1	7 59	3 51	8 9	3 40	8 20	3 28	8 32	3 16	8 44
66	4 18	7 42	4 6	7 54	3 55	8 5	3 44	8 16	3 32	8 28	3 20	8 40	3 7	8 53
66½	4 14	7 46	4 3	7 57	3 52	8 8	3 40	8 20	3 28	8 32	3 15	8 45	3 1	8 59
Lat.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.

Latitude and Declination of contrary Names.

TABLE 26

668

APPARENT TIME OF THE SUN'S RISING AND SETTING

DECLINATION, of the same Name as the Latitude

Lat.	18°		19°		20°		21°		22°		23°		23½°	
	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.
0°	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m	6h 0m
2	5 58	6 2	5 58	6 2	5 58	6 2	5 57	6 3	5 57	6 3	5 57	6 3	5 57	6 3
4	5 55	6 5	5 55	6 5	5 55	6 5	5 54	6 6	5 54	6 6	5 53	6 7	5 53	6 7
6	5 52	6 8	5 52	6 8	5 52	6 8	5 51	6 9	5 51	6 9	5 50	6 10	5 50	6 10
8	5 50	6 10	5 49	6 11	5 49	6 12	5 48	6 12	5 47	6 12	5 47	6 13	5 46	6 14
10	5 47	6 13	5 46	6 14	5 46	6 15	5 45	6 16	5 44	6 16	5 43	6 17	5 43	6 17
12	5 44	6 16	5 44	6 17	5 43	6 18	5 42	6 19	5 41	6 20	5 40	6 21	5 39	6 21
14	5 41	6 19	5 40	6 20	5 39	6 21	5 38	6 22	5 37	6 23	5 36	6 24	5 35	6 25
16	5 39	6 21	5 37	6 23	5 36	6 24	5 35	6 25	5 33	6 27	5 32	6 28	5 31	6 29
18	5 36	6 24	5 34	6 26	5 33	6 27	5 31	6 29	5 30	6 30	5 28	6 32	5 28	6 32
20	5 33	6 27	5 31	6 29	5 30	6 30	5 28	6 32	5 26	6 34	5 24	6 36	5 24	6 38
21	5 31	6 29	5 30	6 30	5 28	6 32	5 26	6 34	5 24	6 36	5 22	6 38	5 22	6 40
22	5 30	6 30	5 28	6 32	5 26	6 34	5 24	6 36	5 22	6 38	5 21	6 39	5 20	6 42
23	5 28	6 32	5 26	6 34	5 24	6 36	5 22	6 38	5 21	6 39	5 19	6 41	5 18	6 44
24	5 27	6 33	5 25	6 35	5 23	6 37	5 21	6 39	5 19	6 41	5 16	6 44	5 15	6 46
25	5 25	6 35	5 23	6 37	5 21	6 39	5 19	6 41	5 17	6 43	5 14	6 46	5 13	6 48
26	5 24	6 36	5 21	6 39	5 19	6 41	5 17	6 43	5 15	6 45	5 12	6 48	5 11	6 50
27	5 22	6 38	5 20	6 40	5 17	6 43	5 15	6 45	5 12	6 48	5 10	6 50	5 9	6 52
28	5 20	6 40	5 18	6 42	5 15	6 45	5 13	6 47	5 10	6 50	5 8	6 52	5 7	6 54
29	5 18	6 42	5 16	6 44	5 13	6 47	5 11	6 49	5 8	6 52	5 6	6 54	5 4	6 56
30	5 17	6 43	5 14	6 46	5 11	6 49	5 9	6 51	5 6	6 54	5 3	6 57	5 2	6 58
31	5 15	6 45	5 12	6 48	5 9	6 51	5 7	6 53	5 4	6 56	5 1	6 59	5 0	7 0
32	5 13	6 47	5 10	6 50	5 7	6 53	5 4	6 56	5 2	6 58	4 59	7 1	4 57	7 3
33	5 11	6 49	5 8	6 52	5 5	6 55	5 2	6 58	4 59	7 1	4 56	7 4	4 55	7 5
34	5 9	6 51	5 6	6 54	5 3	6 57	5 0	7 0	4 57	7 3	4 53	7 7	4 52	7 8
35	5 7	6 53	5 4	6 56	5 1	6 59	4 58	7 2	4 54	7 6	4 51	7 9	4 49	7 11
36	5 5	6 55	5 2	6 58	4 59	7 1	4 55	7 5	4 52	7 8	4 48	7 12	4 46	7 14
37	5 3	6 57	5 0	7 0	4 56	7 4	4 53	7 7	4 49	7 11	4 45	7 15	4 44	7 16
38	5 1	6 59	4 58	7 2	4 56	7 7	4 50	7 10	4 46	7 14	4 43	7 17	4 41	7 19
39	4 59	7 1	4 55	7 5	4 51	7 9	4 48	7 12	4 44	7 16	4 40	7 20	4 38	7 22
40	4 57	7 3	4 53	7 7	4 49	7 11	4 45	7 15	4 41	7 19	4 37	7 23	4 35	7 25
41	4 54	7 6	4 50	7 10	4 46	7 14	4 42	7 18	4 38	7 22	4 33	7 27	4 31	7 29
42	4 52	7 8	4 48	7 12	4 43	7 17	4 39	7 21	4 35	7 25	4 30	7 30	4 28	7 32
43	4 49	7 11	4 45	7 15	4 41	7 19	4 36	7 24	4 31	7 29	4 27	7 33	4 24	7 36
44	4 47	7 13	4 43	7 18	4 38	7 22	4 33	7 27	4 28	7 32	4 23	7 37	4 21	7 39
45	4 44	7 16	4 39	7 21	4 35	7 25	4 30	7 30	4 25	7 35	4 20	7 40	4 17	7 43
46	4 41	7 19	4 36	7 24	4 31	7 29	4 26	7 34	4 21	7 39	4 16	7 44	4 13	7 47
47	4 38	7 22	4 33	7 27	4 28	7 32	4 23	7 37	4 17	7 43	4 12	7 48	4 9	7 51
48	4 35	7 25	4 30	7 30	4 25	7 35	4 19	7 41	4 13	7 47	4 7	7 53	4 5	7 55
49	4 32	7 28	4 27	7 33	4 21	7 39	4 15	7 45	4 9	7 51	4 3	7 57	4 0	8 0
50	4 29	7 31	4 23	7 37	4 17	7 43	4 11	7 49	4 5	7 55	3 58	8 2	3 55	8 5
51	4 25	7 35	4 19	7 41	4 13	7 47	4 7	7 53	4 0	8 0	3 54	8 6	3 50	8 10
52	4 22	7 38	4 15	7 45	4 9	7 51	4 4	7 58	3 55	8 5	3 48	8 12	3 45	8 15
53	4 18	7 42	4 11	7 49	4 4	7 56	3 58	8 2	3 50	8 10	3 43	8 17	3 39	8 21
54	4 14	7 46	4 7	7 53	4 0	8 0	3 52	8 8	3 45	8 15	3 37	8 23	3 33	8 27
55	4 9	7 51	4 2	7 58	3 55	8 5	3 47	8 13	3 39	8 21	3 31	8 29	3 27	8 33
56	4 5	7 55	3 57	8 3	3 49	8 11	3 41	8 19	3 33	8 27	3 24	8 36	3 20	8 40
57	4 0	8 0	3 52	8 8	3 44	8 16	3 35	8 25	3 26	8 34	3 17	8 43	3 12	8 48
58	3 55	8 5	3 46	8 14	3 38	8 22	3 28	8 32	3 19	8 41	3 9	8 51	3 4	8 56
59	3 49	8 11	3 40	8 20	3 31	8 29	3 21	8 39	3 11	8 49	3 0	9 0	2 55	9 5
60	3 43	8 17	3 34	8 26	3 24	8 36	3 13	8 47	3 2	8 58	2 51	9 9	2 45	9 15
61	3 36	8 24	3 26	8 34	3 16	8 44	3 5	8 55	2 53	9 7	2 40	9 20	2 34	9 26
62	3 29	8 31	3 18	8 42	3 7	8 53	2 55	9 5	2 42	9 18	2 28	9 32	2 21	9 39
63	3 22	8 38	3 10	8 50	2 58	9 2	2 44	9 16	2 30	9 30	2 14	9 46	2 6	9 54
64	3 13	8 47	3 0	9 0	2 47	9 13	2 32	9 28	2 16	9 44	1 58	10 2	1 48	10 12
65	3 3	8 57	2 50	9 10	2 35	9 25	2 18	9 42	2 0	10 0	1 38	10 22	1 26	10 34
66	2 53	9 7	2 37	9 23	2 21	9 39	2 2	9 58	1 39	10 21	1 10	10 50	0 51	11 9
66½	2 46	9 14	2 30	9 30	2 12	9 48	1 51	10 9	1 26	10 34	0 48	11 12	0	12 0
Lat.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.	Sett.	Ris.

Latitude and Declination of contrary Names.

APPROXIMATE APPARENT TIMES OF THE
MERIDIAN PASSAGES OF THE PRINCIPAL FIXED STARS
ON THE FIRST DAY OF EACH MONTH, 1902.

Name	Jan.	Feb.	Mar.	April	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.
<i>h m</i>	<i>h m</i>	<i>h m</i>	<i>h m</i>	<i>h m</i>	<i>h m</i>	<i>h m</i>	<i>h m</i>	<i>h m</i>	<i>h m</i>	<i>h m</i>	<i>h m</i>	<i>h m</i>
<i>α</i> Andromeda <i>Alpheratz</i>	5 19	3 6	1 17	23 21	32 19	29 17	25 15	20 13	24 11	36 9	40 7	37 5
<i>γ</i> Pegasi <i>Algenib</i>	5 24	3 11	1 22	23 28	37 19	34 17	30 15	25 13	29 11	41 9	45 7	42 5
<i>α</i> Phoenicis	5 37	3 24	1 35	23 41	50 19	47 17	43 15	38 13	42 11	54 9	58 7	55 5
<i>α</i> Cassiopeiæ <i>Schedar</i>	5 51	3 38	1 49	23 55	22 40	17 57	15 52	13 56	12 18	10 12	8 9	
<i>β</i> Ceti <i>Deneb Kaitos</i>	5 55	3 42	1 53	23 59	22 8	5 18	1 15	56 14	0 12	12 10	16 8	13 6
<i>α</i> Ursæ Minoris <i>Polaris</i>	6 40	4 27	2 37	0 43	22 52	20 49	18 46	16 41	14 46	12 58	11 2	8 59
<i>α</i> Eridani <i>Achernar</i>	6 50	4 37	2 48	0 54	23 32	21 0 18	56 16	51 14	55 13	7 11	11 9	8 6
<i>γ</i> Andromeda <i>Almach</i>	7 14	5 1	3 12	1 18	23 27	21 24	19 17	15 15	19 13	31 11	35 9	32 7
<i>α</i> Arietis <i>Hamel</i>	7 18	5 5	3 16	1 22	23 31	21 28	19 24	17 19	15 23	13 35	11 39	9 37
<i>α</i> Ceti <i>Menkar</i>	8 13	6 0	4 11	2 17	0 26	22 23	20 19	18 14	16 18	14 30	12 34	10 31
<i>α</i> Persei <i>Mirak</i>	8 33	6 20	4 31	2 37	0 46	23 39	18 34	16 38	14 50	12 54	10 51	
<i>α</i> Tauri <i>Aldebaran</i>	9 46	7 33	5 44	3 50	1 59	23 56	21 52	19 47	17 51	16 3	14 7	12 4
<i>α</i> Aurigæ <i>Capella</i>	10 25	8 12	6 23	4 29	2 38	0 35	22 31	20 26	18 31	16 43	14 47	12 43
<i>β</i> Orionis <i>Rigel</i>	10 26	8 13	6 24	4 30	2 39	0 36	22 32	20 27	18 31	16 43	14 47	12 43
<i>β</i> Tauri <i>Nath</i>	10 36	8 23	6 34	4 40	2 49	0 46	22 42	20 37	18 41	16 53	14 57	12 54
<i>β</i> Orionis	10 43	8 30	6 41	4 47	2 56	0 53	22 49	20 44	18 48	17 0	15 4	13 1
<i>α</i> Orionis <i>Anilam</i>	10 47	8 34	6 45	4 51	3 0	0 57	22 53	20 48	18 52	17 4	15 8	13 5
<i>α</i> Columbae <i>Phact</i>	10 52	8 39	6 50	4 56	3 5	1 22	58 20	53 18	57 17	9 15	13 13	10 10
<i>α</i> Orionis <i>Betelgeuse</i>	11 6	8 53	7 4	5 10	3 19	1 16	23 12	21 7	19 17	23 15	27 13	23 10
<i>β</i> Aurigæ <i>Menkalan</i>	11 8	8 55	7 6	5 13	3 21	1 18	23 14	21 9	19 17	23 15	27 13	23 10
<i>α</i> Argus <i>Canopus</i>	11 38	9 25	7 36	5 42	3 51	1 48	23 44	21 39	19 43	17 55	15 59	13 55
<i>γ</i> Geminorum <i>Alhena</i>	11 48	9 35	7 46	5 52	4 1	1 58	23 54	21 49	19 53	18 5	16 9	14 6
<i>α</i> Canis Majoris <i>Sirius</i>	11 57	9 44	7 55	6 1	4 10	2 7	0 32	58 20	53 18	21 14	18 14	16 11
<i>α</i> Canis Majoris <i>Adara</i>	12 11	9 58	8 9	6 15	4 24	2 21	0 17	22 12	20 16	18 28	16 32	14 28
<i>α</i> Geminorum <i>Castor</i>	12 44	10 31	8 42	6 48	4 57	2 54	0 50	22 45	20 49	19 1	17 5	15 2
<i>α</i> Canis Minoris <i>Procyon</i>	12 50	10 37	8 48	6 54	5 3	3 0	0 56	22 51	20 55	19 7	17 11	15 8
<i>β</i> Geminorum <i>Pollux</i>	12 55	10 42	8 53	6 59	5 8	3 5	1 12	56 21	51 19	12 17	16 15	13 12
<i>α</i> Argus	13 16	11 3	9 14	7 20	5 29	3 26	1 22	53 17	21 19	33 17	37 15	34
<i>α</i> Argus	13 58	11 45	9 56	8 2	6 11	4 8	2 4	23 59	22 30	15 18	19 16	16
<i>α</i> Hydre <i>Alnham</i>	14 39	12 26	10 37	8 43	6 52	4 49	2 45	0 40	22 44	20 56	19 0	16 56
<i>α</i> Leonis <i>Negulus</i>	15 19	13 6	11 17	9 23	7 32	5 29	3 25	1 20	23 24	21 36	19 40	17 37
<i>γ</i> Leonis <i>Algebra</i>	15 30	13 17	11 28	9 34	7 43	5 40	3 36	1 31	23 35	21 47	19 51	17 48
<i>γ</i> Argus	15 57	13 44	11 55	10 1	8 10	6 7	4 3	1 58	0 22	14 20	18 18	15
<i>α</i> Ursæ Majoris <i>Dubhe</i>	16 13	14 0	12 11	10 17	8 26	6 23	4 19	2 14	0 18	22 30	24 18	31
<i>β</i> Leonis <i>Zosma</i>	16 25	14 12	12 23	10 29	8 38	6 35	4 31	2 26	0 30	22 42	24 30	31
<i>β</i> Leonis <i>Denebola</i>	17 0	14 47	12 58	11 4	9 13	7 10	5 6	3 1	1 53	17 21	21 19	17
<i>γ</i> Ursæ Majoris <i>Phocda</i>	17 4	14 51	13 2	11 8	9 17	7 14	5 10	3 5	1 9	23 21	25 19	21
<i>α</i> Crucis	17 37	15 24	13 35	11 41	9 50	7 47	5 43	3 38	1 42	23 54	21 58	19 54
<i>β</i> Corvi	17 45	15 32	13 43	11 49	9 58	7 55	5 51	3 46	1 50	0 22	6 20	3
<i>α</i> Canum Venaticorum	18 7	15 54	14 5	12 11	10 20	8 17	6 13	4 8	2 12	0 24	22 28	20 24
<i>α</i> Virginis <i>Spica</i>	18 36	16 23	14 34	12 40	10 49	8 46	6 42	4 37	2 41	0 53	22 57	20 53
<i>γ</i> Ursæ Majoris <i>Benetnasch</i>	19 0	16 47	14 58	13 4	11 13	9 10	7 6	5 1	3 5	1 17	23 21	21 17
<i>β</i> Centauri	19 13	17 0	15 11	13 17	11 26	9 23	7 19	5 14	3 18	1 30	23 34	21 30
<i>α</i> Draconis <i>Thuban</i>	19 18	17 5	15 16	13 21	11 31	9 28	7 24	5 19	3 23	1 35	23 39	21 35
<i>α</i> Bootis <i>Arcturus</i>	19 27	17 14	15 25	13 31	11 40	9 37	7 33	5 28	3 32	1 44	23 48	21 44
<i>α</i> Centauri	19 49	17 36	15 47	13 53	12 2	9 59	7 55	5 50	3 54	2 6	0 10	22 6
<i>α</i> Libræ <i>Zuben el Genubi</i>	20 1	17 48	15 59	14 5	12 10	11 8	7 6	5 2	3 6	2 18	0 22	22 18
<i>β</i> Ursæ Minoris <i>Kochab</i>	20 7	17 54	16 5	14 11	12 20	10 17	8 13	6 8	4 12	2 24	0 28	22 24
<i>β</i> Libræ <i>Zuben el Chamali</i>	20 28	18 15	16 26	14 32	12 41	10 38	8 34	6 29	4 33	2 45	0 49	22 45
<i>α</i> Coronæ Borealis <i>Alphacca</i>	20 47	18 34	16 45	14 51	13 0	10 57	8 53	6 48	4 52	3 4	1 8	23 4
<i>α</i> Serpentis <i>Unukalhas</i>	20 55	18 42	16 53	14 59	13 8	11 5	9 1	6 56	5 0	3 12	1 16	23 12
<i>β</i> Scorpii	21 15	19 2	17 13	15 19	13 28	11 25	9 21	7 16	5 30	3 32	1 36	23 32
<i>α</i> Scorpii <i>Antares</i>	21 39	26 17	24 28	22 34	20 41	18 38	16 34	14 30	12 26	10 22	8 18	6 14
<i>α</i> Trianguli Australis	21 54	19 41	17 52	15 58	14 7	12 4	10 0	7 55	5 59	4 11	2 15	0 11
<i>β</i> Draconis <i>Alcoid</i>	22 44	20 31	18 42	16 48	14 57	12 55	10 50	8 45	6 49	5 1	3 5	1 8
<i>α</i> Ophiuchi <i>Ras Alhague</i>	22 46	20 33	18 44	16 50	14 59	12 57	10 52	8 47	6 51	5 3	3 7	1 4
<i>γ</i> Draconis <i>Rastaban</i>	23 10	20 58	19 8	17 15	15 23	13 21	11 16	9 11	7 15	5 27	3 31	1 28
<i>α</i> Lyræ <i>Vega</i>	23 49	21 37	19 47	17 54	16 3	14 0	11 56	9 51	7 55	6 7	4 11	2 7
<i>α</i> Aquilæ <i>Altair</i>	1 22	49 20	59 19	6 17	15 15	13 13	11 8	9 11	7 19	5 23	3 20	1 17
<i>α</i> Pavonis	1 34	23 21	31 19	38 17	47 15	44 13	40 11	35 9	39 7	51 5	55 3	51 1
<i>α</i> Cygni <i>Deneb</i>	1 54	23 41	31 29	38 27	47 25	44 23	40 21	35 19	39 17	51 15	55 13	51 11
<i>α</i> Cephei <i>Alderamin</i>	2 32	0 19	22 30	26 18	45 16	42 14	38 12	33 10	37 8	49 6	53 4	50 2
<i>α</i> Pegasi	2 55	0 42	22 53	26 41	45 29	42 27	38 25	33 23	37 21	49 19	53 17	50 15
<i>α</i> Græis	3 18	1 5	23 12	21 22	39 11	37 20	34 18	31 16	28 14	40 12	44 10	41 8
<i>β</i> Græis	3 53	1 40	23 51	21 57	40 18	38 27	35 25	32 23	29 21	41 19	45 17	42 15
<i>α</i> Piscis Auct.	4 8	1 55	0 6	24 12	20 21	18 18	16 14	14 12	12 10	25 8	29 6	26 4
<i>α</i> Pegasi <i>Markab</i>	4 16	2 3	0 14	22 20	20 29	18 26	16 22	14 17	12 12	23 10	27 8	24 6

TABLE 27 A

665

CORRECTION OF THE TIMES IN TABLE 27 FOR THE DAY OF THE MONTH, To be Subtracted.												
Days.	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.
1	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0
2	0 4	0 4	0 4	0 4	0 4	0 4	0 4	0 4	0 4	0 4	0 4	0 4
3	0 9	0 8	0 7	0 7	0 8	0 8	0 8	0 8	0 7	0 7	0 8	0 9
4	0 13	0 12	0 11	0 11	0 11	0 12	0 12	0 12	0 11	0 11	0 12	0 13
5	0 18	0 16	0 15	0 15	0 15	0 16	0 16	0 15	0 14	0 15	0 16	0 17
6	0 22	0 20	0 19	0 18	0 19	0 21	0 21	0 19	0 18	0 18	0 20	0 22
7	0 26	0 24	0 22	0 22	0 23	0 25	0 25	0 23	0 22	0 22	0 24	0 26
8	0 30	0 28	0 26	0 26	0 27	0 29	0 29	0 27	0 25	0 25	0 28	0 30
9	0 35	0 32	0 30	0 29	0 30	0 33	0 33	0 31	0 29	0 29	0 32	0 35
10	0 39	0 36	0 33	0 33	0 35	0 37	0 37	0 35	0 32	0 33	0 36	0 39
11	0 43	0 40	0 37	0 36	0 39	0 41	0 41	0 38	0 36	0 37	0 40	0 44
12	0 48	0 44	0 41	0 40	0 42	0 45	0 45	0 42	0 40	0 40	0 44	0 48
13	0 52	0 48	0 44	0 44	0 46	0 49	0 49	0 46	0 43	0 44	0 48	0 52
14	0 56	0 52	0 48	0 48	0 50	0 54	0 53	0 50	0 47	0 48	0 52	0 57
15	1 1	0 56	0 52	0 51	0 54	0 58	0 57	0 53	0 50	0 51	0 56	1 1
16	1 5	1 0	0 55	0 55	0 58	1 2	1 1	0 57	0 54	0 55	1 0	1 6
17	1 9	1 3	0 59	0 59	1 2	1 6	1 5	1 1	0 58	0 59	1 4	1 10
18	1 13	1 7	1 2	1 2	1 6	1 10	1 9	1 5	1 1	1 3	1 9	1 15
19	1 18	1 11	1 6	1 6	1 10	1 14	1 13	1 8	1 5	1 6	1 13	1 19
20	1 22	1 15	1 10	1 10	1 14	1 19	1 17	1 12	1 8	1 10	1 17	1 24
21	1 26	1 19	1 14	1 13	1 18	1 23	1 21	1 16	1 12	1 14	1 21	1 28
22	1 31	1 23	1 17	1 17	1 22	1 27	1 25	1 19	1 16	1 18	1 25	1 32
23	1 35	1 26	1 21	1 21	1 26	1 31	1 29	1 23	1 19	1 21	1 30	1 37
24	1 39	1 30	1 24	1 25	1 30	1 35	1 33	1 27	1 23	1 25	1 34	1 41
25	1 43	1 34	1 28	1 28	1 34	1 39	1 37	1 31	1 26	1 29	1 38	1 46
26	1 47	1 38	1 32	1 32	1 38	1 44	1 41	1 34	1 30	1 33	1 42	1 50
27	1 51	1 42	1 35	1 36	1 42	1 48	1 45	1 38	1 34	1 37	1 47	1 55
28	1 56	1 45	1 39	1 40	1 46	1 52	1 49	1 42	1 37	1 41	1 51	1 59
29	2 0		1 43	1 44	1 50	1 56	1 53	1 45	1 41	1 44	1 55	2 3
30	2 4		1 46	1 47	1 53	2 0	1 57	1 49	1 44	1 48	1 59	2 8
31	2 8		1 50		1 59		2 1	1 52		1 52		2 12

TABLE 28

CORRECTION OF THE TIME OF THE MOON'S MER. PASSAGE															Long. in time.
Long.	Daily Variation of the Moon's Meridian Passage														
	40"	42"	44"	46"	48"	50"	52"	54"	56"	58"	60"	62"	64"	66"	H. M.
5°	1"	1"	1"	1"	1"	1"	1"	1"	1"	1"	1"	1"	1"	1"	0 20
10	1	1	1	1	1	1	1	1	2	2	2	2	2	2	0 40
20	2	2	2	3	3	3	3	3	3	3	3	3	4	4	1 20
30	3	3	4	4	4	4	4	4	5	5	5	5	5	5	2 0
40	4	5	5	5	5	5	6	6	6	6	7	7	7	7	2 40
50	6	6	6	6	7	7	7	7	8	8	8	9	9	9	3 20
60	7	7	7	8	8	8	9	9	9	10	10	10	11	11	4 0
70	8	8	9	9	9	10	10	10	11	11	12	12	13	13	4 40
80	9	9	10	10	11	11	12	12	12	13	13	14	14	15	5 20
90	10	10	11	11	12	12	13	13	14	14	15	15	16	16	6 0
100	11	12	12	13	13	14	14	15	16	16	17	17	18	18	6 40
110	12	13	13	14	15	15	16	16	17	18	18	19	20	20	7 20
120	13	14	15	15	16	17	17	18	19	19	20	21	21	22	8 0
130	14	15	16	17	17	18	19	19	20	21	22	22	23	24	8 40
140	16	16	17	18	19	19	20	21	22	23	23	24	25	26	9 20
150	17	17	18	19	20	21	22	22	23	24	25	26	27	27	10 0
160	18	18	20	20	21	22	23	24	25	26	27	28	28	29	10 40
170	19	20	21	22	23	24	25	25	26	27	28	29	30	31	11 20
180	20	21	22	23	24	25	26	27	28	29	30	31	32	33	12 0

HOUR ANGLE AND ALTITUDE OF A BODY UPON THE PRIME VERTICAL

Lat.	DECLINATION															
	1°		2°		3°		4°		5°		6°		7°		8°	
	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.
0	4 0	30°0														
2	4 0	30°0														
3	4 42	19°5	3 13	41°8												
4	5 2	14°5	4 0	30°0	2 46	48°6										
5	5 14	11°5	4 26	23°6	3 33	36°9	2 28	53°2								
6	5 22	9°6	4 42	19°5	4 0	30°0	3 13	41°8	2 15	56°4						
7	5 27	8°2	4 54	16°6	4 19	25°4	3 42	34°9	2 58	45°7	2 4	59°1				
8	5 31	7°2	5 2	14°5	4 32	22°1	4 1	30°1	3 26	38°6	2 46	48°7	1 56	61°1		
9	5 35	6°4	5 9	12°8	4 43	19°5	4 15	26°5	3 46	33°8	3 14	41°9	2 37	51°2	1 50	62°8
10	5 37	5°8	5 14	11°6	4 51	17°3	4 27	23°7	4 1	30°1	3 34	37°0	3 3	44°6	2 29	53°3
11	5 39	5°3	5 19	10°5	4 57	15°9	4 36	21°6	4 13	27°2	3 49	33°1	3 23	39°7	2 55	46°8
12	5 41	4°8	5 22	9°6	5 3	14°6	4 43	19°6	4 23	24°8	4 1	30°2	3 39	35°9	3 14	42°0
13	5 43	4°5	5 25	8°9	5 8	13°4	4 49	18°1	4 31	22°8	4 12	27°7	3 51	32°8	3 30	38°2
14	5 44	4°1	5 28	8°3	5 11	12°5	4 55	16°8	4 38	21°1	4 20	25°6	4 2	30°2	3 43	35°1
15	5 45	3°9	5 30	7°7	5 15	11°7	4 59	15°6	4 44	19°7	4 28	23°8	4 11	28°1	3 53	32°5
16	5 46	3°6	5 32	7°3	5 18	10°9	5 4	14°7	4 49	18°4	4 34	22°3	4 19	25°2	4 3	30°3
17	5 47	3°4	5 34	6°8	5 21	10°3	5 7	13°8	4 53	17°3	4 40	20°9	4 25	24°6	4 10	28°4
18	5 48	3°2	5 35	6°5	5 23	9°7	5 10	13°1	4 58	16°4	4 44	19°8	4 31	23°2	4 17	26°8
19	5 48	3°1	5 37	6°2	5 25	9°2	5 13	12°4	5 1	15°5	4 49	18°7	4 36	22°0	4 24	25°3
20	5 49	2°9	5 38	5°8	5 27	8°8	5 15	11°8	5 4	14°8	4 53	17°8	4 41	20°8	4 29	24°0
21	5 50	2°8	5 39	5°6	5 29	8°4	5 18	11°2	5 7	14°1	4 56	17°0	4 45	19°8	4 35	22°8
22	5 50	2°7	5 40	5°3	5 30	8°0	5 20	10°7	5 10	13°4	5 0	16°2	4 49	19°0	4 39	21°8
23	5 51	2°6	5 41	5°1	5 32	7°7	5 22	10°3	5 12	12°8	5 3	15°5	4 53	18°2	4 43	20°8
24	5 51	2°5	5 42	4°9	5 33	7°4	5 24	9°8	5 15	12°4	5 5	14°9	4 56	17°4	4 46	20°0
25	5 51	2°4	5 43	4°7	5 34	7°1	5 25	9°5	5 17	11°9	5 8	14°3	4 59	16°8	4 50	19°2
26	5 52	2°3	5 44	4°6	5 35	6°8	5 27	9°1	5 19	11°5	5 10	13°8	5 2	16°1	4 53	18°5
27	5 52	2°2	5 44	4°4	5 36	6°6	5 28	8°8	5 20	11°1	5 12	13°3	5 4	15°5	4 56	17°8
28	5 52	2°1	5 45	4°3	5 37	6°4	5 30	8°5	5 22	10°7	5 14	12°8	5 7	15°0	4 59	17°2
29	5 53	2°1	5 45	4°1	5 38	6°2	5 31	8°2	5 24	10°3	5 16	12°4	5 9	14°6	5 1	16°7
30	5 53	2°0	5 46	4°0	5 39	6°0	5 32	8°0	5 25	10°0	5 18	12°1	5 11	14°1	5 4	16°2
31	5 53	2°0	5 47	3°8	5 40	5°8	5 33	7°8	5 27	9°7	5 20	11°7	5 13	13°7	5 6	15°7
32	5 54	1°9	5 47	3°8	5 41	5°7	5 34	7°6	5 28	9°5	5 21	11°4	5 15	13°3	5 8	15°2
33	5 54	1°8	5 48	3°7	5 41	5°5	5 35	7°4	5 29	9°2	5 23	11°1	5 16	12°9	5 10	14°8
34	5 54	1°8	5 48	3°6	5 42	5°4	5 36	7°2	5 30	9°0	5 24	10°8	5 18	12°6	5 12	14°4
35	5 54	1°8	5 49	3°5	5 43	5°3	5 37	7°0	5 31	8°7	5 25	10°5	5 20	12°3	5 14	14°0
36	5 54	1°7	5 49	3°4	5 43	5°1	5 38	6°8	5 32	8°5	5 27	10°2	5 21	12°0	5 15	13°7
37	5 55	1°7	5 49	3°3	5 44	5°0	5 39	6°7	5 33	8°3	5 28	10°0	5 22	11°7	5 17	13°4
38	5 55	1°6	5 50	3°2	5 45	4°8	5 39	6°5	5 34	8°1	5 29	9°8	5 24	11°4	5 19	13°1
39	5 55	1°6	5 50	3°2	5 45	4°8	5 40	6°4	5 35	8°0	5 30	9°6	5 25	11°2	5 20	12°8
40	5 55	1°5	5 50	3°1	5 46	4°7	5 41	6°2	5 36	7°8	5 31	9°4	5 26	10°9	5 21	12°5
41	5 55	1°5	5 51	3°0	5 46	4°6	5 42	6°1	5 37	7°6	5 32	9°2	5 28	10°7	5 23	12°2
42	5 56	1°5	5 51	3°0	5 47	4°5	5 42	6°0	5 38	7°5	5 33	9°0	5 29	10°5	5 24	12°0
43	5 56	1°5	5 51	2°9	5 47	4°4	5 43	5°9	5 38	7°3	5 34	8°8	5 30	10°3	5 25	11°8
44	5 56	1°4	5 52	2°8	5 48	4°3	5 43	5°8	5 39	7°2	5 35	8°6	5 31	10°1	5 27	11°5
45	5 56	1°4	5 52	2°8	5 48	4°2	5 44	5°7	5 40	7°1	5 36	8°5	5 32	9°9	5 28	11°3
46	5 56	1°4	5 52	2°8	5 48	4°2	5 45	5°6	5 41	7°0	5 37	8°4	5 33	9°7	5 29	11°1
47	5 56	1°4	5 53	2°7	5 49	4°1	5 45	5°5	5 41	6°8	5 37	8°2	5 34	9°6	5 30	11°0
48	5 56	1°3	5 53	2°7	5 49	4°0	5 46	5°4	5 42	6°7	5 38	8°1	5 35	9°4	5 31	10°8
49	5 57	1°3	5 53	2°6	5 50	4°0	5 46	5°3	5 43	6°6	5 39	8°0	5 36	9°3	5 32	10°6
50	5 57	1°3	5 53	2°6	5 50	3°9	5 47	5°2	5 43	6°5	5 40	7°8	5 36	9°1	5 33	10°5
51	5 57	1°3	5 54	2°6	5 50	3°8	5 47	5°1	5 44	6°4	5 40	7°7	5 37	9°0	5 34	10°3
52	5 57	1°3	5 54	2°5	5 51	3°8	5 47	5°1	5 44	6°3	5 41	7°6	5 38	8°9	5 35	10°2
53	5 57	1°3	5 54	2°5	5 51	3°8	5 48	5°0	5 45	6°3	5 42	7°5	5 39	8°8	5 36	10°0
54	5 57	1°2	5 54	2°5	5 51	3°7	5 48	5°0	5 45	6°2	5 42	7°4	5 40	8°6	5 37	9°9
55	5 57	1°2	5 54	2°4	5 52	3°7	5 49	4°9	5 46	6°1	5 43	7°3	5 41	8°5	5 37	9°8
56	5 57	1°2	5 55	2°4	5 52	3°6	5 49	4°8	5 46	6°0	5 44	7°2	5 41	8°4	5 38	9°6
57	5 57	1°2	5 55	2°4	5 52	3°6	5 50	4°8	5 47	6°0	5 45	7°1	5 42	8°3	5 39	9°5
58	5 57	1°2	5 55	2°4	5 52	3°5	5 50	4°7	5 47	5°8	5 45	7°1	5 42	8°3	5 40	9°4
59	5 58	1°2	5 55	2°3	5 53	3°5	5 50	4°7	5 48	5°8	5 46	7°0	5 43	8°2	5 41	9°3
60	5 58	1°1	5 55	2°3	5 53	3°5	5 51	4°6	5 48	5°8	5 46	6°9	5 44	8°1	5 41	9°2
61	5 59	1°1	5 56	2°3	5 53	3°4	5 51	4°6	5 49	5°7	5 47	6°8	5 44	8°0	5 42	9°1

HOUR ANGLE AND ALTITUDE OF A BODY UPON THE PRIME VERTICAL

Lat.	DECLINATION															
	1°		2°		3°		4°		5°		6°		7°		8°	
	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.
62	5 58	1°1	5 56	2°3	5 54	3°4	5 52	4°5	5 49	5°7	5 47	6°8	5 45	7°9	5 43	9°1
63	5 58	1°1	5 56	2°2	5 54	3°4	5 52	4°5	5 50	5°6	5 48	6°7	5 46	7°8	5 44	9°0
64	5 58	1°1	5 56	2°2	5 54	3°3	5 52	4°4	5 50	5°6	5 48	6°7	5 46	7°8	5 44	8°9
65	5 58	1°1	5 56	2°2	5 54	3°3	5 53	4°4	5 51	5°5	5 49	6°6	5 47	7°7	5 45	8°8
66	5 58	1°1	5 56	2°2	5 55	3°3	5 53	4°4	5 51	5°5	5 49	6°6	5 47	7°7	5 46	8°7
67	5 58	1°1	5 57	2°2	5 55	3°2	5 53	4°3	5 51	5°4	5 50	6°5	5 48	7°6	5 46	8°7
68	5 58	1°1	5 57	2°1	5 55	3°2	5 54	4°3	5 52	5°4	5 50	6°5	5 49	7°5	5 47	8°6
69	5 58	1°1	5 57	2°1	5 55	3°2	5 54	4°3	5 52	5°4	5 51	6°4	5 49	7°5	5 48	8°6
70	5 59	1°1	5 57	2°1	5 56	3°2	5 54	4°2	5 53	5°3	5 51	6°4	5 50	7°4	5 48	8°5
10	1 44	64°3														
11	2 22	55°1	1 40	65°5												
12	2 47	48°8	2 16	56°6	1 35	66°6										
13	3 7	44°1	2 41	50°5	2 11	58°0	1 32	67°5								
14	3 32	40°3	3 0	45°9	2 35	52°1	2 6	59°2	1 29	68°5						
15	3 35	37°2	3 16	42°1	2 54	47°5	2 30	53°4	2 2	60°3	1 26	69°2				
16	3 46	34°6	3 28	39°1	3 9	43°8	2 49	49°0	2 26	54°7	1 58	61°4	1 23	69°9		
17	3 55	32°3	3 39	36°4	3 22	40°7	3 4	45°3	2 24	50°3	2 21	55°8	1 55	62°3	1 21	70°5
18	4 3	30°4	3 49	34°2	3 33	38°1	3 17	42°3	2 59	46°7	2 40	51°5	2 18	56°8	1 52	63°1
19	4 10	28°7	3 57	32°2	3 43	35°8	3 28	39°7	3 12	43°7	2 54	48°0	2 36	52°6	2 14	57°8
20	4 17	27°2	4 4	30°5	3 51	33°9	3 37	37°4	3 23	41°1	3 7	45°0	2 50	49°2	2 32	53°7
21	4 23	25°8	4 11	29°0	3 58	32°2	3 46	35°5	3 32	38°8	3 18	42°5	3 3	46°2	2 47	50°3
22	4 28	24°7	4 16	27°3	4 5	30°6	3 53	33°7	3 41	36°9	3 28	40°2	3 14	43°7	2 59	47°4
23	4 32	23°6	4 22	26°4	4 11	29°2	4 0	32°1	3 48	35°1	3 36	38°2	3 23	40°3	3 10	44°9
24	4 37	22°6	4 27	25°3	4 16	28°0	4 6	30°7	3 55	33°6	3 44	36°5	3 32	39°5	3 20	42°7
25	4 41	21°7	4 31	24°3	4 21	26°8	4 12	29°5	4 1	32°1	3 51	34°9	3 40	37°8	3 28	40°7
26	4 44	20°9	4 35	23°3	4 26	25°8	4 17	28°3	4 7	30°8	3 57	33°5	3 47	36°2	3 36	39°0
27	4 48	20°1	4 39	22°5	4 30	24°8	4 21	27°2	4 12	29°7	4 3	32°2	3 54	34°8	3 43	37°4
28	4 51	19°5	4 43	21°7	4 34	24°0	4 26	26°3	4 17	28°6	4 8	31°0	3 59	33°4	3 49	35°9
29	4 54	18°3	4 46	21°0	4 38	23°2	4 30	25°4	4 22	27°6	4 13	29°9	4 4	32°1	3 55	34°6
30	4 56	18°2	4 49	20°3	4 41	22°4	4 34	24°6	4 26	26°7	4 18	28°9	4 9	31°2	4 1	33°4
31	4 59	17°7	4 52	19°7	4 44	21°7	4 37	23°8	4 30	25°9	4 22	28°0	4 14	30°2	4 6	32°4
32	5 1	17°2	4 54	19°1	4 47	21°1	4 40	23°1	4 33	25°4	4 26	27°2	4 18	29°2	4 11	31°3
33	5 4	16°7	4 57	18°6	4 50	20°5	4 44	22°4	4 37	24°4	4 30	26°4	4 22	28°4	4 15	30°4
34	5 6	16°2	4 59	18°1	4 53	19°9	4 47	21°8	4 40	23°7	4 33	25°5	4 26	27°6	4 19	29°5
35	5 8	15°8	5 2	17°6	4 56	19°4	4 49	21°2	4 43	23°1	4 37	24°9	4 30	26°8	4 23	28°7
36	5 10	15°4	5 4	17°2	4 58	18°9	4 52	20°7	4 46	22°5	4 40	24°3	4 33	26°1	4 27	28°0
37	5 11	15°1	5 6	16°8	5 0	18°5	4 54	20°2	4 49	21°9	4 43	23°7	4 37	25°5	4 31	27°2
38	5 13	14°7	5 8	16°4	5 3	18°6	4 57	19°7	4 51	21°4	4 46	23°1	4 40	24°5	4 34	26°6
39	5 15	14°4	5 10	16°0	5 4	18°5	4 59	19°3	4 54	20°9	4 48	22°6	4 43	24°3	4 38	26°0
40	5 16	14°1	5 11	15°7	5 6	17°3	5 1	18°8	4 56	20°5	4 51	22°1	4 46	23°7	4 40	25°4
41	5 18	13°8	5 13	15°3	5 8	16°9	5 3	18°5	4 58	20°0	4 53	21°6	4 48	23°2	4 43	24°8
42	5 19	13°5	5 15	15°2	5 10	16°6	5 5	18°1	5 1	19°6	4 56	21°2	4 51	22°9	4 46	24°3
43	5 21	13°3	5 16	14°7	5 12	16°2	5 7	17°7	5 3	19°3	4 58	20°8	4 53	22°3	4 48	23°8
44	5 22	13°0	5 18	14°5	5 14	15°9	5 9	17°4	5 5	18°9	5 0	10°4	4 56	21°8	4 51	23°4
45	5 24	12°8	5 19	14°2	5 15	15°7	5 11	17°1	5 7	18°5	5 2	20°0	4 58	21°5	4 53	22°9
46	5 25	12°6	5 21	14°0	5 17	15°4	5 13	16°8	5 8	18°2	5 4	19°6	5 0	21°1	4 56	22°5
47	5 26	12°3	5 22	13°7	5 18	15°1	5 14	16°5	5 10	17°9	5 6	19°3	5 2	20°7	4 58	22°1
48	5 27	12°1	5 23	13°5	5 20	14°8	5 16	16°2	5 12	17°6	5 8	19°0	5 4	20°4	5 0	21°8
49	5 28	12°0	5 25	13°3	5 21	14°6	5 17	16°0	5 14	17°3	5 10	18°7	5 6	20°1	5 2	21°4
50	5 29	11°8	5 26	13°2	5 22	14°4	5 19	15°7	5 15	17°1	5 12	18°4	5 8	19°7	5 4	21°1
51	5 31	11°6	5 27	12°9	5 24	14°2	5 20	15°5	5 17	16°8	5 13	18°1	5 10	19°4	5 6	20°8
52	5 32	11°4	5 28	12°7	5 25	14°0	5 22	15°3	5 18	16°6	5 15	17°8	5 12	19°2	5 8	20°5
53	5 33	11°3	5 29	12°6	5 26	13°8	5 23	15°2	5 20	16°4	5 17	17°6	5 14	18°9	5 10	20°2
54	5 34	11°1	5 31	12°4	5 28	13°6	5 24	14°8	5 21	16°1	5 18	17°4	5 16	18°7	5 12	19°9
55	5 35	11°0	5 32	12°2	5 29	13°5	5 26	14°7	5 23	15°9	5 20	17°2	5 17	18°4	5 14	19°7
56	5 35	10°8	5 33	12°1	5 30	13°3	5 27	14°5	5 24	15°7	5 21	17°0	5 18	18°2	5 16	19°4
57	5 36	10°7	5 34	11°9	5 31	13°2	5 28	14°3	5 26	15°6	5 23	16°8	5 20	18°0	5 17	19°2
58	5 37	10°6	5 35	11°8	5 33	13°0	5 29	14°2	5 27	15°4	5 24	16°6	5 22	17°8	5 19	19°0

HOUR ANGLE AND ALTITUDE OF A BODY UPON THE PRIME VERTICAL

Lat.	DECLINATION															
	9°		10°		11°		12°		13°		14°		15°		16°	
	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.
59	5 38	10.5	5 36	11.7	5 33	12.8	5 31	14.0	5 28	15.2	5 26	16.4	5 23	17.6	5 20	18.8
60	5 39	10.4	5 37	11.6	5 34	12.7	5 32	13.8	5 29	15.0	5 27	16.2	5 24	17.4	5 22	18.6
61	5 40	10.3	5 38	11.4	5 35	12.6	5 33	13.7	5 31	14.9	5 28	16.0	5 26	17.2	5 23	18.4
62	5 41	10.2	5 39	11.3	5 36	12.5	5 34	13.6	5 32	14.8	5 30	15.9	5 27	17.0	5 25	18.2
63	5 41	10.1	5 39	11.2	5 37	12.4	5 35	13.5	5 33	14.6	5 31	15.7	5 29	16.8	5 26	18.0
64	5 42	10.0	5 40	11.1	5 38	12.2	5 36	13.4	5 34	14.5	5 32	15.6	5 30	16.7	5 28	17.8
65	5 43	9.9	5 41	11.0	5 39	12.1	5 37	13.3	5 35	14.4	5 33	15.5	5 31	16.6	5 29	17.7
66	5 44	9.8	5 42	10.9	5 40	12.0	5 38	13.2	5 36	14.2	5 34	15.3	5 33	16.4	5 31	17.6
67	5 45	9.8	5 43	10.8	5 41	12.0	5 39	13.0	5 37	14.1	5 36	15.2	5 34	16.3	5 32	17.4
68	5 45	9.7	5 44	10.8	5 42	11.9	5 40	13.0	5 39	14.0	5 37	15.1	5 35	16.2	5 33	17.3
69	5 46	9.6	5 44	10.7	5 43	11.8	5 41	12.8	5 40	13.9	5 38	15.0	5 36	16.1	5 35	17.2
70	5 47	9.6	5 45	10.6	5 44	11.7	5 42	12.8	5 41	13.8	5 39	14.9	5 37	16.0	5 35	17.0
18	1 19	72.0														
19	1 50	63.9														
20	2 11	58.7	1 17	71.6												
21	2 29	54.8	2 9	59.6	1 16	72.1										
22	2 43	51.3	2 26	55.6	1 45	65.3	1 14	72.6								
23	2 56	48.4	2 40	52.3	1 43	60.3	1 43	61.1	1 13	73.1						
24	3 7	46.0	2 53	49.4	2 37	53.2	2 21	57.2	2 2	61.8	1 11	73.5				
25	3 16	43.8	3 3	47.0	2 50	50.4	2 35	54.0	2 18	58.0	2 0	62.4	1 10	73.9		
26	3 25	41.8	3 13	44.8	3 0	48.0	2 47	51.3	2 32	54.8	2 16	58.7	1 58	63.0	1 9	74.3
27	3 33	40.1	3 22	42.9	3 10	45.8	2 58	48.8	2 44	52.1	2 30	55.6	2 14	59.4	1 56	63.6
28	3 40	38.5	3 29	41.2	3 19	43.9	3 7	46.8	2 55	49.8	2 42	52.9	2 28	56.3	2 13	60.0
29	3 47	37.1	3 36	39.6	3 26	42.2	3 16	44.8	3 5	47.7	2 53	50.6	2 40	53.7	2 26	57.0
30	3 52	35.8	3 43	38.2	3 34	40.6	3 24	43.2	3 13	45.8	3 2	48.5	2 51	51.4	2 38	54.4
31	3 58	34.6	3 49	36.8	3 40	39.2	3 31	41.6	3 23	44.1	3 11	46.7	3 0	49.3	2 48	52.1
32	4 3	33.5	3 55	35.7	3 46	37.9	3 37	40.2	3 28	42.6	3 19	45.0	3 9	47.5	2 58	50.1
33	4 8	32.5	4 0	34.6	3 52	36.7	3 44	38.8	3 36	41.1	3 26	43.4	3 17	45.8	3 7	48.1
34	4 12	31.5	4 5	33.5	3 57	35.6	3 49	37.7	3 41	39.8	3 33	42.1	3 24	44.3	3 15	46.7
35	4 16	30.6	4 9	32.6	4 0	34.3	3 55	36.6	3 47	38.7	3 39	40.6	3 31	42.9	3 23	45.2
36	4 20	29.8	4 14	31.7	4 0	33.6	4 0	35.6	3 52	37.7	3 45	39.6	3 37	41.7	3 29	44.3
37	4 24	29.1	4 18	30.9	4 11	32.7	4 4	34.6	3 57	36.6	3 50	38.5	3 43	40.5	3 35	43.5
38	4 28	28.3	4 22	30.1	4 15	31.9	4 9	33.7	4 0	35.6	3 55	37.5	3 49	39.4	3 41	41.4
39	4 31	27.7	4 25	29.4	4 19	31.1	4 13	32.9	4 7	34.7	4 0	36.5	3 54	38.4	3 47	40.3
40	4 35	27.0	4 29	28.7	4 23	30.4	4 17	32.1	4 11	33.8	4 5	35.6	3 58	37.4	3 52	39.2
41	4 38	26.5	4 32	28.1	4 27	29.7	4 21	31.4	4 15	33.2	4 10	34.8	4 3	36.5	3 57	38.3
42	4 41	25.9	4 35	26.9	4 30	29.1	4 25	30.7	4 19	32.4	4 13	34.0	4 7	35.7	4 1	37.4
43	4 43	25.4	4 38	26.6	4 33	28.5	4 28	30.1	4 23	31.7	4 17	33.3	4 12	34.9	4 6	36.6
44	4 46	24.8	4 41	26.2	4 36	27.9	4 31	29.5	4 26	31.1	4 21	32.6	4 16	34.2	4 10	35.8
45	4 49	24.4	4 44	25.9	4 39	27.4	4 35	28.9	4 30	30.4	4 25	32.0	4 20	33.5	4 14	35.1
46	4 51	24.0	4 47	25.4	4 42	26.9	4 38	28.4	4 33	29.8	4 28	31.4	4 23	32.9	4 18	34.4
47	4 54	23.6	4 49	25.0	4 45	26.4	4 41	27.9	4 36	29.3	4 31	30.8	4 27	32.3	4 22	33.8
48	4 56	23.2	4 52	24.6	4 48	25.9	4 43	27.4	4 39	28.8	4 35	30.3	4 30	31.7	4 25	33.2
49	4 58	22.8	4 54	24.2	4 50	25.5	4 46	26.9	4 42	28.3	4 38	29.7	4 33	31.2	4 29	32.6
50	5 1	22.4	4 57	23.8	4 53	25.1	4 49	26.5	4 45	27.9	4 41	29.3	4 37	30.7	4 32	32.1
51	5 3	22.1	4 59	23.4	4 55	24.8	4 51	26.1	4 48	27.5	4 44	28.8	4 40	30.1	4 35	31.6
52	5 5	21.8	5 1	23.1	4 58	24.4	4 54	25.7	4 50	27.0	4 46	28.4	4 43	29.7	4 39	31.1
53	5 7	21.5	5 3	22.8	5 0	24.0	4 56	25.4	4 53	26.6	4 49	28.0	4 45	29.3	4 42	30.7
54	5 9	21.2	5 5	22.4	5 2	23.7	4 59	25.0	4 55	26.3	4 52	27.6	4 48	28.9	4 44	30.2
55	5 11	20.9	5 7	22.1	5 4	23.4	5 1	24.7	4 58	25.9	4 54	27.2	4 51	28.5	4 47	29.8
56	5 12	20.6	5 9	21.9	5 6	23.1	5 3	24.4	5 0	25.6	4 57	26.8	4 53	28.1	4 51	29.4
57	5 14	20.4	5 11	21.6	5 8	22.8	5 5	24.1	5 2	25.3	4 59	26.5	4 56	27.8	4 53	29.0
58	5 16	20.2	5 13	21.4	5 10	22.6	5 7	23.8	5 4	25.0	5 1	26.2	4 58	27.4	4 55	28.7
59	5 18	19.9	5 15	21.1	5 12	22.3	5 9	23.5	5 7	24.7	5 4	25.9	5 1	27.1	4 58	28.3
60	5 19	19.7	5 17	20.9	5 14	22.1	5 11	23.3	5 9	24.4	5 6	25.6	5 3	26.8	5 0	27.0
61	5 21	19.5	5 18	20.7	5 16	21.8	5 13	23.0	5 11	24.2	5 8	25.4	5 6	26.5	5 3	26.7
62	5 23	19.3	5 20	20.5	5 18	21.6	5 15	22.8	5 13	23.9	5 10	25.1	5 8	26.3	5 5	27.4
63	5 24	19.1	5 22	20.3	5 20	21.4	5 17	22.6	5 15	23.7	5 12	24.8	5 10	26.0	5 8	27.2
64	5 26	19.0	5 24	20.1	5 21	21.2	5 19	22.4	5 17	23.5	5 15	24.6	5 12	25.8	5 10	26.9

HOUR ANGLE AND ALTITUDE OF A BODY UPON THE PRIME VERTICAL

Lat.	DECLINATION															
	17°		18°		19°		20°		21°		22°		23°		24°	
	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.
66	5 27	18°8	5 25	19°9	5 23	21°0	5 21	22°2	5 19	23°3	5 17	24°4	5 14	25°5	5 12	26°7
67	5 25	18°7	5 27	19°8	5 24	20°8	5 23	22°0	5 21	23°1	5 19	24°2	5 16	25°3	5 14	26°4
68	5 30	18°5	5 18	19°6	5 26	20°7	5 24	21°8	5 22	22°9	5 20	24°0	5 18	25°1	5 16	26°2
69	5 32	18°4	5 30	19°5	5 28	20°5	5 26	21°6	5 24	22°7	5 22	23°8	5 20	24°9	5 19	26°0
70	5 33	18°2	5 31	19°3	5 30	20°4	5 28	21°5	5 26	22°6	5 24	23°6	5 22	24°7	5 21	25°8
	5 34	18°1	5 33	19°2	5 31	20°3	5 30	21°3	5 28	22°4	5 26	23°5	5 24	24°6	5 23	25°6
26	1 8	74°6														
27	1 35	68°6	1 7	74°9												
28	1 55	64°2	1 34	69°0	1 6	75°3										
29	2 11	60°6	1 53	64°7	1 33	69°5	1 6	75°5								
30	2 25	57°7	2 9	61°2	1 52	65°2	1 32	69°8	1 5	75°8						
31	2 36	55°1	2 22	58°3	2 8	61°8	1 51	65°7	1 31	70°3	1 4	76°1				
32	2 47	52°9	2 35	55°8	2 21	58°9	2 7	62°4	1 50	66°2	1 30	70°6	1 4	76°4		
33	2 56	50°9	2 45	53°0	2 33	56°5	2 20	59°5	2 6	62°9	1 49	66°6	1 29	71°0	1 3	75°6
34	3 5	49°1	2 55	51°6	2 44	54°3	2 32	57°1	2 19	60°1	2 5	63°4	1 48	67°1	1 28	71°4
35	3 13	47°5	3 3	49°8	2 53	52°3	2 42	54°9	2 31	57°7	2 17	60°7	2 4	63°8	1 47	67°5
36	3 20	46°0	3 11	48°2	3 2	50°6	2 51	53°0	2 41	55°6	2 29	58°3	2 17	61°2	2 3	64°3
37	3 27	44°6	3 19	46°7	3 10	49°0	3 0	51°3	2 51	53°7	2 40	56°2	2 28	58°8	2 16	61°7
38	3 33	43°0	3 25	45°4	3 17	47°5	3 8	49°7	2 59	51°9	2 49	54°3	2 39	56°8	2 28	59°3
39	3 39	42°2	3 32	44°1	3 24	46°2	3 16	48°2	3 7	50°4	2 58	52°6	2 49	54°9	2 38	57°3
40	3 45	41°1	3 38	43°3	3 30	44°9	3 23	46°9	3 15	49°0	3 6	51°1	2 58	52°2	2 47	55°5
41	3 50	40°1	3 43	41°9	3 36	43°8	3 29	45°7	3 22	47°6	3 14	49°6	3 5	51°7	2 56	53°8
42	3 55	39°2	3 49	40°9	3 42	42°7	3 35	44°6	3 28	46°4	3 20	48°3	3 13	50°3	3 4	52°4
43	4 0	38°3	3 54	40°0	3 48	41°7	3 41	43°5	3 34	45°3	3 27	47°1	3 20	49°0	3 12	51°0
44	4 4	37°5	3 59	39°1	3 53	40°8	3 46	42°5	3 40	44°3	3 33	46°0	3 26	47°8	3 19	49°7
45	4 9	36°7	4 3	38°3	3 57	39°9	3 52	41°6	3 45	43°3	3 39	45°0	3 32	46°7	3 25	48°5
46	4 13	36°0	4 8	37°5	4 2	39°1	3 56	40°7	3 51	42°4	3 44	44°0	3 38	45°7	3 32	47°4
47	4 17	35°3	4 12	36°8	4 7	38°4	4 1	39°9	3 55	41°5	3 49	43°1	3 44	44°8	3 37	46°4
48	4 21	34°7	4 16	36°1	4 11	37°7	4 6	39°2	4 0	40°7	3 55	42°3	3 49	43°8	3 43	45°5
49	4 24	34°0	4 20	35°5	4 15	37°0	4 10	38°4	4 5	40°0	3 59	41°5	3 54	43°0	3 48	44°6
50	4 28	33°5	4 23	34°9	4 19	36°3	4 14	37°8	4 9	39°3	4 4	40°7	3 59	42°2	3 54	43°7
51	4 31	32°9	4 27	34°3	4 23	35°7	4 18	37°2	4 13	38°6	4 8	40°0	4 4	41°5	3 58	43°0
52	4 35	32°4	4 30	33°8	4 26	35°2	4 22	36°6	4 17	38°0	4 13	39°4	4 8	40°8	4 3	42°3
53	4 38	31°9	4 34	33°3	4 30	34°6	4 26	36°0	4 21	37°4	4 17	38°8	4 12	40°1	4 8	41°6
54	4 41	31°5	4 37	32°8	4 34	34°1	4 30	35°5	4 25	36°8	4 21	38°2	4 16	39°5	4 12	40°9
55	4 44	31°1	4 40	32°3	4 36	33°6	4 33	35°0	4 29	36°3	4 25	37°6	4 20	38°9	4 16	40°3
56	4 47	30°6	4 43	31°9	4 40	33°2	4 36	34°5	4 32	35°8	4 28	37°1	4 24	38°4	4 20	39°7
57	4 49	30°3	4 46	31°5	4 43	32°8	4 39	34°0	4 36	35°3	4 32	36°6	4 28	37°8	4 24	39°2
58	4 52	29°9	4 49	31°1	4 46	32°4	4 42	33°6	4 39	34°8	4 35	36°1	4 32	37°4	4 28	38°7
59	4 55	29°5	4 52	30°7	4 49	32°0	4 45	33°2	4 42	34°4	4 39	35°7	4 35	36°9	4 32	38°2
60	4 58	29°2	4 55	30°4	4 52	31°6	4 48	32°8	4 45	34°0	4 42	35°3	4 39	36°5	4 35	37°7
61	5 0	28°9	4 57	30°1	4 54	31°3	4 51	32°5	4 48	33°7	4 45	34°8	4 42	36°1	4 39	37°3
62	5 3	28°6	5 0	29°7	4 57	30°9	4 54	32°1	4 51	33°3	4 48	34°5	4 45	35°7	4 42	36°8
63	5 5	28°3	5 2	29°5	5 0	30°5	4 57	31°8	4 54	33°0	4 52	34°1	4 48	35°3	4 46	36°5
64	5 7	28°0	5 5	29°2	5 2	30°3	5 0	31°5	4 57	32°6	4 55	33°8	4 50	35°0	4 49	36°1
65	5 10	27°8	5 7	28°9	5 5	30°1	5 3	31°2	5 0	32°3	4 58	33°5	4 53	34°6	4 52	35°8
66	5 12	27°6	5 10	28°7	5 8	29°8	5 5	30°9	5 3	32°0	5 0	33°2	4 56	34°3	4 55	35°4
67	5 14	27°5	5 12	28°4	5 10	29°5	5 8	30°7	5 5	31°8	5 3	32°9	4 59	34°0	4 58	35°1
68	5 17	27°3	5 15	28°2	5 12	29°3	5 10	30°4	5 8	31°5	5 7	32°6	5 1	33°7	5 1	34°8
69	5 19	26°9	5 17	28°0	5 15	29°1	5 13	30°2	5 11	31°3	5 9	32°4	5 5	33°5	5 4	34°6
70	5 21	26°7	5 19	27°8	5 17	28°8	5 15	30°0	5 13	31°1	5 11	32°1	5 8	33°2	5 7	34°3

HOUR ANGLE AND ALTITUDE OF A BODY UPON THE PRIME VERTICAL.

Lat.	DECLINATION															
	33°		34°		35°		36°		37°		38°		39°		40°	
	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.	H. A.	Alt.
34	1 3	76°9														
35	1 28	71°7	1 2	77°1												
36	1 47	67°9	1 27	72°0	1 2	77°4										
37	2 2	64°8	1 46	68°3	1 27	72°4	1 1	77°6								
38	2 15	62°2	2 1	65°3	1 45	68°7	1 26	72°7	1 1	77°8						
39	2 27	59°9	2 14	62°7	2 1	65°7	1 45	69°1	1 26	73°0	1 1	78°0				
40	2 37	57°9	2 26	60°4	2 24	63°2	2 0	66°1	1 44	69°4	1 26	73°3	1 1	78°2		
41	2 47	56°1	2 36	58°5	2 25	61°0	2 13	63°6	2 0	66°5	1 44	69°8	1 25	73°6	1 1	78°5
42	2 55	54°5	2 46	56°7	2 36	59°0	2 25	61°4	2 13	64°1	1 59	66°9	1 44	70°1	1 25	73°9
43	3 3	53°0	2 55	55°1	2 45	57°2	2 35	59°5	2 24	61°9	2 12	64°5	1 59	67°3	1 43	70°5
44	3 11	51°6	3 1	53°6	2 54	55°7	2 45	57°8	2 35	60°0	2 24	62°4	2 12	64°9	1 59	67°7
45	3 18	50°4	3 10	52°3	3 2	54°2	2 54	56°2	2 44	58°3	2 34	60°5	2 24	62°8	2 12	65°4
46	3 25	49°4	3 17	51°0	3 10	52°8	3 2	54°8	2 53	56°8	2 44	58°8	2 34	61°0	2 23	63°3
47	3 30	48°1	3 24	49°8	3 17	51°6	3 9	53°5	3 1	55°4	2 53	57°3	2 44	59°3	2 34	61°5
48	3 37	47°1	3 30	48°8	3 24	50°5	3 17	52°3	3 9	54°1	3 1	55°9	2 53	57°8	2 44	59°9
49	3 43	46°2	3 36	47°8	3 30	49°5	3 23	51°1	3 16	52°8	3 9	54°7	3 1	56°5	2 53	58°4
50	3 48	45°3	3 42	46°8	3 36	48°5	3 30	50°1	3 23	51°8	3 16	53°5	3 9	55°5	3 1	57°0
51	3 53	44°5	3 48	46°0	3 42	47°6	3 36	49°1	3 30	50°4	3 23	52°4	3 16	54°1	3 9	55°8
52	3 58	43°7	3 53	45°2	3 47	46°8	3 42	48°2	3 36	49°8	3 30	51°4	3 23	53°0	3 16	54°7
53	4 2	43°0	3 58	44°4	3 53	45°9	3 47	47°4	3 42	48°9	3 36	50°4	3 30	52°0	3 23	53°6
54	4 7	42°3	4 3	43°7	3 58	45°1	3 53	46°6	3 47	48°1	3 42	49°5	3 36	51°1	3 30	52°6
55	4 12	41°7	4 7	43°0	4 3	44°4	3 58	45°8	3 53	47°3	3 47	48°7	3 42	50°2	3 36	51°7
56	4 16	41°1	4 12	42°4	4 7	43°8	4 3	45°1	3 58	46°5	3 47	47°9	3 42	49°4	3 42	50°8
57	4 20	40°5	4 16	41°8	4 12	43°1	4 7	44°5	4 3	45°8	3 58	47°2	3 53	48°6	3 48	50°0
58	4 24	40°0	4 20	41°2	4 16	42°5	4 12	43°9	4 8	45°2	4 3	46°5	3 58	47°9	3 53	49°3
59	4 28	39°4	4 24	40°7	4 20	43°3	4 16	44°3	4 12	44°6	4 8	45°9	4 4	47°1	3 59	48°6
60	4 32	39°0	4 28	40°2	4 25	41°5	4 21	42°7	4 17	44°0	4 13	45°3	4 4	46°6	4 4	47°9
61	4 36	38°5	4 32	39°7	4 29	41°0	4 25	42°2	4 21	43°5	4 17	44°7	4 13	46°0	4 9	47°3
62	4 39	38°2	4 36	39°3	4 33	40°5	4 29	41°7	4 26	42°9	4 22	44°2	4 18	45°5	4 14	46°7
63	4 43	37°7	4 40	38°8	4 36	40°1	4 33	41°3	4 30	42°5	4 26	43°7	4 23	44°9	4 19	46°2
64	4 47	37°3	4 43	38°5	4 40	39°6	4 37	40°8	4 34	42°0	4 30	43°2	4 27	44°4	4 23	45°7
65	4 49	36°9	4 47	38°1	4 44	39°3	4 41	40°4	4 38	41°6	4 35	42°8	4 31	44°0	4 28	45°2
66	4 53	36°6	4 50	37°7	4 47	38°9	4 44	40°0	4 42	41°2	4 39	42°4	4 35	43°5	4 32	44°7
67	4 56	36°3	4 53	37°4	4 51	38°5	4 48	39°7	4 45	40°8	4 43	42°0	4 43	43°1	4 37	44°3
68	4 59	36°0	4 57	37°1	4 54	38°2	4 52	39°3	4 49	40°5	4 46	41°6	4 44	42°7	4 41	43°8
69	5 2	35°7	5 0	36°8	4 58	37°9	4 55	39°0	4 53	40°1	4 50	41°2	4 48	42°4	4 45	43°5
70	5 5	35°4	5 3	36°5	5 1	37°6	4 59	38°7	4 56	39°8	4 54	40°9	4 51	42°0	4 49	43°2
°																
41°			42°		43°		44°		45°		46°		47°		48°	
42	1 0	78°6														
43	1 25	74°1	1 0	78°8												
44	1 43	70°8	1 25	74°4	1 0	79°0										
45	1 58	68°1	1 43	71°1	1 25	74°7	1 0	79°2								
46	2 12	65°8	1 58	68°5	1 43	71°5	1 25	74°9	1 0	79°4						
47	2 23	63°8	2 12	66°2	1 58	68°8	1 43	71°8	1 25	75°2	1 0	79°6				
48	2 34	62°0	2 23	64°2	2 12	66°6	1 58	69°2	1 43	72°2	1 25	75°5	1 0	79°8		
49	2 44	60°4	2 33	62°4	2 23	64°6	2 12	67°0	1 58	69°5	1 43	72°4	1 25	75°7	1 0	79°9
50	2 53	58°9	2 44	60°9	2 34	62°9	2 23	65°1	2 12	67°4	1 59	69°9	1 43	72°7	1 25	75°9
51	3 1	57°6	2 53	59°4	2 44	61°3	2 34	63°4	2 24	65°5	2 12	67°8	1 59	70°2	1 44	73°0
52	3 9	56°4	3 1	58°1	2 53	59°9	2 44	61°8	2 34	63°8	2 24	65°9	2 12	68°1	1 59	70°6
53	3 16	55°2	3 9	56°9	3 1	58°6	2 53	60°4	2 44	62°3	2 35	65°2	2 24	66°3	2 13	68°5
54	3 23	54°7	3 17	55°8	3 9	57°5	3 2	59°2	2 54	60°9	2 45	62°8	2 35	64°7	2 25	66°7
55	3 30	53°2	3 24	54°8	3 17	56°4	3 10	58°0	3 2	59°7	2 54	61°4	2 45	63°2	2 36	65°1
56	3 36	52°3	3 30	53°8	3 24	55°3	3 17	56°9	3 10	58°5	3 3	60°2	2 55	61°9	2 46	63°7
57	3 43	51°5	3 37	52°9	3 31	54°4	3 25	55°9	3 18	57°5	3 11	59°1	3 3	60°7	2 55	62°4
58	3 48	50°7	3 43	52°1	3 37	53°5	3 32	55°0	3 25	56°5	3 19	58°0	3 12	59°6	3 4	61°2
59	3 54	49°9	3 49	51°3	3 44	52°7	3 38	54°1	3 32	55°6	3 26	57°0	3 20	58°6	3 13	60°2
60	3 59	49°2	3 55	50°6	3 50	51°9	3 44	53°3	3 39	54°7	3 33	56°2	3 27	57°6	3 20	59°1
61	4 5	48°6	4 0	49°9	3 55	51°2	3 51	52°6	3 45	53°9	3 40	55°3	3 34	56°7	3 28	58°2
62	4 10	48°0	4 6	49°3	4 1	50°6	3 56	51°8	3 52	53°2	3 46	54°5	3 41	55°5	3 35	57°3
63	4 15	47°4	4 11	48°7	4 7	49°9	4 2	51°2	3 57	52°5	3 53	53°8	3 48	55°2	3 42	56°5

TABLE 30

APPARENT DIP OF THE SEA HORIZON	
Ht.	Dip.
0	0 0
1	1 0
2	1 24
3	1 42
4	1 58
5	2 12
6	2 25
7	2 36
8	2 47
9	2 57
10	3 7
12	3 25
14	3 41
16	3 56
18	4 11
20	4 24
22	4 37
24	4 49
26	5 1
28	5 13
30	5 24
35	5 49
40	6 13
45	6 36
50	6 58
55	7 18
60	7 37
65	7 56
70	8 14
75	8 31
80	8 48
85	9 4
90	9 20
100	9 51
110	10 19
120	10 47
130	11 14
140	11 39
150	12 3
160	12 27
170	12 50
180	13 12
190	13 34
200	13 55
210	14 16
220	14 36
240	15 15
260	15 52
280	16 27
300	17 0

TABLE 31

MEAN ASTRONOMICAL REFRACTION. (Barometer, 30 inches. Fahrenheit's Thermometer, 50°)											
App. Alt.	Refrac.	D.to 10'	App. Alt.	Refrac.	D.to 10'	App. Alt.	Refrac.	D.to 10'	App. Alt.	Refrac.	D.to 10'
0° 0'	34' 17"	122"	6° 10'	8' 18"	12"	12° 50'	4' 11"	3"	38° 0'	1' 23' 2"	50"
10	32 15	112	15	8 12	12	13 0	4 8	3' 2	30	1 21' 7"	50
20	30 23	102	20	8 6	12	13 10	4 5	3' 1	30	1 20' 2"	47
30	28 41		25	8 1	11	20	4 2	3' 0	30	1 18' 8"	47
40	27 7	94	30	7 56	11	30	3 59	3' 0	37	1 17' 4"	47
50	25 41	86	35	7 50	11	40	3 56	2' 9	30	1 16' 0"	47
1 0	24 22	78	40	7 45	11	50	3 53	2' 9	38	0 1 14' 6"	47
10	23 9	73	45	7 40	10	14 0	3 50	2' 8	30	1 13' 3"	43
20	22 2	62	50	7 35	10	10	3 47	2' 7	39	0 1 12' 0"	45
30	21 0	58	55	7 30	10	20	3 45	2' 6	30	1 10' 7"	43
40	20 2	53	7 0	7 25	10	30	3 42	2' 5	40	0 1 9' 5"	40
50	19 9	49	5	7 20	9	40	3 40	2' 5	41	0 1 7' 1"	38
2 0	18 20	46	10	7 16	9	50	3 37	2' 4	42	0 1 4' 8"	35
10	17 34	44	15	7 11	9	15 0	3 35	2' 4	43	0 1 2' 6"	34
12	17 12	42	20	7 7	9	10	3 32	2' 3	44	0 1 0' 4"	34
14	16 51	40	25	7 3	9	20	3 30	2' 3	45	0 0 58' 4"	33
16	16 31	39	30	6 59	9	30	3 28	2' 2	46	0 0 56' 3"	32
18	16 11	38	35	6 54	9	40	3 25	2' 1	47	0 0 54' 4"	31
20	15 52	37	40	6 50	9	50	3 23	2' 1	48	0 0 52' 6"	30
22	15 34	36	45	6 46	8	16 0	3 21	2' 1	49	0 0 50' 7"	29
24	15 16	35	50	6 42	8	10	3 19	2' 1	50	0 0 49' 0"	28
26	14 59	34	55	6 38	8	20	3 17	2' 1	51	0 0 47' 3"	27
28	14 42	33	8 0	6 35	8	30	3 15	2' 0	52	0 0 45' 6"	26
30	14 26	32	5	6 31	8	40	3 13	2' 0	53	0 0 44' 0"	26
35	14 10	31	10	6 27	7	50	3 11	2' 0	54	0 0 42' 4"	25
40	13 55	30	15	6 23	7	17 0	3 9	1' 9	55	0 0 40' 9"	25
45	13 41	29	20	6 20	7	30	3 3	1' 9	56	0 0 39' 4"	24
50	13 27	28	25	6 16	7	18 0	2 58	1' 8	57	0 0 37' 9"	24
55	13 13	27	30	6 13	7	30	2 53	1' 7	58	0 0 36' 5"	23
60	13 0	26	35	6 9	7	19 0	2 48	1' 6	59	0 0 35' 1"	23
65	12 47	25	40	6 6	6	30	2 44	1' 5	60	0 0 33' 7"	22
70	12 34	25	45	6 3	6	20 0	2 39	1' 4	61	0 0 32' 4"	22
75	12 22	24	50	6 0	6	30	2 35	1' 3	62	0 0 31' 0"	21
80	12 10	24	55	5 57	6	21 0	2 31	1' 2	63	0 0 29' 8"	21
85	11 58	23	9 0	5 54	6	30	2 27	1' 2	64	0 0 28' 5"	21
90	11 47	22	5	5 51	6	22 0	2 24	1' 1	65	0 0 27' 2"	20
100	11 36	21	10	5 48	6	30	2 20	1' 1	66	0 0 26' 0"	20
110	11 26	21	15	5 45	6	23 0	2 17	1' 0	67	0 0 24' 8"	20
120	11 15	20	20	5 42	6	30	2 13	1' 0	68	0 0 23' 6"	20
130	11 5	20	25	5 39	6	24 0	2 10	1' 0	69	0 0 22' 4"	20
140	10 55	19	30	5 36	6	30	2 7	0' 9	70	0 0 21' 3"	20
150	10 46	19	35	5 33	5	25 0	2 5	0' 9	71	0 0 20' 1"	20
160	10 37	18	40	5 31	5	30	2 2	0' 9	72	0 0 19' 0"	19
170	10 28	18	50	5 25	5	26 0	1 59	0' 9	73	0 0 17' 9"	19
180	10 19	18	10 0	5 20	5	30	1 56	0' 9	74	0 0 16' 7"	18
190	10 10	17	10	5 15	5	27 0	1 54	0' 8	75	0 0 15' 7"	18
200	10 2	16	20	5 10	5	30	1 51	0' 8	76	0 0 14' 6"	17
5 0	9 54	16	30	5 6	5	28 0	1 49	0' 8	77	0 0 13' 5"	17
8	9 46	16	40	5 1	5	30	1 47	0' 7	78	0 0 12' 4"	17
10	9 38	15	50	4 56	4	29 0	1 45	0' 7	79	0 0 11' 3"	17
15	9 30	15	11 0	4 52	4	30	1 43	0' 7	80	0 0 10' 3"	17
20	9 23	15	10	4 48	4	30 0	1 41	0' 7	81	0 0 9' 2"	17
25	9 16	14	20	4 44	4	30	1 39	0' 6	82	0 0 8' 2"	17
30	9 9	14	30	4 40	4	31 0	1 37	0' 6	83	0 0 7' 2"	17
35	9 2	14	40	4 36	4	30	1 35	0' 6	84	0 0 6' 1"	17
40	8 55	13	50	4 32	4	32 0	1 33	0' 6	85	0 0 5' 1"	17
45	8 48	13	12 0	4 28	4	30	1 31	0' 6	86	0 0 4' 1"	17
50	8 42	13	10	4 25	4	33 0	1 30	0' 6	87	0 0 3' 1"	17
55	8 36	13	20	4 21	4	30	1 28	0' 5	88	0 0 2' 0"	17
6 0	8 30	12	30	4 18	4	34 0	1 26	0' 5	89	0 0 1' 0"	17
5	8 24		40	4 14	4	30	1 25	0' 5	90	0 0 0	17

**CORRECTION OF THE MEAN REFRACTION FOR THE HEIGHT OF
THE THERMOMETER**

Therm.	ALTITUDES																	
	4°	5°	5½°	6°	6½°	7°	7½°	8°	9°	10°	12°	15°	20°	30°	40°	50°	70°	90°
0	add	add	add	add	add	add	add	add	add	add	add	add	add	add	add	add	add	add
2	69"	61"	57"	54"	51"	48"	46"	43"	39"	36"	30"	25"	18"	12"	8'1"	5'7"	2'5"	0
4	63	56	52	49	46	44	41	39	36	32	28	22	17	11	7'4"	5'2"	2'3"	0
6	60	53	50	47	44	42	39	37	34	31	26	21	16	10	7'0"	4'9"	2'1"	0
8	57	50	47	44	42	40	37	36	32	29	25	20	15	10	6'7"	4'7"	2'0"	0
10	55	48	45	42	40	37	35	34	31	28	24	19	14	9	6'3"	4'4"	1'9"	0
12	51	45	42	40	37	35	34	32	29	26	22	18	14	9	6'0"	4'2"	1'8"	0
14	48	42	40	37	35	33	32	30	27	25	21	17	13	8	5'6"	4'0"	1'7"	0
16	44	40	37	35	33	31	30	28	26	23	20	16	12	8	5'3"	3'7"	1'6"	0
18	42	37	35	33	31	29	28	26	24	22	19	15	11	7	5'0"	3'5"	1'5"	0
20	39	35	33	31	29	28	26	25	22	20	17	14	11	7	4'6"	3'3"	1'4"	0
22	36	32	30	29	27	25	24	23	21	19	16	13	10	6	4'3"	3'0"	1'3"	0
24	33	30	27	26	25	24	22	21	19	17	15	12	9	6	4'0"	2'8"	1'2"	0
26	30	27	26	24	23	22	20	19	18	16	14	11	8	5	3'7"	2'6"	1'1"	0
28	28	25	23	22	21	20	19	18	16	15	13	10	8	5	3'3"	2'4"	1'0"	0
30	26	23	21	20	19	18	17	16	15	13	11	9	7	4	3'0"	2'1"	0'9"	0
32	22	20	19	18	17	16	15	14	13	12	10	8	6	4	2'7"	1'9"	0'8"	0
34	21	18	17	16	15	14	13	12	11	10	9	7	5	3	2'4"	1'7"	0'7"	0
36	18	16	15	14	13	12	12	11	10	9	8	5	5	3	2'1"	1'5"	0'6"	0
38	15	13	12	12	11	10	10	9	9	8	7	5	4	3	1'8"	1'3"	0'5"	0
40	13	11	10	10	9	9	8	8	7	6	5	4	3	2	1'5"	1'0"	0'4"	0
42	10	9	8	8	7	7	7	6	6	5	4	3	2	2	1'2"	0'8"	0'4"	0
44	7	6	6	6	5	5	5	5	5	4	3	3	2	1	0'9"	0'6"	0'3"	0
46	5	4	4	4	4	3	3	3	3	2	2	2	1	1	0'6"	0'4"	0'2"	0
48	2	2	2	2	2	2	2	2	2	1	1	1	1	0	0'3"	0'2"	0'1"	0
50	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
52	sub.	sub.	sub.	sub.	sub.	sub.	sub.	sub.	sub.	sub.	sub.	sub.	sub.	sub.	sub.	sub.	sub.	sub.
54	2	2	2	2	1	1	1	1	1	1	1	1	1	0	0'3"	0'2"	0'1"	0
56	4	4	4	4	3	3	3	3	3	2	2	2	1	1	0'6"	0'4"	0'2"	0
58	7	6	6	6	5	5	5	5	4	4	3	3	2	2	0'9"	0'6"	0'3"	0
60	9	8	8	7	7	7	6	6	5	5	4	3	3	2	1'1"	0'8"	0'4"	0
62	11	10	10	9	9	8	8	8	7	6	5	4	3	2	1'4"	1'0"	0'5"	0
64	14	13	12	11	10	10	9	9	8	7	6	5	4	2	1'7"	1'2"	0'5"	0
66	17	15	14	13	12	12	11	10	9	9	7	6	4	3	2'0"	1'4"	0'6"	0
68	19	17	16	15	14	13	12	12	11	10	8	7	5	3	2'2"	1'6"	0'7"	0
70	21	19	18	16	16	15	14	13	12	11	9	8	6	4	2'5"	1'8"	0'8"	0
72	23	21	19	18	17	16	15	15	13	12	10	8	6	4	2'8"	2'0"	0'8"	0
74	25	22	21	20	19	18	17	16	15	13	11	9	7	4	3'0"	2'1"	0'9"	0
76	27	24	23	22	21	19	18	17	16	14	12	10	8	5	3'3"	2'3"	1'0"	0
78	29	26	25	23	22	21	20	19	17	16	13	11	8	5	3'6"	2'5"	1'1"	0
80	31	28	27	25	24	22	21	20	18	17	14	12	9	6	3'8"	2'7"	1'2"	0
82	33	30	28	27	25	24	23	22	20	18	15	12	9	6	4'1"	2'9"	1'3"	0
84	36	32	30	28	27	25	24	23	21	19	16	13	10	6	4'3"	3'1"	1'3"	0
86	38	34	32	30	28	27	26	24	22	20	17	14	10	7	4'6"	3'2"	1'4"	0
88	40	36	34	32	30	28	27	26	23	21	18	15	11	7	4'9"	3'4"	1'5"	0
90	43	38	35	33	31	30	28	27	24	22	19	15	12	7	5'1"	3'6"	1'6"	0
92	45	39	37	35	33	31	30	28	26	23	20	16	12	8	5'3"	3'8"	1'6"	0
94	47	41	39	36	35	33	31	29	27	24	21	17	13	8	5'6"	3'9"	1'7"	0
96	49	43	40	38	36	34	32	31	28	26	22	18	13	8	5'8"	4'1"	1'8"	0
98	51	45	42	40	37	37	34	32	29	27	23	18	14	9	6'1"	4'3"	1'9"	0
100	53	46	44	41	39	37	35	33	30	28	23	19	14	9	6'3"	4'5"	1'9"	0
100	55	48	45	43	40	38	36	35	31	29	24	20	15	9	6'5"	4'6"	2'0"	0

CORRECTION OF THE MEAN REFRACTION FOR THE HEIGHT OF
THE BAROMETER

Bar.	ALTITUDES																		Par.	
	4°	5°	5½°	6°	6½°	7°	7½°	8°	9°	10°	12°	15°	20°	30°	40°	50°	70°	90°		
sub.	60"	50"	46"	42"	40"	37"	35"	33"	29"	27"	22"	18"	13"	8"	5"8	4"0	1"8	0	add	
27.5	57	48	44	41	38	36	34	32	28	26	21	17	13	8	5"5	3"8	1"7	0		
27.6	54	46	42	39	37	34	32	30	27	25	20	17	12	8	5"3	3"7	1"6	0		
27.7	51	44	40	37	35	33	31	29	26	24	20	16	12	7	5"1	3"5	1"5	0		
27.8	48	42	38	36	33	31	29	28	25	22	19	15	11	7	4"8	3"3	1"5	0		
27.9	46	40	37	34	32	30	28	26	24	21	18	14	11	7	4"6	3"2	1"4	0		
28.0	44	38	35	32	30	28	27	25	22	20	18	14	10	6	4"4	3"0	1"3	0		
28.1	41	36	33	31	29	27	25	24	21	19	17	13	10	6	4"1	2"9	1"3	0		
28.2	39	34	31	29	27	25	24	22	20	18	16	12	9	6	3"9	2"7	1"2	0		
28.3	37	32	29	27	25	24	22	21	19	17	15	12	8	5	3"7	2"6	1"1	0		
28.4	35	30	27	25	24	22	21	20	18	16	14	11	8	5	3"4	2"4	1"0	0	31.6	
28.5	32	28	26	24	22	21	20	18	17	15	13	10	7	5	3"2	2"2	1"0	0	31.4	
28.6	30	26	24	22	21	19	18	17	15	14	12	9	7	4	3"0	1"9	0"9	0	31.3	
28.7	27	24	22	20	19	18	17	16	14	13	11	9	6	4	2"8	1"8	0"8	0	31.2	
28.8	25	22	20	19	17	16	15	15	13	12	10	8	6	4	2"5	1"7	0"8	0	31.1	
28.9	23	20	18	17	16	15	14	13	12	11	9	7	5	3	2"3	1"6	0"7	0	31.0	
29.0	21	18	16	15	14	13	12	11	10	8	6	5	3	2	2"1	1"4	0"6	0	30.9	
29.1	18	16	15	14	13	12	11	11	9	9	7	6	4	3	1"8	1"3	0"6	0	30.8	
29.2	16	14	13	12	11	10	10	9	8	7	6	5	4	2	1"6	1"1	0"5	0	30.7	
29.3	14	12	11	10	10	9	8	8	7	6	5	4	3	2	1"4	1"0	0"4	0	30.6	
29.4	12	10	9	8	8	7	7	7	6	5	4	4	3	2	1"1	0"8	0"3	0	30.5	
29.5	9	8	7	7	6	6	6	6	5	5	4	4	3	2	1	0"9	0"6	0"3	0	30.4
29.6	6	6	5	5	5	4	4	4	4	4	3	3	2	2	1	0"7	0"5	0"2	0	30.3
29.7	4	4	4	3	3	3	3	3	2	2	2	1	1	1	1	0"5	0"3	0"1	0	30.2
29.8	2	2	2	2	2	1	1	1	1	1	1	1	1	0	0"2	0"2	0"1	0	30.1	
29.9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	30.0	

TABLE 34

THE SUN'S PARALLAX IN ALTITUDE,
AND SEMIDIAMETER

Month	Semid.	ALTITUDE										Semid.	Month
		0°	10°	20°	30°	40°	50°	60°	70°	80°	90°		
Jan. 1	16' 17"	8'7	8'6	8'2	7'6	6'7	5'6	4'4	3'0	1'5	0"	16' 15"	Dec. 1
Feb. 1	16 15	8'7	8'6	8'2	7'6	6'6	5'6	4'3	3'0	1'5	0	16 9	Nov. 1
Mar. 1	16 9	8'6	8'5	8'1	7'5	6'6	5'5	4'3	3'0	1'5	0	16 1	Oct. 1
Apr. 1	16 1	8'5	8'4	8'0	7'4	6'5	5'5	4'3	2'9	1'5	0	15 53	Sept. 1
May 1	15 53	8'4	8'3	8'0	7'3	6'5	5'4	4'2	2'9	1'5	0	15 47	Aug. 1
June 1	15 47	8'4	8'3	8'0	7'3	6'4	5'4	4'2	2'9	1'5	0	15 45	July 1

TABLE 35

DIP OF THE SHORE
HORIZON

Dist. in Miles	Ht. of the Eye in ft.									
	5	10	15	20	25	30	35	40		
1	6	12	17	23	28	34	40	45		
1 ½	3	6	9	12	15	17	20	23		
2	2	4	6	8	10	12	14	16		
2 ½	2	4	5	7	8	9	11	12		
3	2	3	4	6	7	8	9	10		
3 ½	2	3	4	5	6	7	8	9		
4	2	3	4	5	6	7	8	9		
4 ½	2	3	4	5	6	7	8	9		
5	2	3	4	5	6	7	8	9		
6	2	3	4	5	6	7	8	9		

CORRESPONDING THERMOMETERS, Fahrenheit, Centigrade, Réaumur.					
F.	C.	R.	F.	C.	R.
0	-17.8	-14.2	60	15.6	12.4
1	-17.2	-13.8	61	16.1	12.9
2	-16.7	-13.3	62	16.7	13.3
3	-16.1	-12.9	63	17.2	13.8
4	-15.6	-12.4	64	17.8	14.2
5	-15.0	-12.0	65	18.3	14.7
6	-14.4	-11.6	66	18.9	15.1
7	-13.9	-11.1	67	19.4	15.6
8	-13.3	-10.7	68	20.0	16.0
9	-12.8	-10.2	69	20.6	16.4
10	-12.2	-9.8	70	21.1	16.9
11	-11.7	-9.3	71	21.7	17.3
12	-11.1	-8.9	72	22.2	17.8
13	-10.6	-8.4	73	22.8	18.2
14	-10.0	-8.0	74	23.3	18.7
15	-9.4	-7.5	75	23.9	19.1
16	-8.9	-7.1	76	24.4	19.6
17	-8.3	-6.7	77	25.0	20.0
18	-7.8	-6.2	78	25.6	20.5
19	-7.2	-5.8	79	26.1	20.9
20	-6.7	-5.3	80	26.7	21.3
21	-6.1	-4.9	81	27.2	21.8
22	-5.6	-4.4	82	27.8	22.2
23	-5.0	-4.0	83	28.3	22.7
24	-4.4	-3.6	84	28.9	23.1
25	-3.9	-3.1	85	29.4	23.6
26	-3.3	-2.7	86	30.0	24.0
27	-2.8	-2.2	87	30.6	24.4
28	-2.2	-1.8	88	31.1	24.9
29	-1.7	-1.3	89	31.7	25.3
30	-1.1	-0.9	90	32.2	25.8
31	-0.6	-0.4	91	32.8	26.2
32	0	0	92	33.3	26.7
33	0.6	0.4	93	33.9	27.1
34	1.1	0.9	94	34.4	27.6
35	1.7	1.3	95	35.0	28.0
36	2.2	1.8	96	35.6	28.4
37	2.8	2.2	97	36.1	28.9
38	3.3	2.7	98	36.7	29.3
39	3.9	3.1	99	37.2	29.8
40	4.4	3.6	100	37.8	30.2
41	5.0	4.0	101	38.3	30.7
42	5.6	4.4	102	38.9	31.1
43	6.1	4.9	103	39.4	31.6
44	6.7	5.3	104	40.0	32.0
45	7.2	5.8	105	40.6	32.4
46	7.8	6.2	106	41.1	32.9
47	8.3	6.7	107	41.7	33.3
48	8.9	7.1	108	42.2	33.8
49	9.4	7.5	109	42.8	34.2
50	10.0	8.0	110	43.3	34.7
51	10.6	8.4	111	43.9	35.1
52	11.1	8.9	112	44.4	35.5
53	11.7	9.3	113	45.0	36.0
54	12.2	9.8	114	45.6	36.4
55	12.8	10.2	115	46.1	36.9
56	13.3	10.7	116	46.7	37.3
57	13.9	11.1	117	47.2	37.8
58	14.4	11.6	118	47.8	38.2
59	15.0	12.0	119	48.3	38.7
60	15.6	12.4	120	48.9	39.1

CORRESPONDING FRENCH & ENGLISH MEASURES							
Fr. Kilomètre, Mètre, Décimètre, Centimètre, Millimètre. Eng. Nautical Miles, Feet, Inches.						Barometer Scales	
Fr.	English					Fr.	Eng.
No.	Miles corr. to Kil.	Feet corr. to Mètre.	Feet corr. to Décim.	In. corr. to Cent.	In. corr. to Mill.	Mill.	In.
1	0.539	3.28	0.33	0.39	0.04	640	25.2
2	1.079	6.56	0.66	0.79	0.08	643	25.3
3	1.618	9.84	0.98	1.18	0.12	645	25.4
4	2.158	13.12	1.31	1.57	0.16	648	25.5
5	2.697	16.40	1.64	1.97	0.20	650	25.6
6	3.237	19.68	1.97	2.36	0.24	653	25.7
7	3.776	22.97	2.30	2.76	0.28	655	25.8
8	4.316	26.25	2.62	3.15	0.31	658	25.9
9	4.855	29.53	2.95	3.54	0.35	660	26.0
10	5.394	32.81	3.28	3.94	0.39	663	26.1
20	10.79	65.62	6.56	7.87	0.79	665	26.2
30	16.18	98.43	9.84	11.81	1.18	668	26.3
40	21.58	131.2	13.1	15.75	1.57	670	26.4
50	26.97	164.0	16.4	19.69	1.97	673	26.5
60	32.37	196.9	19.7	23.62	2.36	676	26.6
70	37.76	229.7	23.0	27.56	2.76	678	26.7
80	43.15	262.5	26.2	31.50	3.15	681	26.8
90	48.55	295.3	29.5	35.43	3.54	683	26.9
100	53.94	328.1	32.8	39.4	3.94	686	27.0
200	107.9	656.2			7.87	688	27.1
300	161.8	984.3			11.81	691	27.2
400	215.8	1312.4			15.75	693	27.3
500	269.7	1640.4			19.68	696	27.4
600	323.7	1968.5			23.62	698	27.5
700	377.6	2296.6			27.56	701	27.6
800	431.5	2624.7			31.50	704	27.7
900	485.5	2952.8			35.43	706	27.8
1000	539.4	3280.9			39.37	709	27.9
						711	28.0
						714	28.1
						716	28.2
						719	28.3
						721	28.4
						724	28.5
						726	28.6
						729	28.7
						732	28.8
						734	28.9
						737	29.0
						739	29.1
						742	29.2
						744	29.3
						747	29.4
						749	29.5
						752	29.6
						754	29.7
						757	29.8
						759	29.9
						762	30.0
						765	30.1
						767	30.2
						770	30.3
						772	30.4
						775	30.5
						777	30.6
						780	30.7
						782	30.8
						785	30.9
						787	31.0

CORRECTIONS OF ALTITUDE OF THE SUN AND STARS
(Involving Dip, Refraction, ☉'s Semid. and Parallax).

FOR APPROXIMATE USE AT SEA.

The SUN. Add the Corr. to the Alt. of the Lower limb, except where marked —.

Height of the Eye in Feet.																					
Alt.	8	10	12	14	16	18	20	22	24	26	28	30	32	34	37	40	45	50	60	Alt.	
4½	2.6	2.3	2.0	1.7	1.4	1.2	1.0	0.7	0.5	0.3	0.1	—	—	—	—	—	—	—	—	4½	
6	3.5	3.2	2.9	2.6	2.4	2.1	1.9	1.6	1.4	1.2	1.0	0.8	0.7	0.5	0.2	0.0	—0.4	—0.8	—1.5	6	
6½	4.2	3.9	3.6	3.3	3.1	2.9	2.7	2.4	2.2	2.0	1.8	1.6	1.4	1.2	1.0	0.7	0.3	—0.1	—0.7	6½	
8	4.9	4.6	4.3	4.0	3.7	3.5	3.3	3.1	2.9	2.6	2.4	2.3	2.1	1.9	1.7	1.4	1.0	0.6	0.0	8	
8½	5.4	5.1	4.8	4.5	4.3	4.0	3.8	3.6	3.4	3.2	3.0	2.8	2.6	2.4	2.2	2.0	1.6	1.2	0.6	8½	
7	6.0	5.6	5.3	5.0	4.8	4.6	4.3	4.1	3.9	3.7	3.5	3.3	3.1	2.9	2.7	2.5	2.1	1.7	1.0	7	
8	6.7	6.4	6.1	5.8	5.6	5.3	5.1	4.9	4.7	4.5	4.3	4.1	3.9	3.7	3.5	3.3	2.9	2.6	1.9	8	
9	7.4	7.1	6.8	6.5	6.3	6.0	5.8	5.6	5.4	5.2	5.0	4.8	4.6	4.4	4.2	4.0	3.6	3.3	2.6	9	
10	8.0	7.7	7.4	7.1	6.8	6.6	6.4	6.1	5.9	5.7	5.5	5.4	5.2	5.0	4.8	4.5	4.2	3.9	3.2	10	
11	8.5	8.1	7.8	7.6	7.3	7.1	6.8	6.6	6.4	6.2	6.0	5.8	5.7	5.5	5.3	5.0	4.7	4.3	3.7	11	
12	8.9	8.6	8.2	8.0	7.7	7.5	7.2	7.0	6.8	6.6	6.4	6.2	6.1	5.9	5.7	5.5	5.1	4.7	4.1	12	
14	9.5	9.2	8.9	8.6	8.3	8.1	7.9	7.6	7.4	7.2	7.1	6.9	6.7	6.5	6.3	6.1	5.7	5.4	4.7	14	
16	10.0	9.7	9.4	9.1	8.8	8.6	8.4	8.1	8.0	7.8	7.6	7.4	7.2	7.0	6.8	6.6	6.3	5.9	5.2	16	
18	10.4	10.1	9.8	9.5	9.2	9.0	8.8	8.5	8.3	8.1	7.9	7.7	7.6	7.4	7.2	6.9	6.6	6.3	5.6	18	
20	10.7	10.4	10.1	9.8	9.5	9.3	9.1	8.9	8.7	8.5	8.3	8.1	7.9	7.7	7.5	7.2	6.9	6.6	5.9	20	
22	11.0	10.6	10.3	10.1	9.8	9.6	9.3	9.1	8.9	8.7	8.5	8.3	8.2	8.0	7.7	7.5	7.2	6.8	6.2	22	
25	11.3	10.9	10.6	10.4	10.1	9.9	9.6	9.4	9.2	9.0	8.8	8.7	8.5	8.3	8.1	7.9	7.5	7.1	6.5	25	
30	11.7	11.3	11.0	10.8	10.5	10.3	10.0	9.8	9.6	9.4	9.2	9.1	8.9	8.7	8.4	8.2	7.8	7.5	6.8	30	
35	12.0	11.6	11.3	11.1	10.8	10.6	10.3	10.1	9.9	9.7	9.5	9.4	9.2	9.0	8.7	8.5	8.1	7.8	7.1	35	
40	12.2	11.8	11.5	11.3	11.0	10.8	10.6	10.3	10.1	9.9	9.7	9.6	9.4	9.2	9.0	8.8	8.4	8.0	7.3	40	
45	12.4	12.0	11.7	11.5	11.2	11.0	10.8	10.5	10.3	10.1	9.9	9.7	9.5	9.4	9.1	8.9	8.5	8.2	7.5	45	
50	12.5	12.2	11.9	11.6	11.3	11.1	10.9	10.7	10.5	10.3	10.1	9.9	9.7	9.5	9.3	9.1	8.7	8.3	7.7	50	
60	12.7	12.4	12.1	11.8	11.6	11.3	11.1	10.9	10.7	10.5	10.3	10.1	9.9	9.8	9.5	9.3	8.9	8.5	7.9	60	
70	12.9	12.6	12.3	12.0	11.8	11.5	11.3	11.1	10.9	10.7	10.5	10.3	10.1	9.9	9.7	9.5	9.1	8.7	8.1	70	
80	13.1	12.7	12.4	12.2	11.9	11.7	11.4	11.2	11.0	10.8	10.6	10.4	10.3	10.1	9.8	9.6	9.2	8.9	8.3	80	
90	13.2	12.9	12.6	12.3	12.0	11.8	11.6	11.4	11.2	11.0	10.8	10.6	10.4	10.2	10.0	9.8	9.4	9.0	8.4	90	
Month																					
Correction to sun's alt. }																					
Jan. Feb. Mar. April May June July Aug. Sept. Oct. Nov. Dec.																					
+0.3 +0.2 +0.1 —0.1 —0.2 —0.2 —0.3 —0.2 —0.1 +0.1 +0.2 +0.3																					

Month	Jan.	Feb.	Mar.	April	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.
Correction to sun's alt. }	+0.3	+0.2	+0.1	—0.1	—0.2	—0.2	—0.3	—0.2	—0.1	+0.1	+0.2	+0.3

A STAR. Subtract the Corr.

	Height of the Eye in Feet.																		
	10	12	14	16	18	20	22	24	26	28	30	32	34	37	40	45	50	60	
0	14.8	15.1	15.4	15.7	16.0	16.2	16.4	16.6	16.8	17.0	17.2	17.4	17.6	17.9	18.1	18.4	18.8	19.6	0
4½	13.8	14.1	14.4	14.7	15.0	15.2	15.4	15.6	15.8	16.0	16.2	16.4	16.6	16.9	17.1	17.4	17.7	18.5	4½
6	12.9	13.2	13.5	13.8	14.1	14.3	14.5	14.7	14.9	15.1	15.3	15.5	15.7	16.0	16.2	16.5	16.9	17.6	6
6½	12.2	12.5	12.8	13.0	13.3	13.5	13.7	13.9	14.1	14.3	14.5	14.7	14.9	15.2	15.4	15.7	16.1	16.8	6½
7	11.5	11.8	12.1	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8	14.0	14.2	14.5	14.7	15.0	15.3	16.2	7
6½	11.0	11.3	11.6	11.9	12.1	12.3	12.5	12.7	12.9	13.1	13.3	13.5	13.7	13.9	14.2	14.4	14.8	15.6	6½
7	10.5	10.8	11.1	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.7	14.0	14.4	15.0	7
8	9.6	9.9	10.2	10.5	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.9	13.2	13.6	14.3	8
9	8.9	9.2	9.5	9.8	10.1	10.3	10.5	10.7	10.9	11.1	11.3	11.5	11.7	11.9	12.2	12.6	13.0	13.7	9
10	8.4	8.7	9.0	9.3	9.6	9.8	10.0	10.2	10.4	10.6	10.8	10.9	11.1	11.3	11.6	12.0	12.3	13.0	10
11	7.9	8.2	8.5	8.8	9.1	9.3	9.5	9.7	9.9	10.1	10.3	10.4	10.6	10.8	11.1	11.5	11.9	12.5	11
12	7.5	7.8	8.1	8.4	8.6	8.9	9.1	9.3	9.5	9.7	9.9	10.0	10.2	10.4	10.6	11.0	11.4	12.0	12
14	6.9	7.2	7.5	7.8	8.0	8.3	8.5	8.7	8.9	9.1	9.3	9.4	9.6	9.8	10.1	10.5	10.8	11.5	14
16	6.4	6.7	7.0	7.3	7.5	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.1	9.3	9.6	10.0	10.4	11.0	16
18	6.0	6.3	6.6	6.9	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.5	8.7	8.9	9.2	9.6	10.0	10.6	18
20	5.7	6.0	6.3	6.6	6.9	7.1	7.3	7.5	7.7	7.9	8.1	8.2	8.4	8.6	8.9	9.3	9.6	10.2	20
22	5.5	5.8	6.1	6.3	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.1	8.4	8.6	8.9	9.3	9.8	22
25	5.2	5.5	5.8	6.0	6.3	6.5	6.7	6.9	7.1	7.3	7.5	7.7	7.8	8.1	8.3	8.6	9.0	9.5	25
30	4.8	5.1	5.4	5.6	5.9	6.1	6.3	6.5	6.7	6.9	7.1	7.2	7.4	7.7	7.9	8.3	8.7	9.3	30
35	4.5	4.8	5.1	5.3	5.6	5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	8.0	8.4	9.0	35
40	4.3	4.6	4.9	5.1	5.3	5.5	5.8	6.0	6.2	6.4	6.5	6.7	6.9	7.1	7.4	7.8	8.2	8.7	40
45	4.1	4.4	4.7	4.9	5.1	5.4	5.6	5.8	6.0	6.2	6.3	6.5	6.7	7.0	7.2	7.6	8.0	8.5	45
50	3.9	4.2	4.5	4.7	5.0	5.2	5.4	5.6	5.8	6.0	6.2	6.4	6.5	6.8	7.0	7.4	7.8	8.3	50
60	3.7	4.0	4.2	4.5	4.8	5.0	5.2	5.4	5.6	5.8	6.0	6.1	6.3	6.6	6.8	7.1	7.5	8.1	60
70	3.5	3.8	4.0	4.3	4.5	4.7	5.0	5.2	5.4	5.6	5.7	5.9	6.1	6.3	6.6	6.9	7.3	7.9	70
80	3.3	3.5	3.8	4.1	4.3	4.6	4.8	5.0	5.2	5.4	5.6	5.7	5.9	6.2	6.4	6.7	7.1	7.7	80
90	3.1	3.4	3.7	3.9	4.2	4.4	4.6	4.8	5.0	5.2	5.4	5.6	5.7	5.9	6.2	6.4	6.7	7.6	90

CORRESPONDING THERMOMETERS, Fahrenheit, Centigrade, Réaumur.					
F.	C.	R.	F.	C.	R.
0	-17.8	-14.2	60	15.6	12.4
1	-17.2	-13.8	61	16.1	12.9
2	-16.7	-13.3	62	16.7	13.3
3	-16.1	-12.9	63	17.2	13.8
4	-15.6	-12.4	64	17.8	14.2
5	-15.0	-12.0	65	18.3	14.7
6	-14.4	-11.6	66	18.9	15.1
7	-13.9	-11.1	67	19.4	15.6
8	-13.3	-10.7	68	20.0	16.0
9	-12.8	-10.2	69	20.6	16.4
10	-12.2	-9.8	70	21.1	16.9
11	-11.7	-9.3	71	21.7	17.3
12	-11.1	-8.9	72	22.2	17.8
13	-10.6	-8.4	73	22.8	18.2
14	-10.0	-8.0	74	23.3	18.7
15	-9.4	-7.5	75	23.9	19.1
16	-8.9	-7.1	76	24.4	19.6
17	-8.3	-6.7	77	25.0	20.0
18	-7.8	-6.2	78	25.6	20.5
19	-7.2	-5.8	79	26.1	20.9
20	-6.7	-5.3	80	26.7	21.3
21	-6.1	-4.9	81	27.2	21.8
22	-5.6	-4.4	82	27.8	22.2
23	-5.0	-4.0	83	28.3	22.7
24	-4.4	-3.6	84	28.9	23.1
25	-3.9	-3.1	85	29.4	23.6
26	-3.3	-2.7	86	30.0	24.0
27	-2.8	-2.2	87	30.6	24.4
28	-2.2	-1.8	88	31.1	24.9
29	-1.7	-1.3	89	31.7	25.3
30	-1.1	-0.9	90	32.2	25.8
31	-0.6	-0.4	91	32.8	26.2
32	0	0	92	33.3	26.7
33	0.6	0.4	93	33.9	27.1
34	1.1	0.9	94	34.4	27.6
35	1.7	1.3	95	35.0	28.0
36	2.2	1.8	96	35.6	28.4
37	2.8	2.2	97	36.1	28.9
38	3.3	2.7	98	36.7	29.3
39	3.9	3.1	99	37.2	29.8
40	4.4	3.6	100	37.8	30.2
41	5.0	4.0	101	38.3	30.7
42	5.6	4.4	102	38.9	31.1
43	6.1	4.9	103	39.4	31.6
44	6.7	5.3	104	40.0	32.0
45	7.2	5.8	105	40.6	32.4
46	7.8	6.2	106	41.1	32.9
47	8.3	6.7	107	41.7	33.3
48	8.9	7.1	108	42.2	33.8
49	9.4	7.5	109	42.8	34.2
50	10.0	8.0	110	43.3	34.7
51	10.6	8.4	111	43.9	35.1
52	11.1	8.9	112	44.4	35.5
53	11.7	9.3	113	45.0	36.0
54	12.2	9.8	114	45.6	36.4
55	12.8	10.2	115	46.1	36.9
56	13.3	10.7	116	46.7	37.3
57	13.9	11.1	117	47.2	37.8
58	14.4	11.6	118	47.8	38.2
59	15.0	12.0	119	48.3	38.7
60	15.6	12.4	120	48.9	39.1

CORRESPONDING FRENCH & ENGLISH MEASURES							
Fr. Kilomètre, Mètre, Décimètre, Centimètre, Millimètre. Eng. Nautical Miles, Feet, Inches.						Barometer Scales	
Fr.	English					Fr.	Eng.
No.	Miles corr. to Kil.	Feet corr. to Mètre.	Feet corr. to Décim.	In. corr. to Cent.	In. corr. to Mill.	MM.	In.
1	0.539	3.28	0.33	0.39	0.04	640	25.2
2	1.079	6.56	0.66	0.79	0.08	643	25.3
3	1.618	9.84	0.98	1.18	0.12	645	25.4
4	2.158	13.12	1.31	1.57	0.16	648	25.5
5	2.697	16.40	1.64	1.97	0.20	650	25.6
6	3.237	19.68	1.97	2.36	0.24	653	25.7
7	3.776	22.97	2.30	2.76	0.28	655	25.8
8	4.316	26.25	2.62	3.15	0.31	658	25.9
9	4.855	29.53	2.95	3.54	0.35	660	26.0
10	5.394	32.81	3.28	3.94	0.39	663	26.1
20	10.79	65.62	6.56	7.87	0.79	665	26.2
30	16.18	98.43	9.84	11.81	1.18	668	26.3
40	21.58	131.2	13.1	15.75	1.57	670	26.4
50	26.97	164.0	16.4	19.69	1.97	673	26.5
60	32.37	196.9	19.7	23.62	2.36	676	26.6
70	37.76	229.7	23.0	27.56	2.76	678	26.7
80	43.15	262.5	26.2	31.50	3.15	681	26.8
90	48.55	295.3	29.5	35.43	3.54	683	26.9
100	53.94	328.1	32.8	39.4	3.94	686	27.0
200	107.9	656.2			7.87	688	27.1
300	161.8	984.3			11.81	691	27.2
400	215.8	1312.4			15.75	693	27.3
500	269.7	1640.4			19.68	696	27.4
600	323.7	1968.5			23.62	698	27.5
700	377.6	2296.6			27.56	701	27.6
800	431.5	2624.7			31.50	704	27.7
900	485.5	2952.8			35.43	706	27.8
1000	539.4	3280.9			39.37	709	27.9
						711	28.0
						714	28.1
						716	28.2
						719	28.3
						721	28.4
						724	28.5
						726	28.6
						729	28.7
						732	28.8
						734	28.9
						737	29.0
						739	29.1
						742	29.2
						744	29.3
						747	29.4
						749	29.5
						752	29.6
						754	29.7
						757	29.8
						759	29.9
						762	30.0
						765	30.1
						767	30.2
						770	30.3
						772	30.4
						775	30.5
						777	30.6
						780	30.7
						782	30.8
						785	30.9
						787	31.0

CORRECTIONS OF ALTITUDE OF THE SUN AND STARS

(Involving Dip, Refraction, ☉'s Semid. and Parallax).

FOR APPROXIMATE USE AT SEA.

The SUN. Add the Corr. to the Alt. of the Lower limb, except where marked —.

Height of the Eye in Feet.																				
Alt.	8	10	12	14	16	18	20	22	24	26	28	30	32	34	37	40	45	50	60	Alt.
4½	2.6	2.3	2.0	1.7	1.4	1.2	1.0	0.7	0.5	0.3	0.1	—	—	—	—	—	—	—	—	4½
5	3.5	3.2	2.9	2.6	2.4	2.1	1.9	1.6	1.4	1.2	1.0	0.8	0.7	0.5	0.2	0.0	—	—	—	5
5½	4.2	3.9	3.6	3.3	3.1	2.9	2.7	2.4	2.2	2.0	1.8	1.6	1.4	1.2	1.0	0.7	0.3	—	—	5½
6	4.9	4.6	4.3	4.0	3.7	3.5	3.3	3.1	2.9	2.6	2.4	2.3	2.1	1.9	1.7	1.4	1.0	0.6	0.0	6
6½	5.4	5.1	4.8	4.5	4.3	4.0	3.8	3.6	3.4	3.2	3.0	2.8	2.6	2.4	2.2	2.0	1.6	1.2	0.6	6½
7	6.0	5.6	5.3	5.0	4.8	4.6	4.3	4.1	3.9	3.7	3.5	3.3	3.1	2.9	2.7	2.5	2.1	1.7	1.0	7
8	6.7	6.4	6.1	5.8	5.6	5.3	5.1	4.9	4.7	4.5	4.3	4.1	3.9	3.7	3.5	3.3	2.9	2.6	1.9	8
9	7.4	7.1	6.8	6.5	6.3	6.0	5.8	5.6	5.4	5.2	5.0	4.8	4.6	4.4	4.2	4.0	3.6	3.3	2.6	9
10	8.0	7.7	7.4	7.1	6.8	6.6	6.4	6.1	5.9	5.7	5.5	5.4	5.2	5.0	4.8	4.5	4.2	3.9	3.2	10
11	8.5	8.1	7.8	7.6	7.3	7.1	6.8	6.6	6.4	6.2	6.0	5.8	5.7	5.5	5.3	5.0	4.7	4.3	3.7	11
12	8.9	8.6	8.2	8.0	7.7	7.5	7.2	7.0	6.8	6.6	6.4	6.2	6.1	5.9	5.7	5.5	5.1	4.7	4.1	12
14	9.5	9.2	8.9	8.6	8.3	8.1	7.9	7.6	7.4	7.2	7.1	6.9	6.7	6.5	6.3	6.1	5.7	5.4	4.7	14
16	10.0	9.7	9.4	9.1	8.8	8.6	8.4	8.1	8.0	7.8	7.6	7.4	7.2	7.0	6.8	6.6	6.3	5.9	5.2	16
18	10.4	10.1	9.8	9.5	9.2	9.0	8.8	8.5	8.3	8.1	7.9	7.7	7.6	7.4	7.2	6.9	6.6	6.3	5.6	18
20	10.7	10.4	10.1	9.8	9.5	9.3	9.1	8.9	8.7	8.5	8.3	8.1	7.9	7.7	7.5	7.2	6.9	6.6	5.9	20
22	11.0	10.6	10.3	10.1	9.8	9.6	9.3	9.1	8.9	8.7	8.5	8.3	8.2	8.0	7.7	7.5	7.2	6.8	6.2	22
25	11.3	10.9	10.6	10.4	10.1	9.9	9.6	9.4	9.2	9.0	8.8	8.7	8.5	8.3	8.1	7.9	7.5	7.1	6.5	25
30	11.7	11.3	11.0	10.8	10.5	10.3	10.0	9.8	9.6	9.4	9.2	9.1	8.9	8.7	8.4	8.2	7.8	7.5	6.8	30
35	12.0	11.6	11.3	11.1	10.8	10.6	10.3	10.1	9.9	9.7	9.5	9.4	9.2	9.0	8.7	8.5	8.1	7.8	7.1	35
40	12.2	11.8	11.5	11.3	11.0	10.8	10.6	10.3	10.1	9.9	9.7	9.6	9.4	9.2	9.0	8.8	8.4	8.0	7.3	40
45	12.4	12.0	11.7	11.5	11.2	11.0	10.8	10.5	10.3	10.1	9.9	9.7	9.5	9.4	9.1	8.9	8.5	8.2	7.5	45
50	12.5	12.2	11.9	11.6	11.3	11.1	10.9	10.7	10.5	10.3	10.1	9.9	9.7	9.5	9.3	9.1	8.7	8.3	7.7	50
60	12.7	12.4	12.1	11.8	11.6	11.3	11.1	10.9	10.7	10.5	10.3	10.1	9.9	9.8	9.5	9.3	8.9	8.5	7.9	60
70	12.9	12.6	12.3	12.0	11.8	11.5	11.3	11.1	10.9	10.7	10.5	10.3	10.1	9.9	9.7	9.5	9.1	8.7	8.1	70
80	13.1	12.7	12.4	12.2	11.9	11.7	11.4	11.2	11.0	10.8	10.6	10.4	10.3	10.1	9.8	9.6	9.2	8.9	8.3	80
90	13.2	12.9	12.6	12.3	12.0	11.8	11.6	11.4	11.2	11.0	10.8	10.6	10.4	10.2	10.0	9.8	9.4	9.0	8.4	90
Month	Jan.	Feb.	Mar.	April	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.								
Correction to sun's alt.	+0.3	+0.2	+0.1	—0.1	—0.2	—0.2	—0.3	—0.2	—0.1	+0.1	+0.2	+0.3								

Month	Jan.	Feb.	Mar.	April	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.
Correction to sun's alt.	+0.3	+0.2	+0.1	—0.1	—0.2	—0.2	—0.3	—0.2	—0.1	+0.1	+0.2	+0.3

A STAR. Subtract the Corr.

	Height of the Eye in Feet.																		
	10	12	14	16	18	20	22	24	26	28	30	32	34	37	40	45	50	60	
4	14.8	15.1	15.4	15.7	16.0	16.2	16.4	16.6	16.8	17.0	17.2	17.4	17.6	17.9	18.1	18.4	18.8	19.6	4
4 $\frac{1}{2}$	13.8	14.1	14.4	14.7	15.0	15.2	15.4	15.6	15.8	16.0	16.2	16.4	16.6	16.9	17.1	17.4	17.7	18.5	4 $\frac{1}{2}$
5	12.9	13.2	13.5	13.8	14.1	14.3	14.5	14.7	14.9	15.1	15.3	15.5	15.7	16.0	16.2	16.5	16.9	17.6	5
5 $\frac{1}{2}$	12.2	12.5	12.8	13.0	13.3	13.5	13.7	13.9	14.1	14.3	14.5	14.7	14.9	15.2	15.4	15.7	16.1	16.8	5 $\frac{1}{2}$
6	11.5	11.8	12.1	12.4	12.6	12.8	13.0	13.2	13.4	13.6	13.8	14.0	14.2	14.5	14.7	15.0	15.3	16.2	6
6 $\frac{1}{2}$	11.0	11.3	11.6	11.9	12.1	12.3	12.5	12.7	12.9	13.1	13.3	13.5	13.7	13.9	14.2	14.4	14.8	15.6	6 $\frac{1}{2}$
7	10.5	10.8	11.1	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.8	13.0	13.2	13.4	13.7	14.0	14.4	15.0	7
8	9.6	9.9	10.2	10.5	10.8	11.0	11.2	11.4	11.6	11.8	12.0	12.2	12.4	12.6	12.9	13.2	13.6	14.3	8
9	8.9	9.2	9.5	9.8	10.1	10.3	10.5	10.7	10.9	11.1	11.3	11.5	11.7	11.9	12.2	12.6	13.0	13.7	9
10	8.4	8.7	9.0	9.3	9.6	9.8	10.0	10.2	10.4	10.6	10.8	10.9	11.1	11.3	11.6	12.0	12.3	13.0	10
11	7.9	8.2	8.5	8.8	9.1	9.3	9.5	9.7	9.9	10.1	10.3	10.4	10.6	10.8	11.1	11.5	11.9	12.5	11
12	7.5	7.8	8.1	8.4	8.6	8.9	9.1	9.3	9.5	9.7	9.9	10.0	10.2	10.4	10.6	11.0	11.4	12.0	12
14	6.9	7.2	7.5	7.8	8.0	8.3	8.5	8.7	8.9	9.1	9.3	9.4	9.6	9.8	10.1	10.5	10.8	11.5	14
16	6.4	6.7	7.0	7.3	7.5	7.8	8.0	8.2	8.4	8.6	8.8	9.0	9.1	9.3	9.6	10.0	10.4	11.0	16
18	6.0	6.3	6.6	6.9	7.2	7.4	7.6	7.8	8.0	8.2	8.4	8.5	8.7	8.9	9.2	9.6	10.0	10.6	18
20	5.7	6.0	6.3	6.6	6.9	7.1	7.3	7.5	7.7	7.9	8.1	8.2	8.4	8.6	8.9	9.2	9.6	10.2	20
22	5.5	5.8	6.1	6.3	6.6	6.8	7.0	7.2	7.4	7.6	7.8	8.0	8.1	8.4	8.6	8.9	9.3	9.8	22
25	5.2	5.5	5.8	6.0	6.3	6.5	6.7	6.9	7.1	7.3	7.5	7.7	7.8	8.1	8.3	8.6	9.0	9.5	25
30	4.8	5.1	5.4	5.6	5.9	6.1	6.3	6.5	6.7	6.9	7.1	7.2	7.4	7.7	7.9	8.3	8.7	9.3	30
35	4.5	4.8	5.1	5.3	5.6	5.8	6.0	6.2	6.4	6.6	6.8	7.0	7.2	7.4	7.6	8.0	8.4	9.0	35
40	4.3	4.6	4.9	5.1	5.3	5.5	5.8	6.0	6.2	6.4	6.5	6.7	6.9	7.1	7.4	7.8	8.2	8.7	40
45	4.1	4.4	4.7	4.9	5.1	5.4	5.6	5.8	6.0	6.2	6.3	6.5	6.7	7.0	7.2	7.6	8.0	8.5	45
50	3.9	4.2	4.5	4.7	5.0	5.2	5.4	5.6	5.8	6.0	6.2	6.4	6.5	6.8	7.0	7.4	7.8	8.3	50
60	3.7	4.0	4.2	4.5	4.8	5.0	5.2	5.4	5.6	5.8	6.0	6.1	6.3	6.6	6.8	7.1	7.5	8.1	60
70	3.5	3.8	4.0	4.3	4.5	4.7	5.0	5.2	5.4	5.6	5.7	5.9	6.1	6.3	6.6	6.9	7.3	7.9	70
80	3.3	3.5	3.8	4.1	4.3	4.6	4.8	5.0	5.2	5.4	5.6	5.7	5.9	6.2	6.4	6.7	7.1	7.7	80
90	3.1	3.4	3.7	3.9	4.2	4.4	4.6	4.8	5.0	5.2	5.4	5.6	5.7	6.0	6.2	6.6	7.0	7.6	90

CORRECTION OF THE MOON'S APPARENT ALTITUDE

(Barometer, 30 inches. Fahrenheit's Thermometer, 50°)

App. Alt.	Horizontal Parallax										" of Par.	Corr. for " of Par. add.					Cor. for " of Alt.
	53'	54'	55'	56'	57'	58'	59'	00'	01'	0"		1"	2"	3"	4"		
0 0	19	14	20	14	21	14	22	14	23	14	24	14	25	14	26	14	27
10	21	6	22	6	23	6	24	6	25	6	26	6	27	6	28	6	29
20	22	51	23	51	24	51	25	51	26	51	27	51	28	51	29	51	30
30	24	28	25	28	26	28	27	28	28	28	29	28	30	28	31	28	32
40	25	58	26	58	27	58	28	58	29	58	30	58	31	58	32	58	33
50	27	21	28	21	29	21	30	21	31	21	32	21	33	21	34	21	35
1 0	28	39	29	39	30	39	31	39	32	39	33	39	34	39	35	39	36
10	29	49	30	49	31	49	32	49	33	49	34	49	35	49	36	49	37
20	30	56	31	56	32	56	33	56	34	56	35	56	36	56	37	56	38
30	31	57	32	57	33	57	34	57	35	57	36	57	37	57	38	57	39
40	32	54	33	54	34	54	35	54	35	54	37	54	38	54	39	54	40
50	33	46	34	46	35	46	36	46	37	46	38	46	39	46	40	46	41
2 0	34	36	35	36	36	37	36	38	36	39	36	40	36	41	36	42	36
10	35	22	36	22	37	22	38	22	39	22	40	22	41	22	42	22	43
20	36	4	37	4	38	4	39	4	40	4	41	4	42	4	43	4	44
30	36	44	37	44	38	44	39	44	40	44	41	44	42	44	43	44	44
40	37	21	38	21	39	21	40	21	41	21	42	21	43	21	44	21	45
50	37	55	38	55	39	55	40	55	41	55	42	55	43	55	44	55	45
3 0	38	28	39	28	40	28	41	28	42	28	43	28	44	28	45	28	46
10	38	59	39	58	40	58	41	58	42	58	43	58	44	58	45	58	46
20	39	27	40	27	41	27	42	27	43	27	44	27	45	27	46	27	47
30	39	53	40	53	41	53	42	53	43	53	44	53	45	53	46	53	47
40	40	19	41	18	42	18	43	18	44	18	45	18	46	18	47	18	48
50	40	42	41	42	42	43	42	44	42	45	42	46	42	47	42	48	41
4 0	41	5	42	5	43	4	44	4	45	4	46	4	47	4	48	4	49
10	41	26	42	26	43	25	44	25	45	25	46	25	47	25	48	25	49
20	41	46	42	45	43	45	44	45	45	45	46	45	47	45	48	44	49
30	42	4	43	4	44	4	45	4	46	4	47	3	48	3	49	3	50
40	42	22	43	22	44	22	45	21	46	21	47	21	48	21	49	21	50
50	42	39	43	38	44	38	45	38	46	38	47	37	48	37	49	37	50
5 0	42	54	43	54	44	54	45	54	46	54	47	53	48	53	49	53	50
10	43	9	44	9	45	9	46	9	47	9	48	8	49	8	50	8	51
20	43	24	44	23	45	23	46	23	47	23	48	22	49	22	50	22	51
30	43	37	44	37	45	37	46	36	47	36	48	36	49	35	50	35	51
40	43	50	44	50	45	49	46	49	47	49	48	49	49	48	51	48	50
50	44	2	45	2	46	1	47	1	48	1	49	0	50	0	51	0	52
6 0	44	14	45	13	46	13	47	13	48	12	49	12	50	12	51	11	52
10	44	24	45	24	46	24	47	23	48	23	49	23	50	22	51	22	52
20	44	35	45	34	46	34	47	34	48	33	49	33	50	33	51	32	52
30	44	45	45	44	46	44	47	44	48	43	49	43	50	43	51	42	52
40	44	54	45	54	46	53	47	53	48	53	49	52	51	52	52	52	50
50	45	4	46	3	47	3	48	2	49	2	50	1	51	1	52	0	53
7 0	45	12	46	12	47	11	48	11	49	11	50	10	51	10	52	9	53
10	45	21	46	20	47	20	48	19	49	19	50	18	51	18	52	17	53
20	45	29	46	28	47	28	48	27	49	27	50	26	51	26	52	25	53
30	45	36	46	35	47	35	48	34	49	34	50	33	51	33	52	32	53
40	45	43	46	42	47	42	48	41	49	41	50	40	51	40	52	39	53
50	45	49	46	49	47	48	48	49	47	50	47	51	46	52	45	53	50
8 0	45	55	46	55	47	54	48	54	49	53	50	53	51	52	52	53	51
10	46	2	47	1	48	0	49	0	49	59	50	59	51	58	52	57	53
20	46	7	47	7	48	6	49	5	50	5	51	4	52	4	53	3	54
30	46	13	47	12	48	12	49	11	50	10	51	10	52	9	53	8	54
40	46	18	47	17	48	17	49	16	50	15	51	15	52	14	53	13	54
50	46	23	47	23	48	22	49	21	50	20	51	20	52	19	53	18	54
9 0	46	28	47	27	48	27	49	26	50	25	51	24	52	24	53	23	54
10	46	33	47	32	48	31	49	31	50	30	51	29	52	28	53	28	54
20	46	37	47	36	48	36	49	36	50	35	51	34	52	34	53	33	54
30	46	41	47	41	48	40	49	39	50	38	51	37	52	37	53	36	54
40	46	45	47	45	48	44	49	43	50	42	51	41	52	40	53	39	54
50	46	49	47	48	48	47	49	47	50	46	51	45	52	44	53	43	54

CORRECTION OF THE MOON'S APPARENT ALTITUDE

(Barometer, 30 inches. Fahrenheit's Thermometer, 50°)

App. Alt.	Horizontal Parallax										" of Par.	Corr. for " of Par. add.					Corr. for " of Alt.
	53'	54'	55'	56'	57'	58'	59'	60'	61'	0"		2"	4"	6"	8"		
10 0	46	53	47	52	48	51	49	50	50	49	51	48	52	47	53	46	0
10 10	46	56	47	55	48	54	49	53	50	53	51	52	52	51	53	50	10
20 0	47	04	47	59	48	58	49	57	50	56	51	55	52	54	53	54	20
20 10	47	07	48	59	49	59	50	58	51	58	52	57	53	56	54	55	30
30 0	47	10	48	59	49	59	50	58	51	58	52	57	53	56	54	55	40
30 10	47	13	48	59	49	59	50	58	51	58	52	57	53	56	54	55	50
40 0	47	16	48	59	49	59	50	58	51	58	52	57	53	56	54	55	60
40 10	47	19	48	59	49	59	50	58	51	58	52	57	53	56	54	55	70
50 0	47	22	48	59	49	59	50	58	51	58	52	57	53	56	54	55	80
50 10	47	25	48	59	49	59	50	58	51	58	52	57	53	56	54	55	90
11 0	47	28	48	59	49	59	50	58	51	58	52	57	53	56	54	55	0
11 10	47	31	48	59	49	59	50	58	51	58	52	57	53	56	54	55	10
20 0	47	34	48	59	49	59	50	58	51	58	52	57	53	56	54	55	20
20 10	47	37	48	59	49	59	50	58	51	58	52	57	53	56	54	55	30
30 0	47	40	48	59	49	59	50	58	51	58	52	57	53	56	54	55	40
30 10	47	43	48	59	49	59	50	58	51	58	52	57	53	56	54	55	50
40 0	47	46	48	59	49	59	50	58	51	58	52	57	53	56	54	55	60
40 10	47	49	48	59	49	59	50	58	51	58	52	57	53	56	54	55	70
50 0	47	52	48	59	49	59	50	58	51	58	52	57	53	56	54	55	80
50 10	47	55	48	59	49	59	50	58	51	58	52	57	53	56	54	55	90
12 0	47	58	48	59	49	59	50	58	51	58	52	57	53	56	54	55	0
12 10	47	61	48	59	49	59	50	58	51	58	52	57	53	56	54	55	10
20 0	47	64	48	59	49	59	50	58	51	58	52	57	53	56	54	55	20
20 10	47	67	48	59	49	59	50	58	51	58	52	57	53	56	54	55	30
30 0	47	70	48	59	49	59	50	58	51	58	52	57	53	56	54	55	40
30 10	47	73	48	59	49	59	50	58	51	58	52	57	53	56	54	55	50
40 0	47	76	48	59	49	59	50	58	51	58	52	57	53	56	54	55	60
40 10	47	79	48	59	49	59	50	58	51	58	52	57	53	56	54	55	70
50 0	47	82	48	59	49	59	50	58	51	58	52	57	53	56	54	55	80
50 10	47	85	48	59	49	59	50	58	51	58	52	57	53	56	54	55	90
13 0	47	88	48	59	49	59	50	58	51	58	52	57	53	56	54	55	0
13 10	47	91	48	59	49	59	50	58	51	58	52	57	53	56	54	55	10
20 0	47	94	48	59	49	59	50	58	51	58	52	57	53	56	54	55	20
20 10	47	97	48	59	49	59	50	58	51	58	52	57	53	56	54	55	30
30 0	47	100	48	59	49	59	50	58	51	58	52	57	53	56	54	55	40
30 10	47	103	48	59	49	59	50	58	51	58	52	57	53	56	54	55	50
40 0	47	106	48	59	49	59	50	58	51	58	52	57	53	56	54	55	60
40 10	47	109	48	59	49	59	50	58	51	58	52	57	53	56	54	55	70
50 0	47	112	48	59	49	59	50	58	51	58	52	57	53	56	54	55	80
50 10	47	115	48	59	49	59	50	58	51	58	52	57	53	56	54	55	90
14 0	47	118	48	59	49	59	50	58	51	58	52	57	53	56	54	55	0
14 10	47	121	48	59	49	59	50	58	51	58	52	57	53	56	54	55	10
20 0	47	124	48	59	49	59	50	58	51	58	52	57	53	56	54	55	20
20 10	47	127	48	59	49	59	50	58	51	58	52	57	53	56	54	55	30
30 0	47	130	48	59	49	59	50	58	51	58	52	57	53	56	54	55	40
30 10	47	133	48	59	49	59	50	58	51	58	52	57	53	56	54	55	50
40 0	47	136	48	59	49	59	50	58	51	58	52	57	53	56	54	55	60
40 10	47	139	48	59	49	59	50	58	51	58	52	57	53	56	54	55	70
50 0	47	142	48	59	49	59	50	58	51	58	52	57	53	56	54	55	80
50 10	47	145	48	59	49	59	50	58	51	58	52	57	53	56	54	55	90
15 0	47	148	48	59	49	59	50	58	51	58	52	57	53	56	54	55	0
15 10	47	151	48	59	49	59	50	58	51	58	52	57	53	56	54	55	10
20 0	47	154	48	59	49	59	50	58	51	58	52	57	53	56	54	55	20
20 10	47	157	48	59	49	59	50	58	51	58	52	57	53	56	54	55	30
30 0	47	160	48	59	49	59	50	58	51	58	52	57	53	56	54	55	40
30 10	47	163	48	59	49	59	50	58	51	58	52	57	53	56	54	55	50
40 0	47	166	48	59	49	59	50	58	51	58	52	57	53	56	54	55	60
40 10	47	169	48	59	49	59	50	58	51	58	52	57	53	56	54	55	70
50 0	47	172	48	59	49	59	50	58	51	58	52	57	53	56	54	55	80
50 10	47	175	48	59	49	59	50	58	51	58	52	57	53	56	54	55	90
16 0	47	178	48	59	49	59	50	58	51	58	52	57	53	56	54	55	0
16 10	47	181	48	59	49	59	50	58	51	58	52	57	53	56	54	55	10
20 0	47	184	48	59	49	59	50	58	51	58	52	57	53	56	54	55	20
20 10	47	187	48	59	49	59	50	58	51	58	52	57	53	56	54	55	30
30 0	47	190	48	59	49	59	50	58	51	58	52	57	53	56	54	55	40
30 10	47	193	48	59	49	59	50	58	51	58	52	57	53	56	54	55	50
40 0	47	196	48	59	49	59	50	58	51	58	52	57	53	56	54	55	60
40 10	47	199	48	59	49	59	50	58	51	58	52	57	53	56	54	55	70
50 0	47	202	48	59	49	59	50	58	51	58	52	57	53	56	54	55	80
50 10	47	205	48	59	49	59	50	58	51	58	52	57	53	56	54	55	90
17 0	47	208	48	59	49	59	50	58	51	58	52	57	53	56	54	55	0
17 10	47	211	48	59	49	59	50	58	51	58	52	57	53	56	54	55	10
20 0	47	214	48	59	49	59	50	58	51	58	52	57	53	56	54	55	20
20 10	47	217	48	59	49	59	50	58	51	58	52	57	53	56	54	55	30
30 0	47	220	48	59	49	59	50	58	51	58	52	57	53	56	54	55	40
30 10	47	223	48	59	49	59	50	58	51	58	52	57	53	56	54	55	50
40 0	47	226	48	59	49	59	50	58	51	58	52	57	53	56	54	55	60
40 10	47	229	48	59	49	59	50	58	51	58	52	57	53	56	54	55	70
50 0	47	232	48	59	49	59	50	58	51	58	52	57	53	56	54	55	80
50 10	47	235	48	59	49	59	50	58	51	58	52	57	53	56	54	55	90
18 0	47	238	48	59	49	59	50	58	51	58	52	57	53	56	54	55	0
18 10	47	241	48	59	49	59	50	58	51	58	52	57	53	56	54	55	10
20 0	47	244	48	59	49	59	50	58	51	58	52	57	53	56	54	55	20
20 10	47	247	48	59	49	59	50	58	51	58	52	57	53	56	54	55	30
30 0	47	250	48	59	49	59	50	58	51	58	52	57	53	56	54	55	40
30 10	47	253	48	59	49	59	50	58	51	58	52	57	53	56	54	55	50
40 0	47	256	48	59	49	59	50	58	51	58	52	57	53	56	54	55	60
40 10	47	259	48	59	49	59	50	58	51	58	52	57	53</				

CORRECTION OF THE MOON'S APPARENT ALTITUDE

(Barometer, 30 inches. Fahrenheit's Thermometer, 60°)

App Alt.	Horizontal Parallax										" of Pa.	Corr. for " of Par. add.					Cor. for " of Alt.
	53'	54'	55'	56'	57'	58'	59'	60'	61'	0"		1"	2"	3"	4"		
20 0	47	10.48	7.49	3.49	59.50	56.51	52.52	49.53	45.54	42	0	0	2	4	6	7	sub.
10 47	9.48	5.49	1.49	58.50	54.51	50.52	47.53	43.54	39	10	9	11	13	15	17		1
20 47	7.48	3.48	59.49	56.50	52.51	48.52	44.53	41.54	37	20	19	21	22	24	26		2
30 47	5.48	1.48	57.49	54.50	50.51	46.52	42.53	38.54	35	30	28	30	32	34	36		3
40 47	3.47	59.48	55.49	51.50	48.51	44.52	40.53	36.54	32	40	37	39	41	43	45		4
50 47	1.47	57.48	53.49	49.50	45.51	41.52	38.53	34.54	30	50	47	49	51	52	54		5
21 0	46	59.47	55.48	51.49	47.50	43.51	39.52	35.53	31.54	27	0	0	2	4	6	7	6
10 46	57.47	53.48	49.49	45.50	41.51	37.52	33.53	29.54	25	10	9	11	13	15	17		7
20 46	55.47	51.48	47.49	43.50	39.51	35.52	31.53	26.54	22	20	19	20	22	24	26		8
30 46	53.47	49.48	44.49	40.50	36.51	32.52	28.53	24.54	19	30	28	30	32	34	35		9
40 46	51.47	46.48	42.49	38.50	34.51	29.52	25.53	21.54	17	40	37	39	41	43	45		
50 46	48.47	44.48	40.49	35.50	31.51	27.52	23.53	18.54	14	50	47	48	50	52	54		
22 0	46	46.47	42.48	37.49	33.50	29.51	24.52	20.53	16.54	11	0	0	2	4	6	7	1
10 46	44.47	39.48	35.49	30.50	26.51	22.52	17.53	13.54	8	10	9	11	13	15	17		2
20 46	41.47	37.48	32.49	28.50	23.51	19.52	14.53	10.54	5	20	18	20	22	24	26		3
30 46	39.47	34.48	30.49	25.50	21.51	16.52	12.53	7.54	3	30	28	30	31	33	35		4
40 46	36.47	32.48	27.49	23.50	18.51	13.52	9.53	4.54	0	40	37	39	41	43	44		5
50 46	34.47	29.48	25.49	20.50	15.51	11.52	6.53	1.53	57	50	46	48	50	52	54		
23 0	46	32.47	27.48	22.49	17.50	12.51	8.52	3.53	58	53	53	0	2	4	6	7	1
10 46	29.47	24.48	19.49	15.50	10.51	5.52	0.53	55.53	50	10	9	11	13	15	17		2
20 46	26.47	22.48	17.49	12.50	7.51	2.52	57.52	52.53	47	20	18	20	22	24	26		3
30 46	24.47	19.48	14.49	9.50	4.51	59.51	54.52	49.53	44	30	28	29	31	33	35		4
40 46	21.47	16.48	11.49	6.50	1.51	56.51	51.52	46.53	41	40	37	39	40	42	44		5
50 46	18.47	13.48	8.49	3.49	58.50	53.51	48.52	43.53	38	50	46	48	50	51	53		
24 0	46	16.47	11.48	5.49	0.49	55.50	50.51	45.52	39.53	34	0	0	2	4	5	7	1
10 46	13.47	8.48	2.48	57.49	52.50	47.51	41.52	36.53	31	10	9	11	13	15	16		2
20 46	10.47	5.47	59.48	54.49	49.50	44.51	38.52	33.53	28	20	18	20	22	24	25		3
30 46	7.47	2.47	56.48	51.49	46.50	40.51	35.52	30.53	24	30	27	29	31	33	35		4
40 46	4.46	59.47	54.48	49.49	43.50	37.51	32.52	26.53	21	40	36	38	40	42	44		5
50 46	2.46	56.47	51.48	45.49	39.50	34.51	28.52	23.53	17	50	46	47	49	51	53		
25 0	45	59.46	53.47	47.48	42.49	36.50	31.51	25.52	19.53	14	0	0	2	4	5	7	1
10 45	56.46	50.47	44.48	39.49	33.50	27.51	21.52	16.53	10	10	9	11	13	14	16		2
20 45	53.46	47.47	41.48	35.49	29.50	24.51	18.52	12.53	6	20	18	20	22	23	25		3
30 45	49.46	44.47	38.48	32.49	26.50	20.51	14.52	9.53	3	30	27	29	31	33	34		4
40 45	46.46	40.47	35.48	29.49	23.50	17.51	11.52	5.53	59	40	36	38	40	42	43		5
50 45	43.46	37.47	31.48	25.49	19.50	13.51	7.52	1.53	58	50	45	47	48	51	52		
26 0	45	40.46	34.47	28.48	22.49	16.50	10.51	4.52	58.52	52	0	0	2	4	5	7	1
10 45	37.46	31.47	25.48	19.49	12.50	6.51	0.52	54.52	48	10	9	11	13	14	16		2
20 45	34.46	27.47	21.48	15.49	9.50	3.50	56.51	50.52	44	20	18	20	22	23	25		3
30 45	31.46	24.47	18.48	11.49	5.49	59.50	53.51	46.52	40	30	27	29	30	32	34		4
40 45	27.46	21.47	14.48	8.49	2.49	55.50	49.51	42.52	36	40	36	38	39	41	43		5
50 45	24.46	17.47	11.48	4.48	58.49	51.50	45.51	38.52	32	50	45	47	48	50	52		
27 0	45	20.46	14.47	7.48	1.48	54.49	48.50	41.51	35.52	28	0	0	2	4	5	7	1
10 45	17.46	10.47	4.47	57.48	50.49	44.50	37.51	31.52	24	10	9	11	12	14	16		2
20 45	13.46	7.47	0.47	53.48	47.49	40.50	33.51	27.52	20	20	18	20	21	23	25		3
30 45	10.46	3.46	56.47	50.48	43.49	36.50	29.51	23.52	16	30	27	28	30	32	34		4
40 45	6.46	0.46	53.47	46.48	39.49	32.50	25.51	19.52	12	40	35	37	39	41	43		5
50 45	3.45	56.46	49.47	42.48	35.49	28.50	21.51	14.52	7	50	44	46	48	50	52		
28 0	44	59.45	52.46	45.47	38.48	31.49	24.50	17.51	10.52	3	0	0	2	4	5	7	1
10 44	56.45	49.46	42.47	34.48	27.49	20.50	13.51	6.52	59	10	9	11	12	14	16		2
20 44	52.45	45.46	38.47	31.48	23.49	16.50	9.51	2.52	55	20	18	19	21	23	25		3
30 44	48.45	41.46	34.47	27.48	19.49	12.50	5.50	58.51	50	30	26	28	30	32	33		4
40 44	45.45	37.46	30.47	23.48	15.49	8.50	1.50	53.51	46	40	35	37	39	40	42		5
50 44	41.45	34.46	26.47	19.48	11.49	4.49	56.50	49.51	42	50	44	46	47	49	51		
29 0	44	37.45	30.46	22.47	15.48	7.49	0.49	52.50	45.51	37	0	0	2	3	5	7	1
10 44	34.45	26.46	18.47	11.48	3.48	56.49	48.50	40.51	33	10	9	10	12	14	16		2
20 44	30.45	22.46	14.47	7.47	59.48	51.49	44.50	36.51	28	20	17	19	21	23	24		3
30 44	26.45	18.46	10.47	2.47	55.48	47.49	39.50	31.51	24	30	26	28	30	32	33		4
40 44	22.45	14.46	6.46	58.47	51.48	43.49	35.50	27.51	19	40	35	37	38	40	42		5
50 44	18.45	10.46	2.46	54.47	46.48	38.49	30.50	22.51	15	50	44	45	47	49	50		

CORRECTION OF THE MOON'S APPARENT ALTITUDE

(Barometer, 30 inches. Fahrenheit's Thermometer, 56°)

App. Alt.	Horizontal Parallax										" of Par.	Corr. for " of Par. add.					Cor. for " of Alt.
	53'	54'	55'	56'	57'	58'	59'	60'	61'	0"		1"	2"	3"	4"		
30 0	44	14.45	6.45	58.46	50.47	42.48	34.49	26.50	18.51	10	6	0	2	3	5	7	sub. 1 0 2 1 3 1 4 1
10	44	10.45	2.45	54.46	46.47	38.48	30.49	21.50	13.51	10	9	10	12	14	16	17	
20	44	6.44	58.45	50.46	42.47	33.48	25.49	17.50	9.51	20	17	19	21	23	24	24	
30	44	2.44	54.45	46.46	37.47	29.48	21.49	12.50	4.50	30	26	28	29	31	33	33	
40	43	58.44	50.45	41.46	33.47	25.48	16.49	8.49	59.50	50	40	34	36	38	40	41	
50	43	54.44	45.45	37.46	29.47	20.48	12.49	3.49	55.50	46	50	43	45	47	48	50	
31 0	43	50.44	41.45	33.46	24.47	16.48	7.48	58.49	50.50	41	0	0	2	3	5	7	4 2 5 2 6 3 7 3 8 4
10	43	46.44	37.45	28.46	20.47	11.48	2.48	54.49	45.50	37	10	9	10	12	14	16	
20	43	41.44	33.45	24.46	15.47	7.47	58.48	49.49	40.50	32	20	17	19	20	22	24	
30	43	37.44	28.45	20.46	11.47	2.47	53.48	44.49	35.50	27	30	26	27	29	31	32	
40	43	33.44	24.45	15.46	6.46	57.47	48.48	39.49	31.50	22	40	34	36	38	39	41	
50	43	29.44	20.45	11.46	2.46	53.47	44.48	35.49	26.50	17	50	43	44	46	48	49	
32 0	43	24.44	15.45	6.45	57.46	48.47	39.48	30.49	21.50	12	0	0	2	3	5	7	1 5 2 15 3 22 4 32 5 41
10	43	20.44	11.45	2.45	53.46	43.47	34.48	25.49	16.50	7	10	8	10	12	13	15	
20	43	16.44	6.44	57.45	48.46	39.47	29.48	20.49	11.50	1	20	17	19	20	22	24	
30	43	11.44	2.44	53.45	43.46	34.47	24.48	15.49	6.49	56	30	25	27	29	30	32	
40	43	7.43	57.44	48.45	39.46	29.47	20.48	10.49	1.49	51	40	34	35	37	39	41	
50	43	3.43	53.44	43.45	34.46	24.47	15.48	5.48	56.49	46	50	42	44	46	47	49	
33 0	42	58.43	48.44	39.45	29.46	19.47	10.48	0.48	50.49	41	0	0	2	3	5	7	2 15 3 23 4 33 5 42 6 52
10	42	54.43	44.44	34.45	24.46	15.47	5.47	55.48	45.49	36	10	8	10	12	13	15	
20	42	49.43	39.44	29.45	20.46	10.47	0.47	50.48	40.49	30	20	17	18	20	22	23	
30	42	45.43	35.44	24.45	15.46	5.46	55.47	45.48	35.49	25	30	25	27	28	30	32	
40	42	40.43	30.44	19.45	10.46	0.46	50.47	40.48	30.49	20	40	33	35	37	38	40	
50	42	35.43	25.44	14.45	5.45	55.46	45.47	35.48	24.49	14	50	42	44	45	47	48	
34 0	42	31.43	21.44	10.45	0.45	50.46	40.47	29.48	19.49	9	0	0	2	3	5	7	3 23 4 32 5 42 6 52 7 62
10	42	26.43	16.44	6.44	55.45	45.46	34.47	24.48	14.49	3	10	8	10	12	13	15	
20	42	21.43	11.44	1.44	50.45	40.46	29.47	19.48	8.48	58	20	16	18	20	21	23	
30	42	17.43	6.43	56.44	45.45	35.46	24.47	14.48	3.48	53	30	25	27	28	30	31	
40	42	12.43	1.43	51.44	40.45	30.46	19.47	8.47	58.48	47	40	33	35	36	38	40	
50	42	7.42	57.43	46.44	35.45	24.46	14.47	3.47	52.48	41	50	41	43	44	46	48	
35 0	42	3.42	52.43	41.44	30.45	19.46	8.46	57.47	47.48	36	0	0	2	3	5	7	4 32 5 42 6 52 7 62 8 72
10	41	58.42	47.43	36.44	25.45	14.46	3.46	52.47	41.48	30	10	8	10	11	13	15	
20	41	53.42	42.43	31.44	20.45	9.45	58.46	47.46	36.48	25	20	16	18	20	21	23	
30	41	48.42	37.43	26.44	15.45	3.45	52.46	41.47	30.48	19	30	24	26	28	29	31	
40	41	43.42	32.43	21.44	9.44	58.45	47.46	36.47	24.48	13	40	33	34	36	38	39	
50	41	38.42	27.43	16.44	4.44	53.45	41.46	30.47	19.48	7	50	41	42	44	46	47	
36 0	41	33.42	22.43	10.43	59.44	48.45	36.46	25.47	13.48	2	0	0	2	3	5	6	5 42 6 52 7 62 8 72 9 82
10	41	28.42	17.43	5.43	54.44	43.45	31.46	19.47	7.47	56	10	8	10	11	13	14	
20	41	23.42	12.43	0.43	48.44	37.45	25.46	13.47	2.47	50	20	16	18	19	21	23	
30	41	18.42	7.42	55.43	43.44	31.45	20.46	8.46	56.47	44	30	24	26	27	29	31	
40	41	13.42	1.42	50.43	38.44	26.45	14.46	2.46	50.47	38	40	32	34	35	37	39	
50	41	8.41	56.42	44.43	32.44	20.45	8.45	56.46	44.47	33	50	40	42	44	45	47	
37 0	41	3.41	51.42	39.43	27.44	15.45	3.45	51.46	39.47	27	0	0	2	3	5	6	6 52 7 62 8 72 9 82 10 92
10	40	58.41	46.42	34.43	22.44	9.44	57.45	45.46	33.47	21	10	8	10	11	13	14	
20	40	53.41	41.42	28.43	16.44	4.44	52.45	39.46	27.47	15	20	16	17	19	21	22	
30	40	48.41	35.42	23.43	11.43	58.44	46.45	33.46	21.47	9	30	24	26	28	29	31	
40	40	43.41	30.42	18.43	5.43	53.44	40.45	28.46	15.47	3	40	32	34	35	37	38	
50	40	37.41	25.42	12.43	0.43	47.44	34.45	22.46	9.46	57	50	40	41	43	44	46	
38 0	40	32.41	19.42	7.42	54.43	41.44	29.45	16.46	3.46	51	0	0	2	3	5	6	7 62 8 72 9 82 10 92 11 102
10	40	27.41	14.42	1.42	48.43	36.44	23.45	10.45	57.46	44	10	8	9	11	12	14	
20	40	22.41	9.41	56.42	43.43	30.44	17.45	4.45	51.46	38	20	16	17	19	20	22	
30	40	16.41	3.41	50.42	37.43	24.44	11.44	58.45	45.46	32	30	23	25	27	28	30	
40	40	11.40	58.41	45.42	32.43	18.44	5.44	52.45	39.46	26	40	31	33	35	36	38	
50	40	6.40	52.41	39.42	26.43	13.43	59.44	46.45	33.46	20	50	39	41	42	44	45	
39 0	40	0.40	47.41	33.42	20.43	7.43	53.44	40.45	27.46	13	0	0	2	3	5	6	8 72 9 82 10 92 11 102 12 112
10	39	55.40	41.41	28.42	14.43	1.43	47.44	34.45	21.46	7	10	8	9	11	12	14	
20	39	49.40	36.41	22.42	9.42	55.43	41.44	28.45	14.46	1	20	15	17	19	20	22	
30	39	44.40	30.41	17.42	3.42	49.43	35.44	22.45	8.45	54	30	23	25	27	28	30	
40	39	38.40	25.41	11.41	57.42	43.43	29.44	16.45	2.45	48	40	31	32	34	36	37	
50	39	33.40	19.41	5.41	51.42	37.43	23.44	9.44	56.45	42	50	39	40	42	43	45	

CORRECTION OF THE MOON'S APPARENT ALTITUDE

(Barometer, 30 inches. Fahrenheit's Thermometer, 56°)

App. Alt.	Horizontal Parallax										° of Par.	Corr. for ° of Par. add.					Cor. for of Alt.	
	53'	54'	55'	56'	57'	58'	59'	60'	61'	0"		1"	2"	3"	4"			
60° 0'	39	27	40	13	40	59	41	45	42	31	43	17	44	3	44	49	45	35
10	39	22	40	8	40	54	41	39	42	25	43	11	43	57	44	43	45	29
20	39	16	40	2	40	48	41	33	42	19	43	5	43	51	44	36	45	22
30	39	11	39	56	40	42	41	28	42	13	42	59	43	44	44	30	45	16
40	39	5	39	51	40	36	41	22	42	7	42	53	43	38	44	24	45	9
50	38	59	39	45	40	30	41	16	42	1	42	46	43	32	44	17	45	3
61° 0'	38	54	39	39	40	24	41	10	41	55	42	40	43	25	44	11	44	56
10	38	48	39	33	40	18	41	4	41	49	42	34	43	19	44	4	44	49
20	38	42	39	27	40	12	40	58	41	43	42	28	43	13	43	58	44	43
30	38	37	39	22	40	6	40	51	41	36	42	21	43	6	43	51	44	36
40	38	31	39	16	40	0	40	45	41	30	42	15	43	0	43	45	44	30
50	38	25	39	10	39	54	40	39	41	24	42	9	42	53	43	38	44	23
62° 0'	38	19	39	4	39	48	40	33	41	18	42	2	42	47	43	31	44	16
10	38	13	38	58	39	42	40	27	41	11	41	56	42	40	43	25	44	9
20	38	8	38	52	39	36	40	21	41	5	41	49	42	34	43	18	44	3
30	38	2	38	46	39	30	40	14	40	59	41	43	42	27	43	11	43	56
40	37	56	38	40	39	24	40	8	40	52	41	36	42	21	43	5	43	49
50	37	50	38	34	39	18	40	2	40	46	41	30	42	14	42	58	43	42
63° 0'	37	44	38	28	39	12	39	56	40	40	41	23	42	7	42	51	43	35
10	37	38	38	22	39	6	39	49	40	33	41	17	42	1	42	44	43	28
20	37	32	38	16	38	59	39	43	40	27	41	10	41	54	42	38	43	21
30	37	26	38	10	38	53	39	37	40	20	41	4	41	47	42	31	43	14
40	37	20	38	3	38	47	39	30	40	14	40	57	41	40	42	24	43	7
50	37	14	37	57	38	41	39	24	40	7	40	50	41	34	42	17	43	0
64° 0'	37	8	37	51	38	34	39	17	40	1	40	44	41	27	42	10	42	53
10	37	2	37	45	38	28	39	11	39	54	40	37	41	20	42	3	42	46
20	36	56	37	39	38	21	39	4	39	47	40	30	41	13	41	56	42	39
30	36	50	37	32	38	15	38	58	39	41	40	24	41	6	41	49	42	32
40	36	43	37	26	38	9	38	51	39	34	40	17	40	59	41	42	42	25
50	36	37	37	20	38	2	38	45	39	27	40	10	40	53	41	35	42	18
65° 0'	36	31	37	13	37	56	38	38	39	21	40	3	40	46	41	28	42	11
10	36	25	37	7	37	49	38	32	39	14	39	56	40	39	41	21	42	3
20	36	19	37	1	37	43	38	25	39	7	39	50	40	32	41	14	41	56
30	36	12	36	54	37	36	38	19	39	1	39	43	40	25	41	7	41	49
40	36	6	36	48	37	30	38	12	38	54	39	36	40	18	41	0	41	42
50	36	0	36	42	37	23	38	5	38	47	39	29	40	11	40	52	41	34
66° 0'	35	53	36	35	37	17	37	59	38	40	39	22	40	4	40	45	41	27
10	35	47	36	29	37	10	37	52	38	33	39	15	39	56	40	38	41	20
20	35	41	36	22	37	4	37	45	38	26	39	8	39	49	40	31	41	12
30	35	34	36	16	36	57	37	38	38	20	39	1	39	42	40	24	41	5
40	35	28	36	9	36	50	37	32	38	13	38	54	39	35	40	16	40	57
50	35	22	36	3	36	44	37	25	38	6	38	47	39	28	40	9	40	50
67° 0'	35	15	35	56	36	37	37	18	37	59	38	40	39	21	40	2	40	43
10	35	9	35	49	36	30	37	11	37	52	38	33	39	13	39	54	40	35
20	35	2	35	43	36	23	37	4	37	45	38	25	39	6	39	47	40	28
30	34	56	35	36	36	17	36	57	37	38	38	18	38	59	39	39	40	20
40	34	49	35	29	36	10	36	50	37	31	38	11	38	52	39	32	40	12
50	34	43	35	23	36	3	36	43	37	24	38	4	38	44	39	25	40	5
68° 0'	34	36	35	16	35	56	36	36	37	17	37	57	38	37	39	17	39	57
10	34	29	35	9	35	49	36	30	37	10	37	50	38	30	39	10	39	50
20	34	23	35	3	35	43	36	23	37	2	37	42	38	22	39	2	39	42
30	34	16	34	56	35	36	36	16	36	55	37	35	38	15	38	55	39	34
40	34	10	34	49	35	29	36	8	36	48	37	28	38	7	38	47	39	27
50	34	3	34	42	35	22	36	1	36	41	37	20	38	0	38	39	39	19
69° 0'	33	56	34	36	35	15	35	54	36	34	37	13	37	52	38	32	39	11
10	33	50	34	29	35	8	35	47	36	27	37	6	37	45	38	24	39	3
20	33	43	34	22	35	1	35	40	36	19	36	58	37	37	38	17	38	56
30	33	36	34	15	34	54	35	33	36	12	36	51	37	30	38	9	38	48
40	33	29	34	8	34	47	35	26	36	5	36	44	37	22	38	1	38	40
50	33	23	34	1	34	40	35	19	35	57	36	36	37	15	37	54	38	32

CORRECTION OF THE MOON'S APPARENT ALTITUDE

(Barometer, 30 inches. Fahrenheit's Thermometer, 50°)

App. Alt.	Horizontal Parallax										" of Par.	Corr. for " of Par add.					Cor. for " of Alt.									
	53'	54'	55'	56'	57'	58'	59'	60'	61'	0"		1"	2"	3"	4"											
50° 0	33	16	33	54	34	33	35	11	35	50	36	29	37	7	37	46	38	24	0	0	1	3	4	5		
10	33	9	33	47	34	26	35	4	35	43	36	21	37	0	37	38	38	16	10	6	7	9	10	11		
20	33	2	33	40	34	19	34	57	35	35	36	14	36	52	37	30	38	9	20	13	14	15	17	18		
30	32	55	33	33	34	12	34	50	35	28	36	6	36	44	37	22	38	1	30	19	20	21	23	24		sub.
40	32	48	33	26	34	4	34	42	35	21	35	59	36	37	37	15	37	53	40	25	27	28	29	31		
50	32	42	33	19	33	57	34	35	35	13	35	51	36	29	37	7	37	45	50	32	33	34	36	37		
51 0	32	35	33	12	33	50	34	28	35	6	35	43	36	21	36	59	37	37	0	0	1	2	4	5		
10	32	28	33	5	33	43	34	21	34	58	35	36	36	13	36	51	37	29	10	6	7	9	10	11		
20	32	21	32	58	33	36	34	13	34	51	35	28	36	6	36	43	37	21	20	12	14	15	16	17		
30	32	14	32	51	33	29	34	6	34	43	35	21	35	58	36	55	37	13	30	19	20	21	22	24		
40	32	7	32	44	33	21	33	59	34	36	35	13	35	50	36	27	37	5	40	25	26	28	29	30		
50	32	0	32	37	33	14	33	51	34	28	35	5	35	42	36	19	36	57	50	31	32	34	35	36		
52 0	31	53	32	30	33	7	33	44	34	21	34	58	35	35	36	11	36	48	0	0	1	2	4	5		
10	31	46	32	23	32	59	33	36	34	13	34	50	35	27	36	3	36	40	10	6	7	9	10	11		
20	31	39	32	15	32	52	33	29	34	5	34	42	35	19	35	55	36	32	20	12	13	15	16	17		
30	31	32	8	32	45	33	21	33	58	34	34	35	11	35	47	36	24	30	18	19	21	22	23			
40	31	25	32	13	32	37	33	14	33	50	34	27	35	3	35	39	36	16	40	24	26	27	28	29		
50	31	17	31	54	32	30	33	6	33	43	34	19	34	55	35	31	36	8	50	30	32	33	34	35		
53 0	31	10	31	47	32	23	32	59	33	35	34	11	34	47	35	23	35	59	0	0	1	2	4	5		
10	31	3	31	39	32	15	32	51	33	27	34	3	34	39	35	15	35	51	10	6	7	8	10	11		
20	30	56	31	32	3	32	44	33	19	33	55	34	31	35	7	35	43	20	12	13	14	15	17			
30	30	49	31	25	32	0	32	36	33	12	33	47	34	23	34	59	35	35	30	18	19	20	21	23		
40	30	42	31	17	31	53	32	28	33	4	33	40	34	15	34	51	35	26	40	24	25	26	27	29		
50	30	35	31	10	31	45	32	21	32	56	33	32	34	7	34	42	35	18	50	30	31	32	33	35		
54 0	30	27	31	3	31	38	32	13	32	48	33	24	33	59	34	34	35	10	0	0	1	2	3	5		
10	30	20	30	55	31	30	32	6	32	41	33	16	33	51	34	26	35	1	10	6	7	8	9	10		
20	30	13	30	48	31	23	31	58	32	33	3	33	43	34	18	34	53	20	12	13	14	15	16			
30	30	6	30	40	31	15	31	50	32	25	33	0	33	35	34	10	34	44	30	17	19	20	21	22		
40	29	58	30	33	31	8	31	42	32	17	32	52	33	27	34	1	34	36	40	23	24	26	27	28		
50	29	51	30	26	31	0	31	35	32	9	32	44	33	18	33	53	34	28	50	29	30	31	32	34		
55 0	29	44	30	18	30	53	31	27	32	1	32	36	33	10	33	45	34	19	0	0	1	2	3	5		
10	29	36	30	11	30	45	31	19	31	54	32	28	33	2	33	36	34	11	10	6	7	8	9	10		
20	29	29	30	3	30	37	31	11	31	46	32	20	32	54	33	28	34	2	20	11	12	14	15	16		
30	29	22	29	56	30	30	31	4	31	38	32	12	32	46	33	20	33	54	30	17	18	19	20	22		
40	29	14	29	48	30	22	30	56	31	30	32	3	32	37	33	11	33	45	40	23	24	25	26	27		
50	29	7	29	41	30	14	30	48	31	22	31	55	32	29	33	3	33	37	50	28	29	31	32	33		
56 0	28	59	29	33	30	7	30	40	31	14	31	47	32	21	32	54	33	28	0	0	1	2	3	4		
10	28	52	29	25	29	59	30	32	31	6	31	39	32	12	32	46	33	19	10	6	7	8	9	10		
20	28	45	29	18	29	51	30	24	30	58	31	31	32	4	32	37	33	11	20	11	12	13	14	15		
30	28	37	29	10	29	43	30	16	30	50	31	23	31	56	32	29	33	2	30	17	18	19	20	21		
40	28	30	29	3	29	36	30	9	30	42	31	15	31	48	32	20	32	53	40	22	23	24	25	26		
50	28	22	28	55	29	28	30	1	30	33	31	6	31	39	32	12	32	45	50	28	29	30	31	32		
57 0	28	15	28	47	29	20	29	53	30	25	30	58	31	31	32	3	32	36	0	0	1	2	3	4		
10	28	7	28	40	29	12	29	45	30	17	30	50	31	22	31	55	32	27	10	5	7	8	9	10		
20	28	0	28	32	29	4	29	37	30	9	30	42	31	14	31	46	32	19	20	11	12	13	14	15		
30	27	52	28	24	28	56	29	29	30	1	30	33	31	5	31	38	32	10	30	16	17	18	19	20		
40	27	44	28	17	28	49	29	21	29	53	30	25	30	57	31	29	32	1	40	21	22	23	24	26		
50	27	37	28	9	28	41	29	13	29	45	30	17	30	49	31	20	31	52	50	27	28	29	30	31		
58 0	27	29	28	1	28	33	29	5	29	36	30	8	30	40	31	12	31	44	0	0	1	2	3	4		
10	27	22	27	53	28	25	28	57	29	28	30	0	30	32	31	3	31	35	10	5	6	7	8	9		
20	27	14	27	45	28	17	28	48	29	20	29	51	30	23	30	55	31	26	20	10	11	13	14	15		
30	27	6	27	38	28	9	28	40	29	12	29	43	30	14	30	46	31	17	30	16	17	18	19	20		
40	26	59	27	30	28	12	28	32	29	3	29	35	30	6	30	37	31	8	40	21	22	23	24	25		
50	26	51	27	22	27	53	28	24	28	55	29	26	29	57	30	28	30	59	50	26	27	28	29	30		
59 0	26	43	27	14	27	45	28	16	28	47	29	18	29	49	30	20	30	51	0	0	1	2	3	4		
10	26	36	27	6	27	37	28	8	28	39	29	9	29	40	30	11	30	42	10	5	6	7	8	9		
20	26	28	26	58	27	29	28	0	28	30	29	1	29	32	30	2	30	33	20	10	11	12	13	14		
30	26	20	26	51	27	21	27	52	28	22	28	52	29	23	29	53	30	24	30	15	16	17	18	19		
40	26	12	26	43	27	13	27	43	28	14	28	44	29	14	29	45	30	15	40	20	21	22	23	24		
50	26	5	26	35	27	5	27	35	28	5	28	35	29	6	29	36	30	6	50	25	26	27	28	29		

CORRECTION OF THE MOON'S APPARENT ALTITUDE

(Barometer, 30 inches Fahrenheit's Thermometer, 50°)

App. Alt.	Horizontal Parallax										" of Par.	Corr. for " of Par add.					Cor. for " of Alt.
	23'	24'	25'	26'	27'	28'	29'	30'	31'	0"		1"	2"	3"	4"		
00	0	25	57	26	27	26	57	27	27	27	28	57	29	27	29	57	0
10	25	49	26	19	26	49	27	29	27	48	28	48	29	18	29	48	10
20	25	41	26	11	26	41	27	10	27	40	28	39	29	9	29	39	20
30	25	33	26	3	26	32	27	2	27	32	28	31	29	0	29	30	30
40	25	26	25	55	26	24	26	54	27	23	27	53	22	28	51	29	40
50	25	18	25	47	26	16	26	45	27	15	27	44	23	13	28	42	50
60	25	10	25	39	26	8	26	37	27	6	27	35	28	4	28	34	60
70	25	2	25	31	26	0	26	29	27	27	27	27	27	27	27	27	70
80	24	54	25	23	25	52	26	20	26	49	27	18	27	47	28	16	80
90	24	46	25	15	25	43	26	12	26	41	27	9	27	38	28	7	90
100	24	38	25	7	25	35	26	4	26	32	27	1	27	29	27	5	100
110	24	30	24	59	25	27	25	55	26	24	26	52	27	20	27	49	110
120	24	22	24	51	25	19	25	47	26	15	26	43	27	11	27	40	120
130	24	14	24	42	25	10	25	38	26	6	26	35	27	3	27	31	130
140	24	6	24	34	25	2	25	30	26	26	26	54	27	22	27	49	140
150	23	58	24	26	24	54	25	22	25	49	26	17	26	45	27	12	150
160	23	50	24	18	24	46	25	13	25	41	26	8	26	36	27	3	160
170	23	42	24	10	24	37	25	5	25	32	25	59	26	27	26	27	170
180	23	34	24	2	24	29	24	56	25	23	25	51	26	18	26	45	180
190	23	26	23	53	24	21	24	48	25	15	25	42	26	9	26	36	190
200	23	18	23	45	24	12	24	39	25	6	25	33	26	0	26	27	200
210	23	10	23	37	24	4	24	31	24	57	25	24	25	51	26	18	210
220	23	2	23	29	23	55	24	22	24	49	25	15	25	42	26	9	220
230	22	54	23	11	23	47	24	14	24	40	25	6	25	33	25	59	230
240	22	46	23	3	23	39	24	5	24	31	24	58	25	24	25	50	240
250	22	38	23	4	23	30	23	56	24	22	24	49	25	15	25	41	250
260	22	30	22	56	23	22	23	48	24	14	24	40	25	6	25	32	260
270	22	22	22	47	23	13	23	39	24	5	24	31	24	57	25	23	270
280	22	13	22	39	23	5	23	31	24	22	24	48	25	13	25	39	280
290	22	5	22	31	23	56	23	22	23	47	24	13	24	38	25	4	290
300	21	57	22	22	22	48	23	13	23	39	24	4	24	29	24	55	300
310	21	49	22	14	22	39	23	5	23	30	23	55	24	20	24	45	310
320	21	41	22	6	22	31	22	56	23	21	23	46	24	11	24	36	320
330	21	33	21	57	22	22	23	47	23	12	23	37	24	2	24	27	330
340	21	24	21	49	22	14	23	39	23	3	23	28	23	53	24	17	340
350	21	16	21	41	22	5	22	30	22	54	23	19	23	44	24	8	350
360	21	8	21	32	21	57	22	21	22	46	23	10	23	34	23	59	360
370	21	0	21	24	21	49	22	12	22	37	23	1	23	25	23	49	370
380	20	51	21	15	21	40	22	4	22	28	22	52	23	16	23	40	380
390	20	43	21	7	21	31	21	55	22	19	22	43	23	7	23	31	390
400	20	35	20	59	21	22	21	46	22	10	22	34	22	57	23	21	400
410	20	27	20	50	21	14	21	37	22	1	22	25	22	48	23	12	410
420	20	18	20	42	21	5	21	29	21	52	22	15	22	39	23	3	420
430	20	10	20	33	20	56	21	20	21	43	22	6	22	30	22	53	430
440	20	2	20	25	20	48	21	11	21	34	21	57	22	20	22	43	440
450	19	53	20	16	20	39	21	2	21	25	21	48	22	11	22	34	450
460	19	45	20	8	20	30	20	53	21	16	21	39	22	2	22	44	460
470	19	36	19	59	20	22	20	44	21	7	21	30	21	52	22	15	470
480	19	28	19	51	20	13	20	36	20	58	21	21	21	43	22	5	480
490	19	20	19	42	20	4	20	27	20	49	21	11	21	34	21	56	490
500	19	11	19	33	19	56	20	18	20	40	21	2	21	24	21	46	500
510	19	3	19	25	19	47	20	9	20	31	20	53	21	15	21	37	510
520	18	54	19	16	19	38	20	0	20	22	20	44	21	5	21	27	520
530	18	46	19	8	19	29	19	51	20	13	20	34	20	56	21	18	530
540	18	38	18	59	19	21	19	42	20	4	20	25	20	47	21	8	540
550	18	29	18	50	19	12	19	33	19	54	20	16	20	37	20	29	550
560	18	21	18	42	19	3	19	24	19	45	20	7	20	28	20	20	560
570	18	12	18	33	18	54	19	15	19	36	19	57	20	18	20	39	570
580	18	4	18	25	18	45	19	6	19	27	19	48	20	9	20	30	580
590	17	55	18	16	18	37	18	57	19	18	19	39	19	59	20	20	590

CORRECTION OF THE MOON'S APPARENT ALTITUDE

(Barometer, 30 inches. Fahrenheit's Thermometer, 50°)

App. Alt.	Horizontal Parallax										" of Par.	Corr. for " of Par. add.					Corr. for " of Alt.
	53'	54'	55'	56'	57'	58'	59'	60'	61'	0"		1"	2"	3"	4"		
70° 0'	17 47	18 7	18 28	18 48	19 9	19 29	19 50	20 10	20 31	0	0	1	1	2	3		
10	17 38	17 59	18 19	18 39	19 0	19 20	19 40	20 0	20 21	10	3	4	5	5	6		
20	17 30	17 50	18 10	18 30	18 51	19 11	19 31	19 51	20 11	20	7	7	8	9	9		
30	17 21	17 41	18 1	18 21	18 41	19 1	19 21	19 41	20 1	30	10	11	11	12	13		
40	17 13	17 33	17 52	18 12	18 32	18 52	19 12	19 32	19 52	40	13	14	15	15	16		
50	17 4	17 24	17 44	18 3	18 23	18 43	19 2	19 22	19 42	50	17	17	18	19	19		
71° 0'	16 56	17 15	17 35	17 54	18 14	18 33	18 53	19 12	19 32	0	0	1	1	2	3		
10	16 47	17 6	17 26	17 45	18 4	18 24	18 43	19 3	19 22	10	3	4	4	5	6		
20	16 38	16 58	17 17	17 36	17 55	18 15	18 34	18 53	19 12	20	6	7	8	8	9		
30	16 30	16 49	17 8	17 27	17 46	18 5	18 24	18 43	19 2	30	10	10	11	11	12		
40	16 21	16 40	16 59	17 18	17 37	17 56	18 15	18 33	18 52	40	13	13	14	15	15		
50	16 13	16 31	16 50	17 9	17 28	17 46	18 5	18 24	18 42	50	16	16	17	18	18		
72° 0'	16 4	16 23	16 41	17 0	17 18	17 37	17 55	18 14	18 32	0	0	1	1	2	2		
10	15 55	16 14	16 32	16 51	17 9	17 27	17 46	18 4	18 22	10	3	4	4	5	5		
20	15 47	16 5	16 23	16 41	17 0	17 18	17 36	17 54	18 13	20	6	7	7	8	8		
30	15 38	15 56	16 14	16 32	16 50	17 8	17 26	17 44	18 3	30	9	10	10	11	11		
40	15 29	15 47	16 5	16 23	16 41	16 59	17 17	17 35	17 53	40	12	13	13	14	14		
50	15 21	15 39	15 56	16 14	16 32	16 49	17 7	17 25	17 43	50	15	16	16	17	17		
73° 0'	15 12	15 30	15 47	16 5	16 22	16 40	16 57	17 15	17 33	0	0	1	1	2	2		
10	15 3	15 21	15 38	15 56	16 13	16 30	16 48	17 5	17 23	10	3	3	4	5	5		
20	14 55	15 12	15 29	15 46	16 4	16 21	16 38	16 55	17 13	20	6	6	7	7	8		
30	14 46	15 3	15 20	15 37	15 54	16 11	16 28	16 45	17 3	30	9	9	10	10	11		
40	14 37	14 54	15 11	15 28	15 45	16 2	16 19	16 36	16 52	40	11	12	12	13	14		
50	14 29	14 45	15 2	15 19	15 36	15 52	16 9	16 26	16 42	50	14	15	15	16	16		
74° 0'	14 20	14 37	14 53	15 10	15 26	15 43	15 59	16 16	16 32	0	0	1	1	2	2	sub. 1 2 3 4 5 6 7 8 9	
10	14 11	14 28	14 44	15 0	15 17	15 33	15 50	16 6	16 22	10	3	3	4	4	5		
20	14 3	14 19	14 35	14 51	15 7	15 24	15 40	15 56	16 12	20	5	6	6	7	7		
30	13 54	14 10	14 26	14 42	14 58	15 14	15 30	15 46	16 2	30	8	9	9	10	10		
40	13 45	14 1	14 17	14 33	14 49	15 4	15 20	15 36	15 52	40	11	11	12	12	13		
50	13 36	13 52	14 8	14 24	14 39	14 55	15 11	15 26	15 42	50	13	14	14	15	15		
75° 0'	13 28	13 43	13 59	14 14	14 30	14 45	15 1	15 16	15 32	0	0	1	1	2	2		
10	13 19	13 34	13 50	14 5	14 20	14 36	14 51	15 6	15 22	10	3	3	4	4	5		
20	13 10	13 25	13 41	13 56	14 11	14 26	14 41	14 56	15 12	20	5	6	6	7	7		
30	13 1	13 16	13 31	13 46	14 1	14 16	14 32	14 47	15 2	30	8	8	9	9	10		
40	12 53	13 7	13 22	13 37	13 52	14 7	14 22	14 37	14 51	40	10	11	11	12	12		
50	12 44	12 58	13 13	13 28	13 43	13 57	14 12	14 27	14 41	50	13	13	14	14	15		
76° 0'	12 35	12 50	13 4	13 19	13 33	13 48	14 2	14 17	14 31	0	0	0	1	1	2		
10	12 26	12 41	12 55	13 9	13 24	13 38	13 52	14 7	14 21	10	2	3	3	4	4		
20	12 17	12 32	12 46	13 0	13 14	13 28	13 42	13 57	14 11	20	5	5	6	6	7		
30	12 9	12 23	12 37	12 51	13 5	13 19	13 33	13 47	14 1	30	7	7	8	8	9		
40	12 0	12 14	12 27	12 41	12 55	13 9	13 23	13 37	13 50	40	9	10	10	11	11		
50	11 51	12 5	12 18	12 32	12 46	12 59	13 13	13 27	13 40	50	12	12	13	13	14		
77° 0'	11 42	11 56	12 9	12 23	12 36	12 50	13 3	13 17	13 30	0	0	0	1	1	2		
10	11 33	11 47	12 0	12 13	12 27	12 40	12 53	13 6	13 20	10	2	3	3	4	4		
20	11 24	11 37	11 51	12 4	12 17	12 30	12 43	12 56	13 10	20	4	5	5	6	6		
30	11 15	11 28	11 41	11 54	12 7	12 20	12 33	12 46	12 59	30	7	7	7	8	8		
40	11 7	11 19	11 32	11 45	11 58	12 11	12 24	12 36	12 49	40	9	9	10	10	10		
50	10 58	11 10	11 23	11 36	11 48	12 1	12 14	12 26	12 39	50	11	11	12	12	13		
78° 0'	10 49	11 1	11 14	11 26	11 39	11 51	12 4	12 16	12 29	0	0	0	1	1	2		
10	10 40	10 52	11 5	11 17	11 29	11 42	11 54	12 6	12 19	10	2	2	3	3	4		
20	10 31	10 43	10 55	11 8	11 20	11 32	11 44	11 56	12 8	20	4	4	5	5	6		
30	10 22	10 34	10 46	10 58	11 10	11 22	11 34	11 46	11 58	30	6	6	7	7	8		
40	10 13	10 25	10 37	10 49	11 1	11 12	11 24	11 36	11 48	40	8	8	9	9	10		
50	10 5	10 16	10 28	10 39	10 51	11 3	11 14	11 26	11 38	50	10	10	11	11	12		
79° 0'	9 56	10 7	10 19	10 30	10 41	10 53	11 4	11 16	11 27	0	0	0	1	1	1		
10	9 47	9 58	10 9	10 21	10 32	10 43	10 54	11 6	11 17	10	2	2	3	3	3		
20	9 38	9 49	10 0	10 11	10 22	10 33	10 44	10 56	11 7	20	4	4	4	5	5		
30	9 29	9 40	9 51	10 2	10 13	10 24	10 34	10 45	10 56	30	5	6	6	7	7		
40	9 20	9 31	9 41	9 52	10 3	10 14	10 25	10 35	10 46	40	7	8	8	8	9		
50	9 11	9 22	9 32	9 43	9 53	10 4	10 15	10 25	10 36	50	9	9	10	10	11		

CORRECTION OF THE MOON'S APPARENT ALTITUDE

(Barometer, 30 inches. Fahrenheit's Thermometer, 50°)

App. Alt.	Horizontal Parallax										" of Par.	Corr. for " of Par. add.					Cor. for " of Alt.
	53'	54'	55'	56'	57'	58'	59'	60'	61'	0"		1"	2"	3"	4"		
80 0	9 2	9 12	9 23	9 33	9 44	9 54	10 5	10 15	10 25	0	0	0	1	1	1		
10	8 53	9 3	9 14	9 24	9 34	9 44	9 55	10 5	10 15	10	2	2	2	3	3		
20	8 44	8 54	9 4	9 14	9 24	9 35	9 45	9 55	10 5	20	3	4	4	4	5		
30	8 35	8 45	8 55	9 5	9 15	9 25	9 35	9 45	9 54	30	5	5	6	6	6		
40	8 26	8 36	8 46	8 56	9 5	9 15	9 25	9 34	9 44	40	7	7	7	8	8		
50	8 17	8 27	8 36	8 46	8 56	9 5	9 15	9 24	9 34	50	8	9	9	9	10		
81 0	8 8	8 18	8 27	8 37	8 46	8 55	9 5	9 14	9 24	0	0	0	1	1	1		
10	7 59	8 9	8 18	8 27	8 36	8 45	8 55	9 4	9 13	10	1	2	2	2	3		
20	7 50	7 59	8 8	8 17	8 26	8 35	8 44	8 53	9 2	20	3	3	4	4	4		
30	7 41	7 50	7 59	8 8	8 17	8 26	8 35	8 44	8 52	30	4	4	5	5	5		
40	7 32	7 41	7 50	7 59	8 7	8 16	8 25	8 33	8 42	40	6	6	7	7	7		
50	7 24	7 32	7 41	7 49	7 58	8 6	8 15	8 23	8 32	50	7	8	8	8	9		
82 0	7 14	7 23	7 31	7 40	7 48	7 56	8 5	8 13	8 21	0	0	0	1	1	1		
10	7 5	7 14	7 22	7 30	7 38	7 46	7 55	8 3	8 11	10	1	2	2	2	2		
20	6 57	7 5	7 13	7 21	7 29	7 37	7 45	7 53	8 1	20	3	3	3	3	4		
30	6 48	6 55	7 3	7 11	7 19	7 27	7 34	7 42	7 50	30	4	4	4	4	5		
40	6 38	6 46	6 54	7 1	7 9	7 17	7 24	7 32	7 40	40	5	5	5	6	6		
50	6 29	6 37	6 44	6 52	6 59	7 7	7 14	7 22	7 29	50	6	7	7	7	8		
83 0	6 20	6 28	6 35	6 42	6 50	6 57	7 4	7 12	7 19	0	0	0	0	1	1		
10	6 11	6 19	6 26	6 33	6 40	6 47	6 54	7 1	7 9	10	1	1	2	2	2		
20	6 2	6 9	6 16	6 23	6 30	6 37	6 44	6 51	6 58	20	2	2	3	3	3		
30	5 53	6 0	6 7	6 14	6 21	6 27	6 34	6 41	6 48	30	3	4	4	4	4		
40	5 44	5 51	5 58	6 4	6 11	6 18	6 24	6 31	6 37	40	5	5	5	5	5		
50	5 35	5 42	5 48	5 55	6 1	6 8	6 14	6 21	6 27	50	6	6	6	6	7		
84 0	5 26	5 33	5 39	5 45	5 51	5 58	6 4	6 10	6 17	0	0	0	0	0	1		
10	5 17	5 23	5 30	5 36	5 42	5 48	5 54	6 0	6 6	10	1	1	1	1	2		
20	5 8	5 14	5 20	5 26	5 32	5 38	5 44	5 50	5 56	20	2	2	2	2	3		
30	4 59	5 5	5 11	5 17	5 23	5 28	5 34	5 40	5 45	30	3	3	3	3	4		
40	4 50	4 56	5 1	5 7	5 13	5 18	5 24	5 29	5 35	40	4	4	4	4	5		
50	4 41	4 47	4 52	4 57	5 3	5 8	5 14	5 19	5 24	50	5	5	5	5	6		
85 0	4 32	4 37	4 43	4 48	4 53	4 58	5 4	5 9	5 14	0	0	0	0	0	1		
10	4 23	4 28	4 33	4 38	4 43	4 48	4 53	4 58	5 4	10	1	1	1	1	1		
20	4 14	4 19	4 24	4 29	4 34	4 38	4 43	4 48	4 53	20	2	2	2	2	2		
30	4 5	4 10	4 14	4 19	4 24	4 28	4 33	4 38	4 43	30	2	2	3	3	3		
40	3 56	4 0	4 5	4 10	4 14	4 19	4 23	4 28	4 32	40	3	3	3	4	4		
50	3 47	3 51	3 56	4 0	4 4	4 9	4 13	4 17	4 22	50	4	4	4	4	5		
86 0	3 38	3 42	3 46	3 50	3 55	3 59	4 3	4 7	4 11	0	0	0	0	0	0		
10	3 29	3 33	3 37	3 41	3 45	3 49	3 53	3 57	4 1	10	1	1	1	1	1		
20	3 20	3 23	3 27	3 31	3 35	3 39	3 43	3 47	3 50	20	1	1	1	1	2		
30	3 11	3 14	3 18	3 22	3 25	3 29	3 33	3 36	3 40	30	2	2	2	2	2		
40	3 2	3 5	3 9	3 12	3 15	3 19	3 22	3 26	3 29	40	2	3	3	3	3		
50	2 53	2 56	2 59	3 2	3 6	3 9	3 12	3 16	3 19	50	3	3	3	3	4		
87 0	2 43	2 47	2 50	2 53	2 56	2 59	3 2	3 5	3 8	0	0	0	0	0	0		
10	2 34	2 37	2 40	2 43	2 46	2 49	2 52	2 55	2 58	10	0	1	1	1	1		
20	2 25	2 28	2 31	2 34	2 36	2 39	2 42	2 45	2 48	20	1	1	1	1	1		
30	2 16	2 19	2 21	2 24	2 27	2 29	2 32	2 35	2 37	30	1	1	1	1	2		
40	2 7	2 10	2 12	2 14	2 17	2 19	2 22	2 24	2 27	40	2	2	2	2	2		
50	1 58	2 0	2 3	2 5	2 7	2 9	2 12	2 14	2 16	50	2	2	2	2	3		
88 0	1 49	1 51	1 53	1 55	1 57	1 59	2 2	2 4	2 6	0	0	0	0	0	0		
10	1 40	1 42	1 44	1 46	1 48	1 50	1 51	1 53	1 55	10	0	0	0	0	0		
20	1 31	1 33	1 34	1 36	1 38	1 40	1 41	1 43	1 45	20	1	1	1	1	1		
30	1 22	1 23	1 25	1 26	1 28	1 30	1 31	1 33	1 34	30	1	1	1	1	1		
40	1 13	1 14	1 15	1 17	1 18	1 20	1 21	1 22	1 24	40	1	1	1	1	1		
50	1 4	1 5	1 6	1 7	1 9	1 10	1 11	1 12	1 13	50	1	1	1	1	1		
89 0	0 54	0 56	0 57	0 58	0 59	1 0	1 1	1 2	1 3	0	0	0	0	0	0		
10	0 45	0 46	0 47	0 48	0 49	0 50	0 51	0 52	0 52	10	0	0	0	0	0		
20	0 36	0 37	0 38	0 38	0 39	0 40	0 41	0 41	0 42	20	0	0	0	0	0		
30	0 27	0 28	0 28	0 29	0 29	0 30	0 30	0 31	0 31	30	0	0	0	0	0		
40	0 18	0 19	0 19	0 19	0 20	0 20	0 20	0 21	0 21	40	0	0	0	0	0		
50	0 9	0 9	0 9	0 10	0 10	0 10	0 10	0 10	0 10	50	1	1	1	1	1		

TABLE 40.

CORRESPONDING HOR. PARALLAX AND SEMIDIAM. OF THE MOON.					
H. Par.	Semid.	H. Par.	Semid.	H. Par.	Semid.
53' 29"	14' 36"	57' 10"	15' 36"	60' 50"	16' 36"
53 33	14 37	57 13	15 37	60 53	16 37
53 37	14 38	57 17	15 38	60 57	16 38
53 40	14 39	57 21	15 39	61 1	16 39
53 44	14 40	57 24	15 40	61 4	16 40
53 48	14 41	57 28	15 41	61 8	16 41
53 51	14 42	57 32	15 42	61 12	16 42
53 55	14 43	57 35	15 43	61 15	16 43
53 59	14 44	57 39	15 44	61 19	16 44
54 3	14 45	57 43	15 45	61 23	16 45
54 6	14 46	57 46	15 46	61 26	16 46
54 10	14 47	57 50	15 47	61 30	16 47
54 14	14 48	57 54	15 48	61 34	16 48
54 17	14 49	57 57	15 49	61 37	16 49
54 21	14 50	58 1	15 50	61 41	16 50
54 25	14 51	58 5	15 51		
54 28	14 52	58 8	15 52		
54 32	14 53	58 12	15 53		
54 36	14 54	58 16	15 54		
54 39	14 55	58 19	15 55		
54 43	14 56	58 23	15 56		
54 47	14 57	58 27	15 57		
54 50	14 58	58 30	15 58		
54 54	14 59	58 34	15 59		
54 58	15 0	58 38	16 0		
55 1	15 1	58 41	16 1		
55 5	15 2	58 45	16 2		
55 9	15 3	58 49	16 3		
55 12	15 4	58 52	16 4		
55 16	15 5	58 56	16 5		
55 20	15 6	59 0	16 6		
55 23	15 7	59 3	16 7		
55 27	15 8	59 7	16 8		
55 31	15 9	59 11	16 9		
55 34	15 10	59 14	16 10		
55 38	15 11	59 18	16 11		
55 42	15 12	59 22	16 12		
55 45	15 13	59 25	16 13		
55 49	15 14	59 29	16 14		
55 53	15 15	59 33	16 15		
55 56	15 16	59 36	16 16		
56 0	15 17	59 40	16 17		
56 4	15 18	59 44	16 18		
56 7	15 19	59 47	16 19		
56 11	15 20	59 51	16 20		
56 15	15 21	59 55	16 21		
56 18	15 22	59 58	16 22		
56 22	15 23	60 2	16 23		
56 26	15 24	60 6	16 24		
56 29	15 25	60 9	16 25		
56 33	15 26	60 13	16 26		
56 37	15 27	60 17	16 27		
56 40	15 28	60 20	16 28		
56 44	15 29	60 24	16 29		
56 48	15 30	60 28	16 30		
56 51	15 31	60 31	16 31		
56 55	15 32	60 35	16 32		
56 59	15 33	60 39	16 33		
57 2	15 34	60 42	16 34		
57 6	15 35	60 46	16 35		

TABLE 41

685

CORRECTION OF THE MOON'S EQUATORIAL PARALLAX FOR THE FIGURE OF THE EARTH.					
Compression $\frac{1}{293}$, (Clarke)					
Lat.	Horizontal Parallax				
	54'	56'	58'	60'	62'
0°	"0	"0	"0	"0	"0
8	0.2	0.2	0.2	0.2	0.2
16	0.8	0.9	0.9	0.9	0.9
20	1.3	1.4	1.4	1.4	1.5
24	1.8	1.9	2.0	2.0	2.1
28	2.4	2.5	2.6	2.7	2.8
32	3.1	3.2	3.4	3.5	3.6
36	3.8	4.0	4.1	4.2	4.4
40	4.6	4.7	4.9	5.1	5.2
44	5.3	5.5	5.7	5.9	6.1
48	6.1	6.3	6.6	6.8	7.0
52	6.9	7.1	7.4	7.6	7.9
56	7.6	7.9	8.2	8.4	8.7
60	8.3	8.6	8.9	9.2	9.5
64	8.9	9.3	9.6	9.9	10.2
68	9.5	9.9	10.2	10.6	10.9
72	10.0	10.4	10.7	11.1	11.5
76	10.4	10.8	11.2	11.6	12.0
80	10.7	11.1	11.5	11.9	12.3

TABLE 42

AUGMENTATION OF THE MOON'S SEMIDIAMETER						
App. Alt.	Semidiameter					
	14'	15'		16'		17'
	30"	0"	30"	0"	30"	0"
0°	0.1	0.1	0.1	0.1	0.1	0.1
2	0.6	0.6	0.7	0.7	0.8	0.8
4	1.0	1.1	1.2	1.3	1.4	1.5
6	1.5	1.6	1.7	1.9	2.0	2.1
8	2.0	2.1	2.2	2.4	2.5	2.7
10	2.4	2.7	2.8	3.0	3.2	3.3
12	2.9	3.2	3.3	3.5	3.7	4.0
14	3.4	3.6	3.8	4.1	4.4	4.6
16	3.9	4.1	4.4	4.7	5.0	5.2
18	4.3	4.6	4.9	5.2	5.5	5.9
21	4.9	5.3	5.7	6.0	6.4	6.7
24	5.6	6.0	6.4	6.8	7.2	7.7
27	6.2	6.7	7.2	7.6	8.1	8.6
30	6.9	7.4	7.9	8.4	8.9	9.4
33	7.5	8.0	8.6	9.1	9.6	10.3
36	8.0	8.6	9.2	9.8	10.4	11.1
39	8.6	9.2	9.9	10.5	11.1	11.8
42	9.1	9.8	10.4	11.2	11.8	12.6
45	9.7	10.3	11.0	11.8	12.5	13.3
48	10.2	10.9	11.6	12.4	13.1	14.0
51	10.6	11.3	12.1	12.9	13.7	14.6
54	11.1	11.8	12.6	13.5	14.3	15.2
57	11.5	12.3	13.1	14.0	14.8	15.7
59	12.2	13.0	13.9	14.8	15.7	16.7
62	12.7	13.7	14.7	15.7	16.6	17.6
70	13.3	14.3	15.3	16.3	17.3	18.4
90	13.5	14.6	15.6	16.7	17.6	18.6

CABLE 43

CORRECTION			
FOR REDUCING THE TRUE ALTITUDE OF THE SUN OR A STAR TO THE APPARENT ALTITUDE			
Alt.	Corr.	Alt.	Corr.
	sub.		sub.
5° 0'	0' 16"	7° 30'	0' 5"
5 30	0 15	8 0	0 5
5 45	0 12	9 0	0 3
6 0	0 11	10 0	0 2
6 30	0 9	13 0	0 1
6 45	0 8	25 0	0 0
7 0	0 7		

TABLE 44

CORRECTION FOR REDUCING THE TRUE ALTITUDE OF THE MOON TO THE APPARENT ALTITUDE			
Alt.	Horizontal Parallax		
	54'	55'	56'
5° 0'	<i>add.</i> 1' 14"	<i>add.</i> 1' 22"	<i>add.</i> 1' 28"
5 10	1 10	1 18	1 23
5 20	1 7	1 15	1 19
5 30	1 5	1 11	1 16
5 40	1 3	1 8	1 13
5 50	1 0	1 5	1 10
6 0	0 57	1 3	1 7
6 20	0 52	0 57	1 2
6 40	0 47	0 51	0 54
7 0	0 45	0 47	0 51
7 30	0 41	0 44	0 47
7 40	0 37	0 40	0 42
8 0	0 34	0 36	0 38
8 30	0 30	0 32	0 33
9 0	0 26	0 28	0 29
9 30	0 22	0 24	0 25
10 0	0 19	0 20	0 20
10 30	0 16	0 17	0 18
11 0	0 14	0 14	0 14
11 30	0 12	0 12	0 11
12 0	0 9	0 9	0 9
13 0	0 6	0 6	0 7
14 0	0 4	0 3	0 2
15 0	0 0	0 0	0 0
16 0	<i>sub.</i> 0 0	<i>sub.</i> 0 2	<i>sub.</i> 0 3
17 0	0 3	0 4	0 6
18 0	0 5	0 6	0 8
20 0	0 8	0 9	0 11
22 0	0 10	0 14	0 15
24 0	0 13	0 15	0 18
26 0	0 15	0 17	0 19
28 0	0 17	0 20	0 21
30 0	0 18	0 22	0 24
34 0	0 20	0 24	0 27
40 0	0 23	0 27	0 30
50 0	0 24	0 27	0 30
60 0	0 21	0 24	0 27
65 0	0 18	0 21	0 23
70 0	0 16	0 18	0 20
74 0	0 13	0 16	0 18
78 0	0 10	0 12	0 13
80 0	0 8	0 10	0 11
82 0	0 6	0 8	0 9
84 0	0 5	0 6	0 6
86 0	0 4	0 4	0 4
88 0	0 2	0 2	0 2
90 0	0 0	0 0	0 0

TABLE 45[illegible]

TABLE 46

**AZIMUTH, AND CORRESPONDING CHANGE OF ALTITUDE
IN 1st OF TIME**

Lat.	Change of Altitude in 1"																
	0'	1'	2'	3'	4'	5'	6'	7'	8'	9'	10'	11'	12'	13'	14'	15'	
0°	0°	4°	8°	12°	15°	19°	24°	28°	32°	37°	42°	47°	51°	60°	69°	8°	
1	0	4	8	12	15	19	24	28	32	37	42	47	53	60	69	87	
4	0	4	8	12	15	20	24	28	32	37	42	47	53	61	69		
6	0	4	8	12	16	20	24	28	32	37	42	48	54	61	70		
8	0	4	8	12	16	20	24	28	33	37	42	48	54	61	71		
10	0	4	8	12	16	20	24	28	33	38	43	48	54	62	71		
11	0	4	8	12	16	20	24	28	33	38	43	48	55	62	72		
12	0	4	8	12	16	20	24	28	33	38	43	49	55	62	73		
13	0	4	8	12	16	20	24	29	33	38	43	49	55	63	73		
14	0	4	8	12	16	20	24	29	33	38	43	49	56	63	74		
15	0	4	8	12	16	20	24	29	34	38	44	49	56	64	75		
16	0	4	8	12	16	20	25	29	34	39	44	50	56	64	76		
17	0	4	8	12	16	20	25	29	34	39	44	50	57	65	77		
18	0	4	8	12	16	21	25	29	34	39	44	50	57	66	79		
19	0	4	8	12	16	21	25	30	34	39	45	51	58	66	81		
20	0	4	8	12	16	21	25	30	35	40	45	51	58	67	83		
21	0	4	8	12	17	21	25	30	35	40	46	52	59	68	89		
22	0	4	8	12	17	21	26	30	35	40	46	52	60	69			
23	0	4	8	13	17	21	26	30	35	41	46	53	60	70			
24	0	4	8	13	17	21	26	31	36	41	47	53	61	72			
25	0	4	8	13	17	22	26	31	36	41	47	54	62	73			
26	0	4	9	13	17	22	26	31	36	42	48	55	63	75			
27	0	4	9	13	17	22	27	32	37	42	48	55	64	77			
28	0	4	9	13	18	22	27	32	37	43	49	56	65	79			
29	0	4	9	13	18	22	27	32	37	43	50	57	66	82			
30	0	4	9	13	18	23	27	33	38	44	50	58	67				
31	0	4	9	13	18	23	28	33	38	44	51	59	69				
32	0	5	9	14	18	23	28	33	39	45	52	60	71				
33	0	5	9	14	19	23	28	34	39	46	53	61	73				
34	0	5	9	14	19	24	29	34	40	46	54	62	75				
35	0	5	9	14	19	24	29	35	41	47	54	64	78				
36	0	5	9	14	19	24	30	35	41	48	55	65	81				
37	0	5	10	14	19	25	30	36	42	49	57	67					
38	0	5	10	15	20	25	30	36	43	49	58	69					
39	0	5	10	15	20	26	31	37	43	51	59	71					
40	0	5	10	15	20	26	31	38	44	52	60	73					
41	0	5	10	15	21	26	32	38	45	53	62	76					
42	0	5	10	16	21	27	33	39	46	54	64	81					
43	0	5	10	16	21	27	33	40	47	55	66						
44	0	5	11	16	22	28	34	40	48	57	68						
45	0	5	11	16	22	28	34	41	49	58	71						
46	0	5	11	17	23	29	35	42	50	60	74						
47	0	6	11	17	23	29	36	43	51	62	78						
48	0	6	11	17	23	30	37	44	53	64	85						
49	0	6	12	18	24	31	38	45	54	66							
50	0	6	12	18	25	31	38	47	56	69							
51	0	6	12	19	25	32	39	48	58	72							
52	0	6	12	19	26	33	41	49	60	77							
53	0	6	13	19	26	34	42	51	61	85							
54	0	7	13	20	27	35	43	53	65								
55	0	7	13	20	28	36	44	54	68								
56	0	7	14	21	28	37	46	57	73								
57	0	7	14	22	29	38	47	59	78								
58	0	7	15	22	30	40	49	62									
59	0	7	15	23	31	40	51	65									
60	0	8	15	24	32	42	53	69									
61	0	8	16	24	33	43	56	74									
62	0	8	16	25	35	45	58	84									
63	0	8	17	26	36	47	62										
64	0	9	18	27	37	49	66										
65	0	9	18	28	39	52	70										
66	0	9	19	29	41	55	80										

LIMITS, AT SEA, OF THE
REDUCTION TO THE MERIDIAN.

Lat.	Declination of the same Name as the Lat.					
	0°	5°	10°	15°	20°	25°
0°	0° 0'	0° 3'	0° 5'	0° 8'	0° 11'	0° 14'
5	0 3	0 0	0 3	0 5	0 8	0 10
10	0 5	0 3	0 0	0 3	0 6	0 7
15	0 8	0 5	0 3	0 0	0 3	0 5
20	0 11	0 8	0 6	0 3	0 0	0 0
25	0 14	0 11	0 9	0 6	0 3	0 0
30	0 17	0 15	0 12	0 9	0 6	0 5
35	0 21	0 18	0 16	0 13	0 10	0 8
40	0 25	0 23	0 20	0 17	0 14	0 12
44	0 29	0 26	0 24	0 21	0 18	0 16
48	0 33	0 31	0 28	0 25	0 22	0 20
52	0 38	0 36	0 33	0 30	0 27	0 26
56	0 44	0 42	0 39	0 36	0 34	0 32
60	0 52	0 49	0 47	0 44	0 41	0 39
64	1 0	0 57	0 55	0 52	0 49	0 47
68	1 10	1 8	1 6	1 3	1 1	0 58
	Declination of contrary Name to the Lat.					
	0°	5°	10°	15°	20°	25°
0	0 0	0 3	0 5	0 8	0 11	0 13
5	0 3	0 5	0 8	0 11	0 14	0 16
10	0 5	0 8	0 11	0 13	0 16	0 18
15	0 8	0 11	0 13	0 16	0 19	0 21
20	0 11	0 14	0 16	0 19	0 22	0 24
25	0 14	0 17	0 19	0 22	0 25	0 27
30	0 17	0 20	0 23	0 25	0 28	0 30
35	0 21	0 24	0 26	0 29	0 32	0 34
40	0 25	0 28	0 30	0 33	0 36	0 38
44	0 29	0 32	0 34	0 37	0 40	0 42
48	0 33	0 36	0 39	0 41	0 44	0 46
52	0 38	0 41	0 44	0 46	0 49	0 51
56	0 44	0 47	0 50	0 52	0 55	0 57
60	0 52	0 55	0 57	1 00	1 3	1 5
64	1 0	1 3	1 6	while visible.		
68	1 10	1 13	1 16			

VALUE OF
THE REDUCTION.
AT WHICH THE 2nd
REDⁿ AMOUNTS TO 1'

Mer. Alt.	Reduc.	Mer. Alt.	Reduc.
5°	4° 40'	45°	1° 23'
6	4 16	46	1 21
7	3 57	47	1 20
8	3 41	48	1 19
9	3 28	49	1 17
10	3 18	50	1 16
11	3 8	51	1 15
12	3 0	52	1 13
13	2 53	53	1 12
14	2 46	54	1 11
15	2 40	55	1 9
16	2 35	56	1 8
17	2 30	57	1 7
18	2 25	58	1 6
19	2 21	59	1 4
20	2 17	60	1 3
21	2 14	61	1 2
22	2 10	62	1 0
23	2 7	63	0 59
24	2 4	64	0 58
25	2 2	65	0 57
26	1 59	66	0 55
27	1 56	67	0 54
28	1 54	68	0 53
29	1 51	69	0 52
30	1 49	70	0 50
31	1 47	71	0 49
32	1 45	72	0 47
33	1 43	73	0 46
34	1 41	74	0 44
35	1 39	75	0 43
36	1 37	76	0 41
37	1 36	77	0 40
38	1 34	78	0 38
39	1 32	79	0 37
40	1 31	80	0 35
41	1 29	81	0 33
42	1 27	82	0 31
43	1 26	83	0 29
44	1 24	84	0 27

TABLE 49

689

FOR COMPUTING THE REDUCTION TO THE MERIDIAN IN SECONDS

0 Hours

s.	0"	1"	2"	3"	4"	5"	6"	7"	8"	9"	10"	11"	12"	
0	0'0	2'0	7'8	17'7	31'4	49'1	70'7	96'2	125'7	159'0	196'3	237'5	282'7	60
1	0'0	2'0	8'0	17'9	31'7	49'4	71'1	96'6	126'2	159'6	197'0	238'3	283'5	59
2	0'0	2'1	8'1	18'1	31'9	49'7	71'5	97'1	126'7	160'2	197'6	239'0	284'2	58
3	0'0	2'2	8'2	18'3	32'2	50'1	71'9	97'6	127'2	160'8	198'3	239'7	285'0	57
4	0'0	2'2	8'4	18'5	32'5	50'4	72'3	98'1	127'8	161'4	198'9	240'4	285'8	56
5	0'0	2'3	8'5	18'7	32'7	50'7	72'7	98'5	128'3	162'0	199'6	241'2	286'6	55
6	0'0	2'4	8'7	18'9	33'0	51'1	73'1	99'0	128'8	162'6	200'3	241'9	287'4	54
7	0'0	2'4	8'8	19'1	33'3	51'4	73'5	99'4	129'4	163'2	200'9	242'6	288'2	53
8	0'0	2'5	8'9	19'3	33'5	51'7	73'9	99'9	129'9	163'8	201'6	243'3	289'0	52
9	0'0	2'6	9'1	19'5	33'8	52'1	74'3	100'4	130'4	164'4	202'2	244'1	289'8	51
10	0'0	2'7	9'2	19'7	34'1	52'4	74'7	100'8	131'0	165'0	202'9	244'8	290'6	50
11	0'1	2'7	9'4	19'9	34'4	52'7	75'1	101'3	131'5	165'6	203'6	245'5	291'4	49
12	0'1	2'8	9'5	20'1	34'6	53'1	75'5	101'8	132'0	166'2	204'2	246'2	292'2	48
13	0'1	2'9	9'6	20'3	34'9	53'4	75'9	102'3	132'6	166'8	204'9	247'0	293'0	47
14	0'1	3'0	9'8	20'5	35'2	53'8	76'3	102'7	133'1	167'4	205'6	247'7	293'8	46
15	0'1	3'1	9'9	20'7	35'5	54'1	76'7	103'2	133'6	168'0	206'3	248'5	294'6	45
16	0'1	3'1	10'1	20'9	35'7	54'5	77'1	103'7	134'2	168'6	206'9	249'2	295'4	44
17	0'2	3'2	10'2	21'2	36'0	54'8	77'5	104'2	134'7	169'2	207'6	249'9	296'2	43
18	0'2	3'3	10'4	21'4	36'3	55'1	77'9	104'6	135'3	169'8	208'3	250'7	297'0	42
19	0'2	3'4	10'5	21'6	36'6	55'5	78'3	105'1	135'8	170'4	208'9	251'4	297'8	41
20	0'2	3'5	10'7	21'8	36'9	55'8	78'8	105'6	136'4	171'0	209'6	252'2	298'6	40
21	0'3	3'6	10'8	22'0	37'2	56'2	79'2	106'1	136'9	171'6	210'3	252'9	299'4	39
22	0'3	3'7	11'0	22'3	37'4	56'5	79'6	106'6	137'4	172'2	211'0	253'6	300'2	38
23	0'3	3'8	11'1	22'5	37'7	56'9	80'0	107'0	138'0	172'9	211'6	254'4	301'0	37
24	0'3	3'8	11'3	22'7	38'0	57'3	80'4	107'5	138'5	173'5	212'3	255'1	301'8	36
25	0'3	3'9	11'5	22'9	38'3	57'6	80'8	108'0	139'1	174'1	213'0	255'9	302'6	35
26	0'4	4'0	11'6	23'1	38'6	58'0	81'3	108'5	139'6	174'7	213'7	256'6	303'5	34
27	0'4	4'1	11'8	23'4	38'9	58'3	81'7	109'0	140'2	175'3	214'4	257'4	304'3	33
28	0'4	4'2	11'9	23'6	39'2	58'7	82'1	109'5	140'7	175'9	215'1	258'2	305'1	32
29	0'5	4'3	12'1	23'8	39'5	59'0	82'5	110'0	141'3	176'6	215'8	258'9	305'9	31
30	0'5	4'4	12'3	24'0	39'8	59'4	83'0	110'4	141'8	177'2	216'4	259'6	306'7	30
31	0'5	4'5	12'4	24'3	40'1	59'8	83'4	110'9	142'4	177'8	217'1	260'4	307'5	29
32	0'6	4'6	12'6	24'5	40'3	60'1	83'8	111'4	143'0	178'4	217'8	261'1	308'4	28
33	0'6	4'7	12'8	24'7	40'6	60'5	84'2	111'9	143'5	179'0	218'5	261'9	309'2	27
34	0'6	4'8	12'9	25'0	40'9	60'8	84'7	112'4	144'1	179'7	219'2	262'6	310'0	26
35	0'7	4'9	13'1	25'2	41'2	61'2	85'1	112'9	144'6	180'3	219'9	263'4	310'8	25
36	0'7	5'0	13'3	25'4	41'5	61'6	85'5	113'4	145'2	180'9	220'6	264'1	311'6	24
37	0'7	5'1	13'4	25'7	41'8	61'9	86'0	113'9	145'8	181'6	221'3	264'9	312'5	23
38	0'8	5'2	13'6	25'9	42'1	62'3	86'4	114'4	146'3	182'2	222'0	265'7	313'3	22
39	0'8	5'3	13'8	26'2	42'5	62'7	86'8	114'9	146'9	182'8	222'7	266'4	314'2	21
40	0'9	5'4	14'0	26'4	42'8	63'0	87'3	115'4	147'5	183'4	223'4	267'2	315'0	20
41	0'9	5'6	14'1	26'6	43'1	63'4	87'7	115'9	148'0	184'1	224'1	267'9	315'8	19
42	1'0	5'7	14'3	26'9	43'4	63'8	88'1	116'4	148'6	184'7	224'8	268'7	316'6	18
43	1'0	5'8	14'5	27'1	43'7	64'2	88'6	116'9	149'2	185'4	225'5	269'5	317'4	17
44	1'1	5'9	14'7	27'4	44'0	64'5	89'0	117'4	149'7	186'0	226'2	270'2	318'3	16
45	1'1	6'0	14'8	27'6	44'3	64'9	89'5	117'9	150'3	186'6	226'9	271'0	319'1	15
46	1'2	6'1	15'0	27'9	44'6	65'3	89'9	118'4	150'9	187'3	227'6	271'8	319'9	14
47	1'2	6'2	15'2	28'1	44'9	65'7	90'3	118'9	151'5	187'9	228'3	272'6	320'8	13
48	1'3	6'4	15'4	28'3	45'2	66'0	90'8	119'5	152'0	188'5	229'0	273'3	321'6	12
49	1'3	6'5	15'6	28'6	45'5	66'4	91'2	120'0	152'6	189'2	229'7	274'1	322'4	11
50	1'4	6'6	15'8	28'8	45'9	66'8	91'7	120'5	153'2	189'8	230'4	274'9	323'3	10
51	1'4	6'7	15'9	29'1	46'2	67'2	92'1	121'0	153'8	190'5	231'1	275'6	324'1	9
52	1'5	6'8	16'1	29'4	46'5	67'6	92'6	121'5	154'4	191'1	231'8	276'4	325'0	8
53	1'5	7'0	16'3	29'6	46'8	68'0	93'0	122'0	154'9	191'8	232'5	277'2	325'8	7
54	1'6	7'1	16'5	29'9	47'1	68'3	93'5	122'5	155'5	192'4	233'3	278'0	326'7	6
55	1'6	7'2	16'7	30'1	47'5	68'7	93'9	123'1	156'1	193'1	234'0	278'9	327'5	5
56	1'7	7'3	16'9	30'4	47'8	69'1	94'4	123'6	156'7	193'7	234'7	279'5	328'4	4
57	1'8	7'5	17'1	30'6	48'1	69'5	94'8	124'1	157'3	194'4	235'4	280'3	329'2	3
58	1'8	7'6	17'3	30'9	48'4	69'9	95'3	124'6	157'8	195'0	236'1	281'1	330'0	2
59	1'9	7'7	17'5	31'1	48'8	70'3	95'7	125'1	158'4	195'7	236'8	281'9	330'9	1
60	2'0	7'8	17'7	31'4	49'1	70'7	96'2	125'7	159'0	196'3	237'5	282'7	331'8	0
	59"	58"	57"	56"	55"	54"	53"	52"	51"	50"	49"	48"	47"	s.

11 Hours

Y Y

TABLE 47

LIMITS, AT SEA, OF THE REDUCTION TO THE MERIDIAN.						
Lat.	Declination of the same Name as the Lat.					
	0°	5°	10°	15°	20°	25°
0°	0° 0'	0° 3'	0° 5'	0° 8'	0° 11'	0° 14'
5	0 3	0 0	0 3	0 5	0 8	0 10
10	0 5	0 3	0 0	0 3	0 6	0 7
15	0 8	0 5	0 3	0 0	0 3	0 5
20	0 11	0 8	0 6	0 3	0 0	0 0
25	0 14	0 11	0 9	0 6	0 3	0 0
30	0 17	0 15	0 12	0 9	0 6	0 5
35	0 21	0 18	0 16	0 13	0 10	0 8
40	0 25	0 23	0 20	0 17	0 14	0 12
44	0 29	0 26	0 24	0 21	0 18	0 16
48	0 33	0 31	0 28	0 25	0 22	0 20
52	0 38	0 36	0 33	0 30	0 27	0 26
56	0 44	0 42	0 39	0 36	0 34	0 32
60	0 52	0 49	0 47	0 44	0 41	0 39
64	1 0	0 57	0 55	0 52	0 49	0 47
68	1 10	1 8	1 6	1 3	1 1	0 58
0	Declination of contrary Name to the Lat.					
	0°	5°	10°	15°	20°	25°
0	0 0	0 3	0 5	0 8	0 11	0 13
5	0 3	0 5	0 8	0 11	0 14	0 16
10	0 5	0 8	0 11	0 13	0 16	0 18
15	0 8	0 11	0 13	0 16	0 19	0 21
20	0 11	0 14	0 16	0 19	0 22	0 24
25	0 14	0 17	0 19	0 22	0 25	0 27
30	0 17	0 20	0 23	0 25	0 28	0 30
35	0 21	0 24	0 26	0 29	0 32	0 34
40	0 25	0 28	0 30	0 33	0 36	0 38
44	0 29	0 32	0 34	0 37	0 40	0 42
48	0 33	0 36	0 39	0 41	0 44	0 46
52	0 38	0 41	0 44	0 46	0 49	0 51
56	0 44	0 47	0 50	0 52	0 55	0 57
60	0 52	0 55	0 57	1 00	1 3	1 5
64	1 0	1 3	1 6	while visible.		
68	1 10	1 13	1 16			

TABLE 48

VALUE OF THE REDUCTION. AT WHICH THE 2 nd RED ⁿ AMOUNTS TO 1'.			
Mer. Alt.	Reduc.	Mer. Alt.	Reduc.
50	4° 40'	45°	1° 23'
6	4 16	46	1 21
7	3 57	47	1 20
8	3 41	48	1 19
9	3 28	49	1 17
10	3 18	50	1 16
11	3 8	51	1 15
12	3 0	52	1 13
13	2 53	53	1 12
14	2 46	54	1 11
15	2 40	55	1 9
16	2 35	56	1 8
17	2 30	57	1 7
18	2 25	58	1 6
19	2 21	59	1 4
20	2 17	60	1 3
21	2 14	61	1 2
22	2 10	62	1 0
23	2 7	63	0 59
24	2 4	64	0 58
25	2 2	65	0 57
26	1 59	66	0 55
27	1 56	67	0 54
28	1 54	68	0 53
29	1 51	69	0 52
30	1 49	70	0 50
31	1 47	71	0 49
32	1 45	72	0 47
33	1 43	73	0 46
34	1 41	74	0 44
35	1 39	75	0 43
36	1 37	76	0 41
37	1 36	77	0 40
38	1 34	78	0 38
39	1 32	79	0 37
40	1 31	80	0 35
41	1 29	81	0 33
42	1 27	82	0 31
43	1 26	83	0 29
44	1 24	84	0 27

TABLE 49

689

FOR COMPUTING THE REDUCTION TO THE MERIDIAN IN SECONDS

0 Hours

a.	0"	1"	2"	3"	4"	5"	6"	7"	8"	9"	10"	11"	12"	
0	0'0	2'0	7'8	17'7	31'4	49'1	70'7	96'2	125'7	159'0	196'3	237'5	282'7	60
1	0'0	2'0	8'0	17'9	31'7	49'4	71'1	96'6	126'2	159'6	197'0	238'3	283'5	59
2	0'0	2'1	8'1	18'1	31'9	49'7	71'5	97'1	126'7	160'2	197'6	239'0	284'2	58
3	0'0	2'2	8'2	18'3	32'2	50'1	71'9	97'6	127'2	160'8	198'3	239'7	285'0	57
4	0'0	2'2	8'4	18'5	32'5	50'4	72'3	98'1	127'8	161'4	198'9	240'4	285'8	56
5	0'0	2'3	8'5	18'7	32'7	50'7	72'7	98'5	128'3	162'0	199'6	241'2	286'6	55
6	0'0	2'4	8'7	18'9	33'0	51'1	73'1	99'0	128'8	162'6	200'3	241'9	287'4	54
7	0'0	2'4	8'8	19'1	33'3	51'4	73'5	99'4	129'4	163'2	200'9	242'6	288'2	53
8	0'0	2'5	8'9	19'3	33'5	51'7	73'9	99'9	129'9	163'8	201'6	243'3	289'0	52
9	0'0	2'6	9'1	19'5	33'8	52'1	74'3	100'4	130'4	164'4	202'2	244'1	289'8	51
10	0'0	2'7	9'2	19'7	34'1	52'4	74'7	100'8	131'0	165'0	202'9	244'8	290'6	50
11	0'1	2'7	9'4	19'9	34'4	52'7	75'1	101'3	131'5	165'6	203'6	245'5	291'4	49
12	0'1	2'8	9'5	20'1	34'6	53'1	75'5	101'8	132'0	166'2	204'2	246'2	292'2	48
13	0'1	2'9	9'6	20'3	34'9	53'4	75'9	102'3	132'6	166'8	204'9	247'0	293'0	47
14	0'1	3'0	9'8	20'5	35'2	53'8	76'3	102'7	133'1	167'4	205'6	247'7	293'8	46
15	0'1	3'1	9'9	20'7	35'5	54'1	76'7	103'2	133'6	168'0	206'3	248'5	294'6	45
16	0'1	3'1	10'1	20'9	35'7	54'5	77'1	103'7	134'2	168'6	206'9	249'2	295'4	44
17	0'2	3'2	10'2	21'2	36'0	54'8	77'5	104'2	134'7	169'2	207'6	249'9	296'2	43
18	0'2	3'3	10'4	21'4	36'3	55'1	77'9	104'6	135'3	169'8	208'3	250'7	297'0	42
19	0'2	3'4	10'5	21'6	36'6	55'5	78'3	105'1	135'8	170'4	208'9	251'4	297'8	41
20	0'2	3'5	10'7	21'8	36'9	55'8	78'8	105'6	136'4	171'0	209'6	252'2	298'6	40
21	0'3	3'6	10'8	22'0	37'2	56'2	79'2	106'1	136'9	171'6	210'3	252'9	299'4	39
22	0'3	3'7	11'0	22'3	37'4	56'5	79'6	106'6	137'4	172'2	211'0	253'6	300'2	38
23	0'3	3'8	11'1	22'5	37'7	56'9	80'0	107'0	138'0	172'9	211'6	254'4	301'0	37
24	0'3	3'8	11'3	22'7	38'0	57'3	80'4	107'5	138'5	173'5	212'3	255'1	301'8	36
25	0'3	3'9	11'5	22'9	38'3	57'6	80'8	108'0	139'1	174'1	213'0	255'9	302'6	35
26	0'4	4'0	11'6	23'1	38'6	58'0	81'3	108'5	139'6	174'7	213'7	256'6	303'5	34
27	0'4	4'1	11'8	23'4	38'9	58'3	81'7	109'0	140'2	175'3	214'4	257'4	304'3	33
28	0'4	4'2	11'9	23'6	39'2	58'7	82'1	109'5	140'7	175'9	215'1	258'2	305'1	32
29	0'5	4'3	12'1	23'8	39'5	59'0	82'5	110'0	141'3	176'6	215'8	258'9	305'9	31
30	0'5	4'4	12'3	24'0	39'8	59'4	83'0	110'4	141'8	177'2	216'4	259'6	306'7	30
31	0'5	4'5	12'4	24'3	40'1	59'8	83'4	110'9	142'4	177'8	217'1	260'4	307'5	29
32	0'6	4'6	12'6	24'5	40'3	60'1	83'8	111'4	143'0	178'4	217'8	261'1	308'4	28
33	0'6	4'7	12'8	24'7	40'6	60'5	84'2	111'9	143'5	179'0	218'5	261'9	309'2	27
34	0'6	4'8	12'9	25'0	40'9	60'8	84'7	112'4	144'1	179'7	219'2	262'6	310'0	26
35	0'7	4'9	13'1	25'2	41'2	61'2	85'1	112'9	144'6	180'3	219'9	263'4	310'8	25
36	0'7	5'0	13'3	25'4	41'5	61'6	85'5	113'4	145'2	180'9	220'6	264'1	311'6	24
37	0'7	5'1	13'4	25'7	41'8	61'9	86'0	113'9	145'8	181'6	221'3	264'9	312'5	23
38	0'8	5'2	13'6	25'9	42'1	62'3	86'4	114'4	146'3	182'2	222'0	265'7	313'3	22
39	0'8	5'3	13'8	26'2	42'5	62'7	86'8	114'9	146'9	182'8	222'7	266'4	314'2	21
40	0'9	5'4	14'0	26'4	42'8	63'0	87'3	115'4	147'5	183'4	223'4	267'2	315'0	20
41	0'9	5'6	14'1	26'6	43'1	63'4	87'7	115'9	148'0	184'1	224'1	267'9	315'8	19
42	1'0	5'7	14'3	26'9	43'4	63'8	88'1	116'4	148'6	184'7	224'8	268'7	316'6	18
43	1'0	5'8	14'5	27'1	43'7	64'2	88'6	116'9	149'2	185'4	225'5	269'5	317'4	17
44	1'1	5'9	14'7	27'4	44'0	64'5	89'0	117'4	149'7	186'0	226'2	270'2	318'3	16
45	1'1	6'0	14'8	27'6	44'3	64'9	89'5	117'9	150'3	186'6	226'9	271'0	319'1	15
46	1'2	6'1	15'0	27'9	44'6	65'3	89'9	118'4	150'9	187'3	227'6	271'8	319'9	14
47	1'2	6'2	15'2	28'1	44'9	65'7	90'3	118'9	151'5	187'9	228'3	272'6	320'8	13
48	1'3	6'4	15'4	28'3	45'2	66'0	90'8	119'5	152'0	188'5	229'0	273'3	321'6	12
49	1'3	6'5	15'6	28'6	45'5	66'4	91'2	120'0	152'6	189'2	229'7	274'1	322'4	11
50	1'4	6'6	15'8	28'8	45'9	66'8	91'7	120'5	153'2	189'8	230'4	274'9	323'3	10
51	1'4	6'7	15'9	29'1	46'2	67'2	92'1	121'0	153'8	190'5	231'1	275'6	324'1	9
52	1'5	6'8	16'1	29'4	46'5	67'6	92'6	121'5	154'4	191'1	231'8	276'4	325'0	8
53	1'5	7'0	16'3	29'6	46'8	68'0	93'0	122'0	154'9	191'8	232'5	277'2	325'8	7
54	1'6	7'1	16'5	29'9	47'1	68'3	93'5	122'5	155'5	192'4	233'3	278'0	326'7	6
55	1'6	7'2	16'7	30'1	47'5	68'7	93'9	123'1	156'1	193'1	234'0	278'9	327'5	5
56	1'7	7'3	16'9	30'4	47'8	69'1	94'4	123'6	156'7	193'7	234'7	279'5	328'4	4
57	1'8	7'5	17'1	30'6	48'1	69'5	94'8	124'1	157'3	194'4	235'4	280'3	329'2	3
58	1'8	7'6	17'3	30'9	48'4	69'9	95'3	124'6	157'8	195'0	236'1	281'1	330'0	2
59	1'9	7'7	17'5	31'1	48'8	70'3	95'7	125'1	158'4	195'7	236'8	281'9	330'9	1
60	2'0	7'8	17'7	31'4	49'1	70'7	96'2	125'7	159'0	196'3	237'5	282'7	331'8	0
	59"	58"	57"	56"	55"	54"	53"	52"	51"	50"	49"	48"	47"	a.

11 Hours

I I

FOR COMPUTING THE REDUCTION TO THE MERIDIAN IN SECONDS

0 Hours

s.	13"	14"	15"	16"	17"	18"	19"	20"	21"	22"	23"	24"	
0	331'8	334'7	441'6	502'5	567'1	635'8	708'3	784'9	865'3	949'6	1037'8	1129'9	60
1	332'6	335'6	442'6	503'5	568'2	636'9	709'5	786'2	866'6	951'0	1039'3	1131'4	59
2	333'4	336'5	443'6	504'6	569'3	638'1	710'8	787'5	868'0	952'4	1040'8	1133'0	58
3	334'3	337'5	444'6	505'6	570'4	639'3	712'1	788'8	869'4	953'8	1042'3	1134'6	57
4	335'2	338'4	445'6	506'7	571'6	640'5	713'4	790'1	870'8	955'3	1043'8	1136'2	56
5	336'0	339'3	446'5	507'7	572'7	641'7	714'6	791'4	872'1	956'7	1045'3	1137'8	55
6	336'9	390'2	447'5	508'8	573'8	642'9	715'9	792'7	873'5	958'2	1046'8	1139'3	54
7	337'7	391'1	448'5	509'8	574'9	644'1	717'1	794'0	874'9	959'6	1048'3	1140'9	53
8	338'6	392'1	449'5	510'9	576'1	645'3	718'4	795'4	876'3	961'1	1049'8	1142'5	52
9	339'4	393'0	450'5	511'9	577'2	646'4	719'6	796'7	877'6	962'5	1051'3	1144'0	51
10	340'3	393'9	451'5	513'0	578'3	647'6	720'9	798'0	879'0	963'9	1052'8	1145'6	50
11	341'2	394'8	452'5	514'0	579'4	648'8	722'1	799'3	880'4	965'4	1054'3	1147'2	49
12	342'0	395'8	453'5	515'1	580'6	650'0	723'4	800'7	881'8	966'9	1055'9	1148'8	48
13	342'9	396'7	454'5	516'1	581'7	651'2	724'6	802'0	883'2	968'3	1057'4	1150'4	47
14	343'7	397'6	455'5	517'2	582'8	652'4	725'9	803'3	884'6	969'8	1058'9	1152'0	46
15	344'6	398'6	456'5	518'3	583'9	653'6	727'1	804'6	886'0	971'2	1060'4	1153'6	45
16	345'5	399'5	457'5	519'4	585'1	654'8	728'4	806'0	887'4	972'7	1062'0	1155'2	44
17	346'3	400'5	458'5	520'4	586'2	656'0	729'6	807'3	888'8	974'1	1063'5	1156'8	43
18	347'2	401'4	459'5	521'4	587'3	657'2	730'9	808'6	890'2	975'5	1065'0	1158'3	42
19	348'1	402'3	460'5	522'5	588'4	658'4	732'2	809'9	891'6	977'0	1066'5	1159'9	41
20	349'0	403'3	461'5	523'5	589'6	659'6	733'5	811'3	893'0	978'5	1068'1	1161'5	40
21	349'8	404'2	462'5	524'6	590'7	660'8	734'7	812'6	894'4	979'9	1069'6	1163'1	39
22	350'7	405'1	463'5	525'7	591'9	662'0	736'0	813'9	895'8	981'4	1071'1	1164'7	38
23	351'6	406'0	464'5	526'8	593'0	663'2	737'2	815'2	897'2	982'9	1072'6	1166'3	37
24	352'5	407'0	465'5	527'9	594'1	664'4	738'5	816'6	898'6	984'4	1074'2	1167'9	36
25	353'3	408'0	466'5	528'9	595'2	665'6	739'7	817'9	900'0	985'8	1075'7	1169'5	35
26	354'2	408'9	467'5	530'0	596'4	666'8	741'0	819'2	901'4	987'3	1077'2	1171'1	34
27	355'1	409'8	468'5	531'1	597'5	668'0	742'3	820'5	902'8	988'8	1078'7	1172'7	33
28	356'0	410'7	469'5	532'2	598'7	669'2	743'6	821'9	904'2	990'3	1080'3	1174'3	32
29	356'9	411'7	470'5	533'2	599'8	670'4	744'8	823'2	905'6	991'8	1081'8	1175'9	31
30	357'7	412'7	471'5	534'3	601'0	671'6	745'2	824'6	907'0	993'2	1083'3	1177'5	30
31	358'6	413'6	472'5	535'4	602'1	672'8	747'4	825'9	908'4	994'7	1084'8	1179'1	29
32	359'5	414'6	473'6	536'5	603'3	674'1	748'7	827'3	909'8	996'1	1086'4	1180'7	28
33	360'3	415'6	474'6	537'5	604'4	675'3	749'9	828'6	911'2	997'6	1087'9	1182'3	27
34	361'2	416'6	475'6	538'6	605'6	676'5	751'2	829'9	912'6	999'1	1089'5	1183'9	26
35	362'1	417'5	476'6	539'7	606'7	677'7	752'5	831'2	914'0	1000'6	1091'0	1185'5	25
36	363'0	418'4	477'6	540'8	607'9	678'9	753'8	832'6	915'5	1002'1	1092'6	1187'1	24
37	363'9	419'4	478'7	541'9	609'0	680'1	755'0	833'9	916'9	1003'5	1094'1	1188'7	23
38	364'8	420'3	479'7	543'0	610'2	681'3	756'3	835'3	918'3	1005'0	1095'7	1190'3	22
39	365'7	421'3	480'7	544'1	611'3	682'5	757'6	836'6	919'7	1006'5	1097'2	1191'9	21
40	366'5	422'2	481'7	545'2	612'5	683'8	758'9	838'0	921'1	1008'0	1098'8	1193'5	20
41	367'5	423'2	482'8	546'2	613'6	685'0	760'2	839'3	922'5	1009'4	1100'3	1195'1	19
42	368'4	424'2	483'8	547'3	614'8	686'2	761'5	840'7	923'9	1010'9	1101'9	1196'7	18
43	369'3	425'1	484'8	548'4	615'9	687'4	762'8	842'0	925'3	1012'4	1103'4	1198'3	17
44	370'2	426'1	485'8	549'5	617'1	688'7	764'0	843'4	926'8	1013'9	1105'0	1199'9	16
45	371'1	427'0	486'9	550'6	618'2	689'9	765'3	844'7	928'2	1015'4	1106'5	1201'5	15
46	372'0	428'0	487'9	551'7	619'4	691'1	766'6	846'1	929'6	1016'9	1108'1	1203'1	14
47	372'9	429'0	488'9	552'8	620'5	692'3	767'9	847'5	931'0	1018'4	1109'6	1204'7	13
48	373'8	430'0	490'0	553'9	621'7	693'6	769'2	848'9	932'4	1019'9	1111'2	1206'4	12
49	374'7	430'9	491'0	55'0	622'8	694'8	770'5	850'2	933'8	1021'4	1112'7	1208'0	11
50	375'6	431'9	492'0	556'1	624'0	696'0	771'8	851'6	935'2	1022'8	1114'3	1209'6	10
51	376'5	432'8	493'1	557'2	625'2	697'2	773'1	852'9	936'6	1024'3	1115'8	1211'2	9
52	377'4	433'8	494'1	558'3	626'4	698'4	774'5	854'3	938'1	1025'8	1117'4	1212'0	8
53	378'3	434'8	495'2	559'4	627'5	699'6	775'8	855'6	939'5	1027'3	1118'9	1213'5	7
54	379'2	435'7	496'2	560'5	628'7	700'9	777'1	857'1	940'9	1028'8	1120'5	1215'1	6
55	380'2	436'7	497'2	561'6	629'9	702'2	778'4	858'4	942'3	1030'3	1122'0	1217'7	5
56	381'1	437'7	498'2	562'7	631'1	703'5	779'7	859'8	943'8	1031'8	1123'6	1218'4	4
57	382'0	438'7	499'2	563'8	632'2	704'7	781'0	861'1	945'2	1033'3	1125'1	1221'0	3
58	382'9	439'6	500'3	564'9	633'4	705'9	782'3	862'5	946'6	1034'8	1126'7	1222'6	2
59	383'8	440'6	501'4	566'0	634'6	707'1	783'6	863'9	948'1	1036'3	1128'3	1224'2	1
60	384'7	441'6	502'5	567'1	635'8	708'3	784'9	865'3	949'6	1037'8	1129'9	1225'9	0
	40"	45"	44"	48"	42"	41"	40"	38"	38"	37"	36"	35"	e.

11 Hours

TABLE 49

FOR COMPUTING THE RED ^N TO THE MER ^N IN SEC ^{DS} .						
0 Hours						
S.	25 ^m	26 ^m	27 ^m	28 ^m	29 ^m	30 ^m
0	1225.9	1325.9	1429.7	1537.5	1649.0	1764.6
1	1227.5	1327.6	1431.4	1539.3	1650.9	1766.6
2	1229.2	1329.3	1433.2	1541.1	1652.8	1768.5
3	1230.8	1331.0	1434.9	1542.9	1654.7	1770.5
4	1232.5	1332.7	1436.7	1544.8	1656.6	1772.4
5	1234.1	1334.4	1438.5	1546.6	1658.5	1774.4
6	1235.7	1336.1	1440.3	1548.4	1660.4	1776.3
7	1237.3	1337.8	1442.1	1550.2	1662.3	1778.3
8	1239.0	1339.5	1443.9	1552.1	1664.2	1780.3
9	1240.6	1341.2	1445.6	1553.9	1666.1	1782.3
10	1242.3	1342.9	1447.4	1555.8	1668.0	1784.2
11	1243.9	1344.6	1449.2	1557.6	1669.9	1786.2
12	1245.6	1346.3	1451.0	1559.5	1671.9	1788.2
13	1247.2	1348.0	1452.8	1561.3	1673.8	1790.1
14	1248.9	1349.7	1454.5	1563.2	1675.7	1792.1
15	1250.5	1351.4	1456.3	1565.0	1677.6	1794.1
16	1252.2	1353.2	1458.1	1566.9	1679.5	1796.1
17	1253.8	1354.9	1459.9	1568.7	1681.4	1798.1
18	1255.5	1356.6	1461.6	1570.5	1683.3	1800.0
19	1257.1	1358.3	1463.4	1572.4	1685.2	1802.0
20	1258.8	1360.1	1465.2	1574.3	1687.2	1804.0
21	1260.4	1361.8	1466.9	1576.1	1689.1	1805.9
22	1262.1	1363.5	1468.7	1578.0	1691.0	1807.9
23	1263.7	1365.2	1470.5	1579.8	1692.9	1809.9
24	1265.4	1367.0	1472.3	1581.7	1694.8	1811.9
25	1267.0	1368.7	1474.0	1583.5	1696.7	1813.9
26	1268.7	1370.4	1475.9	1585.3	1698.6	1815.8
27	1270.3	1372.1	1477.7	1587.2	1700.5	1817.8
28	1272.0	1373.9	1479.5	1589.1	1702.5	1819.8
29	1273.7	1375.6	1481.3	1590.9	1704.4	1821.8
30	1275.4	1377.4	1483.1	1592.7	1706.3	1823.8
31	1277.1	1379.1	1484.9	1594.6	1708.2	1825.8
32	1278.8	1380.8	1486.7	1596.5	1710.2	1827.8
33	1280.4	1382.5	1488.5	1598.3	1712.1	1829.8
34	1282.1	1384.2	1490.3	1600.2	1714.0	1831.8
35	1283.8	1385.9	1492.1	1602.1	1715.9	1833.8
36	1285.5	1387.7	1493.9	1604.0	1717.9	1835.8
37	1287.1	1389.4	1495.7	1605.9	1719.8	1837.8
38	1288.8	1391.2	1497.5	1607.7	1721.7	1839.8
39	1290.5	1392.9	1499.3	1609.6	1723.6	1841.8
40	1292.2	1394.7	1501.1	1611.5	1725.6	1843.8
41	1293.8	1396.4	1502.9	1613.3	1727.5	1845.8
42	1295.5	1398.2	1504.7	1615.2	1729.5	1847.8
43	1297.2	1399.9	1506.5	1617.1	1731.5	1849.8
44	1298.9	1401.7	1508.4	1619.0	1733.4	1851.8
45	1300.5	1403.4	1510.2	1620.8	1735.3	1853.8
46	1302.2	1405.2	1512.0	1622.7	1737.2	1855.8
47	1303.9	1406.9	1513.8	1624.6	1739.2	1857.8
48	1305.6	1408.7	1515.6	1626.5	1741.2	1859.8
49	1307.3	1410.4	1517.4	1628.3	1743.1	1861.8
50	1309.0	1412.2	1519.2	1630.2	1745.1	1863.8
51	1310.7	1413.9	1521.0	1632.1	1747.0	1865.8
52	1312.4	1415.7	1522.9	1634.0	1749.0	1867.8
53	1314.1	1417.4	1524.7	1635.9	1750.9	1869.8
54	1315.7	1419.2	1526.5	1637.7	1752.9	1871.8
55	1317.4	1420.9	1528.3	1639.6	1754.8	1873.8
56	1319.1	1422.7	1530.2	1641.5	1756.8	1875.9
57	1320.8	1424.4	1532.0	1643.3	1758.7	1877.9
58	1322.5	1426.2	1533.8	1645.2	1760.7	1879.9
59	1324.2	1427.9	1535.6	1647.1	1762.6	1882.0
60	1325.9	1429.7	1537.5	1649.0	1764.6	1884.0
31 ^m	33 ^m	32 ^m	31 ^m	30 ^m	29 ^m	S.

11 Hours

TABLE 50 691

FOR COMPUTING THE 2 ^d REDUCTION IN SECONDS			
Hour Angle.	2nd Red.	Hour Angle.	2nd Red.
10 ^m 0 ^s	0.1	23 ^m 50 ^s	3.0
11 0 0.1		24 0 3.1	
11 30 0.2		24 10 3.2	
12 0 0.2		24 20 3.3	
12 30 0.2		24 30 3.4	
13 0 0.3		24 40 3.4	
13 30 0.3		24 50 3.5	
14 0 0.4		25 0 3.6	
14 30 0.4		25 10 3.7	
15 0 0.5		25 20 3.8	
15 30 0.5		25 30 3.9	
16 0 0.6		25 40 4.0	
16 30 0.7		25 50 4.1	
17 0 0.8		26 0 4.3	
17 30 0.9		26 10 4.4	
18 0 1.0		26 20 4.5	
18 30 1.1		26 30 4.6	
19 0 1.2		26 40 4.7	
19 30 1.3		26 50 4.8	
19 40 1.4		27 0 5.0	
19 50 1.4		27 10 5.1	
20 0 1.5		27 20 5.2	
20 10 1.5		27 30 5.3	
20 20 1.6		27 40 5.5	
20 30 1.6		27 50 5.6	
20 40 1.7		28 0 5.7	
20 50 1.8		28 10 5.9	
21 0 1.8		28 20 6.0	
21 10 1.9		28 30 6.1	
21 20 1.9		28 40 6.3	
21 30 2.0		28 50 6.4	
21 40 2.1		29 0 6.6	
21 50 2.1		29 10 6.7	
22 0 2.2		29 20 6.9	
22 10 2.2		29 30 7.1	
22 20 2.3		29 40 7.2	
22 30 2.4		29 50 7.4	
22 40 2.5		30 0 7.5	
22 50 2.5		30 10 7.6	
23 0 2.6		30 20 7.9	
23 10 2.7		30 30 8.1	
23 20 2.8		30 40 8.2	
23 30 2.8		30 50 8.4	
23 40 2.9		31 0 8.6	

CORRECTION OF THE ALTITUDE OF THE POLE-STAR FOR 1890.

R.A. Mer.	ALTITUDES					R.A. Mer.	ALTITUDES					Var. in 10 Years.
	0°	30°	50°	70°	80°		0°	30°	50°	70°	80°	
h m	sub.	sub.	sub.	sub.	sub.	h m	add.	add.	add.	add.	add.	sub.
0 0	1°13'	1°13'	1°13'	1°13'	1°13'	12 0	1°13'	1°13'	1°13'	1°14'	1°14'	3'
0 30	1 15	1 15	1 15	1 15	1 15	12 30	1 15	1 15	1 15	1 15	1 16	3
1 0	1 17	1 17	1 17	1 17	1 17	13 0	1 17	1 17	1 17	1 17	1 17	3
1 30	1 17	1 17	1 17	1 17	1 17	13 30	1 17	1 17	1 17	1 17	1 17	3
2 0	1 16	1 16	1 16	1 16	1 16	14 0	1 16	1 16	1 16	1 16	1 16	3
2 20	1 14	1 14	1 14	1 14	1 13	14 20	1 14	1 14	1 14	1 14	1 14	3
2 40	1 12	1 12	1 12	1 12	1 11	14 40	1 12	1 12	1 12	1 12	1 13	3
3 0	1 9	1 9	1 9	1 9	1 8	15 0	1 9	1 9	1 9	1 10	1 10	2
3 10	1 7	1 7	1 7	1 7	1 6	15 10	1 7	1 8	1 8	1 8	1 9	2
3 20	1 6	1 5	1 5	1 5	1 4	15 20	1 6	1 6	1 6	1 6	1 7	2
3 30	1 5	1 4	1 4	1 4	1 3	15 30	1 5	1 5	1 5	1 5	1 6	2
3 40	1 3	1 3	1 2	1 2	1 1	15 40	1 3	1 3	1 3	1 4	1 5	2
3 50	1 0	1 0	1 0	1 0	0 58	15 50	1 0	1 1	1 1	1 1	1 3	2
4 0	0 58	0 58	0 58	0 57	0 56	16 0	0 58	0 59	0 59	0 59	1	2
4 10	0 56	0 56	0 55	0 55	0 53	16 10	0 56	0 56	0 56	0 57	0 59	1
4 20	0 54	0 54	0 54	0 53	0 52	16 20	0 54	0 55	0 55	0 56	0 57	1
4 30	0 52	0 51	0 51	0 50	0 49	16 30	0 52	0 52	0 52	0 53	0 55	1
4 40	0 49	0 49	0 48	0 48	0 46	16 40	0 49	0 49	0 50	0 51	0 52	1
4 50	0 46	0 46	0 45	0 45	0 43	16 50	0 46	0 47	0 47	0 48	0 50	1
5 0	0 44	0 44	0 44	0 43	0 41	17 0	0 44	0 45	0 45	0 46	0 48	1
5 10	0 41	0 41	0 41	0 40	0 37	17 10	0 41	0 42	0 42	0 43	0 45	1
5 20	0 38	0 38	0 38	0 36	0 34	17 20	0 38	0 39	0 39	0 40	0 43	0
5 30	0 35	0 35	0 34	0 33	0 31	17 30	0 35	0 36	0 36	0 37	0 41	0
5 40	0 32	0 32	0 31	0 30	0 28	17 40	0 32	0 33	0 33	0 34	0 37	0
5 50	0 29	0 28	0 28	0 27	0 24	17 50	0 29	0 29	0 30	0 31	0 33	0
6 0	0 26	0 25	0 25	0 23	0 21	18 0	0 26	0 26	0 27	0 28	0 30	0
6 10	0 22	0 22	0 21	0 20	0 17	18 10	0 22	0 23	0 23	0 25	0 27	0
6 20	0 19	0 18	0 18	0 16	0 14	18 20	0 19	0 19	0 20	0 21	0 24	0
6 30	0 16	0 16	0 15	0 14	0 11	18 30	0 16	0 17	0 17	0 19	0 21	0
6 40	0 13	0 12	0 12	0 10	0 8	18 40	0 13	0 13	0 14	0 15	0 18	0
6 50	0 9	0 9	0 8	0 7	0 4	18 50	0 9	0 10	0 11	0 12	0 15	0
7 0	0 6	0 5	0 5	0 3	0 1	19 0	0 6	0 6	0 7	0 9	0 11	0
7 10	0 3	0 3	0 2	0 1	0 3	19 10	0 3	0 4	0 5	0 6	0 9	0
7 20	add.	add.	add.	0 4	0 6	19 20	sub.	sub.	0 0	0 1	0 4	1
7 30	0 4	0 4	0 5	0 6	0 9	19 30	0 4	0 3	0 2	0 1	0 2	1
7 40	0 7	0 8	0 8	0 10	0 12	19 40	0 7	0 7	0 6	0 5	0 2	1
7 50	0 11	0 11	0 12	0 13	0 16	19 50	0 11	0 10	0 9	0 8	0 5	2
8 0	0 14	0 15	0 15	0 17	0 19	20 0	0 14	0 14	0 13	0 12	0 9	2
8 10	0 17	0 18	0 18	0 20	0 22	20 10	0 17	0 17	0 16	0 15	0 12	2
8 20	0 21	0 21	0 22	0 23	0 26	20 20	0 21	0 20	0 20	0 18	0 16	2
8 30	0 24	0 25	0 25	0 26	0 29	20 30	0 24	0 24	0 23	0 22	0 20	2
8 40	0 27	0 28	0 28	0 30	0 32	20 40	0 27	0 27	0 27	0 25	0 23	2
8 50	0 30	0 30	0 31	0 32	0 34	20 50	0 30	0 29	0 29	0 28	0 25	2
9 0	0 33	0 33	0 34	0 35	0 37	21 0	0 33	0 32	0 32	0 31	0 29	2
9 10	0 36	0 36	0 37	0 38	0 40	21 10	0 36	0 36	0 35	0 34	0 32	3
9 20	0 39	0 39	0 40	0 41	0 43	21 20	0 39	0 39	0 38	0 37	0 35	3
9 30	0 42	0 42	0 43	0 44	0 45	21 30	0 42	0 42	0 41	0 40	0 38	3
9 40	0 45	0 45	0 46	0 47	0 48	21 40	0 45	0 45	0 44	0 43	0 41	3
9 50	0 47	0 47	0 47	0 48	0 50	21 50	0 47	0 46	0 46	0 45	0 43	3
10 0	0 50	0 51	0 51	0 52	0 53	22 0	0 50	0 50	0 50	0 49	0 47	3
10 10	0 53	0 53	0 53	0 54	0 55	22 10	0 53	0 53	0 52	0 52	0 50	3
10 20	0 55	0 56	0 56	0 57	0 58	22 20	0 55	0 55	0 55	0 54	0 53	3
10 30	0 57	0 57	0 57	0 58	0 59	22 30	0 57	0 56	0 56	0 56	0 55	3
10 40	0 59	0 59	0 59	1 0	1 1	22 40	0 59	0 59	0 59	0 58	0 57	3
10 50	1 1	1 1	1 1	1 2	1 3	22 50	1 1	1 1	1 1	1 0	0 59	3
11 0	1 3	1 3	1 3	1 4	1 5	23 0	1 3	1 3	1 3	1 2	1 1	3
11 10	1 7	1 7	1 7	1 7	1 8	23 10	1 7	1 7	1 6	1 6	1 6	3
11 20	1 10	1 10	1 10	1 10	1 10	23 20	1 10	1 10	1 9	1 9	1 9	3
11 30	1 13	1 13	1 13	1 14	1 14	23 30	1 13	1 13	1 13	1 13	1 13	3
11 40	1 13	1 13	1 13	1 14	1 14	23 40	1 13	1 13	1 13	1 13	1 13	3
11 50	1 13	1 13	1 13	1 14	1 14	23 50	1 13	1 13	1 13	1 13	1 13	3
12 0	1 13	1 13	1 13	1 14	1 14	24 0	1 13	1 13	1 13	1 13	1 13	3

TABLE 52

REDUCTION OF LATITUDE					
Compression $\frac{1}{293}$, (Clarke's figure of the earth)					
Lat.	Red.	Lat.	Red.	Lat.	Red.
0°	0' 0"	30°	10' 9"	60°	10' 11"
1	0 24	31	10 21	61	9 58
2	0 49	32	10 32	62	9 45
3	1 13	33	10 42	63	9 31
4	1 38	34	10 52	64	9 16
5	2 2	35	11 1	65	9 1
6	2 26	36	11 9	66	8 44
7	2 50	37	11 16	67	8 27
8	3 13	38	11 23	68	8 10
9	3 37	39	11 28	69	7 52
10	4 0	40	11 33	70	7 34
11	4 23	41	11 37	71	7 15
12	4 45	42	11 40	72	6 55
13	5 8	43	11 42	73	6 35
14	5 30	44	11 44	74	6 14
15	5 51	45	11 44	75	5 53
16	6 12	46	11 44	76	5 32
17	6 33	47	11 43	77	5 10
18	6 53	48	11 40	78	4 47
19	7 12	49	11 38	79	4 25
20	7 31	50	11 34	80	4 2
21	7 50	51	11 29	81	3 38
22	8 8	52	11 24	82	3 15
23	8 25	53	11 17	83	2 51
24	8 42	54	11 10	84	2 27
25	8 58	55	11 2	85	2 3
26	9 14	56	10 54	86	1 38
27	9 28	57	10 44	87	1 14
28	9 43	58	10 34	88	0 49
29	9 56	59	10 23	89	0 25

TABLE 53

693

CORRECTION OF THE LUNAR DISTANCE FOR THE CONTRACTION OF THE VERTICAL SEMIDIAMETER											
Alt.	Angle between the Lun. Dist. and the Plumb Line										
	0°	10°	20°	30°	40°	50°	60°	70°	80°	90°	
3°	51'	49'	45'	38'	30'	21'	13'	6'	1'	0	
4	36	35	32	27	21	15	9	4	1	0	
5	26	24	22	19	15	10	6	3	1	0	
6	20	19	18	15	12	8	5	2	0	0	
7	16	16	14	12	9	6	4	2	0	0	
8	11	11	10	9	7	4	3	1	0	0	
9	10	9	9	7	6	4	2	1	0	0	
10	9	8	7	6	5	3	2	1	0	0	
12	5	5	4	4	3	2	1	1	0	0	
15	3	3	2	2	2	1	1	0	0	0	
20	2	2	2	2	1	1	0	0	0	0	
30	1	1	1	1	0	0	0	0	0	0	
40	0	0	0	0	0	0	0	0	0	0	

For the nearest Limb, sub.; for the farthest Limb, add.

TABLE 54

ERROR OF OBSERVATION ARISING FROM ERROR OF PARALLELISM									
Obser. Angle.	Error of Parallelism of the Telescope								
	10'	20'	30'	40'	50'	1° 0'	1° 10'	1° 20'	
10°	0' 0"	0' 1"	0' 1"	0' 2"	0' 4"	0' 6"	0' 7"	0' 10"	
20	0 0	0 0	10 30	50 8	0 11	0 15	0 20		
30	0 10	20 40	70 12	0 17	0 23	0 30			
40	0 10	30 60	100 20	0 23	0 31	0 40			
50	0 10	30 80	130 20	0 29	0 40	0 52			
60	0 10	40 90	160 25	0 36	0 49	1 4			
70	0 10	50 110	200 31	0 44	1 0	1 18			
80	0 20	60 130	230 37	0 53	1 12	1 33			
90	0 20	70 160	280 44	1 3	1 26	1 52			
100	0 20	80 190	330 52	1 15	1 42	2 13			
110	0 30	100 220	400 1 2	1 30	2 2	2 39			
120	0 30	120 270	480 1 16	1 49	2 28	3 14			

TABLE 55

FOR CORRECTING THE LUNAR DISTANCE FOR THE SPHEROIDAL FIGURE OF THE EARTH										
Latitude	Moon's Altitude									
	0°	10°	20°	30°	40°	50°	60°	70°	80°	90°
0° or 90°	0	0	0	0	0	0	0	0	0	0
3 .. 87	0	20	40	60	80	90	100	110	120	120
5 .. 85	0	30	70	100	130	150	170	190	200	200
8 .. 82	0	50	110	160	200	240	270	300	310	310
10 .. 80	0	70	140	200	260	300	340	360	380	390
13 .. 77	0	90	170	250	320	380	430	470	490	500
16 .. 74	0	110	200	300	390	460	530	570	600	610
19 .. 71	0	120	240	350	450	540	610	660	690	700
22 .. 68	0	140	270	400	500	610	690	740	780	790
26 .. 64	0	160	310	450	580	690	780	850	890	900
31 .. 59	0	180	340	500	650	770	870	950	990	1010
37 .. 53	0	190	370	550	700	840	950	1030	1080	1100
45	0	200	390	600	740	900	990	1070	1120	1140

FOR COMPUTING THE MOON'S SECOND CORRECTION OF DISTANCE

2 ^d Cor. of Alt. or Dist.	Apparent Distance																		
	13°	14°	15°	16°	17°	18°	19°	20°	23°	26°	30°	34°	38°	44°	50°	60°	70°	80°	90°
5	1"	1"	1"	1"	1"	1"	1"	1"	add	0"	0"	0"	0"	0"	0"	0"	0"	0"	0"
8	2	2	2	2	2	2	2	2	1	1	1	1	1	1	1	1	1	1	1
10	4	3	3	3	3	3	3	2	2	2	2	2	2	2	2	2	2	2	2
11	5	4	4	4	4	4	3	3	3	3	3	3	3	3	3	3	3	3	3
12	5	5	5	5	5	5	4	4	4	4	4	4	4	4	4	4	4	4	4
13	6	6	6	6	6	6	5	5	5	5	5	5	5	5	5	5	5	5	5
14	7	7	7	7	7	7	6	6	6	6	6	6	6	6	6	6	6	6	6
15	9	8	8	8	8	8	7	7	7	7	7	7	7	7	7	7	7	7	7
16	10	9	9	9	9	9	8	8	8	8	8	8	8	8	8	8	8	8	8
17	11	10	9	9	9	8	8	7	6	5	4	4	4	3	3	2	1	1	0
18	12	11	11	10	9	9	8	7	6	5	4	4	4	3	2	2	1	0	0
19	14	13	12	11	10	9	9	7	6	5	5	4	4	3	3	2	1	1	0
20	15	14	13	12	11	11	10	8	7	6	5	5	4	4	3	2	1	1	0
21	17	15	14	13	12	11	10	9	8	7	6	6	5	4	3	2	1	1	0
22	18	17	16	15	14	13	12	10	9	7	6	5	5	4	4	3	2	1	0
23	20	19	17	16	15	14	13	11	9	8	7	6	6	5	4	3	2	1	0
24	22	20	19	18	16	15	14	12	10	9	7	6	6	5	4	3	2	1	0
25	24	22	20	19	18	17	15	13	11	9	8	7	6	5	4	3	2	1	0
26	26	24	22	21	19	18	16	14	12	10	9	8	7	6	5	4	3	2	1
27	28	26	24	22	21	20	17	15	13	11	9	8	7	6	5	4	3	2	1
28	30	27	26	24	22	21	19	16	14	12	10	9	7	6	4	4	3	1	0
29	32	29	27	26	24	23	20	17	15	13	11	9	8	7	6	4	3	1	0
30	34	31	29	27	26	24	22	19	16	14	12	10	8	7	5	3	1	0	0
31	36	34	31	29	27	26	23	20	17	15	13	11	9	7	5	3	1	0	0
32	39	36	33	31	29	27	25	21	18	15	13	11	9	7	5	3	2	0	0
33	41	38	35	33	31	29	26	22	19	16	14	12	10	8	5	3	2	0	0
34	44	40	38	35	33	31	28	24	21	17	15	13	10	8	6	4	2	0	0
35	46	43	40	37	35	33	29	25	22	19	16	14	11	9	6	4	2	0	0
36	49	45	42	39	37	35	31	27	23	20	17	14	12	9	7	4	2	0	0
37	52	48	45	42	39	37	33	28	24	21	18	15	12	10	7	4	2	0	0
38	55	51	47	44	41	39	35	30	26	22	19	16	13	11	7	5	2	0	0
39	57	53	50	46	43	41	36	31	27	23	20	17	14	11	8	5	2	0	0
40	60	56	52	49	46	43	38	33	29	24	21	18	14	12	8	5	2	0	0
41	63	59	55	51	48	45	40	35	30	25	22	19	15	12	8	5	3	0	0
42	67	62	57	54	50	47	42	36	32	27	23	20	16	13	9	6	3	0	0
43	70	65	60	56	53	50	44	38	33	28	24	21	17	14	9	6	3	0	0
44	73	68	63	59	55	52	46	40	35	29	25	22	17	14	10	6	3	0	0
45	76	71	66	62	58	54	49	42	36	31	26	23	18	15	10	6	3	0	0
46	80	74	69	64	60	57	51	43	38	32	27	24	19	15	11	7	3	0	0
47	83	77	72	67	63	59	53	45	40	33	29	25	20	16	11	7	3	0	0
48	87	81	75	70	66	62	55	47	41	35	30	26	21	17	12	7	4	0	0
49	91	84	78	73	68	64	58	49	43	36	31	27	22	18	12	8	4	0	0
50	94	87	81	76	71	67	60	51	45	38	32	28	23	18	13	8	4	0	0
51	98	91	85	79	74	70	62	53	47	39	34	29	24	19	13	8	4	0	0
52	102	95	88	82	77	73	65	56	48	41	35	30	24	20	14	9	4	0	0
53	106	98	91	85	80	75	67	58	50	42	36	31	25	21	14	9	4	0	0
54	110	102	95	89	83	78	70	60	52	44	38	33	26	21	15	9	4	0	0
55	114	106	98	92	86	81	72	62	54	46	39	34	27	22	15	10	5	0	0
56	118	110	102	95	89	84	75	64	56	47	41	35	28	23	16	10	5	0	0
57	123	114	106	99	93	87	78	67	58	49	42	36	29	24	16	10	5	0	0
58	127	118	109	102	96	90	81	69	60	51	44	38	30	25	17	11	5	0	0
59	131	122	113	106	99	93	83	72	62	53	45	39	31	25	18	11	5	0	0
60	136	126	117	109	103	97	86	74	64	54	47	40	33	26	18	11	5	0	0
															sub.	sub.	sub.	sub.	sub.
															130°	120°	110°	100°	90°

TABLE 57

695

CORRECTION OF THE GREENWICH MEAN TIME FOR THE 2D DIFFERENCE OF THE LUNAR DISTANCE																										
Diff. of Prop. Log. in the Naut. Alm.	Interval												Diff. of Prop. Log. in the Naut. Alm.	Interval												
	0 ^h						1 ^h							0 ^h						1 ^h						
	0 ^m	10 ^m	20 ^m	30 ^m	40 ^m	50 ^m	0 ^m	10 ^m	20 ^m	30 ^m	40 ^m	50 ^m		0 ^m	10 ^m	20 ^m	30 ^m	40 ^m	50 ^m	0 ^m	10 ^m	20 ^m	30 ^m	40 ^m	50 ^m	
	0	10	20	30	40	50	0	10	20	30	40	50		0	10	20	30	40	50	0	10	20	30	40	50	
6	0	0	1	1	1	1	2	2	2	2	2	2	114	0	0	8	14	20	24	28	31	34	35	35	35	
12	0	0	1	1	2	3	3	3	4	4	4	4	120	0	0	8	15	21	26	30	32	36	37	37	37	
18	0	0	1	2	3	4	4	5	5	6	6	6	126	0	0	9	16	22	27	31	34	37	39	39	39	
24	0	0	2	3	4	5	6	6	7	7	7	7	132	0	0	9	17	23	28	33	36	39	40	41	41	
30	0	0	2	3	5	6	7	8	9	9	9	9	138	0	0	9	18	24	30	34	37	41	42	43	43	
36	0	0	2	4	6	8	9	10	11	11	11	11	144	0	0	10	18	25	31	36	39	43	44	45	45	
42	0	0	3	5	7	9	10	11	12	13	14	15	150	0	0	10	19	26	32	37	40	44	47	47	47	
48	0	0	3	6	8	10	12	13	14	15	15	15	156	0	0	11	20	27	33	39	42	46	48	48	48	
54	0	0	4	7	9	12	13	15	16	17	17	17	162	0	0	11	21	28	35	40	44	48	50	50	50	
60	0	0	4	7	10	13	15	16	18	18	19	19	168	0	0	11	21	29	36	42	45	50	52	52	52	
66	0	0	4	8	11	14	16	18	19	20	20	20	174	0	0	12	22	30	37	43	47	51	53	54	54	
72	0	0	5	9	12	15	18	19	21	22	22	22	180	0	0	12	23	31	39	45	49	53	55	56	56	
78	0	0	5	10	13	17	19	21	23	24	24	24	186	0	0	12	24	32	40	46	50	55	57	58	58	
84	0	0	6	10	14	18	21	23	25	26	26	26	192	0	0	13	24	33	41	48	52	57	59	60	60	
90	0	0	6	11	15	19	22	24	27	28	28	28	198	0	0	13	25	34	43	49	53	58	61	62	62	
96	0	0	7	12	17	21	25	26	28	29	30	30	204	0	0	14	26	35	44	51	55	60	63	63	63	
102	0	0	7	12	18	22	25	27	30	31	32	32	210	0	0	14	26	36	45	52	57	62	64	65	65	
108	0	0	7	13	19	23	27	29	32	33	33	33	216	0	0	14	27	37	46	54	58	64	66	67	67	
	0 ^m	50 ^m	40 ^m	30 ^m	20 ^m	10 ^m	0 ^m	50 ^m	40 ^m	30 ^m				0 ^m	50 ^m	40 ^m	30 ^m	20 ^m	10 ^m	0 ^m	50 ^m	40 ^m	30 ^m			
	3 ^h	2 ^h						1 ^h						3 ^h	2 ^h						1 ^h					
	Interval													Interval												

TABLE 58

ERROR OF THE SHIP'S PLACE IN NAUTICAL MILES, AND OF THE LONG. IN TIME, Corresponding to an Error of 1' in the Lunar Distance.											
Prop. Log. in the Naut. Alm.	Change in 3 hours	Latitude									
		0°	10°	20°	30°	40°	50°	60°	70°	80°	Error of Long. in Time.
2218	1° 48'	25	25	23	22	19	16	12	9	4	1 40
2341	1 45	26	26	24	22	20	17	13	9	4	1 44
2467	1 42	27	27	25	23	21	17	13	9	5	1 48
2596	1 39	28	27	26	24	21	18	14	10	5	1 52
2685	1 37	29	28	27	25	22	19	14	10	5	1 56
2821	1 34	30	29	28	26	23	19	15	10	5	2 0
2962	1 31	31	30	29	27	24	20	15	11	5	2 4
3108	1 28	32	31	30	28	24	21	16	11	5	2 8
3269	1 25	33	32	31	28	25	21	16	11	6	2 12
3415	1 22	34	33	32	29	26	22	17	12	6	2 16
3572	1 20	35	34	33	30	27	23	17	12	6	2 20
3688	1 17	36	35	34	31	28	23	18	12	6	2 24
3800	1 14	37	36	35	32	28	24	18	13	6	2 28
4040	1 11	38	37	36	33	29	24	19	13	7	2 32

CORRECTION OF THE GREENWICH MEAN TIME FOR THE 2D DIFFERENCE OF THE LUNAR DISTANCE																																																													
Diff. of Prop. Log. in the Naut. Alm.	Interval												Diff. of Prop. Log. in the Naut. Alm.	Interval																																															
	0 ^h						1 ^h							0 ^h						1 ^h																																									
	0 ^m	10 ^m	20 ^m	30 ^m	40 ^m	50 ^m	0 ^m	10 ^m	20 ^m	30 ^m	40 ^m	50 ^m		0 ^m	10 ^m	20 ^m	30 ^m	40 ^m	50 ^m	0 ^m	10 ^m	20 ^m	30 ^m	40 ^m	50 ^m	0 ^m	10 ^m	20 ^m	30 ^m	40 ^m	50 ^m																														
6	0	0	1	1	1	2	2	2	2	2	2	2	114	0	8	14	20	24	28	31	34	35	35	0	8	14	20	24	28	31	34	35	35																												
12	0	1	1	2	3	3	3	4	4	4	4	4	120	0	8	15	21	26	30	32	36	37	37	0	8	15	21	26	30	32	36	37	37																												
18	0	1	2	3	4	4	5	5	6	6	6	6	126	0	9	16	22	27	31	34	37	39	39	0	9	16	22	27	31	34	37	39	39																												
24	0	2	3	4	5	6	6	7	7	7	7	7	132	0	9	17	23	28	33	36	39	40	41	0	9	17	23	28	33	36	39	40	41																												
30	0	2	3	5	6	7	8	8	9	9	9	9	138	0	9	18	24	30	34	37	41	42	43	0	9	18	24	30	34	37	41	42	43																												
36	0	2	4	6	8	9	10	11	11	11	11	11	144	0	10	18	25	31	36	39	43	44	45	0	10	18	25	31	36	39	43	44	45																												
42	0	3	5	7	9	10	11	12	13	13	14	15	150	0	10	19	26	32	37	40	44	47	47	0	10	19	26	32	37	40	44	47	47																												
48	0	3	6	8	10	12	13	14	15	15	15	15	156	0	11	20	27	33	39	42	46	48	48	0	11	20	27	33	39	42	46	48	48																												
54	0	4	7	9	12	13	15	16	17	17	17	17	162	0	11	21	28	35	40	44	48	50	50	0	11	21	28	35	40	44	48	50	50																												
60	0	4	7	10	13	15	16	18	18	19	19	19	168	0	11	21	29	36	42	45	50	52	52	0	11	21	29	36	42	45	50	52	52																												
66	0	4	8	11	14	16	18	19	20	20	20	20	174	0	12	22	30	37	43	47	51	53	54	0	12	22	30	37	43	47	51	53	54																												
72	0	5	9	12	15	18	19	21	22	22	22	22	180	0	12	23	31	39	45	49	53	55	56	0	12	23	31	39	45	49	53	55	56																												
78	0	5	10	13	17	19	21	23	24	24	24	24	186	0	12	24	32	40	46	50	55	57	58	0	12	24	32	40	46	50	55	57	58																												
84	0	6	10	14	18	21	23	25	26	26	26	26	192	0	13	24	33	41	48	52	57	59	60	0	13	24	33	41	48	52	57	59	60																												
90	0	6	11	15	19	22	24	27	28	28	28	28	198	0	13	25	34	43	49	53	58	61	62	0	13	25	34	43	49	53	58	61	62																												
96	0	7	12	17	21	25	26	28	29	30	30	30	204	0	14	26	35	44	51	55	60	63	63	0	14	26	35	44	51	55	60	63	63																												
102	0	7	12	18	22	25	27	30	31	32	32	32	210	0	14	26	36	45	52	57	62	64	65	0	14	26	36	45	52	57	62	64	65																												
108	0	7	13	19	23	27	29	32	33	33	33	33	216	0	14	27	37	46	54	58	64	66	67	0	14	27	37	46	54	58	64	66	67																												
	0 ^m	50 ^m	40 ^m	30 ^m	20 ^m	10 ^m	0 ^m	50 ^m	40 ^m	30 ^m	20 ^m	10 ^m		0 ^m	50 ^m	40 ^m	30 ^m	20 ^m	10 ^m	0 ^m	50 ^m	40 ^m	30 ^m		0 ^m	50 ^m	40 ^m	30 ^m	20 ^m	10 ^m	0 ^m	50 ^m	40 ^m	30 ^m																											
	3 ^h	2 ^h					1 ^h							3 ^h	2 ^h					1 ^h							3 ^h	2 ^h					1 ^h																												
	Interval																															Interval																													

TABLE 58

ERROR OF THE SHIP'S PLACE IN NAUTICAL MILES, AND OF THE LONG. IN TIME, Corresponding to an Error of 1' in the Lunar Distance.												
Prop. Log. in the Naut. Alm.	Change in 3 hours	Latitude										Error of Long. in Time.
		0°	10°	20°	30°	40°	50°	60°	70°	80°		
2218	1° 48'	mil.	mil.	mil.	mil.	mil.	mil.	mil.	mil.	mil.	m s	
2341	1 45	25	25	23	22	19	16	12	9	4	1 40	
2407	1 42	26	26	24	22	20	17	13	9	4	1 44	
2506	1 39	27	27	25	23	21	17	13	9	5	1 48	
2685	1 37	28	27	26	24	21	18	14	10	5	1 52	
2821	1 34	29	28	27	25	22	19	14	10	5	1 56	
2962	1 31	30	29	28	26	23	19	15	10	5	2 0	
3108	1 28	31	30	29	27	24	20	15	11	5	2 4	
3259	1 25	32	31	30	28	24	21	16	11	5	2 8	
3415	1 22	33	32	31	28	25	21	16	11	6	2 12	
3572	1 20	34	33	32	29	26	22	17	12	6	2 16	
3688	1 17	35	34	33	30	27	23	17	12	6	2 20	
3860	1 14	36	35	34	31	28	23	18	12	6	2 24	
4040	1 11	37	36	35	32	28	24	18	13	6	2 28	
		38	37	36	33	29	24	19	13	7	2 32	

TABLE 59

AMPLITUDES																
Lat.	DECLINATION															
	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°	15°
0	0	1'0	2'0	3'0	4'0	5'0	6'0	7'0	8'0	9'0	10'0	11'0	12'0	13'0	14'0	15'0
10	0	1'0	2'0	3'0	4'1	5'1	6'1	7'0	8'1	9'1	10'1	11'2	12'2	13'2	14'2	15'2
15	0	1'0	2'1	3'1	4'2	5'2	6'2	7'2	8'3	9'3	10'4	11'4	12'5	13'5	14'5	15'6
20	0	1'1	2'1	3'2	4'3	5'3	6'4	7'5	8'5	9'6	10'6	11'7	12'8	13'8	14'9	15'0
25	0	1'1	2'2	3'3	4'4	5'5	6'6	7'7	8'8	9'9	11'1	12'4	13'3	14'4	15'5	16'6
30	0	1'2	2'3	3'4	4'6	5'8	6'9	8'1	9'3	10'3	11'6	12'7	13'9	15'0	16'2	17'4
32	0	1'2	2'4	3'5	4'7	5'9	7'1	8'3	9'5	10'6	11'8	13'0	14'2	15'4	16'6	17'8
34	0	1'2	2'4	3'6	4'8	6'0	7'2	8'4	9'7	10'8	12'1	13'3	14'5	15'7	17'0	18'2
35	0	1'2	2'4	3'7	4'9	6'1	7'3	8'5	9'8	11'0	12'2	13'5	14'7	15'9	17'2	18'4
36	0	1'2	2'5	3'7	4'9	6'2	7'4	8'7	9'9	11'1	12'4	13'6	14'9	16'1	17'4	18'7
37	0	1'2	2'5	3'7	5'0	6'3	7'5	8'8	10'0	11'3	12'6	13'8	15'1	16'4	17'6	18'9
38	0	1'3	2'5	3'8	5'1	6'3	7'6	8'9	10'2	11'4	12'7	14'0	15'3	16'6	17'9	19'2
39	0	1'3	2'6	3'8	5'1	6'4	7'7	9'0	10'3	11'6	12'9	14'2	15'5	16'8	18'1	19'4
40	0	1'3	2'6	3'9	5'2	6'5	7'8	9'1	10'5	11'8	13'1	14'4	15'7	17'1	18'4	19'7
41	0	1'3	2'6	4'0	5'3	6'6	8'0	9'3	10'6	12'0	13'3	14'6	16'0	17'3	18'7	20'0
42	0	1'3	2'7	4'0	5'4	6'7	8'1	9'4	10'8	12'1	13'5	14'8	16'2	17'6	19'0	20'4
43	0	1'4	2'7	4'1	5'5	6'8	8'2	9'6	11'0	12'3	13'7	15'1	16'5	17'9	19'3	20'7
44	0	1'4	2'8	4'2	5'6	7'0	8'3	9'7	11'1	12'6	14'0	15'4	16'8	18'2	19'6	21'1
45	0	1'4	2'8	4'2	5'7	7'1	8'5	9'9	11'3	12'8	14'2	15'6	17'1	18'5	20'0	21'5
46	0	1'4	2'9	4'3	5'8	7'2	8'6	10'1	11'5	13'0	14'5	15'9	17'4	18'9	20'4	21'9
47	0	1'4	2'9	4'4	5'8	7'3	8'8	10'3	11'8	13'3	14'7	16'2	17'7	19'3	20'8	22'3
48	0	1'5	3'0	4'5	6'0	7'5	9'0	10'5	12'0	13'5	15'0	16'6	18'1	19'5	21'2	22'7
49	0	1'5	3'0	4'6	6'1	7'6	9'2	10'7	12'2	13'8	15'3	16'9	18'5	20'0	21'6	23'2
50	0	1'5	3'1	4'7	6'2	7'8	9'3	10'9	12'5	14'1	15'7	17'3	18'9	20'5	22'1	23'7
51	0	1'6	3'2	4'8	6'4	8'0	9'6	11'2	12'8	14'4	16'0	17'6	19'3	20'9	22'6	24'3
52	0	1'6	3'3	4'9	6'5	8'1	9'7	11'4	13'1	14'7	16'4	18'0	19'7	21'4	23'1	24'9
53	0	1'6	3'3	5'0	6'7	8'3	10'0	11'7	13'4	15'1	16'8	18'5	20'2	21'9	23'7	25'5
54	0	1'7	3'4	5'1	6'8	8'5	10'2	12'0	13'7	15'4	17'2	18'9	20'7	22'5	24'3	26'1
55	0	1'7	3'5	5'2	7'0	8'7	10'5	12'3	14'0	15'8	17'6	19'4	21'2	23'1	24'9	26'8
56	0	1'8	3'6	5'4	7'2	9'0	10'7	12'6	14'4	16'2	18'1	19'9	21'8	23'7	25'6	27'6
57	0	1'8	3'7	5'5	7'4	9'2	11'1	12'9	14'8	16'7	18'3	20'5	22'4	24'4	26'4	28'4
58	0	1'9	3'8	5'7	7'6	9'5	11'4	13'3	15'2	17'2	19'1	21'1	23'1	25'1	27'2	29'2
59	0	1'9	3'8	5'8	7'8	9'7	11'7	13'7	15'7	17'7	19'7	21'7	23'8	25'9	28'0	30'2
60	0	2'0	4'0	6'0	8'0	10'0	12'1	14'1	16'2	18'2	20'3	22'4	24'6	26'7	28'9	31'2
61	0	2'1	4'1	6'2	8'3	10'3	12'5	14'6	16'7	18'8	21'0	23'1	25'4	27'6	29'9	32'2
62	0	2'1	4'3	6'4	8'5	10'7	12'9	15'1	17'3	19'4	21'9	23'9	26'3	28'5	31'0	33'4
63	0	2'2	4'5	6'7	8'8	11'1	13'4	15'6	17'9	20'1	22'5	24'8	27'3	29'6	32'2	34'7
64	0	2'3	4'6	6'9	9'1	11'5	13'9	16'2	18'5	20'9	23'3	25'7	28'3	30'9	33'5	36'2
65	0	2'4	4'8	7'1	9'5	11'9	14'4	16'8	19'3	21'7	24'2	26'8	29'5	32'5	34'9	37'8

TABLE 59 A

CORRECTION OF THE AMPLITUDE OBSERVED ON THE HORIZON, FOR THE EFFECT OF REFRACTION. (Height of the Eye, 16 feet.)								
Lat.	DECLINATION							
	0°	10°	15°	18°	20°	22°	25°	24°
0	0°	0°	0°	0°	0°	0°	0°	0°
10	0	0'1	0'1	0'1	0'1	0'1	0'1	0'1
20	0'2	0'2	0'2	0'3	0'3	0'3	0'3	0'3
30	0'3	0'3	0'3	0'3	0'4	0'4	0'5	0'5
40	0'5	0'5	0'7	0'7	0'7	0'8	0'8	0'8
50	0'7	0'8	0'9	0'9	0'9	0'9	1'0	1'0
55	0'9	0'9	1'1	1'2	1'3	1'3	1'4	1'4
60	1'1	1'1	1'3	1'4	1'5	1'7	1'8	1'9
65	1'3	1'4	1'9	2'3	2'5			

TABLE 59

697

AMPLITUDES														
Lat.	DECLINATION													
	16°	16½°	17°	17½°	18°	18½°	19°	19½°	20°	20½°	21°	21½°	22°	22½°
0	16°0	16°5	17°0	17°5	18°0	18°5	19°0	19°5	20°0	20°5	21°0	21°5	22°0	22°5
10	16°2	16°7	17°3	17°8	18°3	18°8	19°3	19°9	20°3	20°8	21°3	21°8	22°3	22°9
15	16°6	17°1	17°7	18°1	18°7	19°2	19°7	20°2	20°8	21°3	21°8	22°3	22°8	23°3
20	17°1	17°6	18°1	18°7	19°2	19°7	20°3	20°8	21°3	21°9	22°4	22°9	23°5	24°0
25	17°7	18°3	18°8	19°4	19°9	20°5	21°0	21°6	22°1	22°7	23°3	23°8	24°4	24°9
30	18°6	19°1	19°7	20°3	20°9	21°5	22°1	22°7	23°3	23°8	24°4	25°0	25°6	26°2
35	19°0	19°6	20°2	20°8	21°4	22°0	22°6	23°2	23°8	24°4	25°0	25°6	26°2	26°8
40	19°4	20°0	20°6	21°3	21°9	22°5	23°1	23°7	24°4	25°0	25°6	26°2	26°8	27°4
45	19°6	20°3	20°9	21°5	22°2	22°8	23°4	24°0	24°7	25°3	25°9	26°6	27°2	27°8
50	19°9	20°5	21°2	21°8	22°4	23°1	23°7	24°4	25°0	25°6	26°3	26°9	27°6	28°2
55	20°2	20°8	21°5	22°1	22°8	23°4	24°0	24°7	25°3	26°0	26°7	27°3	28°0	28°6
60	20°5	21°1	21°8	22°4	23°1	23°7	24°4	25°1	25°7	26°4	27°0	27°7	28°4	29°0
65	20°8	21°4	22°1	22°8	23°4	24°1	24°8	25°4	26°1	26°8	27°5	28°1	28°8	29°5
70	21°1	21°8	22°4	23°1	23°8	24°5	25°1	25°8	26°5	27°2	27°9	28°6	29°3	30°0
75	21°4	22°1	22°8	23°5	24°2	24°8	25°5	26°2	26°9	27°6	28°3	29°0	29°8	30°5
80	21°8	22°5	23°2	23°8	24°6	25°3	26°0	26°7	27°4	28°1	28°8	29°5	30°3	31°0
85	22°1	22°8	23°6	24°3	25°0	25°7	26°4	27°1	27°8	28°6	29°3	30°1	30°8	31°5
90	22°5	23°2	24°0	24°7	25°6	26°2	26°9	27°6	28°4	29°1	29°8	30°6	31°4	32°1
95	22°9	23°7	24°4	25°2	25°9	26°7	27°4	28°2	28°9	29°7	30°4	31°2	32°0	32°8
100	23°4	24°1	24°8	25°6	26°4	27°2	27°9	28°7	29°5	30°3	31°0	31°8	32°6	33°4
105	23°8	24°6	25°4	26°2	26°9	27°7	28°5	29°3	30°1	30°9	31°7	32°5	33°3	34°1
110	24°3	25°1	25°9	26°7	27°5	28°3	29°1	29°9	30°7	31°6	32°4	33°2	34°0	34°8
115	24°8	25°6	26°5	27°3	28°1	28°9	29°7	30°6	31°4	32°3	33°1	33°9	34°8	35°7
120	25°4	26°2	27°0	27°8	28°7	29°6	30°4	31°3	32°1	33°0	33°9	34°8	35°6	36°5
125	26°0	26°8	27°7	28°5	29°4	30°3	31°1	32°0	32°9	33°8	34°7	35°6	36°5	37°5
130	26°6	27°5	28°3	29°2	30°1	31°0	31°9	32°8	33°7	34°7	35°6	36°5	37°5	38°4
135	27°3	28°2	29°1	30°0	30°9	31°8	32°7	33°7	34°6	35°6	36°5	37°5	38°5	39°5
140	28°0	28°9	29°8	30°8	31°7	32°7	33°6	34°6	35°6	36°6	37°6	38°6	39°6	40°6
145	28°7	29°7	30°6	31°6	32°6	33°6	34°6	35°6	36°6	37°6	38°7	39°7	40°8	41°8
150	29°5	30°5	31°5	32°5	33°5	34°6	35°6	36°6	37°7	38°8	39°8	40°9	42°1	43°2
155	30°4	31°4	32°5	33°5	34°5	35°6	36°7	37°8	38°9	40°0	41°1	42°3	43°4	44°6
160	31°3	32°4	33°5	34°6	35°7	36°8	37°9	39°0	40°2	41°7	42°5	43°8	45°0	46°2
165	32°3	33°5	34°6	35°7	36°8	38°0	39°2	40°4	41°6	42°8	44°1	45°4	46°7	48°0
170	33°4	34°6	35°8	37°0	38°2	39°4	40°6	41°9	43°2	44°5	45°8	47°1	48°5	49°9
175	34°6	35°8	37°1	38°3	39°6	40°8	42°2	43°5	44°8	46°2	47°7	49°1	50°6	52°1
180	35°9	37°2	38°5	39°8	41°2	42°5	43°9	45°3	46°8	48°2	49°8	51°3	52°9	54°6
185	37°4	38°7	40°1	41°5	42°9	44°3	45°8	47°3	48°8	50°5	52°1	53°8	55°6	57°4
190	39°0	40°4	41°8	43°3	44°8	46°4	48°0	49°6	51°3	53°0	54°8	56°7	58°7	60°8
195	40°7	42°2	43°8	45°4	47°0	48°7	50°4	52°2	54°0	56°0	58°0	60°1	62°4	64°9

TABLE 59 A

CORRECTION OF THE AMPLITUDE OBSERVED ON THE HORIZON, FOR THE EFFECT OF REFRACTION. (Height of the Eye, 16 feet.)								
Lat.	DECLINATION							
	0°	10°	15°	18°	20°	22°	23°	24°
0	0°0	0°0	0°0	0°0	0°0	0°0	0°0	0°0
10	0°1	0°1	0°1	0°1	0°1	0°1	0°1	0°1
20	0°2	0°2	0°2	0°3	0°3	0°3	0°3	0°3
30	0°3	0°3	0°3	0°3	0°4	0°4	0°5	0°5
40	0°5	0°5	0°7	0°7	0°7	0°8	0°8	0°8
50	0°7	0°8	0°9	0°9	0°9	0°9	1°0	1°0
55	0°9	0°9	1°1	1°2	1°3	1°3	1°4	1°4
60	1°1	1°1	1°3	1°4	1°5	1°7	1°9	1°9
65	1°3	1°4	1°9	2°3	2°5			

DECLINATION OF THE SUN, FOR THE YEAR 1901,
At Apparent Noon at Greenwich.

Day	Jan.	Feb.	Mar.	April	May	June	July	Aug	Sept.	Oct.	Nov.	Dec.
1	23° 28'S	17° 12'S	7° 44'S	4° 23'N	14° 57'N	22° 0'N	23° 9'N	18° 9'N	8° 27'N	3° 18'S	14° 18'S	21° 45'S
2	22 57	16 55	7 21	4 46	15 15	22 8	23 5	17 54	8 5	3 24	14 37	21 54
3	22 52	16 38	6 58	5 9	15 33	22 16	23 1	17 38	7 43	3 47	14 56	22 3
4	22 46	16 20	6 35	5 32	15 51	22 23	22 56	17 22	7 21	4 11	15 15	22 12
5	22 40	16 2	6 12	5 55	16 8	22 30	22 50	17 6	6 59	4 34	15 33	22 20
6	22 33	15 44	5 49	6 18	16 25	22 37	22 45	16 50	6 37	4 57	15 52	22 27
7	22 26	15 25	5 26	6 40	16 42	22 43	22 39	16 34	6 15	5 20	16 10	22 34
8	22 18	15 7	5 2	7 3	16 58	22 49	22 32	16 17	5 52	5 43	16 27	22 41
9	22 10	14 48	4 39	7 25	17 15	22 54	22 26	16 0	5 29	6 6	16 45	22 47
10	22 1	14 28	4 15	7 48	17 31	22 59	22 18	15 42	5 7	6 29	17 2	22 53
11	21 52	14 9	3 52	8 10	17 46	23 4	22 11	15 25	4 44	6 51	17 19	22 59
12	21 43	13 49	3 29	8 32	18 2	23 8	22 3	15 7	4 21	7 14	17 35	23 3
13	21 33	13 29	3 5	8 54	18 17	23 12	21 54	14 49	3 58	7 37	17 52	23 8
14	21 23	13 9	2 41	9 15	18 31	23 15	21 46	14 31	3 35	7 59	18 8	23 12
15	21 12	12 48	2 18	9 37	18 46	23 18	21 37	14 12	3 12	8 21	18 23	23 15
16	21 1	12 28	1 54	9 58	19 0	23 20	21 27	13 53	2 49	8 44	18 38	23 18
17	20 49	12 7	1 30	10 20	19 14	23 23	21 17	13 34	2 26	9 6	18 53	23 21
18	20 37	11 46	1 6	10 41	19 27	23 24	21 7	13 15	2 3	9 28	19 8	23 23
19	20 25	11 25	0 43	11 2	19 41	23 26	20 56	12 56	1 39	9 50	19 23	23 25
20	20 12	11 3	0 19	11 22	19 53	23 26	20 46	12 36	1 16	10 11	19 36	23 26
21	19 59	10 42	0 5N	11 43	20 6	23 27	20 34	12 16	0 53	10 33	19 50	23 27
22	19 46	10 20	0 28	12 3	20 18	23 27	20 23	11 57	0 29	10 54	20 3	23 27
23	19 32	9 58	0 52	12 23	20 30	23 27	20 11	11 36	0 6N	11 15	20 16	23 27
24	19 18	9 36	1 16	12 43	20 41	23 26	19 58	11 16	0 17S	11 36	20 28	23 26
25	19 3	9 14	1 39	13 3	20 52	23 25	19 46	10 55	0 41	11 57	20 41	23 25
26	18 49	8 52	2 3	13 23	21 3	23 23	19 33	10 35	0 14	12 18	20 52	23 23
27	18 33	8 29	2 26	13 42	21 14	23 21	19 20	10 14	1 27	12 39	21 4	23 21
28	18 18	8 7	2 50	14 1	21 24	23 19	19 6	9 53	1 51	12 59	21 15	23 19
29	18 2		3 13	14 20	21 33	23 16	18 52	9 32	2 14	13 19	21 25	23 16
30	17 46		3 37	14 39	21 43	23 13	18 38	9 10	2 38	13 39	21 35	23 12
31	17 29		4 0		21 51		18 23	8 49		13 59		23 8

DECLINATION OF THE SUN, FOR 1902.

1	23° 4'S	17° 17'S	7° 50'S	4° 17'N	14° 52'N	21° 58'N	23° 10'N	18° 12'N	8° 32'N	2° 55'S	14° 13'S	21° 43'S
2	22 59	17 0	7 27	4 40	15 11	22 6	23 6	17 57	8 10	3 19	14 33	21 52
3	22 53	16 42	7 4	5 4	15 29	22 14	23 2	17 42	7 49	3 42	14 52	22 1
4	22 48	16 25	6 41	5 27	15 46	22 21	22 57	17 26	7 27	4 5	15 10	22 10
5	22 41	16 7	6 18	5 49	16 4	22 28	22 52	17 10	7 4	4 28	15 29	22 18
6	22 35	15 48	5 55	6 12	16 21	22 35	22 46	16 54	6 42	4 52	15 47	22 25
7	22 27	15 30	5 31	6 35	16 38	22 41	22 40	16 38	6 20	5 15	16 5	22 33
8	22 20	15 11	5 8	6 57	16 54	22 47	22 34	16 21	5 57	5 38	16 23	22 39
9	22 12	14 52	4 45	7 20	17 11	22 53	22 27	16 4	5 35	6 0	16 41	22 46
10	22 3	14 33	4 21	7 42	17 27	22 58	22 20	15 47	5 12	6 23	16 58	22 52
11	21 54	14 14	3 58	8 4	17 42	23 3	22 12	15 29	4 49	6 46	17 15	22 57
12	21 45	13 54	3 34	8 26	17 58	23 7	22 5	15 11	4 27	7 9	17 31	23 2
13	21 35	13 34	3 11	8 48	18 13	23 11	21 56	14 53	4 4	7 31	17 48	23 7
14	21 25	13 14	2 47	9 10	18 28	23 14	21 48	14 35	3 41	7 54	18 4	23 11
15	21 14	12 53	2 23	9 32	18 42	23 17	21 39	14 17	3 18	8 16	18 19	23 15
16	21 3	12 33	2 0	9 53	18 57	23 20	21 29	13 58	2 55	8 38	18 35	23 18
17	20 52	12 12	1 36	10 15	19 11	23 22	21 20	13 39	2 31	9 0	18 50	23 20
18	20 40	11 51	1 12	10 36	19 24	23 24	21 9	13 20	2 8	9 22	19 5	23 23
19	20 28	11 30	0 49	10 57	19 37	23 25	20 59	13 1	1 45	9 44	19 19	23 24
20	20 15	11 9	0 25	11 17	19 50	23 26	20 48	12 41	1 22	10 6	19 33	23 26
21	20 3	10 47	0 18	11 38	20 3	23 27	20 37	12 21	0 58	10 28	19 47	23 27
22	19 49	10 25	0 23N	11 58	20 15	23 27	20 25	12 1	0 35	10 49	20 0	23 27
23	19 35	10 4	0 46	12 19	20 27	23 27	20 14	11 41	0 12N	11 10	20 13	23 27
24	19 21	9 42	1 10	12 39	20 39	23 26	20 1	11 21	0 12S	11 31	20 25	23 26
25	19 7	9 19	1 33	12 58	20 50	23 25	19 49	11 0	0 35	11 52	20 38	23 25
26	18 52	8 57	1 57	13 18	21 1	23 23	19 36	10 40	0 58	12 13	20 49	23 24
27	18 37	8 35	2 21	13 37	21 11	23 22	19 23	10 19	1 22	12 34	21 1	23 22
28	18 22	8 12	2 44	13 56	21 21	23 19	19 9	9 58	1 45	12 54	21 12	23 19
29	18 6		3 7	14 15	21 31	23 17	18 55	9 37	2 9	13 14	21 23	23 16
30	17 50		3 31	14 34	21 40	23 13	18 41	9 15	2 32	13 34	21 33	23 13
31	17 33		3 54		21 49		18 27	8 54		13 54		23 9

TABLE 60

DECLINATION OF THE SUN, FOR THE YEAR 1903.

At Apparent Noon at Greenwich.

Day	Jan.	Feb.	Mar.	April	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.
1	23 58.	17 218.	7 55S.	4 12N.	14 48N.	21 56N.	23 11N.	18 16N.	8 37N.	2 50S.	14 9S.	21 40S.
2	23 0	17 4	7 33	4 35	15 6	22 4	23 7	18 1	8 16	3 13	14 28	21 50
3	22 55	16 47	7 10	4 58	15 24	22 12	23 3	17 46	7 54	3 36	14 47	21 59
4	22 49	16 29	6 47	5 21	15 42	22 20	22 58	17 30	7 32	4 0	15 6	22 8
5	22 43	16 11	6 24	5 44	16 0	22 27	22 53	17 14	7 10	4 23	15 25	22 16
6	22 36	15 53	6 0	6 7	16 17	22 34	22 48	16 58	6 48	4 46	15 43	22 24
7	22 29	15 35	5 37	6 29	16 34	22 40	22 42	16 42	6 25	5 9	16 1	22 31
8	22 22	15 16	5 14	6 52	16 50	22 46	22 35	16 25	6 3	5 32	16 19	22 38
9	22 14	14 57	4 51	7 14	17 7	22 52	22 29	16 8	5 40	5 55	16 37	22 44
10	22 6	14 38	4 27	7 37	17 23	22 57	22 22	15 51	5 18	6 18	16 54	22 50
11	21 57	14 19	4 4	7 59	17 39	23 2	22 14	15 33	4 55	6 41	17 11	22 56
12	21 47	13 59	3 40	8 21	17 54	23 6	22 6	15 16	4 32	7 3	17 27	23 1
13	21 38	13 39	3 17	8 43	18 9	23 10	21 58	14 58	4 9	7 26	17 44	23 6
14	21 28	13 19	2 53	9 5	18 24	23 13	21 50	14 40	3 46	7 48	18 0	23 10
15	21 17	12 59	2 29	9 26	18 39	23 16	21 41	14 21	3 23	8 11	18 16	23 14
16	21 6	12 38	2 6	9 48	18 53	23 19	21 32	14 3	3 0	8 33	18 31	23 17
17	20 55	12 17	1 42	10 9	19 7	23 21	21 22	13 44	2 37	8 55	18 46	23 20
18	20 43	11 56	1 18	10 30	19 21	23 23	21 12	13 25	2 14	9 17	19 1	23 22
19	20 31	11 35	0 55	10 51	19 34	23 25	21 2	13 5	1 51	9 39	19 16	23 24
20	20 19	11 14	0 31	11 12	19 47	23 26	20 51	12 46	1 27	10 1	19 30	23 26
21	20 6	10 53	0 7S.	11 33	20 0	23 27	20 40	12 26	1 4	10 23	19 43	23 26
22	19 53	10 31	0 17N.	11 53	20 12	23 27	20 28	12 6	0 41	10 44	19 57	23 27
23	19 39	10 9	0 40	12 14	20 24	23 27	20 16	11 46	0 17N.	11 5	20 10	23 27
24	19 25	9 47	1 4	12 34	20 36	23 26	20 4	11 26	0 6S.	11 26	20 23	23 26
25	19 11	9 25	1 28	12 54	20 47	23 25	19 52	11 5	0 30	11 47	20 35	23 25
26	18 56	9 3	1 51	13 13	20 58	23 24	19 39	10 45	0 53	12 8	20 47	23 24
27	18 41	8 40	2 15	13 33	21 9	23 22	19 26	10 24	1 16	12 29	20 58	23 22
28	18 26	8 18S.	2 38	13 52	21 19	23 20	19 13	10 3	1 40	12 49	21 9	23 20
29	18 10		3 2	14 11	21 29	23 17	18 59	9 42	2 3	13 9	21 20	23 17
30	17 54		3 25	14 30	21 38	23 14N.	18 45	9 20	2 26S.	13 29	21 30S.	23 14
31	17 38S.		3 48N.		N. 21 47N.		18 30N.	8 59N.		13 49S.		23 10S.

DECLINATION OF THE SUN, FOR 1904.

1	23 68.	17 25S.	7 38S.	4 29N.	15 2N.	22 2N.	23 8N.	18 5N.	8 21N.	3 7S.	14 23S.	21 48S.
2	23 1	17 8	7 15	4 52	15 20	22 10	23 4	17 49	7 59	3 31	14 42	21 57
3	22 56	16 51	6 52	5 15	15 38	22 18	22 59	17 34	7 37	3 54	15 1	22 5
4	22 50	16 33	6 29	5 38	15 55	22 25	22 54	17 18	7 15	4 17	15 20	22 14
5	22 44	16 16	6 6	6 1	16 13	22 32	22 49	17 2	6 53	4 40	15 39	22 22
6	22 38	15 58	5 43	6 24	16 30	22 38	22 43	16 46	6 31	5 3	15 57	22 29
7	22 31	15 39	5 20	6 46	16 46	22 44	22 37	16 29	6 8	5 26	16 15	22 36
8	22 24	15 21	4 56	7 9	17 3	22 50	22 30	16 12	5 46	5 49	16 34	22 43
9	22 16	15 2	4 33	7 31	17 19	22 55	22 23	15 55	5 23	6 12	16 50	22 49
10	22 8	14 43	4 9	7 54	17 35	23 0	22 16	15 38	5 1	6 35	17 7	22 55
11	21 59	14 23	3 46	8 16	17 50	23 5	22 8	15 20	4 38	6 58	17 23	23 0
12	21 50	14 4	3 22	8 38	18 6	23 9	22 0	15 2	4 15	7 20	17 40	23 5
13	21 40	13 44	2 59	9 0	18 21	23 12	21 51	14 44	3 52	7 43	17 56	23 9
14	21 30	13 24	2 35	9 21	18 35	23 16	21 43	14 26	3 29	8 5	18 12	23 13
15	21 20	13 4	2 11	9 43	18 50	23 19	21 34	14 7	3 6	8 28	18 27	23 16
16	21 9	12 43	1 48	10 4	19 4	23 21	21 24	13 48	2 43	8 50	18 43	23 19
17	20 58	12 22	1 24	10 25	19 18	23 23	21 14	13 29	2 20	9 12	18 58	23 22
18	20 46	12 1	1 0	10 46	19 31	23 25	21 4	13 10	1 56	9 34	19 12	23 24
19	20 34	11 40	0 37	11 7	19 44	23 26	20 53	12 51	1 33	9 56	19 26	23 25
20	20 22	11 19	0 13S.	11 28	19 57	23 27	20 42	12 31	1 10	10 17	19 40	23 26
21	20 9	10 58	0 11N.	11 48	20 9	23 27	20 31	12 11	0 46	10 39	19 54	23 27
22	19 56	10 36	0 35	12 9	20 21	23 27	20 19	11 51	0 23N.	11 0	20 7	23 27
23	19 42	10 14	0 58	12 29	20 33	23 26	20 7	11 31	0 0	11 21	20 19	23 27
24	19 28	9 52	1 22	12 49	20 44	23 25	19 55	11 10	0 24S.	11 42	20 32	23 26
25	19 14	9 30	1 45	13 8	20 55	23 24	19 42	10 50	0 47	12 3	20 44	23 25
26	19 0	9 8	2 9	13 28	21 6	23 22	19 29	10 29	1 10	12 24	20 55	23 23
27	18 45	8 46	2 33	13 47	21 16	23 20	19 16	10 8	1 34	12 44	21 6	23 20
28	18 29	8 23	2 56	14 6	21 26	23 18	19 2	9 47	1 57	13 4	21 17	23 18
29	18 14	8 0S.	3 19	14 25	21 36	23 15	18 48	9 26	2 21	13 24	21 28	23 15
30	17 58		3 43	14 44N.	21 45	23 12N.	18 34	9 4	2 44S.	13 44	21 38S.	23 11
31	17 42S.		4 6N.		21 54N.		18 19N.	8 43N.		14 4S.		23 7S.

CORRECTION OF THE SUN'S DECLINATION, IN TABLE 60, FOR THE YEARS FOLLOWING 1901, 1902, 1903, 1904.													
Given Years.	Following Years.						Given Years.	Following Years.					
1901	1905	1909	1913	1917	1921	1925	1901	1905	1909	1913	1917	1921	1925
1902	1906	1910	1914	1918	1922	1926	1902	1906	1910	1914	1918	1922	1926
1903	1907	1911	1915	1919	1923	1927	1903	1907	1911	1915	1919	1923	1927
1904	1908	1912	1916	1920	1924	1928	1904	1908	1912	1916	1920	1924	1928
Jan. 1	sub. 0° 1'	sub. 0° 3'	sub. 0° 4'	sub. 0° 6'	sub. 0° 7'	sub. 0° 9'	June 30	sub. 0° 1'	sub. 0° 3'	sub. 0° 4'	sub. 0° 6'	sub. 0° 7'	sub. 0° 8'
10	0° 2'	0° 5'	0° 8'	1° 0'	1° 3'	1° 6'	July 10	0° 2'	0° 5'	0° 8'	1° 0'	1° 3'	1° 6'
20	0° 4'	0° 7'	1° 1'	1° 4'	1° 8'	2° 2'	20	0° 4'	0° 7'	1° 1'	1° 4'	1° 8'	2° 2'
30	0° 5'	1° 0'	1° 5'	2° 0'	2° 5'	3° 0'	30	0° 5'	1° 0'	1° 5'	2° 0'	2° 5'	3° 0'
Feb. 10	0° 6'	1° 1'	1° 6'	2° 2'	2° 8'	3° 4'	Aug. 10	0° 5'	1° 1'	1° 7'	2° 3'	2° 8'	3° 4'
20	0° 6'	1° 2'	1° 9'	2° 5'	3° 1'	3° 7'	20	0° 6'	1° 3'	1° 9'	2° 5'	3° 2'	3° 9'
28	0° 7'	1° 3'	2° 0'	2° 6'	3° 3'	4° 0'	30	0° 7'	1° 4'	2° 0'	2° 7'	3° 4'	4° 1'
Mar. 10	0° 7'	1° 4'	2° 1'	2° 8'	3° 5'	4° 2'	Sept. 10	0° 7'	1° 4'	2° 1'	2° 8'	3° 5'	4° 2'
20	0° 7'	1° 4'	2° 1'	2° 8'	3° 6'	4° 3'	20	0° 7'	1° 4'	2° 1'	2° 9'	3° 6'	4° 3'
	add	add	add	add	add	add		add	add	add	add	add	add
30	0° 7'	1° 4'	2° 1'	2° 8'	3° 5'	4° 2'	30	0° 7'	1° 4'	2° 1'	2° 8'	3° 5'	4° 2'
Apr. 10	0° 7'	1° 4'	2° 1'	2° 7'	3° 4'	4° 1'	Oct. 10	0° 7'	1° 4'	2° 0'	2° 7'	3° 4'	4° 1'
20	0° 6'	1° 3'	1° 9'	2° 5'	3° 2'	3° 9'	20	0° 6'	1° 3'	1° 9'	2° 5'	3° 2'	3° 9'
30	0° 6'	1° 1'	1° 7'	2° 3'	2° 8'	3° 4'	30	0° 5'	1° 1'	1° 6'	2° 2'	2° 8'	3° 4'
May 10	0° 5'	0° 9'	1° 5'	2° 0'	2° 5'	3° 0'	Nov. 10	0° 5'	1° 0'	1° 4'	1° 9'	2° 4'	2° 8'
20	0° 4'	0° 8'	1° 2'	1° 6'	1° 9'	2° 3'	20	0° 4'	0° 8'	1° 2'	1° 5'	2° 0'	2° 5'
30	0° 3'	0° 5'	0° 8'	1° 0'	1° 4'	1° 7'	30	0° 2'	0° 5'	0° 7'	1° 0'	1° 3'	1° 6'
June 10	0° 2'	0° 3'	0° 4'	0° 5'	0° 7'	0° 9'	Dec. 10	0° 2'	0° 3'	0° 4'	0° 6'	0° 7'	0° 8'
20	0° 0'	0° 0'	0° 1'	0° 1'	0° 1'	0° 1'	20	0° 0'	0° 0'	0° 1'	0° 1'	0° 2'	0° 3'
	sub.	sub.	sub.	sub.	sub.	sub.		sub.	sub.	sub.	sub.	sub.	sub.
30	0° 1'	0° 3'	0° 4'	0° 6'	0° 7'	0° 8'	30	0° 1'	0° 3'	0° 4'	0° 6'	0° 7'	0° 9'

TABLE 61

701

SIDEREAL TIME, FOR THE YEAR 1901,
At Mean Noon at Greenwich.

Day	Jan.	Feb.	Mar.	April	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.
	h m	h m	h m	h m	h m	h m	h m	h m	h m	h m	h m	h m
1	18 41.8	20 44	22 34.4	0 36.6	2 34.9	4 37.1	6 35.4	8 37.6	10 39.8	12 38.1	14 40.3	16 38.6
2	18 45.7	20 47.9	22 38.3	0 40.5	2 38.8	4 41	6 39.3	8 41.5	10 43.8	12 42	14 44.3	16 42.5
3	18 49.7	20 51.9	22 42.3	0 44.5	2 42.8	4 45	6 43.3	8 45.5	10 47.7	12 46	14 48.2	16 46.5
4	18 53.6	20 55.8	22 46.2	0 48.4	2 46.7	4 48.9	6 47.2	8 49.4	10 51.6	12 49.9	14 52.1	16 50.4
5	18 57.5	20 59.8	22 50.2	0 52.4	2 50.6	4 52.9	6 51.1	8 53.4	10 55.6	12 53.9	14 56.1	16 54.4
6	19 1.5	21 3.7	22 54.1	0 56.3	2 54.6	4 56.8	6 55.1	8 57.3	10 59.5	12 57.8	15 0	16 58.3
7	19 5.4	21 7.6	22 58	1 0.3	2 58.5	5 0.8	6 59	9 1.3	11 3.5	13 1.7	15 4	17 2.2
8	19 9.4	21 11.6	23 2	1 4.2	3 2.5	5 4.7	7 3	9 5.2	11 7.4	13 5.7	15 7.9	17 6.2
9	19 13.3	21 15.5	23 5.9	1 8.1	3 6.4	5 8.6	7 6.9	9 9.1	11 11.4	13 9.6	15 11.9	17 10.1
10	19 17.3	21 19.5	23 9.9	1 12.1	3 10.4	5 12.6	7 10.9	9 13.1	11 15.3	13 13.6	15 15.8	17 14.1
11	19 21.2	21 23.4	23 13.8	1 16	3 14.3	5 16.5	7 14.8	9 17	11 19.2	13 17.5	15 19.7	17 18
12	19 25.1	21 27.4	23 17.7	1 20	3 18.2	5 20.5	7 18.7	9 21	11 23.2	13 21.5	15 23.7	17 22
13	19 29.1	21 31.3	23 21.7	1 23.9	3 22.2	5 24.4	7 22.7	9 24.9	11 27.1	13 25.4	15 27.6	17 25.9
14	19 33	21 35.2	23 25.6	1 27.9	3 26.1	5 28.3	7 26.6	9 28.8	11 31.1	13 29.3	15 31.6	17 29.8
15	19 37	21 39.2	23 29.6	1 31.8	3 30.1	5 32.3	7 30.6	9 32.8	11 35	13 33.3	15 35.5	17 33.8
16	19 40.9	21 43.1	23 33.5	1 35.7	3 34	5 36.2	7 34.5	9 36.7	11 39	13 37.2	15 39.4	17 37.7
17	19 44.8	21 47.1	23 37.5	1 39.7	3 38	5 40.2	7 38.5	9 40.7	11 42.9	13 41.2	15 43.4	17 41.7
18	19 48.8	21 51	23 41.4	1 43.6	3 41.9	5 44.1	7 42.4	9 44.6	11 46.8	13 45.1	15 47.3	17 45.6
19	19 52.7	21 54	23 45.3	1 47.6	3 45.8	5 48.1	7 46.3	9 48.6	11 50.8	13 49.1	15 51.3	17 49.6
20	19 56.7	21 58.9	23 49.3	1 51.5	3 49.8	5 52	7 50.3	9 52.5	11 54.7	13 53	15 55.2	17 53.5
21	20 0.6	22 2.8	23 53.2	1 55.4	3 53.7	5 55.9	7 54.2	9 56.4	11 58.7	13 56.9	15 59.2	17 57.4
22	20 4.6	22 6.8	23 57.2	1 59.4	3 57.7	5 59.9	7 58.2	10 0.4	12 2.6	14 0.9	16 3.1	18 1.4
23	20 8.5	22 10.7	0 1.1	2 3.3	4 1.6	6 3.8	8 2.1	10 4.3	12 6.6	14 4.8	16 7	18 5.3
24	20 12.4	22 14.7	0 5.1	2 7.3	4 5.6	6 7.8	8 6.1	10 8.3	12 10.5	14 8.8	16 11	18 9.3
25	20 16.4	22 18.6	0 9	2 11.2	4 9.5	6 11.7	8 10	10 12.2	12 14.4	14 12.7	16 14.9	18 13.2
26	20 20.3	22 22.6	0 12.9	2 15.2	4 13.4	6 15.7	8 13.9	10 16.2	12 18.4	14 16.7	16 18.9	18 17.2
27	20 24.3	22 26.5	0 16.9	2 19.1	4 17.4	6 19.6	8 17.9	10 20.1	12 22.3	14 20.6	16 22.8	18 21.1
28	20 28.2	22 30.4	0 20.8	2 23	4 21.3	6 23.5	8 21.8	10 24	12 26.3	14 24.5	16 26.8	18 25
29	20 32.2		0 24.8	2 27	4 25.3	6 27.5	8 25.8	10 28	12 30.2	14 28.5	16 30.7	18 29
30	20 36.1		0 28.7	2 30.9	4 29.2	6 31.4	8 29.7	10 31.9	12 34.1	14 32.4	16 34.6	18 32.9
31	20 40		0 32.7		4 33.2		8 33.7	10 35.9		14 36.4		18 36.9

SIDEREAL TIME, FOR 1902.

1	18 40.8	20 43	22 33.4	0 35.6	2 33.9	4 36.1	6 34.4	8 36.6	10 38.9	12 37.1	14 39.3	16 37.6
2	18 44.8	20 47	22 37.4	0 39.6	2 37.9	4 40.1	6 38.4	8 40.6	10 42.8	12 41.1	14 43.3	16 41.6
3	18 48.7	20 50.9	22 41.3	0 43.5	2 41.8	4 44	6 42.3	8 44.5	10 46.7	12 45	14 47.2	16 45.5
4	18 52.6	20 54.9	22 45.2	0 47.5	2 45.7	4 48	6 46.2	8 48.5	10 50.7	12 49	14 51.2	16 49.5
5	18 56.6	20 58.8	22 49.2	0 51.4	2 49.7	4 51.9	6 50.2	8 52.4	10 54.6	12 52.9	14 55.1	16 53.4
6	19 0.5	21 2.7	22 53.1	0 55.4	2 53.6	4 55.8	6 54.1	8 56.3	10 58.6	12 56.8	14 59.1	16 57.3
7	19 4.5	21 6.7	22 57.1	0 59.3	2 57.6	4 59.8	6 58.1	9 0.3	11 2.5	13 0.8	15 3	17 1.3
8	19 8.4	21 10.6	23 1	1 3.2	3 1.5	5 3.7	7 2	9 4.2	11 6.5	13 4.7	15 6.9	17 5.2
9	19 12.3	21 14.6	23 5	1 7.2	3 5.5	5 7.7	7 6	9 8.2	11 10.4	13 8.7	15 10.9	17 9.2
10	19 16.3	21 18.5	23 8.9	1 11.1	3 9.4	5 11.6	7 9.9	9 12.1	11 14.3	13 12.6	15 14.8	17 13.1
11	19 20.2	21 22.5	23 12.8	1 15.1	3 13.3	5 15.6	7 13.8	9 16.1	11 18.3	13 16.6	15 18.8	17 17.1
12	19 24.2	21 26.4	23 16.8	1 19	3 17.3	5 19.5	7 17.8	9 20	11 22.2	13 20.5	15 22.7	17 21
13	19 28.1	21 30.3	23 20.7	1 23	3 21.2	5 23.4	7 21.7	9 23.9	11 26.2	13 24.4	15 26.7	17 24.9
14	19 32.1	21 34.3	23 24.7	1 26.9	3 25.2	5 27.4	7 25.7	9 27.9	11 30.1	13 28.4	15 30.6	17 28.9
15	19 36	21 38.2	23 28.6	1 30.8	3 29.1	5 31.3	7 29.6	9 31.8	11 34.1	13 32.3	15 34.5	17 32.8
16	19 39.9	21 42.2	23 32.6	1 34.8	3 33.1	5 35.3	7 33.6	9 35.8	11 38	13 36.3	15 38.5	17 36.8
17	19 43.9	21 46.1	23 36.5	1 38.7	3 37	5 39.2	7 37.5	9 39.7	11 41.9	13 40.2	15 42.4	17 40.7
18	19 47.8	21 50.1	23 40.4	1 42.7	3 40.9	5 43.2	7 41.4	9 43.7	11 45.9	13 44.2	15 46.4	17 44.7
19	19 51.8	21 54	23 44.4	1 46.6	3 44.9	5 47.1	7 45.4	9 47.6	11 49.8	13 48.1	15 50.3	17 48.6
20	19 55.7	21 57.9	23 48.3	1 50.5	3 48.8	5 51	7 49.3	9 51.5	11 53.8	13 52	15 54.3	17 52.5
21	19 59.7	22 1.9	23 52.3	1 54.5	3 52.8	5 55	7 53.3	9 55.5	11 57.7	13 56	15 58.2	17 56.5
22	20 3.6	22 5.8	23 56.2	1 58.4	3 56.7	5 58.9	7 57.2	9 59.4	12 1.6	13 59.9	16 2.1	18 0.4
23	20 7.5	22 9.8	0 0.2	2 2.4	4 0.7	6 2.9	8 1.2	10 3.4	12 5.6	14 3.9	16 6.1	18 4.4
24	20 11.5	22 13.7	0 4.1	2 6.3	4 4.6	6 6.8	8 5.1	10 7.3	12 9.5	14 7.8	16 10	18 8.3
25	20 15.4	22 17.7	0 8	2 10.3	4 8.5	6 10.8	8 9	10 11.3	12 13.5	14 11.8	16 14	18 12.3
26	20 19.4	22 21.6	0 12	2 14.2	4 12.5	6 14.7	8 13	10 15.2	12 17.4	14 15.7	16 17.9	18 16.2
27	20 23.3	22 25.5	0 15.9	2 18.1	4 16.4	6 18.6	8 16.9	10 19.1	12 21.4	14 19.6	16 21.9	18 20.1
28	20 27.3	22 29.5	0 19.9	2 22.1	4 20.4	6 22.6	8 20.9	10 23.1	12 25.3	14 23.6	16 25.8	18 24.1
29	20 31.2		0 23.8	2 26	4 24.3	6 26.5	8 24.8	10 27	12 29.2	14 27.5	16 29.7	18 28
30	20 35.1		0 27.7	2 30	4 28.3	6 30.5	8 28.8	10 31	12 33.2	14 31.5	16 33.7	18 32
31	20 39.1		0 31.7		4 32.2		8 32.7	10 34.9		14 35.4		18 35.9

SIDEREAL TIME, FOR THE YEAR 1905,

At Mean Noon at Greenwich.

Day	Jan.	Feb.	Mar.	April	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.
	h m	h m	h m	h m	h m	h m	h m	h m	h m	h m	h m	h m
1	18 39.8	20 42.1	22 32.5	0 34.7	2 33.0	4 35.2	6 33.5	8 35.7	10 37.9	12 36.2	14 38.4	16 36.7
2	18 43.8	20 46.0	22 36.4	0 38.6	2 36.9	4 39.1	6 37.4	8 39.6	10 41.8	12 40.1	14 42.3	16 40.6
3	18 47.7	20 50.0	22 40.3	0 42.6	2 40.8	4 43.1	6 41.3	8 43.6	10 45.8	12 44.1	14 46.3	16 44.6
4	18 51.7	20 53.9	22 44.3	0 46.5	2 44.8	4 47.0	6 45.3	8 47.5	10 49.7	12 48.0	14 50.2	16 48.5
5	18 55.6	20 57.8	22 48.2	0 50.4	2 48.7	4 50.9	6 49.2	8 51.4	10 53.7	12 51.9	14 54.2	16 52.4
6	18 59.6	21 1.8	22 52.2	0 54.4	2 52.7	4 54.9	6 53.2	8 55.4	10 57.6	12 55.9	14 58.1	16 56.4
7	19 3.5	21 5.7	22 56.1	0 58.3	2 56.6	4 58.8	6 57.1	8 59.3	11 1.5	12 59.8	15 2.1	17 0.3
8	19 7.4	21 9.7	23 0.1	1 2.3	3 0.6	5 2.8	7 1.1	9 3.3	11 5.5	13 3.8	15 6.0	17 4.3
9	19 11.4	21 13.6	23 4.0	1 6.2	3 4.5	5 6.7	7 5.0	9 7.2	11 9.4	13 7.7	15 9.9	17 8.2
10	19 15.3	21 17.6	23 7.9	1 10.2	3 8.4	5 10.7	7 8.9	9 11.2	11 13.4	13 11.7	15 13.9	17 12.2
11	19 19.3	21 21.5	23 11.9	1 14.1	3 12.4	5 14.6	7 12.9	9 15.1	11 17.3	13 15.6	15 17.8	17 16.1
12	19 23.2	21 25.4	23 15.8	1 18.0	3 16.3	5 18.5	7 16.8	9 19.0	11 21.3	13 19.5	15 21.8	17 20.0
13	19 27.2	21 29.4	23 19.8	1 22.0	3 20.3	5 22.5	7 20.8	9 23.0	11 25.2	13 23.5	15 25.7	17 24.0
14	19 31.1	21 33.3	23 23.7	1 25.9	3 24.2	5 26.4	7 24.7	9 26.9	11 29.1	13 27.4	15 29.6	17 27.9
15	19 35.0	21 37.3	23 27.7	1 29.9	3 28.2	5 30.4	7 28.7	9 30.9	11 33.1	13 31.4	15 33.6	17 31.9
16	19 39.0	21 41.2	23 31.6	1 33.8	3 32.1	5 34.3	7 32.6	9 34.8	11 37.0	13 35.3	15 37.5	17 35.8
17	19 42.9	21 45.2	23 35.5	1 37.8	3 36.0	5 38.3	7 36.5	9 38.8	11 41.0	13 39.3	15 41.5	17 39.7
18	19 46.9	21 49.1	23 39.5	1 41.7	3 40.0	5 42.2	7 40.5	9 42.7	11 44.9	13 43.2	15 45.4	17 43.7
19	19 50.8	21 53.0	23 43.4	1 45.6	3 43.9	5 46.1	7 44.4	9 46.6	11 48.9	13 47.1	15 49.4	17 47.6
20	19 54.8	21 57.0	23 47.4	1 49.6	3 47.9	5 50.1	7 48.4	9 50.6	11 52.8	13 51.1	15 53.3	17 51.6
21	19 58.7	22 0.9	23 51.3	1 53.5	3 51.8	5 54.0	7 52.3	9 54.5	11 56.7	13 55.0	15 57.2	17 55.5
22	20 2.6	22 4.9	23 55.3	1 57.5	3 55.8	5 58.0	7 56.2	9 58.5	12 0.7	13 59.0	16 1.2	17 59.5
23	20 6.6	22 8.8	23 59.2	2 1.4	3 59.7	6 1.9	8 0.2	10 2.4	12 4.6	14 2.9	16 5.1	18 3.4
24	20 10.5	22 12.7	0 3.1	2 5.4	4 3.6	6 5.9	8 4.2	10 6.4	12 8.6	14 6.8	16 9.1	18 7.3
25	20 14.5	22 16.7	0 7.1	2 9.3	4 7.6	6 9.8	8 8.1	10 10.3	12 12.5	14 10.8	16 13.0	18 11.3
26	20 18.4	22 20.6	0 11.0	2 13.2	4 11.5	6 13.7	8 12.0	10 14.2	12 16.5	14 14.7	16 17.0	18 15.2
27	20 22.4	22 24.6	0 15.0	2 17.2	4 15.5	6 17.7	8 16.0	10 18.2	12 20.4	14 18.7	16 20.9	18 19.2
28	20 26.3	22 28.5	0 18.9	2 21.1	4 19.4	6 21.6	8 19.9	10 22.1	12 24.3	14 22.6	16 24.8	18 23.1
29	20 30.2		0 22.9	2 25.1	4 23.3	6 25.6	8 23.8	10 26.1	12 28.3	14 26.6	16 28.8	18 27.1
30	20 34.2		0 26.8	2 29.0	4 27.3	6 29.5	8 27.8	10 30.0	12 32.2	14 30.5	16 32.7	18 31.0
31	20 38.1		0 30.7		4 31.2		8 31.7	10 34.0		14 34.4		18 34.9

SIDEREAL TIME, FOR 1904.

1	18 38.9	20 41.1	22 35.4	0 37.7	2 35.9	4 38.2	6 36.4	8 38.7	10 40.9	12 39.2	14 41.4	16 39.6
2	18 42.8	20 45.1	22 39.4	0 41.6	2 39.9	4 42.1	6 40.4	8 42.6	10 44.8	12 43.1	14 45.3	16 43.6
3	18 46.8	20 49.0	22 43.3	0 45.5	2 43.8	4 46.0	6 44.3	8 46.5	10 48.8	12 47.0	14 49.3	16 47.6
4	18 50.7	20 52.9	22 47.3	0 49.5	2 47.8	4 49.9	6 48.3	8 50.5	10 52.7	12 51.0	14 53.2	16 51.5
5	18 54.7	20 56.9	22 51.2	0 53.4	2 51.7	4 53.9	6 52.2	8 54.4	10 56.6	12 54.9	14 57.2	16 55.4
6	18 58.6	21 0.8	22 55.2	0 57.4	2 55.7	4 57.9	6 56.1	8 58.4	11 0.6	12 58.9	15 1.1	16 59.4
7	19 2.5	21 4.8	22 59.1	1 1.3	2 59.6	5 1.8	7 0.1	9 2.3	11 4.5	13 2.8	15 5.0	17 3.3
8	19 6.5	21 8.7	23 3.0	1 5.3	3 3.5	5 5.8	7 4.0	9 6.3	11 8.5	13 6.8	15 9.0	17 7.2
9	19 10.4	21 12.6	23 7.0	1 9.2	3 7.5	5 9.7	7 8.0	9 10.2	11 12.4	13 10.7	15 12.9	17 11.1
10	19 14.4	21 16.6	23 10.9	1 13.1	3 11.4	5 13.6	7 11.9	9 14.1	11 16.3	13 14.6	15 16.9	17 15.1
11	19 18.3	21 20.5	23 14.9	1 17.1	3 15.4	5 17.6	7 15.9	9 18.1	11 20.3	13 18.6	15 20.8	17 19.1
12	19 22.3	21 24.5	23 18.8	1 21.0	3 19.3	5 21.5	7 19.8	9 22.0	11 24.2	13 22.5	15 24.7	17 23.0
13	19 26.2	21 28.4	23 22.8	1 24.0	3 23.5	5 25.5	7 23.7	9 26.0	11 28.2	13 26.5	15 28.7	17 27.0
14	19 30.2	21 32.4	23 26.7	1 28.9	3 27.2	5 29.4	7 27.7	9 29.9	11 32.1	13 30.4	15 32.6	17 30.9
15	19 34.1	21 36.3	23 30.6	1 32.9	3 31.1	5 33.4	7 31.6	9 33.9	11 36.1	13 34.3	15 36.6	17 34.8
16	19 38.0	21 40.2	23 34.6	1 36.8	3 35.1	5 37.3	7 35.6	9 37.8	11 40.0	13 38.3	15 40.5	17 38.7
17	19 42.0	21 44.2	23 38.5	1 40.7	3 39.0	5 41.2	7 39.5	9 41.7	11 44.0	13 42.2	15 44.5	17 42.7
18	19 45.9	21 48.1	23 42.5	1 44.7	3 43.0	5 45.2	7 43.5	9 45.7	11 47.9	13 46.2	15 48.4	17 46.7
19	19 49.8	21 52.1	23 46.4	1 48.6	3 46.9	5 49.1	7 47.4	9 49.6	11 51.8	13 50.1	15 52.3	17 50.6
20	19 53.8	21 56.0	23 50.4	1 52.6	3 50.8	5 53.1	7 51.3	9 53.6	11 55.8	13 54.1	15 56.3	17 54.6
21	19 57.7	22 0.0	23 54.3	1 56.5	3 54.8	5 57.0	7 55.3	9 57.5	11 59.7	13 58.0	16 0.2	17 58.5
22	20 1.7	22 3.9	23 58.2	2 0.5	3 58.7	6 1.0	7 59.2	10 1.5	12 3.7	14 1.9	16 4.2	18 2.4
23	20 5.6	22 7.8	0 2.2	2 4.4	4 2.7	6 4.9	8 3.2	10 5.4	12 7.6	14 5.9	16 8.1	18 6.4
24	20 9.6	22 11.8	0 6.1	2 8.3	4 6.6	6 8.8	8 7.1	10 9.3	12 11.6	14 9.8	16 12.1	18 10.3
25	20 13.5	22 15.7	0 10.1	2 12.3	4 10.6	6 12.8	8 11.1	10 13.3	12 15.5	14 13.8	16 16.0	18 14.3
26	20 17.5	22 19.7	0 14.0	2 16.2	4 14.5	6 16.7	8 15.0	10 17.2	12 19.4	14 17.7	16 19.9	18 18.2
27	20 21.4	22 23.6	0 17.9	2 20.2	4 18.4	6 20.7	8 18.9	10 21.2	12 23.4	14 21.7	16 23.9	18 22.2
28	20 25.3	22 27.6	0 21.9	2 24.1	4 22.4	6 24.6	8 22.9	10 25.1	12 27.3	14 25.6	16 27.8	18 26.1
29	20 29.3	22 31.5	0 25.8	2 28.1	4 26.3	6 28.6	8 26.8	10 29.0	12 31.3	14 29.5	16 31.8	18 30.0
30	20 33.2		0 29.8	2 32.0	4 30.3	6 32.5	8 30.8	10 33.0	12 35.2	14 33.5	16 35.7	18 34.0
31	20 37.2		0 33.7		4 34.2		8 34.7	10 36.9		14 37.4		18 37.9

EQUATION OF TIME, FOR THE YEAR 1901,
For Apparent Noon at Greenwich.

Day	Jan.	Feb.	Mar.	April	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.
	<i>add</i>	<i>add</i>	<i>add</i>		<i>sub</i>		<i>add</i>	<i>add</i>		<i>sub</i>	<i>sub</i>	
1	3 ^m 34'	13 ^m 46'	12 ^m 38'	<i>add</i> 4 ^m 7'	2 ^m 55'	<i>sub</i> 2 ^m 30'	3 ^m 27'	6 ^m 8'	<i>add</i> 0 ^m 4'	10 ^m 10'	16 ^m 20'	<i>sub</i> 11 ^m 2'
2	4 2	13 53	12 26	3 49	3 3	2 21	3 39	6 4	<i>sub</i> 0 15	10 30	16 21	10 40
3	4 30	14 0	12 14	3 30	3 10	2 12	3 50	6 0	0 35	10 49	16 22	10 16
4	4 58	14 6	12 1	3 13	3 17	2 2	4 1	5 55	0 54	11 7	16 21	9 53
5	5 25	14 12	11 48	2 55	3 22	1 52	4 12	5 50	1 14	11 25	16 20	9 28
6	5 52	14 16	11 34	2 37	3 28	1 42	4 22	5 44	1 33	11 43	16 18	9 3
7	6 18	14 20	11 20	2 20	3 33	1 31	4 32	5 37	1 54	12 1	16 16	8 38
8	6 44	14 23	11 5	2 3	3 37	1 20	4 42	5 30	2 14	12 18	16 12	8 11
9	7 9	14 25	10 50	1 46	3 41	1 9	4 51	5 23	2 34	12 34	16 8	7 45
10	7 34	14 26	10 34	1 29	3 44	0 57	5 0	5 14	2 55	12 50	16 2	7 18
11	7 58	14 27	10 19	1 13	3 46	0 45	5 9	5 6	3 15	13 6	15 56	6 50
12	8 22	14 27	10 3	0 56	3 48	0 33	5 17	4 56	3 36	13 21	15 49	6 22
13	8 45	14 26	9 46	0 41	3 49	0 21	5 24	4 46	3 57	13 36	15 41	5 54
14	9 7	14 24	9 30	0 25	3 50	<i>sub</i> 0 8	5 32	4 36	4 18	13 50	15 33	5 20
15	9 29	14 22	9 13	<i>add</i> 0 10	3 50	<i>add</i> 0 4	5 38	4 25	4 39	14 4	15 23	4 57
16	9 50	14 19	8 56	<i>sub</i> 0 5	3 49	0 17	5 45	4 13	5 0	14 17	15 13	4 28
17	10 10	14 15	8 39	0 19	3 48	0 30	5 50	4 1	5 21	14 29	15 1	3 58
18	10 30	14 11	8 21	0 33	3 47	0 43	5 56	3 49	5 43	14 41	14 49	3 29
19	10 49	14 6	8 4	0 46	3 45	0 56	6 0	3 35	6 4	14 53	14 37	2 59
20	11 8	14 0	7 46	1 0	3 42	1 9	6 5	3 22	6 25	15 3	14 23	2 29
21	11 25	13 53	7 28	1 12	3 38	1 22	6 8	3 8	6 46	15 14	14 8	2 0
22	11 42	13 46	7 10	1 25	3 35	1 35	6 11	2 53	7 7	15 23	13 53	1 30
23	11 58	13 38	6 52	1 37	3 30	1 48	6 14	2 38	7 28	15 32	13 37	1 0
24	12 13	13 30	6 34	1 48	3 26	2 1	6 15	2 22	7 49	15 40	13 21	0 30
25	12 28	13 21	6 15	1 59	3 20	2 14	6 17	2	8 10	15 48	13 3	<i>sub</i> 0 0
26	12 41	13 11	5 57	2 10	3 14	2 27	6 17	1 50	8 30	15 54	12 45	<i>add</i> 0 30
27	12 54	13 1	5 39	2 20	3 8	2 39	6 17	1 33	8 51	16 1	12 26	0 59
28	13 6	12 50	5 20	2 30	3 1	2 52	6 17	1 16	9 11	16 6	12 6	1 29
29	13 17		5 2	2 39	2 54	3 4	6 15	0 58	9 31	16 11	11 45	1 58
30	13 28		4 43	2 47	2 47	3 16	6 14	0 40	9 51	16 14	11 24	2 27
31	13 37		4 25	2 38	2 38		6 11	0 22		16 17		2 56

EQUATION OF TIME, FOR 1902.

	<i>add</i>	<i>add</i>	<i>add</i>		<i>sub</i>		<i>add</i>	<i>add</i>		<i>sub</i>	<i>sub</i>	
1	5 ^m 25'	13 ^m 42'	12 ^m 40'	<i>add</i> 4 ^m 10'	2 ^m 54'	<i>sub</i> 2 ^m 32'	3 ^m 25'	6 ^m 10'	<i>add</i> 0 ^m 10'	10 ^m 4'	16 ^m 18'	<i>sub</i> 11 ^m 7'
2	3 53	13 50	12 28	3 52	3 2	2 23	3 37	6 7	<i>sub</i> 0 9	10 23	16 19	10 45
3	4 22	13 57	12 16	3 34	3 9	2 14	3 49	6 3	0 28	10 42	16 20	10 22
4	4 49	14 4	12 3	3 16	3 15	2 4	4 0	5 58	0 47	11 1	16 20	9 58
5	5 17	14 9	11 50	2 59	3 21	1 54	4 11	5 13	1 7	11 19	16 19	9 34
6	5 44	14 14	11 36	2 41	3 26	1 43	4 21	5 48	1 26	11 37	16 18	9 9
7	6 10	14 18	11 22	2 24	3 31	1 32	4 32	5 41	1 46	11 54	16 15	8 43
8	6 36	14 22	11 8	2 7	3 35	1 21	4 42	5 34	2 7	12 12	16 12	8 17
9	7 2	14 24	10 53	1 50	3 39	1 10	4 51	5 27	2 27	12 28	16 8	7 51
10	7 27	14 26	10 38	1 33	3 42	0 58	5 0	5 19	2 48	12 45	16 3	7 24
11	7 51	14 27	10 22	1 17	3 44	0 46	5 9	5 10	3 8	13 1	15 57	6 57
12	8 15	14 27	10 7	1 1	3 46	0 34	5 17	5 1	3 29	13 16	15 50	6 30
13	8 38	14 26	9 50	0 45	3 48	0 22	5 25	4 51	3 50	13 31	15 43	6 2
14	9 1	14 25	9 34	0 30	3 49	<i>sub</i> 0 10	5 32	4 40	4 11	13 45	15 34	5 33
15	9 23	14 22	9 17	<i>add</i> 0 14	3 49	<i>add</i> 0 3	5 39	4 29	4 33	13 59	15 25	5 5
16	9 44	14 19	9 0	<i>sub</i> 0 0	3 49	0 15	5 45	4 18	4 54	14 13	15 15	4 36
17	10 5	14 16	8 43	0 15	3 48	0 28	5 51	4 6	5 15	14 26	15 5	4 7
18	10 25	14 11	8 26	0 29	3 46	0 41	5 56	3 53	5 37	14 38	14 53	3 38
19	10 44	14 6	8 8	0 43	3 44	0 54	6 0	3 40	5 58	14 50	14 40	3 8
20	11 2	14 0	7 50	0 56	3 42	1 7	6 5	3 26	6 19	15 1	14 27	2 38
21	11 20	13 54	7 32	1 9	3 39	1 20	6 8	3 12	6 40	15 11	14 13	2 8
22	11 37	13 47	7 14	1 22	3 35	1 33	6 11	2 57	7 1	15 21	13 58	1 39
23	11 53	13 39	6 56	1 34	3 31	1 46	6 14	2 42	7 22	15 30	13 42	1 9
24	12 8	13 30	6 37	1 46	3 27	1 58	6 16	2 27	7 43	15 38	13 25	0 39
25	12 23	13 41	6 19	1 57	3 22	2 11	6 17	2 11	8 4	15 46	13 8	<i>sub</i> 0 9
26	12 36	13 12	6 0	2 8	3 16	2 24	6 18	1 55	8 25	15 53	12 49	<i>add</i> 0 21
27	12 49	13 2	5 42	2 18	3 10	2 37	6 18	1 38	8 45	15 59	12 30	0 51
28	13 1	12 51	5 23	2 28	3 3	2 49	6 18	1 21	9 5	16 4	12 11	1 21
29	13 13		5 5	2 37	2 56	3 1	6 17	1 4	9 25	16 9	11 50	1 50
30	13 23		4 47	2 46	2 48	3 13	6 15	0 46	9 45	16 13	11 29	2 20
31	13 33		4 28		2 40		6 13	0 28		16 16		2 49

EQUATION OF TIME, FOR THE YEAR 1903.
For Apparent Noon at Greenwich.

Day	Jan.	Feb.	Mar.	April	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.
		<i>add</i>	<i>add</i>		<i>sub.</i>		<i>add</i>		<i>sub.</i>	<i>sub.</i>	<i>sub.</i>	
1	<i>add</i> 3 ^m 18 ^s	13 ^m 39 ^s	12 ^m 42 ^s	<i>add</i> 4 ^m 15 ^s	2 ^m 51 ^s	<i>sub.</i> 2 ^m 33 ^s	3 ^m 24 ^s	<i>add</i> 6 ^m 12 ^s	<i>add</i> 0 ^m 14 ^s	9 ^m 59 ^s	16 ^m 17 ^s	<i>sub.</i> 11 ^m 17 ^s
2		3 46	13 47	12 31	3 57	2 59	2 24	3 35	<i>sub.</i> 0 4	10 19	16 19	10 5
3		4 15	13 55	12 19	3 39	3 6	2 15	3 47	0 23	10 38	16 20	10 7
4		4 42	14 2	12 6	3 21	3 13	2 5	3 58	0 43	10 57	16 21	10 9
5		5 10	14 8	11 53	3 3	3 19	1 55	4 9	1 2	11 15	16 20	9 4
6		5 37	14 13	11 40	2 46	3 24	1 45	4 19	1 22	11 33	16 19	9 15
7		6 3	14 17	11 26	2 28	3 29	1 35	4 29	1 42	11 51	16 16	8 5
8		6 29	14 20	11 11	2 11	3 34	1 24	4 39	2 2	12 8	16 13	8 2
9		6 55	14 23	10 56	1 54	3 38	1 13	4 49	2 23	12 25	16 9	7 5
10		7 20	14 24	10 41	1 37	3 41	1 1	4 58	2 44	12 42	16 5	7 3
11		7 44	14 25	10 26	1 21	3 44	0 49	5 6	3 4	12 58	15 59	7 4
12		8 8	14 25	10 10	1 4	3 46	0 37	5 14	3 25	13 13	15 53	6 5
13		8 31	14 25	9 54	0 48	3 48	0 25	5 22	3 46	13 28	15 45	6 4
14		8 54	14 23	9 37	0 33	3 49	0 13	5 29	4 42	13 43	15 37	5 4
15		9 16	14 21	9 20	0 17	3 49	<i>sub.</i> 0 1	5 36	4 31	13 57	15 28	5 12
16		9 37	14 18	9 3	<i>add</i> 0 2	3 49	<i>add</i> 0 12	5 43	4 20	14 10	15 18	4 45
17		9 58	14 15	8 46	<i>sub.</i> 0 12	3 48	0 25	5 49	4 8	14 23	15 7	4 14
18		10 18	14 11	8 29	0 27	3 47	0 38	5 54	3 56	14 35	14 55	3 44
19		10 37	14 6	8 11	0 41	3 45	0 51	5 59	3 43	14 47	14 43	3 14
20		10 56	14 0	7 53	0 54	3 43	1 4	6 3	3 29	14 58	14 30	2 45
21		11 14	13 54	7 35	1 7	3 40	1 17	6 7	3 15	6 35	15 8	14 15
22		11 31	13 47	7 17	1 20	3 36	1 30	6 10	3 1	6 56	15 18	14 0
23		11 47	13 40	6 59	1 32	3 32	1 43	6 13	2 46	7 17	15 27	13 45
24		12 3	13 32	6 41	1 43	3 28	1 56	6 16	2 31	7 38	15 35	13 28
25		12 18	13 23	6 23	1 54	3 23	2 9	6 17	2 15	7 59	15 43	13 11
26		12 32	13 14	6 4	2 5	3 17	2 22	6 18	1 59	8 19	15 50	12 53
27		12 45	13 4	5 46	2 15	3 11	2 34	6 19	1 43	8 40	15 57	12 34
28		12 57	12 53	5 28	2 25	3 4	2 47	6 19	1 26	9 0	16 2	12 15
29		13 9		5 10	2 34	2 57	2 59	6 18	1 9	9 20	16 7	11 55
30		13 20		4 51	<i>sub.</i> 2 43	2 49	<i>add</i> 3 12	6 16	0 51	<i>sub.</i> 9 40	16 11	11 34
31	<i>add</i> 13 30		4 33		2 41		6 14	<i>add</i> 0 33			16 15	<i>add</i> 2 4

EQUATION OF TIME, FOR 1904.

		<i>add</i>	<i>add</i>		<i>sub.</i>		<i>add</i>		<i>sub.</i>	<i>sub.</i>	<i>sub.</i>	
1	<i>add</i> 3 ^m 11 ^s	13 ^m 37 ^s	12 ^m 34 ^s	<i>add</i> 4 ^m 1 ^s	2 ^m 57 ^s	<i>sub.</i> 2 ^m 27 ^s	3 ^m 32 ^s	<i>add</i> 6 ^m 8 ^s	<i>sub.</i> 0 ^m 1 ^s	10 ^m 16 ^s	16 ^m 20 ^s	<i>sub.</i> 10 ^m 19 ^s
2		3 40	13 45	12 22	3 43	3 4	2 18	3 43	0 20	10 35	16 21	10 3
3		4 8	13 53	12 9	3 25	3 11	2 8	3 54	0 39	10 53	16 21	10 1
4		4 35	14 0	11 56	3 7	3 18	1 58	4 5	0 59	11 12	16 21	9 4
5		5 3	14 6	11 43	2 50	3 24	1 48	4 16	1 18	11 30	16 20	9 2
6		5 30	14 11	11 29	2 32	3 29	1 38	4 26	1 38	11 48	16 17	8 5
7		5 57	14 15	11 14	2 15	3 33	1 27	4 36	1 58	12 5	16 14	8 2
8		6 23	14 19	11 0	1 58	3 37	1 16	4 46	2 19	12 22	16 10	8 4
9		6 48	14 22	10 45	1 41	3 40	1 4	4 55	2 39	12 38	16 6	7 5
10		7 13	14 24	10 29	1 25	3 43	0 52	5 4	3 0	12 54	16 0	7 1
11		7 38	14 25	10 14	1 8	3 45	0 40	5 12	5 4	3 20	13 10	15 54
12		8 2	14 25	9 58	0 52	3 47	0 28	5 20	4 55	3 41	13 25	15 47
13		8 26	14 25	9 41	0 37	3 48	0 16	5 28	4 45	4 2	13 39	15 39
14		8 49	14 24	9 25	0 22	3 49	<i>sub.</i> 0 3	5 35	4 34	4 23	13 53	15 30
15		9 11	14 22	9 8	<i>add</i> 0 7	3 49	<i>add</i> 0 10	5 42	4 23	4 44	14 7	15 20
16		9 33	14 20	8 51	<i>sub.</i> 0 8	3 48	0 22	5 48	4 11	5 6	14 20	15 10
17		9 54	14 17	8 34	0 22	3 47	0 35	5 53	3 59	5 27	14 32	14 58
18		10 14	14 13	8 16	0 36	3 45	0 48	5 58	3 46	5 48	14 44	14 46
19		10 34	14 8	7 59	0 50	3 42	1 1	6 3	3 33	6 9	14 55	14 33
20		10 53	14 3	7 41	1 3	3 39	1 14	6 7	3 19	6 30	15 6	14 19
21		11 11	13 57	7 23	1 15	3 36	1 27	6 10	3 4	6 52	15 16	14 5
22		11 28	13 50	7 5	1 27	3 32	1 40	6 13	2 50	7 13	15 26	13 49
23		11 44	13 43	6 47	1 39	3 28	1 53	6 15	2 34	7 34	15 34	13 33
24		12 0	13 35	6 28	1 51	3 23	2 6	6 17	2 18	7 55	15 42	13 16
25		12 15	13 26	6 10	2 2	3 18	2 19	6 18	2 2	8 15	15 50	12 58
26		12 29	13 17	5 52	2 12	3 12	2 31	6 18	1 46	8 36	15 56	12 40
27		12 43	13 7	5 33	2 22	3 5	2 44	6 18	1 29	8 56	16 2	12 21
28		12 55	12 56	5 15	2 32	2 58	2 56	6 17	1 12	9 16	16 7	12 1
29		13 7	12 45	4 56	2 41	2 51	3 8	6 16	0 54	9 36	16 12	11 40
30		13 18		4 38	<i>sub.</i> 2 49	2 43	<i>add</i> 3 20	6 14	0 36	<i>sub.</i> 9 56	16 15	11 18
31	<i>add</i> 13 28		4 20		2 35		6 11	<i>add</i> 0 18			16 18	<i>add</i> 3 3

MEAN PLACES OF THE PRINCIPAL FIXED STARS FOR JAN 1st, 1900.

Name	Mag.	Right Asc.	Ann. Var.	Declination	Ann. Var.
		^h ^m ^s	^s	[°] ['] ["]	["]
α Andromedæ <i>Alpheratz</i>	2	0 3 13	+3.09	28 32 18 N.	+19.9
γ Pegasi <i>Algenib</i>	3	0 8 5	3.08	14 37 39 N.	+20.0
α Phœnicis	2	0 21 20	2.97	42 50 57 S.	-19.5
α Cassiopeiæ <i>Schedar</i>	var.	0 34 50	3.37	55 59 19 N.	+19.8
β Ceti <i>Denib Kaitos</i>	2	0 38 34	3.01	18 32 8 S.	-19.8
α Ursæ Minoris <i>Polaris</i>	2	1 22 33	25.31	88 46 27 N.	+18.8
α Eridani <i>Achernar</i>	1	1 33 59	2.24	57 44 41 S.	-18.3
γ Andromedæ <i>Almach</i>	2	1 57 45	3.66	41 51 0 N.	+17.4
α Arietis <i>Hamel</i>	2	2 1 32	3.37	22 59 23 N.	+17.2
α Ceti <i>Menkar</i>	2, 3	2 57 3	3.13	3 41 51 N.	+14.3
α Persei <i>Mirfak</i>	2	3 17 11	+4.26	49 30 19 N.	+13.1
α Tauri <i>Aldebaran</i>	1	4 30 11	3.44	16 18 30 N.	+7.5
α Aurigæ <i>Capella</i>	1	5 9 18	4.43	45 53 47 N.	+4.0
β Orionis <i>Rigel</i>	1	5 9 44	2.88	8 19 18.	-4.4
β Tauri <i>Nath</i>	2	5 19 58	3.79	28 31 23 N.	+3.3
δ Orionis	2	5 26 54	3.06	0 22 23 S.	-2.9
ε Orionis <i>Alnilum</i>	2	5 31 8	3.04	1 15 57 S.	-2.5
α Columbæ <i>Phact</i>	2	5 36 2	2.18	34 7 38 S.	-2.1
α Orionis <i>Betelgeuse</i>	var.	5 49 45	3.25	7 23 19 N.	+1.0
β Aurigæ <i>Menkalinan</i>	2	5 52 12	4.40	44 50 14 N.	+6.7
α Argûs <i>Canopus</i>	1	6 21 44	+1.33	52 38 27 S.	+1.9
γ Geminorum <i>Athæna</i>	2	6 31 56	3.47	16 29 5 N.	-2.8
α Canis Majoris <i>Sirius</i>	1	6 40 44	2.64	16 34 43 S.	+4.7
ε Canis Majoris <i>Adara</i>	1, 2	6 54 42	2.36	28 50 9 S.	+4.7
α ² Geminorum <i>Castor</i>	2	7 28 13	3.84	32 6 29 N.	-7.6
α Canis Minoris <i>Procyon</i>	1	7 34 4	3.14	5 28 52 N.	-9.0
β Geminorum <i>Pollux</i>	1	7 39 12	3.68	28 16 4 N.	-8.4
ζ Argûs	2	8 0 4	2.11	39 43 16 S.	+10.0
δ Argûs	2	8 41 57	1.65	54 20 32 S.	+15.0
α Hydre <i>Alphard</i>	2	9 22 40	2.95	8 13 30 S.	+15.4
α Leonis <i>Regulus</i>	1, 2	10 3 3	+3.20	12 27 22 N.	-17.5
γ ¹ Leonis <i>Algeiba</i>	2	10 14 28	3.31	20 20 50 N.	-18.1
γ Argûs	var.	10 41 11	2.32	59 9 30 S.	+18.9
α Ursæ Majoris <i>Dubhe</i>	2	10 57 34	3.74	62 17 27 N.	-19.4
δ Leonis <i>Zosma</i>	2, 3	11 8 47	3.20	21 4 18 N.	-19.7
β Leonis <i>Denebola</i>	2	11 43 58	3.06	15 7 52 N.	-20.1
γ Ursæ Majoris <i>Phecda</i>	2, 3	11 48 34	3.18	54 15 3 N.	-20.0
α ¹ Crucis	1	12 21 2	3.30	62 32 41 S.	+20.0
β Corvi	2, 3	12 29 8	3.14	22 50 38 S.	+20.0
α Canum Venaticorum	3	12 51 21	2.81	38 51 30 N.	-19.5
α Virginis <i>Spica</i>	1	13 19 55	+3.15	10 38 22 S.	+18.9
γ Ursæ Majoris <i>Benetnasch</i>	2	13 43 36	2.37	49 48 44 N.	-18.1
β Centauri	1	13 56 46	4.19	59 53 26 S.	+17.6
α Draconis <i>Thuban</i>	3, 4	14 1 41	1.62	64 51 13 N.	-17.3
α Boötis <i>Arcturus</i>	1	14 11 6	2.73	19 42 11 N.	-18.8
α ² Centauri	1	14 32 49	4.05	60 25 10 S.	+15.0
α Libræ <i>Zuben el Genubi</i>	3	14 45 21	+3.31	15 37 35 S.	+15.1
β Ursæ Minoris <i>Kochab</i>	2	14 51 0	-0.22	74 33 51 N.	-14.7
β Libræ <i>Zuben el Chamali</i>	2	15 11 37	+3.22	9 0 51 S.	+13.5
α Coronæ Borealis <i>Alphacca</i>	2	15 30 27	2.54	27 3 4 N.	-12.3
α Serpentis <i>Unukhalhai</i>	2, 3	15 39 20	+2.95	6 44 24 N.	-11.5
β ¹ Scorpïi	3	15 59 37	3.48	19 31 55 S.	+10.1
α Scorpïi <i>Antares</i>	1, 2	16 33 16	3.67	26 12 36 S.	+8.3
α Trianguli Australis	2	16 38 4	6.31	68 50 39 S.	+7.1
β Draconis <i>Alwaid</i>	3	17 28 10	1.35	52 22 31 N.	-2.8
α Ophiuchi <i>Ras Alhague</i>	2	17 30 17	2.78	12 37 58 N.	-2.8
γ Draconis <i>Rastaban</i>	2, 3	17 54 17	1.39	51 30 2 N.	-0.5
α Lyræ <i>Vega</i>	1	18 33 33	2.03	38 41 26 N.	+3.2
α Aquilæ <i>Altair</i>	1	19 45 54	2.93	8 36 14 N.	+9.3
α Pavonis	2	20 17 44	4.78	57 3 20 S.	-11.2
α Cygni <i>Deneb</i>	1, 2	20 38 1	+2.04	44 55 22 N.	+12.7
α Cephei <i>Alderamin</i>	2, 3	21 16 11	1.44	62 9 42 N.	+15.2
ε Pegasi	2, 3	21 39 16	2.95	9 24 59 N.	+16.4
α Gruis	2	22 1 56	3.80	47 26 43 S.	-17.3
β Gruis	2	22 36 42	3.60	47 24 28 S.	-18.7
α Piscis Aust. <i>Fomalhaut</i>	1	22 52 7	3.32	30 9 8 S.	-19.0
α Pegasi <i>Markab</i>	2	22 59 47	2.98	14 40 2 N.	+19.3

LOGARITHMS OF NUMBERS

No. 1 to 100

Log. 0.000000 to 2.000000

No.	Log.	No.	Log.	No.	Log.	No.	Log.	No.	Log.
1	0.000000	21	1.322219	41	1.612784	61	1.785330	81	1.908485
2	0.301030	22	1.342423	42	1.623249	62	1.792392	82	1.913814
3	0.477121	23	1.361728	43	1.633468	63	1.799341	83	1.919078
4	0.602060	24	1.380211	44	1.643453	64	1.806180	84	1.924279
5	0.698970	25	1.397940	45	1.653213	65	1.812913	85	1.929419
6	0.778151	26	1.414973	46	1.662758	66	1.819544	86	1.934498
7	0.845098	27	1.431364	47	1.672098	67	1.826075	87	1.939519
8	0.903090	28	1.447158	48	1.681241	68	1.832509	88	1.944483
9	0.954243	29	1.462398	49	1.690196	69	1.838849	89	1.949390
10	1.000000	30	1.477121	50	1.698970	70	1.845098	90	1.954243
11	1.041393	31	1.491362	51	1.707570	71	1.851258	91	1.959041
12	1.079181	32	1.505150	52	1.716003	72	1.857332	92	1.963788
13	1.113943	33	1.518514	53	1.724276	73	1.863323	93	1.968483
14	1.146128	34	1.531479	54	1.732394	74	1.869232	94	1.973128
15	1.176091	35	1.544068	55	1.740363	75	1.875061	95	1.977724
16	1.204120	36	1.556303	56	1.748188	76	1.880814	96	1.982271
17	1.230449	37	1.568202	57	1.755875	77	1.886491	97	1.986772
18	1.255273	38	1.579784	58	1.763428	78	1.892095	98	1.991226
19	1.278754	39	1.591065	59	1.770852	79	1.897627	99	1.995635
20	1.301030	40	1.602060	60	1.778151	80	1.903090	100	2.000000

No. 1000 to 1149

Log. 0 to 060320

No.	0	1	2	3	4	5	6	7	8	9	D.
100	000000	000434	000868	001301	001734	002166	002598	003029	003461	003891	432
101	004321	004751	005181	005609	006038	006466	006894	007321	007748	008174	428
102	008600	009026	009451	009876	010300	010724	011147	011570	011993	012415	424
103	012837	013259	013680	014100	014521	014940	015360	015779	016197	016616	420
104	017033	017451	017868	018284	018700	019116	019532	019947	020361	020775	416
105	021189	021603	022016	022428	022841	023252	023664	024075	024486	024896	412
106	025306	025715	026125	026533	026942	027350	027757	028164	028571	028978	408
107	029384	029789	030195	030600	031004	031408	031812	032216	032619	033021	404
108	033424	033827	034227	034628	035029	035430	035830	036230	036629	037028	400
109	037426	037825	038223	038620	039017	039414	039811	040207	040602	040998	397
110	041393	041787	042182	042576	042969	043362	043755	044148	044540	044932	393
111	045323	045714	046105	046495	046885	047275	047664	048053	048442	048830	389
112	049218	049606	049993	050380	050766	051153	051538	051924	052309	052694	386
113	053078	053463	053846	054230	054613	054996	055378	055760	056142	056524	383
114	056905	057286	057666	058046	058426	058805	059185	059563	059942	060320	379

No.	0	1	2	3	4	5	6	7	8	9	D.
100	000000	000434	000868	001301	001734	002166	002598	003029	003461	003891	432
101	004321	004751	005181	005609	006038	006466	006894	007321	007748	008174	428
102	008600	009026	009451	009876	010300	010724	011147	011570	011993	012415	424
103	012837	013259	013680	014100	014521	014940	015360	015779	016197	016616	420
104	017033	017451	017868	018284	018700	019116	019532	019947	020361	020775	416
105	021189	021603	022016	022428	022841	023252	023664	024075	024486	024896	412
106	025306	025715	026125	026533	026942	027350	027757	028164	028571	028978	408
107	029384	029789	030195	030600	031004	031408	031812	032216	032619	033021	404
108	033424	033827	034227	034628	035029	035430	035830	036230	036629	037028	400
109	037426	037825	038223	038620	039017	039414	039811	040207	040602	040998	397
110	041393	041787	042182	042576	042969	043362	043755	044148	044540	044932	393
111	045323	045714	046105	046495	046885	047275	047664	048053	048442	048830	389
112	049218	049606	049993	050380	050766	051153	051538	051924	052309	052694	386
113	053078	053463	053846	054230	054613	054996	055378	055760	056142	056524	383
114	056905	057286	057666	058046	058426	058805	059185	059563	059942	060320	379

LOGARITHMS OF NUMBERS

No. 1150 to 1499											Log. 060698 to 175802											
No.	0	1	2	3	4	5	6	7	8	9	D.											
115	060698	061075	061452	061829	062206	062582	062958	063333	063709	064083	376											
116	064458	064832	065206	065580	065953	066326	066699	067071	067443	067815	373											
117	068186	068557	068927	069298	069668	070038	070407	070776	071145	071514	370											
118	071882	072250	072617	072985	073352	073718	074085	074451	074816	075182	366											
119	075547	075912	076276	076640	077004	077368	077731	078094	078457	078819	363											
120	079181	079543	079904	080266	080626	080987	081347	081707	082067	082426	360											
121	082785	083144	083503	083861	084219	084576	084934	085291	085647	086004	357											
122	086360	086716	087071	087426	087781	088136	088490	088845	089198	089552	355											
123	089905	090258	090611	090963	091315	091667	092018	092370	092721	093071	352											
124	093422	093772	094122	094471	094820	095169	095518	095866	096215	096562	349											
125	096910	097257	097604	097951	098298	098644	098990	099335	099681	100026	346											
126	100371	100715	101059	101403	101747	102091	102434	102777	103119	103462	343											
127	103804	104146	104487	104828	105169	105510	105851	106191	106531	106871	341											
128	107210	107549	107888	108227	108565	108903	109241	109579	109916	110253	338											
129	110590	110926	111263	111599	111934	112270	112605	112940	113275	113609	335											
130	113943	114277	114611	114944	115278	115611	115943	116276	116608	116940	333											
131	117271	117603	117934	118265	118595	118926	119256	119586	119915	120245	330											
132	120574	120903	121231	121560	121888	122216	122544	122871	123198	123525	328											
133	123852	124178	124504	124830	125156	125481	125806	126131	126456	126781	325											
134	127105	127429	127753	128076	128399	128722	129045	129368	129690	130012	323											
135	130334	130655	130977	131298	131619	131939	132260	132580	132900	133219	321											
136	133539	133858	134177	134496	134814	135133	135451	135769	136086	136403	318											
137	136721	137037	137354	137671	137987	138303	138618	138934	139249	139564	316											
138	139879	140194	140508	140822	141136	141450	141763	142076	142389	142702	314											
139	143015	143327	143639	143951	144263	144574	144885	145196	145507	145818	311											
140	146128	146438	146748	147058	147367	147676	147985	148294	148603	148911	309											
141	149219	149527	149835	150142	150449	150756	151063	151370	151676	151982	307											
142	152288	152594	152900	153205	153510	153815	154120	154424	154728	155032	305											
143	155336	155640	155943	156246	156549	156852	157154	157457	157759	158061	303											
144	158362	158664	158965	159266	159567	159868	160168	160469	160769	161068	301											
145	161368	161667	161967	162266	162564	162863	163161	163460	163758	164055	299											
146	164553	164850	165147	165443	165739	166034	166330	166626	166922	167227	297											
147	167317	167613	167908	168203	168497	168792	169086	169380	169674	169968	295											
148	170262	170555	170848	171141	171434	171726	172019	172311	172603	172895	293											
149	173186	173478	173769	174060	174351	174641	174932	175222	175512	175802	291											
No.	0	1	2	3	4	5	6	7	8	9	D.											
D.	1	2	3	4	5	6	7	8	9													
290	29	58	87	116	145	174	203	232	261	334	33	67	100	134	167	200	234	267	301			
292	29	58	88	117	146	175	204	234	263	336	34	67	101	134	168	202	235	269	302			
294	29	59	88	118	147	176	206	235	265	338	34	68	101	135	169	203	237	270	304			
296	30	59	89	118	148	178	207	237	266	341	34	68	102	136	170	204	238	272	306			
298	30	60	89	119	149	179	209	238	268	342	34	68	103	137	171	205	239	274	308			
300	30	60	90	120	150	180	210	240	270	344	34	69	103	138	172	206	241	275	310			
302	30	60	91	121	151	181	211	242	272	346	35	69	104	138	173	208	242	277	311			
304	30	61	91	122	152	182	213	243	274	348	35	70	104	139	174	209	244	278	313			
306	31	61	92	122	153	184	214	245	275	350	35	70	105	140	175	210	245	280	315			
308	31	62	92	123	154	185	216	246	277	352	35	70	106	141	176	211	246	282	317			
310	31	62	93	124	155	186	217	248	279	354	35	71	106	142	177	212	248	283	319			
312	31	62	94	125	156	187	218	250	281	356	36	71	107	142	178	214	249	285	320			
314	31	63	94	126	157	188	220	251	283	358	36	72	107	143	179	215	251	286	322			
316	32	63	95	126	158	190	221	253	284	360	36	72	108	144	180	216	252	288	324			
318	32	64	95	127	159	191	223	254	286	362	36	72	109	145	181	217	253	290	326			
320	32	64	96	128	160	192	224	256	288	364	36	73	109	146	182	218	255	291	328			
322	32	64	97	129	161	193	225	258	290	366	37	73	110	146	183	220	256	293	329			
324	32	65	97	130	162	194	227	259	292	368	37	74	110	147	184	221	258	294	331			
326	33	65	98	130	163	196	228	261	293	370	37	74	111	148	185	222	259	296	333			
328	33	66	98	131	164	197	230	262	295	372	37	74	112	149	186	223	260	298	335			
330	33	66	99	132	165	198	231	264	297	374	37	75	112	150	187	224	262	299	337			
332	33	66	100	133	166	199	232	266	299	376	38	75	113	150	188	226	263	301	338			

LOGARITHMS OF NUMBERS

No. 1500 to 1899												Log. 176091 to 278525											
No.	0	1	2	3	4	5	6	7	8	9	D.												
150	176091	176381	176670	176959	177248	177536	177825	178113	178401	178689	289												
151	178977	179264	179552	179839	180126	180413	180699	180986	181272	181558	287												
152	181844	182129	182415	182700	182985	183270	183555	183839	184123	184407	285												
153	184671	184955	185239	185522	185805	186088	186371	186654	186936	187219	283												
154	187521	187803	188084	188366	188647	188928	189209	189490	189771	190051	281												
155	190332	190612	190892	191171	191451	191730	192010	192289	192567	192846	279												
156	193125	193403	193681	193959	194237	194514	194792	195069	195346	195623	278												
157	195900	196176	196453	196729	197005	197281	197556	197832	198107	198382	276												
158	198657	198932	199206	199481	199755	200029	200303	200577	200850	201124	274												
159	201397	201670	201943	202216	202488	202761	203033	203305	203577	203848	272												
160	204120	204391	204663	204934	205204	205475	205746	206016	206286	206556	271												
161	206826	207096	207365	207634	207904	208173	208441	208710	208979	209247	269												
162	209515	209783	210051	210319	210586	210853	211121	211388	211654	211921	267												
163	212188	212454	212720	212986	213252	213518	213783	214049	214314	214579	266												
164	214844	215109	215373	215638	215902	216166	216430	216694	216957	217221	264												
165	217484	217747	218010	218273	218536	218798	219060	219323	219585	219846	262												
166	220108	220370	220631	220892	221153	221414	221675	221936	222196	222456	261												
167	222716	222976	223236	223496	223755	224015	224274	224533	224792	225051	259												
168	225309	225568	225826	226084	226342	226600	226858	227115	227372	227630	258												
169	227887	228144	228400	228657	228913	229170	229426	229682	229938	230193	256												
170	230449	230704	230960	231215	231470	231724	231979	232234	232488	232742	255												
171	232996	233250	233504	233757	234011	234264	234517	234770	235023	235276	253												
172	235528	235781	236033	236285	236537	236789	237041	237292	237544	237795	252												
173	238046	238297	238548	238799	239049	239299	239550	239800	240050	240300	250												
174	240549	240799	241048	241297	241546	241795	242044	242293	242541	242790	249												
175	243038	243286	243534	243782	244030	244277	244525	244772	245019	245266	248												
176	245513	245759	246006	246252	246499	246745	246991	247237	247482	247728	246												
177	247973	248219	248464	248709	248954	249198	249443	249687	249932	250176	245												
178	249420	249664	249908	250151	250395	250638	250881	251125	251368	251610	243												
179	252853	253096	253338	253580	253822	254064	254306	254548	254790	255031	242												
180	255273	255514	255755	255996	256237	256477	256718	256958	257198	257439	241												
181	257679	257918	258158	258398	258637	258877	259116	259355	259594	259833	239												
182	260071	260310	260548	260787	261025	261263	261501	261739	261976	262214	238												
183	262451	262688	262925	263162	263399	263636	263873	264109	264346	264582	237												
184	264818	265054	265290	265525	265761	265996	266232	266467	266702	266937	235												
185	267172	267406	267641	267875	268110	268344	268578	268812	269046	269279	234												
186	269513	269746	269980	270213	270446	270679	270912	271144	271377	271609	233												
187	271842	272074	272306	272538	272770	273001	273233	273464	273696	273927	232												
188	274158	274389	274620	274850	275081	275311	275542	275772	276002	276232	230												
189	276462	276692	276921	277151	277380	277609	277838	278067	278296	278525	229												
No	0	1	2	3	4	5	6	7	8	9	D.												
D.	1	2	3	4	5	6	7	8	9														
228	23	46	68	91	114	137	160	182	205	260	26	52	78	104	130	156	182	208	234	260	286		
230	23	46	69	92	115	138	161	184	207	262	26	52	79	105	131	157	183	210	236	262	288		
232	23	46	70	93	116	139	162	186	209	264	26	53	79	106	132	158	185	211	238	264	290		
234	23	47	70	94	117	140	164	187	211	266	27	53	80	106	133	160	186	213	239	266	292		
236	24	47	71	94	118	142	165	189	212	268	27	54	80	107	134	161	188	214	241	268	294		
238	24	48	71	95	119	143	167	190	214	270	27	54	81	108	135	162	189	216	243	270	296		
240	24	48	72	96	120	144	168	192	216	272	27	54	82	109	136	163	190	218	245	272	298		
242	24	48	73	97	121	145	169	194	218	274	27	55	82	110	137	164	192	219	247	274	300		
244	24	49	73	98	122	146	171	195	220	276	28	55	83	110	138	166	193	221	248	276	302		
246	25	49	74	98	123	148	172	197	221	278	28	56	83	111	139	167	195	222	250	278	304		
248	25	50	74	99	124	149	174	198	223	280	28	56	84	112	140	168	196	224	252	280	306		
250	25	50	75	100	125	150	175	200	225	282	28	56	85	113	141	169	197	226	254	282	308		
252	25	50	76	101	126	151	176	202	227	284	28	57	85	114	142	170	199	227	256	284	310		
254	25	51	76	102	127	152	178	203	229	286	29	57	86	114	143	172	200	229	257	286	312		
256	26	51	77	102	128	154	179	205	230	288	29	58	86	115	144	173	202	230	259	288	314		
258	26	52	77	103	129	155	181	206	232	290	29	58	87	116	145	174	203	232	261	290	316		

LOGARITHMS OF NUMBERS

No. 3350 to 3899											Log. 525045 to 590953											
No.	0	1	2	3	4	5	6	7	8	9	D.											
335	525045	525174	525304	525434	525563	525693	525822	525951	526081	526210	129											
336	526339	526469	526598	526727	526856	526985	527114	527243	527372	527501	129											
337	527630	527759	527888	528016	528145	528274	528402	528531	528660	528788	129											
338	528917	529045	529174	529302	529430	529559	529687	529815	529943	530072	128											
339	530200	530328	530456	530584	530712	530840	530968	531096	531223	531351	128											
340	531479	531607	531734	531862	531990	532117	532245	532372	532500	532627	128											
341	532754	532882	533009	533136	533264	533391	533518	533645	533772	533899	127											
342	534026	534153	534280	534407	534534	534661	534787	534914	535041	535167	127											
343	535294	535421	535547	535674	535800	535927	536053	536180	536306	536432	126											
344	536558	536685	536811	536937	537063	537189	537315	537441	537567	537693	126											
345	537819	537945	538071	538197	538322	538448	538574	538699	538825	538951	126											
346	539076	539202	539327	539452	539578	539703	539829	539954	540079	540204	125											
347	540329	540455	540580	540705	540830	540955	541080	541205	541330	541454	125											
348	541579	541704	541829	541953	542078	542203	542327	542452	542576	542701	125											
349	542825	542950	543074	543199	543323	543447	543571	543696	543820	543944	124											
350	544068	544192	544316	544440	544564	544688	544812	544936	545060	545183	124											
351	545307	545431	545555	545678	545802	545925	546049	546172	546296	546419	124											
352	546543	546666	546789	546913	547036	547159	547282	547405	547528	547651	123											
353	547775	547898	548021	548144	548267	548389	548512	548635	548758	548881	123											
354	549003	549126	549249	549371	549494	549616	549739	549861	549984	550106	123											
355	550228	550351	550473	550595	550717	550840	550962	551084	551206	551328	122											
356	551450	551572	551694	551816	551938	552060	552181	552303	552425	552547	122											
357	552668	552790	552911	553033	553155	553276	553398	553519	553640	553762	121											
358	553883	554004	554126	554247	554368	554489	554610	554731	554852	554973	121											
359	555094	555215	555336	555457	555578	555699	555820	555940	556061	556182	121											
360	556303	556423	556544	556664	556785	556905	557026	557146	557267	557387	120											
361	557507	557627	557748	557868	557988	558108	558228	558349	558469	558589	120											
362	558709	558829	558948	559068	559188	559308	559428	559548	559667	559787	120											
363	559907	560026	560146	560265	560385	560504	560624	560743	560863	560982	119											
364	561101	561221	561340	561459	561578	561698	561817	561936	562055	562174	119											
365	562293	562412	562531	562650	562769	562888	563006	563125	563244	563362	119											
366	563481	563600	563718	563837	563955	564074	564192	564311	564429	564548	119											
367	564666	564784	564903	565021	565139	565257	565376	565494	565612	565730	118											
368	565848	565966	566084	566202	566320	566438	566555	566673	566791	566909	118											
369	567026	567144	567262	567379	567497	567614	567732	567849	567967	568084	118											
370	568202	568319	568436	568554	568671	568788	568905	569023	569140	569257	117											
371	569374	569491	569608	569725	569842	569959	570076	570193	570309	570426	117											
372	570543	570660	570776	570893	571010	571126	571243	571359	571476	571592	117											
373	571709	571825	571942	572058	572174	572291	572407	572523	572639	572755	116											
374	572872	572988	573104	573220	573336	573452	573568	573684	573800	573915	116											
375	574031	574147	574263	574379	574494	574610	574726	574841	574957	575072	116											
376	575188	575303	575419	575534	575650	575765	575880	575996	576111	576226	115											
377	576341	576457	576572	576687	576802	576917	577032	577147	577262	577377	115											
378	577492	577607	577722	577836	577951	578066	578181	578295	578410	578525	115											
379	578639	578754	578868	578983	579097	579212	579326	579441	579555	579669	114											
380	579784	579898	580012	580126	580241	580355	580469	580583	580697	580811	114											
381	580925	581039	581153	581267	581381	581495	581608	581722	581836	581950	114											
382	582063	582177	582291	582404	582518	582631	582745	582858	582972	583085	114											
383	583199	583312	583426	583539	583652	583765	583879	583992	584105	584218	113											
384	584331	584444	584557	584670	584783	584896	585009	585122	585235	585348	113											
385	585461	585574	585686	585799	585912	586024	586137	586250	586362	586475	113											
386	586587	586700	586812	586925	587037	587149	587262	587374	587486	587599	112											
387	587711	587823	587935	588047	588160	588272	588384	588496														

LOGARITHMS OF NUMBERS

No. 3900 to 4449

Log. 591065 to 648262

No.	0	1	2	3	4	5	6	7	8	9	D.
390	591065	591176	591287	591399	591510	591621	591732	591843	591955	592066	111
391	592177	592288	592399	592510	592621	592732	592843	592954	593064	593175	111
392	593286	593397	593508	593618	593729	593840	593950	594061	594171	594282	111
393	594393	594503	594614	594724	594834	594945	595055	595165	595276	595386	110
394	595496	595606	595717	595827	595937	596047	596157	596267	596377	596487	110
395	596597	596707	596817	596927	597037	597146	597256	597366	597476	597586	110
396	597695	597805	597914	598024	598134	598243	598353	598462	598572	598682	110
397	598791	598900	599009	599119	599228	599337	599446	599556	599665	599774	109
398	599883	599992	600101	600210	600319	600428	600537	600646	600755	600864	109
399	600973	601082	601191	601299	601408	601517	601625	601734	601843	601951	109
400	602060	602169	602277	602386	602494	602603	602711	602819	602928	603036	108
401	603144	603253	603361	603469	603577	603686	603794	603902	604010	604118	108
402	604226	604334	604442	604550	604658	604766	604874	604982	605089	605197	108
403	605305	605413	605521	605628	605736	605844	605951	606059	606166	606274	108
404	606381	606489	606596	606704	606811	606919	607026	607133	607241	607348	107
405	607455	607562	607669	607777	607884	607991	608098	608205	608312	608419	107
406	608526	608633	608740	608847	608954	609061	609167	609274	609381	609488	107
407	609594	609701	609808	609914	610021	610128	610234	610341	610447	610554	107
408	610660	610767	610873	610979	611086	611192	611298	611405	611511	611617	106
409	611723	611829	611935	612042	612148	612254	612360	612466	612572	612678	106
410	612784	612890	612996	613102	613207	613313	613419	613525	613630	613736	106
411	613842	613947	614053	614159	614264	614370	614475	614581	614686	614792	106
412	614897	615003	615108	615213	615319	615424	615529	615634	615740	615845	105
413	615950	616055	616160	616265	616370	616476	616581	616686	616790	616895	105
414	617000	617105	617210	617315	617420	617525	617629	617734	617839	617943	105
415	618048	618153	618257	618362	618466	618571	618676	618780	618884	618989	105
416	619093	619198	619302	619406	619511	619615	619719	619824	619928	620032	104
417	620136	620240	620344	620448	620552	620656	620760	620864	620968	621072	104
418	621176	621280	621384	621488	621592	621695	621799	621903	622007	622110	104
419	622214	622318	622421	622525	622628	622732	622835	622939	623042	623146	104
420	623249	623353	623456	623559	623663	623766	623869	623973	624076	624179	103
421	624282	624385	624488	624591	624695	624798	624901	625004	625107	625210	103
422	625312	625415	625518	625621	625724	625827	625929	626032	626135	626238	103
423	626340	626443	626546	626648	626751	626853	626956	627058	627161	627263	103
424	627366	627468	627571	627673	627775	627878	627980	628082	628185	628287	102
425	628389	628491	628593	628695	628797	628900	629002	629104	629206	629308	102
426	629410	629512	629613	629715	629817	629919	630021	630123	630224	630326	102
427	630428	630530	630631	630733	630835	630936	631038	631139	631241	631342	102
428	631444	631545	631647	631748	631849	631951	632052	632153	632255	632356	101
429	632457	632559	632660	632761	632862	632963	633064	633165	633266	633367	101
430	633468	633569	633670	633771	633872	633973	634074	634175	634276	634376	101
431	634477	634578	634679	634779	634880	634981	635081	635182	635283	635383	101
432	635484	635584	635685	635785	635886	635986	636087	636187	636287	636388	100
433	636488	636588	636688	636789	636889	636989	637089	637189	637290	637390	100
434	637490	637590	637690	637790	637890	637990	638090	638190	638290	638389	100
435	638489	638589	638689	638789	638888	638988	639088	639188	639287	639387	100
436	639486	639586	639686	639785	639885	639984	640084	640183	640283	640382	99
437	640481	640581	640680	640779	640879	640978	641077	641177	641276	641375	99
438	641474	641573	641672	641771	641871	641970	642069	642168	642267	642366	99
439	642465	642563	642662	642761	642860	642959	643058	643156	643255	643354	99
440	643453	643551	643650	643749	643847	643946	644044	644143	644242	644340	99
441	644439	644537	644636	644734	644832	644931	645029	645127	645226	645324	98
442	645422	645521	645619	645717	645815	645913	646011	646109	646208	646306	98
443	646404	646502	646600	646698	646796	646894	646992	647089	647187	647285	98
444	647383	647481	647579	647676	647774	647872	647969	648067	648165	648262	98
No.	0	1	2	3	4	5	6	7	8	9	D.
D.	1	2	3	4	5	6	7	8	9		
98	10	20	29	39	49	59	69	78	88		
100	10	20	30	40	50	60	70	80	90		
102	10	20	31	41	51	61	71	82	92		
104	10	21	31	42	52	62	73	83	94		
D.	1	2	3	4	5	6	7	8	9		
106	11	21	32	42	53	64	74	85	95		
108	11	22	32	43	54	65	76	86	97		
110	11	22	33	44	55	66	77	88	99		
112	11	22	34	45	56	67	78	90	101		

LOGARITHMS OF NUMBERS

No. 4450 to 4999											Log. 648360 to 698883											
No.	0	1	2	3	4	5	6	7	8	9	D.											
445	648360	648458	648555	648653	648750	648848	648945	649043	649140	649237	97											
446	649335	649432	649530	649627	649724	649821	649919	650016	650113	650210	97											
447	650308	650405	650502	650599	650696	650793	650890	650987	651084	651181	97											
448	651278	651375	651472	651569	651666	651762	651859	651956	652053	652150	97											
449	652246	652343	652440	652536	652633	652730	652826	652923	653019	653116	97											
450	653213	653309	653405	653502	653598	653695	653791	653888	653984	654080	96											
451	654177	654273	654369	654465	654562	654658	654754	654850	654946	655042	96											
452	655138	655235	655331	655427	655523	655619	655715	655810	655906	656002	96											
453	656098	656194	656290	656386	656482	656577	656673	656769	656864	656960	96											
454	657056	657152	657247	657343	657438	657534	657629	657725	657820	657916	96											
455	658011	658107	658202	658298	658393	658488	658584	658679	658774	658870	95											
456	658965	659060	659155	659250	659346	659441	659536	659631	659726	659821	95											
457	659916	660011	660106	660201	660296	660391	660486	660581	660676	660771	95											
458	660865	660960	661055	661150	661245	661339	661434	661529	661623	661718	95											
459	661813	661907	662002	662096	662191	662286	662380	662475	662569	662663	95											
460	662758	662852	662947	663041	663135	663230	663324	663418	663512	663607	94											
461	663701	663795	663889	663983	664078	664172	664266	664360	664454	664548	94											
462	664642	664736	664830	664924	665018	665112	665206	665299	665393	665487	94											
463	665581	665675	665769	665862	665956	666050	666143	666237	666331	666424	94											
464	666518	666612	666705	666799	666892	666986	667079	667173	667266	667360	94											
465	667453	667546	667640	667733	667826	667920	668013	668106	668199	668293	93											
466	668386	668479	668572	668665	668759	668852	668945	669038	669131	669224	93											
467	669317	669409	669503	669596	669689	669782	669875	669967	670060	670153	93											
468	670246	670339	670431	670524	670617	670710	670802	670895	670988	671080	93											
469	671173	671265	671358	671451	671543	671636	671728	671821	671913	672005	93											
470	672098	672190	672283	672375	672467	672560	672652	672744	672836	672929	92											
471	673021	673113	673205	673297	673390	673482	673574	673666	673758	673850	92											
472	673942	674034	674126	674218	674310	674402	674494	674586	674677	674769	92											
473	674861	674953	675045	675137	675228	675320	675412	675503	675595	675687	92											
474	675778	675870	675962	676053	676145	676236	676328	676419	676511	676602	92											
475	676694	676785	676876	676968	677059	677151	677242	677333	677424	677516	91											
476	677607	677698	677789	677881	677972	678063	678154	678245	678336	678427	91											
477	678518	678609	678700	678791	678882	678973	679064	679155	679246	679337	91											
478	679428	679519	679610	679700	679791	679882	679973	680063	680154	680245	91											
479	680336	680426	680517	680607	680698	680789	680879	680970	681060	681151	91											
480	681241	681332	681422	681513	681603	681693	681784	681874	681964	682055	90											
481	682145	682235	682326	682416	682506	682596	682686	682777	682867	682957	90											
482	683047	683137	683227	683317	683407	683497	683587	683677	683767	683857	90											
483	683947	684037	684127	684217	684307	684396	684486	684576	684666	684756	90											
484	684845	684935	685025	685114	685204	685294	685383	685473	685563	685652	90											
485	685742	685831	685921	686010	686100	686189	686279	686368	686458	686547	89											
486	686636	686726	686815	686904	686994	687083	687172	687261	687351	687440	89											
487	687529	687618	687707	687796	687886	687975	688064	688153	688242	688331	89											
488	688420	688509	688598	688687	688776	688865	688953	689042	689131	689220	89											
489	689309	689398	689486	689575	689664	689753	689841	689930	690019	690107	89											
490	690196	690285	690373	690462	690550	690639	690728	690816	690905	690993	89											
491	691081	691170	691258	691347	691435	691524	691612	691700	691789	691877	88											
492	691965	692053	692142	692230	692318	692406	692494	692582	692671	692759	88											
493	692847	692935	693023	693111	693199	693287	693375	693463	693551	693639	88											
494	693727	693815	693903	693991	694078	694166	694254	694342	694430	694517	88											
495	694605	694693	694781	694868	694956	695044	695131	695219	695307	695394	88											
496	695482	695569	695657	695744	695832	695919	696007	696094	696182	696269	87											
497	696356	696444	696531	696618	696706	696793	696880	696968	697055	697142	87											
498	697229	697317	697404	697491	697578	697665	697752	697839	697926	698014	87											
499	698101	698188	698275	698362	698449	698535	698622	698709	698796	698883	87											
No.	0	1	2	3	4	5	6	7	8	9	D.											
D.	1	2	3	4	5	6	7	8	9													
88	9	18	26	35	44	53	62	70	79													
89	9	18	27	36	44	53	62	71	80													
90	9	18	27	36	45	54	63	72	81													
91	9	18	27	36	45	55	64	73	82													
92	9	18	28	37	46	55	64	74	83													

LOGARITHMS OF NUMBERS

No. 5000 to 5549

Log. 698970 to 744215

No.	0	1	2	3	4	5	6	7	8	9	D.
500	698970	699057	699144	699231	699317	699404	699491	699578	699664	699751	87
501	699838	699924	700011	700098	700184	700271	700358	700444	700531	700617	87
502	700704	700790	700877	700963	701050	701136	701222	701309	701395	701482	86
503	701568	701654	701741	701827	701913	701999	702086	702172	702258	702344	86
504	702431	702517	702603	702689	702775	702861	702947	703033	703119	703205	86
505	703291	703377	703463	703549	703635	703721	703807	703893	703979	704065	86
506	704151	704236	704322	704408	704494	704579	704665	704751	704837	704922	86
507	705008	705094	705179	705265	705350	705436	705522	705607	705693	705778	86
508	705864	705949	706035	706120	706206	706291	706376	706462	706547	706632	85
509	706718	706803	706888	706974	707059	707144	707229	707315	707400	707485	85
510	707570	707655	707740	707826	707911	707996	708081	708166	708251	708336	85
511	708431	708506	708591	708676	708761	708846	708931	709015	709100	709185	85
512	709270	709355	709440	709524	709609	709694	709779	709863	709948	710033	85
513	710117	710202	710287	710371	710456	710540	710625	710710	710794	710879	85
514	710963	711048	711132	711217	711301	711385	711470	711554	711639	711723	84
515	711807	711892	711976	712060	712144	712229	712313	712397	712481	712566	84
516	712650	712734	712818	712902	712986	713070	713154	713238	713323	713407	84
517	713491	713575	713659	713742	713826	713910	713994	714078	714162	714246	84
518	714330	714414	714497	714581	714665	714749	714833	714916	715000	715084	84
519	715167	715251	715335	715418	715502	715586	715669	715753	715836	715920	84
520	716003	716087	716170	716254	716337	716421	716504	716588	716671	716754	83
521	716838	716921	717004	717088	717171	717254	717338	717421	717504	717587	83
522	717671	717754	717837	717920	718003	718086	718169	718253	718336	718419	83
523	718502	718585	718668	718751	718834	718917	719000	719083	719165	719248	83
524	719331	719414	719497	719580	719663	719745	719828	719911	719994	720077	83
525	720159	720242	720325	720407	720490	720573	720655	720738	720821	720903	83
526	720986	721068	721151	721233	721316	721398	721481	721563	721646	721728	82
527	721811	721893	721975	722058	722140	722222	722305	722387	722469	722552	82
528	722634	722716	722798	722881	722963	723045	723127	723209	723291	723374	82
529	723456	723538	723620	723702	723784	723866	723948	724030	724112	724194	82
530	724276	724358	724440	724522	724604	724685	724767	724849	724931	725013	82
531	725095	725176	725258	725340	725422	725503	725585	725667	725748	725830	82
532	725912	725993	726075	726156	726238	726320	726401	726483	726564	726646	82
533	726727	726809	726890	726972	727053	727134	727216	727297	727379	727460	81
534	727541	727623	727704	727785	727866	727948	728029	728110	728191	728273	81
535	728354	728435	728516	728597	728678	728759	728841	728922	729003	729084	81
536	729165	729246	729327	729408	729489	729570	729651	729732	729813	729893	81
537	729974	730055	730136	730217	730298	730378	730459	730540	730621	730702	81
538	730782	730863	730944	731024	731105	731186	731266	731347	731428	731508	81
539	731589	731669	731750	731830	731911	731991	732072	732152	732233	732313	81
540	732394	732474	732555	732635	732715	732796	732876	732956	733037	733117	80
541	733197	733278	733358	733438	733518	733598	733679	733759	733839	733919	80
542	733999	734079	734160	734240	734320	734400	734480	734560	734640	734720	80
543	734800	734880	734960	735040	735120	735200	735279	735359	735439	735519	80
544	735599	735679	735759	735838	735918	735998	736078	736157	736237	736317	80
545	736397	736477	736556	736635	736715	736795	736874	736954	737034	737113	80
546	737193	737272	737352	737431	737511	737590	737670	737749	737829	737908	79
547	737987	738067	738146	738225	738305	738384	738463	738543	738622	738701	79
548	738781	738860	738939	739018	739097	739177	739256	739335	739414	739493	79
549	739572	739651	739731	739810	739889	739968	740047	740126	740205	740284	79
550	740363	740442	740521	740600	740678	740757	740836	740915	740994	741073	79
551	741152	741230	741309	741388	741467	741546	741624	741703	741782	741860	79
552	741939	742018	742096	742175	742254	742332	742411	742489	742568	742647	79
553	742725	742804	742882	742961	743039	743118	743196	743275	743353	743431	78
554	743510	743588	743667	743745	743823	743902	743980	744058	744136	744215	78
No.	0	1	2	3	4	5	6	7	8	9	D.
D.	1	2	3	4	5	6	7	8	9		
78	8	16	23	31	39	47	55	62	70		
79	8	16	24	32	39	47	55	63	71		
80	8	16	24	32	40	48	56	64	72		
41	8	16	24	32	40	49	57	65	73		
22	8	16	25	33	41	49	57	66	74		
D.	1	2	3	4	5	6	7	8	9		
83	8	17	25	33	41	50	58	66	75		
84	8	17	25	34	42	50	59	67	76		
85	8	17	25	34	42	51	59	68	76		
86	9	17	26	34	43	52	60	69	77		
87	9	17	26	35	43	52	61	70	78		

LOGARITHMS OF NUMBERS

No. 5550 to 6099										Log. 744293 to 785259													
No.	0	1	2	3	4	5	6	7	8	9	D.	No.	0	1	2	3	4	5	6	7	8	9	D.
555	744293	744371	744449	744528	744606	744684	744762	744840	744919	744997	78	745	745075	745153	745231	745309	745387	745465	745543	745621	745699	745777	78
556	745075	745153	745231	745309	745387	745465	745543	745621	745699	745777	78	557	745855	745933	746011	746089	746167	746245	746323	746401	746479	746556	78
557	745855	745933	746011	746089	746167	746245	746323	746401	746479	746556	78	558	746634	746712	746790	746868	746945	747023	747101	747179	747256	747334	78
558	746634	746712	746790	746868	746945	747023	747101	747179	747256	747334	78	559	747412	747489	747567	747645	747722	747800	747878	747955	748033	748110	78
559	747412	747489	747567	747645	747722	747800	747878	747955	748033	748110	78	560	748188	748266	748343	748421	748498	748576	748653	748731	748808	748885	77
560	748188	748266	748343	748421	748498	748576	748653	748731	748808	748885	77	561	748963	749040	749118	749195	749272	749350	749427	749504	749582	749659	77
561	748963	749040	749118	749195	749272	749350	749427	749504	749582	749659	77	562	749736	749814	749891	749968	750045	750123	750200	750277	750354	750431	77
562	749736	749814	749891	749968	750045	750123	750200	750277	750354	750431	77	563	750508	750586	750663	750740	750817	750894	750971	751048	751125	751202	77
563	750508	750586	750663	750740	750817	750894	750971	751048	751125	751202	77	564	751279	751356	751433	751510	751587	751664	751741	751818	751895	751972	77
564	751279	751356	751433	751510	751587	751664	751741	751818	751895	751972	77	565	752048	752125	752202	752279	752356	752433	752509	752586	752663	752740	77
565	752048	752125	752202	752279	752356	752433	752509	752586	752663	752740	77	566	752816	752893	752970	753047	753123	753200	753277	753353	753430	753506	77
566	752816	752893	752970	753047	753123	753200	753277	753353	753430	753506	77	567	753583	753660	753736	753813	753889	753966	754042	754119	754195	754272	77
567	753583	753660	753736	753813	753889	753966	754042	754119	754195	754272	77	568	754348	754425	754501	754578	754654	754730	754807	754883	754960	755036	76
568	754348	754425	754501	754578	754654	754730	754807	754883	754960	755036	76	569	755112	755189	755265	755341	755417	755494	755570	755646	755722	755799	76
569	755112	755189	755265	755341	755417	755494	755570	755646	755722	755799	76	570	755875	755951	756027	756103	756180	756256	756332	756408	756484	756560	76
570	755875	755951	756027	756103	756180	756256	756332	756408	756484	756560	76	571	756636	756712	756788	756864	756940	757016	757092	757168	757244	757320	76
571	756636	756712	756788	756864	756940	757016	757092	757168	757244	757320	76	572	757396	757472	757548	757624	757700	757775	757851	757927	758003	758079	76
572	757396	757472	757548	757624	757700	757775	757851	757927	758003	758079	76	573	758155	758230	758306	758382	758458	758533	758609	758685	758761	758836	76
573	758155	758230	758306	758382	758458	758533	758609	758685	758761	758836	76	574	758912	758988	759063	759139	759214	759290	759366	759441	759517	759592	76
574	758912	758988	759063	759139	759214	759290	759366	759441	759517	759592	76	575	759668	759743	759819	759894	759970	760045	760121	760196	760272	760347	75
575	759668	759743	759819	759894	759970	760045	760121	760196	760272	760347	75	576	760422	760498	760573	760649	760724	760799	760875	760950	761025	761101	75
576	760422	760498	760573	760649	760724	760799	760875	760950	761025	761101	75	577	761176	761252	761328	761402	761477	761552	761627	761702	761778	761853	75
577	761176	761252	761328	761402	761477	761552	761627	761702	761778	761853	75	578	761928	762003	762078	762153	762228	762303	762378	762453	762529	762604	75
578	761928	762003	762078	762153	762228	762303	762378	762453	762529	762604	75	579	762679	762754	762829	762903	762978	763053	763128	763203	763278	763353	75
579	762679	762754	762829	762903	762978	763053	763128	763203	763278	763353	75	580	763428	763503	763578	763653	763727	763802	763877	763952	764027	764101	75
580	763428	763503	763578	763653	763727	763802	763877	763952	764027	764101	75	581	764176	764251	764326	764400	764475	764550	764624	764699	764774	764848	75
581	764176	764251	764326	764400	764475	764550	764624	764699	764774	764848	75	582	764923	764998	765072	765147	765221	765296	765370	765445	765520	765594	75
582	764923	764998	765072	765147	765221	765296	765370	765445	765520	765594	75	583	765669	765743	765818	765892	765966	766041	766115	766190	766264	766338	74
583	765669	765743	765818	765892	765966	766041	766115	766190	766264	766338	74	584	766413	766487	766562	766636	766710	766784	766859	766933	767007	767082	74
584	766413	766487	766562	766636	766710	766784	766859	766933	767007	767082	74	585	767156	767230	767304	767379	767453	767527	767601	767675	767749	767823	74
585	767156	767230	767304	767379	767453	767527	767601	767675	767749	767823	74	586	767898	767972	768046	768120	768194	768268	768342	768416	768490	768564	74
586	767898	767972	768046	768120	768194	768268	768342	768416	768490	768564	74	587	768638	768712	768786	768860	768934	769008	769082	769156	769230	769303	74
587	768638	768712	768786	768860	768934	769008	769082	769156	769230	769303	74	588	769377	769451	769525	769599	769673	769746	769820	769894	769968	770042	74
588	769377	769451	769525	769599	769673	769746	769820	769894	769968	770042	74	589	770115	770189	770263	770336	770410	770484	770557	770631	770705	770778	74
589	770115	770189	770263	770336	770410	770484	770557	770631	770705	770778	74	590	770852	770926	770999	771073	771146	771220	771293	771367	771440	771514	74
590	770852	770926	770999	771073	771146	771220	771293	771367	771440	771514	74	591	771587	771661	771734	771808	771881	771955	772028	772102	772175	772248	73
591	771587	771661	771734	771808	771881	771955	772028	772102	772175	772248	73	592	772322	772395	772468	772542	772615	772688	772762	772835	772908	772981	73
592	772322	772395	772468	772542	772615	772688	772762	772835	772908	772981	73	593	773055	773128	773201	773274	773348	773421	773494	773567	773640	773713	73
593	773055	773128	773201	773274	773348	773421	773494	773567	773640	773713	73	594	773786	773860	773933	774006	774079	774152	774225	774298	774371	774444	73
594	773786	773860	773933	774006	774079	774152	774225	774298	774371	774444	73	595	774517	774590	774663	774736	774809	774882	774955	775028	775100	775173	73
595	774517	774590	774663	774736	774809	774882	774955	775028	775100	775173	73	596	775246	775319	775392	775465	775538	775610	775683	775756	775829	775902	73
596	775246	775319	775392	775465	775538	775610	775683	775756	775829	775902	73	597	775974	776047	776120	776193	776265	776338	776411	776483	776556	776629	73
597	775974	776047	776120	776193	776265	776338	776411	776483	776556	776629	73	598	776701	776774	776846	776919	776992	777064	777137	777209	777282	777354	73
598	776701	776774	776846	776919	776992	777064	777137	777209	777282	777354	73	599	777427	777499	777572	777644	777717	777789	777862	777934	778006	778079	72
599	777427	777499	777572	777644	777717	777789	777862	777934	778006	778079	72	600	778151	778224	778296	778368	778441	778513	778585	778658	778730	778802	72
600	778151	778224	778296	778368	778441	778513	778585	778658	778730	778802	72	601	778874	778947	779019	779091	779163	779236	779308	779380	779452	779524	72
601	778874	778947	779019	779091	779163	779236	779308	779380	779452	779524	72	602	779596	779669	77								

LOGARITHMS OF NUMBERS

No. 6100 to 6649

Log. 785390 to 822756

No.	0	1	2	3	4	5	6	7	8	9	D.
610	785330	785401	785472	785543	785615	785686	785757	785828	785899	785970	71
611	786041	786112	786183	786254	786325	786396	786467	786538	786609	786680	71
612	786751	786822	786893	786964	787035	787106	787177	787248	787319	787390	71
613	787460	787531	787602	787673	787744	787815	787885	787956	788027	788098	71
614	788168	788239	788310	788381	788451	788522	788593	788663	788734	788804	71
615	788875	788946	789016	789087	789157	789228	789299	789369	789440	789510	71
616	789581	789651	789722	789792	789863	789933	790004	790074	790144	790215	70
617	790285	790356	790426	790496	790567	790637	790707	790778	790848	790918	70
618	790988	791059	791129	791199	791269	791340	791410	791480	791550	791620	70
619	791691	791761	791831	791901	791971	792041	792111	792181	792252	792322	70
620	792392	792462	792532	792602	792672	792742	792812	792882	792952	793022	70
621	793092	793162	793231	793301	793371	793441	793511	793581	793651	793721	70
622	793790	793860	793930	794000	794070	794139	794209	794279	794349	794418	70
623	794488	794558	794627	794697	794767	794836	794906	794976	795045	795115	70
624	795185	795254	795324	795393	795463	795532	795602	795672	795741	795811	70
625	795880	795949	796019	796088	796158	796227	796297	796366	796436	796505	69
626	796574	796644	796713	796782	796852	796921	796990	797060	797129	797198	69
627	797268	797337	797406	797475	797545	797614	797683	797752	797821	797890	69
628	797960	798029	798098	798167	798236	798305	798374	798443	798512	798582	69
629	798651	798720	798789	798858	798927	798996	799065	799134	799203	799272	69
630	799341	799409	799478	799547	799616	799685	799754	799823	799892	799961	69
631	800029	800098	800167	800236	800305	800373	800442	800511	800580	800648	69
632	800717	800786	800854	800923	800992	801061	801129	801198	801266	801335	69
633	801404	801472	801541	801609	801678	801747	801815	801884	801952	802021	69
634	802089	802158	802226	802295	802363	802432	802500	802568	802637	802705	69
635	802774	802842	802910	802979	803047	803116	803184	803252	803321	803389	68
636	803457	803525	803594	803662	803730	803798	803867	803935	804003	804071	68
637	804139	804208	804276	804344	804412	804480	804548	804616	804685	804753	68
638	804821	804889	804957	805025	805093	805161	805229	805297	805365	805433	68
639	805501	805569	805637	805705	805773	805841	805908	805976	806044	806112	68
640	806180	806248	806316	806384	806451	806519	806587	806655	806723	806790	68
641	806858	806926	806994	807061	807129	807197	807264	807332	807400	807467	68
642	807535	807603	807670	807738	807806	807874	807941	808008	808076	808143	68
643	808211	808279	808346	808414	808481	808549	808616	808684	808751	808818	67
644	808886	808953	809021	809088	809156	809223	809290	809358	809425	809492	67
645	809560	809627	809694	809762	809829	809896	809964	810031	810098	810165	67
646	810233	810300	810367	810434	810501	810569	810636	810703	810770	810837	67
647	810904	810971	811039	811106	811173	811240	811307	811374	811441	811508	67
648	811575	811642	811709	811776	811843	811910	811977	812044	812111	812178	67
649	812245	812312	812379	812445	812512	812579	812646	812713	812780	812847	67
650	812913	812980	813047	813114	813181	813247	813314	813381	813448	813514	67
651	813581	813648	813714	813781	813848	813914	813981	814048	814114	814181	67
652	814248	814314	814381	814447	814514	814581	814647	814714	814780	814847	67
653	814913	814980	815046	815113	815179	815246	815312	815378	815445	815511	66
654	815578	815644	815711	815777	815843	815910	815976	816042	816109	816175	66
655	816241	816308	816374	816440	816506	816573	816639	816705	816771	816838	66
656	816904	816970	817036	817102	817169	817235	817301	817367	817433	817499	66
657	817565	817631	817698	817764	817830	817896	817962	818028	818094	818160	66
658	818226	818292	818358	818424	818490	818556	818622	818688	818754	818820	66
659	818885	818951	819017	819083	819149	819215	819281	819346	819412	819478	66
660	819544	819610	819676	819741	819807	819873	819939	820004	820070	820136	66
661	820201	820267	820333	820399	820464	820530	820595	820661	820727	820792	66
662	820858	820924	820989	821055	821120	821186	821251	821317	821382	821448	66
663	821514	821579	821645	821710	821775	821841	821906	821972	822037	822103	65
664	822168	822233	822299	822364	822430	822495	822560	822626	822691	822756	65
No.	0	1	2	3	4	5	6	7	8	9	D.
D.	1	2	3	4	5	6	7	8	9		
65	6	13	19	26	32	39	45	52	58		
66	7	13	20	26	33	40	46	53	59		
67	7	13	20	27	31	40	47	54	60		
68	7	14	20	27	34	41	48	54	61		
D.	1	2	3	4	5	6	7	8	9		
68	7	14	20	27	34	41	48	54	61		
69	7	14	21	28	34	41	48	55	62		
70	7	14	21	28	35	42	49	56	63		
71	7	14	21	28	35	43	50	57	64		

LOGARITHMS OF NUMBERS

No. 6650 to 7199

Log. 822822 to 857272

No.	0	1	2	3	4	5	6	7	8	9	D.
665	822822	822888	822952	823018	823083	823148	823213	823279	823344	823409	65
666	823474	823539	823605	823670	823735	823800	823865	823930	823996	824061	65
667	824126	824191	824256	824321	824386	824451	824516	824581	824646	824711	65
668	824776	824841	824906	824971	825036	825101	825166	825231	825296	825361	65
669	825426	825491	825556	825621	825686	825751	825815	825880	825945	826010	65
670	826075	826140	826204	826269	826334	826399	826464	826528	826593	826658	65
671	826723	826787	826852	826917	826981	827046	827111	827175	827240	827305	65
672	827369	827434	827499	827563	827628	827692	827757	827821	827886	827951	65
673	828015	828080	828144	828209	828273	828338	828402	828467	828531	828595	64
674	828660	828724	828789	828853	828918	828982	829046	829111	829175	829239	64
675	829304	829368	829432	829497	829561	829625	829690	829754	829818	829882	64
676	829947	830011	830075	830139	830204	830268	830332	830396	830460	830525	64
677	830589	830653	830717	830781	830845	830909	830973	831037	831102	831166	64
678	831230	831294	831358	831422	831486	831550	831614	831678	831742	831806	64
679	831870	831934	831998	832062	832126	832189	832253	832317	832381	832445	64
680	832509	832573	832637	832700	832764	832828	832892	832956	833020	833083	64
681	833147	833211	833275	833338	833402	833466	833530	833593	833657	833721	64
682	833784	833848	833912	833975	834039	834103	834166	834230	834294	834357	64
683	834421	834484	834548	834611	834675	834739	834802	834866	834929	834993	64
684	835056	835120	835183	835247	835310	835373	835437	835500	835564	835627	63
685	835691	835754	835817	835881	835944	836007	836071	836134	836197	836261	63
686	836324	836387	836451	836514	836577	836641	836704	836767	836830	836894	63
687	836957	837020	837083	837146	837210	837273	837336	837399	837462	837525	63
688	837588	837651	837715	837778	837841	837904	837967	838030	838093	838156	63
689	838219	838282	838345	838408	838471	838534	838597	838660	838723	838786	63
690	838849	838912	838975	839038	839101	839164	839227	839289	839352	839415	63
691	839478	839541	839604	839667	839729	839792	839855	839918	839981	840043	63
692	840106	840169	840232	840294	840357	840420	840482	840545	840608	840671	63
693	840733	840796	840859	840921	840984	841046	841109	841172	841234	841297	63
694	841359	841422	841485	841547	841610	841672	841735	841797	841860	841922	62
695	841985	842047	842110	842172	842235	842297	842360	842422	842484	842547	62
696	842609	842672	842734	842796	842859	842921	842983	843046	843108	843170	62
697	843233	843295	843357	843420	843482	843544	843606	843669	843731	843793	62
698	843855	843918	843980	844042	844104	844166	844229	844291	844353	844415	62
699	844477	844539	844601	844664	844726	844788	844850	844912	844974	845036	62
700	845098	845160	845222	845284	845346	845408	845470	845532	845594	845656	62
701	845718	845780	845842	845904	845966	846028	846090	846151	846213	846275	62
702	846337	846399	846461	846523	846585	846646	846708	846770	846832	846894	62
703	846955	847017	847079	847141	847202	847264	847326	847388	847449	847511	62
704	847573	847634	847696	847758	847819	847881	847943	848004	848066	848128	62
705	848189	848251	848312	848374	848435	848497	848559	848620	848682	848743	62
706	848805	848866	848928	848989	849051	849112	849174	849235	849297	849358	61
707	849419	849481	849542	849604	849665	849726	849788	849849	849911	849972	61
708	850033	850095	850156	850217	850279	850340	850401	850462	850524	850585	61
709	850646	850707	850769	850830	850891	850952	851014	851075	851136	851197	61
710	851258	851320	851381	851442	851503	851564	851625	851686	851747	851809	61
711	851870	851931	851992	852053	852114	852175	852236	852297	852358	852419	61
712	852480	852541	852602	852663	852724	852785	852846	852907	852968	853029	61
713	853090	853150	853211	853272	853333	853394	853455	853516	853577	853637	61
714	853698	853759	853820	853881	853941	854002	854063	854124	854185	854245	61
715	854306	854367	854428	854488	854549	854610	854670	854731	854792	854852	61
716	854913	854974	855034	855095	855156	855216	855277	855337	855398	855459	61
717	855519	855580	855640	855701	855761	855822	855882	855943	856003	856064	61
718	856124	856185	856245	856306	856366	856427	856487	856548	856608	856668	60
719	856729	856789	856850	856910	856970	857031	857091	857152	857212	857272	60

No.	0	1	2	3	4	5	6	7	8	9	D.
D.	1	2	3	4	5	6	7	8	9		
60	6	12	18	24	30	36	42	48	54		
61	6	12	18	24	30	37	43	49	55		
62	6	12	19	25	31	37	43	50	56		

TABLE 64

719

LOGARITHMS OF NUMBERS

No. 7200 to 7749

Log. 857332 to 889246

No.	0	1	2	3	4	5	6	7	8	9	D.
720	857332	857393	857453	857513	857574	857634	857694	857755	857815	857875	60
721	857935	857995	858056	858116	858176	858236	858297	858357	858417	858477	60
722	858537	858597	858657	858718	858778	858838	858898	858958	859018	859078	60
723	859138	859198	859258	859318	859379	859439	859499	859559	859619	859679	60
724	859739	859799	859859	859918	859978	860038	860098	860158	860218	860278	60
725	860338	860398	860458	860518	860578	860637	860697	860757	860817	860877	60
726	860937	860996	861056	861116	861176	861236	861295	861355	861415	861475	60
727	861534	861594	861654	861714	861773	861833	861893	861952	862012	862072	60
728	862131	862191	862251	862310	862370	862430	862489	862549	862608	862668	60
729	862728	862787	862847	862906	862966	863025	863085	863144	863204	863263	60
730	863323	863382	863442	863501	863561	863620	863680	863739	863799	863858	59
731	863917	863977	864036	864096	864155	864214	864274	864333	864392	864452	59
732	864511	864570	864630	864689	864748	864808	864867	864926	864985	865045	59
733	865124	865183	865242	865302	865361	865420	865479	865539	865598	865657	59
734	865696	865755	865814	865874	865933	865992	866051	866110	866169	866228	59
735	866287	866346	866405	866465	866524	866583	866642	866701	866760	866819	59
736	866878	866937	866996	867055	867114	867173	867232	867291	867350	867409	59
737	867467	867526	867585	867644	867703	867762	867821	867880	867939	867998	59
738	868056	868115	868174	868233	868292	868350	868409	868468	868527	868586	59
739	868644	868703	868762	868821	868879	868938	868997	869056	869114	869173	59
740	869232	869290	869349	869408	869466	869525	869584	869642	869701	869760	59
741	869818	869877	869935	869994	870053	870111	870170	870228	870287	870345	59
742	870404	870462	870521	870579	870638	870696	870755	870813	870872	870930	58
743	870989	871047	871106	871164	871223	871281	871339	871398	871456	871515	58
744	871573	871631	871690	871748	871806	871865	871923	871981	872040	872098	58
745	872156	872215	872273	872331	872389	872448	872506	872564	872622	872681	58
746	872739	872797	872855	872913	872972	873030	873088	873146	873204	873262	58
747	873321	873379	873437	873495	873553	873611	873669	873727	873785	873844	58
748	873902	873960	874018	874076	874134	874192	874250	874308	874366	874424	58
749	874482	874540	874598	874656	874714	874772	874830	874888	874945	875003	58
750	875061	875119	875177	875235	875293	875351	875409	875466	875524	875582	58
751	875640	875698	875756	875813	875871	875929	875987	876045	876102	876160	58
752	876218	876276	876333	876391	876449	876507	876564	876622	876680	876737	58
753	876795	876853	876910	876968	877026	877083	877141	877199	877256	877314	58
754	877371	877429	877487	877544	877602	877659	877717	877774	877832	877889	58
755	877947	878004	878062	878119	878177	878234	878292	878349	878407	878464	57
756	878522	878579	878637	878694	878752	878809	878866	878924	878981	879039	57
757	879096	879153	879211	879268	879325	879383	879440	879497	879555	879612	57
758	879669	879726	879784	879841	879898	879956	880013	880070	880127	880185	57
759	880242	880299	880356	880413	880471	880528	880585	880642	880699	880756	57
760	880814	880871	880928	880985	881042	881099	881156	881213	881271	881328	57
761	881385	881442	881499	881556	881613	881670	881727	881784	881841	881898	57
762	881955	882012	882069	882126	882183	882240	882297	882354	882411	882468	57
763	882525	882581	882638	882695	882752	882809	882866	882923	882980	883037	57
764	883093	883150	883207	883264	883321	883377	883434	883491	883548	883605	57
765	883661	883718	883775	883832	883888	883945	884002	884059	884115	884172	57
766	884229	884285	884342	884399	884455	884512	884569	884625	884682	884739	57
767	884795	884852	884909	884965	885022	885078	885135	885192	885248	885305	57
768	885361	885418	885474	885531	885587	885644	885700	885757	885813	885870	57
769	885926	885983	886039	886096	886152	886200	886257	886312	886378	886434	56
770	886491	886547	886604	886660	886716	886773	886829	886885	886942	886998	56
771	887054	887111	887167	887223	887280	887336	887392	887449	887505	887561	56
772	887617	887674	887730	887786	887842	887898	887955	888011	888067	888123	56
773	888179	888236	888292	888348	888404	888460	888516	888573	888629	888685	56
774	888741	888797	888853	888909	888965	889021	889077	889134	889190	889246	56
No.	0	1	2	3	4	5	6	7	8	9	D.
D.	1	2	3	4	5	6	7	8	9		
56	6	11	17	22	28	34	39	45	50		
57	6	11	17	23	28	34	40	46	51		
58	6	12	17	23	29	35	41	46	52		
59	6	12	18	24	29	35	41	47	53		
60	5	12	18	24	30	36	42	48	54		

LOGARITHMS OF NUMBERS

No. 7750 to 8299										Log 889302 to 919026													
No.	0	1	2	3	4	5	6	7	8	9	D.	No.	0	1	2	3	4	5	6	7	8	9	D.
775	889302	889358	889414	889470	889526	889582	889638	889694	889750	889806	56	919026	919082	919138	919194	919250	919306	919362	919418	919474	919530	919586	57
776	889862	889918	889974	890030	890086	890141	890197	890253	890309	890365	56	919642	919698	919754	919810	919866	919922	919978	920034	920090	920146	920202	57
777	890421	890477	890533	890589	890645	890700	890756	890812	890868	890924	56	920258	920314	920370	920426	920482	920538	920594	920650	920706	920762	920818	57
778	890980	891035	891091	891147	891203	891259	891314	891370	891426	891482	56	920874	920930	920986	921042	921098	921154	921210	921266	921322	921378	921434	57
779	891537	891593	891649	891705	891760	891816	891872	891928	891983	892039	56	921490	921546	921602	921658	921714	921770	921826	921882	921938	921994	922050	57
780	892095	892150	892206	892262	892317	892373	892429	892484	892540	892595	56	922106	922162	922218	922274	922330	922386	922442	922498	922554	922610	922666	57
781	892651	892707	892762	892818	892873	892929	892985	893040	893096	893151	56	922722	922778	922834	922890	922946	922999	923055	923111	923167	923223	923279	57
782	893207	893262	893318	893373	893429	893484	893540	893595	893651	893706	56	923335	923391	923447	923503	923559	923615	923671	923727	923783	923839	923895	57
783	893762	893817	893873	893928	893984	894039	894094	894150	894205	894261	55	923951	924007	924063	924119	924175	924231	924287	924343	924399	924455	924511	56
784	894316	894371	894427	894482	894538	894593	894648	894704	894759	894814	55	924567	924623	924679	924735	924791	924847	924903	924959	925015	925071	925127	56
785	894870	894925	894980	895036	895091	895146	895201	895257	895312	895367	55	925183	925239	925295	925351	925407	925463	925519	925575	925631	925687	925743	56
786	895423	895478	895533	895588	895644	895699	895754	895809	895864	895920	55	925799	925855	925911	925967	926023	926079	926135	926191	926247	926303	926359	56
787	895975	896030	896085	896140	896195	896251	896306	896361	896416	896471	55	926385	926441	926497	926553	926609	926665	926721	926777	926833	926889	926945	56
788	896526	896581	896636	896692	896747	896802	896857	896912	896967	897022	55	926971	927027	927083	927139	927195	927251	927307	927363	927419	927475	927531	56
789	897077	897132	897187	897242	897297	897352	897407	897462	897517	897572	55	927587	927643	927699	927755	927811	927867	927923	927979	928035	928091	92	

TABLE 64

LOGARITHMS OF NUMBERS

No. 8300 to 8849

Log. 919078 to 946894

No.	0	1	2	3	4	5	6	7	8	9	D.
830	919078	919130	919183	919235	919287	919340	919392	919444	919496	919549	52
831	919601	919653	919706	919758	919810	919862	919914	919967	920019	920071	52
832	920123	920176	920228	920280	920332	920384	920436	920489	920541	920593	52
833	920645	920697	920749	920801	920853	920906	920958	921010	921062	921114	52
834	921166	921218	921270	921322	921374	921426	921478	921530	921582	921634	52
835	921686	921738	921790	921842	921894	921946	921998	922050	922102	922154	52
836	922206	922258	922310	922362	922414	922466	922518	922570	922622	922674	52
837	922725	922777	922829	922881	922933	922985	923037	923089	923140	923192	52
838	923244	923296	923348	923399	923451	923503	923555	923607	923658	923710	52
839	923702	923814	923865	923917	923969	924021	924072	924124	924176	924228	52
840	924279	924331	924383	924434	924486	924538	924589	924641	924693	924744	52
841	924796	924848	924899	924951	925003	925054	925106	925157	925209	925261	52
842	925312	925364	925415	925467	925518	925570	925621	925673	925725	925776	52
843	925828	925879	925931	925982	926034	926085	926137	926188	926240	926291	51
844	926342	926394	926445	926497	926548	926600	926651	926702	926754	926805	51
845	926857	926908	926959	927011	927062	927114	927165	927216	927268	927319	51
846	927370	927422	927473	927524	927576	927627	927678	927730	927781	927832	51
847	927883	927935	927986	928037	928088	928140	928191	928242	928293	928345	51
848	928396	928447	928498	928549	928601	928652	928703	928754	928805	928857	51
849	928908	928959	929010	929061	929112	929163	929215	929266	929317	929368	51
850	929419	929470	929521	929572	929623	929674	929725	929776	929827	929879	51
851	929930	929981	930032	930083	930134	930185	930236	930287	930338	930389	51
852	930440	930491	930542	930593	930643	930694	930745	930796	930847	930898	51
853	930949	931000	931051	931102	931153	931203	931254	931305	931356	931407	51
854	931458	931509	931560	931610	931661	931712	931763	931814	931865	931915	51
855	931966	932017	932068	932118	932169	932220	932271	932322	932372	932423	51
856	932474	932524	932575	932626	932677	932727	932778	932829	932879	932930	51
857	932981	933031	933082	933133	933183	933234	933285	933335	933386	933437	51
858	933487	933538	933589	933639	933690	933740	933791	933841	933892	933943	51
859	933993	934044	934094	934145	934195	934246	934296	934347	934397	934448	51
860	934498	934549	934599	934650	934700	934751	934801	934852	934902	934953	50
861	935003	935054	935104	935154	935205	935255	935306	935356	935406	935457	50
862	935507	935558	935608	935658	935709	935759	935809	935860	935910	935960	50
863	936011	936061	936111	936162	936212	936262	936313	936363	936413	936463	50
864	936514	936564	936614	936665	936715	936765	936815	936865	936916	936966	50
865	937016	937066	937117	937167	937217	937267	937317	937367	937418	937468	50
866	937518	937568	937618	937668	937718	937768	937819	937869	937919	937969	50
867	938019	938069	938119	938169	938219	938269	938319	938370	938420	938470	50
868	938520	938570	938620	938670	938720	938770	938820	938870	938920	938970	50
869	939020	939070	939120	939170	939220	939270	939320	939370	939420	939470	50
870	939519	939569	939619	939669	939719	939769	939819	939869	939918	939968	50
871	940018	940068	940118	940168	940218	940267	940317	940367	940417	940467	50
872	940516	940566	940616	940666	940716	940765	940815	940865	940915	940964	50
873	941014	941064	941114	941163	941213	941263	941313	941362	941412	941462	50
874	941511	941561	941611	941660	941710	941760	941809	941859	941909	941958	50
875	942008	942058	942107	942157	942207	942256	942306	942355	942405	942455	50
876	942504	942554	942603	942653	942702	942752	942801	942851	942901	942950	50
877	943000	943049	943099	943148	943198	943247	943297	943346	943396	943445	49
878	943495	943544	943593	943643	943692	943742	943791	943841	943890	943939	49
879	943989	944038	944088	944137	944186	944236	944285	944335	944384	944433	49
880	944483	944532	944581	944631	944680	944729	944779	944828	944877	944927	49
881	944976	945025	945074	945124	945173	945222	945272	945321	945370	945419	49
882	945469	945518	945567	945616	945665	945715	945764	945813	945862	945912	49
883	945961	946010	946059	946108	946157	946207	946256	946305	946354	946403	49
884	946452	946501	946551	946600	946649	946698	946747	946796	946845	946894	49

No.	0	1	2	3	4	5	6	7	8	9	D.
D.	1	2	3	4	5	6	7	8	9		
49	5	10	15	20	24	29	34	39	44	49	
50	5	10	15	20	25	30	35	40	45	50	

LOGARITHMS OF NUMBERS

No. 8850 to 9419											Log. 946943 to 974005											
No.	0	1	2	3	4	5	6	7	8	9	D.											
885	946943	946992	947041	947090	947140	947189	947238	947287	947336	947385	49											
886	947434	947483	947532	947581	947630	947679	947728	947777	947826	947875	49											
887	947924	947973	948022	948070	948119	948168	948217	948266	948315	948364	49											
888	948413	948462	948511	948560	948609	948657	948706	948755	948804	948853	49											
889	948902	948951	948999	949048	949097	949146	949195	949244	949292	949341	49											
890	949390	949439	949488	949536	949585	949634	949683	949732	949780	949829	49											
891	949878	949926	949975	950024	950073	950121	950170	950219	950267	950316	49											
892	950365	950414	950462	950511	950560	950608	950657	950706	950754	950803	49											
893	950851	950900	950949	950997	951046	951095	951143	951192	951240	951289	49											
894	951338	951386	951435	951483	951532	951580	951629	951677	951726	951775	49											
895	951823	951872	951920	951969	952017	952066	952114	952163	952211	952260	48											
896	952308	952356	952405	952453	952502	952550	952599	952647	952696	952744	48											
897	952792	952841	952889	952938	952986	953034	953083	953131	953180	953228	48											
898	953276	953325	953373	953421	953470	953518	953566	953615	953663	953711	48											
899	953760	953808	953856	953905	953953	954001	954049	954098	954146	954194	48											
900	954243	954291	954339	954387	954435	954483	954532	954580	954628	954677	48											
901	954725	954773	954821	954869	954918	954966	955014	955062	955110	955158	48											
902	955207	955255	955303	955351	955399	955447	955495	955543	955592	955640	48											
903	955688	955736	955784	955832	955880	955928	955976	956024	956072	956120	48											
904	956168	956216	956265	956313	956361	956409	956457	956505	956553	956601	48											
905	956649	956697	956745	956793	956840	956888	956936	956984	957032	957080	48											
906	957128	957176	957224	957272	957320	957368	957416	957464	957512	957559	48											
907	957607	957655	957703	957751	957799	957847	957894	957942	957990	958038	48											
908	958086	958134	958181	958229	958277	958325	958373	958421	958468	958516	48											
909	958564	958612	958659	958707	958755	958803	958850	958898	958946	958994	48											
910	959041	959089	959137	959185	959232	959280	959328	959375	959423	959471	48											
911	959518	959566	959614	959661	959709	959757	959804	959852	959900	959947	48											
912	959995	960042	960090	960138	960185	960233	960280	960328	960376	960423	48											
913	960471	960518	960566	960613	960661	960709	960756	960804	960851	960899	48											
914	960946	960994	961041	961089	961136	961184	961231	961279	961326	961374	47											
915	961421	961469	961516	961563	961611	961658	961706	961753	961801	961848	47											
916	961895	961943	961990	962038	962085	962132	962180	962227	962275	962322	47											
917	962369	962417	962464	962511	962559	962606	962653	962701	962748	962795	47											
918	962843	962890	962937	962985	963032	963079	963126	963174	963221	963268	47											
919	963316	963363	963410	963457	963504	963552	963599	963646	963693	963741	47											
920	963788	963835	963882	963929	963977	964024	964071	964118	964165	964212	47											
921	964260	964307	964354	964401	964448	964495	964542	964590	964637	964684	47											
922	964731	964778	964825	964872	964919	964966	965013	965061	965108	965155	47											
923	965202	965249	965296	965343	965390	965437	965484	965531	965578	965625	47											
924	965672	965719	965766	965813	965860	965907	965954	966001	966048	966095	47											
925	966142	966189	966236	966283	966329	966376	966423	966470	966517	966564	47											
926	966611	966658	966705	966752	966799	966845	966892	966939	966986	967033	47											
927	967080	967127	967173	967220	967267	967314	967361	967408	967454	967501	47											
928	967548	967595	967642	967688	967735	967782	967829	967875	967922	967969	47											
929	968016	968063	968109	968156	968203	968249	968296	968343	968390	968436	47											
930	968483	968530	968576	968623	968670	968716	968763	968810	968856	968903	47											
931	968950	968996	969043	969090	969136	969183	969229	969276	969323	969369	47											
932	969416	969463	969509	969556	969602	969649	969695	969742	969789	969835	47											
933	969882	969928	969975	970021	970068	970114	970161	970207	970254	970300	47											
934	970347	970393	970440	970486	970533	970579	970626	970672	970719	970765	46											
935	970812	970858	970904	970951	970997	971044	971090	971137	971183	971229	46											
936	971276	971322	971369	971415	971461	971508	971554	971601	971647	971693	46											
937	971740	971786	971832	971879	971925	971971	972018	972064	972110	972157	46											
938	972203	972249	972295	972342	972388	972434	972481	972527	972573	972619	46											
939	972666	972712	972758	972804	972851	972897	972943	972989	973035	973082	46											
940	973128	973174	973220	973266	973313	973359	973405	973451	973497	973543	46											
941	973590	973636	973682	973728	973774	973820	973866	973913	973959	974005	46											
No.	0	1	2	3	4	5	6	7	8	9	D.											
D.	1	2	3	4	5	6	7	8	9			D.	1	2	3	4	5	6	7	8	9	
46	5	9	14	18	23	28	32	37	41			48	5	10	14	19	24	29	34	38	43	
47	5	9	14	19	23	28	33	38	42			48	5	10	15	20	24	29	34	39	44	

LOGARITHMS OF NUMBERS

No. 9420 to 9999

Log. 974051 to 999957

No.	0	1	2	3	4	5	6	7	8	9	D.
942	974051	974097	974143	974189	974235	974281	974327	974374	974420	974466	46
943	974512	974558	974604	974650	974696	974742	974788	974834	974880	974926	46
944	974972	975018	975064	975110	975156	975202	975248	975294	975340	975386	46
945	975432	975478	975524	975570	975616	975662	975707	975753	975799	975845	46
946	975891	975937	975983	976029	976075	976121	976167	976212	976258	976304	46
947	976350	976396	976442	976488	976533	976579	976625	976671	976717	976763	46
948	976808	976854	976900	976946	976992	977037	977083	977129	977175	977220	46
949	977266	977312	977358	977403	977449	977495	977541	977586	977632	977678	46
950	977724	977769	977815	977861	977906	977952	977998	978043	978089	978135	46
951	978181	978226	978272	978317	978363	978409	978454	978500	978546	978591	46
952	978637	978683	978728	978774	978819	978865	978911	978956	979002	979047	46
953	979093	979138	979184	979230	979275	979321	979366	979412	979457	979503	46
954	979548	979594	979639	979685	979730	979776	979821	979867	979912	979958	46
955	980003	980049	980094	980140	980185	980231	980276	980322	980367	980412	45
956	980458	980503	980549	980594	980640	980685	980730	980776	980821	980867	45
957	980912	980957	981003	981048	981093	981139	981184	981229	981275	981320	45
958	981366	981411	981456	981501	981547	981592	981637	981683	981728	981773	45
959	981819	981864	981909	981954	982000	982045	982090	982135	982181	982226	45
960	982271	982316	982362	982407	982452	982497	982543	982588	982633	982678	45
961	982723	982769	982814	982859	982904	982949	982994	983040	983085	983130	45
962	983175	983220	983265	983310	983356	983401	983446	983491	983536	983581	45
963	983626	983671	983716	983762	983807	983852	983897	983942	983987	984032	45
964	984077	984122	984167	984212	984257	984302	984347	984392	984437	984482	45
965	984527	984572	984617	984662	984707	984752	984797	984842	984887	984932	45
966	984977	985022	985067	985112	985157	985202	985247	985292	985337	985382	45
967	985426	985471	985516	985561	985606	985651	985696	985741	985786	985830	45
968	985875	985920	985965	986010	986055	986100	986144	986189	986234	986279	45
969	986324	986369	986413	986458	986503	986548	986593	986637	986682	986727	45
970	986772	986817	986861	986906	986951	986996	987040	987085	987130	987175	45
971	987219	987264	987309	987353	987398	987443	987488	987532	987577	987622	45
972	987666	987711	987756	987800	987845	987890	987934	987979	988024	988068	45
973	988113	988157	988202	988247	988291	988336	988381	988425	988470	988514	45
974	988559	988604	988648	988693	988737	988782	988826	988871	988916	988960	45
975	989005	989049	989094	989138	989183	989227	989272	989316	989361	989405	45
976	989450	989494	989539	989583	989628	989672	989717	989761	989806	989850	44
977	989895	989939	989983	990028	990072	990117	990161	990206	990250	990294	44
978	990339	990383	990428	990472	990516	990561	990605	990650	990694	990738	44
979	990783	990827	990871	990916	990960	991004	991049	991093	991137	991182	44
980	991226	991270	991315	991359	991403	991448	991492	991536	991580	991625	44
981	991669	991713	991758	991802	991846	991890	991935	991979	992023	992067	44
982	992111	992156	992200	992244	992288	992333	992377	992421	992465	992509	44
983	992554	992598	992642	992686	992730	992774	992819	992863	992907	992951	44
984	992995	993039	993083	993127	993172	993216	993260	993304	993348	993392	44
985	993436	993480	993524	993568	993613	993657	993701	993745	993789	993833	44
986	993877	993921	993965	994009	994053	994097	994141	994185	994229	994273	44
987	994317	994361	994405	994449	994493	994537	994581	994625	994669	994713	44
988	994757	994801	994845	994889	994933	994977	995021	995065	995108	995152	44
989	995196	995240	995284	995328	995372	995416	995460	995504	995547	995591	44
990	995635	995679	995723	995767	995811	995854	995898	995942	995986	996030	44
991	996074	996117	996161	996205	996249	996293	996337	996381	996424	996468	44
992	996512	996555	996599	996643	996687	996731	996774	996818	996862	996907	44
993	996949	996993	997037	997080	997124	997168	997212	997255	997299	997343	44
994	997386	997430	997474	997517	997561	997605	997648	997692	997736	997779	44
995	997823	997867	997910	997954	997998	998041	998085	998129	998172	998216	44
996	998259	998303	998347	998390	998434	998477	998521	998564	998608	998652	44
997	998695	998739	998782	998826	998869	998913	998956	999000	999043	999087	44
998	999131	999174	999218	999261	999305	999348	999392	999435	999479	999522	44
999	999565	999609	999652	999696	999739	999783	999826	999870	999913	999957	43
No.	0	1	2	3	4	5	6	7	8	9	D.
D.	1	2	3	4	5	6	7	8	9		
43	4	9	13	17	21	26	30	34	39		
44	4	9	13	18	22	26	31	35	40		

SPHEROIDAL TABLES. COMPRESSION $\frac{1}{298}$									
Latitude.					Longitude.				
Latitude.	Length of one degree in statute miles.	Length in feet of a			Latitude.	Length of one degree in minutes of latitude or nautical miles.	Length in feet of a		
		Degree.	Minute.	Second.			Degree.	Minute.	Second.
0	68.704	362755.6	6045.93	100.77	0	60.410	365233.7	6087.23	101.454
2	68.704	362760.1	6046.00	100.77	2	60.373	365012.7	6083.54	101.392
4	68.707	362773.6	6046.23	100.77	4	60.261	364350.0	6072.50	101.208
6	68.711	362795.9	6046.60	100.78	6	60.074	363246.3	6054.11	100.902
8	68.717	362827.1	6047.12	100.79	8	59.814	361703.0	6028.38	100.473
10	68.725	362866.9	6047.78	100.80	10	59.480	359721.7	5995.36	99.923
12	68.734	362815.2	6048.59	100.81	12	59.072	357304.8	5955.08	99.251
14	68.745	362971.8	6049.53	100.83	14	58.592	354455.1	5907.59	98.460
16	68.757	363036.3	6050.61	100.84	16	58.040	351175.7	5852.93	97.549
18	68.771	363108.4	6051.81	100.85	18	57.416	347470.5	5791.18	96.520
20	68.786	363187.9	6053.13	100.89	20	56.722	343343.7	5722.40	95.373
22	68.801	363274.3	6054.57	100.91	22	55.958	338800.1	5646.67	94.111
24	68.819	363367.2	6056.12	100.94	24	55.125	333845.0	5564.08	92.735
26	68.838	363466.2	6057.77	100.96	26	54.225	328484.1	5474.74	91.245
28	68.858	363570.8	6059.51	100.99	28	53.259	322723.6	5378.73	89.645
30	68.879	363680.5	6061.34	101.02	30	52.228	316570.3	5276.17	87.936
32	68.900	363794.8	6063.25	101.05	32	51.133	310031.2	5167.19	86.119
34	68.923	363913.1	6065.22	101.09	34	49.976	303114.2	5051.90	84.198
36	68.946	364034.9	6067.25	101.12	36	48.758	295827.2	4930.45	82.174
38	68.970	364159.5	6069.33	101.16	38	47.481	288178.9	4802.98	80.050
40	68.994	364286.3	6071.44	101.19	40	46.146	280178.2	4669.64	77.817
42	69.018	364414.9	6073.58	101.23	42	44.757	271834.7	4530.58	75.509
44	69.042	364544.4	6075.74	101.26	44	43.313	263158.3	4385.97	73.100
46	69.067	364674.4	6077.91	101.30	46	41.817	254159.2	4235.99	70.600
48	69.092	364804.1	6080.07	101.33	48	40.270	244848.2	4080.80	68.013
50	69.116	364932.9	6082.22	101.37	50	38.676	235236.5	3920.61	65.343
52	69.140	365060.2	6084.34	101.41	52	37.035	225335.5	3755.59	62.593
54	69.164	365185.4	6086.42	101.44	54	35.350	215157.2	3585.95	59.706
56	69.187	365307.9	6088.47	101.47	56	33.623	204714.0	3411.90	56.865
58	69.210	365427.0	6090.45	101.51	58	31.856	19.018.3	3233.64	53.891
60	69.231	365542.2	6092.37	101.54	60	30.051	183083.3	3051.39	50.856
62	69.252	365652.9	6094.22	101.57	62	28.211	171922.1	2865.37	47.756
64	69.272	365758.5	6095.98	101.60	64	26.337	160548.6	2675.81	44.597
66	69.291	365858.6	6097.64	101.63	66	24.432	148976.3	2482.94	41.382
68	69.309	365952.7	6099.21	101.65	68	22.498	137219.7	2287.00	38.110
70	69.326	366040.2	6100.67	101.68	70	20.536	125293.2	2088.22	34.804
72	69.343	366120.7	6102.01	101.70	72	18.553	113211.4	1886.86	31.448
74	69.355	366193.9	6103.23	101.72	74	16.547	100989.1	1683.15	28.053
76	69.367	366259.6	6104.32	101.74	76	14.521	88641.6	1477.36	24.623
78	69.378	366316.7	6105.28	101.75	78	12.478	76184.0	1269.73	21.162
80	69.387	366365.8	6106.10	101.77	80	10.421	63631.8	1060.53	17.676
82	69.395	366406.3	6106.77	101.78	82	8.352	51000.6	850.01	14.167
84	69.401	366438.0	6107.30	101.79	84	6.272	38306.1	638.44	10.641
86	69.405	366460.7	6107.63	101.79	86	4.186	25563.9	426.07	7.101
88	69.408	366474.4	6107.91	101.80	88	2.094	12789.9	213.17	3.553
90	69.409	366479.0	6107.98	101.80	90	0.0	0.0	0.0	0.0

* The figures in this column, divided by 6, will give the length, in cables, of a minute of longitude in its corresponding latitude, thus: in latitude $84^{\circ} 6' 57'' + 6 = 105$ cable in a minute of longitude.

NOTE.—These tables have been calculated for every ten minutes of latitude, and are published by J. D. Potter, 145 MINNESOTA, N.

TABLE 65.

NATURAL SINES, COSINES, &c.							
•	Sine.	Cosec.	Tangent.	Cotang.	Secant.	Cosine.	•
0	•0000	Infinite	•0000	Infinite	1•0000	1•0000	90
1	•0175	57•2987	•0175	57•2900	1•0002	•9998	89
2	•0349	28•6537	•0349	28•6363	1•0006	•9994	88
3	•0523	19•1073	•0524	19•0811	1•0014	•9986	87
4	•0698	14•3356	•0699	14•3007	1•0024	•9976	86
5	•0872	11•4737	•0875	11•4301	1•0038	•9962	85
6	•1045	9•5668	•1051	9•5144	1•0055	•9945	84
7	•1219	8•2055	•1228	8•1443	1•0075	•9925	83
8	•1392	7•1853	•1405	7•1154	1•0098	•9903	82
9	•1564	6•3925	•1584	6•3138	1•0125	•9877	81
10	•1736	5•7588	•1763	5•0713	1•0154	•9848	80
11	•1908	5•2408	•1944	5•1446	1•0187	•9816	79
12	•2079	4•8097	•2126	4•7046	1•0223	•9781	78
13	•2250	4•4454	•2309	4•3315	1•0263	•9744	77
14	•2419	4•1336	•2493	4•0108	1•0306	•9703	76
15	•2588	3•8037	•2679	3•7321	1•0353	•9659	75
16	•2756	3•6280	•2867	3•4874	1•0403	•9613	74
17	•2924	3•4203	•3057	3•2709	1•0457	•9563	73
18	•3090	3•2361	•3249	3•0777	1•0515	•9511	72
19	•3256	3•0716	•3443	2•9042	1•0576	•9455	71
20	•3420	2•9238	•3640	2•7475	1•0642	•9397	70
21	•3584	2•7904	•3839	2•6051	1•0711	•9336	69
22	•3746	2•6695	•4040	2•4751	1•0785	•9272	68
23	•3907	2•5593	•4245	2•3559	1•0864	•9205	67
24	•4067	2•4586	•4452	2•2460	1•0946	•9135	66
25	•4226	2•3662	•4663	2•1445	1•1034	•9063	65
26	•4384	2•2812	•4877	2•0503	1•1126	•8988	64
27	•4540	2•2027	•5095	1•9626	1•1223	•8910	63
28	•4695	2•1301	•5317	1•8807	1•1326	•8829	62
29	•4848	2•0627	•5543	1•8040	1•1434	•8746	61
30	•5000	2•0000	•5774	1•7320	1•1547	•8660	60
31	•5150	1•9416	•6009	1•6643	1•1666	•8572	59
32	•5299	1•8871	•6249	1•6003	1•1792	•8480	58
33	•5446	1•8361	•6494	1•5399	1•1924	•8387	57
34	•5592	1•7883	•6745	1•4826	1•2062	•8290	56
35	•5736	1•7434	•7002	1•4281	1•2208	•8192	55
36	•5878	1•7013	•7265	1•3764	1•2361	•8090	54
37	•6018	1•6616	•7536	1•3270	1•2521	•7986	53
38	•6157	1•6243	•7813	1•2799	1•2690	•7880	52
39	•6293	1•5890	•8098	1•2349	1•2868	•7771	51
40	•6428	1•5572	•8391	1•1918	1•3054	•7660	50
41	•6561	1•5243	•8693	1•1504	1•3250	•7547	49
42	•6691	1•4945	•9004	1•1106	1•3456	•7431	48
43	•6820	1•4663	•9325	1•0724	1•3673	•7314	47
44	•6947	1•4396	•9657	1•0355	1•3902	•7193	46
45	•7071	1•4142	1•0000	1•0000	1•4142	•7071	45
•	Cosine.	Secant.	Cotang.	Tangent.	Cosec.	Sine.	•

LOG SINES OF SMALL ARCS TO EACH SECOND

"	0° 0'	0° 1'	0° 2'	0° 3'	0° 4'	0° 5'	0° 6'	0° 7'	0° 8'	0° 9'	"
0	— ∞	46373	76476	6'94085	06579	16270	24188	30882	36682	41797	60
1	4'68557	47090	76836	6'94325	06759	16414	24308	30986	36772	41877	59
2	4'98660	47797	77193	6'94565	06939	16558	24428	31089	36862	41957	58
3	5'16270	48492	77548	6'94803	07118	16702	24548	31191	36952	42037	57
4	5'28763	49175	77900	6'95039	07296	16845	24668	31294	37042	42117	56
5	5'38454	49849	78248	6'95275	07474	16987	24787	31396	37132	42197	55
6	5'46373	50512	78595	6'95509	07651	17130	24906	31498	37221	42277	54
7	5'53067	51165	78938	6'95742	07827	17271	25024	31600	37310	42356	53
8	5'58866	51808	79278	6'95973	08003	17413	25142	31702	37399	42435	52
9	5'63982	52442	79616	6'96204	08177	17553	25260	31803	37488	42515	51
10	5'68557	53067	79952	6'96433	08351	17694	25378	31904	37577	42594	50
11	5'72697	53683	80285	6'96661	08525	17834	25495	32005	37666	42673	49
12	5'76476	54291	80615	6'96888	08698	17973	25612	32106	37754	42751	48
13	5'79952	54890	80943	6'97113	08870	18112	25728	32206	37842	42830	47
14	5'83170	55481	81268	6'97338	09041	18250	25845	32306	37930	42908	46
15	5'86167	56064	81591	6'97561	09211	18389	25961	32406	38018	42987	45
16	5'88969	56639	81911	6'97783	09381	18526	26076	32506	38106	43065	44
17	5'91602	57207	82230	6'98004	09551	18663	26192	32606	38193	43143	43
18	5'94085	57767	82545	6'98224	09719	18800	26307	32705	38280	43221	42
19	5'96433	58320	82859	6'98443	09887	18937	26421	32804	38367	43299	41
20	5'98660	58866	83170	6'98660	10055	19072	26536	32903	38454	43376	40
21	6'00779	59406	83479	6'98877	10222	19208	26650	33001	38541	43454	39
22	6'02800	59939	83786	6'99093	10388	19343	26764	33100	38628	43531	38
23	6'04730	60465	84091	6'99307	10553	19478	26877	33198	38714	43608	37
24	6'06579	60985	84394	6'99520	10718	19612	26991	33296	38800	43685	36
25	6'08351	61499	84694	6'99733	10882	19746	27104	33393	38887	43762	35
26	6'10055	62007	84993	6'99944	11046	19879	27216	33491	38972	43839	34
27	6'11694	62509	85289	7'00155	11209	20012	27329	33588	39058	43916	33
28	6'13273	63006	85584	7'00364	11371	20145	27441	33685	39144	43992	32
29	6'14797	63496	85876	7'00572	11533	20277	27552	33782	39229	44069	31
30	6'16270	63982	86167	7'00779	11694	20409	27664	33879	39314	44145	30
31	6'17694	64462	86455	7'00986	11854	20540	27775	33975	39400	44221	29
32	6'19072	64936	86742	7'01191	12014	20671	27886	34071	39484	44297	28
33	6'20409	65406	87027	7'01395	12174	20802	27997	34167	39569	44373	27
34	6'21705	65870	87310	7'01599	12333	20932	28107	34263	39654	44449	26
35	6'22964	66330	87591	7'01801	12491	21062	28217	34359	39738	44524	25
36	6'24188	66785	87870	7'02003	12648	21191	28327	34454	39822	44600	24
37	6'25378	67235	88147	7'02203	12805	21320	28437	34549	39906	44675	23
38	6'26536	67680	88423	7'02403	12962	21449	28546	34644	39990	44750	22
39	6'27664	68121	88697	7'02602	13118	21577	28655	34739	40074	44825	21
40	6'28763	68557	88969	7'02800	13273	21705	28763	34833	40158	44900	20
41	6'29836	68990	89240	7'02997	13428	21833	28872	34928	40241	44975	19
42	6'30882	69418	89509	7'03193	13582	21960	28980	35022	40324	45050	18
43	6'31904	69841	89776	7'03388	13736	22087	29088	35116	40408	45124	17
44	6'32903	70261	90042	7'03582	13889	22213	29196	35209	40491	45199	16
45	6'33879	70676	90306	7'03776	14042	22339	29303	35303	40573	45273	15
46	6'34833	71088	90568	7'03968	14194	22465	29410	35396	40656	45347	14
47	6'35767	71496	90829	7'04160	14346	22590	29517	35489	40739	45421	13
48	6'36682	71900	91088	7'04351	14497	22715	29623	35582	40821	45495	12
49	6'37577	72300	91346	7'04541	14647	22840	29730	35675	40903	45569	11
50	6'38454	72697	91602	7'04730	14797	22964	29836	35767	40985	45643	10
51	6'39315	73090	91857	7'04919	14947	23088	29942	35860	41067	45716	9
52	6'40158	73479	92110	7'05106	15096	23211	30047	35952	41149	45790	8
53	6'40985	73865	92362	7'05293	15244	23335	30152	36044	41230	45863	7
54	6'41797	74248	92612	7'05479	15392	23458	30257	36135	41312	45936	6
55	6'42594	74627	92861	7'05664	15540	23580	30362	36227	41393	46009	5
56	6'43376	75003	93109	7'05849	15687	23702	30467	36318	41474	46082	4
57	6'44145	75376	93355	7'06032	15833	23824	30571	36409	41555	46155	3
58	6'44900	75746	93599	7'06215	15979	23946	30675	36500	41636	46228	2
59	6'45643	76112	93843	7'06397	16125	24067	30779	36591	41716	46300	1
(60)	6'46373	76476	94085	7'06579	16270	24188	30882	36682	41797	46373	0
"	80° 59'	80° 58'	80° 57'	80° 56'	80° 55'	80° 54'	80° 53'	80° 52'	80° 51'	80° 50'	"

COSINE

LOG. SINES OF SMALL ARCS TO EACH SECOND

//	1° 10'	1° 11'	1° 12'	1° 13'	1° 14'	1° 15'	1° 16'	1° 17'	1° 18'	1° 19'	//
0	46373	50512	54291	57767	60985	63982	66784	69417	71900	74248	00
1	46445	50578	54351	57822	61037	64030	66830	69460	71940	74286	01
2	46517	50643	54411	57878	61089	64078	66875	69502	71980	74324	02
3	46589	50709	54471	57934	61140	64126	66920	69545	72020	74362	03
4	46661	50774	54531	57989	61192	64174	66965	69587	72060	74400	04
5	46733	50840	54591	58044	61243	64222	67010	69630	72100	74438	05
6	46805	50905	54651	58100	61294	64270	67055	69672	72140	74476	06
7	46876	50970	54711	58155	61346	64318	67100	69714	72180	74514	07
8	46948	51035	54771	58210	61397	64366	67145	69757	72220	74551	08
9	47019	51100	54830	58265	61448	64414	67190	69799	72260	74589	09
10	47090	51165	54890	58320	61499	64461	67234	69841	72300	74627	10
11	47162	51230	54949	58375	61550	64509	67279	69883	72340	74665	11
12	47233	51294	55008	58430	61601	64557	67324	69925	72380	74703	12
13	47303	51359	55068	58485	61652	64604	67369	69967	72419	74740	13
14	47374	51423	55127	58539	61703	64652	67413	70009	72459	74778	14
15	47445	51488	55186	58594	61754	64699	67458	70051	72499	74815	15
16	47515	51552	55245	58649	61805	64747	67502	70093	72538	74853	16
17	47586	51616	55304	58703	61855	64794	67547	70135	72578	74891	17
18	47656	51680	55363	58758	61906	64842	67591	70177	72618	74928	18
19	47726	51744	55422	58812	61957	64889	67636	70219	72657	74966	19
20	47797	51808	55481	58866	62007	64936	67680	70261	72697	75003	20
21	47867	51872	55539	58921	62058	64983	67724	70302	72736	75040	21
22	47936	51936	55598	58975	62108	65030	67768	70344	72775	75078	22
23	48006	51999	55656	59029	62158	65078	67813	70386	72815	75115	23
24	48076	52063	55715	59083	62209	65125	67857	70427	72854	75153	24
25	48145	52126	55773	59137	62259	65172	67901	70469	72894	75190	25
26	48215	52190	55831	59191	62309	65218	67945	70510	72933	75227	26
27	48284	52253	55889	59245	62359	65265	67989	70552	72972	75264	27
28	48353	52316	55948	59299	62409	65312	68033	70593	73011	75302	28
29	48422	52379	56006	59352	62459	65359	68077	70635	73050	75339	29
30	48491	52442	56064	59406	62509	65406	68121	70676	73090	75376	30
31	48560	52505	56121	59459	62559	65452	68165	70718	73129	75413	31
32	48629	52568	56179	59513	62609	65499	68208	70759	73168	75450	32
33	48698	52631	56237	59566	62659	65545	68252	70800	73207	75487	33
34	48766	52693	56295	59620	62708	65592	68296	70841	73246	75524	34
35	48835	52756	56352	59673	62758	65638	68340	70883	73285	75561	35
36	48903	52818	56410	59726	62808	65685	68383	70924	73324	75598	36
37	48971	52881	56467	59780	62857	65731	68427	70965	73363	75635	37
38	49039	52943	56524	59833	62907	65778	68470	71006	73401	75672	38
39	49107	53005	56582	59886	62956	65824	68514	71047	73440	75709	39
40	49175	53067	56639	59939	63006	65870	68557	71088	73479	75745	40
41	49243	53129	56696	59992	63055	65916	68601	71129	73518	75782	41
42	49311	53191	56753	60045	63104	65962	68644	71170	73557	75819	42
43	49379	53253	56810	60097	63153	66008	68687	71211	73595	75856	43
44	49446	53315	56867	60150	63203	66055	68731	71251	73634	75892	44
45	49513	53376	56924	60203	63252	66101	68774	71292	73673	75929	45
46	49581	53438	56980	60255	63301	66146	68817	71333	73711	75966	46
47	49648	53499	57037	60308	63350	66192	68860	71374	73750	76002	47
48	49715	53561	57094	60360	63399	66238	68903	71414	73788	76039	48
49	49782	53622	57150	60413	63448	66284	68946	71455	73827	76075	49
50	49849	53683	57206	60465	63496	66330	68989	71496	73865	76112	50
51	49916	53744	57263	60517	63545	66375	69032	71536	73904	76148	51
52	49982	53805	57319	60570	63594	66421	69075	71577	73942	76185	52
53	50049	53866	57375	60622	63642	66467	69118	71617	73980	76221	53
54	50115	53927	57431	60674	63691	66512	69161	71658	74019	76258	54
55	50182	53988	57488	60726	63740	66558	69204	71698	74057	76294	55
56	50248	54049	57544	60778	63788	66603	69247	71739	74095	76330	56
57	50314	54109	57599	60830	63837	66649	69289	71779	74133	76367	57
58	50380	54170	57655	60882	63885	66694	69332	71819	74171	76403	58
59	50446	54230	57711	60934	63933	66739	69375	71859	74210	76439	59
60	50512	54291	57767	60985	63982	66784	69417	71900	74248	76475	60
//	89° 49'	89° 48'	89° 47'	89° 46'	89° 45'	89° 44'	89° 43'	89° 42'	89° 41'	89° 40'	//

LOG. SINES OF SMALL ARCS TO EACH SECOND

//	0° 20'	0° 21'	0° 22'	0° 23'	0° 24'	0° 25'	0° 26'	0° 27'	0° 28'	0° 29'	//
0	76475	78594	80615	82545	84393	86166	87870	89509	91088	92612	60
1	76512	78629	80647	82577	84424	86195	87897	89535	91114	92637	59
2	76548	78663	80680	82608	84454	86224	87925	89562	91140	92662	58
3	76584	78698	80713	82639	84484	86253	87953	89589	91165	92687	57
4	76620	78732	80746	82671	84514	86282	87981	89616	91191	92712	56
5	76656	78766	80779	82702	84544	86311	88008	89642	91217	92737	55
6	76692	78801	80812	82733	84574	86340	88036	89669	91243	92761	54
7	76728	78835	80844	82765	84604	86368	88064	89696	91269	92786	53
8	76764	78869	80877	82796	84634	86397	88092	89722	91294	92811	52
9	76800	78903	80910	82827	84664	86426	88119	89749	91320	92836	51
10	76836	78938	80942	82859	84694	86455	88147	89776	91346	92861	50
11	76872	78972	80975	82890	84724	86484	88175	89802	91371	92886	49
12	76907	79006	81008	82921	84754	86512	88202	89829	91397	92910	48
13	76943	79040	81040	82952	84784	86541	88230	89856	91423	92935	47
14	76979	79074	81073	82983	84814	86570	88258	89882	91448	92960	46
15	77015	79108	81105	83015	84843	86598	88285	89909	91474	92985	45
16	77051	79142	81138	83046	84873	86627	88313	89935	91500	93009	44
17	77086	79176	81170	83077	84903	86656	88340	89962	91525	93034	43
18	77122	79210	81203	83108	84933	86684	88368	89988	91551	93059	42
19	77158	79244	81235	83139	84963	86713	88395	90015	91576	93084	41
20	77193	79278	81268	83170	84992	86741	88423	90041	91602	93108	40
21	77229	79312	81300	83201	85022	86770	88450	90068	91627	93133	39
22	77264	79346	81332	83232	85052	86799	88478	90094	91653	93158	38
23	77300	79380	81365	83263	85082	86827	88505	90121	91678	93182	37
24	77335	79414	81397	83294	85111	86856	88533	90147	91704	93207	36
25	77371	79448	81429	83325	85141	86884	88560	90174	91729	93231	35
26	77406	79481	81462	83356	85171	86913	88587	90200	91755	93256	34
27	77442	79515	81494	83387	85200	86941	88615	90226	91780	93281	33
28	77477	79549	81526	83417	85230	86969	88642	90253	91806	93305	32
29	77512	79582	81558	83448	85259	86998	88669	90279	91831	93330	31
30	77548	79616	81591	83479	85289	87026	88697	90305	91857	93354	30
31	77583	79650	81623	83510	85318	87055	88724	90332	91882	93379	29
32	77618	79683	81655	83541	85348	87083	88751	90358	91907	93403	28
33	77654	79717	81687	83571	85377	87111	88779	90384	91933	93428	27
34	77689	79751	81719	83602	85407	87140	88806	90411	91958	93452	26
35	77724	79784	81751	83633	85436	87168	88833	90437	91983	93477	25
36	77759	79818	81783	83663	85466	87196	88860	90463	92009	93501	24
37	77794	79851	81815	83694	85495	87224	88888	90489	92034	93526	23
38	77829	79885	81847	83725	85525	87253	88915	90515	92059	93550	22
39	77864	79918	81879	83755	85554	87281	88942	90542	92085	93575	21
40	77899	79952	81911	83786	85583	87309	88969	90568	92110	93599	20
41	77934	79985	81943	83817	85613	87337	88996	90594	92135	93623	19
42	77969	80018	81975	83847	85642	87366	89023	90620	92160	93648	18
43	78004	80052	82007	83878	85671	87394	89050	90646	92186	93672	17
44	78039	80085	82039	83908	85700	87422	89077	90672	92211	93696	16
45	78074	80118	82070	83939	85730	87450	89105	90698	92236	93721	15
46	78109	80152	82102	83969	85759	87478	89132	90725	92261	93745	14
47	78144	80185	82134	84000	85788	87506	89159	90751	92286	93769	13
48	78179	80218	82166	84030	85817	87534	89186	90777	92311	93794	12
49	78213	80251	82198	84060	85847	87562	89213	90803	92336	93818	11
50	78248	80284	82229	84091	85876	87590	89240	90829	92362	93842	10
51	78283	80317	82261	84121	85905	87618	89267	90855	92387	93866	9
52	78318	80351	82293	84151	85934	87646	89294	90881	92412	93891	8
53	78352	80384	82324	84182	85963	87674	89320	90907	92437	93915	7
54	78387	80417	82356	84212	85992	87702	89347	90933	92462	93939	6
55	78422	80450	82387	84242	86021	87730	89374	90958	92487	93963	5
56	78456	80483	82419	84273	86050	87758	89401	90984	92512	93988	4
57	78491	80516	82451	84303	86079	87786	89428	91010	92537	94012	3
58	78525	80549	82482	84333	86108	87814	89455	91036	92562	94036	2
59	78560	80582	82514	84363	86137	87842	89482	91062	92587	94060	1
60	78594	80615	82545	84393	86166	87870	89509	91088	92612	94084	0
//	89° 39'	89° 38'	89° 37'	89° 36'	89° 35'	89° 34'	89° 33'	89° 32'	89° 31'	89° 30'	//

TABLE 66

729

LOG. SINES OF SMALL ARCS TO EACH SECOND

//	0° 30'	0° 31'	0° 32'	0° 33'	0° 34'	0° 35'	0° 36'	0° 37'	0° 38'	0° 39'	//
	7°	7°	7°	7°	7°	8°	8°	8°	8°	8°	
0	94084	95508	96887	98223	7°99520	00779	02002	03192	04350	05478	60
1	94108	95532	96910	98245	7°99541	00799	02022	03211	04369	05497	59
2	94132	95555	96932	98267	7°99562	00820	02042	03231	04388	05515	58
3	94157	95578	96955	98289	7°99584	00841	02062	03251	04407	05534	57
4	94181	95601	96977	98311	7°99605	00861	02082	03270	04426	05552	56
5	94205	95625	97000	98333	7°99626	00882	02102	03290	04445	05571	55
6	94229	95648	97022	98355	7°99647	00903	02123	03309	04464	05589	54
7	94253	95671	97045	98377	7°99669	00923	02143	03329	04483	05608	53
8	94277	95695	97068	98398	7°99690	00944	02163	03348	04502	05626	52
9	94301	95718	97090	98420	7°99711	00964	02183	03368	04521	05645	51
10	94325	95741	97113	98442	7°99732	00985	02203	03387	04540	05663	50
11	94349	95764	97135	98464	7°99753	01006	02223	03407	04559	05682	49
12	94373	95787	97158	98486	7°99775	01026	02243	03426	04578	05700	48
13	94397	95811	97180	98508	7°99796	01047	02263	03446	04597	05719	47
14	94421	95834	97202	98529	7°99817	01067	02283	03465	04616	05737	46
15	94445	95857	97225	98551	7°99838	01088	02303	03484	04635	05756	45
16	94469	95880	97247	98573	7°99859	01108	02323	03504	04654	05774	44
17	94492	95903	97270	98595	7°99880	01129	02343	03523	04673	05792	43
18	94516	95926	97292	98616	7°99901	01149	02362	03543	04692	05811	42
19	94540	95950	97315	98638	7°99922	01170	02382	03562	04710	05829	41
20	94564	95973	97337	98660	7°99943	01190	02402	03581	04729	05848	40
21	94588	95996	97359	98682	7°99965	01211	02422	03601	04748	05866	39
22	94612	96019	97382	98703	7°99986	01231	02442	03620	04767	05885	38
23	94636	96042	97404	98725	8°00007	01252	02462	03640	04786	05903	37
24	94659	96065	97426	98747	8°00028	01272	02482	03659	04805	05921	36
25	94683	96088	97449	98768	8°00049	01293	02502	03678	04824	05940	35
26	94707	96111	97471	98790	8°00070	01313	02522	03698	04843	05958	34
27	94731	96134	97493	98812	8°00091	01333	02542	03717	04861	05976	33
28	94755	96157	97516	98833	8°00112	01354	02561	03736	04880	05995	32
29	94778	96180	97538	98855	8°00133	01374	02581	03756	04899	06013	31
30	94802	96203	97560	98876	8°00154	01395	02601	03775	04918	06031	30
31	94826	96226	97583	98898	8°00175	01415	02621	03794	04937	06050	29
32	94849	96249	97605	98920	8°00196	01435	02641	03813	04955	06068	28
33	94873	96272	97627	98941	8°00217	01456	02661	03833	04974	06086	27
34	94897	96295	97649	98963	8°00238	01476	02680	03852	04993	06105	26
35	94921	96318	97672	98984	8°00259	01496	02700	03871	05012	06123	25
36	94944	96341	97694	99006	8°00279	01517	02720	03891	05030	06141	24
37	94968	96364	97716	99027	8°00300	01537	02740	03910	05049	06159	23
38	94991	96386	97738	99049	8°00321	01557	02759	03929	05068	06178	22
39	95015	96409	97760	99070	8°00342	01578	02779	03948	05087	06196	21
40	95039	96432	97782	99092	8°00363	01598	02799	03967	05105	06214	20
41	95062	96455	97805	99113	8°00384	01618	02819	03987	05124	06232	19
42	95086	96478	97827	99135	8°00405	01639	02838	04006	05143	06251	18
43	95109	96501	97849	99156	8°00426	01659	02858	04025	05161	06269	17
44	95133	96524	97871	99178	8°00447	01679	02878	04044	05180	06287	16
45	95157	96546	97893	99199	8°00467	01699	02898	04063	05199	06305	15
46	95180	96569	97915	99221	8°00488	01720	02917	04083	05218	06324	14
47	95204	96592	97937	99242	8°00509	01740	02937	04102	05236	06342	13
48	95227	96615	97959	99264	8°00530	01760	02957	04121	05255	06360	12
49	95251	96637	97981	99285	8°00551	01780	02976	04140	05274	06378	11
50	95274	96660	98003	99306	8°00571	01801	02996	04159	05292	06396	10
51	95298	96683	98025	99328	8°00592	01821	03016	04178	05311	06414	9
52	95321	96706	98048	99349	8°00613	01841	03035	04197	05329	06433	8
53	95344	96728	98070	99371	8°00634	01861	03055	04217	05348	06451	7
54	95368	96751	98092	99392	8°00654	01881	03074	04236	05367	06469	6
55	95391	96774	98114	99413	8°00675	01901	03094	04255	05385	06487	5
56	95415	96796	98136	99435	8°00696	01922	03114	04274	05404	06505	4
57	95438	96819	98157	99456	8°00717	01942	03133	04293	05422	06523	3
58	95461	96842	98179	99477	8°00737	01962	03153	04312	05441	06541	2
59	95485	96864	98201	99498	8°00758	01982	03172	04331	05460	06560	1
60	95508	96887	98223	99520	8°00779	02002	03192	04350	05478	06578	0
//	80° 29'	80° 28'	80° 27'	80° 26'	80° 25'	80° 24'	80° 23'	80° 22'	80° 21'	80° 20'	//

COSINE

LOG. SINES OF SMALL ARCS TO EACH SECOND												
"	0° 40'	0° 41'	0° 42'	0° 43'	0° 44'	0° 45'	0° 46'	0° 47'	0° 48'	0° 49'	"	"
0	8°	8°	8°	8°	8°	8°	8°	8°	8°	8°	8°	00
1	06558	07650	08696	09718	10717	11693	12647	13581	14495	15391	00	00
2	06556	07668	08714	09735	10733	11709	12663	13596	14510	15406	00	50
3	06614	07685	08731	09752	10750	11725	12679	13612	14525	15420	50	58
4	06632	07703	08748	09769	10766	11741	12694	13627	14541	15435	58	87
5	06650	07721	08765	09786	10782	11757	12710	13643	14556	15450	86	56
6	06668	07738	08783	09802	10799	11773	12726	13658	14571	15465	55	55
7	06686	07756	08800	09819	10815	11789	12741	13673	14586	15479	54	54
8	06704	07773	08817	09836	10832	11805	12757	13689	14601	15494	53	53
9	06722	07791	08834	09853	10848	11821	12773	13704	14616	15509	52	52
10	06740	07809	08851	09870	10864	11837	12788	13719	14631	15523	51	51
11	06758	07826	08868	09886	10881	11853	12804	13735	14646	15538	50	50
12	06776	07844	08886	09903	10897	11869	12820	13750	14661	15553	49	49
13	06794	07861	08903	09920	10914	11885	12835	13765	14676	15568	48	48
14	06812	07879	08920	09937	10930	11901	12851	13781	14691	15582	47	47
15	06830	07896	08937	09953	10946	11917	12867	13796	14706	15597	46	46
16	06848	07914	08954	09970	10963	11933	12882	13811	14721	15612	45	45
17	06866	07932	08971	09987	10979	11949	12898	13827	14736	15626	44	44
18	06884	07949	08988	10004	10995	11965	12914	13842	14751	15641	43	43
19	06902	07967	09006	10020	11012	11981	12929	13857	14766	15656	42	42
20	06920	07984	09023	10037	11028	11997	12945	13873	14781	15670	41	41
21	06938	08002	09040	10054	11044	12013	12961	13888	14796	15685	40	40
22	06956	08019	09057	10070	11061	12029	12976	13903	14811	15700	39	39
23	06974	08037	09074	10087	11077	12045	12992	13919	14826	15714	38	38
24	06992	08054	09091	10104	11093	12061	13007	13934	14841	15729	37	37
25	07010	08072	09108	10120	11110	12077	13023	13949	14856	15744	36	36
26	07028	08089	09125	10137	11126	12093	13039	13964	14871	15758	35	35
27	07046	08107	09142	10154	11142	12109	13054	13980	14886	15773	34	34
28	07063	08124	09159	10170	11159	12125	13070	13995	14901	15788	33	33
29	07081	08141	09176	10187	11175	12141	13085	14010	14915	15802	32	32
30	07099	08159	09193	10204	11191	12157	13101	14025	14930	15817	31	31
31	07117	08176	09210	10220	11207	12172	13117	14041	14945	15832	30	30
32	07135	08194	09227	10237	11224	12188	13132	14056	14960	15846	29	29
33	07153	08211	09244	10254	11240	12204	13148	14071	14975	15861	28	28
34	07171	08229	09261	10270	11256	12220	13163	14086	14990	15875	27	27
35	07189	08246	09278	10287	11272	12236	13179	14101	15005	15890	26	26
36	07206	08263	09295	10303	11289	12252	13194	14117	15020	15905	25	25
37	07224	08281	09312	10320	11305	12268	13210	14132	15035	15919	24	24
38	07242	08298	09329	10337	11321	12284	13225	14147	15050	15934	23	23
39	07260	08316	09346	10353	11337	12300	13241	14162	15065	15948	22	22
40	07278	08333	09363	10370	11354	12315	13256	14178	15079	15963	21	21
41	07295	08350	09380	10386	11370	12331	13272	14193	15094	15978	20	20
42	07313	08368	09397	10403	11386	12347	13287	14208	15109	15992	19	19
43	07331	08385	09414	10420	11402	12363	13303	14223	15124	16007	18	18
44	07349	08403	09431	10436	11418	12379	13318	14238	15139	16021	17	17
45	07367	08420	09448	10453	11435	12395	13334	14253	15154	16036	16	16
46	07384	08437	09465	10469	11451	12410	13349	14269	15169	16050	15	15
47	07402	08455	09482	10486	11467	12426	13365	14284	15183	16065	14	14
48	07420	08472	09499	10502	11483	12442	13380	14299	15198	16079	13	13
49	07438	08489	09516	10519	11499	12458	13396	14314	15213	16094	12	12
50	07455	08506	09533	10535	11515	12474	13411	14329	15228	16109	11	11
51	07473	08524	09550	10552	11531	12489	13427	14344	15243	16123	10	10
52	07491	08541	09567	10568	11548	12505	13442	14359	15258	16138	9	9
53	07509	08558	09583	10585	11564	12521	13458	14375	15273	16152	8	8
54	07526	08576	09600	10601	11580	12537	13473	14390	15287	16167	7	7
55	07544	08593	09617	10618	11596	12553	13489	14405	15302	16181	6	6
56	07562	08610	09634	10634	11612	12568	13504	14420	15317	16196	5	5
57	07579	08627	09651	10651	11628	12584	13519	14435	15332	16210	4	4
58	07597	08645	09668	10667	11644	12600	13535	14450	15346	16225	3	3
59	07615	08662	09685	10684	11660	12616	13550	14465	15361	16239	2	2
60	07632	08679	09701	10700	11677	12631	13566	14480	15376	16254	1	1
61	07650	08696	09718	10717	11693	12647	13581	14495	15391	16268	0	0
"	89° 19'	89° 18'	89° 17'	89° 16'	89° 15'	89° 14'	89° 13'	89° 12'	89° 11'	89° 10'	"	"

COSINE

LOG. SINES OF SMALL ARCS TO EACH SECOND

"	0° 50'	0° 51'	0° 52'	0° 53'	0° 54'	0° 55'	0° 56'	0° 57'	0° 58'	0° 59'	"
0	16268	17128	17971	18798	19610	20407	21189	21958	22713	23456	60
1	16283	17142	17985	18812	19624	20420	21202	21971	22726	23468	59
2	16297	17156	17999	18826	19637	20433	21215	21983	22738	23480	58
3	16311	17171	18013	18839	19650	20446	21228	21996	22751	23492	57
4	16326	17185	18027	18853	19664	20460	21241	22009	22763	23505	56
5	16340	17199	18041	18867	19677	20473	21254	22022	22776	23517	55
6	16355	17213	18055	18880	19691	20486	21267	22034	22788	23529	54
7	16369	17227	18069	18894	19704	20499	21280	22047	22801	23541	53
8	16384	17241	18082	18908	19717	20512	21293	22060	22814	23554	52
9	16398	17256	18096	18921	19731	20525	21306	22072	22826	23566	51
10	16413	17270	18110	18935	19744	20538	21319	22085	22838	23578	50
11	16427	17284	18124	18948	19757	20552	21331	22098	22850	23590	49
12	16441	17298	18138	18962	19771	20565	21344	22110	22863	23603	48
13	16456	17312	18152	18976	19784	20578	21357	22123	22875	23615	47
14	16470	17326	18166	18989	19797	20591	21370	22136	22888	23627	46
15	16485	17340	18180	19003	19811	20604	21383	22148	22900	23639	45
16	16499	17355	18193	19016	19824	20617	21396	22161	22913	23652	44
17	16513	17369	18207	19030	19837	20630	21409	22173	22925	23664	43
18	16528	17383	18221	19044	19851	20643	21422	22186	22937	23676	42
19	16542	17397	18235	19057	19864	20656	21434	22199	22950	23688	41
20	16557	17411	18249	19071	19877	20669	21447	22211	22962	23700	40
21	16571	17425	18263	19084	19891	20682	21460	22224	22975	23713	39
22	16585	17439	18276	19098	19904	20696	21473	22237	22987	23725	38
23	16600	17453	18290	19111	19917	20709	21486	22249	22999	23737	37
24	16614	17467	18304	19125	19931	20722	21499	22262	23012	23749	36
25	16628	17481	18318	19139	19944	20735	21511	22274	23024	23761	35
26	16643	17495	18332	19152	19957	20748	21524	22287	23037	23773	34
27	16657	17510	18345	19166	19971	20761	21537	22300	23049	23786	33
28	16672	17524	18359	19179	19984	20774	21550	22312	23061	23798	32
29	16686	17538	18373	19193	19997	20787	21563	22325	23074	23810	31
30	16700	17552	18387	19206	20010	20800	21576	22337	23086	23822	30
31	16715	17566	18401	19220	20024	20813	21588	22350	23098	23834	29
32	16729	17580	18414	19233	20037	20826	21601	22363	23111	23846	28
33	16743	17594	18428	19247	20050	20839	21614	22375	23123	23859	27
34	16757	17608	18442	19260	20064	20852	21627	22388	23136	23871	26
35	16772	17622	18456	19274	20077	20865	21640	22400	23148	23884	25
36	16786	17636	18469	19287	20090	20878	21652	22413	23160	23895	24
37	16800	17650	18483	19301	20103	20891	21665	22425	23173	23907	23
38	16815	17664	18497	19314	20117	20904	21678	22438	23185	23919	22
39	16829	17678	18511	19328	20130	20917	21691	22451	23197	23931	21
40	16843	17692	18524	19341	20143	20930	21703	22463	23210	23944	20
41	16858	17706	18538	19355	20156	20943	21716	22476	23222	23956	19
42	16872	17720	18552	19368	20170	20956	21729	22488	23234	23968	18
43	16886	17734	18566	19382	20183	20969	21742	22501	23247	23980	17
44	16900	17748	18579	19395	20196	20982	21754	22513	23259	23992	16
45	16915	17762	18593	19409	20209	20995	21767	22526	23271	24004	15
46	16929	17776	18607	19422	20222	21008	21780	22538	23284	24016	14
47	16943	17790	18621	19436	20236	21021	21793	22551	23296	24028	13
48	16957	17804	18634	19449	20249	21034	21805	22563	23308	24041	12
49	16972	17818	18648	19463	20262	21047	21818	22576	23321	24053	11
50	16986	17832	18662	19476	20275	21060	21831	22588	23333	24065	10
51	17000	17846	18675	19489	20288	21073	21844	22601	23345	24077	9
52	17014	17860	18689	19503	20302	21086	21856	22613	23357	24089	8
53	17029	17874	18703	19516	20315	21099	21869	22626	23370	24101	7
54	17043	17888	18716	19530	20328	21112	21882	22638	23382	24113	6
55	17057	17902	18730	19543	20341	21125	21895	22651	23394	24125	5
56	17071	17916	18744	19557	20354	21138	21907	22663	23407	24137	4
57	17085	17930	18757	19570	20368	21151	21920	22676	23419	24149	3
58	17100	17943	18771	19583	20381	21164	21933	22688	23431	24161	2
59	17114	17957	18785	19597	20394	21177	21945	22701	23443	24173	1
60	17128	17971	18798	19610	20407	21189	21958	22713	23456	24186	0
"	89° 5'	89° 8'	89° 7'	89° 6'	89° 5'	89° 4'	89° 3'	89° 2'	89° 1'	89° 0'	"

COSINE

LOG. SINES OF SMALL ARCS TO EACH SECOND

"	1° 0'	1° 1'	1° 2'	1° 3'	1° 4'	1° 5'	1° 6'	1° 7'	1° 8'	1° 9'	"
0	241855	249033	256094	263042	269881	276614	283243	289773	296207	302546	00
1	241976	249152	256211	263157	269994	276725	283353	289881	296313	302651	59
2	242097	249270	256328	263272	270107	276836	283463	289988	296420	302756	58
3	242217	249389	256444	263387	270220	276948	283572	290097	296526	302861	57
4	242338	249507	256561	263502	270333	277059	283682	290205	296632	302965	56
5	242458	249626	256678	263616	270446	277170	283791	290313	296739	303070	55
6	242578	249744	256794	263731	270559	277281	283901	290421	296845	303175	54
7	242699	249863	256911	263846	270672	277392	284010	290529	296951	303280	53
8	242819	249981	257027	263960	270785	277503	284120	290637	297057	303384	52
9	242940	250100	257144	264075	270898	277615	284229	290745	297164	303489	51
10	243060	250218	257260	264190	271010	277726	284339	290852	297270	303594	50
11	243180	250336	257376	264304	271123	277837	284448	290960	297376	303698	49
12	243300	250455	257493	264419	271236	277948	284557	291068	297482	303803	48
13	243421	250573	257609	264533	271349	278059	284667	291175	297588	303907	47
14	243541	250691	257725	264648	271461	278170	284776	291283	297694	304012	46
15	243661	250809	257842	264762	271574	278281	284885	291391	297800	304117	45
16	243781	250927	257958	264877	271687	278391	284994	291498	297906	304221	44
17	243901	251045	258074	264991	271799	278502	285104	291606	298012	304325	43
18	244021	251164	258190	265105	271912	278613	285213	291713	298118	304430	42
19	244141	251282	258307	265220	272024	278724	285322	291821	298224	304534	41
20	244261	251400	258423	265334	272137	278835	285431	291928	298330	304639	40
21	244381	251518	258539	265448	272249	278946	285540	292036	298436	304743	39
22	244501	251636	258655	265562	272362	279056	285649	292143	298542	304847	38
23	244621	251754	258771	265677	272474	279167	285758	292251	298648	304952	37
24	244741	251871	258888	265791	272587	279278	285867	292358	298754	305056	36
25	244861	251989	259003	265905	272699	279388	285976	292466	298859	305160	35
26	244980	252107	259119	266019	272811	279499	286085	292573	298965	305265	34
27	245100	252225	259235	266133	272924	279610	286194	292680	299071	305369	33
28	245220	252343	259351	266247	273036	279720	286303	292787	299177	305473	32
29	245339	252460	259466	266361	273148	279831	286412	292895	299282	305577	31
30	245459	252578	259582	266475	273260	279941	286521	293002	299388	305681	30
31	245579	252696	259698	266589	273373	280052	286629	293109	299494	305785	29
32	245698	252813	259814	266703	273485	280162	286738	293216	299599	305890	28
33	245818	252931	259929	266817	273597	280272	286847	293324	299705	305994	27
34	245937	253049	260045	266931	273709	280383	286956	293431	299810	306098	26
35	246057	253166	260161	267045	273821	280493	287064	293538	299916	306202	25
36	246176	253284	260276	267158	273933	280604	287173	293645	300021	306306	24
37	246296	253401	260392	267272	274045	280714	287282	293752	300127	306410	23
38	246415	253519	260508	267386	274157	280824	287390	293859	300232	306514	22
39	246534	253636	260623	267500	274269	280934	287499	293966	300338	306618	21
40	246654	253753	260739	267613	274381	281045	287608	294073	300443	306721	20
41	246773	253871	260854	267727	274493	281155	287716	294180	300549	306825	19
42	246892	253988	260970	267841	274605	281265	287825	294287	300654	306929	18
43	247011	254105	261085	267954	274717	281375	287933	294394	300759	307033	17
44	247131	254223	261200	268068	274828	281485	288042	294500	300865	307137	16
45	247250	254340	261316	268181	274940	281595	288150	294607	300970	307241	15
46	247369	254457	261431	268295	275052	281705	288259	294714	301075	307344	14
47	247488	254574	261546	268408	275164	281815	288367	294821	301180	307448	13
48	247607	254691	261662	268522	275275	281925	288475	294928	301286	307552	12
49	247726	254808	261777	268635	275387	282035	288584	295034	301391	307655	11
50	247845	254925	261892	268749	275499	282145	288692	295141	301496	307759	10
51	247964	255042	262007	268862	275610	282255	288800	295248	301601	307863	9
52	248083	255159	262122	268975	275722	282365	288908	295354	301706	307966	8
53	248202	255276	262237	269089	275833	282475	289017	295461	301811	308070	7
54	248321	255393	262353	269202	275945	282585	289125	295568	301916	308173	6
55	248440	255510	262468	269315	276057	282695	289233	295674	302021	308277	5
56	248558	255627	262583	269428	276168	282805	289341	295781	302126	308380	4
57	248677	255744	262698	269542	276279	282914	289449	295887	302231	308484	3
58	248796	255861	262813	269655	276391	283024	289557	295994	302336	308587	2
59	248914	255978	262927	269768	276502	283134	289665	296100	302441	308691	1
60	249033	256094	263042	269881	276614	283243	289773	296207	302546	308794	0
"	88° 50'	88° 58'	88° 57'	88° 56'	88° 55'	88° 54'	88° 53'	88° 52'	88° 51'	88° 50'	"

COSINE

LOG. SINES OF SMALL ARCS TO EACH SECOND

"	1° 10'	1° 11'	1° 12'	1° 13'	1° 14'	1° 15'	1° 16'	1° 17'	1° 18'	1° 19'	"
0	308794	314954	321027	327016	332924	338753	344504	350181	355783	361315	60
1	308898	315056	321127	327115	333022	338849	344600	350275	355876	361407	59
2	309001	315157	321228	327215	333120	338946	344695	350368	355969	361498	58
3	309104	315259	321328	327314	333218	339042	344790	350462	356062	361590	57
4	309208	315361	321429	327413	333315	339139	344885	350556	356154	361681	56
5	309311	315463	321529	327512	333413	339235	344980	350650	356247	361773	55
6	309414	315565	321630	327611	333511	339332	345075	350744	356340	361864	54
7	309517	315667	321730	327710	333608	339428	345170	350838	356432	361956	53
8	309620	315768	321830	327809	333706	339524	345265	350932	356525	362047	52
9	309724	315870	321931	327908	333804	339621	345361	351026	356618	362139	51
10	309827	315972	322031	328007	333901	339717	345456	351119	356710	362230	50
11	309930	316073	322131	328106	333999	339813	345551	351213	356803	362321	49
12	310033	316175	322231	328204	334096	339909	345646	351307	356895	362413	48
13	310136	316277	322332	328303	334194	340006	345740	351401	356988	362504	47
14	310239	316378	322432	328402	334291	340102	345835	351494	357080	362596	46
15	310342	316480	322532	328501	334389	340198	345930	351588	357173	362687	45
16	310445	316581	322632	328600	334486	340294	346025	351682	357265	362778	44
17	310548	316683	322732	328698	334584	340390	346120	351775	357358	362870	43
18	310651	316785	322832	328797	334681	340486	346215	351869	357450	362961	42
19	310754	316886	322932	328896	334779	340582	346310	351963	357543	363052	41
20	310857	316987	323033	328995	334876	340679	346405	352056	357635	363143	40
21	310960	317089	323133	329093	334973	340775	346499	352150	357728	363234	39
22	311063	317190	323233	329192	335071	340871	346594	352243	357820	363326	38
23	311166	317292	323333	329291	335168	340967	346688	352337	357912	363417	37
24	311268	317393	323433	329389	335265	341063	346784	352430	358005	363508	36
25	311371	317494	323533	329488	335362	341159	346878	352524	358097	363599	35
26	311474	317596	323632	329586	335460	341255	346973	352617	358189	363690	34
27	311577	317697	323732	329685	335557	341350	347068	352711	358281	363781	33
28	311679	317798	323832	329783	335654	341446	347162	352804	358374	363872	32
29	311782	317900	323932	329882	335751	341542	347257	352898	358466	363963	31
30	311885	318001	324032	329980	335848	341638	347352	352991	358558	364055	30
31	311987	318102	324132	330079	335946	341734	347446	353084	358650	364146	29
32	312090	318203	324232	330177	336043	341830	347541	353178	358742	364237	28
33	312193	318304	324331	330276	336140	341926	347635	353271	358835	364328	27
34	312295	318406	324431	330374	336237	342021	347730	353364	358927	364419	26
35	312398	318507	324531	330472	336334	342117	347824	353458	359019	364509	25
36	312500	318608	324630	330571	336431	342213	347919	353551	359111	364600	24
37	312603	318709	324730	330669	336528	342309	348013	353644	359203	364691	23
38	312705	318810	324830	330767	336625	342404	348108	353737	359295	364782	22
39	312808	318911	324929	330866	336722	342500	348202	353831	359387	364873	21
40	312910	319012	325029	330964	336819	342596	348297	353924	359479	364964	20
41	313013	319113	325129	331062	336916	342691	348391	354017	359571	365055	19
42	313115	319214	325228	331160	337013	342787	348485	354110	359663	365146	18
43	313217	319315	325328	331259	337109	342882	348580	354203	359755	365236	17
44	313320	319416	325427	331357	337206	342978	348674	354296	359847	365327	16
45	313422	319516	325527	331455	337303	343074	348768	354389	359939	365418	15
46	313524	319617	325626	331553	337400	343169	348863	354483	360031	365509	14
47	313626	319718	325726	331651	337497	343265	348957	354576	360122	365599	13
48	313729	319819	325825	331749	337593	343360	349051	354669	360214	365690	12
49	313831	319920	325924	331847	337690	343456	349145	354762	360306	365781	11
50	313933	320021	326024	331945	337787	343551	349240	354855	360398	365871	10
51	314035	320122	326123	332043	337884	343646	349334	354948	360490	365962	9
52	314137	320222	326223	332141	337980	343742	349428	355041	360582	366053	8
53	314239	320323	326322	332239	338077	343837	349522	355133	360673	366143	7
54	314342	320423	326421	332337	338174	343933	349616	355226	360765	366234	6
55	314444	320524	326520	332435	338270	344028	349710	355319	360857	366324	5
56	314546	320625	326620	332533	338367	344123	349804	355412	360948	366415	4
57	314648	320725	326719	332631	338463	344219	349898	355505	361040	366505	3
58	314750	320826	326818	332729	338560	344314	349993	355598	361132	366596	2
59	314852	320926	326917	332826	338656	344409	350087	355691	361223	366686	1
60	314954	321027	327016	332924	338753	344504	350181	355783	361315	366777	0
"	88° 48'	88° 48'	88° 47'	88° 46'	88° 45'	88° 44'	88° 43'	88° 42'	88° 41'	88° 40'	"

COSINE

LOG. SINES OF SMALL ARCS TO EACH SECOND

"	1° 20'	1° 21'	1° 22'	1° 23'	1° 24'	1° 25'	1° 26'	1° 27'	1° 28'	1° 29'	"
0	366777	372171	377499	382762	387962	393101	398179	403199	408161	413068	60
1	366867	372260	377587	382849	388048	393186	398263	403282	408244	413149	59
2	366958	372350	377675	382936	388134	393271	398348	403365	408326	413230	58
3	367048	372439	377763	383024	388221	393356	398432	403442	408408	413311	57
4	367139	372528	377852	383111	388307	393441	398516	403522	408490	413393	56
5	367229	372617	377940	383198	388393	393526	398600	403615	408572	413474	55
6	367319	372707	378028	383285	388479	393611	398684	403698	408654	413555	54
7	367410	372796	378116	383372	388565	393696	398768	403781	408737	413636	53
8	367500	372885	378204	383459	388651	393781	398852	403864	408819	413718	52
9	367590	372974	378292	383546	388737	393866	398936	403947	408901	413799	51
10	367681	373063	378380	383633	388823	393951	399020	404030	408983	413880	50
11	367771	373153	378469	383720	388909	394036	399104	404113	409065	413961	49
12	367861	373242	378557	383807	388995	394121	399188	404196	409147	414042	48
13	367951	373331	378645	383894	389081	394206	399272	404279	409229	414123	47
14	368042	373420	378733	383981	389167	394291	399356	404362	409311	414204	46
15	368132	373509	378821	384068	389253	394376	399440	404445	409393	414286	45
16	368222	373598	378909	384155	389338	394461	399524	404528	409475	414367	44
17	368312	373687	378997	384242	389424	394546	399607	404611	409557	414448	43
18	368402	373776	379084	384329	389510	394631	399691	404694	409639	414529	42
19	368492	373865	379172	384415	389596	394715	399775	404777	409721	414610	41
20	368582	373954	379260	384502	389682	394800	399859	404859	409803	414691	40
21	368672	374043	379348	384589	389768	394885	399943	404942	409885	414772	39
22	368763	374132	379436	384676	389853	394970	400027	405025	409967	414853	38
23	368853	374221	379524	384763	389939	395055	400110	405108	410049	414934	37
24	368943	374310	379612	384850	390025	395139	400194	405191	410131	415015	36
25	369033	374399	379700	384936	390111	395224	400278	405274	410212	415096	35
26	369123	374488	379787	385023	390196	395309	400362	405356	410294	415177	34
27	369213	374577	379875	385110	390282	395393	400445	405439	410376	415257	33
28	369302	374665	379963	385197	390368	395478	400529	405522	410458	415338	32
29	369392	374754	380051	385283	390453	395563	400613	405605	410540	415419	31
30	369482	374843	380138	385370	390539	395647	400696	405687	410621	415500	30
31	369572	374932	380226	385457	390625	395732	400780	405770	410703	415581	29
32	369662	375021	380314	385543	390710	395817	400864	405853	410785	415662	28
33	369752	375109	380401	385630	390796	395901	400947	405935	410867	415743	27
34	369842	375198	380489	385716	390882	395986	401031	406018	410948	415823	26
35	369932	375287	380577	385803	390967	396070	401115	406101	411030	415904	25
36	370021	375375	380664	385890	391053	396155	401198	406183	411112	415985	24
37	370111	375464	380752	385976	391138	396240	401282	406266	411193	416066	23
38	370201	375553	380840	386063	391224	396324	401365	406348	411275	416146	22
39	370291	375641	380927	386149	391309	396409	401449	406431	411357	416227	21
40	370380	375730	381015	386236	391395	396493	401532	406514	411438	416308	20
41	370470	375819	381102	386322	391480	396578	401616	406596	411520	416389	19
42	370560	375907	381190	386409	391566	396662	401699	406679	411602	416469	18
43	370649	375996	381277	386495	391651	396746	401783	406761	411683	416550	17
44	370739	376084	381365	386582	391736	396831	401866	406844	411765	416631	16
45	370829	376173	381452	386668	391822	396915	401950	406926	411846	416711	15
46	370918	376261	381540	386754	391907	397000	402033	407009	411928	416792	14
47	371008	376350	381627	386841	391993	397084	402116	407091	412009	416872	13
48	371097	376438	381714	386927	392078	397168	402200	407173	412091	416953	12
49	371187	376527	381802	387013	392163	397253	402283	407256	412172	417034	11
50	371277	376615	381889	387100	392249	397337	402366	407338	412254	417114	10
51	371366	376704	381977	387186	392334	397421	402450	407421	412335	417195	9
52	371456	376792	382064	387272	392419	397506	402533	407503	412417	417275	8
53	371545	376881	382151	387359	392504	397590	402616	407585	412498	417356	7
54	371635	376969	382239	387445	392590	397674	402700	407668	412579	417436	6
55	371724	377057	382326	387531	392675	397758	402783	407750	412661	417517	5
56	371813	377146	382413	387617	392760	397843	402866	407832	412742	417597	4
57	371903	377234	382500	387704	392845	397927	402949	407915	412824	417678	3
58	371992	377322	382588	387790	392930	398011	403033	407997	412905	417758	2
59	372082	377411	382675	387876	393016	398095	403116	408079	412986	417839	1
60	372171	377499	382762	387962	393101	398179	403199	408161	413068	417919	0
"	88° 30'	88° 36'	88° 37'	88° 36'	88° 35'	88° 34'	88° 33'	88° 32'	88° 31'	88° 30'	"

COSINE

LOG. SINES OF SMALL ARCS TO TEN SECONDS

0	1	2	3	4	5	6	7	8	9	Parts	0	1
0	1	2	3	4	5	6	7	8	9	Parts	0	1
1	30	417919	418722	419524	420325	421123	421921	422717	32' 37"	88 29	0	1
1	31	422717	423511	424304	425096	425886	426675	427462	1" 78 74	88 28	0	2
1	32	427462	428248	429032	429815	430597	431377	432156	2 156 148	88 27	0	3
1	33	432156	432934	433710	434484	435257	436029	436800	3 235 223	88 26	0	4
1	34	436800	437569	438337	439103	439868	440632	441394	4 313 297	88 25	0	5
1	35	441394	442156	442915	443674	444431	445186	445941	5 391 371	88 24	0	6
1	36	445941	446694	447446	448196	448946	449694	450440	6 469 445	88 23	0	7
1	37	450440	451186	451930	452673	453414	454154	454893	7 547 519	88 22	0	8
1	38	454893	455631	456368	457103	457837	458570	459301	8 626 594	88 21	0	9
1	39	459301	460032	460761	461489	462215	462941	463665	9 704 668	88 20	0	0
1	40	463665	464388	465110	465830	466550	467268	467985	48' 47"	88 19	0	1
1	41	467985	468701	469416	470129	470841	471553	472263	1' 71 67	88 18	0	2
1	42	472263	472971	473679	474386	475091	475795	476498	2 141 135	88 17	0	3
1	43	476498	477200	477901	478601	479299	479997	480693	3 212 202	88 16	0	4
1	44	480693	481388	482083	482776	483467	484158	484848	4 282 269	88 15	0	5
1	45	484848	485536	486224	486910	487596	488280	488963	5 353 336	88 14	0	6
1	46	488963	489645	490326	491006	491685	492363	493040	6 424 404	88 13	0	7
1	47	493040	493715	494390	495064	495736	496408	497078	7 494 471	88 12	0	8
1	48	497078	497748	498416	499084	499750	500416	501080	8 565 538	88 11	0	9
1	49	501080	501743	502405	503067	503727	504386	505045	9 635 606	88 10	0	0
1	50	505045	505702	506358	507014	507668	508321	508974	58' 57"	88 9	0	1
1	51	508974	509625	510275	510925	511573	512221	512867	1" 64 62	88 8	0	2
1	52	512867	513513	514157	514801	515444	516086	516726	2 129 123	88 7	0	3
1	53	516726	517366	518005	518643	519280	519916	520551	3 193 185	88 6	0	4
1	54	520551	521186	521819	522451	523083	523713	524343	4 257 246	88 5	0	5
1	55	524343	524972	525599	526226	526852	527477	528102	5 321 308	88 4	0	6
1	56	528102	528725	529347	529969	530590	531209	531828	6 386 370	88 3	0	7
1	57	531828	532446	533063	533679	534295	534909	535523	7 450 431	88 2	0	8
1	58	535523	536136	536747	537358	537969	538578	539186	8 514 493	88 1	0	9
1	59	539186	539792	540401	541007	541612	542216	542819	9 579 554	88 0	0	0
2	0	542819	543422	544023	544624	545224	545823	546422	2' 54	87 59	0	1
2	1	546422	547019	547616	548212	548807	549401	549995	1" 59 57	87 58	0	2
2	2	549995	550587	551179	551770	552361	552950	553539	2 118 113	87 57	0	3
2	3	553539	554126	554713	555300	555885	556470	557054	3 177 170	87 56	0	4
2	4	557054	557637	558219	558801	559381	559961	560540	4 236 227	87 55	0	5
2	5	560540	561119	561696	562273	562849	563425	563999	5 295 284	87 54	0	6
2	6	563999	564573	565146	565719	566290	566861	567431	6 355 340	87 53	0	7
2	7	567431	568001	568569	569137	569704	570270	570835	7 414 397	87 52	0	8
2	8	570835	571401	571965	572528	573091	573653	574214	8 473 454	87 51	0	9
2	9	574214	574774	575334	575893	576451	577009	577566	9 532 510	87 50	0	0
2	10	577566	578122	578678	579232	579786	580340	580892	18' 17"	87 49	0	1
2	11	580892	581444	581995	582546	583096	583645	584193	1" 55 53	87 48	0	2
2	12	584193	584741	585288	585834	586380	586925	587469	2 109 103	87 47	0	3
2	13	587469	588013	588556	589098	589640	590181	590721	3 164 158	87 46	0	4
2	14	590721	591260	591799	592338	592875	593412	593948	4 218 210	87 45	0	5
2	15	593948	594484	595019	595553	596086	596619	597152	5 273 263	87 44	0	6
2	16	597152	597683	598214	598745	599274	599803	600332	6 328 316	87 43	0	7
2	17	600332	600859	601387	601913	602439	602964	603489	7 382 368	87 42	0	8
2	18	603489	604012	604536	605058	605580	606102	606623	8 437 421	87 41	0	9
2	19	606623	607143	607662	608181	608699	609217	609734	9 491 473	87 40	0	0
2	20	609734	610251	610766	611282	611796	612310	612823	22' 27"	87 39	0	1
2	21	612823	613336	613848	614360	614871	615381	615891	1" 51 49	87 38	0	2
2	22	615891	616400	616909	617417	617924	618431	618937	2 102 98	87 37	0	3
2	23	618937	619442	619947	620452	620956	621459	621962	3 152 147	87 36	0	4
2	24	621962	622464	622965	623466	623966	624466	624965	4 203 196	87 35	0	5
2	25	624965	625464	625962	626459	626956	627453	627948	5 254 245	87 34	0	6
2	26	627948	628444	628938	629432	629926	630419	630911	6 305 294	87 33	0	7
2	27	630911	631403	631894	632385	632875	633365	633854	7 356 343	87 32	0	8
2	28	633854	634342	634830	635317	635804	636291	636776	8 406 392	87 31	0	9
2	29	636776	637262	637746	638230	638714	639197	639680	9 457 441	87 30	0	0
2	30	639680	640162	640643	641124	641604	642084	642563		87 29	0	1
0	1	00"	01"	02"	03"	04"	05"	06"	Parts	0	1	

COSINE

LOG. SINES OF SMALL ARCS TO TEN SECONDS

0	0"	10"	20"	30"	40"	50"	60"	Parts	0
2 30	8. 039680	8. 640162	8. 640643	8. 641124	8. 641604	8. 642084	8. 642563	32' 37'	87 29
2 31	644563	643042	643520	643998	644475	644952	645428	1" 47 46	87 28
2 32	645428	645904	646379	646854	647328	647801	648274	2 95 92	87 27
2 33	648274	648747	649219	649690	650161	650632	651102	3 142 138	87 26
2 34	651102	651571	652040	652508	652976	653444	653911	4 190 184	87 25
2 35	653911	654377	654843	655308	655773	656238	656702	5 237 229	87 24
2 36	656702	657165	657628	658090	658552	659014	659475	6 284 275	87 23
2 37	659475	659935	660395	660855	661314	661772	662230	7 332 321	87 22
2 38	662230	662688	663145	663602	664058	664513	664968	8 379 367	87 21
2 39	664968	665423	665877	666331	666784	667237	667689	9 427 413	87 20
2 40	667689	668141	668592	669043	669494	669944	670393	42' 47'	87 19
2 41	670393	670842	671291	671739	672187	672634	673080	1" 45 43	87 18
2 42	673080	673527	673972	674418	674863	675307	675751	2 89 86	87 17
2 43	675751	676194	676638	677080	677522	677964	678405	3 133 130	87 16
2 44	678405	678846	679286	679726	680166	680605	681043	4 178 173	87 15
2 45	681043	681481	681919	682356	682793	683230	683665	5 223 216	87 14
2 46	683665	684101	684536	684971	685405	685838	686272	6 267 259	87 13
2 47	686272	686705	687137	687569	688001	688432	688863	7 312 302	87 12
2 48	688863	689293	689723	690152	690581	691010	691438	8 356 346	87 11
2 49	691438	691866	692293	692720	693146	693572	693998	9 400 389	87 10
2 50	693998	694423	694848	695272	695696	696120	696543	52' 57'	87 9
2 51	696543	696966	697388	697810	698232	698653	699073	1" 42 41	87 8
2 52	699073	699494	699913	700333	700752	701171	701589	2 84 82	87 7
2 53	701589	702007	702424	702841	703258	703674	704090	3 126 122	87 6
2 54	704090	704505	704920	705335	705749	706163	706577	4 168 163	87 5
2 55	706577	706990	707402	707815	708226	708638	709049	5 209 204	87 4
2 56	709049	709460	709870	710280	710690	711099	711507	6 251 244	87 3
2 57	711507	711916	712324	712731	713139	713546	713952	7 293 285	87 2
2 58	713952	714358	714764	715169	715574	715979	716383	8 335 326	87 1
2 59	716383	716787	717190	717593	717996	718398	718800	9 377 366	87 0
3 0	718800	719202	719603	720004	720404	720804	721204	3' 7'	86 59
3 1	721204	721603	722002	722401	722799	723197	723595	1" 40 39	86 58
3 2	723595	723992	724389	724785	725181	725577	725972	2 79 77	86 57
3 3	725972	726367	726762	727156	727550	727943	728337	3 119 116	86 56
3 4	728337	728729	729122	729514	729906	730297	730688	4 158 154	86 55
3 5	730688	731079	731469	731859	732249	732638	733027	5 198 193	86 54
3 6	733027	733416	733804	734192	734579	734967	735354	6 238 232	86 53
3 7	735354	735740	736126	736512	736898	737283	737667	7 277 270	86 52
3 8	737667	738052	738436	738820	739203	739586	739969	8 317 309	86 51
3 9	739969	740352	740734	741115	741497	741878	742259	9 356 347	86 50
3 10	742259	742639	743019	743399	743778	744157	744536	12' 17'	86 49
3 11	744536	744914	745293	745670	746048	746425	746802	1" 38 37	86 48
3 12	746802	747178	747554	747930	748305	748680	749055	2 75 73	86 47
3 13	749055	749430	749804	750178	750551	750924	751297	3 113 110	86 46
3 14	751297	751670	752042	752414	752786	753157	753528	4 150 146	86 45
3 15	753528	753898	754269	754639	755008	755378	755747	5 188 183	86 44
3 16	755747	756116	756484	756852	757220	757587	757955	6 226 220	86 43
3 17	757955	758321	758688	759054	759420	759786	760151	7 263 256	86 42
3 18	760151	760516	760881	761245	761609	761973	762337	8 301 293	86 41
3 19	762337	762700	763063	763425	763787	764149	764511	9 338 329	86 40
3 20	764511	764872	765234	765594	765955	766315	766675	22' 27'	86 39
3 21	766675	767034	767394	767752	768111	768469	768828	1" 36 35	86 38
3 22	768828	769185	769543	769900	770257	770613	770970	2 71 70	86 37
3 23	770970	771326	771681	772037	772392	772747	773101	3 107 105	86 36
3 24	773101	773456	773810	774163	774517	774870	775223	4 143 139	86 35
3 25	775223	775575	775927	776279	776631	776982	777333	5 178 174	86 34
3 26	777333	777684	778035	778385	778735	779085	779434	6 214 209	86 33
3 27	779434	779783	780132	780480	780829	781177	781524	7 250 244	86 32
3 28	781524	781872	782219	782566	782912	783259	783605	8 286 278	86 31
3 29	783605	783951	784296	784641	784986	785331	785675	9 321 313	86 30
3 30	785675	786019	786363	786707	787050	787393	787736		86 29
0	60"	50"	40"	30"	20"	10"	0"	Parts	0

COSINE

TABLE 67

737

LOG. SINES OF SMALL ARCS TO TEN SECONDS

° /	0'	10'	20'	30'	40'	50'	60'	Parts	° /
3 30	8° 785675	8° 786019	8° 786363	8° 786707	8° 787050	8° 787393	8° 787736	32 37	86 29
3 31	787736	788078	788421	788762	789104	789446	789787	1" 34 33	86 28
3 32	789787	790128	790468	790808	791149	791488	791828	2 68 66	86 27
3 33	791828	792167	792506	792845	793183	793521	793859	3 102 100	86 26
3 34	793859	794197	794534	794872	795208	795545	795881	4 136 133	86 25
3 35	795881	796218	796553	796889	797224	797559	797894	5 170 166	86 24
3 36	797894	798229	798563	798897	799231	799564	799897	6 204 199	86 23
3 37	799897	800230	800563	800896	801228	801560	801892	7 238 232	86 22
3 38	801892	802223	802554	802885	803216	803546	803876	8 272 266	86 21
3 39	803876	804206	804536	804866	805195	805524	805852	9 306 299	86 20
3 40	805852	806181	806509	806837	807165	807492	807819	42" 47"	86 19
3 41	807819	808146	808473	808799	809126	809451	809776	1" 32 32	86 18
3 42	809776	810103	810428	810753	811078	811402	811726	2 65 64	86 17
3 43	811726	812050	812374	812698	813021	813344	813667	3 97 95	86 16
3 44	813667	813989	814312	814634	814956	815277	815599	4 130 127	86 15
3 45	815599	815920	816241	816561	816882	817202	817522	5 162 159	86 14
3 46	817522	817841	818161	818480	818799	819118	819436	6 195 191	86 13
3 47	819436	819755	820073	820390	820708	821025	821343	7 228 223	86 12
3 48	821343	821659	821976	822292	822609	822925	823240	8 261 254	86 11
3 49	823240	823556	823871	824186	824501	824816	825130	9 293 286	86 10
3 50	825130	825444	825758	826072	826385	826698	827011	52" 57"	86 9
3 51	827011	827324	827637	827949	828261	828573	828884	1" 31 30	86 8
3 52	828884	829196	829507	829818	830129	830439	830749	2 62 61	86 7
3 53	830749	831060	831369	831679	831988	832298	832607	3 93 91	86 6
3 54	832607	832915	833224	833532	833840	834148	834456	4 124 122	86 5
3 55	834456	834763	835070	835377	835684	835991	836297	5 155 152	86 4
3 56	836297	836603	836909	837215	837520	837825	838130	6 187 182	86 3
3 57	838130	838435	838740	839044	839348	839652	839956	7 218 213	86 2
3 58	839956	840260	840563	840866	841169	841472	841774	8 249 243	86 1
3 59	841774	842076	842378	842680	842982	843283	843585	9 280 274	86 0
4 0	843585	843886	844186	844487	844787	845087	845387	2" 7"	85 59
4 1	845387	845687	845987	846286	846585	846884	847183	1" 30 29	85 58
4 2	847183	847481	847780	848078	848376	848673	848971	2 60 58	85 57
4 3	848971	849268	849565	849862	850159	850455	850751	3 89 88	85 56
4 4	850751	851047	851343	851639	851934	852229	852525	4 119 117	85 55
4 5	852525	852819	853114	853408	853703	853997	854291	5 149 146	85 54
4 6	854291	854584	854878	855171	855464	855757	856049	6 179 175	85 53
4 7	856049	856342	856634	856926	857218	857501	857781	7 209 197	85 52
4 8	857781	858092	858383	858674	858965	859255	859546	8 238 234	85 51
4 9	859546	859836	860126	860415	860705	860994	861283	9 268 263	85 50
4 10	861283	861572	861861	862149	862438	862726	863014	12" 17"	85 49
4 11	863014	863302	863589	863877	864164	864451	864738	1" 30 28	85 48
4 12	864738	865024	865311	865597	865883	866169	866455	2 57 56	85 47
4 13	866455	866740	867025	867310	867595	867880	868165	3 86 84	85 46
4 14	868165	868449	868733	869017	869301	869585	869868	4 114 112	85 45
4 15	869868	870151	870434	870717	871000	871282	871565	5 143 140	85 44
4 16	871565	871847	872129	872410	872692	872973	873255	6 172 169	85 43
4 17	873255	873536	873817	874097	874378	874658	874938	7 200 197	85 42
4 18	874938	875218	875498	875777	876057	876336	876615	8 229 225	85 41
4 19	876615	876894	877172	877451	877729	878007	878285	9 257 253	85 40
4 20	878285	878563	878841	879118	879395	879672	879949	22" 27"	85 39
4 21	879949	880226	880503	880779	881055	881331	881607	1" 28 27	85 38
4 22	881607	881883	882158	882433	882708	882983	883258	2 55 54	85 37
4 23	883258	883533	883807	884081	884355	884629	884903	3 82 81	85 36
4 24	884903	885177	885450	885723	885996	886269	886542	4 110 108	85 35
4 25	886542	886814	887087	887359	887631	887903	888174	5 137 135	85 34
4 26	888174	888446	888717	888988	889259	889530	889801	6 165 162	85 33
4 27	889801	890071	890341	890612	890882	891151	891421	7 192 189	85 32
4 28	891421	891690	891960	892229	892498	892767	893035	8 220 216	85 31
4 29	893035	893304	893572	893840	894108	894376	894643	9 247 243	85 30
4 30	894643	894911	895178	895445	895712	895979	896246		85 29
° /	60"	50"	40"	30"	20"	10"	0'	Parts	° /

COSINE

LOG. SINES OF SMALL ARCS TO TEN SECONDS

0'	0"	10"	20"	30"	40"	50"	60"	Parts	0'
2 30	8° 039680	8° 640162	8° 640643	8° 641124	8° 641604	8° 642084	8° 642563	32' 37'	87 29
2 31	644563	643042	643520	643998	644475	644952	645428	1" 47 46	87 28
2 32	645428	645904	646379	646854	647328	647801	648274	2 95 92	87 27
2 33	648274	648747	649219	649690	650161	650632	651102	3 142 138	87 26
2 34	651102	651571	652040	652508	652976	653444	653911	4 190 184	87 25
2 35	653911	654377	654843	655308	655773	656238	656702	5 237 229	87 24
2 36	656702	657165	657628	658090	658552	659014	659475	6 284 275	87 23
2 37	659475	659935	660395	660855	661314	661772	662230	7 332 321	87 22
2 38	662230	662688	663145	663602	664058	664513	664968	8 379 367	87 21
2 39	664968	665423	665877	666331	666784	667237	667689	9 427 413	87 20
2 40	667689	668141	668592	669043	669494	669944	670393	42' 47'	87 19
2 41	670393	670842	671291	671739	672187	672634	673080	1" 45 43	87 18
2 42	673080	673527	673972	674418	674863	675307	675751	2 89 86	87 17
2 43	675751	676194	676638	677080	677522	677964	678405	3 133 150	87 16
2 44	678405	678846	679286	679726	680166	680605	681043	4 178 173	87 15
2 45	681043	681481	681919	682356	682793	683230	683665	5 223 216	87 14
2 46	683665	684101	684536	684971	685405	685838	686272	6 267 259	87 13
2 47	686272	686705	687137	687569	688001	688432	688863	7 312 302	87 12
2 48	688863	689293	689723	690152	690581	691010	691438	8 356 346	87 11
2 49	691438	691866	692293	692720	693146	693572	693998	9 400 389	87 10
2 50	693998	694423	694848	695272	695696	696120	696543	52' 57'	87 9
2 51	696543	696966	697388	697810	698232	698653	699073	1" 42 41	87 8
2 52	699073	699494	699913	700333	700752	701171	701589	2 84 82	87 7
2 53	701589	702007	702424	702841	703258	703674	704090	3 126 122	87 6
2 54	704090	704505	704920	705335	705749	706163	706577	4 168 163	87 5
2 55	706577	706990	707402	707815	708226	708638	709049	5 209 204	87 4
2 56	709049	709460	709870	710280	710690	711099	711507	6 251 244	87 3
2 57	711507	711916	712324	712731	713139	713546	713952	7 293 285	87 2
2 58	713952	714358	714764	715169	715574	715979	716383	8 335 326	87 1
2 59	716383	716787	717190	717593	717996	718398	718800	9 377 366	87 0
3 0	718800	719202	719603	720004	720404	720804	721204	2' 7'	86 59
3 1	721204	721603	722002	722401	722799	723197	723595	1" 40 39	86 58
3 2	723595	723992	724389	724785	725181	725577	725972	2 79 177	86 57
3 3	725972	726367	726762	727156	727550	727943	728337	3 119 116	86 56
3 4	728337	728729	729122	729514	729906	730297	730688	4 158 154	86 55
3 5	730688	731079	731469	731859	732249	732638	733027	5 198 193	86 54
3 6	733027	733416	733804	734192	734579	734967	735354	6 238 232	86 53
3 7	735354	735740	736126	736512	736898	737283	737667	7 277 270	86 52
3 8	737667	738052	738436	738820	739203	739586	739969	8 317 309	86 51
3 9	739969	740352	740734	741115	741497	741878	742259	9 356 347	86 50
3 10	742259	742639	743019	743399	743778	744157	744536	12' 17'	86 49
3 11	744536	744914	745293	745670	746048	746425	746802	1" 38 37	86 48
3 12	746802	747178	747554	747930	748305	748680	749055	2 75 73	86 47
3 13	749055	749430	749804	750178	750551	750924	751297	3 113 110	86 46
3 14	751297	751670	752042	752414	752786	753157	753528	4 150 146	86 45
3 15	753528	753898	754269	754639	755008	755378	755747	5 188 183	86 44
3 16	755747	756116	756484	756852	757220	757587	757955	6 226 220	86 43
3 17	757955	758321	758688	759054	759420	759786	760151	7 263 256	86 42
3 18	760151	760516	760881	761245	761609	761973	762337	8 301 293	86 41
3 19	762337	762700	763063	763425	763787	764149	764511	9 338 329	86 40
3 20	764511	764872	765234	765594	765955	766315	766675	28' 27'	86 39
3 21	766675	767034	767394	767752	768111	768469	768828	1" 38 35	86 38
3 22	768828	769185	769543	769900	770257	770613	770970	2 71 70	86 37
3 23	770970	771326	771681	772037	772392	772747	773101	3 107 105	86 36
3 24	773101	773456	773810	774163	774517	774870	775223	4 143 139	86 35
3 25	775223	775575	775927	776279	776631	776982	777333	5 178 174	86 34
3 26	777333	777684	778035	778385	778735	779085	779434	6 214 209	86 33
3 27	779434	779783	780132	780480	780829	781177	781524	7 250 244	86 32
3 28	781524	781872	782219	782566	782912	783259	783605	8 286 278	86 31
3 29	783605	783951	784296	784641	784986	785331	785675	9 321 313	86 30
3 30	785675	786019	786363	786707	787050	787393	787736		86 29
0'	60"	50"	40"	30"	20"	10"	0"	Parts	0'

COSINE

TABLE 67

737

LOG. SINES OF SMALL ARCS TO TEN SECONDS

0	1	0'	10'	20'	30'	40'	50'	60'	Parts	0	1
3	30	8°	8°	8°	8°	8°	8°	8°	32	37	86 29
3	31	785675	786019	786163	786707	787050	787393	787736	1"	34	86 28
3	32	787736	788078	788421	788762	789104	789446	789787	2	68	86 27
3	33	789787	790128	790468	790808	791149	791488	791828	3	102	86 26
3	34	791828	792167	792506	792845	793183	793521	793859	4	136	86 25
3	35	793859	794197	794534	794872	795208	795545	795881	5	170	86 24
3	36	795881	796218	796553	796889	797224	797559	797894	6	204	86 23
3	37	797894	798229	798563	798897	799231	799564	799897	7	238	86 22
3	38	799897	800230	800563	800896	801228	801560	801892	8	272	86 21
3	39	801892	802223	802554	802885	803216	803546	803876	9	306	86 20
3	40	803876	804206	804536	804866	805195	805524	805852	42'	47'	86 19
3	41	805852	806181	806509	806837	807165	807492	807819	1"	32	86 18
3	42	807819	808146	808473	808799	809126	809451	809777	2	65	86 17
3	43	809777	810103	810428	810753	811078	811402	811726	3	97	86 16
3	44	811726	812050	812374	812698	813021	813344	813667	4	130	86 15
3	45	813667	813989	814312	814634	814956	815277	815599	5	162	86 14
3	46	815599	815920	816241	816561	816882	817202	817522	6	195	86 13
3	47	817522	817841	818161	818480	818799	819118	819436	7	228	86 12
3	48	819436	819755	820073	820390	820708	821025	821343	8	261	86 11
3	49	821343	821659	821976	822292	822609	822925	823240	9	293	86 10
3	50	823240	823556	823871	824186	824501	824816	825130	52'	57'	86 9
3	51	825130	825444	825758	826072	826385	826698	827011	1"	31	86 8
3	52	827011	827324	827637	827949	828261	828573	828884	2	62	86 7
3	53	828884	829196	829507	829818	830129	830439	830749	3	93	86 6
3	54	830749	831060	831369	831679	831988	832298	832607	4	124	86 5
3	55	832607	832915	833224	833532	833840	834148	834456	5	155	86 4
3	56	834456	834763	835070	835377	835684	835991	836297	6	187	86 3
3	57	836297	836603	836909	837215	837520	837825	838130	7	218	86 2
3	58	838130	838435	838740	839044	839348	839652	839956	8	249	86 1
3	59	839956	840260	840563	840866	841169	841472	841774	9	280	86 0
4	0	841774	842076	842378	842680	842982	843283	843585	2'	7'	85 59
4	1	843585	843886	844186	844487	844787	845087	845387	1"	30	85 58
4	2	845387	845687	845987	846286	846585	846884	847183	2	60	85 57
4	3	847183	847481	847780	848078	848376	848673	848971	3	89	85 56
4	4	848971	849268	849565	849862	850159	850455	850751	4	119	85 55
4	5	850751	851047	851343	851639	851934	852229	852525	5	149	85 54
4	6	852525	852819	853114	853408	853703	853997	854291	6	179	85 53
4	7	854291	854584	854878	855171	855464	855757	856049	7	209	85 52
4	8	856049	856342	856634	856926	857218	857510	857801	8	238	85 51
4	9	857801	858092	858383	858674	858965	859255	859546	9	268	85 50
4	10	859546	859836	860126	860415	860705	860994	861283	12'	17'	85 49
4	11	861283	861572	861861	862149	862438	862726	863014	1"	30	85 48
4	12	863014	863302	863589	863877	864164	864451	864738	2	57	85 47
4	13	864738	865024	865311	865597	865883	866169	866455	3	86	85 46
4	14	866455	866740	867025	867310	867595	867880	868165	4	114	85 45
4	15	868165	868449	868733	869017	869301	869585	869868	5	143	85 44
4	16	869868	870151	870434	870717	871000	871282	871565	6	172	85 43
4	17	871565	871847	872129	872410	872692	872973	873255	7	200	85 42
4	18	873255	873536	873817	874097	874378	874658	874938	8	229	85 41
4	19	874938	875218	875498	875777	876057	876336	876615	9	257	85 40
4	20	876615	876894	877172	877451	877729	878007	878285	22'	27'	85 39
4	21	878285	878563	878841	879118	879395	879672	879949	1"	28	85 38
4	22	879949	880226	880503	880779	881055	881331	881607	2	55	85 37
4	23	881607	881883	882158	882433	882708	882983	883258	3	82	85 36
4	24	883258	883533	883807	884081	884355	884629	884903	4	110	85 35
4	25	884903	885177	885450	885723	885996	886269	886542	5	137	85 34
4	26	886542	886814	887087	887359	887631	887903	888174	6	165	85 33
4	27	888174	888446	888717	888988	889259	889530	889801	7	192	85 32
4	28	889801	890071	890341	890612	890882	891151	891421	8	220	85 31
4	29	891421	891690	891960	892229	892498	892767	893035	9	247	85 30
4	30	893035	893304	893572	893840	894108	894376	894643	24'	24'	85 29
4	31	894643	894911	895178	895445	895712	895979	896246			
0	1	60'	50'	40'	30'	20'	10'	0'	Parts	0	1

COSINE

LOG. SINES, COSINES, &c.											
0° 0'						0°					
°	'	Sine	D.	Cosec.	Tangent	D.	Cotang.	Secant	D.	Cosine	°
0	0	—	—	—	—	—	—	10.000000	0	10.000000	90
1	0	6.162696	477121	13.837304	6.162696	477121	13.837304	10.000000	0	10.000000	89
2	0	6.463726	221749	13.536274	6.463726	221749	13.536274	10.000000	0	10.000000	88
3	0	6.639817	146128	13.360183	6.639817	146128	13.360183	10.000000	0	10.000000	87
4	0	6.764756	109145	13.235244	6.764756	109145	13.235244	10.000000	0	10.000000	86
5	0	6.861666	87150	13.138334	6.861666	87150	13.138334	10.000000	0	10.000000	85
6	0	6.940847	72550	13.059153	6.940847	72551	13.059153	10.000000	0	10.000000	84
7	0	7.007794	62148	12.992206	7.007794	62148	12.992206	10.000000	0	10.000000	83
8	0	7.065786	54158	12.934214	7.065786	54157	12.934214	10.000000	0	10.000000	82
9	0	7.116939	48305	12.883061	7.116939	48305	12.883061	10.000000	0	10.000000	81
10	0	7.162696	43465	12.837304	7.162696	43466	12.837304	10.000000	0	10.000000	80
11	0	7.204089	39509	12.795911	7.204089	39508	12.795911	10.000001	0	9.999999	79
12	0	7.241877	36212	12.758122	7.241878	36213	12.758122	10.000001	0	9.999999	78
13	0	7.276639	33424	12.723361	7.276640	33425	12.723361	10.000001	0	9.999999	77
14	0	7.308824	31034	12.691176	7.308825	31035	12.691175	10.000001	0	9.999999	76
15	0	7.338787	28963	12.661213	7.338788	28964	12.661212	10.000001	0	9.999999	75
16	0	7.366816	27153	12.633184	7.366817	27152	12.633183	10.000001	0	9.999999	74
17	0	7.393145	25554	12.606855	7.393146	25554	12.606854	10.000001	0	9.999999	73
18	0	7.417968	24133	12.582032	7.417970	24134	12.582030	10.000001	0	9.999999	72
19	0	7.441449	22863	12.558551	7.441451	22863	12.558549	10.000002	0	9.999998	71
20	0	7.463726	21719	12.536274	7.463727	21719	12.536273	10.000002	0	9.999998	70
21	0	7.484915	20685	12.515085	7.484917	20685	12.515083	10.000002	0	9.999998	69
22	0	7.505118	19744	12.494882	7.505120	19744	12.494880	10.000002	0	9.999998	68
23	0	7.524423	18858	12.475577	7.524426	18858	12.475574	10.000002	0	9.999998	67
24	0	7.542906	18098	12.457094	7.542909	18098	12.457091	10.000003	0	9.999997	66
25	0	7.560635	17374	12.439365	7.560638	17374	12.439362	10.000003	0	9.999997	65
26	0	7.577668	16706	12.422332	7.577672	16706	12.422328	10.000003	0	9.999997	64
27	0	7.594059	16087	12.405931	7.594062	16087	12.405928	10.000003	0	9.999997	63
28	0	7.609853	15512	12.390147	7.609857	15512	12.390143	10.000004	0	9.999996	62
29	0	7.625095	14977	12.374907	7.625097	14978	12.374903	10.000004	0	9.999996	61
30	0	7.639816	14478	12.360184	7.639820	14478	12.360180	10.000004	0	9.999996	60
31	0	7.654056	14010	12.345944	7.654061	14011	12.345939	10.000004	0	9.999996	59
32	0	7.667845	13573	12.332155	7.667849	13573	12.332151	10.000005	0	9.999995	58
33	0	7.681208	13161	12.318792	7.681213	13161	12.318787	10.000005	0	9.999995	57
34	0	7.694173	12774	12.305827	7.694179	12775	12.305821	10.000005	0	9.999995	56
35	0	7.706762	12410	12.293238	7.706768	12409	12.293232	10.000006	0	9.999994	55
36	0	7.718997	12064	12.281003	7.719003	12065	12.280997	10.000006	0	9.999994	54
37	0	7.730896	11738	12.269104	7.730902	11739	12.269098	10.000006	0	9.999994	53
38	0	7.742478	11430	12.257522	7.742484	11429	12.257516	10.000007	0	9.999993	52
39	0	7.753758	11136	12.246242	7.753765	11137	12.246235	10.000007	0	9.999993	51
40	0	7.764754	10858	12.235246	7.764761	10858	12.235239	10.000007	0	9.999993	50
41	0	7.775477	10593	12.224523	7.775485	10593	12.224515	10.000008	0	9.999992	49
42	0	7.785943	10340	12.214057	7.785951	10342	12.214049	10.000008	0	9.999992	48
43	0	7.796162	10100	12.203838	7.796170	10100	12.203830	10.000009	0	9.999991	47
44	0	7.806146	9871	12.193854	7.806155	9871	12.193845	10.000009	0	9.999991	46
45	0	7.815906	9651	12.184094	7.815915	9652	12.184085	10.000009	0	9.999991	45
46	0	7.825451	9442	12.174549	7.825460	9442	12.174540	10.000010	0	9.999990	44
47	0	7.834791	9240	12.165209	7.834801	9241	12.165199	10.000010	0	9.999990	43
48	0	7.843934	9048	12.156066	7.843944	9048	12.156056	10.000011	0	9.999989	42
49	0	7.852889	8864	12.147111	7.852900	8864	12.147100	10.000011	0	9.999989	41
50	0	7.861662	8686	12.138338	7.861674	8686	12.138326	10.000011	0	9.999989	40
51	0	7.870262	8515	12.129738	7.870274	8516	12.129729	10.000012	0	9.999988	39
52	0	7.878695	8352	12.121305	7.878708	8353	12.121296	10.000012	0	9.999988	38
53	0	7.886963	8195	12.113032	7.886981	8195	12.113019	10.000013	0	9.999987	37
54	0	7.895085	8042	12.104915	7.895099	8043	12.104901	10.000013	0	9.999987	36
55	0	7.903054	7896	12.096946	7.903068	7897	12.096932	10.000014	0	9.999986	35
56	0	7.910879	7756	12.089121	7.910894	7755	12.089106	10.000014	0	9.999986	34
57	0	7.918566	7619	12.081434	7.918581	7620	12.081419	10.000015	0	9.999985	33
58	0	7.926119	7488	12.073881	7.926134	7488	12.073866	10.000015	0	9.999985	32
59	0	7.933543	7361	12.066457	7.933559	7362	12.066441	10.000016	0	9.999984	31
60	0	7.940842	7238	12.059158	7.940858	7239	12.059142	10.000017	0	9.999983	30
80°											
5° 58'											
°	'	Sine	D.	Secant	Cotang.	D.	Tangent	Cosec.	D.	Sine	°

LOG. SINES. COSINES, &c.

(1) 2 ^m		U ^o											
1	2	Sine	D.	Cosec.	Tangent	D.	Cotang.	Secant	D.	Cosine	3 ^m	4 ^m	
30	0	7.940842	7238	12.059158	7.940853	7239	12.059142	10.000017	1	9.999983	30	30	
30	1	7.948020	7119	12.051980	7.948037	7120	12.051963	10.000017	1	9.999983	30	30	
31	4	7.955082	7005	12.044918	7.955100	7005	12.044900	10.000018	1	9.999982	30	29	
30	6	7.962031	6894	12.037969	7.962049	6894	12.037951	10.000018	1	9.999982	30	28	
32	8	7.968870	6785	12.031130	7.968889	6787	12.031111	10.000019	1	9.999981	30	28	
30	10	7.975603	6682	12.024397	7.975622	6682	12.024378	10.000019	1	9.999981	30	27	
33	12	7.982233	6580	12.017767	7.982253	6580	12.017747	10.000020	1	9.999980	30	27	
30	14	7.988764	6482	12.011236	7.988785	6483	12.011215	10.000021	1	9.999979	30	26	
34	16	7.995198	6387	12.004802	7.995219	6387	12.004781	10.000021	1	9.999979	42	26	
30	18	8.001538	6294	11.998462	8.001560	6295	11.998440	10.000022	1	9.999978	42	25	
35	20	8.007787	6204	11.992213	8.007809	6204	11.992191	10.000023	1	9.999977	40	25	
30	22	8.013947	6116	11.986053	8.013970	6118	11.986030	10.000023	1	9.999977	38	25	
36	24	8.020021	6032	11.979979	8.020045	6032	11.979956	10.000024	1	9.999976	36	24	
30	26	8.026011	5949	11.973989	8.026035	5950	11.973965	10.000024	1	9.999976	34	24	
37	28	8.031919	5869	11.968081	8.031945	5869	11.968055	10.000025	1	9.999975	32	23	
30	30	8.037749	5790	11.962251	8.037775	5792	11.962225	10.000026	1	9.999974	30	23	
38	32	8.043501	5715	11.956499	8.043527	5714	11.956473	10.000027	1	9.999973	28	22	
30	34	8.049178	5640	11.950822	8.049205	5641	11.950795	10.000027	1	9.999973	26	20	
30	36	8.054781	5567	11.945219	8.054809	5569	11.945191	10.000028	1	9.999972	24	21	
30	38	8.060314	5498	11.939686	8.060342	5498	11.939658	10.000029	1	9.999971	22	20	
40	40	8.065776	5428	11.934224	8.065806	5429	11.934194	10.000029	1	9.999971	20	20	
30	42	8.071171	5362	11.928829	8.071201	5362	11.928799	10.000030	1	9.999970	18	20	
41	44	8.076500	5296	11.923500	8.076531	5297	11.923469	10.000031	1	9.999969	16	19	
30	46	8.081764	5232	11.918236	8.081795	5233	11.918205	10.000032	1	9.999968	14	20	
42	48	8.086965	5170	11.913035	8.086997	5171	11.913003	10.000032	1	9.999968	12	18	
30	50	8.092104	5109	11.907896	8.092137	5110	11.907863	10.000033	1	9.999967	10	20	
43	52	8.097183	5050	11.902817	8.097217	5050	11.902783	10.000034	1	9.999966	8	17	
30	54	8.102204	4991	11.897796	8.102239	4993	11.897761	10.000035	1	9.999965	6	20	
44	56	8.107167	4935	11.892833	8.107203	4935	11.892797	10.000036	1	9.999964	4	16	
30	58	8.112074	4880	11.887926	8.112110	4881	11.887890	10.000036	1	9.999964	2	20	
45	60	8.116926	4825	11.883074	8.116963	4826	11.883037	10.000037	1	9.999963	0	15	
30	2	8.121725	4772	11.878275	8.121763	4773	11.878237	10.000038	1	9.999962	30	30	
46	4	8.126471	4721	11.873529	8.126510	4721	11.873490	10.000039	1	9.999961	30	14	
30	6	8.131166	4669	11.868834	8.131206	4671	11.868794	10.000040	1	9.999960	30	13	
47	8	8.135810	4620	11.864190	8.135851	4620	11.864149	10.000041	1	9.999959	30	13	
30	10	8.140406	4572	11.859594	8.140447	4572	11.859553	10.000041	1	9.999959	30	30	
48	12	8.144953	4523	11.855047	8.144996	4525	11.855004	10.000042	1	9.999958	30	12	
30	14	8.149453	4477	11.850547	8.149497	4478	11.850503	10.000043	1	9.999957	30	30	
49	16	8.153907	4431	11.846093	8.153952	4432	11.846048	10.000044	1	9.999956	44	11	
30	18	8.158316	4387	11.841684	8.158361	4388	11.841639	10.000045	1	9.999955	42	30	
50	20	8.162681	4343	11.837319	8.162727	4343	11.837273	10.000046	1	9.999954	40	10	
30	22	8.167002	4299	11.832998	8.167049	4301	11.832951	10.000047	1	9.999953	38	30	
51	24	8.171280	4258	11.828720	8.171328	4258	11.828672	10.000048	1	9.999952	36	0	
30	26	8.175517	4216	11.824483	8.175566	4217	11.824434	10.000049	1	9.999951	34	30	
52	28	8.179713	4176	11.820287	8.179763	4177	11.820237	10.000050	1	9.999950	32	8	
30	30	8.183869	4136	11.816131	8.183919	4137	11.816081	10.000051	1	9.999949	30	30	
53	32	8.187985	4096	11.812015	8.188036	4097	11.811964	10.000052	1	9.999948	28	7	
30	34	8.192062	4059	11.807938	8.192115	4060	11.807885	10.000053	1	9.999947	26	30	
54	36	8.196102	4021	11.803898	8.196156	4022	11.803844	10.000054	1	9.999946	24	6	
30	38	8.200104	3984	11.799896	8.200159	3985	11.799841	10.000055	1	9.999945	22	30	
55	40	8.204070	3948	11.795930	8.204126	3949	11.795874	10.000056	1	9.999944	20	5	
30	42	8.208000	3912	11.792000	8.208057	3913	11.791943	10.000057	1	9.999943	18	30	
56	44	8.211895	3877	11.788105	8.211953	3878	11.788047	10.000058	1	9.999942	16	4	
30	46	8.215755	3843	11.784245	8.215814	3844	11.784186	10.000059	1	9.999941	14	30	
57	48	8.219581	3810	11.780419	8.219641	3811	11.780359	10.000060	1	9.999940	12	3	
30	50	8.223374	3776	11.776626	8.223434	3777	11.776566	10.000061	1	9.999939	10	20	
58	52	8.227134	3743	11.772866	8.227195	3745	11.772805	10.000062	1	9.999938	8	2	
30	54	8.230861	3712	11.769139	8.230924	3712	11.769076	10.000063	1	9.999937	6	30	
59	56	8.234557	3680	11.765443	8.234621	3681	11.765379	10.000064	1	9.999936	4	1	
30	58	8.238221	3649	11.761779	8.238286	3651	11.761714	10.000065	1	9.999935	2	30	
60	60	8.241855	3619	11.758145	8.241921	3620	11.758079	10.000066	1	9.999934	0	0	
1	2	Cosine	D.	Secant	Cotang.	D.	Tangent	Cosec.	D.	Sine	3 ^m	4 ^m	

TABLE 68

LOG. SINES, COSINES, &c.													
(1) st 4 ^m		1 ^o											
°	'	Sine	D.	Cosec.	Tangent	D.	Cotang.	Secant	Parts	Cosine	sec.	'	"
0	0	8'241855	3619	11'758145	8'241921	3620	11'758079	10'000066					
30	1	8'245459	3589	11'754541	8'245526	3590	11'754474	10'000067	1 ^o	9'999934	56	60	
30	2	8'249033	3559	11'750967	8'249102	3560	11'750898	10'000068	2	9'999932	56	59	
30	3	8'252578	3531	11'747422	8'252648	3532	11'747352	10'000069	3	9'999931	54	58	
30	4	8'256094	3502	11'743906	8'256165	3503	11'743835	10'000071	4	9'999929	52	58	
30	5	8'259582	3474	11'740418	8'259654	3475	11'740346	10'000072	5	9'999928	50	58	
30	6	8'263042	3446	11'736958	8'263115	3448	11'736885	10'000073	6	9'999927	48	57	
30	7	8'266475	3419	11'733525	8'266549	3420	11'733451	10'000074	7	9'999926	46	56	
30	8	8'269881	3393	11'730119	8'269956	3394	11'730044	10'000075	8	9'999925	44	56	
30	9	8'273260	3366	11'726740	8'273337	3367	11'726663	10'000076	9	9'999924	42	56	
30	10	8'276614	3341	11'723386	8'276691	3342	11'723309	10'000078	10	9'999922	40	55	
30	11	8'279941	3314	11'720001	8'280020	3316	11'719980	10'000079	11	9'999921	38	55	
30	12	8'283243	3290	11'716757	8'283323	3291	11'716677	10'000080	12	9'999920	36	54	
30	13	8'286521	3265	11'713479	8'286602	3266	11'713398	10'000081	13	9'999919	34	54	
30	14	8'289773	3241	11'710227	8'289856	3242	11'710144	10'000082	14	9'999918	32	53	
30	15	8'293002	3216	11'706998	8'293086	3218	11'706914	10'000084	15	9'999916	30	53	
30	16	8'296207	3193	11'703793	8'296292	3194	11'703708	10'000085	16	9'999915	28	52	
30	17	8'299388	3170	11'700612	8'299474	3171	11'700526	10'000086	17	9'999914	26	52	
30	18	8'302546	3147	11'697454	8'302634	3148	11'697366	10'000087	18	9'999913	24	51	
30	19	8'305681	3124	11'694319	8'305770	3125	11'694230	10'000089	19	9'999911	22	50	
30	20	8'308794	3102	11'691206	8'308884	3103	11'691116	10'000090	20	9'999910	20	50	
30	21	8'311885	3080	11'688115	8'311976	3081	11'688024	10'000091	21	9'999909	18	50	
30	22	8'314954	3058	11'685046	8'315046	3059	11'684954	10'000093	22	9'999907	16	49	
30	23	8'318001	3036	11'681999	8'318095	3038	11'681905	10'000094	23	9'999906	14	49	
30	24	8'321027	3016	11'678973	8'321122	3017	11'678878	10'000095	24	9'999905	12	48	
30	25	8'324032	2995	11'675968	8'324129	2996	11'675871	10'000097	25	9'999903	10	48	
30	26	8'327016	2974	11'672984	8'327114	2975	11'672886	10'000098	26	9'999902	8	47	
30	27	8'329980	2954	11'670020	8'330080	2956	11'669920	10'000099	27	9'999901	6	46	
30	28	8'332924	2934	11'667076	8'333025	2935	11'666975	10'000101	28	9'999899	4	46	
30	29	8'335848	2914	11'664152	8'335950	2916	11'664050	10'000102	29	9'999898	2	45	
30	30	8'338753	2895	11'661247	8'338856	2896	11'661144	10'000103	30	9'999897	58	45	
30	31	8'341638	2876	11'658362	8'341743	2877	11'658257	10'000105	1	9'999895	56	45	
30	32	8'344504	2856	11'655496	8'344610	2858	11'655390	10'000106	2	9'999894	54	44	
30	33	8'347351	2838	11'652648	8'347459	2840	11'652541	10'000108	3	9'999892	51	44	
30	34	8'350181	2820	11'649819	8'350289	2821	11'649711	10'000109	4	9'999891	52	43	
30	35	8'352901	2801	11'646909	8'353101	2803	11'646899	10'000110	5	9'999890	50	43	
30	36	8'355783	2784	11'644217	8'355895	2784	11'644105	10'000112	6	9'999888	48	42	
30	37	8'358558	2766	11'641442	8'358671	2768	11'641329	10'000113	7	9'999887	46	42	
30	38	8'361315	2748	11'638685	8'361430	2749	11'638570	10'000115	8	9'999885	44	41	
30	39	8'364055	2731	11'635945	8'364171	2733	11'635829	10'000116	9	9'999884	42	40	
30	40	8'366777	2714	11'633223	8'366895	2715	11'633105	10'000118	10	9'999882	40	40	
30	41	8'369482	2697	11'630518	8'369601	2699	11'630399	10'000119	11	9'999881	38	39	
30	42	8'372171	2680	11'627829	8'372292	2681	11'627708	10'000121	12	9'999879	36	39	
30	43	8'374843	2664	11'625157	8'374965	2666	11'625035	10'000122	13	9'999878	34	38	
30	44	8'377499	2648	11'622501	8'377622	2649	11'622378	10'000124	14	9'999876	32	38	
30	45	8'380138	2631	11'619862	8'380263	2633	11'619737	10'000125	15	9'999875	30	38	
30	46	8'382762	2616	11'617238	8'382889	2617	11'617111	10'000127	16	9'999873	28	37	
30	47	8'385370	2600	11'614630	8'385498	2602	11'614502	10'000128	17	9'999872	26	37	
30	48	8'387962	2585	11'612038	8'388092	2586	11'611908	10'000130	18	9'999870	24	36	
30	49	8'390539	2569	11'609461	8'390670	2571	11'609330	10'000131	19	9'999869	22	36	
30	50	8'393101	2554	11'606899	8'393234	2556	11'606766	10'000133	20	9'999867	20	36	
30	51	8'395647	2539	11'604352	8'395782	2540	11'604218	10'000134	21	9'999866	18	35	
30	52	8'398179	2525	11'601821	8'398315	2526	11'601685	10'000136	22	9'999864	16	34	
30	53	8'400696	2510	11'599304	8'400834	2512	11'599166	10'000137	23	9'999863	14	34	
30	54	8'403199	2495	11'596801	8'403338	2497	11'596662	10'000139	24	9'999861	12	33	
30	55	8'405687	2481	11'594313	8'405828	2483	11'594172	10'000141	25	9'999859	10	33	
30	56	8'408161	2467	11'591839	8'408304	2468	11'591696	10'000142	26	9'999858	8	32	
30	57	8'410621	2453	11'589379	8'410765	2455	11'589232	10'000144	27	9'999856	6	32	
30	58	8'413068	2440	11'586932	8'413213	2441	11'586787	10'000146	28	9'999854	4	31	
30	59	8'415500	2425	11'584500	8'415647	2427	11'584353	10'000147	29	9'999853	2	30	
30	60	8'417919	2412	11'582081	8'418068	2414	11'581932	10'000149	30	9'999851	0	30	
1 st	2 nd	Cosine	D.	Secant	Cotang.	D.	Tangent	Cosec.	Parts	Sine	sec.	'	"
88°													
51 54 ^m													

LOG. SINES, COSINES, &c.

0° 6'			1°												
°	'	m.	Sine	D.	Cosec.	Tangent	D.	Cotang.	Secant	Parts	Cosine	m.	°		
30	0	8	417919	2412	11582081	8418068	2414	11581932	10000149		9999851	58	30		
30	2	8	420325	2399	11579675	8420475	2401	11579525	10000151	1 0	9999849	58	30		
31	1	8	422717	2386	11577283	8422869	2387	11577131	10000152	2 0	9999848	58	29		
30	6	8	425096	2373	11574904	8425250	2374	11574750	10000154	3 0	9999846	58	30		
32	8	8	427462	2359	11572538	8427618	2362	11572382	10000156	4 0	9999844	52	28		
30	10	8	429815	2347	11570185	8429973	2348	11570027	10000157	5 0	9999843	50	30		
33	12	8	432156	2335	11567844	8432315	2336	11567685	10000159	6 0	9999841	48	27		
30	14	8	434484	2322	11565516	8434645	2324	11565355	10000161	7 0	9999839	46	30		
34	16	8	436800	2309	11563200	8436962	2311	11563038	10000162	8 0	9999838	44	26		
30	18	8	439103	2297	11560897	8439267	2299	11560733	10000164	9 0	9999836	42	30		
35	20	8	441394	2286	11558606	8441560	2287	11558440	10000166	10 1	9999834	40	25		
30	22	8	443674	2273	11556326	8443841	2275	11556159	10000168	11 1	9999832	38	30		
36	24	8	445941	2261	11554059	8446110	2263	11553890	10000169	12 1	9999831	36	24		
30	26	8	448196	2250	11551804	8448368	2252	11551632	10000171	13 1	9999829	34	30		
37	28	8	450440	2238	11549560	8450613	2240	11549387	10000173	14 1	9999827	32	23		
30	30	8	452673	2226	11547327	8452847	2228	11547153	10000175	15 1	9999825	30	30		
38	32	8	454893	2216	11545107	8455070	2217	11544930	10000176	16 1	9999824	28	22		
30	34	8	457103	2203	11542897	8457281	2206	11542719	10000178	17 1	9999822	26	30		
30	36	8	459301	2193	11540699	8459481	2194	11540519	10000180	18 1	9999820	24	21		
30	38	8	461489	2182	11538511	8461670	2184	11538330	10000182	19 1	9999818	22	30		
40	40	8	463665	2171	11536335	8463849	2173	11536151	10000184	20 1	9999816	20	20		
30	42	8	465830	2160	11534170	8466016	2162	11533984	10000186	21 1	9999814	18	30		
41	44	8	467985	2149	11532015	8468172	2151	11531828	10000187	22 1	9999813	16	19		
30	46	8	470129	2139	11529871	8470318	2140	11529682	10000189	23 1	9999811	14	30		
42	48	8	472263	2128	11527737	8472454	2131	11527546	10000191	24 1	9999809	12	18		
30	50	8	474386	2118	11525614	8474579	2119	11525421	10000193	25 2	9999807	10	30		
43	52	8	476498	2108	11523502	8476693	2110	11523307	10000195	26 2	9999805	8	17		
30	54	8	478601	2097	11521399	8478798	2095	11521202	10000197	27 2	9999803	6	30		
44	56	8	480693	2088	11519307	8480892	2089	11519108	10000199	28 2	9999801	4	16		
30	58	8	482776	2077	11517224	8482976	2080	11517024	10000201	29 2	9999799	2	30		
45	0	8	484848	2067	11515152	8485050	2069	11514950	10000203	30 2	9999797	0	15		
30	2	8	486910	2058	11513090	8487115	2060	11512885	10000205	1 0	9999795	58	28		
46	4	8	488963	2048	11511037	8489170	2049	11510830	10000206	2 0	9999794	56	14		
30	6	8	491006	2038	11508994	8491215	2041	11508785	10000208	3 0	9999792	54	3		
47	8	8	493040	2029	11506960	8493250	2030	11506750	10000210	4 0	9999790	52	13		
30	10	8	495064	2019	11504936	8495276	2022	11504724	10000212	5 0	9999788	50	30		
48	12	8	497078	2010	11502922	8497293	2012	11502707	10000214	6 0	9999786	48	12		
30	14	8	499084	2001	11500916	8499300	2002	11500700	10000216	7 0	9999784	46	30		
49	16	8	501080	1991	11498920	8501298	1994	11498702	10000218	8 1	9999782	44	11		
30	18	8	503067	1983	11496933	8503287	1984	11496713	10000220	9 1	9999780	42	30		
50	20	8	505045	1973	11494955	8505267	1976	11494733	10000222	10 1	9999778	40	10		
30	22	8	507014	1965	11492986	8507238	1966	11492762	10000224	11 1	9999776	38	30		
51	24	8	508974	1955	11491026	8509200	1958	11490800	10000226	12 1	9999774	36	9		
30	26	8	510925	1947	11489075	8511153	1949	11488847	10000228	13 1	9999772	34	30		
52	28	8	512867	1938	11487133	8513098	1940	11486902	10000230	14 1	9999769	32	8		
30	30	8	514801	1930	11485199	8515034	1931	11484966	10000233	15 1	9999767	30	30		
53	32	8	516726	1921	11483274	8516961	1923	11483039	10000235	16 1	9999765	28	7		
30	34	8	518643	1912	11481357	8518880	1915	11481120	10000237	17 1	9999763	26	30		
54	36	8	520551	1904	11479449	8520790	1906	11479210	10000239	18 1	9999761	24	6		
30	38	8	522451	1896	11477549	8522692	1898	11477308	10000241	19 1	9999759	22	30		
55	40	8	524343	1888	11475657	8524586	1890	11475414	10000243	20 1	9999757	20	5		
30	42	8	526226	1879	11473774	8526472	1881	11473528	10000245	21 1	9999755	18	30		
56	44	8	528102	1871	11471898	8528349	1874	11471651	10000247	22 2	9999753	16	4		
30	46	8	529969	1864	11470031	8530218	1865	11469782	10000249	23 2	9999751	14	30		
57	48	8	531828	1855	11468172	8532080	1857	11467920	10000252	24 2	9999748	12	3		
30	50	8	533679	1847	11466321	8533933	1850	11466067	10000254	25 2	9999746	10	30		
58	52	8	535523	1840	11464477	8535779	1842	11464221	10000256	26 2	9999744	8	2		
30	54	8	537358	1831	11462642	8537617	1834	11462383	10000258	27 2	9999742	6	30		
59	56	8	539186	1824	11460814	8539447	1826	11460553	10000260	28 2	9999740	4	1		
30	58	8	541007	1817	11458993	8541269	1818	11458731	10000262	29 2	9999738	2	30		
60	0	8	542819	1809	11457181	8543084	1811	11456916	10000265	30 2	9999735	0	0		
°	'	m.	Cosine	D.	Secant	Cotang.	D.	Tangent	Cosec.	Parts	Sine	m.	°		

85°

5° 52m

LOG. SINES, COSINES, &c.

(h 8m		2°											
' "	m.	Sine	D.	Cosec.	Tangent	D.	Cotang.	Secant	Parts	Cosine	m.	' "	' "
0	0	8.542819	1809	11.457181	8.543084	1811	11.456116	10.000265		9.999735	52	60	
0	1	8.544624	1801	11.455376	8.544891	1804	11.455109	10.000267	1" 0	9.999733	56	30	
1	4	8.546422	1794	11.453578	8.546691	1796	11.453309	10.000269	2 0	9.999731	56	50	
2	6	8.548212	1786	11.451788	8.548483	1789	11.451517	10.000271	3 0	9.999729	54	30	
3	8	8.549995	1779	11.450005	8.550268	1781	11.449732	10.000274	4 0	9.999726	52	58	
30	10	8.551770	1772	11.448230	8.552046	1774	11.447954	10.000276	5 0	9.999724	50	30	
3	12	8.553539	1765	11.446461	8.553817	1767	11.446183	10.000278	6 0	9.999722	48	57	
30	14	8.555300	1758	11.444700	8.555580	1760	11.444420	10.000280	7 1	9.999720	46	30	
4	16	8.557054	1750	11.442946	8.557336	1753	11.442664	10.000283	8 1	9.999717	44	56	
5	18	8.558801	1743	11.441199	8.559085	1745	11.440915	10.000285	9 1	9.999715	42	30	
5	20	8.560540	1737	11.439460	8.560828	1739	11.439172	10.000287	10 1	9.999713	40	55	
20	22	8.562273	1729	11.437727	8.562563	1732	11.437437	10.000289	11 1	9.999711	38	30	
6	24	8.563999	1723	11.436001	8.564291	1725	11.435709	10.000292	12 1	9.999708	36	54	
20	26	8.565719	1716	11.434281	8.566013	1718	11.433987	10.000294	13 1	9.999706	34	30	
7	28	8.567431	1709	11.432569	8.567727	1711	11.432273	10.000296	14 1	9.999704	32	53	
20	30	8.569137	1702	11.430863	8.569435	1705	11.430565	10.000299	15 1	9.999701	30	30	
8	32	8.570836	1696	11.429164	8.571137	1698	11.428863	10.000301	16 1	9.999699	28	52	
20	34	8.572528	1689	11.427472	8.572832	1692	11.427168	10.000304	17 1	9.999696	26	30	
9	36	8.574214	1682	11.425786	8.574520	1684	11.425480	10.000306	18 1	9.999694	24	51	
20	38	8.575893	1676	11.424107	8.576201	1679	11.423799	10.000308	19 1	9.999692	22	30	
10	40	8.577566	1670	11.422434	8.577877	1672	11.422123	10.000311	20 2	9.999689	20	50	
30	42	8.579232	1663	11.420768	8.579545	1665	11.420455	10.000313	21 2	9.999687	18	30	
11	44	8.580892	1657	11.419108	8.581208	1660	11.418792	10.000315	22 2	9.999685	16	49	
20	46	8.582546	1650	11.417454	8.582864	1652	11.417136	10.000318	23 2	9.999682	14	30	
12	48	8.584193	1645	11.415807	8.584514	1647	11.415486	10.000320	24 2	9.999680	12	48	
30	50	8.585834	1638	11.414166	8.586157	1641	11.413843	10.000323	25 2	9.999677	10	30	
13	52	8.587469	1632	11.412531	8.587795	1634	11.412205	10.000325	26 2	9.999675	8	47	
20	54	8.589098	1625	11.410902	8.589426	1628	11.410574	10.000328	27 2	9.999672	6	30	
14	56	8.590721	1620	11.409279	8.591051	1622	11.408949	10.000330	28 2	9.999670	4	46	
20	58	8.592338	1614	11.407662	8.592670	1616	11.407330	10.000332	29 2	9.999668	2	30	
15	0	8.593948	1607	11.406052	8.594283	1611	11.405717	10.000335	30 2	9.999665	51	45	
30	2	8.595553	1602	11.404447	8.595890	1604	11.404110	10.000337	1 0	9.999663	38	30	
16	4	8.597152	1596	11.402848	8.597492	1598	11.402508	10.000340	2 0	9.999660	36	44	
20	6	8.598745	1590	11.401254	8.599087	1593	11.400913	10.000342	3 0	9.999658	34	30	
17	8	8.600332	1584	11.399668	8.600677	1586	11.399323	10.000345	4 0	9.999655	32	43	
30	10	8.601913	1579	11.398087	8.602260	1581	11.397740	10.000347	5 0	9.999653	30	30	
18	12	8.603489	1572	11.396511	8.603839	1576	11.396161	10.000350	6 1	9.999650	28	42	
20	14	8.605058	1567	11.394942	8.605411	1569	11.394589	10.000353	7 1	9.999647	26	30	
19	16	8.606623	1562	11.393377	8.606978	1564	11.393022	10.000355	8 1	9.999645	24	41	
30	18	8.608181	1555	11.391819	8.608539	1558	11.391461	10.000358	9 1	9.999642	22	30	
20	20	8.609734	1551	11.390266	8.610094	1553	11.389906	10.000360	10 1	9.999640	20	40	
30	22	8.611282	1544	11.388718	8.611644	1547	11.388356	10.000363	11 1	9.999637	18	30	
21	24	8.612823	1539	11.387177	8.613189	1542	11.386811	10.000365	12 1	9.999635	16	30	
20	26	8.614360	1534	11.385640	8.614728	1536	11.385272	10.000368	13 1	9.999632	14	30	
22	28	8.615891	1529	11.384109	8.616262	1531	11.383738	10.000371	14 1	9.999629	12	38	
30	30	8.617417	1522	11.382583	8.617790	1526	11.382210	10.000373	15 1	9.999627	10	30	
23	32	8.618937	1518	11.381063	8.619313	1520	11.380687	10.000376	16 1	9.999624	8	37	
20	34	8.620452	1512	11.379548	8.620830	1515	11.379170	10.000378	17 2	9.999622	6	30	
24	36	8.621962	1508	11.378038	8.622343	1510	11.377657	10.000381	18 2	9.999619	21	36	
20	38	8.623466	1501	11.376534	8.623850	1505	11.376150	10.000384	19 2	9.999616	22	30	
25	40	8.624965	1497	11.375035	8.625352	1499	11.374648	10.000386	20 2	9.999614	20	35	
26	42	8.626459	1492	11.373541	8.626849	1494	11.373151	10.000389	21 2	9.999611	18	30	
20	44	8.627948	1486	11.372052	8.628340	1489	11.371660	10.000392	22 2	9.999608	16	34	
20	46	8.629432	1481	11.370568	8.629827	1484	11.370173	10.000394	23 2	9.999606	14	30	
27	48	8.630911	1477	11.369089	8.631308	1479	11.368692	10.000397	24 2	9.999603	12	33	
30	50	8.632385	1471	11.367615	8.632785	1474	11.367215	10.000400	25 2	9.999600	10	30	
28	52	8.633854	1466	11.366146	8.634256	1469	11.365744	10.000403	26 2	9.999597	8	32	
20	54	8.635317	1462	11.364683	8.635723	1464	11.364277	10.000405	27 2	9.999595	6	30	
20	56	8.636776	1456	11.363224	8.637184	1459	11.362816	10.000408	28 3	9.999592	4	31	
30	58	8.638230	1452	11.361770	8.638641	1455	11.361359	10.000411	29 3	9.999589	2	30	
30	60	8.639680	1446	11.360320	8.640093	1449	11.359907	10.000414	30 3	9.999586	0	30	
' "	m.	Cosine	D.	Secant	Cotang.	D.	Tangent	Cosec.	Parts	Sine	m.	' "	' "

TABLE 68

748

LOG. SINES, COSINES, &c.

0° 10'		2°											
°	'	Sine	D.	Cosec.	Tangent	D.	Cotang.	Secant	Parts	Cosine	m.	°	'
30	0	8.639680	1446	11.360320	8.640093	1449	11.359907	10.000414		9.999586	80	30	0
30	1	8.641124	1442	11.358876	8.641540	1445	11.358460	10.000416	1"	9.999584	58	30	1
31	0	8.642563	1437	11.357437	8.642982	1440	11.357018	10.000419	2	9.999581	56	30	0
31	1	8.643998	1433	11.356002	8.644420	1435	11.355580	10.000422	3	9.999578	54	30	1
32	0	8.645428	1427	11.354572	8.645853	1431	11.354147	10.000425	4	9.999575	52	30	0
32	1	8.646854	1423	11.353146	8.647281	1425	11.352719	10.000427	5	9.999573	50	30	1
33	0	8.648274	1419	11.351726	8.648704	1421	11.351296	10.000430	6	9.999570	48	30	0
33	1	8.649690	1413	11.350310	8.650123	1417	11.349877	10.000433	7	9.999567	46	30	1
34	0	8.651102	1410	11.348898	8.651537	1412	11.348463	10.000436	8	9.999564	44	30	0
34	1	8.652508	1404	11.347492	8.652947	1407	11.347053	10.000439	9	9.999561	42	30	1
35	0	8.653911	1400	11.346089	8.654352	1403	11.345648	10.000442	10	9.999558	40	30	0
35	1	8.655308	1396	11.344692	8.655753	1399	11.344247	10.000444	11	9.999556	38	30	1
36	0	8.656702	1391	11.343298	8.657149	1393	11.342851	10.000447	12	9.999553	36	30	0
36	1	8.658090	1386	11.341910	8.658541	1390	11.341459	10.000450	13	9.999550	34	30	1
37	0	8.659475	1382	11.340525	8.659928	1385	11.340072	10.000453	14	9.999547	32	30	0
37	1	8.660855	1378	11.339145	8.661311	1381	11.338689	10.000456	15	9.999544	30	30	1
38	0	8.662230	1373	11.337770	8.662689	1376	11.337311	10.000459	16	9.999541	28	30	0
38	1	8.663602	1370	11.336398	8.664063	1372	11.335937	10.000462	17	9.999538	26	30	1
39	0	8.664968	1364	11.335032	8.665433	1367	11.334567	10.000465	18	9.999535	24	30	0
39	1	8.666331	1361	11.333666	8.666799	1364	11.333201	10.000468	19	9.999532	22	30	1
40	0	8.667689	1356	11.332311	8.668160	1359	11.331840	10.000471	20	9.999529	20	30	0
40	1	8.669043	1352	11.330957	8.669517	1355	11.330483	10.000473	21	9.999527	18	30	1
41	0	8.670393	1348	11.329607	8.670870	1351	11.329130	10.000476	22	9.999524	16	30	0
41	1	8.671739	1343	11.328261	8.672218	1346	11.327782	10.000479	23	9.999521	14	30	1
42	0	8.673080	1340	11.326920	8.673563	1343	11.326437	10.000482	24	9.999518	12	30	0
42	1	8.674418	1335	11.325582	8.674903	1338	11.325097	10.000485	25	9.999515	10	30	1
43	0	8.675751	1331	11.324249	8.676239	1334	11.323761	10.000488	26	9.999512	8	30	0
43	1	8.677080	1327	11.322920	8.677572	1330	11.322428	10.000491	27	9.999509	6	30	1
44	0	8.678405	1323	11.321595	8.678900	1326	11.321100	10.000494	28	9.999506	4	30	0
44	1	8.679726	1319	11.320274	8.680224	1322	11.319776	10.000497	29	9.999503	2	30	1
45	0	8.681043	1315	11.318957	8.681544	1318	11.318456	10.000500	30	9.999500	0	30	0
45	1	8.682356	1311	11.317644	8.682860	1314	11.317140	10.000503	1	9.999497	58	30	1
46	0	8.683665	1308	11.316333	8.684172	1311	11.315828	10.000507	2	9.999493	56	30	0
46	1	8.684971	1303	11.315029	8.685480	1306	11.314520	10.000510	3	9.999490	54	30	1
47	0	8.686272	1299	11.313728	8.686784	1302	11.313216	10.000513	4	9.999487	52	30	0
47	1	8.687569	1295	11.312431	8.688085	1299	11.311915	10.000516	5	9.999484	50	30	1
48	0	8.688863	1292	11.311137	8.689381	1294	11.310619	10.000519	6	9.999481	48	30	0
48	1	8.690152	1288	11.309848	8.690674	1291	11.309326	10.000522	7	9.999478	46	30	1
49	0	8.691438	1283	11.308562	8.691963	1287	11.308037	10.000525	8	9.999475	44	30	0
49	1	8.692720	1280	11.307280	8.693248	1283	11.306752	10.000528	9	9.999472	42	30	1
50	0	8.693998	1277	11.306002	8.694529	1280	11.305471	10.000531	10	9.999469	40	30	0
50	1	8.695272	1272	11.304728	8.695807	1275	11.304193	10.000534	11	9.999466	38	30	1
51	0	8.696543	1269	11.303457	8.697081	1272	11.302919	10.000537	12	9.999463	36	30	0
51	1	8.697810	1265	11.302190	8.698351	1268	11.301649	10.000541	13	9.999459	34	30	1
52	0	8.699073	1262	11.300927	8.699617	1265	11.300383	10.000544	14	9.999456	32	30	0
52	1	8.700333	1257	11.299667	8.700880	1261	11.299120	10.000547	15	9.999453	30	30	1
53	0	8.701589	1255	11.298411	8.702139	1257	11.297861	10.000550	16	9.999450	28	30	0
53	1	8.702841	1250	11.297159	8.703395	1254	11.296605	10.000553	17	9.999447	26	30	1
54	0	8.704090	1247	11.295910	8.704646	1250	11.295354	10.000557	18	9.999443	24	30	0
54	1	8.705335	1243	11.294665	8.705895	1247	11.294105	10.000560	19	9.999440	22	30	1
55	0	8.706577	1240	11.293423	8.707140	1243	11.292860	10.000563	20	9.999437	20	30	0
55	1	8.707815	1236	11.292185	8.708381	1239	11.291619	10.000566	21	9.999434	18	30	1
56	0	8.709049	1233	11.290951	8.709618	1236	11.290382	10.000569	22	9.999431	16	30	0
56	1	8.710280	1229	11.289720	8.710853	1233	11.289147	10.000573	23	9.999427	14	30	1
57	0	8.711507	1226	11.288493	8.712083	1228	11.287917	10.000576	24	9.999424	12	30	0
57	1	8.712731	1222	11.287268	8.713311	1226	11.286689	10.000579	25	9.999421	10	30	1
58	0	8.713952	1219	11.286048	8.714534	1222	11.285466	10.000582	26	9.999418	8	30	0
58	1	8.715169	1216	11.284831	8.715755	1219	11.284245	10.000586	27	9.999414	6	30	1
59	0	8.716383	1212	11.283617	8.716972	1215	11.283028	10.000589	28	9.999411	4	30	0
59	1	8.717593	1208	11.282406	8.718186	1212	11.281814	10.000592	29	9.999408	2	30	1
60	0	8.718800	1205	11.281200	8.719396	1209	11.281060	10.000596	30	9.999404	0	30	0
60	1												
61	0												
61	1												
62	0												
62	1												
63	0												
63	1												
64	0												
64	1												
65	0												
65	1												
66	0												
66	1												
67	0												
67	1												
68	0												
68	1												
69	0												
69	1												
70	0												
70	1												

LOG. SINES, COSINES, &c.

0 ^h 12 ^m		3 ^o									
°	'	Sine	D.	Cosec.	Tangent	D.	Cotang.	Secant	Parts	Cosine	°
0	0	8°718800	1205	11°281200	8°719396	1209	11°280604	10°000596		9°999404	0
30	2	8°720004	1202	11°279996	8°720603	1205	11°279397	10°000599	1°0	9°999401	30
1	4	8°721204	1199	11°278796	8°721806	1202	11°278194	10°000602	2 0	9°999398	60
2	6	8°722401	1195	11°277599	8°723007	1198	11°276993	10°000606	3 0	9°999394	90
3	8	8°723595	1192	11°276405	8°724204	1196	11°275796	10°000609	4 0	9°999391	120
4	10	8°724785	1189	11°275215	8°725397	1192	11°274603	10°000612	5 1	9°999388	150
5	12	8°725972	1185	11°274028	8°726588	1189	11°273412	10°000616	6 1	9°999384	180
6	14	8°727156	1183	11°272844	8°727775	1185	11°272225	10°000619	7 1	9°999381	210
7	16	8°728337	1179	11°271663	8°728959	1183	11°271041	10°000622	8 1	9°999378	240
8	18	8°729514	1176	11°270486	8°730140	1179	11°269860	10°000626	9 1	9°999374	270
9	20	8°730688	1172	11°269312	8°731317	1176	11°268683	10°000629	10 1	9°999371	300
10	22	8°731859	1170	11°268141	8°732492	1173	11°267508	10°000633	11 1	9°999367	330
11	24	8°733027	1166	11°266973	8°733663	1170	11°266337	10°000636	12 1	9°999364	360
12	26	8°734192	1163	11°265808	8°734831	1166	11°265169	10°000639	13 1	9°999361	390
13	28	8°735354	1160	11°264646	8°735996	1164	11°264004	10°000642	14 2	9°999357	420
14	30	8°736512	1157	11°263488	8°737158	1160	11°262842	10°000646	15 2	9°999354	450
15	32	8°737667	1154	11°262333	8°738317	1158	11°261683	10°000650	16 2	9°999350	480
16	34	8°738820	1151	11°261180	8°739473	1154	11°260527	10°000653	17 2	9°999347	510
17	36	8°739969	1148	11°260031	8°740626	1151	11°259374	10°000657	18 2	9°999343	540
18	38	8°741115	1144	11°258885	8°741776	1148	11°258224	10°000660	19 2	9°999340	570
19	40	8°742259	1142	11°257741	8°742922	1146	11°257078	10°000664	20 2	9°999336	600
20	42	8°743399	1139	11°256601	8°744066	1142	11°255934	10°000667	21 2	9°999333	630
21	44	8°744536	1136	11°255464	8°745207	1139	11°254793	10°000671	22 3	9°999329	660
22	46	8°745670	1132	11°254330	8°746344	1136	11°253656	10°000674	23 3	9°999326	690
23	48	8°746802	1130	11°253198	8°747479	1134	11°252521	10°000678	24 3	9°999322	720
24	50	8°747930	1127	11°252070	8°748611	1130	11°251389	10°000681	25 3	9°999319	750
25	52	8°749055	1124	11°250945	8°749740	1127	11°250260	10°000685	26 3	9°999315	780
26	54	8°750178	1121	11°249822	8°750866	1125	11°249134	10°000688	27 3	9°999312	810
27	56	8°751297	1118	11°248703	8°751989	1122	11°248011	10°000692	28 3	9°999308	840
28	58	8°752414	1115	11°247586	8°753109	1119	11°246891	10°000695	29 3	9°999305	870
29	60	8°753528	1113	11°246472	8°754227	1116	11°245773	10°000699	30 3	9°999301	900
30	2	8°754639	1109	11°245361	8°755341	1113	11°244659	10°000703	1 0	9°999297	930
31	4	8°755747	1107	11°244253	8°756453	1110	11°243547	10°000706	2 0	9°999294	960
32	6	8°756852	1104	11°243148	8°757562	1107	11°242438	10°000710	3 0	9°999290	990
33	8	8°757955	1101	11°242045	8°758668	1105	11°241332	10°000713	4 0	9°999287	1020
34	10	8°759054	1098	11°240946	8°759771	1102	11°240229	10°000717	5 1	9°999283	1050
35	12	8°760151	1096	11°239849	8°760872	1099	11°239128	10°000721	6 1	9°999279	1080
36	14	8°761245	1092	11°238755	8°761990	1097	11°238030	10°000724	7 1	9°999276	1110
37	16	8°762337	1090	11°237663	8°763065	1093	11°236935	10°000728	8 1	9°999272	1140
38	18	8°763425	1088	11°236575	8°764157	1091	11°235843	10°000732	9 1	9°999268	1170
39	20	8°764511	1084	11°235489	8°765246	1088	11°234754	10°000735	10 1	9°999265	1200
40	22	8°765594	1082	11°234406	8°766333	1086	11°233667	10°000739	11 1	9°999261	1230
41	24	8°766675	1079	11°233325	8°767417	1083	11°232583	10°000743	12 1	9°999257	1260
42	26	8°767752	1076	11°232248	8°768499	1080	11°231501	10°000746	13 2	9°999254	1290
43	28	8°768828	1074	11°231172	8°769578	1077	11°230422	10°000750	14 2	9°999250	1320
44	30	8°769900	1071	11°230100	8°770654	1075	11°229346	10°000754	15 2	9°999246	1350
45	32	8°770970	1069	11°229030	8°771727	1072	11°228273	10°000758	16 2	9°999242	1380
46	34	8°772037	1065	11°227963	8°772798	1070	11°227202	10°000761	17 2	9°999239	1410
47	36	8°773101	1064	11°226899	8°773866	1067	11°226134	10°000765	18 2	9°999235	1440
48	38	8°774163	1060	11°225837	8°774932	1064	11°225068	10°000769	19 2	9°999231	1470
49	40	8°775223	1058	11°224777	8°775995	1062	11°224005	10°000773	20 2	9°999227	1500
50	42	8°776279	1056	11°223721	8°777056	1059	11°222944	10°000776	21 3	9°999224	1530
51	44	8°777333	1053	11°222667	8°778114	1057	11°221886	10°000780	22 3	9°999220	1560
52	46	8°778385	1050	11°221615	8°779169	1054	11°220831	10°000784	23 3	9°999216	1590
53	48	8°779434	1048	11°220566	8°780222	1051	11°219778	10°000788	24 3	9°999212	1620
54	50	8°780480	1045	11°219520	8°781272	1049	11°218728	10°000792	25 3	9°999208	1650
55	52	8°781524	1043	11°218476	8°782320	1047	11°217680	10°000795	26 3	9°999205	1680
56	54	8°782566	1040	11°217434	8°783365	1044	11°216635	10°000799	27 3	9°999201	1710
57	56	8°783605	1037	11°216395	8°784408	1041	11°215592	10°000803	28 3	9°999197	1740
58	58	8°784641	1036	11°215359	8°785448	1040	11°214552	10°000807	29 4	9°999193	1770
59	60	8°785675	1032	11°214325	8°786486	1036	11°213514	10°000811	30 4	9°999189	1800
°	'	Cosine	D.	Secant	Cotang.	D.	Tangent	Cosec.	Parts	Sine	°

TABLE 68

745

LOG. SINES, COSINES, &c.

0° 14'			3°												
°	'	m.	Sine	D.	Cosec.	Tangent	D.	Cotang.	Secant	Parts	Cosine	m.	°	'	
30	0	8.785675	1032	11.214325	8.786486	1036	11.213514	10.000811	1	9.999189	46	30			
30	2	8.786707	1031	11.213293	8.787521	1034	11.212479	10.000815	2	9.999185	58	30			
31	4	8.787737	1028	11.212264	8.788554	1032	11.211446	10.000819	3	9.999181	50	29			
31	6	8.788762	1025	11.211238	8.789585	1029	11.210415	10.000822	4	9.999178	51	30			
32	8	8.789787	1023	11.210213	8.790613	1027	11.209387	10.000826	5	9.999174	52	28			
32	10	8.790808	1020	11.209192	8.791639	1025	11.208361	10.000830	6	9.999170	50	30			
33	12	8.791828	1019	11.208172	8.792662	1022	11.207338	10.000834	7	9.999166	48	27			
33	14	8.792845	1015	11.207155	8.793683	1019	11.206317	10.000838	8	9.999162	46	30			
34	16	8.793859	1014	11.206141	8.794701	1018	11.205299	10.000842	9	9.999158	44	28			
34	18	8.794872	1011	11.205128	8.795718	1015	11.204282	10.000846	10	9.999154	42	30			
35	20	8.795881	1009	11.204119	8.796731	1012	11.203269	10.000850	11	9.999150	40	25			
35	22	8.796889	1006	11.203111	8.797743	1011	11.202257	10.000854	12	9.999146	38	30			
35	24	8.797894	1004	11.202106	8.798752	1008	11.201248	10.000858	13	9.999142	36	24			
36	26	8.798897	1001	11.201103	8.799759	1005	11.200241	10.000862	14	9.999138	34	30			
37	28	8.799897	1000	11.200103	8.800763	1004	11.199237	10.000866	15	9.999134	32	23			
37	30	8.800896	997	11.199104	8.801765	1001	11.198235	10.000870	16	9.999130	30	30			
38	32	8.801892	995	11.198108	8.802765	998	11.197235	10.000874	17	9.999126	28	22			
38	34	8.802885	992	11.197115	8.803763	997	11.196237	10.000878	18	9.999122	26	30			
39	36	8.803876	990	11.196124	8.804758	994	11.195242	10.000882	19	9.999118	24	21			
39	38	8.804866	988	11.195134	8.805751	992	11.194249	10.000886	20	9.999114	22	30			
40	40	8.805852	986	11.194148	8.806742	990	11.193258	10.000890	21	9.999110	20	26			
40	42	8.806837	983	11.193163	8.807731	987	11.192269	10.000894	22	9.999106	18	30			
41	44	8.807819	982	11.192181	8.808717	986	11.191283	10.000898	23	9.999102	16	19			
41	46	8.808799	979	11.191201	8.809701	983	11.190299	10.000902	24	9.999098	14	30			
42	48	8.809777	976	11.190223	8.810683	981	11.189317	10.000906	25	9.999094	12	18			
42	50	8.810753	975	11.189247	8.811663	978	11.188337	10.000910	26	9.999090	10	30			
43	52	8.811726	972	11.188274	8.812641	977	11.187359	10.000914	27	9.999086	8	17			
43	54	8.812698	971	11.187302	8.813616	974	11.186384	10.000918	28	9.999082	6	30			
44	56	8.813667	968	11.186333	8.814589	972	11.185411	10.000923	29	9.999077	4	16			
44	58	8.814634	965	11.185366	8.815560	970	11.184440	10.000927	30	9.999073	2	30			
45	0	8.815599	964	11.184401	8.816529	968	11.183471	10.000931	31	9.999069	0	15			
45	2	8.816561	962	11.183439	8.817496	966	11.182504	10.000935	1	9.999065	58	30			
46	4	8.817522	959	11.182478	8.818461	963	11.181539	10.000939	2	9.999061	56	14			
46	6	8.818480	958	11.181520	8.819423	962	11.180577	10.000943	3	9.999057	54	30			
47	8	8.819436	955	11.180564	8.820384	959	11.179616	10.000947	4	9.999053	52	13			
47	10	8.820390	953	11.179610	8.821342	958	11.178658	10.000952	5	9.999048	50	30			
48	12	8.821343	951	11.178657	8.822298	955	11.177702	10.000956	6	9.999044	48	12			
48	14	8.822292	949	11.177708	8.823253	953	11.176747	10.000960	7	9.999040	46	30			
49	16	8.823240	947	11.176760	8.824205	951	11.175795	10.000964	8	9.999036	44	11			
49	18	8.824186	944	11.175814	8.825155	949	11.174845	10.000968	9	9.999032	42	30			
50	20	8.825130	943	11.174870	8.826103	947	11.173897	10.000973	10	9.999027	40	10			
50	22	8.826072	941	11.173928	8.827049	945	11.172951	10.000977	11	9.999023	38	30			
51	24	8.827011	938	11.172989	8.827992	943	11.172008	10.000981	12	9.999019	36	9			
51	26	8.827949	937	11.172051	8.828934	941	11.171066	10.000985	13	9.999015	34	30			
52	28	8.828884	934	11.171116	8.829874	938	11.170126	10.000990	14	9.999010	32	8			
52	30	8.829818	933	11.170182	8.830812	937	11.169188	10.000994	15	9.999006	30	30			
53	32	8.830749	931	11.169251	8.831748	935	11.168252	10.000998	16	9.999002	28	7			
53	34	8.831679	928	11.168321	8.832682	933	11.167318	10.001003	17	9.999000	26	30			
54	36	8.832607	927	11.167393	8.833613	931	11.166387	10.001007	18	9.999000	24	6			
54	38	8.833532	924	11.166468	8.834543	929	11.165457	10.001011	19	9.999000	22	30			
55	40	8.834456	923	11.165544	8.835471	926	11.164529	10.001016	20	9.999000	20	5			
55	42	8.835377	920	11.164623	8.836397	925	11.163603	10.001020	21	9.999000	18	30			
56	44	8.836297	919	11.163703	8.837321	923	11.162679	10.001024	22	9.999000	16	4			
56	46	8.837215	917	11.162785	8.838243	922	11.161757	10.001029	23	9.999000	14	30			
57	48	8.838130	915	11.161870	8.839163	919	11.160837	10.001033	24	9.999000	12	3			
57	50	8.839044	912	11.160956	8.840081	917	11.159919	10.001037	25	9.999000	10	30			
58	52	8.839956	911	11.160044	8.840998	915	11.159002	10.001042	26	9.999000	8	2			
58	54	8.840866	909	11.159134	8.841912	914	11.158088	10.001046	27	9.999000	6	30			
59	56	8.841774	907	11.158226	8.842825	911	11.157175	10.001050	28	9.999000	4	1			
59	58	8.842680	906	11.157320	8.843735	910	11.156265	10.001055	29	9.999000	2	30			
60	0	8.843585	903	11.156415	8.844644	907	11.155356	10.001059	30	9.999000	0	0			
°	'	m.	Cosine	D.	Secant	Cotang.	D.	Tangent	Cosec.	Parts	Sine	m.	°	'	

86°

5° 44'

LOG. SINES, COSINES, &c.

0° 16'			4°												
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'		
0	0	8.843585		11.156415	8.844644	11.155356	10.001059	9.998941	11.155356	10.001059	9.998941	0	0		
1	1	8.844487	1 30	11.155513	8.845551	11.154449	10.001064	9.998936	11.154449	10.001064	9.998936	1	1		
2	2	8.845387	2 60	11.154613	8.846455	11.153345	10.001068	9.998932	11.153345	10.001068	9.998932	2	2		
3	3	8.846286	3 30	11.153714	8.847358	11.152442	10.001073	9.998927	11.152442	10.001073	9.998927	3	3		
4	4	8.847183	4 119	11.152817	8.848260	11.151540	10.001077	9.998923	11.151540	10.001077	9.998923	4	4		
5	5	8.848078	5 149	11.151922	8.849159	11.150641	10.001081	9.998919	11.150641	10.001081	9.998919	5	5		
6	6	8.848971	6 179	11.151029	8.850057	11.149743	10.001086	9.998914	11.149743	10.001086	9.998914	6	6		
7	7	8.849862	7 208	11.150138	8.850952	11.148848	10.001090	9.998910	11.148848	10.001090	9.998910	7	7		
8	8	8.850755	8 238	11.149249	8.851846	11.147954	10.001095	9.998905	11.147954	10.001095	9.998905	8	8		
9	9	8.851639	9 268	11.148361	8.852738	11.147062	10.001099	9.998901	11.147062	10.001099	9.998901	9	9		
10	10	8.852525	10 298	11.147475	8.853628	11.146172	10.001104	9.998896	11.146172	10.001104	9.998896	10	10		
11	11	8.853408	11 29	11.146592	8.854517	11.145283	10.001108	9.998892	11.145283	10.001108	9.998892	11	11		
12	12	8.854291	12 58	11.145709	8.855403	11.144397	10.001113	9.998887	11.144397	10.001113	9.998887	12	12		
13	13	8.855171	13 88	11.144829	8.856288	11.143512	10.001117	9.998883	11.143512	10.001117	9.998883	13	13		
14	14	8.856049	14 117	11.143951	8.857171	11.142629	10.001122	9.998878	11.142629	10.001122	9.998878	14	14		
15	15	8.856926	15 146	11.143074	8.858053	11.141747	10.001127	9.998873	11.141747	10.001127	9.998873	15	15		
16	16	8.857801	16 175	11.142199	8.858932	11.140868	10.001131	9.998869	11.140868	10.001131	9.998869	16	16		
17	17	8.858674	17 204	11.141326	8.859810	11.140000	10.001136	9.998864	11.140000	10.001136	9.998864	17	17		
18	18	8.859546	18 233	11.140454	8.860686	11.139134	10.001140	9.998860	11.139134	10.001140	9.998860	18	18		
19	19	8.860415	19 263	11.139585	8.861560	11.138269	10.001145	9.998855	11.138269	10.001145	9.998855	19	19		
20	20	8.861283	20 292	11.138717	8.862433	11.137407	10.001149	9.998851	11.137407	10.001149	9.998851	20	20		
21	21	8.862149	21 29	11.137851	8.863303	11.136549	10.001154	9.998846	11.136549	10.001154	9.998846	21	21		
22	22	8.863014	22 57	11.136986	8.864173	11.135697	10.001159	9.998841	11.135697	10.001159	9.998841	22	22		
23	23	8.863877	23 86	11.136123	8.865040	11.134850	10.001163	9.998837	11.134850	10.001163	9.998837	23	23		
24	24	8.864738	24 114	11.135262	8.865906	11.134009	10.001168	9.998832	11.134009	10.001168	9.998832	24	24		
25	25	8.865597	25 143	11.134403	8.866769	11.133173	10.001173	9.998827	11.133173	10.001173	9.998827	25	25		
26	26	8.866455	26 172	11.133545	8.867632	11.132348	10.001177	9.998823	11.132348	10.001177	9.998823	26	26		
27	27	8.867310	27 200	11.132690	8.868494	11.131528	10.001182	9.998818	11.131528	10.001182	9.998818	27	27		
28	28	8.868165	28 229	11.131835	8.869351	11.130713	10.001187	9.998813	11.130713	10.001187	9.998813	28	28		
29	29	8.869017	29 257	11.130983	8.870208	11.129902	10.001191	9.998809	11.129902	10.001191	9.998809	29	29		
30	30	8.869868	30 286	11.130132	8.871064	11.129096	10.001196	9.998804	11.129096	10.001196	9.998804	30	30		
31	31	8.870717	31 28	11.129283	8.871918	11.128292	10.001201	9.998799	11.128292	10.001201	9.998799	31	31		
32	32	8.871565	32 56	11.128435	8.872770	11.127490	10.001205	9.998795	11.127490	10.001205	9.998795	32	32		
33	33	8.872410	33 84	11.127590	8.873620	11.126688	10.001210	9.998790	11.126688	10.001210	9.998790	33	33		
34	34	8.873255	34 112	11.126745	8.874469	11.125887	10.001215	9.998785	11.125887	10.001215	9.998785	34	34		
35	35	8.874097	35 140	11.125903	8.875317	11.125088	10.001219	9.998781	11.125088	10.001219	9.998781	35	35		
36	36	8.874938	36 168	11.125062	8.876162	11.124290	10.001224	9.998776	11.124290	10.001224	9.998776	36	36		
37	37	8.875777	37 196	11.124223	8.877006	11.123494	10.001229	9.998771	11.123494	10.001229	9.998771	37	37		
38	38	8.876615	38 224	11.123385	8.877849	11.122700	10.001234	9.998766	11.122700	10.001234	9.998766	38	38		
39	39	8.877451	39 252	11.122549	8.878689	11.121907	10.001238	9.998762	11.121907	10.001238	9.998762	39	39		
40	40	8.878285	40 280	11.121715	8.879529	11.121116	10.001243	9.998757	11.121116	10.001243	9.998757	40	40		
41	41	8.879118	41 27	11.120882	8.880366	11.120326	10.001248	9.998752	11.120326	10.001248	9.998752	41	41		
42	42	8.879949	42 55	11.120051	8.881202	11.119538	10.001253	9.998747	11.119538	10.001253	9.998747	42	42		
43	43	8.880779	43 82	11.119221	8.882037	11.118753	10.001258	9.998742	11.118753	10.001258	9.998742	43	43		
44	44	8.881607	44 110	11.118393	8.882869	11.117969	10.001263	9.998737	11.117969	10.001263	9.998737	44	44		
45	45	8.882433	45 137	11.117567	8.883701	11.117187	10.001267	9.998733	11.117187	10.001267	9.998733	45	45		
46	46	8.883258	46 165	11.116742	8.884530	11.116407	10.001272	9.998728	11.116407	10.001272	9.998728	46	46		
47	47	8.884081	47 192	11.115919	8.885358	11.115634	10.001277	9.998723	11.115634	10.001277	9.998723	47	47		
48	48	8.884903	48 220	11.115097	8.886185	11.114862	10.001282	9.998718	11.114862	10.001282	9.998718	48	48		
49	49	8.885723	49 247	11.114277	8.887010	11.114092	10.001287	9.998713	11.114092	10.001287	9.998713	49	49		
50	50	8.886542	50 275	11.113458	8.887833	11.113324	10.001292	9.998708	11.113324	10.001292	9.998708	50	50		
51	51	8.887359	51 27	11.112641	8.888655	11.112554	10.001296	9.998704	11.112554	10.001296	9.998704	51	51		
52	52	8.888174	52 54	11.111826	8.889476	11.111784	10.001301	9.998699	11.111784	10.001301	9.998699	52	52		
53	53	8.888988	53 81	11.111012	8.890295	11.111012	10.001306	9.998694	11.111012	10.001306	9.998694	53	53		
54	54	8.889801	54 108	11.110199	8.891112	11.110200	10.001311	9.998689	11.110200	10.001311	9.998689	54	54		
55	55	8.890612	55 135	11.109388	8.891928	11.110397	10.001316	9.998684	11.110397	10.001316	9.998684	55	55		
56	56	8.891421	56 162	11.108579	8.892742	11.110594	10.001321	9.998679	11.110594	10.001321	9.998679	56	56		
57	57	8.892229	57 189	11.107771	8.893555	11.110791	10.001326	9.998674	11.110791	10.001326	9.998674	57	57		
58	58	8.893035	58 216	11.106965	8.894366	11.110988	10.001331	9.998669	11.110988	10.001331	9.998669	58	58		
59	59	8.893840	59 243	11.106160	8.895176	11.111184	10.001336	9.998664	11.111184	10.001336	9.998664	59	59		
60	60	8.894643	60 270	11.105357	8.895984	11.111381	10.001341	9.998659	11.111381	10.001341	9.998659	60	60		
°	'	Cosine	Parts	Secant	Cotang.	Tangent	Cosec.	Parts	Sine	Parts	°	'			

5° 42'

TABLE 68

747

LOG. SINES, COSINES, &c.

0° 18'

4°

''	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	''
30	0	8° 894643		11° 105357	8° 895984		11° 104016	10° 001341		9° 998659	2	30
30	2	8° 895445	1° 26	11° 104555	8° 896791	1° 27	11° 103209	10° 001346	1° 0	9° 998654	58	30
31	4	8° 896246	3 53	11° 103754	8° 897596	2 53	11° 102404	10° 001351	2 0	9° 998649	36	29
30	6	8° 897044	3 79	11° 102956	8° 898400	3 80	11° 101600	10° 001356	3 1	9° 998644	54	30
32	8	8° 897842	4 106	11° 102158	8° 899203	4 107	11° 100797	10° 001361	4 1	9° 998639	52	28
30	10	8° 898638	5 132	11° 101362	8° 900004	5 133	11° 099996	10° 001366	5 1	9° 998634	50	30
33	12	8° 899432	6 159	11° 100568	8° 900803	6 160	11° 099197	10° 001371	6 1	9° 998629	48	27
36	14	8° 900225	7 185	11° 099775	8° 901601	7 186	11° 098399	10° 001376	7 1	9° 998624	46	30
34	16	8° 901017	8 212	11° 098983	8° 902398	8 213	11° 097602	10° 001381	8 1	9° 998619	44	26
30	18	8° 901807	9 238	11° 098193	8° 903193	9 240	11° 096807	10° 001386	9 2	9° 998614	42	30
36	20	8° 902596	10 265	11° 097404	8° 903987	10 266	11° 096013	10° 001391	10 2	9° 998609	40	25
30	22	8° 903383	1 26	11° 096617	8° 904779	1 26	11° 095221	10° 001396	11 2	9° 998604	38	30
36	24	8° 904169	2 52	11° 095831	8° 905570	2 52	11° 094430	10° 001401	12 2	9° 998599	36	24
30	26	8° 904953	3 78	11° 095047	8° 906359	3 79	11° 093641	10° 001406	13 2	9° 998594	34	30
37	28	8° 905736	4 104	11° 094264	8° 907147	4 105	11° 092853	10° 001411	14 2	9° 998589	32	23
30	30	8° 906517	5 130	11° 093483	8° 907934	5 131	11° 092066	10° 001416	15 3	9° 998584	30	30
38	32	8° 907297	6 156	11° 092703	8° 908719	6 157	11° 091281	10° 001422	16 3	9° 998578	28	22
30	34	8° 908076	7 182	11° 091924	8° 909503	7 183	11° 090497	10° 001427	17 3	9° 998573	26	30
39	36	8° 908853	8 208	11° 091147	8° 910285	8 209	11° 089715	10° 001432	18 3	9° 998568	24	21
30	38	8° 909629	9 234	11° 090371	8° 911066	9 236	11° 088934	10° 001437	19 3	9° 998563	22	30
40	40	8° 910404	10 260	11° 089596	8° 911846	10 262	11° 088154	10° 001442	20 3	9° 998558	20	20
30	42	8° 911177	1 26	11° 088823	8° 912624	1 26	11° 087376	10° 001447	21 4	9° 998553	18	30
41	44	8° 911949	2 51	11° 088051	8° 913401	2 51	11° 086599	10° 001452	22 4	9° 998548	16	19
30	46	8° 912719	3 77	11° 087281	8° 914177	3 77	11° 085823	10° 001458	23 4	9° 998542	14	30
42	48	8° 913488	4 102	11° 086512	8° 914955	4 103	11° 085049	10° 001463	24 4	9° 998537	12	18
30	50	8° 914256	5 128	11° 085744	8° 915724	5 129	11° 084276	10° 001468	25 4	9° 998532	10	30
43	52	8° 915022	6 153	11° 084978	8° 916495	6 154	11° 083505	10° 001473	26 4	9° 998527	8	17
30	54	8° 915787	7 179	11° 084213	8° 917265	7 180	11° 082735	10° 001478	27 5	9° 998522	6	30
44	56	8° 916550	8 204	11° 083450	8° 918034	8 206	11° 081966	10° 001484	28 5	9° 998516	4	16
30	58	8° 917313	9 230	11° 082687	8° 918801	9 231	11° 081199	10° 001489	29 5	9° 998511	2	30
45	60	8° 918073	10 255	11° 081927	8° 919568	10 257	11° 080432	10° 001494	30 5	9° 998506	0	15
30	2	8° 918833	1 25	11° 081167	8° 920332	1 25	11° 079668	10° 001499	1 0	9° 998501	38	30
46	4	8° 919591	2 50	11° 080409	8° 921096	2 51	11° 078904	10° 001505	2 0	9° 998495	36	14
30	6	8° 920348	3 75	11° 079652	8° 921858	3 76	11° 078142	10° 001510	3 1	9° 998490	34	30
47	8	8° 921103	4 100	11° 078897	8° 922619	4 101	11° 077381	10° 001515	4 1	9° 998485	32	13
30	10	8° 921858	5 125	11° 078142	8° 923378	5 126	11° 076622	10° 001521	5 1	9° 998479	30	30
48	12	8° 922610	6 150	11° 077390	8° 924136	6 152	11° 075864	10° 001526	6 1	9° 998474	28	12
30	14	8° 923362	7 175	11° 076638	8° 924893	7 177	11° 075107	10° 001531	7 1	9° 998469	26	30
49	16	8° 924112	8 201	11° 075888	8° 925649	8 202	11° 074351	10° 001536	8 1	9° 998464	24	11
30	18	8° 924861	9 226	11° 075139	8° 926403	9 227	11° 073597	10° 001542	9 2	9° 998458	22	30
50	20	8° 925609	10 251	11° 074391	8° 927156	10 253	11° 072844	10° 001547	10 2	9° 998453	20	10
30	22	8° 926355	1 25	11° 073645	8° 927908	1 25	11° 072092	10° 001552	11 2	9° 998448	18	30
51	24	8° 927100	2 49	11° 072890	8° 928658	2 50	11° 071342	10° 001558	12 2	9° 998442	16	9
30	26	8° 927844	3 74	11° 072156	8° 929407	3 74	11° 070593	10° 001563	13 2	9° 998437	14	30
52	28	8° 928587	4 99	11° 071413	8° 930155	4 99	11° 069845	10° 001569	14 3	9° 998431	12	8
30	30	8° 929328	5 123	11° 070672	8° 930902	5 124	11° 069098	10° 001574	15 3	9° 998426	10	30
53	32	8° 930068	6 148	11° 069932	8° 931647	6 149	11° 068353	10° 001579	16 3	9° 998421	8	7
30	34	8° 930806	7 173	11° 069194	8° 932391	7 174	11° 067609	10° 001585	17 3	9° 998415	6	30
54	36	8° 931544	8 197	11° 068456	8° 933134	8 199	11° 066866	10° 001590	18 3	9° 998410	4	6
30	38	8° 932280	9 222	11° 067720	8° 933876	9 223	11° 066124	10° 001596	19 3	9° 998404	2	30
55	40	8° 933015	10 247	11° 066985	8° 934616	10 248	11° 065384	10° 001601	20 4	9° 998399	0	5
30	42	8° 933749	1 24	11° 066251	8° 935355	1 24	11° 064645	10° 001606	21 4	9° 998394	18	30
56	44	8° 934481	2 48	11° 065519	8° 936093	2 49	11° 063907	10° 001612	22 4	9° 998388	16	4
30	46	8° 935212	3 73	11° 064788	8° 936830	3 73	11° 063170	10° 001617	23 4	9° 998383	14	30
57	48	8° 935942	4 97	11° 064058	8° 937565	4 98	11° 062435	10° 001623	24 4	9° 998377	12	3
30	50	8° 936671	5 121	11° 063329	8° 938299	5 122	11° 061701	10° 001628	25 4	9° 998372	10	30
58	52	8° 937398	6 145	11° 062602	8° 939032	6 147	11° 060968	10° 001634	26 5	9° 998366	8	2
30	54	8° 938125	7 170	11° 061875	8° 939764	7 171	11° 060236	10° 001639	27 5	9° 998361	6	30
59	56	8° 938850	8 194	11° 061150	8° 940494	8 195	11° 059506	10° 001645	28 5	9° 998355	4	1
30	58	8° 939573	9 218	11° 060427	8° 941224	9 220	11° 058776	10° 001650	29 5	9° 998350	2	30
60	60	8° 940296	10 242	11° 059704	8° 941952	10 244	11° 058048	10° 001656	30 5	9° 998344	0	0
''	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	''

M.5°

5° 40'

LOG. SINES, COSINES, &c.

0° 20"				5°															
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.
0	0	8°940296		11°059704	8°941952		11°058048	10°001656		9°998344		0	0	8°940296		11°059704	8°941952		11°058048
30	2	8°941017	1" 24	11°058983	8°942679	1" 24	11°057321	10°001660	1" 0	9°998339	50	30	2	8°941017	1" 24	11°058983	8°942679	1" 24	11°057321
1	4	8°941738	2 48	11°058262	8°943404	2 48	11°056596	10°001667	2 0	9°998333	56	30	4	8°941738	2 48	11°058262	8°943404	2 48	11°056596
30	6	8°942457	3 71	11°057543	8°944129	3 71	11°055871	10°001672	3 1	9°998328	61	30	6	8°942457	3 71	11°057543	8°944129	3 71	11°055871
2	8	8°943174	4 95	11°056826	8°944852	4 96	11°055148	10°001678	4 1	9°998322	67	30	8	8°943174	4 95	11°056826	8°944852	4 96	11°055148
30	10	8°943891	5 119	11°056109	8°945574	5 120	11°054426	10°001684	5 1	9°998316	73	30	10	8°943891	5 119	11°056109	8°945574	5 120	11°054426
3	12	8°944606	6 143	11°055394	8°946295	6 144	11°053705	10°001689	6 1	9°998311	79	30	12	8°944606	6 143	11°055394	8°946295	6 144	11°053705
30	14	8°945321	7 167	11°054679	8°947015	7 168	11°052985	10°001695	7 1	9°998305	85	30	14	8°945321	7 167	11°054679	8°947015	7 168	11°052985
4	16	8°946034	8 191	11°053966	8°947734	8 192	11°052266	10°001700	8 2	9°998300	91	30	16	8°946034	8 191	11°053966	8°947734	8 192	11°052266
30	18	8°946745	9 214	11°053255	8°948451	9 216	11°051549	10°001706	9 2	9°998294	97	30	18	8°946745	9 214	11°053255	8°948451	9 216	11°051549
5	20	8°947456	10 238	11°052544	8°949168	10 240	11°050832	10°001711	10 2	9°998289	103	30	20	8°947456	10 238	11°052544	8°949168	10 240	11°050832
30	22	8°948166	11 263	11°051834	8°949883	11 264	11°050117	10°001717	11 2	9°998283	109	30	22	8°948166	11 263	11°051834	8°949883	11 264	11°050117
30	24	8°948874	12 287	11°051126	8°950597	12 288	11°049403	10°001723	12 2	9°998277	115	30	24	8°948874	12 287	11°051126	8°950597	12 288	11°049403
30	26	8°949581	13 311	11°050419	8°951309	13 312	11°048691	10°001728	13 2	9°998272	121	30	26	8°949581	13 311	11°050419	8°951309	13 312	11°048691
7	28	8°950287	14 335	11°049713	8°952021	14 336	11°047979	10°001734	14 2	9°998266	127	30	28	8°950287	14 335	11°049713	8°952021	14 336	11°047979
30	30	8°950992	15 359	11°049008	8°952732	15 360	11°047268	10°001740	15 2	9°998260	133	30	30	8°950992	15 359	11°049008	8°952732	15 360	11°047268
8	32	8°951696	16 383	11°048304	8°953441	16 384	11°046559	10°001745	16 2	9°998255	139	30	32	8°951696	16 383	11°048304	8°953441	16 384	11°046559
30	34	8°952398	17 407	11°047602	8°954149	17 408	11°045851	10°001751	17 2	9°998249	145	30	34	8°952398	17 407	11°047602	8°954149	17 408	11°045851
9	36	8°953100	18 431	11°046900	8°954856	18 432	11°045144	10°001757	18 2	9°998243	151	30	36	8°953100	18 431	11°046900	8°954856	18 432	11°045144
30	38	8°953800	19 455	11°046200	8°955562	19 456	11°044438	10°001762	19 2	9°998238	157	30	38	8°953800	19 455	11°046200	8°955562	19 456	11°044438
10	40	8°954499	20 479	11°045501	8°956267	20 480	11°043733	10°001768	20 2	9°998232	163	30	40	8°954499	20 479	11°045501	8°956267	20 480	11°043733
30	42	8°955197	21 503	11°044803	8°956971	21 504	11°043029	10°001774	21 2	9°998226	169	30	42	8°955197	21 503	11°044803	8°956971	21 504	11°043029
11	44	8°955894	22 527	11°044106	8°957674	22 528	11°042326	10°001780	22 2	9°998220	175	30	44	8°955894	22 527	11°044106	8°957674	22 528	11°042326
30	46	8°956590	23 551	11°043410	8°958375	23 552	11°041625	10°001785	23 2	9°998215	181	30	46	8°956590	23 551	11°043410	8°958375	23 552	11°041625
12	48	8°957284	24 575	11°042716	8°959075	24 576	11°040925	10°001791	24 2	9°998209	187	30	48	8°957284	24 575	11°042716	8°959075	24 576	11°040925
30	50	8°957978	25 600	11°042022	8°959775	25 601	11°040225	10°001797	25 2	9°998203	193	30	50	8°957978	25 600	11°042022	8°959775	25 601	11°040225
13	52	8°958670	26 624	11°041330	8°960473	26 625	11°039527	10°001803	26 2	9°998197	199	30	52	8°958670	26 624	11°041330	8°960473	26 625	11°039527
30	54	8°959362	27 648	11°040638	8°961170	27 649	11°038830	10°001808	27 2	9°998192	205	30	54	8°959362	27 648	11°040638	8°961170	27 649	11°038830
14	56	8°960052	28 672	11°039948	8°961866	28 673	11°038134	10°001814	28 2	9°998186	211	30	56	8°960052	28 672	11°039948	8°961866	28 673	11°038134
30	58	8°960741	29 696	11°039259	8°962561	29 697	11°037439	10°001820	29 2	9°998180	217	30	58	8°960741	29 696	11°039259	8°962561	29 697	11°037439
15	60	8°961429	30 720	11°038571	8°963255	30 721	11°036745	10°001826	30 2	9°998174	223	30	60	8°961429	30 720	11°038571	8°963255	30 721	11°036745
30	62	8°962116	31 744	11°037884	8°963947	31 745	11°036053	10°001832	31 2	9°998168	229	30	62	8°962116	31 744	11°037884	8°963947	31 745	11°036053
16	64	8°962801	32 768	11°037199	8°964639	32 769	11°035361	10°001837	32 2	9°998163	235	30	64	8°962801	32 768	11°037199	8°964639	32 769	11°035361
30	66	8°963486	33 792	11°036514	8°965329	33 793	11°034671	10°001843	33 2	9°998157	241	30	66	8°963486	33 792	11°036514	8°965329	33 793	11°034671
17	68	8°964170	34 816	11°035830	8°966019	34 817	11°033981	10°001849	34 2	9°998151	247	30	68	8°964170	34 816	11°035830	8°966019	34 817	11°033981
30	70	8°964852	35 840	11°035148	8°966707	35 841	11°033293	10°001855	35 2	9°998145	253	30	70	8°964852	35 840	11°035148	8°966707	35 841	11°033293
18	72	8°965534	36 864	11°034466	8°967394	36 865	11°032606	10°001861	36 2	9°998139	259	30	72	8°965534	36 864	11°034466	8°967394	36 865	11°032606
30	74	8°966214	37 888	11°033786	8°968081	37 889	11°031919	10°001867	37 2	9°998133	265	30	74	8°966214	37 888	11°033786	8°968081	37 889	11°031919
19	76	8°966893	38 912	11°033107	8°968766	38 913	11°031234	10°001872	38 2	9°998128	271	30	76	8°966893	38 912	11°033107	8°968766	38 913	11°031234
30	78	8°967572	39 936	11°032428	8°969450	39 937	11°030550	10°001878	39 2	9°998122	277	30	78	8°967572	39 936	11°032428	8°969450	39 937	11°030550
20	80	8°968249	40 960	11°031751	8°970133	40 961	11°029867	10°001884	40 2	9°998116	283	30	80	8°968249	40 960	11°031751	8°970133	40 961	11°029867
30	82	8°968925	41 984	11°031075	8°970815	41 985	11°029185	10°001890	41 2	9°998110	289	30	82	8°968925	41 984	11°031075	8°970815	41 985	11°029185
21	84	8°969600	42 1008	11°030400	8°971496	42 1009	11°028504	10°001896	42 2	9°998104	295	30	84	8°969600	42 1008	11°030400	8°971496	42 1009	11°028504
30	86	8°970274	43 1032	11°029726	8°972176	43 1033	11°027824	10°001902	43 2	9°998098	301	30	86	8°970274	43 1032	11°029726	8°972176	43 1033	11°027824
22	88	8°970947	44 1056	11°029053	8°972855	44 1057	11°027145	10°001908	44 2	9°998092	307	30	88	8°970947	44 1056	11°029053	8°972855	44 1057	11°027145
30	90	8°971619	45 1080	11°028381	8°973532	45 1081	11°026468	10°001914	45 2	9°998086	313	30	90	8°971619	45 1080	11°028381	8°973532	45 1081	11°026468
23	92	8°972289	46 1104	11°027711	8°974209	46 1105	11°025791	10°001920	46 2	9°998080	319	30	92	8°972289	46 1104	11°027711	8°974209	46 1105	11°025791
30	94	8°972959	47 1128	11°027041	8°974885	47 1129	11°025115	10°001926	47 2	9°998074	325	30	94	8°972959	47 1128	11°027041	8°974885	47 1129	11°025115
24	96	8°973628	48 1152	11°026372	8°975560	48 1153	11°024440	10°											

TABLE 68

749

LOG. SINES, COSINES, &c.

0° 22'				5°																	
°	'	m.	Parts	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	'							
30	0	8	981573			11	018427	8	983577	1	22	11	016423	10	002004	1	0	9	997996	38	30
30	2	8	982228	1	22	11	017772	8	984238	1	22	11	015762	10	002010	1	0	9	997996	38	30
31	4	8	982883	2	43	11	017117	8	984899	2	44	11	015101	10	002016	2	0	9	997984	50	29
31	6	8	983536	3	65	11	016464	8	985559	3	66	11	014441	10	002022	3	1	9	997978	51	30
32	8	8	984189	4	87	11	015811	8	986217	4	88	11	013783	10	002028	4	1	9	997972	52	28
32	10	8	984840	5	109	11	015160	8	986875	5	110	11	013125	10	002035	5	1	9	997965	53	30
33	12	8	985491	6	130	11	014509	8	987532	6	131	11	012468	10	002041	6	1	9	997959	48	27
33	14	8	986141	7	152	11	013859	8	988187	7	153	11	011813	10	002047	7	1	9	997953	46	30
34	16	8	986789	8	174	11	013211	8	988842	8	175	11	011158	10	002053	8	2	9	997947	41	26
34	18	8	987437	9	195	11	012563	8	989496	9	197	11	010504	10	002059	9	2	9	997941	42	30
35	20	8	988083	10	217	11	011917	8	990149	10	219	11	009851	10	002065	10	2	9	997935	40	25
35	22	8	988729	1	21	11	011271	8	990801	1	22	11	009199	10	002071	11	2	9	997929	38	30
36	24	8	989374	2	43	11	010626	8	991451	2	43	11	008549	10	002078	12	2	9	997922	35	24
36	26	8	990017	3	64	11	009983	8	992101	3	65	11	007899	10	002084	13	3	9	997916	34	30
37	28	8	990660	4	85	11	009340	8	992750	4	86	11	007250	10	002090	14	3	9	997910	32	23
37	30	8	991302	5	107	11	008698	8	993398	5	108	11	006602	10	002096	15	3	9	997904	30	30
38	32	8	991943	6	128	11	008057	8	994045	6	129	11	005955	10	002103	16	3	9	997897	28	22
38	34	8	992583	7	150	11	007417	8	994692	7	151	11	005308	10	002109	17	4	9	997891	26	30
39	36	8	993222	8	171	11	006778	8	995337	8	173	11	004663	10	002115	18	4	9	997885	24	21
39	38	8	993860	9	192	11	006140	8	995981	9	194	11	004019	10	002121	19	4	9	997879	22	30
40	40	8	994497	10	214	11	005503	8	996624	10	216	11	003376	10	002128	20	4	9	997872	20	20
40	42	8	995133	1	21	11	004867	8	997267	1	21	11	002733	10	002134	21	4	9	997866	18	30
41	44	8	995768	2	42	11	004232	8	997908	2	43	11	002092	10	002140	22	5	9	997860	16	19
41	46	8	996402	3	63	11	003598	8	998549	3	64	11	001451	10	002146	23	5	9	997854	14	30
42	48	8	997036	4	84	11	002964	8	999188	4	85	11	000812	10	002153	24	5	9	997847	12	18
42	50	8	997668	5	105	11	002332	8	999827	5	106	11	000173	10	002159	25	5	9	997841	10	30
43	52	8	998309	6	126	11	001701	9	000465	6	128	10	999535	10	002165	26	5	9	997835	8	17
43	54	8	998930	7	147	11	001070	9	001102	7	149	10	998898	10	002172	27	6	9	997828	6	30
44	56	8	999560	8	168	11	000440	9	001738	8	170	10	998262	10	002178	28	6	9	997822	4	16
44	58	8	999188	9	189	10	999812	9	002373	9	191	10	997627	10	002184	29	6	9	997816	2	30
45	20	8	999816	10	210	10	999184	9	003007	10	213	10	996993	10	002191	30	6	9	997810	0	37
45	22	8	999443	1	21	10	998557	9	003640	1	21	10	996360	10	002197	1	6	9	997803	58	30
46	24	8	999069	2	41	10	997931	9	004272	2	42	10	995728	10	002203	2	6	9	997797	56	14
46	26	8	998694	3	62	10	997306	9	004904	3	63	10	995096	10	002210	3	1	9	997790	54	30
47	28	8	998318	4	83	10	996682	9	005534	4	84	10	994466	10	002216	4	1	9	997784	52	13
47	30	8	997941	5	104	10	996059	9	006164	5	105	10	993836	10	002223	5	1	9	997777	50	30
48	32	8	997563	6	124	10	995437	9	006792	6	126	10	993208	10	002229	6	1	9	997771	48	2
48	34	8	997185	7	145	10	994815	9	007420	7	147	10	992580	10	002235	7	1	9	997765	46	30
49	36	8	996805	8	166	10	994195	9	008047	8	167	10	991953	10	002242	8	2	9	997758	44	11
49	38	8	996425	9	187	10	993575	9	008673	9	188	10	991327	10	002248	9	2	9	997752	42	30
50	40	8	996044	10	207	10	992956	9	009298	10	209	10	990702	10	002255	10	2	9	997745	40	10
50	42	8	995661	1	20	10	992339	9	009923	1	21	10	990077	10	002261	11	2	9	997739	38	30
51	24	8	995278	2	41	10	991722	9	010546	2	41	10	989454	10	002268	12	3	9	997732	36	9
51	26	8	994894	3	61	10	991106	9	011169	3	62	10	988831	10	002274	13	3	9	997726	34	30
52	28	8	994510	4	82	10	990490	9	011790	4	83	10	988510	10	002281	14	3	9	997719	32	8
52	30	8	994124	5	102	10	989876	9	012411	5	103	10	988189	10	002287	15	3	9	997713	30	30
53	32	8	993737	6	123	10	989263	9	013031	6	124	10	987569	10	002294	16	3	9	997706	28	7
53	34	8	993350	7	143	10	988650	9	013650	7	145	10	986950	10	002300	17	4	9	997700	26	30
54	36	8	992962	8	165	10	988038	9	014268	8	166	10	986252	10	002307	18	4	9	997693	24	6
54	38	8	992572	9	184	10	987428	9	014886	9	186	10	985514	10	002313	19	4	9	997687	22	30
55	40	8	992182	10	204	10	986818	9	015502	10	207	10	984798	10	002320	20	4	9	997680	20	5
55	42	8	991791	1	20	10	986209	9	016118	1	20	10	984182	10	002326	21	4	9	997674	18	30
56	44	8	991400	2	40	10	985600	9	016732	2	41	10	983568	10	002333	22	5	9	997667	16	4
56	46	8	991007	3	61	10	984993	9	017346	3	61	10	982654	10	002339	23	5	9	997661	14	30
57	48	8	990613	4	81	10	984383	9	017959	4	81	10	982041	10	002346	24	5	9	997654	12	3
57	50	8	990219	5	101	10	983771	9	018572	5	102	10	981517	10	002353	25	5	9	997647	10	30
58	52	8	989824	6	121	10	983156	9	019183	6	122	10	980817	10	002359	26	5	9	997641	8	2
58	54	8	989428	7	141	10	982572	9	019794	7	143	10	980206	10	002366	27	6	9	997634	6	30
59	56	8	989031	8	161	10	981969	9	020403	8	163	10	979797	10	002372	28	6	9	997628	4	1
59	58	8	988633	9	182	10	981367	9	021012	9	183	10	979288	10	002379	29	6	9	997621	2	30
60	20	8	988235	10	202	10	980765	9	021620	10	204	10	978780	10	002386	30	6	9	997614	0	0
°	'	m.	Cosine	Parts	Secant	Cotang.	Tangent	Parts	Tangent	Cosec.	Parts	Sine	m.	'							

84°

5° 36'

LOG. SINES, COSINES, &c.

0° 24'				6°									
°	'	Sec.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Sec.	'
0	0	9°019235	1"	20	10°980765	9°021620	10	9°978380	10°002386	10	9°997614	86	00
30	2	9°019835	1"	20	10°980165	9°022227	11	9°977773	10°002392	11	9°997608	85	30
1	4	9°020435	2	40	10°979565	9°022834	12	9°977166	10°002399	12	9°997601	84	50
2	6	9°021034	3	60	10°978966	9°023439	13	9°976561	10°002406	13	9°997594	83	30
3	8	9°021632	4	79	10°978368	9°024044	14	9°975956	10°002412	14	9°997588	82	58
4	10	9°022229	6	99	10°977771	9°024648	15	9°975352	10°002419	15	9°997581	81	30
5	12	9°022825	6	119	10°977175	9°025251	16	9°974749	10°002426	16	9°997574	80	57
6	14	9°023421	7	139	10°976579	9°025853	17	9°974147	10°002432	17	9°997568	79	30
7	16	9°024016	8	159	10°975984	9°026455	18	9°973545	10°002439	18	9°997561	78	55
8	18	9°024610	9	179	10°975390	9°027055	19	9°972945	10°002446	19	9°997554	77	30
9	20	9°025203	10	199	10°974797	9°027655	20	9°972345	10°002453	20	9°997547	76	55
10	22	9°025795	1	20	10°974205	9°028254	1	9°971746	10°002459	11	9°997541	75	30
11	24	9°026386	2	39	10°973614	9°028852	2	9°971148	10°002466	12	9°997534	74	54
12	26	9°026977	3	59	10°973023	9°029450	3	9°970550	10°002473	13	9°997527	73	30
13	28	9°027567	4	78	10°972433	9°030046	4	9°969954	10°002480	14	9°997520	72	53
14	30	9°028156	5	98	10°971844	9°030643	5	9°969358	10°002486	15	9°997514	71	30
15	32	9°028744	6	118	10°971256	9°031237	6	9°968763	10°002493	16	9°997507	70	52
16	34	9°029332	7	137	10°970668	9°031831	7	9°968169	10°002500	17	9°997500	69	30
17	36	9°029918	8	157	10°970082	9°032425	8	9°967575	10°002507	18	9°997493	68	51
18	38	9°030504	9	176	10°969496	9°033017	9	9°966983	10°002513	19	9°997487	67	30
19	40	9°031089	10	196	10°968911	9°033609	10	9°966391	10°002520	20	9°997480	66	50
20	42	9°031673	1	19	10°968327	9°034200	1	9°965800	10°002527	21	9°997473	65	30
21	44	9°032257	2	39	10°967743	9°034791	2	9°965209	10°002534	22	9°997466	64	49
22	46	9°032839	3	58	10°967161	9°035380	3	9°964620	10°002541	23	9°997459	63	30
23	48	9°033421	4	77	10°966579	9°035969	4	9°964031	10°002548	24	9°997452	62	48
24	50	9°034002	5	97	10°965998	9°036557	5	9°963443	10°002555	25	9°997445	61	30
25	52	9°034582	6	116	10°965418	9°037144	6	9°962856	10°002561	26	9°997439	60	47
26	54	9°035162	7	135	10°964838	9°037730	7	9°962270	10°002568	27	9°997432	59	30
27	56	9°035741	8	155	10°964259	9°038316	8	9°961684	10°002575	28	9°997425	58	46
28	58	9°036319	9	174	10°963681	9°038901	9	9°961099	10°002582	29	9°997418	57	30
29	60	9°036896	10	193	10°963104	9°039485	10	9°960515	10°002589	30	9°997411	56	45
30	2	9°037472	1	19	10°962528	9°040068	1	9°959932	10°002596	1	9°997404	55	30
31	4	9°038048	2	38	10°961952	9°040651	2	9°959349	10°002603	2	9°997397	54	44
32	6	9°038623	3	57	10°961377	9°041232	3	9°958768	10°002610	3	9°997390	53	30
33	8	9°039197	4	76	10°960803	9°041813	4	9°958187	10°002617	4	9°997383	52	43
34	10	9°039770	5	95	10°960230	9°042394	5	9°957606	10°002624	5	9°997376	51	30
35	12	9°040342	6	114	10°959658	9°042973	6	9°957027	10°002631	6	9°997369	50	42
36	14	9°040914	7	133	10°959086	9°043552	7	9°956448	10°002638	7	9°997362	49	30
37	16	9°041485	8	153	10°958515	9°044130	8	9°955870	10°002645	8	9°997355	48	41
38	18	9°042055	9	172	10°957945	9°044707	9	9°955293	10°002652	9	9°997348	47	30
39	20	9°042625	10	191	10°957375	9°045284	10	9°954716	10°002659	10	9°997341	46	40
40	22	9°043194	1	19	10°956806	9°045859	1	9°954141	10°002666	11	9°997334	45	30
41	24	9°043762	2	38	10°956238	9°046434	2	9°953566	10°002673	12	9°997327	44	39
42	26	9°044329	3	56	10°955671	9°047009	3	9°952991	10°002680	13	9°997320	43	30
43	28	9°044895	4	75	10°955105	9°047582	4	9°952418	10°002687	14	9°997313	42	38
44	30	9°045461	5	94	10°954539	9°048155	5	9°951845	10°002694	15	9°997306	41	30
45	32	9°046026	6	113	10°953974	9°048727	6	9°951273	10°002701	16	9°997299	40	37
46	34	9°046590	7	132	10°953410	9°049298	7	9°950702	10°002708	17	9°997292	39	30
47	36	9°047154	8	151	10°952846	9°049869	8	9°950131	10°002715	18	9°997285	38	36
48	38	9°047717	9	169	10°952283	9°050439	9	9°949561	10°002722	19	9°997278	37	30
49	40	9°048279	10	188	10°951721	9°051008	10	9°948992	10°002729	20	9°997271	36	35
50	42	9°048840	1	19	10°951160	9°051576	1	9°948424	10°002736	21	9°997264	35	30
51	44	9°049400	2	37	10°950600	9°052144	2	9°947856	10°002743	22	9°997257	34	34
52	46	9°049960	3	56	10°950040	9°052711	3	9°947289	10°002751	23	9°997249	33	30
53	48	9°050519	4	74	10°949481	9°053277	4	9°946723	10°002758	24	9°997242	32	33
54	50	9°051078	5	93	10°948922	9°053843	5	9°946157	10°002765	25	9°997235	31	30
55	52	9°051635	6	111	10°948365	9°054407	6	9°945593	10°002772	26	9°997228	30	32
56	54	9°052192	7	130	10°947808	9°054972	7	9°945028	10°002779	27	9°997221	29	30
57	56	9°052749	8	149	10°947251	9°055535	8	9°944465	10°002786	28	9°997214	28	31
58	58	9°053304	9	167	10°946696	9°056098	9	9°943902	10°002794	29	9°997207	27	30
59	60	9°053859	10	186	10°946141	9°056659	10	9°943341	10°002801	30	9°997199	26	30
°	'	Sec.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	Sec.	'

85°

5° 34'

TABLE 68

751

LOG. SINES, COSINES, &c.

0° 26'										6°									
' "	m.	Sine	Parts	Coser.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	' "	m.	' "	Sine	Parts	Coser.	Tangent	Parts
30	0	9°053859		10°946111	9°056659		10°943341	10°002801		9°597199	30	30	30	30	9°597199	30	30	30	30
31	1	9°054413	1" 18	10°945587	9°057221	1" 19	10°942779	10°002802	1" 0	9°597192	30	30	30	30	9°597185	30	30	30	30
32	2	9°054966	2 37	10°945034	9°057781	2 37	10°942219	10°002815	2 0	9°597185	30	30	30	30	9°597178	30	30	30	30
33	3	9°055519	3 55	10°944481	9°058341	3 56	10°941659	10°002822	3 1	9°597178	30	30	30	30	9°597170	30	30	30	30
34	4	9°056071	4 73	10°943929	9°058900	4 74	10°941100	10°002830	4 1	9°597170	30	30	30	30	9°597163	30	30	30	30
35	5	9°056622	5 92	10°943378	9°059459	5 93	10°940541	10°002837	5 1	9°597163	30	30	30	30	9°597156	30	30	30	30
36	6	9°057172	6 110	10°942828	9°060016	6 111	10°939934	10°002844	6 1	9°597156	30	30	30	30	9°597149	30	30	30	30
37	7	9°057722	7 128	10°942278	9°060573	7 130	10°939427	10°002851	7 2	9°597149	30	30	30	30	9°597141	30	30	30	30
38	8	9°058271	8 147	10°941729	9°061130	8 149	10°938870	10°002859	8 2	9°597141	30	30	30	30	9°597134	30	30	30	30
39	9	9°058820	9 165	10°941180	9°061685	9 167	10°938315	10°002866	9 2	9°597134	30	30	30	30	9°597127	30	30	30	30
40	10	9°059367	10 183	10°940633	9°062240	10 186	10°937760	10°002873	10 2	9°597127	30	30	30	30	9°597120	30	30	30	30
41	11	9°059914	11 18	10°940086	9°062795	11 18	10°937205	10°002880	11 3	9°597120	30	30	30	30	9°597112	30	30	30	30
42	12	9°060460	12 36	10°939540	9°063348	12 37	10°936652	10°002888	12 3	9°597112	30	30	30	30	9°597105	30	30	30	30
43	13	9°061006	13 54	10°938994	9°063901	13 55	10°936099	10°002895	13 3	9°597105	30	30	30	30	9°597098	30	30	30	30
44	14	9°061551	14 73	10°938449	9°064453	14 73	10°935547	10°002902	14 4	9°597098	30	30	30	30	9°597090	30	30	30	30
45	15	9°062095	15 91	10°937905	9°065005	15 92	10°934995	10°002910	15 4	9°597090	30	30	30	30	9°597083	30	30	30	30
46	16	9°062639	16 109	10°937361	9°065556	16 110	10°934444	10°002917	16 4	9°597083	30	30	30	30	9°597076	30	30	30	30
47	17	9°063181	17 127	10°936819	9°066106	17 129	10°933894	10°002924	17 4	9°597076	30	30	30	30	9°597068	30	30	30	30
48	18	9°063724	18 145	10°936276	9°066655	18 147	10°933345	10°002932	18 4	9°597068	30	30	30	30	9°597061	30	30	30	30
49	19	9°064265	19 163	10°935735	9°067204	19 165	10°932796	10°002939	19 4	9°597061	30	30	30	30	9°597053	30	30	30	30
50	20	9°064806	20 181	10°935194	9°067752	20 184	10°932248	10°002947	20 5	9°597053	30	30	30	30	9°597046	30	30	30	30
51	21	9°065346	21 18	10°934654	9°068300	21 18	10°931700	10°002954	21 5	9°597046	30	30	30	30	9°597039	30	30	30	30
52	22	9°065885	22 36	10°934115	9°068846	22 36	10°931154	10°002961	22 5	9°597039	30	30	30	30	9°597031	30	30	30	30
53	23	9°066424	23 54	10°933576	9°069393	23 54	10°930607	10°002969	23 6	9°597031	30	30	30	30	9°597024	30	30	30	30
54	24	9°066962	24 72	10°933038	9°069938	24 73	10°930062	10°002976	24 6	9°597024	30	30	30	30	9°597016	30	30	30	30
55	25	9°067499	25 90	10°932501	9°070483	25 91	10°929517	10°002984	25 6	9°597016	30	30	30	30	9°597009	30	30	30	30
56	26	9°068036	26 107	10°931964	9°071027	26 109	10°928973	10°002991	26 7	9°597009	30	30	30	30	9°597002	30	30	30	30
57	27	9°068572	27 125	10°931428	9°071570	27 127	10°928430	10°002998	27 7	9°597002	30	30	30	30	9°596994	30	30	30	30
58	28	9°069107	28 143	10°930893	9°072113	28 145	10°927887	10°003006	28 7	9°596994	30	30	30	30	9°596987	30	30	30	30
59	29	9°069642	29 161	10°930358	9°072655	29 163	10°927345	10°003013	29 7	9°596987	30	30	30	30	9°596979	30	30	30	30
60	30	9°070176	30 179	10°929824	9°073197	30 181	10°926803	10°003021	30 7	9°596979	30	30	30	30	9°596972	30	30	30	30
61	1	9°070709	1 18	10°929291	9°073738	1 18	10°926262	10°003028	1 0	9°596972	30	30	30	30	9°596964	30	30	30	30
62	2	9°071242	2 35	10°928758	9°074278	2 36	10°925722	10°003036	2 1	9°596964	30	30	30	30	9°596957	30	30	30	30
63	3	9°071774	3 53	10°928226	9°074817	3 54	10°925183	10°003043	3 1	9°596957	30	30	30	30	9°596949	30	30	30	30
64	4	9°072306	4 71	10°927694	9°075356	4 72	10°924644	10°003051	4 1	9°596949	30	30	30	30	9°596942	30	30	30	30
65	5	9°072836	5 88	10°927164	9°075895	5 90	10°924105	10°003058	5 1	9°596942	30	30	30	30	9°596934	30	30	30	30
66	6	9°073366	6 106	10°926634	9°076432	6 107	10°923568	10°003066	6 2	9°596934	30	30	30	30	9°596927	30	30	30	30
67	7	9°073896	7 124	10°926104	9°076969	7 125	10°923031	10°003073	7 2	9°596927	30	30	30	30	9°596919	30	30	30	30
68	8	9°074424	8 141	10°925576	9°077505	8 143	10°922495	10°003081	8 2	9°596919	30	30	30	30	9°596911	30	30	30	30
69	9	9°074952	9 159	10°925047	9°078041	9 161	10°921959	10°003089	9 2	9°596911	30	30	30	30	9°596904	30	30	30	30
70	10	9°075480	10 177	10°924520	9°078576	10 179	10°921424	10°003096	10 3	9°596904	30	30	30	30	9°596896	30	30	30	30
71	11	9°076007	11 17	10°923993	9°079110	11 18	10°920890	10°003104	11 3	9°596896	30	30	30	30	9°596889	30	30	30	30
72	12	9°076533	12 35	10°923467	9°079644	12 35	10°920356	10°003111	12 3	9°596889	30	30	30	30	9°596881	30	30	30	30
73	13	9°077058	13 52	10°922942	9°080177	13 53	10°919823	10°003119	13 3	9°596881	30	30	30	30	9°596874	30	30	30	30
74	14	9°077583	14 70	10°922417	9°080710	14 71	10°919290	10°003126	14 4	9°596874	30	30	30	30	9°596866	30	30	30	30
75	15	9°078107	15 87	10°921893	9°081241	15 89	10°918755	10°003134	15 4	9°596866	30	30	30	30	9°596858	30	30	30	30
76	16	9°078631	16 105	10°921369	9°081773	16 106	10°918227	10°003142	16 4	9°596858	30	30	30	30	9°596851	30	30	30	30
77	17	9°079154	17 122	10°920846	9°082303	17 124	10°917697	10°003149	17 4	9°596851	30	30	30	30	9°596843	30	30	30	30
78	18	9°079676	18 140	10°920324	9°082833	18 142	10°917167	10°003157	18 5	9°596843	30	30	30	30	9°596835	30	30	30	30
79	19	9°080198	19 157	10°919802	9°083362	19 160	10°916638	10°003165	19 5	9°596835	30	30	30	30	9°596828	30	30	30	30
80	20	9°080719	20 175	10°919281	9°083891	20 177	10°916109	10°003172	20 5	9°596828	30	30	30	30	9°596820	30	30	30	30
81	21	9°081239	21 17	10°918761	9°084419	21 18	10°915581	10°003180	21 5	9°596820	30	30	30	30	9°596812	30	30	30	30
82	22	9°081759	22 34	10°918241	9°084947	22 35	10°915053	10°003188	22 6	9°596812	30	30	30	30	9°596805	30	30	30	30
83	23	9°082278	23 52	10°917722	9°085473	23 53	10°914527	10°003195	23 6	9°596805	30	30	30	30	9°596797	30	30	30	30
84	24	9°082797	24 69	10°917203	9°086000	24 70	10°914000	10°003203	24 6	9°596797	30	30	30	30	9°596789	30	30	30	30
85	25	9°083314	25 86	10°916685	9°086525	25 88	10°913475	10°003211	25 6	9°596789	30	30	30	30	9°596782	30	30	30	30
86	26	9°083832	26 103	10°916168	9°087050	26 105	10°912950	10°003218	26 7	9°596782	30	30	30	30	9°596774	30	30	30	30
87	27	9°084358	27 121	10°915652	9°087574	27 123	10°912426	10°003226	27 7	9°596774	30	30	30	30	9°596766	30	30	30	30
88	28	9°084884	28 138	10°915136	9°088098	28 140	10°911902	10°003234	28 7	9°596766	30	30	30	30	9°596758	30	30	30	30
89	29	9°085409	29 155	10°914620	9°088621	29 158	10°911379	10°003242	29 7	9°596758	30	30	30	30	9°596751	30	30	30	30
90	30	9°085934	30 172	10°914106	9°089144	30 175	10°910856												

LOG. SINES, COSINES, &c.

N ^o 28m				7 ^o									
N	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	N	
0	0	9°085894		10°914106	9°089144	10°910886	10°003249		10°996751	32	60	0	
0	2	9°086409	1" 77	10°913591	9°089666	10°910334	10°003257		9°996743	36	28	0	
1	4	9°086922	2 34	10°913078	9°090187	2 35	10°909813	10°003265	1 0	9°996735	36	50	0
2	6	9°087435	3 51	10°912565	9°090708	3 52	10°909292	10°003273	2 1	9°996727	54	30	0
3	8	9°087947	4 68	10°912053	9°091228	4 69	10°908772	10°003280	3 1	9°996720	32	58	0
4	10	9°088459	5 85	10°911541	9°091747	5 87	10°908253	10°003288	4 1	9°996712	50	38	0
5	12	9°088970	6 102	10°911030	9°092266	6 104	10°907734	10°003296	5 2	9°996704	48	57	0
6	14	9°089480	7 119	10°910520	9°092784	7 121	10°907216	10°003304	6 2	9°996696	46	36	0
7	16	9°089990	8 136	10°910010	9°093302	8 138	10°906698	10°003312	7 2	9°996688	44	56	0
8	18	9°090500	9 153	10°909500	9°093819	9 156	10°906181	10°003320	8 2	9°996680	42	34	0
9	20	9°091008	10 170	10°908992	9°094336	10 173	10°905664	10°003327	9 3	9°996673	30	55	0
10	22	9°091516	1 17	10°908484	9°094851	1 17	10°905149	10°003335	11 3	9°996665	38	28	0
11	24	9°092024	2 34	10°907976	9°095367	2 34	10°904633	10°003343	12 3	9°996657	36	54	0
12	26	9°092530	3 50	10°907470	9°095881	3 51	10°904119	10°003351	13 3	9°996649	34	30	0
13	28	9°093037	4 67	10°906963	9°096395	4 68	10°903605	10°003359	14 4	9°996641	32	53	0
14	30	9°093542	5 84	10°906458	9°096909	5 86	10°903091	10°003367	15 4	9°996633	30	28	0
15	32	9°094047	6 101	10°905953	9°097422	6 103	10°902578	10°003375	16 4	9°996625	28	52	0
16	34	9°094552	7 118	10°905448	9°097934	7 120	10°902066	10°003383	17 4	9°996618	26	30	0
17	36	9°095056	8 135	10°904944	9°098446	8 137	10°901554	10°003390	18 5	9°996610	24	51	0
18	38	9°095559	9 151	10°904441	9°098957	9 154	10°901043	10°003398	19 5	9°996602	22	30	0
19	40	9°096062	10 168	10°903938	9°099468	10 171	10°900532	10°003406	20 5	9°996594	20	50	0
20	42	9°096564	1 17	10°903436	9°099978	1 17	10°900022	10°003414	21 6	9°996586	18	28	0
21	44	9°097066	2 33	10°902935	9°100487	2 34	10°899513	10°003422	22 6	9°996578	16	49	0
22	46	9°097566	3 50	10°902434	9°100996	3 51	10°899004	10°003430	23 6	9°996570	14	28	0
23	48	9°098066	4 67	10°901934	9°101504	4 68	10°898496	10°003438	24 6	9°996562	12	48	0
24	50	9°098566	5 83	10°901434	9°102012	5 85	10°897988	10°003446	25 7	9°996554	10	26	0
25	52	9°099065	6 100	10°900935	9°102519	6 101	10°897481	10°003454	26 7	9°996546	8	47	0
26	54	9°099564	7 116	10°900436	9°103026	7 118	10°896974	10°003462	27 7	9°996538	6	28	0
27	56	9°100062	8 133	10°899938	9°103532	8 135	10°896468	10°003470	28 7	9°996530	4	46	0
28	58	9°100559	9 150	10°899441	9°104037	9 152	10°895963	10°003478	29 8	9°996522	2	25	0
29	60	9°101056	10 166	10°898944	9°104542	10 169	10°895458	10°003486	30 8	9°996514	0	45	0
30	2	9°101552	1 16	10°898448	9°105046	1 17	10°894954	10°003494	1 0	9°996506	38	28	0
31	4	9°102048	2 33	10°897952	9°105550	2 33	10°894450	10°003502	2 1	9°996498	36	44	0
32	6	9°102543	3 49	10°897457	9°106053	3 50	10°893947	10°003510	3 1	9°996490	34	30	0
33	8	9°103037	4 66	10°896963	9°106556	4 67	10°893444	10°003518	4 1	9°996482	32	43	0
34	10	9°103531	5 82	10°896469	9°107058	5 84	10°892942	10°003527	5 1	9°996474	30	22	0
35	12	9°104025	6 99	10°895975	9°107559	6 100	10°892441	10°003535	6 2	9°996466	28	42	0
36	14	9°104517	7 115	10°895483	9°108060	7 117	10°891940	10°003543	7 2	9°996457	26	38	0
37	16	9°105010	8 132	10°894990	9°108560	8 134	10°891440	10°003551	8 2	9°996449	24	41	0
38	18	9°105501	9 148	10°894499	9°109060	9 150	10°890940	10°003559	9 2	9°996441	22	30	0
39	20	9°105992	10 165	10°894008	9°109559	10 167	10°890441	10°003567	10 3	9°996433	20	40	0
40	22	9°106483	1 16	10°893517	9°110058	1 17	10°889942	10°003575	11 3	9°996425	38	28	0
41	24	9°106973	2 33	10°893027	9°110556	2 33	10°889444	10°003583	12 3	9°996417	36	38	0
42	26	9°107462	3 49	10°892538	9°111054	3 50	10°888946	10°003591	13 4	9°996409	34	30	0
43	28	9°107951	4 65	10°892049	9°111551	4 66	10°888449	10°003600	14 4	9°996400	32	28	0
44	30	9°108439	5 81	10°891561	9°112047	5 83	10°887953	10°003608	15 4	9°996392	30	26	0
45	32	9°108927	6 98	10°891073	9°112543	6 99	10°887457	10°003616	16 4	9°996384	28	37	0
46	34	9°109414	7 114	10°890586	9°113039	7 116	10°886961	10°003624	17 5	9°996376	26	36	0
47	36	9°109901	8 130	10°890099	9°113533	8 132	10°886467	10°003632	18 5	9°996368	24	38	0
48	38	9°110387	9 146	10°889613	9°114028	9 149	10°885972	10°003640	19 5	9°996359	22	30	0
49	40	9°110873	10 163	10°889127	9°114521	10 165	10°885479	10°003649	20 5	9°996351	20	26	0
50	42	9°111358	1 16	10°888642	9°115015	1 16	10°884985	10°003657	21 6	9°996343	18	38	0
51	44	9°111843	2 32	10°888158	9°115507	2 33	10°884493	10°003665	22 6	9°996335	16	34	0
52	46	9°112326	3 48	10°887674	9°115999	3 49	10°884001	10°003674	23 6	9°996327	14	30	0
53	48	9°112809	4 64	10°887191	9°116491	4 65	10°883509	10°003682	24 7	9°996318	12	23	0
54	50	9°113292	5 80	10°886708	9°116982	5 82	10°883018	10°003690	25 7	9°996310	10	20	0
55	52	9°113774	6 96	10°886226	9°117472	6 98	10°882528	10°003698	26 7	9°996302	8	28	0
56	54	9°114256	7 112	10°885744	9°117962	7 114	10°882038	10°003707	27 7	9°996293	6	28	0
57	56	9°114737	8 129	10°885263	9°118452	8 131	10°881548	10°003715	28 8	9°996285	4	21	0
58	58	9°115218	9 145	10°884782	9°118941	9 147	10°881059	10°003723	29 8	9°996277	2	20	0
59	60	9°115698	10 161	10°884302	9°119429	10 163	10°880571	10°003731	30 8	9°996269	0	20	0
N	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	N	

TABLE 68

755

LOG. SINES, COSINES, &c.

0 ^h 30 ^m												7 ^o												
°		Sine		Parts		Cossec.		Tangent		Parts		Cotang.		Secant		Parts		Cosine		m.		°		
30	0	9°115698				10°882302	9°119429			10°880571	10°003731			9°996269	30	30								
30	2	9°116177	1° 16			10°883823	9°119917	1° 16		10°880083	10°003740	1° 16		9°996260	30	30								
31	4	9°116656	2 32			10°883344	9°120404	2 32		10°879596	10°003748	2 32		9°996252	30	29								
30	6	9°117135	3 48			10°882865	9°120891	3 48		10°879109	10°003756	3 48		9°996244	30	28								
32	8	9°117613	4 64			10°882387	9°121377	4 64		10°878623	10°003765	4 64		9°996235	30	27								
30	10	9°118090	5 80			10°881910	9°121863	5 80		10°878137	10°003773	5 80		9°996227	30	26								
33	12	9°118567	6 95			10°881433	9°122348	6 95		10°877652	10°003781	6 95		9°996219	30	25								
30	14	9°119043	7 111			10°880957	9°122833	7 111		10°877167	10°003790	7 111		9°996210	30	24								
34	16	9°119519	8 127			10°880481	9°123317	8 127		10°876683	10°003798	8 127		9°996202	30	23								
30	18	9°119994	9 143			10°880006	9°123801	9 143		10°876199	10°003807	9 143		9°996193	30	22								
35	20	9°120469	10 159			10°879531	9°124284	10 159		10°875716	10°003815	10 159		9°996185	30	21								
30	22	9°120943	1 16			10°879057	9°124766	1 16		10°875234	10°003823	1 16		9°996177	30	20								
36	24	9°121417	2 32			10°878583	9°125249	2 32		10°874751	10°003832	2 32		9°996168	30	19								
30	26	9°121890	3 47			10°878110	9°125730	3 47		10°874270	10°003840	3 47		9°996160	30	18								
37	28	9°122362	4 63			10°877638	9°126211	4 63		10°873789	10°003849	4 63		9°996151	30	17								
30	30	9°122835	5 79			10°877165	9°126692	5 79		10°873308	10°003857	5 79		9°996143	30	16								
38	32	9°123306	6 94			10°876694	9°127172	6 94		10°872828	10°003866	6 94		9°996134	30	15								
30	34	9°123777	7 110			10°876223	9°127651	7 110		10°872349	10°003874	7 110		9°996126	30	14								
39	36	9°124248	8 126			10°875752	9°128130	8 126		10°871870	10°003883	8 126		9°996117	30	13								
30	38	9°124718	9 141			10°875282	9°128609	9 141		10°871391	10°003891	9 141		9°996109	30	12								
40	40	9°125187	10 157			10°874813	9°129087	10 157		10°870913	10°003900	10 157		9°996100	30	11								
30	42	9°125656	1 16			10°874344	9°129564	1 16		10°870436	10°003908	1 16		9°996092	30	10								
41	44	9°126125	2 31			10°873875	9°130041	2 31		10°869959	10°003917	2 31		9°996083	30	9								
30	46	9°126593	3 47			10°873407	9°130518	3 47		10°869482	10°003925	3 47		9°996075	30	8								
42	48	9°127060	4 62			10°872940	9°130994	4 62		10°869006	10°003934	4 62		9°996066	30	7								
30	50	9°127527	5 78			10°872473	9°131469	5 78		10°868531	10°003942	5 78		9°996058	30	6								
43	52	9°127993	6 93			10°872007	9°131944	6 93		10°868056	10°003951	6 93		9°996049	30	5								
30	54	9°128459	7 109			10°871541	9°132419	7 109		10°867581	10°003959	7 109		9°996041	30	4								
44	56	9°128925	8 124			10°871075	9°132893	8 124		10°867107	10°003968	8 124		9°996032	30	3								
30	58	9°129390	9 140			10°870610	9°133366	9 140		10°866634	10°003977	9 140		9°996023	30	2								
45	60	9°129854	10 155			10°870146	9°133839	10 155		10°866161	10°003985	10 155		9°996015	30	1								
30	2	9°130318	1 15			10°869682	9°134312	1 15		10°865688	10°003994	1 15		9°996006	30	0								
46	4	9°130781	2 31			10°869219	9°134784	2 31		10°865216	10°004002	2 31		9°995998	30	0								
30	6	9°131244	3 46			10°868756	9°135255	3 46		10°864745	10°004011	3 46		9°995989	30	0								
47	8	9°131706	4 62			10°868294	9°135726	4 62		10°864274	10°004020	4 62		9°995980	30	0								
30	10	9°132168	5 77			10°867832	9°136197	5 77		10°863803	10°004028	5 77		9°995972	30	0								
48	12	9°132630	6 92			10°867370	9°136667	6 92		10°863333	10°004037	6 92		9°995963	30	0								
30	14	9°133091	7 108			10°866909	9°137136	7 108		10°862864	10°004046	7 108		9°995954	30	0								
49	16	9°133551	8 123			10°866449	9°137605	8 123		10°862395	10°004054	8 123		9°995946	30	0								
30	18	9°134011	9 139			10°865989	9°138074	9 139		10°861926	10°004063	9 139		9°995937	30	0								
50	20	9°134470	10 154			10°865530	9°138542	10 154		10°861458	10°004072	10 154		9°995928	30	0								
30	22	9°134929	1 15			10°865071	9°139009	1 15		10°860991	10°004080	1 15		9°995920	30	0								
51	24	9°135387	2 30			10°864613	9°139476	2 30		10°860524	10°004089	2 30		9°995911	30	0								
30	26	9°135845	3 46			10°864155	9°139943	3 46		10°860057	10°004098	3 46		9°995902	30	0								
52	28	9°136303	4 61			10°863697	9°140409	4 61		10°859591	10°004106	4 61		9°995894	30	0								
30	30	9°136760	5 76			10°863240	9°140875	5 76		10°859125	10°004115	5 76		9°995885	30	0								
53	32	9°137216	6 91			10°862784	9°141340	6 91		10°858660	10°004124	6 91		9°995876	30	0								
30	34	9°137672	7 106			10°862328	9°141805	7 106		10°858195	10°004133	7 106		9°995867	30	0								
54	36	9°138128	8 122			10°861872	9°142269	8 122		10°857731	10°004141	8 122		9°995859	30	0								
30	38	9°138582	9 137			10°861418	9°142733	9 137		10°857267	10°004150	9 137		9°995850	30	0								
55	40	9°139037	10 152			10°860963	9°143196	10 152		10°856804	10°004159	10 152		9°995841	30	0								
30	42	9°139491	1 15			10°860509	9°143659	1 15		10°856341	10°004168	1 15		9°995833	30	0								
56	44	9°139944	2 30			10°860056	9°144121	2 30		10°855879	10°004177	2 30		9°995824	30	0								
30	46	9°140398	3 45			10°859602	9°144583	3 45		10°855417	10°004185	3 45		9°995815	30	0								
57	48	9°140850	4 60			10°859150	9°145044	4 60		10°854956	10°004194	4 60		9°995806	30	0								
30	50	9°141302	5 75			10°858698	9°145505	5 75		10°854495	10°004203	5 75		9°995797	30	0								
58	52	9°141755	6 90			10°858246	9°145966	6 90		10°854034	10°004212	6 90		9°995788	30	0								
30	54	9°142205	7 105			10°857795	9°146425	7 105		10°853575	10°004221	7 105		9°995779	30	0								
59	56	9°142655	8 121			10°857345	9°146885	8 121		10°853115	10°004229	8 121		9°995771	30	0								
30	58	9°143106	9 136			10°856894	9°147344	9 136		10°852656	10°004238	9 136		9°995762	30	0								
60	60	9°143555	10 151			10°856445	9°147803	10 151		10°852197	10°004247	10 151		9°995753	30	0								
°												82 ^o												

LOG. SINES, COSINES, &c.

0° 32'				8°											
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'	Sine	Parts
0	0	9°143555		10°856445	9°147803	1°15	10°852197	10°004247	1°0	9°995753	28	0	0	9°143555	28
1	2	9°144005	15	10°855995	9°148261	2	10°851739	10°004256	1	9°995744	29	1	2	9°144005	29
2	4	9°144453	30	10°855547	9°148718	3	10°851282	10°004265	2	9°995735	30	2	4	9°144453	30
3	6	9°144902	45	10°855098	9°149175	4	10°850825	10°004274	3	9°995726	31	3	6	9°144902	31
4	8	9°145349	59	10°854651	9°149632	5	10°850368	10°004283	4	9°995717	32	4	8	9°145349	32
5	10	9°145797	74	10°854203	9°150088	6	10°849912	10°004292	5	9°995708	33	5	10	9°145797	33
6	12	9°146243	89	10°853757	9°150544	7	10°849456	10°004301	6	9°995699	34	6	12	9°146243	34
7	14	9°146690	104	10°853310	9°151000	8	10°849000	10°004310	7	9°995690	35	7	14	9°146690	35
8	16	9°147136	119	10°852864	9°151454	9	10°848546	10°004319	8	9°995681	36	8	16	9°147136	36
9	18	9°147581	134	10°852419	9°151909	10	10°848091	10°004328	9	9°995672	37	9	18	9°147581	37
10	20	9°148026	149	10°851974	9°152363	11	10°847637	10°004336	10	9°995664	38	10	20	9°148026	38
11	22	9°148471	165	10°851529	9°152816	12	10°847184	10°004345	11	9°995655	39	11	22	9°148471	39
12	24	9°148915	180	10°851085	9°153269	13	10°846731	10°004354	12	9°995646	40	12	24	9°148915	40
13	26	9°149358	195	10°850642	9°153722	14	10°846278	10°004363	13	9°995637	41	13	26	9°149358	41
14	28	9°149802	210	10°850198	9°154174	15	10°845826	10°004372	14	9°995628	42	14	28	9°149802	42
15	30	9°150244	225	10°849756	9°154626	16	10°845374	10°004381	15	9°995619	43	15	30	9°150244	43
16	32	9°150686	240	10°849314	9°155077	17	10°844923	10°004390	16	9°995610	44	16	32	9°150686	44
17	34	9°151128	255	10°848872	9°155528	18	10°844472	10°004400	17	9°995601	45	17	34	9°151128	45
18	36	9°151569	270	10°848431	9°155978	19	10°844022	10°004409	18	9°995592	46	18	36	9°151569	46
19	38	9°152010	285	10°847990	9°156428	20	10°843572	10°004418	19	9°995583	47	19	38	9°152010	47
20	40	9°152451	300	10°847549	9°156877	21	10°843123	10°004427	20	9°995574	48	20	40	9°152451	48
21	42	9°152891	315	10°847109	9°157326	22	10°842674	10°004436	21	9°995565	49	21	42	9°152891	49
22	44	9°153330	330	10°846670	9°157775	23	10°842225	10°004445	22	9°995556	50	22	44	9°153330	50
23	46	9°153769	345	10°846231	9°158223	24	10°841777	10°004454	23	9°995547	51	23	46	9°153769	51
24	48	9°154208	360	10°845792	9°158671	25	10°841329	10°004463	24	9°995538	52	24	48	9°154208	52
25	50	9°154646	375	10°845354	9°159118	26	10°840882	10°004472	25	9°995529	53	25	50	9°154646	53
26	52	9°155083	390	10°844917	9°159565	27	10°840435	10°004481	26	9°995520	54	26	52	9°155083	54
27	54	9°155521	405	10°844479	9°160011	28	10°839989	10°004490	27	9°995511	55	27	54	9°155521	55
28	56	9°155957	420	10°844043	9°160457	29	10°839543	10°004499	28	9°995502	56	28	56	9°155957	56
29	58	9°156394	435	10°843608	9°160902	30	10°839098	10°004509	29	9°995493	57	29	58	9°156394	57
30	60	9°156830	450	10°843170	9°161347	31	10°838653	10°004518	30	9°995484	58	30	60	9°156830	58
31	2	9°157265	465	10°842735	9°161792	32	10°838208	10°004527	31	9°995475	59	31	2	9°157265	59
32	4	9°157700	480	10°842300	9°162236	33	10°837764	10°004536	32	9°995466	60	32	4	9°157700	60
33	6	9°158135	495	10°841865	9°162680	34	10°837320	10°004545	33	9°995457	61	33	6	9°158135	61
34	8	9°158569	510	10°841431	9°163123	35	10°836877	10°004554	34	9°995448	62	34	8	9°158569	62
35	10	9°159002	525	10°840998	9°163566	36	10°836434	10°004564	35	9°995439	63	35	10	9°159002	63
36	12	9°159435	540	10°840565	9°164008	37	10°835992	10°004573	36	9°995430	64	36	12	9°159435	64
37	14	9°159868	555	10°840132	9°164450	38	10°835550	10°004582	37	9°995421	65	37	14	9°159868	65
38	16	9°160301	570	10°839699	9°164892	39	10°835108	10°004591	38	9°995412	66	38	16	9°160301	66
39	18	9°160732	585	10°839268	9°165333	40	10°834667	10°004601	39	9°995403	67	39	18	9°160732	67
40	20	9°161164	600	10°838836	9°165774	41	10°834226	10°004610	40	9°995394	68	40	20	9°161164	68
41	22	9°161595	615	10°838405	9°166214	42	10°833786	10°004619	41	9°995385	69	41	22	9°161595	69
42	24	9°162025	630	10°837975	9°166654	43	10°833346	10°004628	42	9°995376	70	42	24	9°162025	70
43	26	9°162456	645	10°837544	9°167093	44	10°832907	10°004638	43	9°995367	71	43	26	9°162456	71
44	28	9°162885	660	10°837115	9°167532	45	10°832468	10°004647	44	9°995358	72	44	28	9°162885	72
45	30	9°163315	675	10°836685	9°167971	46	10°832029	10°004656	45	9°995349	73	45	30	9°163315	73
46	32	9°163743	690	10°836257	9°168409	47	10°831591	10°004666	46	9°995340	74	46	32	9°163743	74
47	34	9°164172	705	10°835828	9°168847	48	10°831153	10°004675	47	9°995331	75	47	34	9°164172	75
48	36	9°164600	720	10°835400	9°169284	49	10°830716	10°004684	48	9°995322	76	48	36	9°164600	76
49	38	9°165027	735	10°834973	9°169721	50	10°830279	10°004694	49	9°995313	77	49	38	9°165027	77
50	40	9°165454	750	10°834546	9°170157	51	10°829843	10°004703	50	9°995304	78	50	40	9°165454	78
51	42	9°165881	765	10°834119	9°170593	52	10°829407	10°004712	51	9°995295	79	51	42	9°165881	79
52	44	9°166307	780	10°833693	9°171029	53	10°828971	10°004722	52	9°995286	80	52	44	9°166307	80
53	46	9°166733	795	10°833267	9°171464	54	10°828536	10°004731	53	9°995277	81	53	46	9°166733	81
54	48	9°167159	810	10°832841	9°171899	55	10°828101	10°004740	54	9°995268	82	54	48	9°167159	82
55	50	9°167584	825	10°832416	9°172333	56	10°827667	10°004750	55	9°995259	83	55	50	9°167584	83
56	52	9°168008	840	10°831992	9°172767	57	10°827233	10°004759	56	9°995250	84	56	52	9°168008	84
57	54	9°168432	855	10°831568	9°173201	58	10°826799	10°004769	57	9°995241	85	57	54	9°168432	85
58	56	9°168856	870	10°831144	9°173634	59	10°826366	10°004778	58	9°995232	86	58	56	9°168856	86
59	58	9°169279	885	10°830721	9°174067	60	10°825933	10°004787	59	9°995223	87	59	58	9°169279	87
60	60	9°169702	900	10°830298	9°174499	61	10°825501	10°004797	60	9°995214	88	60	60	9°169702	88
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	Parts	°	'	Cosine	Parts
81	0	9°143555		10°856445	9°147803	1°15	10°852197	10°004247	1°0	9°995753	28	81	0	9°143555	28
81	1	9°144005	15	10°855995	9°148261	2	10°851739	10°004256	1	9°995744	29	81	1	9°144005	29
81	2	9°144453	30	10°855547	9°148718	3	10°851282	10°004265	2	9°995735	30	81	2	9°144453	30
81	3	9°144902	45	10°855098	9°149175	4	10°850825	10°004274	3	9°995726	31	81	3	9°144902	31
81	4	9°145349	59	10°854651	9°149632	5	10°850368	10°004283	4	9°995717	32	81	4	9°145349	32
81	5	9°145797	74	10°854203	9°150088	6	10°849912	10°004292	5	9°995708	33	81	5	9°145797	33
81	6	9°146243	89	10°853757	9°150544	7	10°849456	10°004301	6	9°995699	34	81	6	9°146243	34
81	7	9°146690	104	10°853310	9°151000	8	10°849000	10°004310	7	9°995690	35	81	7	9°146690	35
81	8	9°147136	119	10°852864	9°151454	9	10°848546	10°004319	8	9°995681	36	81	8	9°147136	36
81	9	9°147581	134	10°852419	9°151909	10	10°848091	10°004328	9	9°995672	37	81	9	9°147581	37
81	10	9°148026	149	10°851974	9°152363	11	10°847637	10°004336	10	9°995664	38	81	10	9°148026	38
81	11	9°148471	165	10°851529	9°152816	12	10°847184	10°004345	11						

LOG. SINES. COSINES, &c.

0° 34'				8°											
°	'	m.	n.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	n.	
30	0			9°169702		10°830298	9°174499		10°825501	10°004797		9°995203	26	30	
30	2			9°170125	1" 14	10°829875	9°174951	1" 14	10°825069	10°004806	1" 14	9°995194	28	30	
31	4			9°170547	2 28	10°829453	9°175362	2 28	10°824638	10°004816	2 1	9°995184	30	29	
30	6			9°170968	3 42	10°829032	9°175793	3 43	10°824207	10°004825	3 1	9°995175	32	31	
32	8			9°171389	4 56	10°828611	9°176224	4 57	10°823776	10°004835	4 1	9°995165	34	28	
30	10			9°171810	5 70	10°828190	9°176654	5 72	10°823346	10°004844	5 2	9°995156	36	30	
33	12			9°172230	6 84	10°827770	9°177084	6 86	10°822916	10°004854	6 2	9°995146	38	27	
30	14			9°172650	7 98	10°827350	9°177513	7 100	10°822487	10°004863	7 2	9°995137	40	30	
34	16			9°173070	8 112	10°826930	9°177942	8 115	10°822058	10°004873	8 3	9°995127	42	26	
30	18			9°173489	9 126	10°826511	9°178371	9 129	10°821629	10°004882	9 3	9°995118	44	31	
35	20			9°173908	10 140	10°826092	9°178799	10 143	10°821201	10°004892	10 3	9°995108	46	26	
30	22			9°174326	1 14	10°825674	9°179227	1 14	10°820773	10°004901	11 4	9°995099	48	30	
36	24			9°174744	2 28	10°825256	9°179655	2 28	10°820345	10°004911	12 4	9°995089	50	24	
30	26			9°175161	3 41	10°824839	9°180083	3 43	10°819918	10°004920	13 4	9°995080	52	30	
37	28			9°175578	4 55	10°824422	9°180508	4 57	10°819492	10°004930	14 4	9°995070	54	23	
30	30			9°175995	5 69	10°824005	9°180934	5 71	10°819066	10°004939	15 5	9°995061	56	30	
38	32			9°176411	6 83	10°823589	9°181360	6 85	10°818640	10°004949	16 5	9°995051	58	22	
30	34			9°176827	7 97	10°823173	9°181786	7 99	10°818214	10°004958	17 5	9°995041	60	30	
39	36			9°177242	8 111	10°822758	9°182211	8 114	10°817789	10°004968	18 6	9°995032	62	21	
30	38			9°177657	9 124	10°822343	9°182635	9 128	10°817365	10°004978	19 6	9°995022	64	30	
40	40			9°178072	10 138	10°821928	9°183059	10 142	10°816941	10°004987	20 6	9°995013	66	20	
30	42			9°178486	1 14	10°821514	9°183483	1 14	10°816517	10°004997	21 7	9°995003	68	30	
41	44			9°178900	2 27	10°821100	9°183907	2 28	10°816093	10°005007	22 7	9°994993	70	19	
30	46			9°179315	3 41	10°820687	9°184330	3 42	10°815670	10°005016	23 7	9°994984	72	30	
42	48			9°179726	4 55	10°820274	9°184752	4 56	10°815248	10°005026	24 8	9°994974	74	18	
30	50			9°180139	5 69	10°819861	9°185175	5 70	10°814825	10°005036	25 8	9°994964	76	30	
43	52			9°180551	6 82	10°819449	9°185597	6 84	10°814403	10°005045	26 8	9°994955	78	17	
30	54			9°180963	7 96	10°819037	9°186018	7 98	10°813982	10°005055	27 9	9°994945	80	30	
44	56			9°181374	8 110	10°818626	9°186439	8 113	10°813561	10°005065	28 9	9°994935	82	16	
30	58			9°181785	9 124	10°818215	9°186860	9 127	10°813140	10°005075	29 9	9°994925	84	30	
45	60			9°182196	10 137	10°817804	9°187280	10 141	10°812720	10°005084	30 10	9°994916	86	15	
30	2			9°182606	1 14	10°817394	9°187700	1 14	10°812300	10°005094	1 0	9°994906	88	30	
46	4			9°183016	2 27	10°816984	9°188120	2 28	10°811880	10°005104	2 1	9°994896	90	14	
30	6			9°183425	3 41	10°816575	9°188539	3 42	10°811461	10°005113	3 1	9°994887	92	30	
47	8			9°183834	4 54	10°816166	9°188958	4 56	10°811042	10°005123	4 1	9°994877	94	13	
30	10			9°184243	5 68	10°815757	9°189376	5 70	10°810624	10°005133	5 2	9°994867	96	30	
48	12			9°184651	6 82	10°815349	9°189794	6 84	10°810206	10°005143	6 2	9°994857	98	12	
30	14			9°185059	7 95	10°814941	9°190212	7 98	10°809788	10°005153	7 2	9°994847	100	30	
49	16			9°185466	8 109	10°814534	9°190629	8 111	10°809371	10°005162	8 3	9°994838	102	11	
30	18			9°185874	9 122	10°814126	9°191046	9 125	10°808954	10°005172	9 3	9°994828	104	30	
50	20			9°186280	10 136	10°813720	9°191462	10 139	10°808538	10°005182	10 3	9°994818	106	10	
30	22			9°186686	1 13	10°813314	9°191878	1 14	10°808122	10°005192	11 4	9°994808	108	30	
51	24			9°187092	2 27	10°812908	9°192294	2 28	10°807706	10°005202	12 4	9°994798	110	9	
30	26			9°187498	3 40	10°812502	9°192709	3 41	10°807291	10°005211	13 4	9°994789	112	30	
52	28			9°187903	4 54	10°812097	9°193124	4 55	10°806876	10°005221	14 5	9°994779	114	8	
30	30			9°188308	5 67	10°811692	9°193539	5 69	10°806461	10°005231	15 5	9°994769	116	30	
53	32			9°188712	6 81	10°811288	9°193953	6 83	10°806047	10°005241	16 5	9°994759	118	7	
30	34			9°189116	7 94	10°810884	9°194367	7 97	10°805633	10°005251	17 6	9°994749	120	30	
54	36			9°189519	8 108	10°810481	9°194780	8 110	10°805220	10°005261	18 6	9°994739	122	6	
30	38			9°189923	9 121	10°810077	9°195193	9 124	10°804807	10°005271	19 6	9°994729	124	30	
55	40			9°190325	10 135	10°809675	9°195606	10 138	10°804394	10°005280	20 7	9°994720	126	5	
30	42			9°190728	1 13	10°809272	9°196018	1 14	10°803982	10°005290	21 7	9°994710	128	30	
56	44			9°191130	2 27	10°808870	9°196432	2 27	10°803570	10°005300	22 7	9°994700	130	4	
30	46			9°191532	3 40	10°808468	9°196843	3 41	10°803158	10°005310	23 8	9°994690	132	30	
57	48			9°191933	4 53	10°808067	9°197253	4 55	10°802747	10°005320	24 8	9°994680	134	3	
30	50			9°192334	5 67	10°807666	9°197664	5 68	10°802336	10°005330	25 8	9°994670	136	30	
58	52			9°192734	6 80	10°807266	9°198074	6 82	10°801926	10°005340	26 9	9°994660	138	2	
30	54			9°193134	7 93	10°806866	9°198484	7 96	10°801516	10°005350	27 9	9°994650	140	30	
59	56			9°193534	8 107	10°806466	9°198894	8 109	10°801106	10°005360	28 9	9°994640	142	1	
30	58			9°193933	9 120	10°806067	9°199304	9 123	10°800696	10°005370	29 10	9°994630	144	30	
60	60			9°194332	10 133	10°805668	9°199713	10 137	10°800287	10°005380	30 10	9°994620	146	0	
°	'	m.	n.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	n.	
81°				8° 24'											

LOG. SINES, COSINES, &c.

36°		90°										36°	
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'
0	0	9°194332		10°805668	9°199715		10°802287	10°005380		9°994620		0	0
30	2	9°194731	1° 13	10°805269	9°200121	1° 13	10°799879	10°005390	1° 0	9°994610	58	30	2
1	4	9°195129	2 26	10°804871	9°200529	2 27	10°799471	10°005400	2 1	9°994600	56	58	4
30	6	9°195527	3 39	10°804473	9°200937	3 40	10°799063	10°005410	3 1	9°994590	54	30	6
2	8	9°195925	4 52	10°804075	9°201345	4 54	10°798655	10°005420	4 1	9°994580	52	54	8
30	10	9°196322	5 65	10°803678	9°201752	5 67	10°798248	10°005430	5 2	9°994570	50	30	10
3	12	9°196719	6 79	10°803281	9°202159	6 81	10°797841	10°005440	6 2	9°994560	48	57	12
30	14	9°197115	7 92	10°802885	9°202565	7 94	10°797435	10°005450	7 2	9°994550	46	30	14
4	16	9°197511	8 105	10°802489	9°202971	8 108	10°797029	10°005460	8 3	9°994540	44	56	16
30	18	9°197907	9 118	10°802093	9°203377	9 121	10°796623	10°005470	9 3	9°994530	42	30	18
5	20	9°198302	10 131	10°801698	9°203782	10 134	10°796218	10°005480	10 3	9°994520	40	55	20
30	22	9°198697	11 144	10°801303	9°204188	11 148	10°795812	10°005490	11 4	9°994509	38	30	22
6	24	9°199091	12 157	10°800909	9°204592	12 161	10°795408	10°005500	12 4	9°994499	36	54	24
30	26	9°199486	13 170	10°800514	9°204996	13 175	10°795004	10°005510	13 4	9°994489	34	30	26
7	28	9°199879	14 183	10°800121	9°205400	14 188	10°794600	10°005520	14 5	9°994479	32	53	28
30	30	9°200273	15 197	10°799727	9°205804	15 201	10°794196	10°005530	15 5	9°994469	30	30	30
8	32	9°200666	16 210	10°799334	9°206207	16 215	10°793793	10°005540	16 5	9°994459	28	52	32
30	34	9°201059	17 223	10°798941	9°206610	17 229	10°793390	10°005550	17 6	9°994448	26	30	34
9	36	9°201451	18 236	10°798549	9°207013	18 242	10°792987	10°005560	18 6	9°994438	24	51	36
30	38	9°201843	19 249	10°798157	9°207415	19 255	10°792585	10°005570	19 6	9°994428	22	30	38
10	40	9°202234	20 262	10°797766	9°207817	20 269	10°792183	10°005580	20 7	9°994418	20	50	40
30	42	9°202626	21 275	10°797374	9°208218	21 282	10°791782	10°005590	21 7	9°994408	18	30	42
11	44	9°203017	22 288	10°796983	9°208619	22 295	10°791381	10°005600	22 7	9°994398	16	49	44
30	46	9°203407	23 301	10°796593	9°209020	23 309	10°790980	10°005610	23 8	9°994387	14	30	46
12	48	9°203797	24 315	10°796203	9°209420	24 323	10°790580	10°005620	24 8	9°994377	12	48	48
30	50	9°204187	25 328	10°795813	9°209820	25 336	10°790180	10°005630	25 8	9°994367	10	30	50
13	52	9°204577	26 341	10°795423	9°210220	26 350	10°789780	10°005640	26 9	9°994357	8	47	52
30	54	9°204966	27 354	10°795034	9°210619	27 363	10°789381	10°005650	27 9	9°994346	6	30	54
14	56	9°205354	28 367	10°794646	9°211018	28 376	10°788982	10°005660	28 9	9°994336	4	46	56
30	58	9°205743	29 380	10°794257	9°211417	29 390	10°788583	10°005670	29 10	9°994326	2	30	58
15	59	9°206131	30 393	10°793869	9°211815	30 403	10°788185	10°005680	30 10	9°994316	23	45	59
30	2	9°206519	1 13	10°793481	9°212213	1 13	10°787787	10°005690	1 0	9°994305	58	30	2
16	4	9°206906	2 25	10°793094	9°212611	2 26	10°787389	10°005700	2 1	9°994295	56	44	4
30	6	9°207293	3 38	10°792707	9°213008	3 39	10°786990	10°005710	3 1	9°994285	54	30	6
17	8	9°207679	4 51	10°792321	9°213405	4 52	10°786595	10°005720	4 1	9°994274	52	43	8
30	10	9°208066	5 64	10°791934	9°213802	5 65	10°786198	10°005730	5 2	9°994264	50	30	10
18	12	9°208452	6 76	10°791548	9°214198	6 79	10°785802	10°005740	6 2	9°994254	48	42	12
30	14	9°208837	7 89	10°791163	9°214594	7 92	10°785406	10°005750	7 2	9°994243	46	30	14
19	16	9°209222	8 102	10°790778	9°214989	8 105	10°785011	10°005760	8 3	9°994233	44	41	16
30	18	9°209607	9 115	10°790393	9°215385	9 118	10°784615	10°005770	9 3	9°994223	42	30	18
20	20	9°209992	10 127	10°790008	9°215780	10 131	10°784220	10°005780	10 3	9°994212	40	40	20
30	22	9°210376	11 140	10°789624	9°216174	11 144	10°783826	10°005790	11 4	9°994202	38	30	22
21	24	9°210760	12 153	10°789240	9°216568	12 157	10°783432	10°005800	12 4	9°994191	36	39	24
30	26	9°211143	13 166	10°788857	9°216962	13 170	10°783038	10°005810	13 4	9°994181	34	30	26
22	28	9°211526	14 178	10°788474	9°217356	14 183	10°782644	10°005820	14 5	9°994171	32	38	28
30	30	9°211909	15 191	10°788091	9°217749	15 196	10°782251	10°005830	15 5	9°994160	30	30	30
23	32	9°212291	16 204	10°787709	9°218142	16 210	10°781858	10°005840	16 5	9°994150	28	37	32
30	34	9°212674	17 217	10°787326	9°218534	17 223	10°781466	10°005850	17 6	9°994139	26	30	34
24	36	9°213055	18 229	10°786945	9°218926	18 236	10°781074	10°005860	18 6	9°994129	24	36	36
30	38	9°213437	19 242	10°786563	9°219318	19 249	10°780682	10°005870	19 6	9°994118	22	30	38
25	40	9°213818	20 255	10°786182	9°219710	20 262	10°780290	10°005880	20 7	9°994108	20	35	40
30	42	9°214198	21 268	10°785802	9°220101	21 275	10°779899	10°005890	21 7	9°994097	18	30	42
26	44	9°214579	22 280	10°785421	9°220492	22 288	10°779508	10°005900	22 7	9°994087	16	34	44
30	46	9°214959	23 293	10°785041	9°220882	23 301	10°779118	10°005910	23 8	9°994076	14	30	46
27	48	9°215338	24 306	10°784662	9°221272	24 314	10°778728	10°005920	24 8	9°994066	12	33	48
30	50	9°215718	25 319	10°784282	9°221662	25 327	10°778338	10°005930	25 8	9°994055	10	30	50
28	52	9°216097	26 331	10°783903	9°222052	26 341	10°777948	10°005940	26 9	9°994045	8	32	52
30	54	9°216475	27 344	10°783525	9°222441	27 354	10°777559	10°005950	27 9	9°994034	6	30	54
29	56	9°216854	28 357	10°783146	9°222830	28 367	10°777170	10°005960	28 10	9°994024	4	31	56
30	58	9°217232	29 370	10°782768	9°223218	29 380	10°776782	10°005970	29 10	9°994013	2	30	58
30	59	9°217609	30 382	10°782391	9°223607	30 393	10°776393	10°005980	30 10	9°994003	0	30	59
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	Parts	°	'

TABLE 68

757

LOG. SINES, COSINES, &c.

0° 38'										9°									
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant
30	0	9'217609		10'782391	9'223607		10'776393	10'005997		9'994003	30	0	9'217609		10'782391	9'223607		10'776393	10'005997
30	1	9'217987	1"	10'782013	9'223994	1"	10'776006	10'006008	1"	9'993992	30	1	9'217987	1"	10'782013	9'223994	1"	10'776006	10'006008
31	1	9'218363	3 25	10'781637	9'224382	3 25	10'775618	10'006019	3 25	9'993971	31	1	9'218363	3 25	10'781637	9'224382	3 25	10'775618	10'006019
31	2	9'218740	3 37	10'781260	9'224769	3 37	10'775231	10'006029	3 37	9'993950	31	2	9'218740	3 37	10'781260	9'224769	3 37	10'775231	10'006029
32	0	9'219116	4 50	10'780884	9'225156	4 50	10'774844	10'006040	4 50	9'993928	32	0	9'219116	4 50	10'780884	9'225156	4 50	10'774844	10'006040
32	1	9'219492	5 62	10'780508	9'225543	5 62	10'774457	10'006050	5 62	9'993907	32	1	9'219492	5 62	10'780508	9'225543	5 62	10'774457	10'006050
33	0	9'219868	6 74	10'780132	9'225929	6 74	10'774071	10'006061	6 74	9'993886	33	0	9'219868	6 74	10'780132	9'225929	6 74	10'774071	10'006061
33	1	9'220243	7 87	10'779757	9'226315	7 87	10'773685	10'006072	7 87	9'993864	33	1	9'220243	7 87	10'779757	9'226315	7 87	10'773685	10'006072
34	0	9'220618	8 99	10'779382	9'226700	8 99	10'773300	10'006082	8 99	9'993842	34	0	9'220618	8 99	10'779382	9'226700	8 99	10'773300	10'006082
34	1	9'220993	9 112	10'779007	9'227086	9 112	10'772914	10'006093	9 112	9'993820	34	1	9'220993	9 112	10'779007	9'227086	9 112	10'772914	10'006093
35	0	9'221367	10 124	10'778633	9'227471	10 124	10'772529	10'006103	10 124	9'993797	35	0	9'221367	10 124	10'778633	9'227471	10 124	10'772529	10'006103
35	1	9'221741	11 136	10'778259	9'227855	11 140	10'772145	10'006114	11 140	9'993775	35	1	9'221741	11 136	10'778259	9'227855	11 140	10'772145	10'006114
36	0	9'222115	12 149	10'777883	9'228239	12 153	10'771761	10'006125	12 153	9'993753	36	0	9'222115	12 149	10'777883	9'228239	12 153	10'771761	10'006125
36	1	9'222488	13 161	10'777512	9'228623	13 166	10'771377	10'006136	13 166	9'993731	36	1	9'222488	13 161	10'777512	9'228623	13 166	10'771377	10'006136
37	0	9'222861	14 174	10'777139	9'229007	14 179	10'770993	10'006146	14 179	9'993709	37	0	9'222861	14 174	10'777139	9'229007	14 179	10'770993	10'006146
37	1	9'223234	15 186	10'776766	9'229390	15 192	10'770610	10'006157	15 192	9'993687	37	1	9'223234	15 186	10'776766	9'229390	15 192	10'770610	10'006157
38	0	9'223606	16 198	10'776394	9'229773	16 204	10'770227	10'006168	16 204	9'993665	38	0	9'223606	16 198	10'776394	9'229773	16 204	10'770227	10'006168
38	1	9'223978	17 211	10'776022	9'230156	17 217	10'769844	10'006178	17 217	9'993643	38	1	9'223978	17 211	10'776022	9'230156	17 217	10'769844	10'006178
39	0	9'224349	18 223	10'775651	9'230539	18 230	10'769461	10'006189	18 230	9'993621	39	0	9'224349	18 223	10'775651	9'230539	18 230	10'769461	10'006189
39	1	9'224721	19 236	10'775279	9'230921	19 243	10'769079	10'006200	19 243	9'993599	39	1	9'224721	19 236	10'775279	9'230921	19 243	10'769079	10'006200
40	0	9'225092	20 248	10'774908	9'231302	20 255	10'768698	10'006211	20 255	9'993577	40	0	9'225092	20 248	10'774908	9'231302	20 255	10'768698	10'006211
40	1	9'225462	21 261	10'774538	9'231684	21 268	10'768316	10'006222	21 268	9'993555	40	1	9'225462	21 261	10'774538	9'231684	21 268	10'768316	10'006222
41	0	9'225833	22 273	10'774167	9'232065	22 281	10'767935	10'006232	22 281	9'993533	41	0	9'225833	22 273	10'774167	9'232065	22 281	10'767935	10'006232
41	1	9'226203	23 286	10'773797	9'232446	23 294	10'767554	10'006243	23 294	9'993511	41	1	9'226203	23 286	10'773797	9'232446	23 294	10'767554	10'006243
42	0	9'226573	24 298	10'773427	9'232826	24 307	10'767174	10'006254	24 307	9'993489	42	0	9'226573	24 298	10'773427	9'232826	24 307	10'767174	10'006254
42	1	9'226942	25 310	10'773058	9'233206	25 320	10'766794	10'006265	25 320	9'993467	42	1	9'226942	25 310	10'773058	9'233206	25 320	10'766794	10'006265
43	0	9'227311	26 323	10'772689	9'233586	26 332	10'766414	10'006275	26 332	9'993445	43	0	9'227311	26 323	10'772689	9'233586	26 332	10'766414	10'006275
43	1	9'227680	27 335	10'772320	9'233966	27 345	10'766034	10'006286	27 345	9'993423	43	1	9'227680	27 335	10'772320	9'233966	27 345	10'766034	10'006286
44	0	9'228048	28 348	10'771952	9'234345	28 358	10'765655	10'006297	28 358	9'993401	44	0	9'228048	28 348	10'771952	9'234345	28 358	10'765655	10'006297
44	1	9'228416	29 360	10'771584	9'234724	29 371	10'765276	10'006308	29 371	9'993379	44	1	9'228416	29 360	10'771584	9'234724	29 371	10'765276	10'006308
45	0	9'228784	30 372	10'771216	9'235103	30 383	10'764897	10'006319	30 383	9'993357	45	0	9'228784	30 372	10'771216	9'235103	30 383	10'764897	10'006319
45	1	9'229151	1 12	10'770849	9'235481	1 12	10'764519	10'006330	1 12	9'993335	45	1	9'229151	1 12	10'770849	9'235481	1 12	10'764519	10'006330
46	0	9'229518	2 24	10'770482	9'235859	2 25	10'764141	10'006340	2 25	9'993313	46	0	9'229518	2 24	10'770482	9'235859	2 25	10'764141	10'006340
46	1	9'229885	3 36	10'770115	9'236237	3 37	10'763763	10'006351	3 37	9'993291	46	1	9'229885	3 36	10'770115	9'236237	3 37	10'763763	10'006351
47	0	9'230252	4 48	10'769748	9'236614	4 50	10'763386	10'006362	4 50	9'993269	47	0	9'230252	4 48	10'769748	9'236614	4 50	10'763386	10'006362
47	1	9'230618	5 60	10'769382	9'236991	5 62	10'763009	10'006373	5 62	9'993247	47	1	9'230618	5 60	10'769382	9'236991	5 62	10'763009	10'006373
48	0	9'230984	6 73	10'769016	9'237368	6 75	10'762632	10'006384	6 75	9'993225	48	0	9'230984	6 73	10'769016	9'237368	6 75	10'762632	10'006384
48	1	9'231349	7 85	10'768651	9'237744	7 87	10'762256	10'006395	7 87	9'993203	48	1	9'231349	7 85	10'768651	9'237744	7 87	10'762256	10'006395
49	0	9'231715	8 97	10'768285	9'238120	8 100	10'761880	10'006406	8 100	9'993181	49	0	9'231715	8 97	10'768285	9'238120	8 100	10'761880	10'006406
49	1	9'232079	9 109	10'767921	9'238496	9 112	10'761504	10'006417	9 112	9'993159	49	1	9'232079	9 109	10'767921	9'238496	9 112	10'761504	10'006417
50	0	9'232444	10 121	10'767556	9'238872	10 125	10'761128	10'006428	10 125	9'993137	50	0	9'232444	10 121	10'767556	9'238872	10 125	10'761128	10'006428
50	1	9'232808	11 133	10'767192	9'239247	11 137	10'760753	10'006439	11 137	9'993115	50	1	9'232808	11 133	10'767192	9'239247	11 137	10'760753	10'006439
51	0	9'233172	12 145	10'766828	9'239622	12 150	10'760378	10'006450	12 150	9'993093	51	0	9'233172	12 145	10'766828	9'239622	12 150	10'760378	10'006450
51	1	9'233536	13 157	10'766464	9'239996	13 162	10'760004	10'006461	13 162	9'993071	51	1	9'233536	13 157	10'766464	9'239996	13 162	10'760004	10'006461
52	0	9'233899	14 169	10'766101	9'240371	14 175	10'759629	10'006472	14 175	9'993049	52	0	9'233899	14 169	10'766101	9'240371	14 175	10'759629	10'006472
52	1	9'234262	15 181	10'765738	9'240745	15 187	10'759255	10'006483	15 187	9'993027	52	1	9'234262	15 181	10'765738	9'240745	15 187	10'759255	10'006483
53	0	9'234625	16 193	10'765375	9'241118	16 200	10'758882	10'006494	16 200	9'993005	53	0	9'234625	16 193	10'765375	9'241118	16 200	10'758882	10'006494
53	1	9'234987	17 206	10'765013	9'241492	17 212	10'758508	10'006505	17 212	9'992983	53	1	9'234987	17 206	10'765013	9'241492	17 212	10'758508	10'006505
54	0	9'235349	18 218	10'764651	9'241865	18 224	10'758135	10'006516	18 224	9'992961	54	0	9'235349	18 218	10'764651	9'241865	18 224	10'758135	10'006516
54	1	9'235711	19 230	10'764289	9'242238	19 237	10'757762	10'006527	19 237	9'992939	54	1	9'235711	19 230	10'764289	9'242238	19 237	10'757762	10'006527
55	0	9'236073	20 242	10'763927	9'242610	20 249	10'757390	10'006538	20 249	9'992917	55	0	9'236073	20 242	10'763927	9'242610	20 249	10'757390	10'006538
55	1	9'236434	21 254	10'763566	9'242982	21 261	10'757018	10'006549	21 261	9'992895	55	1	9'236434	21 254</					

LOG. SINES, COSINES, &c.

0° 40'										10°									
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant
0	0	9°239670		10°760330	9°246319	1°12	10°753681	10°006649		9°993351	20	60	9°239670		10°760330	9°246319	1°12	10°753681	10°006649
30	2	9°240028	1°12	10°759972	9°246688	1°12	10°753312	10°006660	1°0	9°993340	50	30	9°240028	1°12	10°759972	9°246688	1°12	10°753312	10°006660
1	4	9°240386	2 24	10°759614	9°247057	2 24	10°752943	10°006671	2 1	9°993329	50	30	9°240386	2 24	10°759614	9°247057	2 24	10°752943	10°006671
30	6	9°240744	3 35	10°759256	9°247426	3 35	10°752574	10°006682	3 1	9°993318	51	29	9°240744	3 35	10°759256	9°247426	3 35	10°752574	10°006682
2	8	9°241101	4 47	10°758899	9°247794	4 47	10°752206	10°006693	4 2	9°993307	52	58	9°241101	4 47	10°758899	9°247794	4 47	10°752206	10°006693
20	10	9°241458	5 59	10°758542	9°248162	5 59	10°751838	10°006704	5 2	9°993296	50	30	9°241458	5 59	10°758542	9°248162	5 59	10°751838	10°006704
3	12	9°241814	6 71	10°758186	9°248530	6 71	10°751470	10°006716	6 2	9°993284	48	57	9°241814	6 71	10°758186	9°248530	6 71	10°751470	10°006716
30	14	9°242170	7 83	10°757830	9°248897	7 83	10°751103	10°006727	7 3	9°993273	46	30	9°242170	7 83	10°757830	9°248897	7 83	10°751103	10°006727
4	16	9°242526	8 94	10°757474	9°249264	8 94	10°750736	10°006738	8 3	9°993262	44	56	9°242526	8 94	10°757474	9°249264	8 94	10°750736	10°006738
20	18	9°242882	9 106	10°757118	9°249631	9 110	10°750369	10°006749	9 3	9°993251	42	30	9°242882	9 106	10°757118	9°249631	9 110	10°750369	10°006749
5	20	9°243237	10 118	10°756763	9°249998	10 122	10°750002	10°006760	10 4	9°993240	40	55	9°243237	10 118	10°756763	9°249998	10 122	10°750002	10°006760
30	22	9°243592	11 130	10°756403	9°250364	11 134	10°749636	10°006772	11 5	9°993228	38	30	9°243592	11 130	10°756403	9°250364	11 134	10°749636	10°006772
6	24	9°243947	12 141	10°756058	9°250730	12 146	10°749270	10°006783	12 5	9°993217	36	54	9°243947	12 141	10°756058	9°250730	12 146	10°749270	10°006783
30	26	9°244302	13 53	10°755698	9°251096	13 158	10°748904	10°006794	13 5	9°993206	34	30	9°244302	13 53	10°755698	9°251096	13 158	10°748904	10°006794
7	28	9°244656	14 155	10°755344	9°251461	14 170	10°748539	10°006805	14 5	9°993195	32	53	9°244656	14 155	10°755344	9°251461	14 170	10°748539	10°006805
30	30	9°245010	15 177	10°754990	9°251826	15 183	10°748174	10°006817	15 6	9°993183	30	30	9°245010	15 177	10°754990	9°251826	15 183	10°748174	10°006817
8	32	9°245363	16 189	10°754637	9°252191	16 195	10°747809	10°006828	16 6	9°993172	28	52	9°245363	16 189	10°754637	9°252191	16 195	10°747809	10°006828
30	34	9°245717	17 200	10°754283	9°252556	17 207	10°747444	10°006839	17 6	9°993161	26	30	9°245717	17 200	10°754283	9°252556	17 207	10°747444	10°006839
9	36	9°246069	18 212	10°753931	9°252920	18 219	10°747080	10°006851	18 7	9°993149	24	51	9°246069	18 212	10°753931	9°252920	18 219	10°747080	10°006851
30	38	9°246422	19 224	10°753578	9°253284	19 231	10°746716	10°006862	19 7	9°993138	22	30	9°246422	19 224	10°753578	9°253284	19 231	10°746716	10°006862
10	40	9°246775	20 236	10°753225	9°253648	20 243	10°746352	10°006873	20 8	9°993127	20	50	9°246775	20 236	10°753225	9°253648	20 243	10°746352	10°006873
30	42	9°247127	21 248	10°752873	9°254011	21 256	10°745989	10°006885	21 8	9°993115	18	30	9°247127	21 248	10°752873	9°254011	21 256	10°745989	10°006885
11	44	9°247478	22 259	10°752522	9°254374	22 268	10°745626	10°006896	22 8	9°993104	16	49	9°247478	22 259	10°752522	9°254374	22 268	10°745626	10°006896
30	46	9°247830	23 271	10°752170	9°254737	23 280	10°745263	10°006907	23 9	9°993093	14	30	9°247830	23 271	10°752170	9°254737	23 280	10°745263	10°006907
12	48	9°248181	24 283	10°751819	9°255100	24 292	10°744900	10°006919	24 9	9°993081	12	48	9°248181	24 283	10°751819	9°255100	24 292	10°744900	10°006919
30	50	9°248532	25 295	10°751468	9°255462	25 304	10°744538	10°006930	25 9	9°993070	10	30	9°248532	25 295	10°751468	9°255462	25 304	10°744538	10°006930
13	52	9°248883	26 307	10°751117	9°255824	26 316	10°744176	10°006941	26 10	9°993059	8	47	9°248883	26 307	10°751117	9°255824	26 316	10°744176	10°006941
30	54	9°249233	27 318	10°750767	9°256186	27 327	10°743814	10°006953	27 10	9°993047	6	30	9°249233	27 318	10°750767	9°256186	27 327	10°743814	10°006953
14	56	9°249583	28 330	10°750417	9°256547	28 341	10°743453	10°006964	28 11	9°993036	4	46	9°249583	28 330	10°750417	9°256547	28 341	10°743453	10°006964
30	58	9°249933	29 342	10°750066	9°256908	29 353	10°743092	10°006976	29 11	9°993024	2	30	9°249933	29 342	10°750066	9°256908	29 353	10°743092	10°006976
15	60	9°250282	30 354	10°749713	9°257269	30 365	10°742731	10°006987	30 11	9°993013	1	45	9°250282	30 354	10°749713	9°257269	30 365	10°742731	10°006987
30	62	9°250631	1°11	10°749369	9°257630	1 12	10°742370	10°006998	1 0	9°993002	38	30	9°250631	1°11	10°749369	9°257630	1 12	10°742370	10°006998
16	4	9°250980	2 23	10°749020	9°257990	2 24	10°742010	10°007010	2 1	9°992990	56	44	9°250980	2 23	10°749020	9°257990	2 24	10°742010	10°007010
30	6	9°251329	3 34	10°748671	9°258350	3 35	10°741650	10°007021	3 1	9°992979	54	30	9°251329	3 34	10°748671	9°258350	3 35	10°741650	10°007021
17	8	9°251677	4 46	10°748323	9°258710	4 48	10°741290	10°007033	4 2	9°992967	52	43	9°251677	4 46	10°748323	9°258710	4 48	10°741290	10°007033
30	10	9°252025	5 57	10°747975	9°259069	5 59	10°740931	10°007044	5 2	9°992956	50	30	9°252025	5 57	10°747975	9°259069	5 59	10°740931	10°007044
18	12	9°252373	6 69	10°747627	9°259429	6 71	10°740571	10°007056	6 2	9°992944	48	42	9°252373	6 69	10°747627	9°259429	6 71	10°740571	10°007056
30	14	9°252720	7 80	10°747280	9°259787	7 83	10°740213	10°007067	7 3	9°992933	46	30	9°252720	7 80	10°747280	9°259787	7 83	10°740213	10°007067
19	16	9°253067	8 92	10°746933	9°260146	8 95	10°739854	10°007079	8 3	9°992921	44	41	9°253067	8 92	10°746933	9°260146	8 95	10°739854	10°007079
30	18	9°253414	9 103	10°746586	9°260504	9 107	10°739496	10°007090	9 3	9°992910	42	30	9°253414	9 103	10°746586	9°260504	9 107	10°739496	10°007090
20	20	9°253761	10 115	10°746239	9°260863	10 119	10°739137	10°007102	10 4	9°992898	40	40	9°253761	10 115	10°746239	9°260863	10 119	10°739137	10°007102
30	22	9°254107	11 126	10°745893	9°261220	11 131	10°738780	10°007113	11 4	9°992887	38	30	9°254107	11 126	10°745893	9°261220	11 131	10°738780	10°007113
21	24	9°254453	12 138	10°745547	9°261578	12 143	10°738422	10°007125	12 5	9°992875	36	30	9°254453	12 138	10°745547	9°261578	12 143	10°738422	10°007125
30	26	9°254799	13 149	10°745201	9°261935	13 155	10°738065	10°007136	13 5	9°992864	34	30	9°254799	13 149	10°745201	9°261935	13 155	10°738065	10°007136
22	28	9°255144	14 161	10°744856	9°262292	14 167	10°737708	10°007148	14 5	9°992852	32	38	9°255144	14 161	10°744856	9°262292	14 167	10°737708	10°007148
30	30	9°255490	15 172	10°744510	9°262649	15 178	10°737351	10°007159	15 6	9°992841	30	30	9°255490	15 172	10°744510	9°262649	15 178	10°737351	10°007159
23	32	9°255834	16 184	10°744166	9°263005	16 190	10°736995	10°007171	16 6	9°992829	28	37	9°255834	16 184	10°744166	9°263005	16 190	10°736995	10°007171
30	34	9°256179	17 195	10°743821	9°263361	17 202	10°736639	10°007182	17 6	9°992818	26	30	9°256179	17 195	10°743821	9°263361	17 202	10°736639	10°007182
24	36	9°256523	18 207	10°743477	9°263717	18 214	10°736283	10°007194	18 7	9°992806	24	36	9°256523	18 207	10°743477	9°263717	18 214	10°736283	10°007194
30	38	9°256867	19 218	10°743133	9°264073	19 226	10°735927	10°007206	19 7	9°992794	22	30	9°256867	19 218	10°743133	9°264073	19 226	10°735927	10°007206
25	40	9°257211	20 230	10°742789	9°264428	20 238	10°735572	10°007217	20 8	9°992783	20	35	9°257211	20 230	10°742789	9°264428	20 238	10°735572	10°007217
30	42	9°257554	21 241	10°742446	9°264783	21 250	10°735217	10°007229	21 8	9°992771	18								

LOG. SINES, COSINES, &c.

0° 42'										10°									
°	'	m.	Sine	Parts	Secant	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	'	°	'	m.	Sine	Parts	Secant
30	0	0	9'260633		10'739367	9'267967		10'732033	10'007334		9'992666	30	0	30	0	0	9'992666		10'007334
30	1	1	9'260974	1" 11	10'739026	9'268319	1" 12	10'731681	10'007346	1" 0	9'992654	30	1	30	1	1	9'992654	1" 11	10'007346
31	1	2	9'261314	2 22	10'738686	9'268671	2 23	10'731329	10'007357	2 1	9'992643	31	1	29	2	2	9'992643	2 22	10'007357
31	2	3	9'261654	3 34	10'738346	9'269023	3 35	10'730977	10'007369	3 1	9'992631	31	2	30	3	3	9'992631	3 34	10'007369
32	2	4	9'261994	4 45	10'738006	9'269375	4 46	10'730625	10'007381	4 2	9'992619	32	2	28	4	4	9'992619	4 45	10'007381
32	3	5	9'262334	5 56	10'737666	9'269726	5 58	10'730274	10'007393	5 2	9'992607	32	3	29	5	5	9'992607	5 56	10'007393
33	3	6	9'262673	6 67	10'737327	9'270077	6 70	10'729923	10'007404	6 2	9'992596	33	3	27	6	6	9'992596	6 67	10'007404
33	4	7	9'263012	7 78	10'736988	9'270428	7 81	10'729572	10'007416	7 3	9'992584	33	4	28	7	7	9'992584	7 78	10'007416
34	4	8	9'263351	8 90	10'736649	9'270779	8 93	10'729221	10'007428	8 3	9'992572	34	4	26	8	8	9'992572	8 90	10'007428
34	5	9	9'263689	9 101	10'736311	9'271129	9 105	10'728871	10'007440	9 4	9'992560	34	5	27	9	9	9'992560	9 101	10'007440
35	5	10	9'264027	10 112	10'735973	9'271479	10 116	10'728521	10'007451	10 4	9'992549	35	5	25	10	10	9'992549	10 112	10'007451
35	6	11	9'264365	11 123	10'735635	9'271829	11 128	10'728171	10'007463	11 5	9'992537	35	6	26	11	11	9'992537	11 123	10'007463
36	6	12	9'264703	12 135	10'735297	9'272178	12 139	10'727822	10'007475	12 5	9'992525	36	6	24	12	12	9'992525	12 135	10'007475
36	7	13	9'265040	13 146	10'734960	9'272527	13 151	10'727473	10'007487	13 5	9'992513	36	7	25	13	13	9'992513	13 146	10'007487
37	7	14	9'265377	14 157	10'734623	9'272876	14 162	10'727124	10'007499	14 6	9'992501	37	7	23	14	14	9'992501	14 157	10'007499
37	8	15	9'265714	15 168	10'734286	9'273225	15 174	10'726775	10'007511	15 6	9'992489	37	8	20	15	15	9'992489	15 168	10'007511
38	8	16	9'266051	16 179	10'733949	9'273573	16 186	10'726427	10'007522	16 6	9'992478	38	8	22	16	16	9'992478	16 179	10'007522
38	9	17	9'266387	17 191	10'733613	9'273921	17 197	10'726079	10'007534	17 7	9'992466	38	9	21	17	17	9'992466	17 191	10'007534
39	9	18	9'266723	18 202	10'733277	9'274269	18 209	10'725731	10'007546	18 7	9'992454	39	9	20	18	18	9'992454	18 202	10'007546
39	10	19	9'267059	19 213	10'732941	9'274617	19 221	10'725383	10'007558	19 7	9'992442	39	10	19	19	19	9'992442	19 213	10'007558
40	10	20	9'267395	20 224	10'732605	9'274964	20 232	10'725036	10'007570	20 8	9'992430	40	10	18	20	20	9'992430	20 224	10'007570
40	11	21	9'267730	21 236	10'732270	9'275312	21 244	10'724688	10'007582	21 8	9'992418	40	11	17	21	21	9'992418	21 236	10'007582
41	11	22	9'268065	22 247	10'731935	9'275658	22 256	10'724342	10'007594	22 9	9'992406	41	11	16	22	22	9'992406	22 247	10'007594
41	12	23	9'268399	23 258	10'731601	9'276005	23 267	10'723995	10'007606	23 9	9'992394	41	12	15	23	23	9'992394	23 258	10'007606
42	12	24	9'268734	24 269	10'731266	9'276351	24 279	10'723649	10'007618	24 9	9'992382	42	12	14	24	24	9'992382	24 269	10'007618
42	13	25	9'269068	25 280	10'730932	9'276698	25 290	10'723302	10'007630	25 10	9'992370	42	13	13	25	25	9'992370	25 280	10'007630
43	13	26	9'269402	26 292	10'730598	9'277043	26 302	10'722957	10'007641	26 10	9'992359	43	13	12	26	26	9'992359	26 292	10'007641
43	14	27	9'269736	27 303	10'730264	9'277389	27 314	10'722611	10'007653	27 11	9'992347	43	14	11	27	27	9'992347	27 303	10'007653
44	14	28	9'270069	28 315	10'729931	9'277734	28 325	10'722266	10'007665	28 11	9'992335	44	14	10	28	28	9'992335	28 315	10'007665
44	15	29	9'270402	29 326	10'729598	9'278079	29 337	10'721921	10'007677	29 12	9'992323	44	15	9	29	29	9'992323	29 326	10'007677
45	15	30	9'270735	30 337	10'729265	9'278424	30 349	10'721575	10'007689	30 12	9'992311	45	15	8	30	30	9'992311	30 337	10'007689
45	16	31	9'271067	1 11	10'728933	9'278769	1 11	10'721231	10'007701	1 0	9'992299	45	16	7	31	31	9'992299	1 11	10'007701
46	16	32	9'271400	2 22	10'728600	9'279113	2 23	10'720887	10'007713	2 1	9'992287	46	16	6	32	32	9'992287	2 22	10'007713
46	17	33	9'271732	3 33	10'728268	9'279457	3 34	10'720543	10'007725	3 1	9'992275	46	17	5	33	33	9'992275	3 33	10'007725
47	17	34	9'272064	4 44	10'727936	9'279801	4 45	10'720209	10'007737	4 2	9'992263	47	17	4	34	34	9'992263	4 44	10'007737
47	18	35	9'272395	5 55	10'727605	9'280144	5 57	10'719856	10'007749	5 2	9'992251	47	18	3	35	35	9'992251	5 55	10'007749
48	18	36	9'272726	6 66	10'727274	9'280488	6 68	10'719512	10'007761	6 2	9'992239	48	18	2	36	36	9'992239	6 66	10'007761
48	19	37	9'273057	7 77	10'726943	9'280831	7 79	10'719169	10'007774	7 3	9'992226	48	19	1	37	37	9'992226	7 77	10'007774
49	19	38	9'273388	8 88	10'726612	9'281174	8 91	10'718826	10'007786	8 3	9'992214	49	19	0	38	38	9'992214	8 88	10'007786
49	20	39	9'273718	9 99	10'726281	9'281516	9 102	10'718484	10'007798	9 4	9'992202	49	20	0	39	39	9'992202	9 99	10'007798
50	20	40	9'274049	10 110	10'725951	9'281858	10 114	10'718142	10'007810	10 4	9'992190	50	20	0	40	40	9'992190	10 110	10'007810
50	21	41	9'274379	11 121	10'725621	9'282201	11 125	10'717799	10'007822	11 4	9'992178	50	21	0	41	41	9'992178	11 121	10'007822
51	21	42	9'274708	12 132	10'725292	9'282542	12 136	10'717458	10'007834	12 5	9'992166	51	21	0	42	42	9'992166	12 132	10'007834
51	22	43	9'275038	13 143	10'724962	9'282884	13 148	10'717116	10'007846	13 5	9'992154	51	22	0	43	43	9'992154	13 143	10'007846
52	22	44	9'275367	14 153	10'724633	9'283225	14 159	10'716775	10'007858	14 6	9'992142	52	22	0	44	44	9'992142	14 153	10'007858
52	23	45	9'275696	15 164	10'724304	9'283566	15 170	10'716434	10'007870	15 6	9'992130	52	23	0	45	45	9'992130	15 164	10'007870
53	23	46	9'276025	16 175	10'723975	9'283907	16 182	10'716093	10'007882	16 6	9'992118	53	23	0	46	46	9'992118	16 175	10'007882
53	24	47	9'276353	17 186	10'723647	9'284248	17 193	10'715752	10'007895	17 7	9'992105	53	24	0	47	47	9'992105	17 186	10'007895
54	24	48	9'276681	18 197	10'723319	9'284588	18 205	10'715412	10'007907	18 7	9'992093	54	24	0	48	48	9'992093	18 197	10'007907
54	25	49	9'277009	19 208	10'722991	9'284928	19 216	10'715072	10'007919	19 8	9'992081	54	25	0	49	49	9'992081	19 208	10'007919
55	25	50	9'277337	20 219	10'722663	9'285268	20 227	10'714732	10'007931	20 8	9'992069	55	25	0	50	50	9'992069	20 219	10'007931
55	26	51	9'277664	21 230	10'722336	9'285607	21 239	10'714393	10'007943	21 8	9'992057	55	26	0	51	51	9'992057	21 230	10'007943
56	26	52	9'277991	22 241	10'722009	9'285947	22 250	10'714053	10'007956	22 9	9'992044	56	26	0	52	52	9'992044	22 241	10'007956
56	27	53	9'278318	23 252	10'721682	9'286286	23 261	10'713714	10'007968	23 9	9'992032	56	27	0	53	53	9'992032	23 252	10'007968
57	27	54	9'278645	24 263	10'721355	9'286624	24 273	10'713376	10'007980	24 10	9'992020	57	27	0	54	54	9'992020	24 263	10'007980
57	28	55	9'278971	25 274	10'721029	9'286963	25 284	10'713037	10'007992	25 10	9'992008	57	28	0	55	55	9'992008	25 274	10'007992
58	28	56	9'279297	26 285	10'720703	9'287301	26 295	10'712699	10'008004	26 10	9'991996	58	28	0	56	56	9'991996	26 285	10'008004
58	29	57	9'279623	27 296	10'720377	9'287639	27 307	10'712361	10'008017	27 11	9'991983								

LOG. SINES, COSINES, &c.

0° 44'				11°							
m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	11°
0	9° 280399		10° 719401	9° 288652	10° 711348	10° 008053	9° 991947	10	9° 991947	10	60
1	9° 280924	17 11	10° 719076	9° 288989	10° 711011	10° 008066	9° 991934	10	9° 991934	10	59
2	9° 281448	2 21	10° 718752	9° 289326	10° 710674	10° 008078	9° 991921	10	9° 991921	10	58
3	9° 281973	3 33	10° 718427	9° 289663	10° 710337	10° 008090	9° 991910	10	9° 991910	10	57
4	9° 282497	4 43	10° 718103	9° 289999	10° 710001	10° 008103	9° 991897	10	9° 991897	10	56
5	9° 283022	5 53	10° 717780	9° 290335	10° 709665	10° 008115	9° 991885	10	9° 991885	10	55
6	9° 283546	6 64	10° 717456	9° 290671	10° 709329	10° 008127	9° 991873	10	9° 991873	10	54
7	9° 284071	7 75	10° 717133	9° 291007	10° 708993	10° 008140	9° 991860	10	9° 991860	10	53
8	9° 284595	8 86	10° 716810	9° 291342	10° 708658	10° 008152	9° 991848	10	9° 991848	10	52
9	9° 285120	9 96	10° 716487	9° 291678	10° 708322	10° 008164	9° 991836	10	9° 991836	10	51
10	9° 285644	10 107	10° 716164	9° 292013	10° 707987	10° 008177	9° 991823	10	9° 991823	10	50
11	9° 286168	11 118	10° 715842	9° 292347	10° 707653	10° 008189	9° 991811	10	9° 991811	10	49
12	9° 286693	12 128	10° 715520	9° 292682	10° 707318	10° 008201	9° 991799	10	9° 991799	10	48
13	9° 287217	13 139	10° 715198	9° 293016	10° 706984	10° 008214	9° 991788	10	9° 991788	10	47
14	9° 287742	14 150	10° 714876	9° 293350	10° 706650	10° 008226	9° 991776	10	9° 991776	10	46
15	9° 288266	15 160	10° 714555	9° 293684	10° 706316	10° 008239	9° 991764	10	9° 991764	10	45
16	9° 288791	16 171	10° 714234	9° 294017	10° 705983	10° 008251	9° 991752	10	9° 991752	10	44
17	9° 289315	17 182	10° 713913	9° 294351	10° 705649	10° 008264	9° 991740	10	9° 991740	10	43
18	9° 289840	18 193	10° 713592	9° 294684	10° 705316	10° 008276	9° 991728	10	9° 991728	10	42
19	9° 290364	19 203	10° 713272	9° 295016	10° 704984	10° 008288	9° 991716	10	9° 991716	10	41
20	9° 290889	20 214	10° 712953	9° 295349	10° 704651	10° 008301	9° 991704	10	9° 991704	10	40
21	9° 291413	21 225	10° 712632	9° 295681	10° 704317	10° 008313	9° 991692	10	9° 991692	10	39
22	9° 291938	22 235	10° 712312	9° 296013	10° 703987	10° 008326	9° 991680	10	9° 991680	10	38
23	9° 292462	23 246	10° 711993	9° 296345	10° 703655	10° 008338	9° 991668	10	9° 991668	10	37
24	9° 292987	24 257	10° 711674	9° 296677	10° 703323	10° 008351	9° 991656	10	9° 991656	10	36
25	9° 293511	25 267	10° 711355	9° 297009	10° 702992	10° 008363	9° 991644	10	9° 991644	10	35
26	9° 294036	26 278	10° 711036	9° 297339	10° 702661	10° 008376	9° 991632	10	9° 991632	10	34
27	9° 294560	27 289	10° 710718	9° 297670	10° 702330	10° 008388	9° 991620	10	9° 991620	10	33
28	9° 295085	28 300	10° 710400	9° 298001	10° 702000	10° 008401	9° 991608	10	9° 991608	10	32
29	9° 295609	29 310	10° 710082	9° 298332	10° 701668	10° 008414	9° 991596	10	9° 991596	10	31
30	9° 296134	30 321	10° 709764	9° 298662	10° 701338	10° 008426	9° 991584	10	9° 991584	10	30
31	9° 296658	1 10	10° 709447	9° 298992	10° 701008	10° 008439	9° 991572	10	9° 991572	10	29
32	9° 297183	2 21	10° 709130	9° 299322	10° 700678	10° 008451	9° 991560	10	9° 991560	10	28
33	9° 297707	3 31	10° 708813	9° 299651	10° 700349	10° 008464	9° 991548	10	9° 991548	10	27
34	9° 298232	4 42	10° 708496	9° 300000	10° 700020	10° 008476	9° 991536	10	9° 991536	10	26
35	9° 298756	5 52	10° 708180	9° 300309	10° 699691	10° 008489	9° 991524	10	9° 991524	10	25
36	9° 299281	6 63	10° 707863	9° 300638	10° 699362	10° 008502	9° 991512	10	9° 991512	10	24
37	9° 299805	7 73	10° 707547	9° 300967	10° 699033	10° 008514	9° 991500	10	9° 991500	10	23
38	9° 300330	8 84	10° 707232	9° 301295	10° 698705	10° 008527	9° 991488	10	9° 991488	10	22
39	9° 300854	9 94	10° 706916	9° 301624	10° 698376	10° 008539	9° 991476	10	9° 991476	10	21
40	9° 301379	10 105	10° 706601	9° 301951	10° 698049	10° 008552	9° 991464	10	9° 991464	10	20
41	9° 301903	11 115	10° 706286	9° 302279	10° 697721	10° 008565	9° 991452	10	9° 991452	10	19
42	9° 302428	12 126	10° 705971	9° 302607	10° 697393	10° 008578	9° 991440	10	9° 991440	10	18
43	9° 302952	13 136	10° 705656	9° 302934	10° 697066	10° 008590	9° 991428	10	9° 991428	10	17
44	9° 303477	14 147	10° 705342	9° 303261	10° 696739	10° 008603	9° 991416	10	9° 991416	10	16
45	9° 304001	15 157	10° 705028	9° 303588	10° 696412	10° 008616	9° 991404	10	9° 991404	10	15
46	9° 304526	16 168	10° 704714	9° 303914	10° 696086	10° 008628	9° 991392	10	9° 991392	10	14
47	9° 305050	17 178	10° 704400	9° 304241	10° 695759	10° 008641	9° 991380	10	9° 991380	10	13
48	9° 305575	18 188	10° 704087	9° 304567	10° 695433	10° 008654	9° 991368	10	9° 991368	10	12
49	9° 306099	19 199	10° 703774	9° 304893	10° 695107	10° 008667	9° 991356	10	9° 991356	10	11
50	9° 306624	20 209	10° 703461	9° 305218	10° 694782	10° 008679	9° 991344	10	9° 991344	10	10
51	9° 307148	21 220	10° 703148	9° 305544	10° 694456	10° 008692	9° 991332	10	9° 991332	10	9
52	9° 307673	22 230	10° 702835	9° 305869	10° 694131	10° 008705	9° 991320	10	9° 991320	10	8
53	9° 308197	23 241	10° 702522	9° 306194	10° 693806	10° 008718	9° 991308	10	9° 991308	10	7
54	9° 308722	24 251	10° 702210	9° 306519	10° 693481	10° 008730	9° 991296	10	9° 991296	10	6
55	9° 309246	25 262	10° 701898	9° 306843	10° 693157	10° 008743	9° 991284	10	9° 991284	10	5
56	9° 309771	26 272	10° 701588	9° 307168	10° 692832	10° 008756	9° 991272	10	9° 991272	10	4
57	9° 310295	27 283	10° 701277	9° 307492	10° 692508	10° 008769	9° 991260	10	9° 991260	10	3
58	9° 310820	28 293	10° 700966	9° 307816	10° 692184	10° 008782	9° 991248	10	9° 991248	10	2
59	9° 311344	29 304	10° 700655	9° 308139	10° 691861	10° 008794	9° 991236	10	9° 991236	10	1
60	9° 311869	30 314	10° 700343	9° 308463	10° 691537	10° 008807	9° 991224	10	9° 991224	10	0
m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	11°

LOG. SINES. COSINES, &c.

0° 46'				11°									
°	'	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	'
30	0	0	9°299655		10°700345	9°308463		10°691537	10°008807		9°991193	10	30
30	1	1	9°299666	1" 10	10°700034	9°308786	1" 11	10°691214	10°008820	1" 0	9°991180	58	30
31	4	4	9°300276	2 21	10°699724	9°309109	2 21	10°690891	10°008833	2 1	9°991167	56	20
31	6	6	9°300586	3 31	10°699414	9°309432	3 32	10°690568	10°008846	3 1	9°991154	54	30
32	8	8	9°300895	4 41	10°699105	9°309754	4 43	10°690246	10°008859	4 2	9°991141	52	28
32	10	10	9°301205	5 51	10°698795	9°310076	5 53	10°689924	10°008872	5 2	9°991128	50	30
33	12	12	9°301514	6 61	10°698486	9°310399	6 64	10°689601	10°008885	6 3	9°991115	48	27
33	14	14	9°301823	7 71	10°698177	9°310720	7 75	10°689280	10°008897	7 3	9°991103	46	30
34	16	16	9°302132	8 82	10°697868	9°311042	8 85	10°688958	10°008910	8 3	9°991090	44	26
34	18	18	9°302440	9 92	10°697560	9°311364	9 96	10°688636	10°008923	9 4	9°991077	42	30
35	20	20	9°302748	10 102	10°697252	9°311685	10 107	10°688315	10°008936	10 4	9°991064	40	26
35	22	22	9°303057	11 113	10°696943	9°312006	11 117	10°687994	10°008949	11 5	9°991051	38	30
36	24	24	9°303364	12 123	10°696636	9°312327	12 128	10°687673	10°008962	12 5	9°991038	36	24
36	26	26	9°303672	13 133	10°696328	9°312647	13 139	10°687353	10°008975	13 6	9°991025	34	30
37	28	28	9°303979	14 143	10°696021	9°312968	14 149	10°687032	10°008988	14 6	9°991012	32	23
37	30	30	9°304287	15 153	10°695713	9°313288	15 160	10°686712	10°009001	15 6	9°990999	30	30
38	32	32	9°304593	16 164	10°695407	9°313608	16 171	10°686392	10°009014	16 7	9°990986	28	22
38	34	34	9°304900	17 174	10°695100	9°313927	17 181	10°686073	10°009027	17 7	9°990973	26	30
39	36	36	9°305207	18 184	10°694793	9°314247	18 192	10°685753	10°009040	18 8	9°990960	24	21
39	38	38	9°305513	19 194	10°694487	9°314566	19 203	10°685434	10°009053	19 8	9°990947	22	30
40	40	40	9°305819	20 205	10°694181	9°314885	20 213	10°685115	10°009066	20 9	9°990934	20	20
40	42	42	9°306125	21 215	10°693875	9°315204	21 224	10°684796	10°009079	21 9	9°990921	18	30
41	44	44	9°306430	22 225	10°693570	9°315523	22 235	10°684477	10°009092	22 10	9°990908	16	19
41	46	46	9°306736	23 235	10°693264	9°315841	23 245	10°684159	10°009105	23 10	9°990895	14	30
42	48	48	9°307041	24 245	10°692959	9°316159	24 256	10°683841	10°009118	24 10	9°990882	12	18
42	50	50	9°307346	25 256	10°692654	9°316477	25 267	10°683523	10°009132	25 11	9°990868	10	30
43	52	52	9°307650	26 266	10°692350	9°316795	26 277	10°683205	10°009145	26 11	9°990855	8	17
43	54	54	9°307955	27 276	10°692045	9°317113	27 288	10°682887	10°009158	27 12	9°990842	6	30
44	56	56	9°308259	28 286	10°691741	9°317430	28 299	10°682570	10°009171	28 12	9°990829	4	16
44	58	58	9°308563	29 297	10°691437	9°317747	29 309	10°682253	10°009184	29 13	9°990816	2	30
45	60	60	9°308867	30 307	10°691133	9°318064	30 320	10°681936	10°009197	30 13	9°990803	0	15
45	62	62	9°309170	1 10	10°690830	9°318381	1 10	10°681619	10°009210	1 0	9°990790	58	30
46	4	4	9°309474	2 20	10°690526	9°318697	2 21	10°681303	10°009223	2 1	9°990777	56	14
46	6	6	9°309777	3 30	10°690223	9°319013	3 31	10°680987	10°009237	3 1	9°990763	54	30
47	8	8	9°310080	4 40	10°689920	9°319330	4 42	10°680670	10°009250	4 2	9°990750	52	13
47	10	10	9°310382	5 50	10°689618	9°319645	5 52	10°680355	10°009263	5 2	9°990737	50	30
48	12	12	9°310685	6 60	10°689315	9°319961	6 63	10°680039	10°009276	6 3	9°990724	48	12
48	14	14	9°310987	7 70	10°689013	9°320277	7 73	10°679723	10°009289	7 3	9°990711	46	30
49	16	16	9°311289	8 80	10°688711	9°320592	8 84	10°679408	10°009303	8 4	9°990697	44	11
49	18	18	9°311591	9 90	10°688409	9°320907	9 94	10°679093	10°009316	9 4	9°990684	42	30
50	20	20	9°311893	10 100	10°688107	9°321222	10 104	10°678778	10°009329	10 4	9°990671	40	10
50	22	22	9°312194	11 110	10°687806	9°321536	11 115	10°678464	10°009342	11 5	9°990658	38	30
51	24	24	9°312495	12 120	10°687505	9°321851	12 125	10°678149	10°009355	12 5	9°990645	36	9
51	26	26	9°312796	13 130	10°687204	9°322165	13 136	10°677835	10°009369	13 6	9°990631	34	30
52	28	28	9°313097	14 140	10°686903	9°322479	14 146	10°677521	10°009382	14 6	9°990618	32	8
52	30	30	9°313397	15 150	10°686603	9°322793	15 157	10°677207	10°009395	15 7	9°990605	30	30
53	32	32	9°313698	16 160	10°686302	9°323106	16 167	10°676894	10°009409	16 7	9°990591	28	7
53	34	34	9°313998	17 170	10°686002	9°323420	17 178	10°676580	10°009422	17 8	9°990578	26	30
54	36	36	9°314297	18 180	10°685703	9°323733	18 188	10°676267	10°009435	18 8	9°990565	24	6
54	38	38	9°314597	19 190	10°685403	9°324046	19 199	10°675954	10°009449	19 8	9°990552	22	30
55	40	40	9°314897	20 200	10°685103	9°324358	20 209	10°675642	10°009462	20 9	9°990538	20	5
55	42	42	9°315196	21 210	10°684804	9°324671	21 219	10°675329	10°009475	21 9	9°990525	18	30
56	44	44	9°315495	22 220	10°684505	9°324983	22 230	10°675017	10°009489	22 10	9°990511	16	4
56	46	46	9°315793	23 230	10°684207	9°325295	23 240	10°674705	10°009502	23 10	9°990498	14	30
57	48	48	9°316092	24 240	10°683908	9°325607	24 251	10°674393	10°009515	24 11	9°990485	12	3
57	50	50	9°316390	25 250	10°683610	9°325919	25 261	10°674081	10°009529	25 11	9°990471	10	30
58	52	52	9°316689	26 260	10°683311	9°326231	26 272	10°673769	10°009542	26 12	9°990458	8	2
58	54	54	9°316986	27 270	10°683014	9°326542	27 282	10°673458	10°009555	27 12	9°990445	6	30
59	56	56	9°317284	28 280	10°682716	9°326853	28 293	10°673147	10°009569	28 12	9°990431	4	1
59	58	58	9°317582	29 290	10°682418	9°327164	29 303	10°672836	10°009582	29 13	9°990418	2	30
60	60	60	9°317879	30 300	10°682121	9°327475	30 313	10°672525	10°009596	30 13	9°990404	0	0
°	'	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	'

78°

51 12'

LOG. SINES, COSINES, &c.

0° 48"										12°									
°	'	Secant	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cotang.	Secant	Parts	Cotang.	Sine	Parts	Cotang.	Secant	Parts
0	0	9'317879			10'682121	9'327475			10'672525	10'009596			1'0	9'990404	2.2	68			
1	0	9'318176	1"	10	10'681824	9'327785	1"	10	10'672215	10'009609	1"	10	1'0	9'990391	36	30			
2	0	9'318473	2	20	10'681527	9'328095	2	20	10'671905	10'009622	2	20	2	9'990378	56	50			
3	0	9'318769	3	30	10'681231	9'328405	3	30	10'671595	10'009636	3	30	3	9'990364	64	30			
4	0	9'319066	4	40	10'680934	9'328715	4	40	10'671285	10'009649	4	40	4	9'990351	32	58			
5	0	9'319362	5	50	10'680638	9'329025	5	50	10'670975	10'009663	5	50	5	9'990337	30	20			
6	0	9'319658	6	60	10'680342	9'329334	6	60	10'670666	10'009676	6	60	6	9'990324	48	57			
7	0	9'319954	7	70	10'680046	9'329644	7	70	10'670356	10'009690	7	70	7	9'990310	44	56			
8	0	9'320249	8	80	10'679751	9'329953	8	80	10'670047	10'009703	8	80	8	9'990297	42	20			
9	0	9'320545	9	90	10'679455	9'330262	9	90	10'669738	10'009717	9	90	9	9'990283	40	55			
10	0	9'320840	10	100	10'679160	9'330570	10	100	10'669430	10'009730	10	100	10	9'990270	38	20			
11	0	9'321135	11	110	10'678865	9'330879	11	110	10'669121	10'009744	11	110	11	9'990256	36	30			
12	0	9'321430	12	120	10'678570	9'331187	12	120	10'668813	10'009757	12	120	12	9'990243	34	54			
13	0	9'321724	13	130	10'678276	9'331495	13	130	10'668505	10'009771	13	130	13	9'990229	32	30			
14	0	9'322019	14	140	10'677981	9'331803	14	140	10'668197	10'009785	14	140	14	9'990215	30	53			
15	0	9'322313	15	150	10'677687	9'332111	15	150	10'667889	10'009798	15	150	15	9'990202	28	20			
16	0	9'322607	16	160	10'677393	9'332418	16	160	10'667582	10'009812	16	160	16	9'990188	26	52			
17	0	9'322900	17	170	10'677100	9'332726	17	170	10'667274	10'009825	17	170	17	9'990175	24	30			
18	0	9'323194	18	180	10'676806	9'333033	18	180	10'666967	10'009839	18	180	18	9'990161	22	51			
19	0	9'323487	19	190	10'676513	9'333340	19	190	10'666660	10'009852	19	190	19	9'990148	20	20			
20	0	9'323780	20	200	10'676220	9'333646	20	200	10'666354	10'009866	20	200	20	9'990134	18	50			
21	0	9'324073	21	210	10'675927	9'333953	21	210	10'666047	10'009880	21	210	21	9'990120	16	30			
22	0	9'324366	22	220	10'675634	9'334259	22	220	10'665741	10'009893	22	220	22	9'990107	14	49			
23	0	9'324658	23	230	10'675342	9'334565	23	230	10'665435	10'009907	23	230	23	9'990093	12	48			
24	0	9'324950	24	240	10'675050	9'334871	24	240	10'665129	10'009921	24	240	24	9'990079	10	20			
25	0	9'325243	25	250	10'674757	9'335177	25	250	10'664823	10'009934	25	250	25	9'990066	8	47			
26	0	9'325534	26	260	10'674466	9'335482	26	260	10'664518	10'009948	26	260	26	9'990052	6	30			
27	0	9'325826	27	270	10'674174	9'335788	27	270	10'664212	10'009962	27	270	27	9'990038	4	46			
28	0	9'326117	28	280	10'673883	9'336093	28	280	10'663907	10'009975	28	280	28	9'990025	2	20			
29	0	9'326409	29	290	10'673591	9'336398	29	290	10'663602	10'009989	29	290	29	9'990011	0	30			
30	0	9'326700	30	300	10'673300	9'336702	30	300	10'663298	10'010003	30	300	30	9'989997	2.2	45			
31	0	9'326991	1	10	10'673009	9'337007	1	10	10'662993	10'010016	1	10	1	9'989984	30	20			
32	0	9'327281	2	20	10'672719	9'337311	2	20	10'662689	10'010030	2	20	2	9'989970	36	44			
33	0	9'327572	3	30	10'672428	9'337615	3	30	10'662385	10'010044	3	30	3	9'989956	54	30			
34	0	9'327862	4	40	10'672138	9'337919	4	40	10'662081	10'010058	4	40	4	9'989942	32	43			
35	0	9'328152	5	50	10'671848	9'338223	5	50	10'661777	10'010071	5	50	5	9'989929	30	20			
36	0	9'328442	6	60	10'671558	9'338527	6	60	10'661473	10'010085	6	60	6	9'989915	48	43			
37	0	9'328731	7	70	10'671269	9'338830	7	70	10'661170	10'010099	7	70	7	9'989901	46	30			
38	0	9'329021	8	80	10'670979	9'339133	8	80	10'660867	10'010113	8	80	8	9'989887	44	41			
39	0	9'329310	9	90	10'670690	9'339436	9	90	10'660564	10'010127	9	90	9	9'989873	42	30			
40	0	9'329599	10	100	10'670401	9'339739	10	100	10'660261	10'010140	10	100	10	9'989860	40	40			
41	0	9'329888	11	110	10'670112	9'340042	11	110	10'659958	10'010154	11	110	11	9'989846	38	30			
42	0	9'330176	12	120	10'669824	9'340344	12	120	10'659656	10'010168	12	120	12	9'989832	36	30			
43	0	9'330465	13	130	10'669535	9'340646	13	130	10'659354	10'010182	13	130	13	9'989818	34	30			
44	0	9'330753	14	140	10'669247	9'340948	14	140	10'659052	10'010196	14	140	14	9'989804	32	30			
45	0	9'331041	15	150	10'668959	9'341250	15	150	10'658750	10'010210	15	150	15	9'989790	30	20			
46	0	9'331320	16	160	10'668671	9'341552	16	160	10'658448	10'010223	16	160	16	9'989777	28	37			
47	0	9'331616	17	170	10'668384	9'341853	17	170	10'658147	10'010237	17	170	17	9'989763	26	30			
48	0	9'331903	18	180	10'668097	9'342155	18	180	10'657845	10'010251	18	180	18	9'989749	24	36			
49	0	9'332191	19	190	10'667809	9'342456	19	190	10'657544	10'010265	19	190	19	9'989735	22	30			
50	0	9'332478	20	200	10'667522	9'342757	20	200	10'657243	10'010279	20	200	20	9'989721	20	20			
51	0	9'332764	21	210	10'667236	9'343057	21	210	10'656943	10'010293	21	210	21	9'989707	18	30			
52	0	9'333051	22	220	10'666949	9'343358	22	220	10'656642	10'010307	22	220	22	9'989693	16	34			
53	0	9'333337	23	230	10'666661	9'343658	23	230	10'656342	10'010321	23	230	23	9'989679	14	30			
54	0	9'333624	24	240	10'666376	9'343958	24	240	10'656042	10'010335	24	240	24	9'989665	12	38			
55	0	9'333910	25	250	10'666090	9'344258	25	250	10'655742	10'010349	25	250	25	9'989651	10	30			
56	0	9'334195	26	260	10'665805	9'344558	26	260	10'655442	10'010363	26	260	26	9'989637	8	32			
57	0	9'334481	27	270	10'665519	9'344858	27	270	10'655142	10'010377	27	270	27	9'989623	6	30			
58	0	9'334767	28	280	10'665233	9'345157	28	280	10'654843	10'010390	28	280	28	9'989610	4	31			
59	0	9'335052	29	290	10'664948	9'345456	29	290	10'654544	10'010404	29	290	29	9'989596	2	30			
60	0	9'335337	30	300	10'664663	9'345755	30	300	10'654245	10'010418	30	300	30	9'989582	0	30			
°	'	Cotang.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Cosec.	Parts	Tangent	Cotang.	Parts	Sine	Parts	Cotang.	Cosec.	Parts	Sine

LOG. SINES, COSINES, &c.

LOG. SINES, COSINES, &c.													
0° 50'm				12°									
°	'	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	'
30	0	9	335337		10664663	9'348'755		10'654'245	10'010'418		9'989'582	10	30
30	2	9	335622	1	10664378	9'346'054	1"	10'653'946	10'010'432	1"	9'989'568	58	30
31	4	9	335906	2	10664094	9'346'353	2	10'653'647	10'010'447	2	9'989'553	36	29
30	6	9	336191	3	10663809	9'346'651	3	10'653'349	10'010'461	3	9'989'539	31	30
32	8	9	336475	4	10663525	9'346'949	4	10'653'051	10'010'475	4	9'989'525	32	28
30	10	9	336759	5	10663241	9'347'248	5	10'652'752	10'010'489	5	9'989'511	50	30
33	12	9	337043	6	10662957	9'347'545	6	10'652'455	10'010'503	6	9'989'497	44	27
30	14	9	337326	7	10662674	9'347'843	7	10'652'157	10'010'517	7	9'989'483	40	30
34	16	9	337610	8	10662390	9'348'141	8	10'651'859	10'010'531	8	9'989'469	44	26
30	18	9	337893	9	10662107	9'348'438	9	10'651'562	10'010'545	9	9'989'455	42	30
35	20	9	338176	10	10661824	9'348'735	10	10'651'265	10'010'559	10	9'989'441	40	26
30	22	9	338459	11	10661541	9'349'032	11	10'650'968	10'010'573	11	9'989'427	38	30
36	24	9	338742	12	10661258	9'349'329	12	10'650'671	10'010'587	12	9'989'413	36	24
30	26	9	339024	13	10660976	9'349'626	13	10'650'374	10'010'601	13	9'989'399	34	30
37	28	9	339307	14	10660693	9'349'922	14	10'650'078	10'010'615	14	9'989'385	32	23
30	30	9	339589	15	10660411	9'350'218	15	10'649'782	10'010'630	15	9'989'370	30	30
38	32	9	339871	16	10660129	9'350'514	16	10'649'486	10'010'644	16	9'989'356	28	22
30	34	9	340152	17	10659848	9'350'810	17	10'649'190	10'010'658	17	9'989'342	26	30
39	36	9	340434	18	10659566	9'351'106	18	10'648'894	10'010'672	18	9'989'328	24	21
30	38	9	340715	19	10659285	9'351'401	19	10'648'599	10'010'686	19	9'989'314	22	30
40	40	9	340996	20	10659004	9'351'697	20	10'648'303	10'010'700	20	9'989'300	20	20
30	42	9	341277	21	10658723	9'351'992	21	10'648'008	10'010'715	21	9'989'285	18	30
41	44	9	341558	22	10658442	9'352'287	22	10'647'713	10'010'729	22	9'989'271	16	19
30	46	9	341839	23	10658161	9'352'582	23	10'647'418	10'010'743	23	9'989'257	14	30
42	48	9	342119	24	10657881	9'352'876	24	10'647'124	10'010'757	24	9'989'243	12	18
30	50	9	342399	25	10657601	9'353'171	25	10'646'829	10'010'772	25	9'989'228	10	30
43	52	9	342679	26	10657321	9'353'465	26	10'646'535	10'010'786	26	9'989'214	8	17
30	54	9	342959	27	10657041	9'353'759	27	10'646'241	10'010'800	27	9'989'200	6	30
44	56	9	343239	28	10656761	9'354'053	28	10'645'947	10'010'814	28	9'989'186	4	16
30	58	9	343518	29	10656482	9'354'347	29	10'645'653	10'010'828	29	9'989'171	2	30
45	60	9	343797	30	10656203	9'354'640	30	10'645'360	10'010'843	30	9'989'157	0	15
30	2	9	344076	1	10655924	9'354'934	1	10'645'066	10'010'857	1	9'989'143	58	30
46	4	9	344355	2	10655645	9'355'227	2	10'644'773	10'010'872	2	9'989'128	56	14
30	6	9	344634	3	10655366	9'355'520	3	10'644'480	10'010'886	3	9'989'114	54	30
47	8	9	344912	4	10655088	9'355'813	4	10'644'187	10'010'900	4	9'989'100	52	13
30	10	9	345191	5	10654809	9'356'105	5	10'643'895	10'010'915	5	9'989'085	50	30
48	12	9	345469	6	10654531	9'356'398	6	10'643'602	10'010'929	6	9'989'071	48	12
30	14	9	345747	7	10654253	9'356'690	7	10'643'310	10'010'943	7	9'989'057	46	30
49	16	9	346024	8	10653976	9'356'982	8	10'643'018	10'010'958	8	9'989'042	44	11
30	18	9	346302	9	10653698	9'357'274	9	10'642'726	10'010'972	9	9'989'028	42	30
50	20	9	346579	10	10653421	9'357'566	10	10'642'434	10'010'986	10	9'989'014	40	10
30	22	9	346857	11	10653143	9'357'857	11	10'642'143	10'011'001	11	9'988'999	38	30
51	24	9	347134	12	10652866	9'358'149	12	10'641'851	10'011'015	12	9'988'985	36	9
30	26	9	347410	13	10652590	9'358'440	13	10'641'560	10'011'030	13	9'988'970	34	30
52	28	9	347687	14	10652313	9'358'731	14	10'641'269	10'011'044	14	9'988'956	32	8
30	30	9	347963	15	10652037	9'359'022	15	10'640'978	10'011'058	15	9'988'942	30	30
53	32	9	348240	16	10651760	9'359'313	16	10'640'687	10'011'073	16	9'988'927	28	7
30	34	9	348516	17	10651484	9'359'603	17	10'640'397	10'011'087	17	9'988'913	26	30
54	36	9	348792	18	10651208	9'359'893	18	10'640'107	10'011'102	18	9'988'898	24	6
30	38	9	349067	19	10650933	9'360'184	19	10'639'816	10'011'116	19	9'988'884	22	30
55	40	9	349343	20	10650657	9'360'474	20	10'639'526	10'011'131	20	9'988'869	20	5
30	42	9	349618	21	10650382	9'360'763	21	10'639'237	10'011'145	21	9'988'855	18	30
56	44	9	349893	22	10650107	9'361'053	22	10'638'947	10'011'160	22	9'988'840	16	4
30	46	9	350168	23	10649832	9'361'343	23	10'638'657	10'011'174	23	9'988'826	14	30
57	48	9	350443	24	10649557	9'361'632	24	10'638'368	10'011'189	24	9'988'811	12	30
30	50	9	350718	25	10649282	9'361'921	25	10'638'079	10'011'203	25	9'988'797	10	30
58	52	9	350992	26	10649008	9'362'210	26	10'637'790	10'011'218	26	9'988'782	8	2
30	54	9	351266	27	10648734	9'362'499	27	10'637'501	10'011'232	27	9'988'768	6	30
59	56	9	351540	28	10648460	9'362'787	28	10'637'213	10'011'247	28	9'988'753	4	1
30	58	9	351814	29	10648186	9'363'076	29	10'636'924	10'011'261	29	9'988'739	2	30
60	60	9	352088	30	10647912	9'363'364	30	10'636'636	10'011'276	30	9'988'724	0	0
°	'	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	'

77°

5h 8m

LOG. SINES, COSINES, &c.

0° 52'		13°											
<i>m</i>	<i>sec</i>	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	<i>m</i>	<i>sec</i>	<i>m</i>
0	0	9°352083		10°647912	9°363364		10°636636	10°011276		9°988524	8	00	
1	1	9°352162	1" 9	10°647838	9°363522	1" 10	10°636348	10°011291	1" 0	9°988709	30	20	50
2	2	9°352240	2 18	10°647765	9°363680	2 19	10°636030	10°011305	2 1	9°988895	50	40	50
3	3	9°352318	3 27	10°647692	9°363838	3 29	10°635712	10°011320	3 1	9°989080	51	20	
4	4	9°352396	4 36	10°647619	9°363995	4 38	10°635485	10°011334	4 2	9°989266	52	58	
5	5	9°352474	5 45	10°647546	9°364153	5 48	10°635197	10°011349	5 3	9°989451	53	20	
6	6	9°352552	6 54	10°647474	9°364310	6 57	10°634910	10°011364	6 4	9°989636	54	57	
7	7	9°352630	7 63	10°647401	9°364468	7 67	10°634623	10°011378	7 5	9°989821	55	20	
8	8	9°352708	8 72	10°647329	9°364626	8 76	10°634336	10°011393	8 6	9°990007	56	56	
9	9	9°352786	9 81	10°647256	9°364784	9 86	10°634049	10°011408	9 7	9°990192	57	20	
10	10	9°352864	10 90	10°647185	9°364942	10 95	10°633763	10°011422	10 8	9°990378	58	55	
11	11	9°352942	11 99	10°647113	9°365100	11 105	10°633476	10°011437	11 9	9°990563	59	20	
12	12	9°353020	12 108	10°647042	9°365258	12 114	10°633190	10°011451	12 10	9°990749	60	54	
13	13	9°353098	13 117	10°646970	9°365416	13 124	10°632904	10°011466	13 11	9°990934	61	20	
14	14	9°353176	14 126	10°646899	9°365574	14 133	10°632618	10°011481	14 12	9°991120	62	53	
15	15	9°353254	15 135	10°646828	9°365732	15 143	10°632332	10°011496	15 13	9°991305	63	20	
16	16	9°353332	16 144	10°646757	9°365890	16 152	10°632047	10°011511	16 14	9°991491	64	52	
17	17	9°353410	17 153	10°646686	9°366048	17 162	10°631761	10°011525	17 15	9°991676	65	20	
18	18	9°353488	18 162	10°646615	9°366206	18 171	10°631476	10°011540	18 16	9°991862	66	51	
19	19	9°353566	19 171	10°646544	9°366364	19 181	10°631191	10°011555	19 17	9°992047	67	20	
20	20	9°353644	20 181	10°646473	9°366522	20 190	10°630906	10°011570	20 18	9°992233	68	50	
21	21	9°353722	21 190	10°646402	9°366680	21 200	10°630622	10°011584	21 19	9°992418	69	20	
22	22	9°353800	22 199	10°646331	9°366838	22 209	10°630337	10°011599	22 20	9°992604	70	49	
23	23	9°353878	23 208	10°646260	9°366996	23 219	10°630053	10°011614	23 21	9°992789	71	20	
24	24	9°353956	24 217	10°646189	9°367154	24 228	10°629768	10°011629	24 22	9°992975	72	48	
25	25	9°354034	25 226	10°646118	9°367312	25 238	10°629484	10°011644	25 23	9°993160	73	20	
26	26	9°354112	26 235	10°646047	9°367470	26 248	10°629201	10°011658	26 24	9°993346	74	47	
27	27	9°354190	27 244	10°645976	9°367628	27 257	10°628917	10°011673	27 25	9°993531	75	20	
28	28	9°354268	28 253	10°645905	9°367786	28 267	10°628633	10°011688	28 26	9°993717	76	46	
29	29	9°354346	29 262	10°645834	9°367944	29 276	10°628350	10°011703	29 27	9°993902	77	20	
30	30	9°354424	30 271	10°645763	9°368102	30 286	10°628067	10°011718	30 28	9°994088	78	45	
31	31	9°354502	1 9	10°639516	9°372216	1 10	10°627784	10°011733	1 9	9°994273	79	20	
32	32	9°354580	2 18	10°639248	9°372499	2 19	10°627501	10°011748	2 10	9°994459	80	44	
33	33	9°354658	3 26	10°638981	9°372782	3 28	10°627218	10°011763	3 11	9°994644	81	20	
34	34	9°354736	4 35	10°638713	9°373064	4 37	10°626935	10°011777	4 12	9°994830	82	43	
35	35	9°354814	5 44	10°638446	9°373347	5 47	10°626653	10°011792	5 13	9°995015	83	20	
36	36	9°354892	6 53	10°638178	9°373629	6 56	10°626371	10°011807	6 14	9°995201	84	42	
37	37	9°354970	7 62	10°637911	9°373911	7 65	10°626089	10°011822	7 15	9°995386	85	20	
38	38	9°355048	8 70	10°637644	9°374193	8 75	10°625807	10°011837	8 16	9°995572	86	41	
39	39	9°355126	9 79	10°637377	9°374475	9 84	10°625525	10°011852	9 17	9°995757	87	20	
40	40	9°355204	10 88	10°637111	9°374756	10 93	10°625244	10°011867	10 18	9°995943	88	40	
41	41	9°355282	11 97	10°636844	9°375038	11 103	10°624962	10°011882	11 19	9°996128	89	20	
42	42	9°355360	12 106	10°636578	9°375319	12 112	10°624681	10°011897	12 20	9°996314	90	39	
43	43	9°355438	13 115	10°636312	9°375600	13 121	10°624400	10°011912	13 21	9°996500	91	20	
44	44	9°355516	14 124	10°636046	9°375881	14 131	10°624119	10°011927	14 22	9°996685	92	38	
45	45	9°355594	15 133	10°635780	9°376162	15 140	10°623838	10°011942	15 23	9°996871	93	20	
46	46	9°355672	16 142	10°635515	9°376442	16 150	10°623558	10°011957	16 24	9°997056	94	37	
47	47	9°355750	17 151	10°635249	9°376723	17 158	10°623277	10°011972	17 25	9°997242	95	20	
48	48	9°355828	18 159	10°634984	9°377003	18 168	10°622997	10°011987	18 26	9°997427	96	36	
49	49	9°355906	19 168	10°634719	9°377283	19 178	10°622717	10°012002	19 27	9°997613	97	20	
50	50	9°355984	20 177	10°634454	9°377563	20 187	10°622437	10°012017	20 28	9°997798	98	35	
51	51	9°356062	21 186	10°634190	9°377843	21 196	10°622157	10°012032	21 29	9°997984	99	20	
52	52	9°356140	22 195	10°633925	9°378122	22 206	10°621877	10°012047	22 30	9°998169	100	34	
53	53	9°356218	23 203	10°633661	9°378402	23 215	10°621598	10°012063	23 31	9°998355	101	20	
54	54	9°356296	24 212	10°633396	9°378681	24 224	10°621319	10°012078	24 32	9°998540	102	33	
55	55	9°356374	25 221	10°633132	9°378960	25 234	10°621040	10°012093	25 33	9°998726	103	20	
56	56	9°356452	26 230	10°632867	9°379239	26 243	10°620761	10°012108	26 34	9°998911	104	32	
57	57	9°356530	27 239	10°632605	9°379518	27 252	10°620482	10°012123	27 35	9°999097	105	20	
58	58	9°356608	28 248	10°632341	9°379797	28 262	10°620203	10°012138	28 36	9°999282	106	31	
59	59	9°356686	29 257	10°632078	9°380076	29 271	10°619925	10°012153	29 37	9°999468	107	20	
60	60	9°356764	30 266	10°631815	9°380354	30 280	10°619646	10°012168	30 38	9°999653	108	30	
<i>m</i>	<i>sec</i>	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	<i>m</i>	<i>sec</i>	<i>m</i>

TABLE 68

765

LOG. SINES, COSINES, &c.

0° 54'				13°									
°	'	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	°
30	0	9	9'368185		10'631815	9'380354		10'619646	10'012168		9'987832	6	30
30	2	9	9'368448	1" 9	10'631552	9'380632	1" 9	10'619368	10'012184	1" 1	9'987816	38	30
31	4	9	9'368711	2 17	10'631289	9'380910	2 18	10'619090	10'012199	2 1	9'987801	56	29
30	6	9	9'368974	3 26	10'631026	9'381188	3 28	10'618812	10'012214	3 2	9'987786	74	30
32	8	9	9'369236	4 35	10'630764	9'381466	4 37	10'618534	10'012229	4 2	9'987771	92	28
30	10	9	9'369499	5 43	10'630501	9'381743	5 46	10'618257	10'012244	5 3	9'987756	50	30
33	12	9	9'369761	6 52	10'630239	9'382020	6 55	10'617980	10'012260	6 3	9'987740	48	27
30	14	9	9'370023	7 61	10'629977	9'382298	7 64	10'617702	10'012275	7 4	9'987725	46	30
34	16	9	9'370285	8 70	10'629715	9'382575	8 74	10'617425	10'012290	8 4	9'987710	44	26
30	18	9	9'370546	9 78	10'629454	9'382852	9 83	10'617148	10'012305	9 5	9'987695	42	30
35	20	9	9'370808	10 87	10'629192	9'383129	10 92	10'616871	10'012321	10 5	9'987679	40	25
30	22	9	9'371069	11 95	10'628931	9'383405	11 101	10'616595	10'012336	11 6	9'987664	38	30
36	24	9	9'371330	12 104	10'628670	9'383682	12 110	10'616318	10'012351	12 6	9'987649	36	24
30	26	9	9'371591	13 113	10'628409	9'383958	13 120	10'616042	10'012366	13 7	9'987634	34	30
37	28	9	9'371852	14 122	10'628148	9'384234	14 129	10'615766	10'012382	14 7	9'987618	32	23
30	30	9	9'372113	15 130	10'627887	9'384510	15 138	10'615490	10'012397	15 8	9'987603	30	30
38	32	9	9'372373	16 139	10'627627	9'384786	16 147	10'615214	10'012412	16 8	9'987588	28	22
30	34	9	9'372634	17 148	10'627366	9'385062	17 156	10'614938	10'012428	17 9	9'987572	26	30
39	36	9	9'372894	18 156	10'627106	9'385337	18 166	10'614663	10'012443	18 9	9'987557	24	21
30	38	9	9'373154	19 165	10'626846	9'385612	19 175	10'614388	10'012458	19 10	9'987542	22	31
40	40	9	9'373414	20 174	10'626586	9'385888	20 184	10'614112	10'012474	20 10	9'987526	20	20
30	42	9	9'373674	21 182	10'626326	9'386163	21 193	10'613837	10'012489	21 11	9'987511	18	30
41	44	9	9'373933	22 191	10'626067	9'386438	22 202	10'613562	10'012504	22 11	9'987496	16	19
30	46	9	9'374192	23 200	10'625808	9'386712	23 212	10'613288	10'012520	23 12	9'987480	14	30
42	48	9	9'374452	24 208	10'625548	9'386987	24 221	10'613013	10'012535	24 12	9'987465	12	18
30	50	9	9'374711	25 217	10'625289	9'387261	25 230	10'612739	10'012551	25 13	9'987449	10	30
43	52	9	9'374970	26 226	10'625030	9'387536	26 239	10'612464	10'012566	26 13	9'987434	8	17
30	54	9	9'375228	27 235	10'624772	9'387810	27 248	10'612190	10'012581	27 14	9'987419	6	30
44	56	9	9'375487	28 243	10'624513	9'388084	28 258	10'611916	10'012597	28 14	9'987403	4	16
30	58	9	9'375745	29 252	10'624255	9'388358	29 267	10'611642	10'012612	29 15	9'987388	2	30
45	60	9	9'376003	30 261	10'623997	9'388631	30 276	10'611369	10'012628	30 15	9'987372	8	15
30	2	9	9'376261	1 8	10'623739	9'388905	1 9	10'611095	10'012643	1 1	9'987357	58	30
46	4	9	9'376519	2 17	10'623481	9'389178	2 18	10'610822	10'012659	2 1	9'987341	56	14
30	6	9	9'376777	3 25	10'623223	9'389451	3 27	10'610549	10'012674	3 2	9'987326	54	30
47	8	9	9'377035	4 34	10'622965	9'389724	4 36	10'610276	10'012690	4 2	9'987310	52	13
30	10	9	9'377292	5 42	10'622708	9'389997	5 45	10'610003	10'012705	5 3	9'987295	50	30
48	12	9	9'377549	6 51	10'622451	9'390270	6 54	10'609730	10'012721	6 3	9'987279	48	12
30	14	9	9'377806	7 59	10'622194	9'390543	7 63	10'609457	10'012737	7 4	9'987264	46	30
49	16	9	9'378063	8 68	10'621937	9'390815	8 72	10'609185	10'012752	8 4	9'987248	44	11
30	18	9	9'378320	9 76	10'621680	9'391087	9 81	10'608913	10'012767	9 5	9'987233	42	30
50	20	9	9'378577	10 85	10'621423	9'391360	10 90	10'608640	10'012783	10 5	9'987217	40	10
30	22	9	9'378833	11 94	10'621167	9'391632	11 99	10'608368	10'012798	11 6	9'987202	38	30
51	24	9	9'379089	12 102	10'620911	9'391903	12 108	10'608097	10'012814	12 6	9'987186	36	9
30	26	9	9'379345	13 111	10'620654	9'392175	13 118	10'607825	10'012830	13 7	9'987170	34	30
52	28	9	9'379601	14 119	10'620399	9'392447	14 127	10'607553	10'012845	14 7	9'987155	32	8
30	30	9	9'379857	15 128	10'620143	9'392718	15 136	10'607282	10'012861	15 8	9'987139	30	30
53	32	9	9'380113	16 136	10'619887	9'392989	16 145	10'607011	10'012876	16 8	9'987124	28	7
30	34	9	9'380368	17 145	10'619632	9'393260	17 154	10'606740	10'012892	17 9	9'987108	26	30
54	36	9	9'380624	18 153	10'619376	9'393531	18 162	10'606469	10'012908	18 9	9'987092	24	6
30	38	9	9'380879	19 162	10'619121	9'393802	19 172	10'606198	10'012923	19 10	9'987077	22	30
55	40	9	9'381134	20 170	10'618866	9'394073	20 181	10'605927	10'012939	20 10	9'987061	20	5
30	42	9	9'381389	21 179	10'618611	9'394343	21 190	10'605657	10'012955	21 11	9'987045	18	30
56	44	9	9'381643	22 187	10'618357	9'394614	22 199	10'605386	10'012970	22 11	9'987030	16	1
30	46	9	9'381898	23 196	10'618102	9'394884	23 208	10'605116	10'012986	23 12	9'987014	14	30
57	48	9	9'382152	24 204	10'617848	9'395154	24 217	10'604846	10'013002	24 12	9'986998	12	8
30	50	9	9'382406	25 213	10'617594	9'395424	25 226	10'604576	10'013017	25 13	9'986983	10	30
58	52	9	9'382661	26 222	10'617339	9'395694	26 235	10'604306	10'013033	26 14	9'986967	8	2
30	54	9	9'382914	27 230	10'617086	9'395963	27 244	10'604037	10'013049	27 14	9'986951	6	30
59	56	9	9'383168	28 239	10'616832	9'396233	28 253	10'603767	10'013064	28 15	9'986936	4	1
30	58	9	9'383422	29 247	10'616578	9'396502	29 262	10'603498	10'013080	29 15	9'986920	2	30
60	60	9	9'383675	30 256	10'616325	9'396771	30 271	10'603229	10'013096	30 16	9'986904	0	0
°	'	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	°

76°

5° 4'

76°

5° 4'

LOG. SINES, COSINES, &c.

0° 56'										14°									
°	'	Sine	Parts	Cosec.	Tang mt	Parts	Cotang.	Secant	Parts	Cosine	°	'	Sine	Parts	Cosec.	Tang mt	Parts	Cotang.	Secant
0	0	9°383675		10°616325	9°396771	1°	9	10°603229	10°013096	9°986904	0	0	9°383675		10°616325	9°396771	1°	9	10°603229
1	1	9°383928	1°	10°616072	9°397040	2	18	10°602960	10°013112	9°986888	1	1	9°383928	1°	10°616072	9°397040	2	18	10°602960
2	2	9°384182	2	10°615818	9°397309	3	27	10°602691	10°013127	9°986873	2	2	9°384182	2	10°615818	9°397309	3	27	10°602691
3	3	9°384435	3	10°615565	9°397578	4	36	10°602422	10°013143	9°986857	3	3	9°384435	3	10°615565	9°397578	4	36	10°602422
4	4	9°384687	4	10°615313	9°397846	5	44	10°602154	10°013159	9°986841	4	4	9°384687	4	10°615313	9°397846	5	44	10°602154
5	5	9°384940	5	10°615060	9°398115	6	53	10°601885	10°013175	9°986825	5	5	9°384940	5	10°615060	9°398115	6	53	10°601885
6	6	9°385192	6	10°614808	9°398383	7	62	10°601617	10°013191	9°986809	6	6	9°385192	6	10°614808	9°398383	7	62	10°601617
7	7	9°385445	7	10°614555	9°398651	8	71	10°601349	10°013206	9°986794	7	7	9°385445	7	10°614555	9°398651	8	71	10°601349
8	8	9°385697	8	10°614303	9°398919	9	80	10°601081	10°013222	9°986778	8	8	9°385697	8	10°614303	9°398919	9	80	10°601081
9	9	9°385949	9	10°614051	9°399187	10	89	10°600813	10°013238	9°986762	9	9	9°385949	9	10°614051	9°399187	10	89	10°600813
10	10	9°386201	10	10°613799	9°399455	11	98	10°600545	10°013254	9°986746	10	10	9°386201	10	10°613799	9°399455	11	98	10°600545
11	11	9°386452	11	10°613548	9°399722	12	107	10°600278	10°013270	9°986730	11	11	9°386452	11	10°613548	9°399722	12	107	10°600278
12	12	9°386704	12	10°613296	9°399990	13	116	10°600010	10°013286	9°986714	12	12	9°386704	12	10°613296	9°399990	13	116	10°600010
13	13	9°386955	13	10°613045	9°400257	14	125	10°599743	10°013301	9°986699	13	13	9°386955	13	10°613045	9°400257	14	125	10°599743
14	14	9°387207	14	10°612793	9°400524	15	133	10°599476	10°013317	9°986683	14	14	9°387207	14	10°612793	9°400524	15	133	10°599476
15	15	9°387458	15	10°612542	9°400791	16	142	10°599209	10°013333	9°986667	15	15	9°387458	15	10°612542	9°400791	16	142	10°599209
16	16	9°387709	16	10°612291	9°401058	17	151	10°598942	10°013349	9°986651	16	16	9°387709	16	10°612291	9°401058	17	151	10°598942
17	17	9°387959	17	10°612041	9°401325	18	160	10°598675	10°013365	9°986635	17	17	9°387959	17	10°612041	9°401325	18	160	10°598675
18	18	9°388210	18	10°611790	9°401591	19	169	10°598409	10°013381	9°986619	18	18	9°388210	18	10°611790	9°401591	19	169	10°598409
19	19	9°388461	19	10°611539	9°401857	20	178	10°598143	10°013397	9°986603	19	19	9°388461	19	10°611539	9°401857	20	178	10°598143
20	20	9°388711	20	10°611289	9°402124	21	187	10°597876	10°013413	9°986587	20	20	9°388711	20	10°611289	9°402124	21	187	10°597876
21	21	9°388961	21	10°611039	9°402390	22	196	10°597610	10°013429	9°986571	21	21	9°388961	21	10°611039	9°402390	22	196	10°597610
22	22	9°389211	22	10°610789	9°402656	23	205	10°597344	10°013445	9°986555	22	22	9°389211	22	10°610789	9°402656	23	205	10°597344
23	23	9°389461	23	10°610539	9°402922	24	214	10°597078	10°013461	9°986539	23	23	9°389461	23	10°610539	9°402922	24	214	10°597078
24	24	9°389711	24	10°610289	9°403187	25	223	10°596813	10°013477	9°986523	24	24	9°389711	24	10°610289	9°403187	25	223	10°596813
25	25	9°389960	25	10°610040	9°403453	26	231	10°596547	10°013493	9°986507	25	25	9°389960	25	10°610040	9°403453	26	231	10°596547
26	26	9°390210	26	10°609790	9°403718	27	240	10°596282	10°013509	9°986491	26	26	9°390210	26	10°609790	9°403718	27	240	10°596282
27	27	9°390459	27	10°609541	9°403983	28	249	10°596017	10°013525	9°986475	27	27	9°390459	27	10°609541	9°403983	28	249	10°596017
28	28	9°390708	28	10°609292	9°404249	29	258	10°595751	10°013541	9°986459	28	28	9°390708	28	10°609292	9°404249	29	258	10°595751
29	29	9°390957	29	10°609043	9°404514	30	267	10°595486	10°013557	9°986443	29	29	9°390957	29	10°609043	9°404514	30	267	10°595486
30	30	9°391206	30	10°608794	9°404778	31	276	10°595222	10°013573	9°986427	30	30	9°391206	30	10°608794	9°404778	31	276	10°595222
31	31	9°391454	1	10°608546	9°405043	1	9	10°594957	10°013589	9°986411	31	31	9°391454	1	10°608546	9°405043	1	9	10°594957
32	32	9°391703	2	10°608297	9°405308	2	17	10°594692	10°013605	9°986395	32	32	9°391703	2	10°608297	9°405308	2	17	10°594692
33	33	9°391951	3	10°608049	9°405572	3	26	10°594428	10°013621	9°986379	33	33	9°391951	3	10°608049	9°405572	3	26	10°594428
34	34	9°392199	4	10°607801	9°405836	4	35	10°594164	10°013637	9°986363	34	34	9°392199	4	10°607801	9°405836	4	35	10°594164
35	35	9°392447	5	10°607553	9°406100	5	44	10°593900	10°013653	9°986347	35	35	9°392447	5	10°607553	9°406100	5	44	10°593900
36	36	9°392695	6	10°607305	9°406364	6	52	10°593636	10°013669	9°986331	36	36	9°392695	6	10°607305	9°406364	6	52	10°593636
37	37	9°392943	7	10°607057	9°406628	7	61	10°593372	10°013685	9°986315	37	37	9°392943	7	10°607057	9°406628	7	61	10°593372
38	38	9°393191	8	10°606809	9°406892	8	70	10°593108	10°013701	9°986299	38	38	9°393191	8	10°606809	9°406892	8	70	10°593108
39	39	9°393438	9	10°606562	9°407155	9	79	10°592845	10°013718	9°986283	39	39	9°393438	9	10°606562	9°407155	9	79	10°592845
40	40	9°393685	10	10°606315	9°407419	10	87	10°592581	10°013734	9°986266	40	40	9°393685	10	10°606315	9°407419	10	87	10°592581
41	41	9°393932	11	10°606068	9°407682	11	96	10°592318	10°013750	9°986250	41	41	9°393932	11	10°606068	9°407682	11	96	10°592318
42	42	9°394179	12	10°605821	9°407945	12	105	10°592055	10°013766	9°986234	42	42	9°394179	12	10°605821	9°407945	12	105	10°592055
43	43	9°394426	13	10°605574	9°408208	13	114	10°591792	10°013782	9°986218	43	43	9°394426	13	10°605574	9°408208	13	114	10°591792
44	44	9°394673	14	10°605327	9°408471	14	122	10°591529	10°013798	9°986202	44	44	9°394673	14	10°605327	9°408471	14	122	10°591529
45	45	9°394919	15	10°605081	9°408734	15	131	10°591266	10°013814	9°986186	45	45	9°394919	15	10°605081	9°408734	15	131	10°591266
46	46	9°395166	16	10°604834	9°408996	16	140	10°591004	10°013831	9°986169	46	46	9°395166	16	10°604834	9°408996	16	140	10°591004
47	47	9°395412	17	10°604588	9°409259	17	149	10°590741	10°013847	9°986153	47	47	9°395412	17	10°604588	9°409259	17	149	10°590741
48	48	9°395658	18	10°604342	9°409521	18	157	10°590479	10°013863	9°986137	48	48	9°395658	18	10°604342	9°409521	18	157	10°590479
49	49	9°395904	19	10°604096	9°409783	19	166	10°590217	10°013879	9°986121	49	49	9°395904	19	10°604096	9°409783	19	166	10°590217
50	50	9°396150	20	10°603850	9°410045	20	175	10°589955	10°013896	9°986104	50	50	9°396150	20	10°603850	9°410045	20	175	10°589955
51	51	9°396395	21	10°603605	9°410307	21	184	10°589693	10°013912	9°986088	51	51	9°396395	21	10°603605	9°410307	21	184	10°589693
52	52	9°396641	22	10°603359	9°410569	22	192	10°589431	10°013928	9°986072	52	52	9°396641	22	10°603359	9°410569	22	192	10°589431
53	53	9°396886	23	10°603114	9°410831	23	201	10°589169	10°013944	9°986056	53	53	9°396886	23	10°603114	9°410831	23	201	10°589169
54	54	9°397132	24	10°602868	9°411092	24	210	10°588908	10°013961	9°986040	54	54	9°397132	24	10°602868	9°411092	24	210	10°588908
55	55	9°397377	25	10°602623	9°411353	25	219	10°588647	10°013977	9°986024	55	55	9°397377	25	10°602623	9°411353	25	219	10°588647
56	56	9°397621	26	10°602379	9°411615	26	227	10°588385	10°013993	9°986007	56	56	9°397621	26	10°602379	9°411615	26	227	10°588385

LOG. SINES, COSINES, &c.

0° 58'										14°									
°	'	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	°	'	m.	Sine	Parts	Cosec.	Tangent
30	0	0	9°398600		10°601400	9°412658		10°587342	10°014658		9°985942	2	30	0	0	9°985942		10°601400	9°412658
30	1	1	9°398844	1	10°601156	9°412919	1	10°587081	10°014975	1	9°985925	38	30	1	1	9°985925	1	10°601156	9°412919
31	4	4	9°399088	2	10°600912	9°413179	2	10°586821	10°014991	2	9°985909	76	30	4	4	9°985909	2	10°600912	9°413179
31	5	5	9°399332	3	10°600668	9°413439	3	10°586561	10°014107	3	9°985893	54	30	5	5	9°985893	3	10°600668	9°413439
32	8	8	9°399575	4	10°600425	9°413699	4	10°586301	10°014124	4	9°985876	52	30	8	8	9°985876	4	10°600425	9°413699
32	10	10	9°399819	5	10°600181	9°413959	5	10°586041	10°014141	5	9°985860	50	30	10	10	9°985860	5	10°600181	9°413959
33	12	12	9°400062	6	10°599938	9°414219	6	10°585781	10°014157	6	9°985843	48	30	12	12	9°985843	6	10°599938	9°414219
33	14	14	9°400306	7	10°599694	9°414479	7	10°585521	10°014173	7	9°985827	46	30	14	14	9°985827	7	10°599694	9°414479
34	16	16	9°400549	8	10°599451	9°414738	8	10°585262	10°014189	8	9°985811	44	30	16	16	9°985811	8	10°599451	9°414738
34	18	18	9°400792	9	10°599208	9°414998	9	10°585002	10°014206	9	9°985794	42	30	18	18	9°985794	9	10°599208	9°414998
35	20	20	9°401035	10	10°598965	9°415257	10	10°584743	10°014222	10	9°985778	40	30	20	20	9°985778	10	10°598965	9°415257
35	22	22	9°401277	11	10°598723	9°415516	11	10°584484	10°014239	11	9°985761	38	30	22	22	9°985761	11	10°598723	9°415516
36	24	24	9°401520	12	10°598480	9°415775	12	10°584225	10°014255	12	9°985745	36	30	24	24	9°985745	12	10°598480	9°415775
36	26	26	9°401762	13	10°598238	9°416034	13	10°583966	10°014272	13	9°985728	34	30	26	26	9°985728	13	10°598238	9°416034
37	28	28	9°402005	14	10°597995	9°416293	14	10°583707	10°014288	14	9°985712	32	30	28	28	9°985712	14	10°597995	9°416293
37	30	30	9°402247	15	10°597751	9°416551	15	10°583449	10°014305	15	9°985695	30	30	30	30	9°985695	15	10°597751	9°416551
38	32	32	9°402489	16	10°597511	9°416810	16	10°583190	10°014321	16	9°985679	28	30	32	32	9°985679	16	10°597511	9°416810
38	34	34	9°402731	17	10°597269	9°417068	17	10°582932	10°014338	17	9°985662	26	30	34	34	9°985662	17	10°597269	9°417068
39	36	36	9°402972	18	10°597028	9°417326	18	10°582674	10°014354	18	9°985646	24	30	36	36	9°985646	18	10°597028	9°417326
39	38	38	9°403214	19	10°596786	9°417585	19	10°582415	10°014371	19	9°985629	22	30	38	38	9°985629	19	10°596786	9°417585
40	40	40	9°403455	20	10°596545	9°417842	20	10°582157	10°014387	20	9°985613	20	30	40	40	9°985613	20	10°596545	9°417842
40	42	42	9°403697	21	10°596303	9°418100	21	10°581900	10°014404	21	9°985596	18	30	42	42	9°985596	21	10°596303	9°418100
41	44	44	9°403939	22	10°596062	9°418358	22	10°581642	10°014420	22	9°985580	16	30	44	44	9°985580	22	10°596062	9°418358
41	46	46	9°404179	23	10°595821	9°418616	23	10°581384	10°014437	23	9°985563	14	30	46	46	9°985563	23	10°595821	9°418616
42	48	48	9°404420	24	10°595580	9°418873	24	10°581127	10°014453	24	9°985547	12	30	48	48	9°985547	24	10°595580	9°418873
42	50	50	9°404660	25	10°595340	9°419130	25	10°580870	10°014470	25	9°985530	10	30	50	50	9°985530	25	10°595340	9°419130
43	52	52	9°404901	26	10°595099	9°419387	26	10°580613	10°014486	26	9°985514	8	30	52	52	9°985514	26	10°595099	9°419387
43	54	54	9°405141	27	10°594859	9°419644	27	10°580356	10°014503	27	9°985497	6	30	54	54	9°985497	27	10°594859	9°419644
44	56	56	9°405382	28	10°594618	9°419901	28	10°580099	10°014520	28	9°985480	4	30	56	56	9°985480	28	10°594618	9°419901
44	58	58	9°405622	29	10°594378	9°420158	29	10°579842	10°014536	29	9°985464	2	30	58	58	9°985464	29	10°594378	9°420158
45	60	60	9°405862	30	10°594138	9°420415	30	10°579585	10°014553	30	9°985447	1	30	60	60	9°985447	30	10°594138	9°420415
45	0	0	9°406102	1	10°593898	9°420671	1	10°579329	10°014570	1	9°985430	58	30	0	0	9°985430	1	10°593898	9°420671
46	2	2	9°406341	2	10°593659	9°420927	2	10°579071	10°014586	2	9°985414	56	30	2	2	9°985414	2	10°593659	9°420927
46	4	4	9°406581	3	10°593419	9°421184	3	10°578813	10°014603	3	9°985397	54	30	4	4	9°985397	3	10°593419	9°421184
47	6	6	9°406820	4	10°593180	9°421440	4	10°578556	10°014619	4	9°985381	52	30	6	6	9°985381	4	10°593180	9°421440
47	8	8	9°407060	5	10°592940	9°421696	5	10°578304	10°014636	5	9°985364	50	30	8	8	9°985364	5	10°592940	9°421696
48	10	10	9°407299	6	10°592701	9°421952	6	10°578048	10°014653	6	9°985347	48	30	10	10	9°985347	6	10°592701	9°421952
48	12	12	9°407538	7	10°592462	9°422207	7	10°577793	10°014670	7	9°985330	46	30	12	12	9°985330	7	10°592462	9°422207
48	14	14	9°407777	8	10°592223	9°422463	8	10°577537	10°014686	8	9°985314	44	30	14	14	9°985314	8	10°592223	9°422463
49	16	16	9°408015	9	10°591985	9°422718	9	10°577282	10°014703	9	9°985297	42	30	16	16	9°985297	9	10°591985	9°422718
49	18	18	9°408254	10	10°591746	9°422974	10	10°577026	10°014720	10	9°985280	40	30	18	18	9°985280	10	10°591746	9°422974
49	20	20	9°408492	11	10°591508	9°423229	11	10°576771	10°014736	11	9°985264	38	30	20	20	9°985264	11	10°591508	9°423229
50	22	22	9°408731	12	10°591269	9°423484	12	10°576516	10°014753	12	9°985247	36	30	22	22	9°985247	12	10°591269	9°423484
50	24	24	9°408969	13	10°591031	9°423739	13	10°576261	10°014770	13	9°985230	34	30	24	24	9°985230	13	10°591031	9°423739
51	26	26	9°409207	14	10°590793	9°423993	14	10°576007	10°014787	14	9°985213	32	30	26	26	9°985213	14	10°590793	9°423993
51	28	28	9°409445	15	10°590555	9°424248	15	10°575752	10°014803	15	9°985197	30	30	28	28	9°985197	15	10°590555	9°424248
52	30	30	9°409682	16	10°590318	9°424503	16	10°575497	10°014820	16	9°985180	28	30	30	30	9°985180	16	10°590318	9°424503
52	32	32	9°409920	17	10°590080	9°424757	17	10°575243	10°014837	17	9°985163	26	30	32	32	9°985163	17	10°590080	9°424757
53	34	34	9°410157	18	10°589843	9°425011	18	10°574989	10°014854	18	9°985146	24	30	34	34	9°985146	18	10°589843	9°425011
53	36	36	9°410395	19	10°589605	9°425265	19	10°574735	10°014871	19	9°985129	22	30	36	36	9°985129	19	10°589605	9°425265
54	38	38	9°410632	20	10°589368	9°425519	20	10°574481	10°014887	20	9°985113	20	30	38	38	9°985113	20	10°589368	9°425519
54	40	40	9°410869	21	10°589131	9°425773	21	10°574227	10°014904	21	9°985096	18	30	40	40	9°985096	21	10°589131	9°425773
55	42	42	9°411106	22	10°588894	9°426027	22	10°573973	10°014921	22	9°985079	16	30	42	42	9°985079	22	10°588894	9°426027
55	44	44	9°411343	23	10°588657	9°426281	23	10°573719	10°014938	23	9°985062	14	30	44	44	9°985062	23	10°588657	9°426281
56	46	46	9°411579	24	10°588421	9°426534	24	10°573465	10°014955	24	9°985045	12	30	46	46	9°985045	24	10°588421	9°426534
56	48	48	9°411816	25	10°588184	9°426787	25	10°573212	10°014972	25	9°985028	10	30	48	48	9°985028	25	10°588184	9°426787
57	50	50	9°412052	26	10°587948	9°427041	26	10°572959	10°014989	26	9°985011	8	30	50	50	9°985011	26	10°587948	9°427041
57	52	52	9°412288	27	10°587712	9°427294	27	10°572706	10°015005	27	9°984995	6	30	52	52	9°984995	27	10°587712	9°427294
58	54	54	9°412524	28	10°587476	9°427547	28	10°572453	10°015022	28	9°984978	4	30	54	54	9°984978	28	10°587476	9°427547
58	56	56	9°412760	29	10°587240	9°427800	29	10°5722											

LOG. SINES, COSINES, &c.											
1° 0'				15°							
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	°
0	0	9'412996	1	10'587004	9'428052	10'571948	10'015056	9'984944	60	60	0
0	2	9'413232	1	10'586768	9'428305	10'571695	10'015073	9'984927	58	58	2
0	4	9'413467	2	10'586533	9'428558	10'571442	10'015090	9'984910	56	56	4
0	6	9'413703	3	10'586297	9'428810	10'571190	10'015107	9'984893	54	54	6
0	8	9'413938	4	10'586062	9'429062	10'570938	10'015124	9'984876	52	52	8
0	10	9'414173	5	10'585827	9'429314	10'570686	10'015141	9'984859	50	50	10
0	12	9'414408	6	10'585592	9'429566	10'570434	10'015158	9'984842	48	48	12
0	14	9'414643	7	10'585357	9'429818	10'570182	10'015175	9'984825	46	46	14
0	16	9'414878	8	10'585122	9'430070	10'569930	10'015192	9'984808	44	44	16
0	18	9'415112	9	10'584888	9'430321	10'569679	10'015209	9'984791	42	42	18
0	20	9'415347	10	10'584653	9'430573	10'569427	10'015226	9'984774	40	40	20
0	22	9'415581	11	10'584419	9'430824	10'569176	10'015243	9'984757	38	38	22
0	24	9'415815	12	10'584185	9'431075	10'568925	10'015260	9'984740	36	36	24
0	26	9'416049	13	10'583951	9'431326	10'568674	10'015277	9'984723	34	34	26
0	28	9'416283	14	10'583717	9'431577	10'568423	10'015294	9'984706	32	32	28
0	30	9'416517	15	10'583483	9'431828	10'568172	10'015311	9'984689	30	30	30
0	32	9'416751	16	10'583249	9'432079	10'567921	10'015328	9'984672	28	28	32
0	34	9'416984	17	10'583016	9'432329	10'567671	10'015345	9'984655	26	26	34
0	36	9'417217	18	10'582783	9'432580	10'567420	10'015362	9'984638	24	24	36
0	38	9'417451	19	10'582549	9'432830	10'567170	10'015379	9'984621	22	22	38
0	40	9'417684	20	10'582316	9'433080	10'566920	10'015397	9'984603	20	20	40
0	42	9'417917	21	10'582083	9'433331	10'566669	10'015414	9'984586	18	18	42
0	44	9'418150	22	10'581850	9'433580	10'566420	10'015431	9'984569	16	16	44
0	46	9'418382	23	10'581618	9'433830	10'566170	10'015448	9'984552	14	14	46
0	48	9'418615	24	10'581385	9'434080	10'565920	10'015465	9'984535	12	12	48
0	50	9'418847	25	10'581153	9'434330	10'565670	10'015482	9'984518	10	10	50
0	52	9'419079	26	10'580921	9'434579	10'565421	10'015500	9'984500	8	8	52
0	54	9'419312	27	10'580688	9'434828	10'565172	10'015517	9'984483	6	6	54
0	56	9'419544	28	10'580456	9'435078	10'564922	10'015534	9'984466	4	4	56
0	58	9'419776	29	10'580224	9'435327	10'564673	10'015551	9'984449	2	2	58
0	60	9'420007	30	10'579993	9'435576	10'564424	10'015568	9'984432	0	0	60
1	0	9'420239	1	10'579761	9'435825	10'564175	10'015586	9'984414	39	39	1
1	2	9'420470	2	10'579530	9'436073	10'563927	10'015603	9'984397	37	37	3
1	4	9'420702	3	10'579298	9'436322	10'563678	10'015620	9'984380	35	35	5
1	6	9'420933	4	10'579067	9'436570	10'563430	10'015637	9'984363	33	33	7
1	8	9'421164	5	10'578836	9'436819	10'563181	10'015655	9'984345	31	31	9
1	10	9'421395	6	10'578605	9'437067	10'562933	10'015672	9'984328	29	29	11
1	12	9'421626	7	10'578374	9'437315	10'562685	10'015689	9'984311	27	27	13
1	14	9'421857	8	10'578143	9'437563	10'562437	10'015706	9'984294	25	25	15
1	16	9'422087	9	10'577911	9'437811	10'562189	10'015724	9'984276	23	23	17
1	18	9'422318	10	10'577682	9'438059	10'561941	10'015741	9'984259	21	21	19
1	20	9'422548	11	10'577452	9'438306	10'561694	10'015758	9'984242	19	19	21
1	22	9'422778	12	10'577222	9'438554	10'561446	10'015776	9'984224	17	17	23
1	24	9'423008	13	10'576992	9'438801	10'561199	10'015793	9'984207	15	15	25
1	26	9'423238	14	10'576762	9'439048	10'560952	10'015810	9'984190	13	13	27
1	28	9'423468	15	10'576532	9'439296	10'560704	10'015828	9'984172	11	11	29
1	30	9'423697	16	10'576303	9'439543	10'560457	10'015845	9'984155	9	9	31
1	32	9'423927	17	10'576073	9'439790	10'560210	10'015863	9'984137	7	7	33
1	34	9'424156	18	10'575844	9'440036	10'559964	10'015880	9'984120	5	5	35
1	36	9'424386	19	10'575614	9'440283	10'559717	10'015897	9'984103	3	3	37
1	38	9'424615	20	10'575385	9'440529	10'559471	10'015915	9'984085	1	1	39
1	40	9'424844	21	10'575156	9'440776	10'559224	10'015932	9'984068	39	39	41
1	42	9'425073	22	10'574927	9'441022	10'558978	10'015950	9'984050	37	37	43
1	44	9'425301	23	10'574699	9'441268	10'558732	10'015967	9'984033	35	35	45
1	46	9'425530	24	10'574470	9'441514	10'558486	10'015985	9'984015	33	33	47
1	48	9'425758	25	10'574242	9'441760	10'558240	10'016002	9'983998	31	31	49
1	50	9'425987	26	10'574013	9'442006	10'557994	10'016019	9'983981	29	29	51
1	52	9'426215	27	10'573785	9'442252	10'557748	10'016037	9'983963	27	27	53
1	54	9'426443	28	10'573557	9'442497	10'557503	10'016054	9'983946	25	25	55
1	56	9'426671	29	10'573329	9'442743	10'557257	10'016072	9'983928	23	23	57
1	58	9'426899	30	10'573101	9'442988	10'557012	10'016089	9'983911	21	21	59
1	60										60
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	°

TABLE 68

769

LOG. SINES, COSINES, &c.

1 ^h 2 ^m		15 ^c										74 ^o		4 ^h 56 ^m	
m.	s.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	m.	s.	m.	s.
30	0	9°426899		10°573101	9°442988		10°557012	10°016089		9°983911	58	30			
30	2	9°427127	1" 8	10°572873	9°443234	1" 8	10°556766	10°016107	1" 1	9°983893	58	30			
31	4	9°427354	2 15	10°572646	9°443479	2 16	10°556521	10°016125	2 1	9°983875	58	29			
30	6	9°427582	3 23	10°572418	9°443724	3 24	10°556276	10°016142	3 2	9°983858	58	30			
32	8	9°427809	4 30	10°572191	9°443968	4 32	10°556032	10°016160	4 2	9°983840	58	28			
30	10	9°428036	5 38	10°571964	9°444213	5 41	10°555787	10°016177	5 3	9°983823	58	30			
33	12	9°428263	6 45	10°571737	9°444458	6 49	10°555542	10°016195	6 4	9°983805	48	27			
30	14	9°428490	7 53	10°571510	9°444702	7 57	10°555298	10°016212	7 4	9°983788	46	30			
34	16	9°428717	8 60	10°571283	9°444947	8 65	10°555053	10°016230	8 5	9°983770	44	26			
30	18	9°428944	9 68	10°571056	9°445191	9 73	10°554809	10°016248	9 5	9°983752	42	30			
35	20	9°429170	10 75	10°570830	9°445435	10 81	10°554565	10°016265	10 6	9°983735	40	25			
30	22	9°429397	11 83	10°570603	9°445679	11 89	10°554321	10°016283	11 6	9°983717	38	30			
36	24	9°429623	12 90	10°570377	9°445923	12 97	10°554077	10°016300	12 7	9°983700	36	24			
30	26	9°429849	13 98	10°570151	9°446167	13 106	10°553833	10°016318	13 8	9°983682	34	38			
37	28	9°430075	14 105	10°569925	9°446411	14 114	10°553589	10°016336	14 8	9°983664	32	23			
30	30	9°430301	15 113	10°569699	9°446654	15 122	10°553346	10°016353	15 9	9°983647	30	38			
38	32	9°430527	16 120	10°569473	9°446898	16 130	10°553102	10°016371	16 9	9°983629	28	28			
30	34	9°430752	17 128	10°569248	9°447141	17 138	10°552859	10°016389	17 10	9°983611	26	30			
39	36	9°430978	18 135	10°569022	9°447384	18 146	10°552616	10°016406	18 11	9°983594	24	21			
30	38	9°431203	19 143	10°568797	9°447627	19 154	10°552373	10°016424	19 11	9°983576	22	30			
40	40	9°431429	20 151	10°568571	9°447870	20 162	10°552130	10°016442	20 12	9°983558	20	20			
30	42	9°431654	21 158	10°568346	9°448113	21 171	10°551887	10°016460	21 12	9°983540	18	30			
41	44	9°431879	22 166	10°568121	9°448356	22 179	10°551644	10°016477	22 13	9°983523	16	19			
30	46	9°432104	23 173	10°567896	9°448599	23 187	10°551401	10°016495	23 14	9°983505	14	30			
42	48	9°432329	24 181	10°567671	9°448841	24 195	10°551159	10°016513	24 14	9°983487	12	18			
30	50	9°432553	25 188	10°567447	9°449084	25 203	10°550916	10°016531	25 15	9°983469	10	30			
43	52	9°432778	26 196	10°567222	9°449326	26 211	10°550674	10°016548	26 15	9°983452	8	17			
30	54	9°433002	27 203	10°566998	9°449568	27 219	10°550432	10°016566	27 16	9°983434	6	30			
44	56	9°433226	28 210	10°566774	9°449810	28 227	10°550190	10°016584	28 17	9°983416	4	16			
30	58	9°433451	29 217	10°566549	9°450052	29 235	10°549948	10°016602	29 17	9°983398	2	30			
45	60	9°433675	30 226	10°566325	9°450294	30 244	10°549706	10°016619	30 18	9°983381	0	15			
30	2	9°433898	1 7	10°566102	9°450536	1 8	10°549464	10°016637	1 1	9°983363	58	30			
46	4	9°434122	2 15	10°565878	9°450777	2 16	10°549223	10°016655	2 1	9°983345	56	14			
30	6	9°434346	3 22	10°565654	9°451019	3 24	10°548981	10°016673	3 2	9°983327	54	30			
47	8	9°434569	4 30	10°565431	9°451260	4 32	10°548740	10°016691	4 2	9°983309	52	13			
30	10	9°434793	5 37	10°565207	9°451502	5 40	10°548498	10°016709	5 3	9°983291	50	30			
48	12	9°435016	6 44	10°564984	9°451743	6 48	10°548257	10°016727	6 4	9°983273	48	12			
30	14	9°435239	7 52	10°564761	9°451984	7 56	10°548016	10°016744	7 4	9°983256	46	30			
49	16	9°435462	8 59	10°564538	9°452225	8 64	10°547775	10°016762	8 5	9°983238	44	11			
30	18	9°435685	9 67	10°564315	9°452465	9 72	10°547535	10°016780	9 5	9°983220	42	30			
50	20	9°435908	10 74	10°564092	9°452706	10 80	10°547294	10°016798	10 6	9°983202	40	10			
30	22	9°436131	11 82	10°563869	9°452947	11 88	10°547053	10°016816	11 7	9°983184	38	30			
51	24	9°436353	12 89	10°563647	9°453187	12 96	10°546813	10°016834	12 7	9°983166	36	9			
30	26	9°436576	13 97	10°563424	9°453428	13 104	10°546572	10°016852	13 8	9°983148	34	30			
52	28	9°436798	14 104	10°563202	9°453668	14 112	10°546332	10°016870	14 8	9°983130	32	8			
30	30	9°437020	15 111	10°562980	9°453908	15 120	10°546092	10°016888	15 9	9°983112	30	70			
53	32	9°437242	16 118	10°562758	9°454148	16 128	10°545852	10°016906	16 10	9°983094	28	7			
30	34	9°437464	17 126	10°562536	9°454388	17 136	10°545612	10°016924	17 10	9°983076	26	30			
54	36	9°437686	18 133	10°562314	9°454628	18 144	10°545372	10°016942	18 11	9°983058	24	6			
30	38	9°437908	19 141	10°562092	9°454867	19 152	10°545133	10°016960	19 11	9°983040	22	30			
55	40	9°438129	20 148	10°561871	9°455107	20 160	10°544893	10°016978	20 12	9°983022	20	5			
30	42	9°438351	21 156	10°561649	9°455346	21 168	10°544654	10°016996	21 13	9°983004	18	30			
56	44	9°438572	22 163	10°561428	9°455586	22 176	10°544414	10°017014	22 13	9°982986	16	4			
30	46	9°438793	23 171	10°561207	9°455825	23 184	10°544175	10°017032	23 14	9°982968	14	30			
57	48	9°439014	24 178	10°560986	9°456064	24 192	10°543936	10°017050	24 14	9°982950	12	3			
30	50	9°439235	25 185	10°560765	9°456303	25 200	10°543697	10°017068	25 15	9°982932	10	30			
58	52	9°439456	26 192	10°560544	9°456542	26 208	10°543458	10°017086	26 16	9°982914	8	2			
30	54	9°439677	27 200	10°560323	9°456781	27 216	10°543219	10°017104	27 16	9°982896	6	30			
59	56	9°439898	28 207	10°560103	9°457019	28 224	10°542981	10°017122	28 17	9°982878	4	1			
30	58	9°440118	29 215	10°559882	9°457258	29 232	10°542742	10°017140	29 17	9°982860	2	30			
60	60	9°440338	30 222	10°559662	9°457496	30 240	10°542504	10°017158	30 18	9°982842	0	0			

LOG. SINES. COSINES, &c.													
1 ^h 4 ^m				16°									
"	m.	Sine	Parts	Secant	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	"	
0	0	9°440338		10°559662	9°457496	1	10°542504	10°017158		9°982842	56	141	
1	2	9°440558	1"	10°559441	9°457735	8	10°542265	10°017176	1"	9°982824	56	140	
2	4	9°440778	2 15	10°559222	9°457973	16	10°542027	10°017195	2 15	9°982805	56	139	
3	6	9°440998	3 22	10°559002	9°458211	24	10°541789	10°017213	3 22	9°982787	56	138	
4	8	9°441218	4 29	10°558782	9°458449	32	10°541551	10°017231	4 29	9°982769	56	137	
5	10	9°441438	5 36	10°558562	9°458687	40	10°541313	10°017249	5 36	9°982751	56	136	
6	12	9°441658	6 44	10°558342	9°458925	48	10°541075	10°017267	6 44	9°982733	56	135	
7	14	9°441877	7 51	10°558123	9°459163	56	10°540837	10°017285	7 51	9°982715	56	134	
8	16	9°442096	8 58	10°557904	9°459400	64	10°540600	10°017304	8 58	9°982697	56	133	
9	18	9°442316	9 65	10°557684	9°459638	72	10°540362	10°017322	9 65	9°982679	56	132	
10	20	9°442535	10 73	10°557465	9°459875	80	10°540125	10°017340	10 73	9°982660	56	131	
11	22	9°442754	11 80	10°557246	9°460112	88	10°539888	10°017358	11 80	9°982642	56	130	
12	24	9°442973	12 87	10°557027	9°460349	96	10°539651	10°017376	12 87	9°982624	56	129	
13	26	9°443192	13 95	10°556808	9°460586	104	10°539414	10°017395	13 95	9°982605	56	128	
14	28	9°443410	14 102	10°556590	9°460823	112	10°539177	10°017413	14 102	9°982587	56	127	
15	30	9°443629	15 109	10°556371	9°461060	120	10°538940	10°017431	15 109	9°982569	56	126	
16	32	9°443847	16 116	10°556153	9°461297	128	10°538703	10°017449	16 116	9°982551	56	125	
17	34	9°444066	17 124	10°555934	9°461533	136	10°538467	10°017468	17 124	9°982532	56	124	
18	36	9°444284	18 131	10°555716	9°461770	144	10°538230	10°017486	18 131	9°982514	56	123	
19	38	9°444502	19 138	10°555498	9°462006	152	10°537994	10°017504	19 138	9°982496	56	122	
20	40	9°444720	20 146	10°555280	9°462242	160	10°537758	10°017523	20 146	9°982477	56	121	
21	42	9°444938	21 153	10°555062	9°462478	168	10°537521	10°017541	21 153	9°982459	56	120	
22	44	9°445155	22 160	10°554845	9°462715	176	10°537286	10°017559	22 160	9°982441	56	119	
23	46	9°445373	23 167	10°554627	9°462950	184	10°537050	10°017578	23 167	9°982422	56	118	
24	48	9°445590	24 175	10°554410	9°463186	192	10°536814	10°017596	24 175	9°982404	56	117	
25	50	9°445808	25 182	10°554192	9°463422	200	10°536578	10°017614	25 182	9°982386	56	116	
26	52	9°446025	26 189	10°553975	9°463658	208	10°536342	10°017633	26 189	9°982367	56	115	
27	54	9°446242	27 196	10°553758	9°463893	216	10°536107	10°017651	27 196	9°982349	56	114	
28	56	9°446459	28 204	10°553541	9°464128	224	10°535872	10°017669	28 204	9°982331	56	113	
29	58	9°446676	29 211	10°553324	9°464364	232	10°535636	10°017688	29 211	9°982312	56	112	
30	0	9°446893	30 218	10°553107	9°464599	240	10°535401	10°017706	30 218	9°982294	56	111	
31	2	9°447109	1 7	10°552891	9°464834	1 8	10°535166	10°017725	1 8	9°982275	56	110	
32	4	9°447326	2 14	10°552674	9°465069	2 16	10°534931	10°017743	2 14	9°982257	56	109	
33	6	9°447542	3 22	10°552458	9°465304	3 23	10°534696	10°017761	3 22	9°982239	56	108	
34	8	9°447759	4 29	10°552241	9°465539	4 31	10°534461	10°017779	4 29	9°982220	56	107	
35	10	9°447975	5 36	10°552025	9°465773	5 39	10°534227	10°017798	5 36	9°982202	56	106	
36	12	9°448191	6 43	10°551809	9°466008	6 47	10°533992	10°017817	6 43	9°982183	56	105	
37	14	9°448407	7 50	10°551593	9°466242	7 54	10°533758	10°017835	7 50	9°982165	56	104	
38	16	9°448623	8 57	10°551377	9°466477	8 62	10°533523	10°017854	8 57	9°982146	56	103	
39	18	9°448838	9 64	10°551162	9°466711	9 70	10°533289	10°017873	9 64	9°982128	56	102	
40	20	9°449054	10 72	10°550946	9°466945	10 78	10°533055	10°017891	10 72	9°982109	56	101	
41	22	9°449269	11 79	10°550731	9°467179	11 86	10°532821	10°017909	11 79	9°982091	56	100	
42	24	9°449485	12 86	10°550515	9°467413	12 93	10°532587	10°017928	12 86	9°982072	56	99	
43	26	9°449700	13 93	10°550300	9°467647	13 101	10°532353	10°017946	13 93	9°982054	56	98	
44	28	9°449915	14 100	10°550085	9°467880	14 109	10°532120	10°017965	14 100	9°982035	56	97	
45	30	9°450130	15 107	10°549870	9°468114	15 117	10°531886	10°017984	15 107	9°982016	56	96	
46	32	9°450345	16 114	10°549655	9°468347	16 124	10°531653	10°018002	16 114	9°981998	56	95	
47	34	9°450560	17 122	10°549440	9°468581	17 132	10°531419	10°018021	17 122	9°981979	56	94	
48	36	9°450775	18 129	10°549225	9°468814	18 140	10°531186	10°018039	18 129	9°981961	56	93	
49	38	9°450989	19 136	10°549011	9°469047	19 148	10°530953	10°018058	19 136	9°981942	56	92	
50	40	9°451204	20 143	10°548796	9°469280	20 156	10°530720	10°018076	20 143	9°981924	56	91	
51	42	9°451418	21 150	10°548582	9°469513	21 163	10°530487	10°018095	21 150	9°981905	56	90	
52	44	9°451632	22 157	10°548368	9°469746	22 171	10°530254	10°018114	22 157	9°981886	56	89	
53	46	9°451846	23 165	10°548154	9°469979	23 179	10°530021	10°018132	23 165	9°981868	56	88	
54	48	9°452060	24 172	10°547940	9°470211	24 187	10°529789	10°018151	24 172	9°981849	56	87	
55	50	9°452274	25 179	10°547726	9°470444	25 194	10°529556	10°018170	25 179	9°981830	56	86	
56	52	9°452488	26 186	10°547512	9°470676	26 202	10°529323	10°018188	26 186	9°981812	56	85	
57	54	9°452702	27 193	10°547298	9°470909	27 210	10°529091	10°018207	27 193	9°981793	56	84	
58	56	9°452915	28 200	10°547085	9°471141	28 218	10°528857	10°018226	28 200	9°981774	56	83	
59	58	9°453129	29 208	10°546871	9°471373	29 226	10°528624	10°018244	29 208	9°981756	56	82	
60	0	9°453342	30 215	10°546658	9°471605	30 233	10°528395	10°018263	30 215	9°981737	56	81	
"	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Secant	Parts	Sine	m.	"	
78°													
4 ^h 54 ^m													

LOG. SINES, COSINES, &c.

1° 8'		17°										17°	
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'
0	0	9°465935		10°534065	9°485339	1" 7	10°514661	10°019404		9°980596	52	60	
30	2	9°466142	1" 7	10°533858	9°485565	2 15	10°514435	10°019423	1" 1	9°980577	36	30	
1	4	9°466348	2 14	10°533652	9°485791	2 15	10°514209	10°019442	2 1	9°980558	56	59	
30	6	9°466555	3 20	10°533445	9°486016	3 22	10°513984	10°019462	3 2	9°980538	54	30	
2	8	9°466761	4 27	10°533239	9°486242	4 30	10°513758	10°019481	4 3	9°980519	52	58	
30	10	9°466967	5 34	10°533033	9°486467	5 37	10°513533	10°019500	5 3	9°980500	50	30	
3	12	9°467173	6 41	10°532827	9°486693	6 45	10°513307	10°019520	6 4	9°980480	48	57	
30	14	9°467379	7 48	10°532621	9°486918	7 52	10°513082	10°019539	7 5	9°980461	46	30	
4	16	9°467585	8 55	10°532415	9°487143	8 60	10°512857	10°019558	8 5	9°980442	44	56	
30	18	9°467790	9 61	10°532210	9°487368	9 67	10°512632	10°019578	9 6	9°980422	42	30	
5	20	9°467996	10 68	10°532004	9°487593	10 71	10°512407	10°019597	10 6	9°980403	40	55	
6	22	9°468202	11 75	10°531798	9°487818	11 82	10°512182	10°019617	11 7	9°980383	38	30	
30	24	9°468407	12 82	10°531593	9°488043	12 90	10°511957	10°019636	12 8	9°980364	36	54	
30	26	9°468612	13 89	10°531388	9°488268	13 97	10°511732	10°019656	13 8	9°980344	34	30	
7	28	9°468817	14 96	10°531183	9°488492	14 105	10°511508	10°019675	14 9	9°980325	32	53	
30	30	9°469022	15 102	10°530978	9°488717	15 112	10°511283	10°019694	15 10	9°980306	30	30	
8	32	9°469227	16 109	10°530773	9°488941	16 120	10°511059	10°019714	16 10	9°980286	28	52	
30	34	9°469432	17 116	10°530568	9°489166	17 127	10°510834	10°019733	17 11	9°980267	26	30	
9	36	9°469637	18 123	10°530363	9°489390	18 135	10°510610	10°019753	18 12	9°980247	24	51	
30	38	9°469842	19 130	10°530158	9°489614	19 142	10°510386	10°019772	19 12	9°980228	22	30	
10	40	9°470046	20 137	10°529954	9°489838	20 150	10°510162	10°019792	20 13	9°980208	20	50	
30	42	9°470251	21 143	10°529749	9°490062	21 157	10°509937	10°019811	21 14	9°980189	18	30	
11	44	9°470455	22 150	10°529545	9°490286	22 165	10°509714	10°019831	22 14	9°980169	16	49	
30	46	9°470659	23 157	10°529341	9°490510	23 172	10°509490	10°019851	23 15	9°980149	14	30	
12	48	9°470863	24 164	10°529137	9°490733	24 180	10°509267	10°019870	24 16	9°980130	12	48	
30	50	9°471067	25 171	10°528933	9°490957	25 187	10°509043	10°019890	25 16	9°980110	10	30	
13	52	9°471271	26 178	10°528729	9°491180	26 194	10°508820	10°019909	26 17	9°980091	8	47	
30	54	9°471475	27 184	10°528525	9°491404	27 202	10°508596	10°019929	27 18	9°980071	6	30	
14	56	9°471679	28 191	10°528321	9°491627	28 209	10°508373	10°019948	28 18	9°980052	4	46	
30	58	9°471882	29 198	10°528118	9°491850	29 217	10°508150	10°019968	29 19	9°980032	2	30	
15	0	9°472086	30 205	10°527914	9°492073	30 224	10°507927	10°019988	30 19	9°980012	0	45	
30	2	9°472289	1 7	10°527711	9°492296	1 7	10°507704	10°020007	1 1	9°979993	58	30	
16	4	9°472492	2 13	10°527508	9°492519	2 15	10°507481	10°020027	2 1	9°979973	56	44	
30	6	9°472695	3 20	10°527305	9°492742	3 22	10°507258	10°020046	3 2	9°979954	54	30	
17	8	9°472898	4 27	10°527102	9°492965	4 30	10°507035	10°020066	4 3	9°979934	52	43	
30	10	9°473101	5 34	10°526899	9°493187	5 37	10°506813	10°020086	5 3	9°979914	50	30	
18	12	9°473304	6 40	10°526696	9°493410	6 44	10°506590	10°020105	6 4	9°979895	48	42	
30	14	9°473507	7 47	10°526493	9°493632	7 52	10°506368	10°020125	7 5	9°979875	46	30	
19	16	9°473710	8 54	10°526290	9°493854	8 59	10°506146	10°020145	8 5	9°979855	44	41	
30	18	9°473912	9 61	10°526088	9°494077	9 66	10°505923	10°020164	9 6	9°979836	42	30	
20	20	9°474115	10 67	10°525885	9°494299	10 74	10°505701	10°020184	10 7	9°979816	40	40	
30	22	9°474317	11 74	10°525683	9°494521	11 81	10°505479	10°020204	11 7	9°979796	38	30	
21	24	9°474519	12 81	10°525481	9°494743	12 89	10°505257	10°020224	12 8	9°979776	36	39	
30	26	9°474721	13 88	10°525279	9°494965	13 96	10°505035	10°020244	13 9	9°979757	34	30	
22	28	9°474923	14 94	10°525077	9°495186	14 103	10°504814	10°020263	14 9	9°979737	32	38	
30	30	9°475125	15 101	10°524875	9°495408	15 111	10°504592	10°020283	15 10	9°979717	30	30	
23	32	9°475327	16 108	10°524673	9°495630	16 118	10°504370	10°020303	16 11	9°979697	28	37	
30	34	9°475529	17 115	10°524471	9°495851	17 126	10°504149	10°020322	17 11	9°979678	26	30	
24	36	9°475730	18 122	10°524270	9°496073	18 133	10°503927	10°020342	18 12	9°979658	24	36	
30	38	9°475932	19 128	10°524068	9°496294	19 140	10°503706	10°020362	19 13	9°979638	22	30	
25	40	9°476133	20 135	10°523867	9°496515	20 148	10°503485	10°020382	20 13	9°979618	20	35	
30	42	9°476335	21 142	10°523665	9°496736	21 155	10°503264	10°020402	21 14	9°979598	18	30	
26	44	9°476536	22 149	10°523463	9°496957	22 163	10°503043	10°020421	22 15	9°979579	16	34	
30	46	9°476737	23 155	10°523263	9°497178	23 170	10°502822	10°020441	23 15	9°979559	14	30	
27	48	9°476938	24 161	10°523062	9°497399	24 177	10°502601	10°020461	24 16	9°979539	12	33	
30	50	9°477139	25 168	10°522861	9°497620	25 185	10°502380	10°020481	25 16	9°979519	10	30	
28	52	9°477340	26 175	10°522660	9°497841	26 192	10°502159	10°020501	26 17	9°979499	8	32	
30	54	9°477540	27 181	10°522460	9°498061	27 200	10°501939	10°020521	27 18	9°979479	6	30	
29	56	9°477741	28 188	10°522259	9°498282	28 207	10°501718	10°020541	28 18	9°979459	4	31	
30	58	9°477941	29 195	10°522059	9°498502	29 214	10°501498	10°020561	29 19	9°979439	2	30	
30	0	9°478142	30 202	10°521858	9°498722	30 222	10°501278	10°020580	30 20	9°979420	0	30	
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	Parts	°	'

17°

4° 50'

TABLE 68

LOG. SINES, COSINES, &c.															
1°		18°													
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	Secant	Parts	Sine	Parts
0	0	9.489982	1	10.510018	9.511776	1	10.488224	10.021794	1	9.978206	1	10.021794	1	9.978206	1
0	1	9.490177	1	10.509823	9.511991	1	10.488009	10.021814	1	9.978186	1	10.021814	1	9.978186	1
0	2	9.490371	2	10.509629	9.512206	2	10.487794	10.021835	2	9.978165	2	10.021835	2	9.978165	2
0	3	9.490565	3	10.509435	9.512420	3	10.487580	10.021855	3	9.978145	3	10.021855	3	9.978145	3
0	4	9.490759	4	10.509241	9.512635	4	10.487365	10.021876	4	9.978124	4	10.021876	4	9.978124	4
0	5	9.490953	5	10.509047	9.512850	5	10.487150	10.021896	5	9.978104	5	10.021896	5	9.978104	5
0	6	9.491147	6	10.508853	9.513064	6	10.486935	10.021917	6	9.978083	6	10.021917	6	9.978083	6
0	7	9.491341	7	10.508659	9.513278	7	10.486722	10.021937	7	9.978062	7	10.021937	7	9.978062	7
0	8	9.491535	8	10.508465	9.513493	8	10.486507	10.021958	8	9.978042	8	10.021958	8	9.978042	8
0	9	9.491728	9	10.508272	9.513707	9	10.486293	10.021979	9	9.978021	9	10.021979	9	9.978021	9
0	10	9.491922	10	10.508078	9.513921	10	10.486079	10.021999	10	9.978001	10	10.021999	10	9.978001	10
0	11	9.492115	11	10.507885	9.514135	11	10.485865	10.022020	11	9.977980	11	10.022020	11	9.977980	11
0	12	9.492308	12	10.507692	9.514349	12	10.485651	10.022041	12	9.977959	12	10.022041	12	9.977959	12
0	13	9.492502	13	10.507498	9.514563	13	10.485437	10.022061	13	9.977939	13	10.022061	13	9.977939	13
0	14	9.492695	14	10.507305	9.514777	14	10.485223	10.022082	14	9.977918	14	10.022082	14	9.977918	14
0	15	9.492888	15	10.507112	9.514990	15	10.485010	10.022103	15	9.977897	15	10.022103	15	9.977897	15
0	16	9.493081	16	10.506919	9.515204	16	10.484796	10.022124	16	9.977877	16	10.022124	16	9.977877	16
0	17	9.493273	17	10.506727	9.515417	17	10.484583	10.022144	17	9.977856	17	10.022144	17	9.977856	17
0	18	9.493466	18	10.506534	9.515631	18	10.484369	10.022165	18	9.977835	18	10.022165	18	9.977835	18
0	19	9.493659	19	10.506341	9.515844	19	10.484156	10.022185	19	9.977815	19	10.022185	19	9.977815	19
0	20	9.493851	20	10.506149	9.516057	20	10.483943	10.022206	20	9.977794	20	10.022206	20	9.977794	20
0	21	9.494044	21	10.505956	9.516271	21	10.483729	10.022227	21	9.977773	21	10.022227	21	9.977773	21
0	22	9.494236	22	10.505764	9.516484	22	10.483516	10.022248	22	9.977752	22	10.022248	22	9.977752	22
0	23	9.494428	23	10.505572	9.516697	23	10.483303	10.022268	23						

TABLE 68

775

LOG. SINES, COSINES, &c.

14°		18°											
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'
30	0	9°501476		10°498524	9°524520	10°475480	10°023043			9°976957	46	30	0
30	1	9°501665	1"	10°498335	9°524730	10°475270	10°023065		1"	9°976935	58	30	1
31	0	9°501854	2 12	10°498146	9°524940	10°475060	10°023086		2 1	9°976914	50	29	0
30	3	9°502042	3 19	10°497958	9°525149	10°474851	10°023107		3 2	9°976893	51	30	3
32	0	9°502231	4 25	10°497769	9°525359	10°474641	10°023128		4 3	9°976872	52	28	0
30	6	9°502419	5 31	10°497581	9°525568	10°474432	10°023149		5 4	9°976851	50	30	6
33	0	9°502607	6 37	10°497393	9°525778	10°474222	10°023170		6 4	9°976830	48	27	0
30	9	9°502796	7 44	10°497204	9°525987	10°474013	10°023192		7 5	9°976808	46	26	0
34	0	9°502984	8 50	10°497016	9°526197	10°473803	10°023213		8 6	9°976787	44	26	0
30	12	9°503172	9 56	10°496828	9°526406	10°473594	10°023234		9 6	9°976766	42	30	12
35	0	9°503360	10 62	10°496640	9°526615	10°473385	10°023255		10 7	9°976745	40	25	0
30	15	9°503548	11 69	10°496452	9°526824	10°473176	10°023277		11 8	9°976723	38	30	15
36	0	9°503735	12 75	10°496265	9°527033	10°472967	10°023298		12 9	9°976702	36	24	0
30	18	9°503923	13 81	10°496077	9°527242	10°472758	10°023319		13 9	9°976681	34	30	18
37	0	9°504110	14 87	10°495890	9°527451	10°472549	10°023340		14 10	9°976660	32	23	0
30	21	9°504298	15 94	10°495702	9°527660	10°472340	10°023362		15 11	9°976638	30	30	21
38	0	9°504485	16 100	10°495515	9°527868	10°472132	10°023383		16 11	9°976617	28	22	0
30	24	9°504673	17 106	10°495327	9°528077	10°471923	10°023404		17 12	9°976596	26	30	24
39	0	9°504860	18 112	10°495140	9°528285	10°471715	10°023426		18 13	9°976574	24	21	0
30	27	9°505047	19 119	10°494953	9°528494	10°471506	10°023447		19 13	9°976553	22	30	27
40	0	9°505234	20 125	10°494766	9°528702	10°471298	10°023468		20 14	9°976532	20	20	0
30	30	9°505421	21 131	10°494579	9°528910	10°471090	10°023490		21 15	9°976510	18	30	30
41	0	9°505608	22 137	10°494392	9°529119	10°470881	10°023511		22 16	9°976489	16	19	0
30	33	9°505794	23 144	10°494206	9°529327	10°470673	10°023532		23 16	9°976468	14	30	33
42	0	9°505981	24 150	10°494019	9°529535	10°470465	10°023554		24 17	9°976446	12	18	0
30	36	9°506168	25 156	10°493832	9°529743	10°470257	10°023575		25 18	9°976425	10	30	36
43	0	9°506354	26 162	10°493646	9°529951	10°470049	10°023596		26 18	9°976404	8	17	0
30	39	9°506541	27 169	10°493459	9°530158	10°469842	10°023618		27 19	9°976382	6	30	39
44	0	9°506727	28 175	10°493273	9°530366	10°469634	10°023639		28 20	9°976361	4	16	0
30	42	9°506913	29 181	10°493087	9°530574	10°469426	10°023661		29 21	9°976339	2	30	42
45	0	9°507099	30 187	10°492901	9°530781	10°469219	10°023682		30 21	9°976318	0	15	0
30	45	9°507285	1 6	10°492715	9°530989	10°469011	10°023704		1 1	9°976296	58	30	45
46	0	9°507471	2 12	10°492529	9°531196	10°468804	10°023725		2 1	9°976275	54	14	0
30	48	9°507657	3 18	10°492343	9°531403	10°468597	10°023746		3 2	9°976254	51	30	48
47	0	9°507843	4 25	10°492157	9°531611	10°468389	10°023768		4 3	9°976232	48	13	0
30	51	9°508028	5 31	10°491972	9°531818	10°468182	10°023789		5 4	9°976211	50	30	51
48	0	9°508214	6 37	10°491786	9°532025	10°467975	10°023811		6 4	9°976189	48	12	0
30	54	9°508400	7 43	10°491600	9°532232	10°467768	10°023832		7 5	9°976168	46	30	54
49	0	9°508585	8 49	10°491415	9°532439	10°467561	10°023854		8 6	9°976146	44	11	0
30	57	9°508770	9 55	10°491230	9°532646	10°467354	10°023875		9 6	9°976125	42	30	57
50	0	9°508956	10 62	10°491044	9°532853	10°467147	10°023897		10 7	9°976103	40	10	0
30	60	9°509141	11 68	10°490859	9°533059	10°466941	10°023919		11 8	9°976081	38	30	60
51	0	9°509326	12 74	10°490674	9°533266	10°466734	10°023940		12 9	9°976060	36	9	0
30	63	9°509511	13 80	10°490489	9°533472	10°466528	10°023962		13 9	9°976038	31	30	63
52	0	9°509696	14 86	10°490304	9°533679	10°466321	10°023983		14 10	9°976017	32	8	0
30	66	9°509880	15 92	10°490120	9°533885	10°466115	10°024005		15 11	9°975995	30	30	66
53	0	9°510065	16 99	10°489935	9°534092	10°465908	10°024026		16 12	9°975974	28	7	0
30	69	9°510250	17 105	10°489750	9°534298	10°465702	10°024048		17 12	9°975952	26	30	69
54	0	9°510434	18 111	10°489566	9°534504	10°465496	10°024070		18 13	9°975930	24	6	0
30	72	9°510619	19 117	10°489381	9°534710	10°465290	10°024091		19 14	9°975909	22	30	72
55	0	9°510803	20 123	10°489197	9°534916	10°465084	10°024113		20 14	9°975887	20	5	0
30	75	9°510987	21 129	10°489013	9°535122	10°464878	10°024135		21 15	9°975865	18	30	75
56	0	9°511172	22 135	10°488828	9°535328	10°464672	10°024156		22 16	9°975844	16	4	0
30	78	9°511356	23 142	10°488644	9°535534	10°464466	10°024178		23 17	9°975822	14	30	78
57	0	9°511540	24 148	10°488460	9°535739	10°464261	10°024200		24 17	9°975800	12	3	0
30	81	9°511724	25 154	10°488276	9°535945	10°464055	10°024221		25 18	9°975779	10	30	81
58	0	9°511907	26 160	10°488093	9°536150	10°463850	10°024243		26 19	9°975757	8	2	0
30	84	9°512091	27 166	10°487909	9°536356	10°463644	10°024265		27 19	9°975735	6	30	84
59	0	9°512275	28 172	10°487725	9°536561	10°463439	10°024286		28 20	9°975714	4	1	0
30	87	9°512458	29 179	10°487542	9°536767	10°463233	10°024308		29 21	9°975692	2	30	87
60	0	9°512642	30 185	10°487358	9°536972	10°463028	10°024330		30 22	9°975670	0	0	0

71°

44° 44'

LOG. SINES, COSINES, &c.

1 ^h 16 ^m				19 ^o							
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	°
0	0	9.512642		10.487358	9.536972		10.463028	10.024330		9.975670	0
30	2	9.512825	1 ^m 6	10.487175	9.537177	1 ^m 7	10.462823	10.024352	1 ^m 1	9.975648	30
1	4	9.513009	2 12	10.486991	9.537382	2 14	10.462618	10.024373	2 1	9.975627	30
30	6	9.513192	3 18	10.486808	9.537587	3 20	10.462413	10.024395	3 2	9.975605	30
2	10	9.513375	4 24	10.486625	9.537792	4 27	10.462208	10.024417	4 3	9.975583	30
30	12	9.513558	5 30	10.486442	9.537997	5 34	10.462003	10.024439	5 4	9.975561	30
3	12	9.513741	6 36	10.486259	9.538202	6 41	10.461798	10.024461	6 4	9.975539	30
30	14	9.513924	7 43	10.486076	9.538406	7 48	10.461594	10.024482	7 5	9.975518	30
4	16	9.514107	8 49	10.485893	9.538611	8 54	10.461389	10.024504	8 6	9.975496	41
30	18	9.514289	9 55	10.485711	9.538816	9 61	10.461184	10.024526	9 7	9.975474	30
5	20	9.514472	10 61	10.485528	9.539020	10 68	10.460980	10.024548	10 7	9.975452	30
30	22	9.514655	11 67	10.485345	9.539224	11 75	10.460776	10.024570	11 8	9.975430	30
6	24	9.514837	12 73	10.485163	9.539429	12 82	10.460571	10.024592	12 9	9.975408	30
30	26	9.515019	13 79	10.484981	9.539633	13 88	10.460367	10.024614	13 9	9.975386	30
7	28	9.515202	14 85	10.484798	9.539837	14 95	10.460163	10.024635	14 10	9.975365	30
30	30	9.515384	15 91	10.484616	9.540041	15 102	10.459959	10.024657	15 11	9.975343	30
8	32	9.515566	16 97	10.484434	9.540245	16 109	10.459755	10.024679	16 12	9.975321	30
30	34	9.515748	17 103	10.484252	9.540449	17 116	10.459551	10.024701	17 12	9.975299	30
9	36	9.515930	18 109	10.484070	9.540653	18 122	10.459347	10.024723	18 13	9.975277	30
30	38	9.516112	19 115	10.483888	9.540857	19 129	10.459143	10.024745	19 14	9.975255	30
10	40	9.516294	20 121	10.483706	9.541061	20 136	10.458939	10.024767	20 15	9.975233	30
30	42	9.516475	21 127	10.483525	9.541264	21 143	10.458736	10.024789	21 15	9.975211	30
11	44	9.516657	22 134	10.483343	9.541468	22 150	10.458532	10.024811	22 16	9.975189	30
30	46	9.516838	23 140	10.483162	9.541671	23 156	10.458329	10.024833	23 17	9.975167	30
12	48	9.517020	24 146	10.482980	9.541875	24 163	10.458125	10.024855	24 18	9.975145	30
30	50	9.517201	25 152	10.482799	9.542078	25 170	10.457922	10.024877	25 18	9.975123	30
13	52	9.517382	26 158	10.482618	9.542281	26 177	10.457719	10.024899	26 19	9.975101	30
30	54	9.517564	27 164	10.482436	9.542485	27 184	10.457515	10.024921	27 20	9.975079	30
14	56	9.517745	28 170	10.482255	9.542688	28 190	10.457312	10.024943	28 20	9.975057	30
30	58	9.517926	29 176	10.482074	9.542891	29 197	10.457109	10.024965	29 21	9.975035	30
15	59	9.518107	30 182	10.481893	9.543094	30 204	10.456906	10.024987	30 22	9.975013	30
30	2	9.518287	1 6	10.481713	9.543297	1 7	10.456703	10.025009	1 1	9.974991	30
16	4	9.518468	2 12	10.481532	9.543499	2 13	10.456501	10.025031	2 1	9.974969	30
30	6	9.518649	3 18	10.481351	9.543702	3 20	10.456298	10.025053	3 2	9.974947	30
17	8	9.518829	4 24	10.481171	9.543905	4 27	10.456095	10.025075	4 3	9.974925	30
30	10	9.519010	5 30	10.480990	9.544107	5 34	10.455893	10.025098	5 4	9.974903	30
18	12	9.519190	6 36	10.480810	9.544310	6 40	10.455690	10.025120	6 4	9.974880	30
30	14	9.519371	7 42	10.480629	9.544512	7 47	10.455488	10.025142	7 5	9.974858	30
19	16	9.519551	8 48	10.480449	9.544715	8 54	10.455285	10.025164	8 6	9.974836	30
30	18	9.519731	9 54	10.480269	9.544917	9 61	10.455083	10.025186	9 7	9.974814	30
20	20	9.519911	10 60	10.480089	9.545119	10 67	10.454881	10.025208	10 7	9.974792	30
30	22	9.520091	11 66	10.479909	9.545322	11 74	10.454678	10.025230	11 8	9.974770	30
21	24	9.520271	12 72	10.479729	9.545524	12 81	10.454476	10.025252	12 9	9.974748	30
30	26	9.520451	13 78	10.479549	9.545726	13 87	10.454274	10.025275	13 10	9.974725	30
22	28	9.520631	14 84	10.479369	9.545928	14 94	10.454072	10.025297	14 10	9.974703	30
30	30	9.520810	15 90	10.479190	9.546129	15 101	10.453871	10.025319	15 11	9.974681	30
23	32	9.520990	16 96	10.479010	9.546331	16 108	10.453669	10.025341	16 12	9.974659	30
30	34	9.521169	17 102	10.478831	9.546533	17 114	10.453467	10.025364	17 13	9.974637	30
24	36	9.521349	18 108	10.478651	9.546735	18 121	10.453265	10.025386	18 13	9.974614	30
30	38	9.521528	19 114	10.478472	9.546936	19 128	10.453064	10.025408	19 14	9.974592	30
25	40	9.521708	20 120	10.478293	9.547138	20 135	10.452862	10.025430	20 15	9.974570	30
30	42	9.521887	21 126	10.478113	9.547339	21 141	10.452661	10.025453	21 16	9.974547	30
26	44	9.522066	22 132	10.477934	9.547540	22 148	10.452460	10.025475	22 16	9.974525	30
30	46	9.522245	23 138	10.477755	9.547742	23 155	10.452258	10.025497	23 17	9.974503	30
27	48	9.522424	24 144	10.477576	9.547943	24 162	10.452057	10.025519	24 18	9.974481	30
30	50	9.522602	25 150	10.477398	9.548144	25 168	10.451856	10.025542	25 18	9.974459	30
28	52	9.522781	26 156	10.477219	9.548345	26 175	10.451655	10.025564	26 19	9.974436	30
30	54	9.522960	27 162	10.477040	9.548546	27 182	10.451454	10.025586	27 20	9.974414	30
29	56	9.523138	28 168	10.476862	9.548747	28 188	10.451253	10.025609	28 21	9.974391	30
30	58	9.523317	29 174	10.476683	9.548948	29 195	10.451052	10.025631	29 21	9.974369	30
30	59	9.523495	30 180	10.476505	9.549149	30 202	10.450851	10.025653	30 22	9.974347	30
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	°

71^o

4^h 42^m

LOG. SINES, COSINES, &c.

18°										19°									
''	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	''	m.	''					
30	0	9°523495		10°476505	9°549149		10°450851	10°025553		9°974347	42	30							
30	2	9°523674	1'' 6	10°476326	9°549349	1'' 7	10°450651	10°025676	1'' 1	9°974324	38	31							
31	4	9°523852	2 12	10°476148	9°549550	2 13	10°450450	10°025698	2 1	9°974302	34	32							
31	6	9°524030	3 18	10°475970	9°549751	3 20	10°450249	10°025721	3 2	9°974279	31	33							
32	8	9°524208	4 24	10°475792	9°549951	4 27	10°450049	10°025743	4 3	9°974257	28	34							
32	10	9°524386	5 30	10°475614	9°550152	5 33	10°449848	10°025765	5 4	9°974235	25	35							
33	12	9°524564	6 35	10°475436	9°550352	6 40	10°449648	10°025788	6 4	9°974212	22	36							
33	14	9°524742	7 41	10°475258	9°550552	7 47	10°449448	10°025810	7 5	9°974190	19	37							
34	16	9°524920	8 47	10°475080	9°550752	8 53	10°449248	10°025833	8 6	9°974167	16	38							
34	18	9°525097	9 53	10°474903	9°550952	9 60	10°449048	10°025855	9 7	9°974145	13	39							
35	20	9°525275	10 59	10°474725	9°551153	10 66	10°448847	10°025878	10 7	9°974122	10	40							
35	22	9°525452	11 65	10°474548	9°551353	11 73	10°448647	10°025900	11 8	9°974100	8	41							
36	24	9°525630	12 71	10°474370	9°551552	12 80	10°448448	10°025923	12 9	9°974077	5	42							
36	26	9°525807	13 77	10°474193	9°551752	13 86	10°448248	10°025945	13 10	9°974055	3	43							
37	28	9°525984	14 83	10°474016	9°551952	14 93	10°448048	10°025968	14 10	9°974032	2	44							
37	30	9°526162	15 89	10°473838	9°552152	15 98	10°447848	10°025990	15 11	9°974010	0	45							
38	32	9°526339	16 94	10°473661	9°552351	16 106	10°447649	10°026013	16 12	9°973987	0	46							
38	34	9°526516	17 100	10°473484	9°552551	17 113	10°447449	10°026035	17 13	9°973965	0	47							
39	36	9°526693	18 106	10°473307	9°552750	18 120	10°447250	10°026058	18 13	9°973942	0	48							
39	38	9°526870	19 112	10°473130	9°552950	19 126	10°447050	10°026080	19 14	9°973920	0	49							
40	40	9°527046	20 118	10°472954	9°553149	20 133	10°446851	10°026103	20 15	9°973897	0	50							
40	42	9°527223	21 124	10°472777	9°553348	21 140	10°446652	10°026126	21 16	9°973875	0	51							
41	44	9°527400	22 130	10°472600	9°553548	22 146	10°446452	10°026148	22 16	9°973852	0	52							
41	46	9°527576	23 136	10°472424	9°553747	23 153	10°446253	10°026171	23 17	9°973829	0	53							
42	48	9°527753	24 142	10°472247	9°553946	24 160	10°446054	10°026193	24 18	9°973807	0	54							
42	50	9°527929	25 148	10°472071	9°554145	25 166	10°445855	10°026216	25 19	9°973784	0	55							
43	52	9°528105	26 153	10°471895	9°554344	26 173	10°445656	10°026239	26 19	9°973761	0	56							
43	54	9°528282	27 159	10°471718	9°554543	27 180	10°445457	10°026261	27 20	9°973739	0	57							
44	56	9°528458	28 165	10°471542	9°554741	28 186	10°445259	10°026284	28 21	9°973716	0	58							
44	58	9°528634	29 171	10°471366	9°554940	29 193	10°445060	10°026307	29 22	9°973694	0	59							
45	60	9°528810	30 177	10°471190	9°555139	30 199	10°444861	10°026329	30 22	9°973671	0	60							
45	2	9°528986	1 6	10°471014	9°555337	1 7	10°444663	10°026352	1 1	9°973648	0	61							
46	4	9°529161	2 12	10°470837	9°555536	2 13	10°444464	10°026375	2 2	9°973625	0	62							
46	6	9°529337	3 17	10°470663	9°555734	3 20	10°444266	10°026397	3 2	9°973603	0	63							
47	8	9°529513	4 23	10°470487	9°555933	4 26	10°444067	10°026420	4 3	9°973580	0	64							
47	10	9°529688	5 29	10°470312	9°556131	5 33	10°443869	10°026443	5 4	9°973557	0	65							
48	12	9°529864	6 35	10°470136	9°556329	6 40	10°443671	10°026465	6 5	9°973535	0	66							
48	14	9°530039	7 41	10°469961	9°556527	7 46	10°443473	10°026488	7 5	9°973512	0	67							
49	16	9°530215	8 47	10°469785	9°556725	8 53	10°443275	10°026511	8 6	9°973489	0	68							
49	18	9°530390	9 52	10°469610	9°556923	9 59	10°443077	10°026534	9 7	9°973466	0	69							
50	20	9°530565	10 58	10°469435	9°557121	10 66	10°442879	10°026556	10 8	9°973444	0	70							
50	22	9°530740	11 64	10°469260	9°557319	11 72	10°442681	10°026579	11 8	9°973421	0	71							
51	24	9°530915	12 70	10°469085	9°557517	12 79	10°442483	10°026602	12 9	9°973398	0	72							
51	26	9°531090	13 76	10°468910	9°557715	13 86	10°442285	10°026625	13 10	9°973375	0	73							
52	28	9°531265	14 81	10°468735	9°557913	14 92	10°442087	10°026648	14 10	9°973352	0	74							
52	30	9°531440	15 87	10°468560	9°558110	15 99	10°441890	10°026671	15 11	9°973330	0	75							
53	32	9°531614	16 93	10°468386	9°558308	16 105	10°441692	10°026693	16 12	9°973307	0	76							
53	34	9°531789	17 99	10°468211	9°558505	17 112	10°441495	10°026716	17 13	9°973284	0	77							
54	36	9°531963	18 105	10°468037	9°558703	18 119	10°441297	10°026739	18 14	9°973261	0	78							
54	38	9°532138	19 111	10°467862	9°558900	19 125	10°441100	10°026762	19 14	9°973238	0	79							
55	40	9°532312	20 117	10°467688	9°559097	20 132	10°440903	10°026785	20 15	9°973215	0	80							
55	42	9°532487	21 123	10°467513	9°559294	21 138	10°440706	10°026808	21 16	9°973192	0	81							
56	44	9°532661	22 128	10°467339	9°559491	22 145	10°440509	10°026831	22 17	9°973169	0	82							
56	46	9°532835	23 134	10°467165	9°559688	23 152	10°440312	10°026854	23 17	9°973146	0	83							
57	48	9°533009	24 140	10°466991	9°559885	24 158	10°440115	10°026877	24 18	9°973124	0	84							
57	50	9°533183	25 146	10°466817	9°560082	25 165	10°439918	10°026899	25 19	9°973101	0	85							
58	52	9°533357	26 152	10°466643	9°560279	26 171	10°439721	10°026922	26 20	9°973078	0	86							
58	54	9°533531	27 158	10°466469	9°560476	27 178	10°439524	10°026945	27 21	9°973055	0	87							
59	56	9°533704	28 164	10°466296	9°560673	28 185	10°439327	10°026968	28 21	9°973032	0	88							
59	58	9°533878	29 169	10°466122	9°560869	29 191	10°439131	10°026991	29 22	9°973009	0	89							
60	60	9°534052	30 175	10°465948	9°561066	30 198	10°438934	10°027014	30 23	9°972986	0	90							
''	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	''							

LOG. SINES, COSINES, &c.											
1° 20'						20°					
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	°
0	0	9°54052		10°465948	9°561066		10°438934	10°027014		9°972986	60
30	2	9°534225	1° 6	10°465775	9°561262	1° 7	10°438738	10°027037	1° 1	9°972963	58
1	4	9°534399	2 11	10°465601	9°561459	2 13	10°438541	10°027060	2 2	9°972940	56
30	6	9°534572	3 17	10°465428	9°561655	3 20	10°438345	10°027083	3 2	9°972917	54
2	8	9°534745	4 23	10°465255	9°561851	4 26	10°438149	10°027106	4 3	9°972894	52
30	10	9°534918	5 29	10°465082	9°562048	5 33	10°437953	10°027129	5 4	9°972871	50
3	12	9°535092	6 34	10°464908	9°562244	6 39	10°437756	10°027152	6 5	9°972848	48
30	14	9°535265	7 40	10°464735	9°562440	7 46	10°437560	10°027175	7 5	9°972825	46
4	16	9°535438	8 46	10°464562	9°562636	8 52	10°437364	10°027198	8 6	9°972802	44
30	18	9°535610	9 52	10°464390	9°562832	9 59	10°437168	10°027222	9 7	9°972778	42
5	20	9°535783	10 57	10°464217	9°563028	10 65	10°436972	10°027245	10 8	9°972755	40
6	22	9°535956	11 63	10°464044	9°563224	11 72	10°436776	10°027268	11 8	9°972732	38
30	24	9°536129	12 69	10°463871	9°563419	12 78	10°436581	10°027291	12 9	9°972709	36
7	26	9°536301	13 75	10°463699	9°563615	13 85	10°436385	10°027314	13 10	9°972686	34
30	28	9°536474	14 80	10°463526	9°563811	14 91	10°436189	10°027337	14 11	9°972663	32
8	30	9°536646	15 86	10°463354	9°564006	15 98	10°435994	10°027360	15 12	9°972640	30
9	32	9°536818	16 92	10°463182	9°564202	16 104	10°435798	10°027383	16 12	9°972617	28
30	34	9°536991	17 98	10°463009	9°564397	17 111	10°435603	10°027407	17 13	9°972593	26
10	36	9°537163	18 103	10°462837	9°564593	18 117	10°435407	10°027430	18 14	9°972570	24
30	38	9°537335	19 109	10°462665	9°564788	19 124	10°435212	10°027453	19 15	9°972547	22
11	40	9°537507	20 115	10°462493	9°564983	20 130	10°435017	10°027476	20 15	9°972524	20
12	42	9°537679	21 121	10°462321	9°565178	21 137	10°434822	10°027499	21 16	9°972501	18
30	44	9°537851	22 126	10°462149	9°565373	22 143	10°434627	10°027522	22 17	9°972478	16
13	46	9°538023	23 132	10°461977	9°565568	23 150	10°434432	10°027546	23 18	9°972454	14
30	48	9°538194	24 138	10°461806	9°565763	24 156	10°434237	10°027569	24 18	9°972431	12
14	50	9°538366	25 144	10°461634	9°565958	25 163	10°434042	10°027592	25 19	9°972408	10
15	52	9°538538	26 149	10°461462	9°566153	26 170	10°433847	10°027615	26 20	9°972385	8
30	54	9°538709	27 155	10°461291	9°566348	27 176	10°433652	10°027639	27 21	9°972361	6
16	56	9°538880	28 161	10°461120	9°566542	28 183	10°433458	10°027662	28 22	9°972338	4
30	58	9°539052	29 167	10°460948	9°566737	29 189	10°433263	10°027685	29 22	9°972315	2
17	60	9°539223	30 172	10°460777	9°566932	30 196	10°433068	10°027709	30 23	9°972291	0
18	2	9°539394	1 6	10°460606	9°567126	1 6	10°432874	10°027732	1 1	9°972268	58
30	4	9°539565	2 11	10°460435	9°567320	2 13	10°432680	10°027755	2 2	9°972245	56
19	6	9°539736	3 17	10°460264	9°567515	3 19	10°432485	10°027779	3 2	9°972221	54
30	8	9°539907	4 23	10°460093	9°567709	4 26	10°432291	10°027802	4 3	9°972198	52
20	10	9°540078	5 28	10°459922	9°567903	5 32	10°432097	10°027825	5 4	9°972175	50
21	12	9°540249	6 34	10°459751	9°568098	6 39	10°431902	10°027849	6 5	9°972151	48
30	14	9°540420	7 40	10°459580	9°568292	7 45	10°431708	10°027872	7 5	9°972128	46
22	16	9°540590	8 45	10°459410	9°568486	8 52	10°431514	10°027895	8 6	9°972105	44
30	18	9°540761	9 51	10°459239	9°568680	9 58	10°431320	10°027919	9 7	9°972081	42
23	20	9°540931	10 57	10°459069	9°568873	10 64	10°431127	10°027942	10 8	9°972058	40
24	22	9°541102	11 62	10°458898	9°569067	11 71	10°430933	10°027966	11 9	9°972034	38
30	24	9°541272	12 68	10°458728	9°569261	12 77	10°430739	10°027989	12 9	9°972011	36
25	26	9°541442	13 74	10°458558	9°569455	13 84	10°430545	10°028012	13 10	9°971988	34
30	28	9°541613	14 79	10°458387	9°569648	14 90	10°430352	10°028036	14 11	9°971964	32
26	30	9°541783	15 85	10°458217	9°569842	15 97	10°430158	10°028059	15 12	9°971941	30
27	32	9°541953	16 91	10°458047	9°570035	16 103	10°429965	10°028083	16 12	9°971917	28
30	34	9°542123	17 96	10°457877	9°570229	17 110	10°429771	10°028106	17 13	9°971894	26
28	36	9°542293	18 102	10°457707	9°570422	18 116	10°429578	10°028130	18 14	9°971870	24
30	38	9°542462	19 108	10°457538	9°570616	19 123	10°429384	10°028153	19 15	9°971847	22
29	40	9°542632	20 113	10°457368	9°570809	20 129	10°429191	10°028177	20 16	9°971823	20
30	42	9°542802	21 119	10°457198	9°571002	21 135	10°428998	10°028200	21 16	9°971800	18
31	44	9°542971	22 125	10°457029	9°571195	22 142	10°428805	10°028224	22 17	9°971776	16
30	46	9°543141	23 130	10°456859	9°571388	23 148	10°428612	10°028247	23 18	9°971753	14
32	48	9°543310	24 136	10°456690	9°571581	24 155	10°428419	10°028271	24 19	9°971729	12
30	50	9°543480	25 142	10°456520	9°571774	25 161	10°428226	10°028294	25 19	9°971706	10
33	52	9°543649	26 147	10°456351	9°571967	26 168	10°428033	10°028318	26 20	9°971682	8
30	54	9°543818	27 153	10°456182	9°572160	27 174	10°427840	10°028342	27 21	9°971658	6
34	56	9°543987	28 159	10°456013	9°572352	28 181	10°427648	10°028365	28 22	9°971635	4
30	58	9°544156	29 164	10°455844	9°572545	29 187	10°427455	10°028389	29 23	9°971611	2
35	60	9°544325	30 170	10°455675	9°572738	30 193	10°427262	10°028412	30 23	9°971588	0
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	°

TABLE 68.

779

LOG. SINES, COSINES, &c

1 ^h 22 ^m		20°										20°	
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	°	'
30	0	9°544325		10°455675	9°572738		10°427262	10°028412		9°971588	30	30	0
30	1	9°544494	1"	10°455506	9°572930	1"	10°427070	10°028436	1"	9°971564	58	30	1
31	2	9°544663	2 11	10°455337	9°573123	2 13	10°426877	10°028460	2 2	9°971540	50	29	2
31	3	9°544832	3 17	10°455168	9°573315	3 19	10°426685	10°028483	3 2	9°971517	51	30	3
32	4	9°545000	4 22	10°455000	9°573507	4 26	10°426493	10°028507	4 3	9°971493	52	28	4
32	5	9°545169	5 28	10°454831	9°573700	5 32	10°426300	10°028531	5 4	9°971469	50	30	5
33	6	9°545338	6 34	10°454662	9°573892	6 38	10°426108	10°028554	6 5	9°971446	48	27	6
33	7	9°545506	7 39	10°454494	9°574084	7 45	10°425916	10°028578	7 6	9°971422	46	30	7
34	8	9°545674	8 45	10°454326	9°574276	8 51	10°425724	10°028602	8 6	9°971398	44	26	8
34	9	9°545843	9 50	10°454157	9°574468	9 58	10°425532	10°028625	9 7	9°971375	42	30	9
35	10	9°546011	10 56	10°453989	9°574660	10 64	10°425340	10°028649	10 8	9°971351	40	25	10
35	11	9°546179	11 61	10°453821	9°574852	11 70	10°425148	10°028673	11 9	9°971327	38	30	11
36	12	9°546347	12 67	10°453653	9°575044	12 77	10°424956	10°028697	12 9	9°971303	36	24	12
36	13	9°546515	13 72	10°453485	9°575236	13 83	10°424764	10°028720	13 10	9°971280	34	30	13
37	14	9°546683	14 78	10°453317	9°575427	14 89	10°424573	10°028744	14 11	9°971256	32	23	14
37	15	9°546851	15 84	10°453149	9°575619	15 96	10°424381	10°028768	15 12	9°971232	30	30	15
38	16	9°547019	16 90	10°452981	9°575810	16 102	10°424190	10°028792	16 13	9°971208	28	22	16
38	17	9°547187	17 95	10°452813	9°576002	17 109	10°423998	10°028815	17 13	9°971185	26	30	17
39	18	9°547354	18 101	10°452646	9°576193	18 115	10°423807	10°028839	18 14	9°971161	24	21	18
39	19	9°547522	19 107	10°452478	9°576385	19 121	10°423615	10°028863	19 15	9°971137	22	30	19
40	20	9°547689	20 112	10°452311	9°576576	20 128	10°423424	10°028887	20 16	9°971113	20	20	20
40	21	9°547857	21 118	10°452143	9°576767	21 134	10°423233	10°028911	21 17	9°971089	18	30	21
41	22	9°548024	22 123	10°451976	9°576959	22 141	10°423041	10°028934	22 17	9°971066	16	19	22
41	23	9°548191	23 129	10°451809	9°577150	23 147	10°422850	10°028958	23 18	9°971042	14	30	23
42	24	9°548359	24 134	10°451641	9°577341	24 153	10°422659	10°028982	24 19	9°971018	12	18	24
42	25	9°548526	25 140	10°451474	9°577532	25 160	10°422468	10°029006	25 20	9°970994	10	30	25
43	26	9°548693	26 145	10°451307	9°577723	26 166	10°422277	10°029030	26 21	9°970970	8	17	26
43	27	9°548860	27 151	10°451140	9°577914	27 173	10°422086	10°029054	27 21	9°970946	6	30	27
44	28	9°549027	28 156	10°450973	9°578104	28 179	10°421896	10°029078	28 22	9°970922	4	16	28
44	29	9°549193	29 162	10°450807	9°578295	29 185	10°421705	10°029102	29 23	9°970898	2	30	29
45	30	9°549360	30 168	10°450640	9°578486	30 192	10°421514	10°029126	30 24	9°970874	2	15	30
45	31	9°549527	1 6	10°450473	9°578676	1 6	10°421324	10°029150	1 1	9°970850	58	30	31
46	2	9°549693	2 11	10°450307	9°578867	2 13	10°421133	10°029173	2 2	9°970827	56	14	46
46	3	9°549860	3 17	10°450140	9°579057	3 19	10°420943	10°029197	3 2	9°970803	54	30	47
47	4	9°550026	4 22	10°449974	9°579248	4 25	10°420752	10°029221	4 3	9°970779	52	13	48
47	5	9°550193	5 28	10°449807	9°579438	5 32	10°420562	10°029245	5 4	9°970755	50	30	49
48	6	9°550359	6 33	10°449641	9°579629	6 38	10°420371	10°029269	6 5	9°970731	48	12	50
48	7	9°550525	7 39	10°449475	9°579819	7 44	10°420181	10°029293	7 6	9°970707	46	30	51
49	8	9°550692	8 44	10°449308	9°580009	8 51	10°419991	10°029317	8 6	9°970683	44	11	52
49	9	9°550858	9 50	10°449142	9°580199	9 57	10°419801	10°029341	9 7	9°970659	42	30	53
50	10	9°551024	10 55	10°448976	9°580389	10 63	10°419611	10°029365	10 8	9°970635	40	10	54
50	11	9°551190	11 0	10°448810	9°580579	11 70	10°419421	10°029389	11 9	9°970611	38	30	55
51	12	9°551356	12 66	10°448644	9°580769	12 76	10°419231	10°029414	12 10	9°970586	36	9	56
51	13	9°551521	13 72	10°448479	9°580959	13 82	10°419041	10°029438	13 10	9°970562	34	30	57
52	14	9°551687	14 77	10°448313	9°581149	14 88	10°418851	10°029462	14 11	9°970538	32	8	58
52	15	9°551853	15 83	10°448147	9°581339	15 95	10°418661	10°029486	15 12	9°970514	30	30	59
53	16	9°552018	16 88	10°447982	9°581528	16 101	10°418472	10°029510	16 13	9°970490	28	7	60
53	17	9°552184	17 94	10°447816	9°581718	17 107	10°418282	10°029534	17 14	9°970466	26	30	61
54	18	9°552349	18 99	10°447651	9°581907	18 114	10°418093	10°029558	18 14	9°970442	24	6	62
54	19	9°552515	19 105	10°447485	9°582097	19 120	10°417903	10°029582	19 15	9°970418	22	30	63
55	20	9°552680	20 110	10°447320	9°582286	20 126	10°417714	10°029606	20 16	9°970394	20	5	64
55	21	9°552845	21 116	10°447155	9°582476	21 133	10°417524	10°029630	21 17	9°970370	18	30	65
56	22	9°553010	22 121	10°446990	9°582665	22 139	10°417335	10°029655	22 18	9°970345	16	4	66
56	23	9°553176	23 127	10°446824	9°582854	23 145	10°417146	10°029679	23 18	9°970321	14	30	67
57	24	9°553341	24 132	10°446659	9°583044	24 152	10°416956	10°029703	24 19	9°970297	12	3	68
57	25	9°553506	25 138	10°446494	9°583233	25 158	10°416767	10°029727	25 20	9°970273	10	30	69
58	26	9°553670	26 143	10°446330	9°583422	26 164	10°416578	10°029751	26 21	9°970249	8	2	70
58	27	9°553835	27 149	10°446165	9°583611	27 171	10°416389	10°029776	27 22	9°970224	6	30	71
59	28	9°554000	28 154	10°446000	9°583800	28 177	10°416200	10°029800	28 23	9°970200	4	1	72
59	29	9°554165	29 160	10°445835	9°583989	29 183	10°416011	10°029824	29 23	9°970176	2	30	73
60	30	9°554329	30 166	10°445671	9°584177	30 190	10°415823	10°029848	30 24	9°970152	0	0	74
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	°	'

LOG. SINES, COSINES, &c.													
1° 20'							20°						
'''	min.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	min.	'''	'''
0	8	9°544052		10°461948	9°561066		10°438934	10°027014		9°972986	40	60	
30	2	9°543225	1° 6	10°465775	9°561262	1° 7	10°437838	10°027037	1° 1	9°972963	58	38	
1	4	9°543499	2 11	10°465601	9°561459	2 13	10°438541	10°027060	2 2	9°972940	56	59	
30	6	9°543572	3 17	10°465428	9°561655	3 20	10°438345	10°027083	3 2	9°972917	54	30	
2	8	9°543745	4 23	10°465255	9°561851	4 26	10°438149	10°027106	4 3	9°972894	52	88	
30	10	9°543918	5 29	10°465082	9°562048	5 33	10°437952	10°027129	5 4	9°972871	50	38	
3	12	9°545092	6 34	10°464908	9°562244	6 39	10°437756	10°027152	6 5	9°972848	48	57	
30	14	9°545265	7 40	10°464735	9°562440	7 46	10°437560	10°027175	7 5	9°972825	46	38	
4	16	9°545438	8 46	10°464562	9°562636	8 52	10°437364	10°027198	8 6	9°972802	44	56	
30	18	9°545610	9 52	10°464390	9°562832	9 59	10°437168	10°027222	9 7	9°972778	42	38	
5	20	9°545783	10 57	10°464217	9°563028	10 65	10°436972	10°027245	10 8	9°972755	40	56	
30	22	9°545956	11 63	10°464044	9°563224	11 72	10°436776	10°027268	11 8	9°972732	38	38	
6	24	9°546129	12 69	10°463871	9°563419	12 78	10°436581	10°027291	12 9	9°972709	36	54	
30	26	9°546301	13 75	10°463699	9°563615	13 85	10°436385	10°027314	13 10	9°972686	34	38	
7	28	9°546474	14 80	10°463526	9°563811	14 91	10°436189	10°027337	14 11	9°972663	32	83	
30	30	9°546646	15 86	10°463354	9°564006	15 98	10°435994	10°027360	15 12	9°972640	30	38	
8	32	9°546818	16 92	10°463182	9°564202	16 104	10°435798	10°027383	16 12	9°972617	28	52	
30	34	9°546991	17 98	10°463009	9°564397	17 111	10°435603	10°027407	17 13	9°972593	26	38	
9	36	9°547163	18 103	10°462837	9°564593	18 117	10°435407	10°027430	18 14	9°972570	24	51	
30	38	9°547335	19 109	10°462665	9°564788	19 124	10°435212	10°027453	19 15	9°972547	22	38	
10	40	9°547507	20 115	10°462493	9°564983	20 130	10°435017	10°027476	20 15	9°972524	20	80	
30	42	9°547679	21 121	10°462321	9°565178	21 137	10°434822	10°027499	21 16	9°972501	18	38	
11	44	9°547851	22 126	10°462149	9°565373	22 143	10°434627	10°027522	22 17	9°972478	16	48	
30	46	9°548023	23 132	10°461977	9°565568	23 150	10°434432	10°027546	23 18	9°972454	14	38	
12	48	9°548194	24 138	10°461806	9°565763	24 156	10°434237	10°027569	24 18	9°972431	12	48	
30	50	9°548366	25 144	10°461634	9°565958	25 163	10°434042	10°027592	25 19	9°972408	10	38	
13	52	9°548538	26 149	10°461462	9°566153	26 170	10°433847	10°027615	26 20	9°972385	8	47	
30	54	9°548709	27 155	10°461291	9°566348	27 176	10°433652	10°027639	27 21	9°972361	6	38	
14	56	9°548880	28 161	10°461120	9°566542	28 183	10°433457	10°027662	28 22	9°972338	4	46	
30	58	9°549052	29 167	10°460948	9°566737	29 189	10°433263	10°027685	29 22	9°972315	2	38	
15	60	9°549223	30 172	10°460777	9°566932	30 196	10°433068	10°027709	30 23	9°972291	30	45	
30	2	9°549394	1 6	10°460606	9°567126	1 6	10°432874	10°027732	1 1	9°972268	28	38	
16	4	9°549565	2 11	10°460435	9°567320	2 13	10°432680	10°027755	2 2	9°972245	26	44	
30	6	9°549736	3 17	10°460264	9°567515	3 19	10°432485	10°027779	3 2	9°972221	24	38	
17	8	9°549907	4 23	10°460093	9°567709	4 26	10°432291	10°027802	4 3	9°972198	22	43	
30	10	9°550078	5 28	10°459922	9°567903	5 32	10°432097	10°027825	5 4	9°972175	20	38	
18	12	9°550249	6 34	10°459751	9°568098	6 39	10°431902	10°027849	6 5	9°972151	18	42	
30	14	9°550420	7 40	10°459580	9°568292	7 45	10°431708	10°027872	7 5	9°972128	16	38	
19	16	9°550590	8 45	10°459410	9°568486	8 52	10°431514	10°027895	8 6	9°972105	14	41	
30	18	9°550761	9 51	10°459239	9°568680	9 58	10°431320	10°027919	9 7	9°972081	12	38	
20	20	9°550931	10 57	10°459069	9°568873	10 64	10°431127	10°027942	10 8	9°972058	10	40	
30	22	9°551102	11 62	10°458898	9°569067	11 71	10°430933	10°027966	11 9	9°972034	8	38	
21	24	9°551272	12 68	10°458728	9°569261	12 77	10°430739	10°027989	12 9	9°972011	6	38	
30	26	9°551442	13 74	10°458558	9°569455	13 84	10°430545	10°028012	13 10	9°971988	4	38	
22	28	9°551613	14 79	10°458387	9°569648	14 90	10°430352	10°028036	14 11	9°971964	2	38	
30	30	9°551783	15 85	10°458217	9°569842	15 97	10°430158	10°028059	15 12	9°971941	30	38	
23	32	9°551953	16 91	10°458047	9°570035	16 103	10°429965	10°028083	16 12	9°971917	28	37	
30	34	9°552123	17 96	10°457877	9°570229	17 110	10°429771	10°028106	17 13	9°971894	26	38	
24	36	9°552293	18 102	10°457707	9°570422	18 116	10°429578	10°028130	18 14	9°971870	24	36	
30	38	9°552462	19 108	10°457538	9°570616	19 123	10°429384	10°028153	19 15	9°971847	22	38	
25	40	9°552632	20 113	10°457368	9°570809	20 129	10°429191	10°028177	20 16	9°971823	20	33	
30	42	9°552802	21 119	10°457198	9°571002	21 135	10°428998	10°028200	21 16	9°971800	18	38	
26	44	9°552971	22 125	10°457029	9°571195	22 142	10°428805	10°028224	22 17	9°971776	16	34	
30	46	9°553141	23 130	10°456859	9°571388	23 148	10°428612	10°028247	23 18	9°971753	14	38	
27	48	9°553310	24 136	10°456690	9°571581	24 155	10°428419	10°028271	24 19	9°971729	12	33	
30	50	9°553480	25 142	10°456520	9°571774	25 161	10°428226	10°028294	25 19	9°971706	10	38	
28	52	9°553649	26 147	10°456351	9°571967	26 168	10°428033	10°028318	26 20	9°971682	8	32	
30	54	9°553818	27 153	10°456182	9°572160	27 174	10°427840	10°028342	27 21	9°971658	6	38	
29	56	9°553987	28 159	10°456013	9°572352	28 181	10°427648	10°028365	28 22	9°971635	4	31	
30	58	9°554156	29 164	10°455844	9°572545	29 187	10°427455	10°028389	29 23	9°971611	2	38	
30	60	9°554325	30 170	10°455675	9°572738	30 193	10°427262	10°028412	30 23	9°971588	0	38	
'''	min.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	min.	'''	'''

TABLE 68.

779

LOG. SINES, COSINES, &c

1 ^h 22 ^m		20°										1 ^h 23 ^m	
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'
30	0	9°544325		10°455675	9°572738		10°427262	10°028412		9°971588		30	30
30	1	9°544494	1 ⁿ 6	10°455506	9°572930	1 ⁿ 6	10°427070	10°028436	1 ⁿ 1	9°971564	38	30	30
31	0	9°544663	2 11	10°455337	9°573123	2 13	10°426877	10°028460	2 2	9°971540	36	29	30
31	1	9°544832	3 17	10°455168	9°573315	3 19	10°426685	10°028483	3 2	9°971517	34	30	30
32	0	9°545000	4 22	10°455000	9°573507	4 26	10°426493	10°028507	4 3	9°971493	32	28	30
32	1	9°545169	5 28	10°454831	9°573700	5 32	10°426300	10°028531	5 4	9°971469	30	28	30
33	0	9°545338	6 34	10°454662	9°573892	6 38	10°426108	10°028554	6 5	9°971446	28	27	30
33	1	9°545506	7 39	10°454494	9°574084	7 45	10°425916	10°028578	7 6	9°971422	26	30	30
34	0	9°545674	8 45	10°454326	9°574276	8 51	10°425724	10°028602	8 6	9°971398	24	26	30
34	1	9°545843	9 50	10°454157	9°574468	9 58	10°425532	10°028625	9 7	9°971375	22	30	30
35	0	9°546011	10 56	10°453989	9°574660	10 64	10°425340	10°028649	10 8	9°971351	20	25	30
35	1	9°546179	11 61	10°453821	9°574852	11 70	10°425148	10°028673	11 9	9°971327	18	30	30
36	0	9°546347	12 67	10°453653	9°575044	12 77	10°424956	10°028697	12 9	9°971303	16	24	30
36	1	9°546515	13 72	10°453485	9°575236	13 83	10°424764	10°028720	13 10	9°971280	14	30	30
37	0	9°546683	14 78	10°453317	9°575427	14 89	10°424573	10°028744	14 11	9°971256	12	23	30
37	1	9°546851	15 84	10°453149	9°575619	15 96	10°424381	10°028768	15 12	9°971232	10	30	30
38	0	9°547019	16 90	10°452981	9°575810	16 102	10°424190	10°028792	16 13	9°971208	8	22	30
38	1	9°547187	17 95	10°452813	9°576002	17 109	10°423998	10°028815	17 13	9°971185	6	30	30
39	0	9°547354	18 101	10°452646	9°576193	18 115	10°423807	10°028839	18 14	9°971161	4	21	30
39	1	9°547522	19 107	10°452478	9°576385	19 121	10°423615	10°028863	19 15	9°971137	2	30	30
40	0	9°547689	20 112	10°452311	9°576576	20 128	10°423424	10°028887	20 16	9°971113	0	20	30
40	1	9°547857	21 118	10°452143	9°576767	21 134	10°423233	10°028911	21 17	9°971089	0	30	30
41	0	9°548024	22 123	10°451976	9°576959	22 141	10°423041	10°028934	22 17	9°971066	16	19	30
41	1	9°548191	23 129	10°451809	9°577150	23 147	10°422850	10°028958	23 18	9°971042	14	30	30
42	0	9°548359	24 134	10°451641	9°577341	24 153	10°422659	10°028982	24 19	9°971018	12	18	30
42	1	9°548526	25 140	10°451474	9°577532	25 160	10°422468	10°029006	25 20	9°970994	10	30	30
43	0	9°548693	26 145	10°451307	9°577723	26 166	10°422277	10°029030	26 21	9°970970	8	17	30
43	1	9°548860	27 151	10°451140	9°577914	27 173	10°422086	10°029054	27 21	9°970946	6	30	30
44	0	9°549027	28 156	10°450973	9°578104	28 179	10°421896	10°029078	28 22	9°970922	4	16	30
44	1	9°549193	29 162	10°450807	9°578295	29 185	10°421705	10°029102	29 23	9°970898	2	30	30
45	0	9°549360	30 168	10°450640	9°578486	30 192	10°421514	10°029126	30 24	9°970874	0	15	30
45	1	9°549527	1 6	10°450473	9°578676	1 6	10°421324	10°029150	1 1	9°970850	0	30	30
46	0	9°549693	2 11	10°450307	9°578867	2 13	10°421133	10°029173	2 2	9°970827	56	14	30
46	1	9°549860	3 17	10°450140	9°579057	3 19	10°420943	10°029197	3 2	9°970803	54	30	30
47	0	9°550026	4 22	10°449974	9°579248	4 25	10°420752	10°029221	4 3	9°970779	52	13	30
47	1	9°550193	5 28	10°449807	9°579438	5 32	10°420562	10°029245	5 4	9°970755	50	30	30
48	0	9°550359	6 33	10°449641	9°579629	6 38	10°420371	10°029269	6 5	9°970731	48	12	30
48	1	9°550525	7 39	10°449475	9°579819	7 44	10°420181	10°029293	7 6	9°970707	46	30	30
49	0	9°550692	8 44	10°449308	9°580009	8 51	10°419991	10°029317	8 6	9°970683	44	11	30
49	1	9°550858	9 50	10°449142	9°580199	9 57	10°419801	10°029341	9 7	9°970659	42	30	30
50	0	9°551024	10 55	10°448976	9°580389	10 63	10°419611	10°029365	10 8	9°970635	40	10	30
50	1	9°551190	11 6	10°448810	9°580579	11 70	10°419421	10°029389	11 9	9°970611	38	30	30
51	0	9°551356	12 66	10°448644	9°580769	12 76	10°419231	10°029414	12 10	9°970586	36	9	30
51	1	9°551521	13 72	10°448479	9°580959	13 82	10°419041	10°029438	13 10	9°970562	34	30	30
52	0	9°551687	14 77	10°448313	9°581149	14 88	10°418851	10°029462	14 11	9°970538	32	8	30
52	1	9°551853	15 83	10°448147	9°581339	15 95	10°418661	10°029486	15 12	9°970514	30	30	30
53	0	9°552018	16 88	10°447982	9°581528	16 101	10°418472	10°029510	16 13	9°970490	28	7	30
53	1	9°552184	17 94	10°447816	9°581718	17 107	10°418282	10°029534	17 14	9°970466	26	30	30
54	0	9°552349	18 99	10°447651	9°581907	18 114	10°418093	10°029558	18 14	9°970442	24	6	30
54	1	9°552515	19 105	10°447485	9°582097	19 120	10°417903	10°029582	19 15	9°970418	22	30	30
55	0	9°552680	20 110	10°447320	9°582286	20 126	10°417714	10°029606	20 16	9°970394	20	5	30
55	1	9°552845	21 116	10°447155	9°582476	21 133	10°417524	10°029630	21 17	9°970370	18	30	30
56	0	9°553010	22 121	10°446990	9°582665	22 139	10°417335	10°029655	22 18	9°970345	16	4	30
56	1	9°553176	23 127	10°446824	9°582854	23 145	10°417146	10°029679	23 18	9°970321	14	30	30
57	0	9°553341	24 132	10°446659	9°583044	24 152	10°416956	10°029703	24 19	9°970297	12	3	30
57	1	9°553506	25 138	10°446494	9°583233	25 158	10°416767	10°029727	25 20	9°970273	10	30	30
58	0	9°553670	26 143	10°446330	9°583422	26 164	10°416578	10°029751	26 21	9°970249	8	2	30
58	1	9°553835	27 149	10°446165	9°583611	27 171	10°416389	10°029776	27 22	9°970224	6	30	30
59	0	9°554000	28 154	10°446000	9°583800	28 177	10°416200	10°029800	28 22	9°970200	4	1	30
59	1	9°554165	29 160	10°445835	9°583989	29 183	10°416011	10°029824	29 23	9°970176	2	30	30
60	0	9°554329	30 166	10°445671	9°584177	30 190	10°415823	10°029848	30 24	9°970152	0	0	30
1 ^h 22 ^m	°	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	Parts	1 ^h 23 ^m	°

69°

36^m

LOG. SINES, COSINES, &c.

1° 24'		21°										21°	
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'
0	0	9°554329		10°445671	9°584177	10°415823	10°029848		9°970155	36	00	0	0
1	1	9°554494	1"	10°445506	9°584366	10°415634	10°029873	1	9°970127	35	39	1	1
2	2	9°554658	2 11	10°445342	9°584555	10°415445	10°029897	2	9°970105	34	59	2	2
3	3	9°554822	3 16	10°445178	9°584744	10°415256	10°029921	3	9°970079	34	38	3	3
4	4	9°554987	4 22	10°445013	9°584932	10°415068	10°029945	4	9°970055	33	58	4	4
5	5	9°555151	5 27	10°444849	9°585121	10°414879	10°029970	5	9°970030	32	58	5	5
6	6	9°555315	6 33	10°444685	9°585309	10°414691	10°030004	6	9°970006	31	57	6	6
7	7	9°555479	7 38	10°444521	9°585498	10°414502	10°030038	7	9°969982	30	56	7	7
8	8	9°555643	8 44	10°444357	9°585686	10°414314	10°030073	8	9°969957	29	56	8	8
9	9	9°555807	9 49	10°444193	9°585874	10°414126	10°030107	9	9°969933	28	55	9	9
10	10	9°555971	10 54	10°444029	9°586062	10°413938	10°030141	10	9°969909	27	55	10	10
11	11	9°556135	11 60	10°443865	9°586251	10°413749	10°030176	11	9°969884	26	54	11	11
12	12	9°556299	12 65	10°443701	9°586439	10°413561	10°030210	12	9°969860	25	54	12	12
13	13	9°556463	13 71	10°443537	9°586627	10°413373	10°030245	13	9°969836	24	53	13	13
14	14	9°556626	14 76	10°443374	9°586815	10°413185	10°030280	14	9°969811	23	53	14	14
15	15	9°556789	15 82	10°443211	9°587003	10°412997	10°030315	15	9°969787	22	52	15	15
16	16	9°556953	16 87	10°443047	9°587190	10°412810	10°030350	16	9°969762	21	52	16	16
17	17	9°557116	17 93	10°442884	9°587378	10°412622	10°030385	17	9°969738	20	51	17	17
18	18	9°557280	18 98	10°442720	9°587566	10°412434	10°030420	18	9°969714	19	51	18	18
19	19	9°557443	19 104	10°442557	9°587754	10°412246	10°030455	19	9°969689	18	50	19	19
20	20	9°557606	20 109	10°442394	9°587941	10°412059	10°030490	20	9°969665	17	50	20	20
21	21	9°557769	21 115	10°442231	9°588129	10°411871	10°030525	21	9°969640	16	49	21	21
22	22	9°557932	22 120	10°442068	9°588316	10°411684	10°030560	22	9°969616	15	49	22	22
23	23	9°558095	23 126	10°441905	9°588504	10°411496	10°030595	23	9°969591	14	48	23	23
24	24	9°558258	24 131	10°441742	9°588691	10°411309	10°030630	24	9°969567	13	48	24	24
25	25	9°558421	25 137	10°441579	9°588878	10°411122	10°030665	25	9°969542	12	47	25	25
26	26	9°558583	26 142	10°441417	9°589066	10°410934	10°030700	26	9°969518	11	47	26	26
27	27	9°558746	27 147	10°441254	9°589253	10°410747	10°030735	27	9°969493	10	46	27	27
28	28	9°558909	28 153	10°441091	9°589440	10°410560	10°030770	28	9°969469	9	46	28	28
29	29	9°559071	29 158	10°440929	9°589627	10°410373	10°030805	29	9°969444	8	45	29	29
30	30	9°559234	30 163	10°440766	9°589814	10°410186	10°030840	30	9°969420	7	45	30	30
31	31	9°559396	1 5	10°440604	9°590001	10°409999	10°030875	1	9°969395	6	44	31	31
32	32	9°559558	2 11	10°440442	9°590188	10°409812	10°030910	2	9°969370	5	44	32	32
33	33	9°559721	3 16	10°440279	9°590375	10°409625	10°030945	3	9°969346	4	43	33	33
34	34	9°559883	4 22	10°440117	9°590562	10°409438	10°030980	4	9°969321	3	43	34	34
35	35	9°560045	5 27	10°439955	9°590748	10°409251	10°031015	5	9°969297	2	42	35	35
36	36	9°560207	6 32	10°439793	9°590935	10°409065	10°031050	6	9°969272	1	42	36	36
37	37	9°560369	7 38	10°439631	9°591122	10°408878	10°031085	7	9°969247	0	41	37	37
38	38	9°560531	8 43	10°439469	9°591308	10°408692	10°031120	8	9°969223	0	41	38	38
39	39	9°560693	9 48	10°439307	9°591495	10°408505	10°031155	9	9°969198	0	40	39	39
40	40	9°560855	10 54	10°439145	9°591681	10°408319	10°031190	10	9°969173	0	40	40	40
41	41	9°561016	11 59	10°438984	9°591867	10°408132	10°031225	11	9°969149	0	39	41	41
42	42	9°561178	12 65	10°438822	9°592054	10°407946	10°031260	12	9°969124	0	39	42	42
43	43	9°561339	13 70	10°438661	9°592240	10°407760	10°031295	13	9°969099	0	38	43	43
44	44	9°561501	14 75	10°438499	9°592426	10°407574	10°031330	14	9°969075	0	38	44	44
45	45	9°561662	15 81	10°438338	9°592612	10°407388	10°031365	15	9°969050	0	37	45	45
46	46	9°561824	16 86	10°438176	9°592799	10°407201	10°031400	16	9°969025	0	37	46	46
47	47	9°561985	17 91	10°438015	9°592985	10°407015	10°031435	17	9°969000	0	36	47	47
48	48	9°562146	18 97	10°437854	9°593171	10°406829	10°031470	18	9°968976	0	36	48	48
49	49	9°562307	19 102	10°437693	9°593356	10°406644	10°031505	19	9°968951	0	35	49	49
50	50	9°562468	20 108	10°437532	9°593542	10°406458	10°031540	20	9°968926	0	35	50	50
51	51	9°562629	21 113	10°437371	9°593728	10°406272	10°031575	21	9°968901	0	34	51	51
52	52	9°562790	22 119	10°437210	9°593914	10°406086	10°031610	22	9°968877	0	34	52	52
53	53	9°562951	23 124	10°437049	9°594099	10°405901	10°031645	23	9°968852	0	33	53	53
54	54	9°563112	24 129	10°436888	9°594285	10°405715	10°031680	24	9°968827	0	33	54	54
55	55	9°563273	25 135	10°436727	9°594471	10°405529	10°031715	25	9°968802	0	32	55	55
56	56	9°563433	26 140	10°436567	9°594656	10°405344	10°031750	26	9°968777	0	32	56	56
57	57	9°563594	27 145	10°436406	9°594842	10°405158	10°031785	27	9°968752	0	31	57	57
58	58	9°563755	28 151	10°436245	9°595027	10°404973	10°031820	28	9°968728	0	31	58	58
59	59	9°563915	29 156	10°436085	9°595212	10°404788	10°031855	29	9°968703	0	30	59	59
60	60	9°564075	30 161	10°435925	9°595398	10°404602	10°031890	30	9°968678	0	30	60	60
1° 24'		Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	Parts	68°	
												4° 34'	

LOG. SINES, COSINES, &c.

1° 26'											
21°											
''	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m. ''
30	0	9°564075		10°435925	9°595398		10°404602	10°031322		9°568678	30
30	2	9°564236	1" 5	10°435764	9°595583	1" 6	10°404417	10°031347	1" 1	9°568653	30
31	4	9°564396	2 11	10°435604	9°595768	2 12	10°404232	10°031372	2 2	9°568628	30
30	6	9°564556	3 16	10°435444	9°595953	3 18	10°404047	10°031397	3 3	9°568603	30
32	8	9°564716	4 21	10°435284	9°596138	4 25	10°403862	10°031422	4 3	9°568578	30
30	10	9°564876	5 27	10°435124	9°596323	5 31	10°403677	10°031447	5 4	9°568553	30
33	12	9°565036	6 32	10°434964	9°596508	6 37	10°403492	10°031472	6 5	9°568528	30
30	14	9°565196	7 37	10°434804	9°596693	7 43	10°403307	10°031497	7 6	9°568503	30
34	16	9°565356	8 42	10°434644	9°596878	8 49	10°403122	10°031521	8 7	9°568479	30
30	18	9°565516	9 48	10°434484	9°597062	9 55	10°402937	10°031546	9 8	9°568454	30
35	20	9°565676	10 53	10°434324	9°597247	10 61	10°402753	10°031571	10 8	9°568429	30
30	22	9°565835	11 58	10°434165	9°597432	11 68	10°402568	10°031596	11 9	9°568404	30
36	24	9°565995	12 64	10°434005	9°597616	12 74	10°402384	10°031621	12 10	9°568379	30
30	26	9°566154	13 69	10°433846	9°597801	13 80	10°402199	10°031646	13 11	9°568354	30
37	28	9°566314	14 74	10°433686	9°597985	14 86	10°402015	10°031671	14 12	9°568329	30
30	30	9°566473	15 80	10°433527	9°598170	15 92	10°401830	10°031697	15 12	9°568303	30
38	32	9°566632	16 85	10°433368	9°598354	16 98	10°401646	10°031722	16 13	9°568278	30
30	34	9°566792	17 90	10°433208	9°598538	17 105	10°401462	10°031747	17 14	9°568253	30
39	36	9°566951	18 96	10°433049	9°598722	18 111	10°401278	10°031772	18 15	9°568228	30
30	38	9°567110	19 101	10°432890	9°598907	19 117	10°401093	10°031797	19 16	9°568203	30
40	40	9°567269	20 106	10°432731	9°599091	20 123	10°400909	10°031822	20 17	9°568178	30
30	42	9°567428	21 112	10°432572	9°599275	21 129	10°400725	10°031847	21 17	9°568153	30
41	44	9°567587	22 117	10°432413	9°599459	22 135	10°400541	10°031872	22 18	9°568128	30
30	46	9°567746	23 122	10°432254	9°599643	23 141	10°400357	10°031897	23 19	9°568103	30
42	48	9°567904	24 127	10°432096	9°599827	24 148	10°400173	10°031922	24 20	9°568078	30
30	50	9°568063	25 133	10°431937	9°600011	25 154	10°399989	10°031947	25 21	9°568053	30
43	52	9°568222	26 138	10°431778	9°600194	26 160	10°399806	10°031973	26 22	9°568027	30
30	54	9°568380	27 143	10°431620	9°600378	27 166	10°399622	10°031998	27 22	9°568002	30
44	56	9°568539	28 149	10°431461	9°600562	28 172	10°399438	10°032023	28 23	9°567977	30
30	58	9°568697	29 154	10°431303	9°600745	29 178	10°399255	10°032048	29 24	9°567952	30
45	20	9°568856	30 159	10°431144	9°600929	30 184	10°399071	10°032073	30 25	9°567927	30
30	2	9°569014	1 5	10°430986	9°601112	1 6	10°398888	10°032099	1 1	9°567901	30
46	4	9°569172	2 10	10°430828	9°601296	2 12	10°398704	10°032124	2 2	9°567876	30
30	6	9°569330	3 16	10°430670	9°601479	3 18	10°398521	10°032149	3 3	9°567851	30
47	8	9°569488	4 21	10°430512	9°601663	4 24	10°398337	10°032174	4 3	9°567826	30
30	10	9°569646	5 26	10°430354	9°601846	5 30	10°398154	10°032199	5 4	9°567801	30
48	12	9°569804	6 31	10°430196	9°602029	6 37	10°397971	10°032225	6 5	9°567775	30
30	14	9°569962	7 37	10°430038	9°602212	7 43	10°397788	10°032250	7 6	9°567750	30
49	16	9°570120	8 42	10°429880	9°602395	8 49	10°397605	10°032275	8 7	9°567725	30
30	18	9°570278	9 47	10°429722	9°602578	9 55	10°397422	10°032301	9 8	9°567700	30
50	20	9°570435	10 52	10°429565	9°602761	10 61	10°397239	10°032326	10 8	9°567674	30
30	22	9°570593	11 58	10°429407	9°602944	11 67	10°397056	10°032351	11 9	9°567649	30
51	24	9°570751	12 63	10°429249	9°603127	12 73	10°396873	10°032376	12 10	9°567624	30
30	26	9°570909	13 68	10°429092	9°603310	13 79	10°396690	10°032402	13 11	9°567599	30
52	28	9°571066	14 73	10°428934	9°603493	14 85	10°396507	10°032427	14 12	9°567573	30
30	30	9°571223	15 79	10°428777	9°603675	15 91	10°396325	10°032453	15 13	9°567547	30
53	32	9°571380	16 84	10°428620	9°603858	16 97	10°396142	10°032478	16 14	9°567522	30
30	34	9°571537	17 89	10°428463	9°604041	17 104	10°395959	10°032503	17 14	9°567497	30
54	36	9°571695	18 95	10°428305	9°604223	18 110	10°395777	10°032529	18 15	9°567471	30
30	38	9°571852	19 100	10°428148	9°604406	19 116	10°395594	10°032554	19 16	9°567446	30
55	40	9°572009	20 105	10°427991	9°604588	20 122	10°395412	10°032579	20 17	9°567421	30
30	42	9°572166	21 110	10°427834	9°604771	21 128	10°395229	10°032605	21 18	9°567395	30
56	44	9°572323	22 116	10°427677	9°604953	22 134	10°395047	10°032630	22 19	9°567370	30
30	46	9°572479	23 121	10°427521	9°605135	23 140	10°394865	10°032656	23 20	9°567344	30
57	48	9°572636	24 126	10°427364	9°605317	24 146	10°394683	10°032681	24 20	9°567319	30
30	50	9°572793	25 131	10°427207	9°605500	25 152	10°394500	10°032707	25 21	9°567293	30
58	52	9°572950	26 137	10°427050	9°605682	26 158	10°394318	10°032732	26 22	9°567268	30
30	54	9°573106	27 142	10°426894	9°605864	27 164	10°394136	10°032758	27 23	9°567242	30
59	56	9°573263	28 147	10°426737	9°606046	28 171	10°393954	10°032783	28 24	9°567217	30
30	58	9°573419	29 152	10°426581	9°606228	29 177	10°393772	10°032809	29 25	9°567191	30
60	20	9°573575	30 157	10°426425	9°606410	30 183	10°393590	10°032834	30 25	9°567166	30
''	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m. ''

LOG. SINES, COSINES, &c.

1° 28"					22°					
m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.
0	9°573575		10°426425	9°606410		10°393590	10°032834		9°967166	32
1	9°573732	1"	10°426468	9°606591	1"	10°393409	10°032860	1"	9°967140	31
2	9°573888	2	10°426512	9°606773	2	10°393227	10°032885	2	9°967115	30
3	9°574044	3	10°426556	9°606955	3	10°393045	10°032911	3	9°967089	29
4	9°574200	4	10°426600	9°607137	4	10°392863	10°032936	4	9°967064	28
5	9°574356	5	10°426644	9°607318	5	10°392682	10°032962	5	9°967038	27
6	9°574512	6	10°426688	9°607500	6	10°392500	10°032987	6	9°967013	26
7	9°574668	7	10°426732	9°607681	7	10°392319	10°033013	7	9°966987	25
8	9°574824	8	10°426776	9°607863	8	10°392137	10°033039	8	9°966961	24
9	9°574980	9	10°426820	9°608044	9	10°391956	10°033064	9	9°966936	23
10	9°575136	10	10°426864	9°608225	10	10°391775	10°033090	10	9°966910	22
11	9°575291	11	10°426909	9°608407	11	10°391593	10°033116	11	9°966884	21
12	9°575447	12	10°426953	9°608588	12	10°391412	10°033141	12	9°966859	20
13	9°575602	13	10°426998	9°608769	13	10°391231	10°033167	13	9°966833	19
14	9°575758	14	10°427042	9°608950	14	10°391050	10°033192	14	9°966808	18
15	9°575913	15	10°427087	9°609131	15	10°390869	10°033218	15	9°966782	17
16	9°576069	16	10°427131	9°609312	16	10°390688	10°033244	16	9°966756	16
17	9°576224	17	10°427176	9°609493	17	10°390507	10°033270	17	9°966730	15
18	9°576379	18	10°427220	9°609674	18	10°390326	10°033295	18	9°966705	14
19	9°576534	19	10°427265	9°609855	19	10°390145	10°033321	19	9°966679	13
20	9°576689	20	10°427310	9°610036	20	10°389964	10°033347	20	9°966653	12
21	9°576844	21	10°427354	9°610217	21	10°389783	10°033372	21	9°966628	11
22	9°576999	22	10°427399	9°610397	22	10°389603	10°033398	22	9°966602	10
23	9°577154	23	10°427443	9°610578	23	10°389422	10°033424	23	9°966576	9
24	9°577309	24	10°427488	9°610759	24	10°389241	10°033450	24	9°966550	8
25	9°577464	25	10°427532	9°610939	25	10°389061	10°033475	25	9°966525	7
26	9°577618	26	10°427577	9°611120	26	10°388880	10°033501	26	9°966499	6
27	9°577773	27	10°427621	9°611300	27	10°388700	10°033527	27	9°966473	5
28	9°577927	28	10°427666	9°611480	28	10°388520	10°033553	28	9°966447	4
29	9°578082	29	10°427710	9°611661	29	10°388339	10°033579	29	9°966421	3
30	9°578236	30	10°427755	9°611841	30	10°388159	10°033605	30	9°966395	2
31	9°578391	31	10°427800	9°612021	31	10°387979	10°033630	31	9°966370	1
32	9°578545	32	10°427844	9°612201	32	10°387799	10°033656	32	9°966344	0
33	9°578699	3	10°427889	9°612381	3	10°387619	10°033682	3	9°966318	54
34	9°578853	4	10°427933	9°612561	4	10°387439	10°033708	4	9°966292	53
35	9°579008	5	10°427978	9°612741	5	10°387259	10°033734	5	9°966266	52
36	9°579162	6	10°428022	9°612921	6	10°387079	10°033760	6	9°966240	51
37	9°579316	7	10°428067	9°613101	7	10°386899	10°033786	7	9°966214	50
38	9°579470	8	10°428111	9°613281	8	10°386719	10°033812	8	9°966188	49
39	9°579623	9	10°428156	9°613461	9	10°386539	10°033838	9	9°966162	48
40	9°579777	10	10°428200	9°613641	10	10°386359	10°033864	10	9°966136	47
41	9°579931	11	10°428245	9°613820	11	10°386180	10°033890	11	9°966110	46
42	9°580085	12	10°428289	9°614000	12	10°386000	10°033915	12	9°966085	45
43	9°580238	13	10°428334	9°614180	13	10°385820	10°033941	13	9°966059	44
44	9°580392	14	10°428378	9°614359	14	10°385641	10°033967	14	9°966033	43
45	9°580545	15	10°428423	9°614539	15	10°385461	10°033993	15	9°966007	42
46	9°580699	16	10°428467	9°614718	16	10°385282	10°034019	16	9°965981	41
47	9°580852	17	10°428512	9°614897	17	10°385103	10°034045	17	9°965955	40
48	9°581005	18	10°428556	9°615077	18	10°384923	10°034071	18	9°965929	39
49	9°581158	19	10°428601	9°615256	19	10°384744	10°034098	19	9°965902	38
50	9°581312	20	10°428645	9°615435	20	10°384565	10°034124	20	9°965876	37
51	9°581465	21	10°428690	9°615614	21	10°384386	10°034150	21	9°965850	36
52	9°581618	22	10°428734	9°615793	22	10°384207	10°034176	22	9°965824	35
53	9°581771	23	10°428779	9°615972	23	10°384028	10°034202	23	9°965798	34
54	9°581924	24	10°428823	9°616151	24	10°383849	10°034228	24	9°965772	33
55	9°582076	25	10°428868	9°616330	25	10°383670	10°034254	25	9°965746	32
56	9°582229	26	10°428912	9°616509	26	10°383491	10°034280	26	9°965720	31
57	9°582382	27	10°428957	9°616688	27	10°383312	10°034306	27	9°965694	30
58	9°582535	28	10°429001	9°616867	28	10°383133	10°034332	28	9°965668	29
59	9°582687	29	10°429046	9°617046	29	10°382954	10°034358	29	9°965642	28
60	9°582840	30	10°429090	9°617224	30	10°382776	10°034385	30	9°965615	27
m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.
67°					4° 30'					

TABLE 63

783

LOG. SINES, COSINES, &c.

1 ^h 30 ^m				22 ^o						
m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.
30	9°582840		10°417160	9°617224	1	6	10°382776	10°034385	9°965615	30
30	9°582992	1" 5	10°417008	9°617403	1" 6	10°382597	10°034411	1" 1	9°965589	30
31	9°583145	2 10	10°416855	9°617582	2 12	10°382418	10°034437	2 2	9°965563	30
31	9°583297	3 15	10°416703	9°617760	3 18	10°382240	10°034463	3 3	9°965537	30
32	9°583449	4 20	10°416551	9°617939	4 24	10°382061	10°034489	4 4	9°965511	30
32	9°583601	5 25	10°416399	9°618117	5 30	10°381883	10°034516	5 4	9°965484	30
33	9°583754	6 30	10°416246	9°618295	6 36	10°381705	10°034542	6 5	9°965458	30
33	9°583906	7 35	10°416094	9°618474	7 42	10°381526	10°034568	7 6	9°965432	30
34	9°584058	8 40	10°415942	9°618652	8 47	10°381348	10°034594	8 7	9°965406	30
34	9°584210	9 45	10°415790	9°618830	9 53	10°381170	10°034621	9 8	9°965379	30
35	9°584361	10 50	10°415639	9°619008	10 59	10°380992	10°034647	10 9	9°965353	30
35	9°584513	11 56	10°415487	9°619186	11 65	10°380814	10°034673	11 10	9°965327	30
36	9°584665	12 61	10°415335	9°619364	12 71	10°380636	10°034699	12 11	9°965301	30
36	9°584817	13 66	10°415183	9°619543	13 77	10°380457	10°034726	13 11	9°965274	30
37	9°584968	14 71	10°415032	9°619720	14 83	10°380280	10°034752	14 12	9°965248	30
37	9°585120	15 76	10°414880	9°619898	15 90	10°380102	10°034778	15 13	9°965222	30
38	9°585272	16 81	10°414728	9°620076	16 95	10°379924	10°034805	16 14	9°965195	30
38	9°585423	17 86	10°414577	9°620254	17 101	10°379746	10°034831	17 15	9°965169	30
39	9°585574	18 91	10°414426	9°620432	18 107	10°379568	10°034857	18 16	9°965143	30
39	9°585726	19 96	10°414274	9°620610	19 113	10°379390	10°034884	19 17	9°965116	30
40	9°585877	20 101	10°414123	9°620787	20 119	10°379213	10°034910	20 18	9°965090	30
40	9°586028	21 106	10°413972	9°620965	21 125	10°379035	10°034936	21 18	9°965064	30
41	9°586179	22 111	10°413821	9°621142	22 130	10°378858	10°034963	22 19	9°965037	30
41	9°586331	23 116	10°413669	9°621320	23 136	10°378680	10°034989	23 20	9°965011	30
42	9°586482	24 121	10°413518	9°621497	24 142	10°378503	10°035016	24 21	9°964984	30
42	9°586633	25 126	10°413367	9°621675	25 148	10°378325	10°035042	25 22	9°964958	30
43	9°586783	26 131	10°413217	9°621852	26 154	10°378148	10°035069	26 23	9°964931	30
43	9°586934	27 136	10°413066	9°622029	27 160	10°377971	10°035095	27 24	9°964905	30
44	9°587085	28 141	10°412915	9°622207	28 166	10°377793	10°035121	28 25	9°964879	30
44	9°587236	29 146	10°412764	9°622384	29 172	10°377616	10°035148	29 26	9°964852	30
45	9°587386	30 151	10°412614	9°622561	30 178	10°377439	10°035174	30 26	9°964826	30
45	9°587537	1 5	10°412463	9°622738	1 6	10°377262	10°035201	1 1	9°964799	30
46	9°587688	2 10	10°412312	9°622915	2 12	10°377085	10°035227	2 2	9°964773	30
46	9°587838	3 15	10°412162	9°623092	3 18	10°376908	10°035254	3 3	9°964746	30
47	9°587989	4 20	10°412011	9°623269	4 24	10°376731	10°035280	4 4	9°964720	30
47	9°588139	5 25	10°411861	9°623446	5 29	10°376554	10°035307	5 4	9°964693	30
48	9°588289	6 30	10°411711	9°623623	6 35	10°376377	10°035334	6 5	9°964666	30
48	9°588439	7 35	10°411561	9°623800	7 41	10°376200	10°035360	7 6	9°964640	30
49	9°588590	8 40	10°411410	9°623976	8 47	10°376024	10°035387	8 7	9°964613	30
49	9°588740	9 45	10°411260	9°624153	9 53	10°375847	10°035413	9 8	9°964586	30
50	9°588890	10 50	10°411110	9°624330	10 59	10°375670	10°035440	10 9	9°964560	30
50	9°589040	11 55	10°410960	9°624507	11 65	10°375494	10°035466	11 10	9°964534	30
51	9°589190	12 60	10°410810	9°624683	12 71	10°375317	10°035493	12 11	9°964507	30
51	9°589340	13 65	10°410660	9°624859	13 76	10°375141	10°035520	13 12	9°964480	30
52	9°589489	14 70	10°410511	9°625036	14 82	10°374964	10°035546	14 12	9°964454	30
52	9°589639	15 75	10°410361	9°625212	15 88	10°374788	10°035573	15 13	9°964427	30
53	9°589789	16 80	10°410211	9°625388	16 94	10°374612	10°035600	16 14	9°964400	30
53	9°589938	17 85	10°410062	9°625565	17 100	10°374435	10°035626	17 15	9°964374	30
54	9°590088	18 90	10°409912	9°625741	18 106	10°374259	10°035653	18 16	9°964347	30
54	9°590237	19 95	10°409763	9°625917	19 112	10°374083	10°035680	19 17	9°964320	30
55	9°590387	20 100	10°409613	9°626093	20 118	10°373907	10°035706	20 18	9°964294	30
55	9°590536	21 105	10°409464	9°626269	21 123	10°373731	10°035733	21 19	9°964267	30
56	9°590686	22 110	10°409314	9°626445	22 129	10°373555	10°035760	22 20	9°964240	30
56	9°590835	23 115	10°409165	9°626621	23 135	10°373379	10°035786	23 20	9°964214	30
57	9°590984	24 120	10°409016	9°626797	24 141	10°373203	10°035813	24 21	9°964187	30
57	9°591133	25 125	10°408867	9°626973	25 147	10°373027	10°035840	25 22	9°964160	30
58	9°591282	26 130	10°408718	9°627149	26 153	10°372851	10°035867	26 23	9°964133	30
58	9°591431	27 135	10°408569	9°627325	27 159	10°372675	10°035894	27 24	9°964106	30
59	9°591580	28 140	10°408420	9°627501	28 165	10°372499	10°035920	28 25	9°964080	30
59	9°591729	29 145	10°408271	9°627676	29 171	10°372324	10°035947	29 26	9°964053	30
60	9°591878	30 150	10°408122	9°627852	30 176	10°372148	10°035974	30 27	9°964026	30
m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.

67°

4^h 28^m

67°

4^h 28^m

LOG. SINES, COSINES, &c.

1° 32'										
23°										
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine
0	0	9°591878		10°408122	9°627852	10°372148	10°035974	9°964026	20	60
30	2	9°592027	1" 5	10°407973	9°628028	1" 6	10°371972	10°036001	1" 1	9°963999
1	4	9°592176	2 10	10°407824	9°628203	2 12	10°371797	10°036028	2 2	9°963972
30	6	9°592324	3 15	10°407676	9°628379	3 17	10°371621	10°036054	3 3	9°963946
2	8	9°592473	4 20	10°407527	9°628554	4 23	10°371446	10°036081	4 4	9°963919
30	10	9°592621	5 25	10°407379	9°628729	5 29	10°371271	10°036108	5 4	9°963892
3	12	9°592770	6 30	10°407230	9°628905	6 35	10°371095	10°036135	6 5	9°963865
30	14	9°592918	7 35	10°407082	9°629080	7 41	10°370920	10°036162	7 6	9°963838
4	16	9°593067	8 39	10°406933	9°629255	8 47	10°370745	10°036189	8 7	9°963811
30	18	9°593215	9 44	10°406785	9°629431	9 52	10°370569	10°036216	9 8	9°963784
5	20	9°593363	10 49	10°406637	9°629606	10 58	10°370394	10°036243	10 9	9°963757
30	22	9°593511	11 54	10°406489	9°629781	11 64	10°370219	10°036270	11 10	9°963730
6	24	9°593659	12 59	10°406341	9°629956	12 70	10°370044	10°036296	12 11	9°963704
30	26	9°593807	13 64	10°406193	9°630131	13 76	10°369869	10°036323	13 12	9°963677
7	28	9°593955	14 69	10°406045	9°630306	14 82	10°369694	10°036350	14 13	9°963650
30	30	9°594103	15 74	10°405897	9°630481	15 87	10°369519	10°036377	15 13	9°963623
8	32	9°594251	16 79	10°405749	9°630656	16 93	10°369344	10°036404	16 14	9°963596
30	34	9°594399	17 84	10°405601	9°630830	17 99	10°369170	10°036431	17 15	9°963569
9	36	9°594547	18 89	10°405453	9°631005	18 105	10°368995	10°036458	18 16	9°963542
30	38	9°594695	19 94	10°405305	9°631180	19 111	10°368820	10°036485	19 17	9°963515
10	40	9°594842	20 99	10°405157	9°631355	20 117	10°368645	10°036512	20 18	9°963488
30	42	9°594990	21 104	10°405010	9°631529	21 122	10°368471	10°036539	21 19	9°963461
11	44	9°595137	22 109	10°404863	9°631704	22 128	10°368296	10°036566	22 20	9°963434
30	46	9°595285	23 114	10°404715	9°631878	23 134	10°368122	10°036593	23 21	9°963407
12	48	9°595432	24 118	10°404568	9°632053	24 140	10°367947	10°036621	24 22	9°963379
30	50	9°595580	25 123	10°404420	9°632227	25 146	10°367773	10°036648	25 22	9°963352
13	52	9°595727	26 128	10°404273	9°632402	26 152	10°367598	10°036675	26 23	9°963325
30	54	9°595874	27 133	10°404126	9°632576	27 157	10°367424	10°036702	27 24	9°963298
14	56	9°596021	28 138	10°403979	9°632750	28 163	10°367250	10°036729	28 25	9°963271
30	58	9°596168	29 143	10°403832	9°632924	29 169	10°367076	10°036756	29 26	9°963244
15	60	9°596315	30 148	10°403685	9°633099	30 175	10°366901	10°036783	30 27	9°963217
30	62	9°596462	1 5	10°403538	9°633273	1 6	10°366727	10°036810	1 1	9°963190
16	4	9°596609	2 10	10°403391	9°633447	2 12	10°366553	10°036837	2 2	9°963163
30	6	9°596756	3 15	10°403244	9°633621	3 17	10°366379	10°036865	3 3	9°963135
17	8	9°596903	4 20	10°403097	9°633795	4 23	10°366205	10°036892	4 4	9°963108
30	10	9°597050	5 24	10°402950	9°633969	5 29	10°366031	10°036919	5 5	9°963081
18	12	9°597196	6 29	10°402804	9°634143	6 35	10°365857	10°036946	6 6	9°963054
30	14	9°597343	7 34	10°402657	9°634316	7 40	10°365684	10°036973	7 7	9°963027
19	16	9°597490	8 39	10°402510	9°634490	8 46	10°365510	10°037001	8 8	9°962999
30	18	9°597636	9 44	10°402364	9°634664	9 52	10°365336	10°037028	9 9	9°962972
20	20	9°597783	10 49	10°402217	9°634838	10 58	10°365162	10°037055	10 10	9°962945
30	22	9°597929	11 54	10°402071	9°635011	11 64	10°364989	10°037082	11 10	9°962918
21	24	9°598075	12 58	10°401925	9°635185	12 69	10°364815	10°037110	12 11	9°962890
30	26	9°598222	13 63	10°401778	9°635359	13 75	10°364641	10°037137	13 12	9°962863
22	28	9°598368	14 68	10°401632	9°635532	14 81	10°364468	10°037164	14 13	9°962836
30	30	9°598514	15 73	10°401486	9°635706	15 87	10°364294	10°037191	15 14	9°962809
23	32	9°598660	16 78	10°401340	9°635879	16 92	10°364121	10°037219	16 15	9°962781
30	34	9°598806	17 83	10°401194	9°636052	17 98	10°363948	10°037246	17 15	9°962754
24	36	9°598952	18 88	10°401048	9°636226	18 104	10°363774	10°037273	18 16	9°962727
30	38	9°599098	19 93	10°400902	9°636399	19 110	10°363601	10°037301	19 17	9°962699
25	40	9°599244	20 98	10°400756	9°636572	20 116	10°363428	10°037328	20 18	9°962672
30	42	9°599390	21 102	10°400610	9°636745	21 121	10°363255	10°037355	21 19	9°962645
26	44	9°599536	22 107	10°400464	9°636919	22 127	10°363081	10°037383	22 20	9°962617
30	46	9°599681	23 112	10°400319	9°637092	23 133	10°362908	10°037410	23 21	9°962590
27	48	9°599827	24 117	10°400173	9°637265	24 139	10°362735	10°037438	24 22	9°962562
30	50	9°599973	25 122	10°400027	9°637438	25 144	10°362562	10°037465	25 23	9°962535
28	52	9°600118	26 127	10°399882	9°637611	26 150	10°362389	10°037492	26 24	9°962508
30	54	9°600264	27 131	10°399736	9°637783	27 156	10°362217	10°037520	27 25	9°962480
29	56	9°600409	28 136	10°399591	9°637956	28 162	10°362044	10°037547	28 25	9°962453
30	58	9°600554	29 141	10°399446	9°638129	29 168	10°361871	10°037575	29 26	9°962425
30	60	9°600700	30 146	10°399300	9°638302	30 173	10°361698	10°037602	30 27	9°962398
1°	32'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine

I.O.G. SINES, COSINES, &c.

1 ^h 34 ^m				23°									
°	'	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	'
30	0	0	9'607000		10'399300	9'638302	1" 6	10'361698	10'037602	1" 1	9'962398	26	30
30	2	0	9'608045	1" 5	10'399155	9'638475	1" 6	10'361525	10'037630	1" 1	9'962370	26	30
31	0	0	9'609090	2 10	10'399010	9'638647	2 11	10'361353	10'037657	2 2	9'962343	26	30
30	6	0	9'601135	3 14	10'398865	9'638820	3 17	10'361180	10'037685	3 3	9'962315	26	30
32	0	0	9'601280	4 19	10'398720	9'638992	4 23	10'361008	10'037712	4 4	9'962288	26	30
30	8	0	9'601425	5 24	10'398575	9'639165	5 29	10'360835	10'037740	5 5	9'962260	26	30
33	0	0	9'601570	6 29	10'398430	9'639337	6 34	10'360663	10'037767	6 6	9'962233	26	30
30	14	0	9'601715	7 34	10'398285	9'639510	7 40	10'360490	10'037795	7 6	9'962205	26	30
34	0	0	9'601860	8 38	10'398140	9'639682	8 46	10'360318	10'037822	8 7	9'962178	26	30
35	0	0	9'602005	9 43	10'397995	9'639855	9 52	10'360145	10'037850	9 8	9'962150	26	30
35	20	0	9'602150	10 48	10'397850	9'640027	10 57	10'359973	10'037877	10 9	9'962123	26	30
36	0	0	9'602294	11 53	10'397706	9'640199	11 63	10'359801	10'037905	11 10	9'962095	26	30
36	24	0	9'602439	12 58	10'397561	9'640371	12 69	10'359629	10'037933	12 11	9'962067	26	30
36	48	0	9'602583	13 62	10'397417	9'640544	13 74	10'359456	10'037960	13 12	9'962040	26	30
37	0	0	9'602728	14 67	10'397272	9'640716	14 80	10'359284	10'037988	14 13	9'962012	26	30
30	28	0	9'602872	15 72	10'397128	9'640888	15 86	10'359112	10'038015	15 14	9'961985	26	30
38	0	0	9'603017	16 77	10'396983	9'641060	16 92	10'358940	10'038043	16 15	9'961957	26	30
30	34	0	9'603161	17 82	10'396839	9'641232	17 97	10'358768	10'038071	17 16	9'961929	26	30
39	0	0	9'603305	18 87	10'396695	9'641404	18 103	10'358596	10'038098	18 17	9'961902	26	30
30	38	0	9'603449	19 92	10'396551	9'641575	19 109	10'358425	10'038126	19 17	9'961874	26	30
40	0	0	9'603594	20 96	10'396406	9'641747	20 115	10'358253	10'038154	20 18	9'961846	26	30
30	42	0	9'603738	21 101	10'396262	9'641919	21 120	10'358081	10'038181	21 19	9'961819	26	30
41	0	0	9'603882	22 106	10'396118	9'642091	22 126	10'357909	10'038209	22 20	9'961791	26	30
30	46	0	9'604026	23 111	10'395974	9'642263	23 132	10'357737	10'038237	23 21	9'961763	26	30
42	0	0	9'604170	24 115	10'395830	9'642434	24 138	10'357566	10'038265	24 22	9'961735	26	30
30	50	0	9'604313	25 120	10'395687	9'642606	25 143	10'357394	10'038292	25 23	9'961708	26	30
43	0	0	9'604457	26 125	10'395543	9'642777	26 149	10'357223	10'038320	26 24	9'961680	26	30
30	54	0	9'604601	27 130	10'395399	9'642949	27 155	10'357051	10'038348	27 25	9'961652	26	30
44	0	0	9'604745	28 134	10'395255	9'643120	28 160	10'356880	10'038376	28 26	9'961624	26	30
30	58	0	9'604889	29 139	10'395112	9'643292	29 166	10'356708	10'038403	29 27	9'961597	26	30
45	0	0	9'605032	30 144	10'394968	9'643463	30 172	10'356537	10'038431	30 28	9'961569	26	30
30	2	0	9'605176	1 5	10'394824	9'643634	1 6	10'356366	10'038459	1 1	9'961541	26	30
46	0	0	9'605319	2 10	10'394681	9'643806	2 11	10'356194	10'038487	2 2	9'961513	26	30
30	6	0	9'605462	3 14	10'394538	9'643977	3 17	10'356023	10'038515	3 3	9'961485	26	30
47	0	0	9'605606	4 19	10'394394	9'644148	4 23	10'355852	10'038542	4 4	9'961458	26	30
30	10	0	9'605749	5 24	10'394251	9'644319	5 28	10'355681	10'038570	5 5	9'961430	26	30
48	0	0	9'605892	6 29	10'394108	9'644490	6 34	10'355510	10'038598	6 6	9'961402	26	30
30	14	0	9'606035	7 33	10'393965	9'644661	7 40	10'355339	10'038626	7 7	9'961374	26	30
49	0	0	9'606179	8 38	10'393821	9'644832	8 46	10'355168	10'038654	8 7	9'961346	26	30
30	18	0	9'606322	9 43	10'393678	9'645003	9 51	10'354997	10'038682	9 8	9'961318	26	30
50	0	0	9'606465	10 48	10'393535	9'645174	10 57	10'354826	10'038710	10 9	9'961290	26	30
30	22	0	9'606608	11 52	10'393392	9'645345	11 63	10'354655	10'038737	11 10	9'961263	26	30
51	0	0	9'606751	12 57	10'393249	9'645516	12 68	10'354484	10'038765	12 11	9'961235	26	30
30	26	0	9'606893	13 62	10'393107	9'645687	13 74	10'354313	10'038793	13 12	9'961207	26	30
52	0	0	9'607036	14 67	10'392964	9'645857	14 80	10'354143	10'038821	14 13	9'961179	26	30
30	30	0	9'607179	15 71	10'392821	9'646028	15 85	10'353972	10'038849	15 14	9'961151	26	30
53	0	0	9'607322	16 76	10'392678	9'646199	16 91	10'353801	10'038877	16 15	9'961123	26	30
30	34	0	9'607464	17 81	10'392536	9'646369	17 97	10'353631	10'038905	17 16	9'961095	26	30
54	0	0	9'607607	18 86	10'392393	9'646540	18 102	10'353460	10'038933	18 17	9'961067	26	30
30	38	0	9'607749	19 90	10'392251	9'646710	19 108	10'353290	10'038961	19 18	9'961039	26	30
55	0	0	9'607892	20 95	10'392108	9'646881	20 114	10'353119	10'038989	20 19	9'961011	26	30
30	42	0	9'608034	21 100	10'391966	9'647051	21 119	10'352949	10'039017	21 20	9'960983	26	30
56	0	0	9'608177	22 105	10'391823	9'647222	22 125	10'352778	10'039045	22 20	9'960955	26	30
30	46	0	9'608319	23 110	10'391681	9'647392	23 131	10'352608	10'039073	23 21	9'960927	26	30
57	0	0	9'608461	24 114	10'391539	9'647562	24 137	10'352438	10'039101	24 22	9'960899	26	30
30	50	0	9'608603	25 119	10'391397	9'647733	25 142	10'352267	10'039129	25 23	9'960871	26	30
58	0	0	9'608745	26 124	10'391255	9'647903	26 148	10'352097	10'039157	26 24	9'960843	26	30
30	54	0	9'608887	27 128	10'391113	9'648073	27 154	10'351927	10'039186	27 25	9'960815	26	30
59	0	0	9'609029	28 133	10'390971	9'648243	28 159	10'351757	10'039214	28 26	9'960787	26	30
30	58	0	9'609171	29 138	10'390829	9'648413	29 165	10'351587	10'039242	29 27	9'960759	26	30
60	0	0	9'609313	30 143	10'390687	9'648583	30 171	10'351417	10'039270	30 28	9'960730	26	30
°	'	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	'

66°

4^h 24^m

LOG. SINES, COSINES, &c.											
1° 36"						24°					
"	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	"
0	0	9°609313		10°390687	9°648583		10°351417	10°039270		9°960730	24 68
1	1	9°609455	1 5	10°390545	9°648753	1 6	10°351247	10°039298	1 1	9°960702	24 69
2	2	9°609597	2 10	10°390403	9°648923	2 11	10°351077	10°039326	2 2	9°960674	24 70
3	3	9°609739	3 14	10°390261	9°649093	3 17	10°350907	10°039354	3 3	9°960646	24 71
4	4	9°609880	4 19	10°390120	9°649263	4 23	10°350737	10°039382	4 4	9°960618	24 72
5	5	9°610022	5 23	10°389978	9°649433	5 28	10°350567	10°039411	5 5	9°960590	24 73
6	6	9°610164	6 28	10°389836	9°649602	6 34	10°350398	10°039439	6 6	9°960561	24 74
7	7	9°610305	7 33	10°389695	9°649772	7 39	10°350228	10°039467	7 7	9°960533	24 75
8	8	9°610447	8 38	10°389553	9°649942	8 45	10°350058	10°039495	8 8	9°960505	24 76
9	9	9°610588	9 42	10°389412	9°650111	9 51	10°349889	10°039523	9 9	9°960477	24 77
10	10	9°610729	10 47	10°389271	9°650281	10 56	10°349719	10°039552	10 9	9°960448	24 78
11	11	9°610871	11 52	10°389129	9°650450	11 62	10°349550	10°039580	11 10	9°960420	24 79
12	12	9°611012	12 56	10°388988	9°650620	12 68	10°349380	10°039608	12 11	9°960392	24 80
13	13	9°611153	13 61	10°388847	9°650789	13 73	10°349211	10°039636	13 12	9°960364	24 81
14	14	9°611294	14 66	10°388706	9°650959	14 79	10°349041	10°039665	14 13	9°960335	24 82
15	15	9°611435	15 71	10°388565	9°651128	15 85	10°348872	10°039693	15 14	9°960307	24 83
16	16	9°611576	16 75	10°388424	9°651297	16 90	10°348703	10°039721	16 15	9°960279	24 84
17	17	9°611717	17 80	10°388283	9°651467	17 96	10°348533	10°039750	17 16	9°960250	24 85
18	18	9°611858	18 85	10°388142	9°651636	18 102	10°348364	10°039778	18 17	9°960222	24 86
19	19	9°611999	19 89	10°388001	9°651805	19 107	10°348195	10°039806	19 18	9°960194	24 87
20	20	9°612140	20 94	10°387860	9°651974	20 113	10°348026	10°039835	20 19	9°960165	24 88
21	21	9°612280	21 99	10°387720	9°652143	21 118	10°347857	10°039863	21 20	9°960137	24 89
22	22	9°612421	22 103	10°387579	9°652312	22 124	10°347688	10°039891	22 21	9°960109	24 90
23	23	9°612562	23 108	10°387438	9°652481	23 130	10°347519	10°039920	23 22	9°960080	24 91
24	24	9°612702	24 113	10°387298	9°652650	24 135	10°347350	10°039948	24 23	9°960052	24 92
25	25	9°612843	25 117	10°387157	9°652819	25 141	10°347181	10°039976	25 23	9°960024	24 93
26	26	9°612983	26 122	10°387017	9°652988	26 147	10°347012	10°040005	26 24	9°959995	24 94
27	27	9°613124	27 127	10°386876	9°653157	27 152	10°346843	10°040033	27 25	9°959967	24 95
28	28	9°613264	28 132	10°386736	9°653326	28 158	10°346674	10°040062	28 26	9°959938	24 96
29	29	9°613404	29 136	10°386596	9°653494	29 164	10°346506	10°040090	29 27	9°959910	24 97
30	30	9°613545	30 141	10°386455	9°653663	30 169	10°346337	10°040118	30 28	9°959882	24 98
31	31	9°613685	31 145	10°386315	9°653832	31 175	10°346168	10°040147	31 29	9°959853	24 99
32	32	9°613825	32 150	10°386175	9°654000	32 181	10°346000	10°040175	32 30	9°959825	24 100
33	33	9°613965	33 154	10°386035	9°654169	33 187	10°345831	10°040204	33 31	9°959796	24 101
34	34	9°614105	34 159	10°385895	9°654337	34 192	10°345663	10°040232	34 32	9°959768	24 102
35	35	9°614245	35 163	10°385755	9°654506	35 198	10°345494	10°040261	35 33	9°959739	24 103
36	36	9°614385	36 168	10°385615	9°654674	36 204	10°345326	10°040289	36 34	9°959711	24 104
37	37	9°614525	37 172	10°385475	9°654843	37 209	10°345157	10°040318	37 35	9°959682	24 105
38	38	9°614665	38 177	10°385335	9°655011	38 215	10°344989	10°040346	38 36	9°959654	24 106
39	39	9°614804	39 182	10°385195	9°655179	39 220	10°344821	10°040375	39 37	9°959625	24 107
40	40	9°614944	40 186	10°385056	9°655348	40 226	10°344652	10°040404	40 38	9°959596	24 108
41	41	9°615084	41 191	10°384916	9°655516	41 231	10°344484	10°040432	41 39	9°959568	24 109
42	42	9°615223	42 195	10°384777	9°655684	42 237	10°344316	10°040461	42 40	9°959539	24 110
43	43	9°615363	43 200	10°384637	9°655852	43 242	10°344148	10°040489	43 41	9°959511	24 111
44	44	9°615502	44 204	10°384498	9°656020	44 248	10°343980	10°040518	44 42	9°959482	24 112
45	45	9°615642	45 209	10°384358	9°656188	45 253	10°343812	10°040547	45 43	9°959453	24 113
46	46	9°615781	46 213	10°384219	9°656356	46 259	10°343644	10°040575	46 44	9°959425	24 114
47	47	9°615921	47 218	10°384079	9°656524	47 264	10°343476	10°040604	47 45	9°959396	24 115
48	48	9°616060	48 222	10°383940	9°656692	48 270	10°343308	10°040632	48 46	9°959368	24 116
49	49	9°616199	49 227	10°383801	9°656860	49 275	10°343140	10°040661	49 47	9°959339	24 117
50	50	9°616338	50 231	10°383662	9°657028	50 281	10°342972	10°040690	50 48	9°959310	24 118
51	51	9°616477	51 236	10°383523	9°657196	51 286	10°342804	10°040718	51 49	9°959282	24 119
52	52	9°616616	52 240	10°383384	9°657364	52 292	10°342636	10°040747	52 50	9°959253	24 120
53	53	9°616755	53 245	10°383245	9°657531	53 297	10°342469	10°040776	53 51	9°959224	24 121
54	54	9°616894	54 249	10°383106	9°657699	54 303	10°342301	10°040805	54 52	9°959195	24 122
55	55	9°617033	55 254	10°382967	9°657867	55 308	10°342133	10°040833	55 53	9°959167	24 123
56	56	9°617172	56 258	10°382828	9°658034	56 314	10°341966	10°040862	56 54	9°959138	24 124
57	57	9°617311	57 263	10°382689	9°658202	57 319	10°341798	10°040891	57 55	9°959109	24 125
58	58	9°617450	58 267	10°382550	9°658369	58 325	10°341631	10°040920	58 56	9°959080	24 126
59	59	9°617588	59 272	10°382412	9°658537	59 330	10°341463	10°040948	59 57	9°959052	24 127
60	60	9°617727	60 276	10°382273	9°658704	60 336	10°341296	10°040977	60 58	9°959023	24 128
"	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	"

LOG. SINKS, COSINES, &c.

1^h 38^m

24°

" "	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	" "
30	0	9°6'17727		10°382273	9°658704		10°341296	10°040977		9°959c23	22	30
30	2	9°6'18666	1 5	10°382134	9°658871	1 6	10°341129	10°041006	1 1	9°958994	58	30
31	4	9°6'18004	2 9	10°381906	9°659039	2 11	10°340961	10°041035	2 2	9°958965	56	29
31	6	9°6'18143	3 14	10°381857	9°659206	3 17	10°340794	10°041063	3 3	9°958937	54	29
32	8	9°6'18281	4 18	10°381719	9°659373	4 22	10°340627	10°041092	4 4	9°958908	52	28
32	10	9°6'18419	5 23	10°381581	9°659540	5 28	10°340460	10°041121	5 5	9°958879	50	28
33	12	9°6'18558	6 28	10°381442	9°659708	6 33	10°340292	10°041150	6 6	9°958850	48	27
33	14	9°6'18696	7 32	10°381304	9°659875	7 39	10°340125	10°041179	7 7	9°958821	46	30
34	16	9°6'18834	8 37	10°381166	9°660042	8 44	10°339958	10°041208	8 8	9°958792	44	26
34	18	9°6'18972	9 41	10°381028	9°660209	9 50	10°339791	10°041237	9 9	9°958763	42	30
35	20	9°6'19110	10 46	10°380890	9°660376	10 56	10°339624	10°041266	10 10	9°958734	40	26
35	22	9°6'19248	11 50	10°380752	9°660543	11 61	10°339457	10°041294	11 11	9°958706	38	30
36	24	9°6'19386	12 55	10°380614	9°660710	12 67	10°339290	10°041323	12 12	9°958677	36	24
36	26	9°6'19524	13 59	10°380476	9°660877	13 72	10°339123	10°041352	13 12	9°958648	34	30
37	28	9°6'19662	14 64	10°380338	9°661043	14 78	10°338957	10°041381	14 13	9°958619	32	23
37	30	9°6'19800	15 69	10°380200	9°661210	15 83	10°338790	10°041410	15 14	9°958590	30	30
38	32	9°6'19938	16 73	10°380062	9°661377	16 89	10°338623	10°041439	16 15	9°958561	28	22
38	34	9°6'20076	17 78	10°379924	9°661544	17 95	10°338456	10°041468	17 16	9°958532	26	30
39	36	9°6'20213	18 83	10°379787	9°661710	18 100	10°338290	10°041497	18 17	9°958503	24	21
39	38	9°6'20351	19 87	10°379649	9°661877	19 106	10°338123	10°041526	19 18	9°958474	22	30
40	40	9°6'20488	20 92	10°379512	9°662043	20 111	10°337957	10°041555	20 19	9°958445	20	20
40	42	9°6'20626	21 96	10°379374	9°662210	21 117	10°337790	10°041584	21 20	9°958416	18	30
41	44	9°6'20763	22 101	10°379237	9°662376	22 122	10°337624	10°041613	22 21	9°958387	16	19
41	46	9°6'20901	23 105	10°379099	9°662543	23 128	10°337457	10°041642	23 22	9°958358	14	30
42	48	9°6'21038	24 110	10°378962	9°662709	24 133	10°337291	10°041671	24 23	9°958329	12	18
42	50	9°6'21175	25 114	10°378825	9°662876	25 139	10°337124	10°041700	25 24	9°958300	10	30
43	52	9°6'21313	26 119	10°378687	9°663042	26 145	10°336958	10°041729	26 25	9°958271	8	17
43	54	9°6'21450	27 124	10°378550	9°663208	27 150	10°336792	10°041758	27 26	9°958242	6	30
44	56	9°6'21587	28 129	10°378413	9°663375	28 156	10°336625	10°041787	28 27	9°958213	4	16
44	58	9°6'21724	29 133	10°378276	9°663541	29 161	10°336459	10°041817	29 28	9°958183	2	30
45	60	9°6'21861	30 138	10°378139	9°663707	30 167	10°336293	10°041846	30 29	9°958154	2	15
45	2	9°6'21998	1 5	10°378002	9°663873	1 6	10°336127	10°041875	1 1	9°958125	58	30
46	4	9°6'22135	2 9	10°377865	9°664039	2 11	10°335961	10°041904	2 2	9°958096	56	14
46	6	9°6'22272	3 14	10°377728	9°664205	3 17	10°335795	10°041933	3 3	9°958067	54	30
47	8	9°6'22409	4 18	10°377591	9°664371	4 22	10°335629	10°041962	4 4	9°958038	52	13
47	10	9°6'22546	5 23	10°377454	9°664537	5 28	10°335463	10°041991	5 5	9°958009	50	30
48	12	9°6'22682	6 27	10°377318	9°664703	6 33	10°335297	10°042020	6 6	9°957979	48	12
48	14	9°6'22819	7 32	10°377181	9°664869	7 39	10°335131	10°042050	7 7	9°957950	46	30
49	16	9°6'22956	8 36	10°377044	9°665035	8 44	10°334965	10°042079	8 8	9°957921	44	11
49	18	9°6'23092	9 41	10°376908	9°665200	9 50	10°334800	10°042108	9 9	9°957892	42	30
50	20	9°6'23229	10 45	10°376771	9°665366	10 55	10°334634	10°042137	10 10	9°957863	40	10
50	22	9°6'23365	11 50	10°376635	9°665532	11 61	10°334468	10°042167	11 11	9°957833	38	30
51	24	9°6'23502	12 54	10°376498	9°665698	12 66	10°334302	10°042196	12 12	9°957804	36	9
51	26	9°6'23638	13 59	10°376362	9°665863	13 72	10°334137	10°042225	13 13	9°957775	34	30
52	28	9°6'23774	14 63	10°376226	9°666029	14 77	10°333971	10°042254	14 14	9°957746	32	8
52	30	9°6'23911	15 68	10°376089	9°666194	15 83	10°333806	10°042284	15 15	9°957716	30	30
53	32	9°6'24047	16 72	10°375953	9°666360	16 88	10°333640	10°042313	16 16	9°957687	28	7
53	34	9°6'24183	17 77	10°375817	9°666525	17 94	10°333475	10°042342	17 17	9°957658	26	30
54	36	9°6'24319	18 82	10°375681	9°666691	18 99	10°333309	10°042371	18 18	9°957628	24	6
54	38	9°6'24455	19 86	10°375545	9°666856	19 105	10°333144	10°042401	19 19	9°957599	22	30
55	40	9°6'24591	20 91	10°375409	9°667021	20 110	10°332979	10°042430	20 20	9°957570	20	5
55	42	9°6'24727	21 95	10°375273	9°667187	21 116	10°332813	10°042460	21 20	9°957540	18	30
56	44	9°6'24863	22 100	10°375137	9°667352	22 121	10°332648	10°042489	22 21	9°957511	16	4
56	46	9°6'24999	23 104	10°375001	9°667517	23 127	10°332483	10°042518	23 22	9°957482	14	30
57	48	9°6'25135	24 109	10°374865	9°667682	24 132	10°332318	10°042547	24 23	9°957452	12	3
57	50	9°6'25270	25 113	10°374730	9°667847	25 138	10°332153	10°042577	25 24	9°957423	10	30
58	52	9°6'25406	26 118	10°374594	9°668013	26 144	10°331987	10°042607	26 25	9°957393	8	2
58	54	9°6'25542	27 123	10°374458	9°668178	27 149	10°331822	10°042636	27 26	9°957364	6	30
59	56	9°6'25677	28 127	10°374323	9°668343	28 155	10°331657	10°042665	28 27	9°957335	4	1
59	58	9°6'25813	29 132	10°374187	9°668508	29 160	10°331492	10°042695	29 28	9°957305	2	30
60	60	9°6'25948	30 136	10°374052	9°668672	30 166	10°331327	10°042724	30 29	9°957276	0	0

65°

4^h 20^m

LOG. SINES, COSINES, &c.

1 ^h 40 ^m					25°														
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant
0	0	9.625948		10.374052	9.668673	1	10.331327	10.042724	1	9.957276	20	0	9.957276	1	10.042724	9.668673	1	10.331327	10.374052
0	1	9.626084	1	10.373916	9.668837	2	10.331163	10.042754	2	9.957246	20	1	9.957246	2	10.042754	9.669002	2	10.330998	10.373781
0	2	9.626219	2	10.373781	9.669002	3	10.330998	10.042783	3	9.957217	20	2	9.957217	3	10.042783	9.669167	3	10.330833	10.373646
0	3	9.626354	3	10.373646	9.669167	4	10.330833	10.042813	4	9.957187	20	3	9.957187	4	10.042813	9.669332	4	10.330668	10.373510
0	4	9.626490	4	10.373510	9.669332	5	10.330668	10.042842	5	9.957158	20	4	9.957158	5	10.042842	9.669497	5	10.330503	10.373375
0	5	9.626625	5	10.373375	9.669497	6	10.330503	10.042872	6	9.957128	20	5	9.957128	6	10.042872	9.669661	6	10.330339	10.373240
0	6	9.626760	6	10.373240	9.669661	7	10.330339	10.042901	7	9.957099	20	6	9.957099	7	10.042901	9.669826	7	10.330174	10.373105
0	7	9.626895	7	10.373105	9.669826	8	10.330174	10.042931	8	9.957069	20	7	9.957069	8	10.042931	9.669991	8	10.330009	10.372970
0	8	9.627030	8	10.372970	9.669991	9	10.330009	10.042960	9	9.957040	20	8	9.957040	9	10.042960	9.670155	9	10.329845	10.372835
0	9	9.627165	9	10.372835	9.670155	10	10.329845	10.042990	10	9.957010	20	9	9.957010	10	10.042990	9.670320	10	10.329680	10.372700
0	10	9.627300	10	10.372700	9.670320	11	10.329680	10.043019	11	9.956981	20	10	9.956981	11	10.043019	9.670484	11	10.329515	10.372565
0	11	9.627435	11	10.372565	9.670484	12	10.329515	10.043049	12	9.956951	20	11	9.956951	12	10.043049	9.670649	12	10.329351	10.372430
0	12	9.627570	12	10.372430	9.670649	13	10.329351	10.043079	13	9.956921	20	12	9.956921	13	10.043079	9.670813	13	10.329187	10.372295
0	13	9.627705	13	10.372295	9.670813	14	10.329187	10.043108	14	9.956892	20	13	9.956892	14	10.043108	9.670977	14	10.329023	10.372160
0	14	9.627840	14	10.372160	9.670977	15	10.329023	10.043138	15	9.956862	20	14	9.956862	15	10.043138	9.671142	15	10.328858	10.372026
0	15	9.627974	15	10.372026	9.671142	16	10.328858	10.043167	16	9.956833	20	15	9.956833	16	10.043167	9.671306	16	10.328694	10.371891
0	16	9.628109	16	10.371891	9.671306	17	10.328694	10.043197	17	9.956803	20	16	9.956803	17	10.043197	9.671470	17	10.328530	10.371756
0	17	9.628244	17	10.371756	9.671470	18	10.328530	10.043227	18	9.956773	20	17	9.956773	18	10.043227	9.671635	18	10.328365	10.371622
0	18	9.628378	18	10.371622	9.671635	19	10.328365	10.043256	19	9.956744	20	18	9.956744	19	10.043256	9.671799	19	10.328201	10.371487
0	19	9.628513	19	10.371487	9.671799	20	10.328201	10.043286	20	9.956714	20	19	9.956714	20	10.043286	9.671963	20	10.328037	10.371353
0	20	9.628647	20	10.371353	9.671963	21	10.328037	10.043316	21	9.956684	20	20	9.956684	21	10.043316	9.672127	21	10.327873	10.371218
0	21	9.628782	21	10.371218	9.672127	22	10.327873	10.043345	22	9.956655	20	21	9.956655	22	10.043345	9.672291	22	10.327709	10.371084
0	22	9.628916	22	10.371084	9.672291	23	10.327709	10.043375	23	9.956625	20	22	9.956625	23	10.043375	9.672455	23	10.327545	10.370950
0	23	9.629050	23	10.370950	9.672455	24	10.327545	10.043405	24	9.956595	20	23	9.956595	24	10.043405	9.672619	24	10.327381	10.370815
0	24	9.629185	24	10.370815	9.672619	25	10.327381	10.043434	25	9.956565	20	24	9.956565	25	10.043434	9.672783	25	10.327217	10.370681
0	25	9.629319	25	10.370681	9.672783	26	10.327217	10.043464	26	9.956536	20	25	9.956536	26	10.043464	9.672947	26	10.327053	10.370547
0	26	9.629453	26	10.370547	9.672947	27	10.327053	10.043494	27	9.956506	20	26	9.956506	27	10.043494	9.673111	27	10.326889	10.370413
0	27	9.629587	27	10.370413	9.673111	28	10.326889	10.043524	28	9.956476	20	27	9.956476	28	10.043524	9.673274	28	10.326726	10.370279
0	28	9.629721	28	10.370279	9.673274	29	10.326726	10.043553	29	9.956447	20	28	9.956447	29	10.043553	9.673438	29	10.326562	10.370145
0	29	9.629855	29	10.370145	9.673438	30	10.326562	10.043583	30	9.956417	20	29	9.956417	30	10.043583	9.673602	30	10.326398	10.370011
0	30	9.629989	30	10.370011	9.673602	31	10.326398	10.043613	31	9.956387	20	30	9.956387	31	10.043613	9.673766	31	10.326234	10.369877
0	31	9.630123	31	10.369877	9.673766	32	10.326234	10.043643	32	9.956357	20	31	9.956357	32	10.043643	9.673929	32	10.326071	10.369743
0	32	9.630257	32	10.369743	9.673929	33	10.326071	10.043673	33	9.956327	20	32	9.956327	33	10.043673	9.674093	33	10.325907	10.369609
0	33	9.630391	33	10.369609	9.674093	34	10.325907	10.043702	34	9.956298	20	33	9.956298	34	10.043702	9.674257	34	10.325743	10.369476
0	34	9.630524	34	10.369476	9.674257	35	10.325743	10.043732	35	9.956268	20	34	9.956268	35	10.043732	9.674420	35	10.325580	10.369342
0	35	9.630658	35	10.369342	9.674420	36	10.325580	10.043762	36	9.956238	20	35	9.956238	36	10.043762	9.674584	36	10.325416	10.369208
0	36	9.630792	36	10.369208	9.674584	37	10.325416	10.043792	37	9.956208	20	36	9.956208	37	10.043792	9.674747	37	10.325253	10.369075
0	37	9.630925	37	10.369075	9.674747	38	10.325253	10.043822	38	9.956178	20	37	9.956178	38	10.043822	9.674911	38	10.325089	10.368941
0	38	9.631059	38	10.368941	9.674911	39	10.325089	10.043852	39	9.956148	20	38	9.956148	39	10.043852	9.675074	39	10.324926	10.368807
0	39	9.631192	39	10.368807	9.675074	40	10.324926	10.043882	40	9.956118	20	39	9.956118	40	10.043882	9.675237	40	10.324763	10.368674
0	40	9.631326	40	10.368674	9.675237	41	10.324763	10.043911	41	9.956089	20	40	9.956089	41	10.043911	9.675401	41	10.324600	10.368541
0	41	9.631459	41	10.368541	9.675401	42	10.324600	10.043941	42	9.956059	20	41	9.956059	42	10.043941	9.675564	42	10.324437	10.368407
0	42	9.631593	42	10.368407	9.675564	43	10.324437	10.043971	43	9.956029	20	42	9.956029	43	10.043971	9.675727	43	10.324273	10.368274
0	43	9.631726	43	10.368274	9.675727	44	10.324273	10.044001	44	9.955999	20	43	9.955999	44	10.044001	9.675890	44	10.324110	10.368141
0	44	9.631859	44	10.368141	9.675890	45	10.324110	10.044031	45	9.955969	20	44	9.955969	45	10.044031	9.676053	45	10.323947	10.368008
0	45	9.631992	45	10.368008	9.676053	46	10.323947	10.044061	46	9.955939	20	45	9.955939	46	10.044061	9.676217	46	10.323783	10.367875
0	46	9.632125	46	10.367875	9.676217	47	10.323783	10.044091	47	9.955909	20	46	9.955909	47	10.044091	9.676380	47	10.323620	10.367741
0	47	9.632258	47	10.367741	9.676380	48	10.323620	10.044121	48	9.955879	20	47	9.955879	48	10.044121	9.676545	48	10.323457	10.367607
0	48	9.632392	48	10.367607	9.676545	49	10.323457	10.044151	49	9.955849	20	48	9.955849	49	10.044151	9.676706	49	10.323294	10.367475
0	49	9.632525	49	10.367475	9.676706	50	10.323294	10.044181	50	9.955819	20	49	9.955819	50	10.044181	9.676869	50	10.323131	10.367342
0	50	9.632658	50	10.367342	9.676869	51	10.323131	10.044211	51	9.955789	20	50	9.955789	51	10.044211	9.677032	51	10.322968	

LOG. SINES, COSINES, &c.

1 ^h 42 ^m										25°									
°	'	''	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	'	''	m.	'	''	m.
30	0			9°633984		10°366016	9°678496		10°321504	10°044512		9°955488	18	30					
30	1			9°634117	1" 4	10°365883	9°678659	1" 5	10°321341	10°044542	1" 1	9°955458	50	30					
31	1			9°634249	2 9	10°365751	9°678821	2 11	10°321179	10°044572	2 2	9°955428	50	21					
30	0			9°634381	3 13	10°365619	9°678984	3 16	10°321016	10°044602	3 3	9°955398	50	30					
32	8			9°634514	4 18	10°365486	9°679146	4 22	10°320854	10°044632	4 4	9°955368	52	21					
30	10			9°634646	5 22	10°365354	9°679308	5 27	10°320692	10°044663	5 5	9°955337	50	30					
33	12			9°634778	6 26	10°365222	9°679471	6 32	10°320529	10°044693	6 6	9°955307	48	27					
30	14			9°634910	7 31	10°365090	9°679633	7 38	10°320367	10°044723	7 7	9°955277	46	30					
34	16			9°635042	8 35	10°364958	9°679795	8 43	10°320205	10°044753	8 8	9°955247	44	26					
30	18			9°635174	9 40	10°364826	9°679958	9 49	10°320043	10°044783	9 9	9°955217	42	30					
35	20			9°635306	10 44	10°364694	9°680120	10 54	10°319880	10°044814	10 10	9°955186	40	26					
30	22			9°635438	11 48	10°364562	9°680282	11 59	10°319718	10°044844	11 11	9°955156	38	30					
36	24			9°635570	12 53	10°364430	9°680444	12 65	10°319556	10°044874	12 12	9°955126	36	24					
30	26			9°635702	13 57	10°364298	9°680606	13 70	10°319394	10°044904	13 13	9°955096	34	30					
37	28			9°635834	14 61	10°364166	9°680768	14 76	10°319232	10°044935	14 14	9°955065	32	23					
30	30			9°635965	15 66	10°364035	9°680930	15 81	10°319070	10°044965	15 15	9°955035	30	30					
38	32			9°636097	16 70	10°363903	9°681092	16 86	10°318908	10°044995	16 16	9°955005	28	22					
30	34			9°636229	17 75	10°363771	9°681254	17 92	10°318746	10°045026	17 17	9°954974	26	30					
39	36			9°636360	18 79	10°363640	9°681416	18 97	10°318584	10°045056	18 18	9°954944	24	21					
30	38			9°636492	19 83	10°363508	9°681578	19 103	10°318422	10°045086	19 19	9°954914	22	30					
40	40			9°636623	20 88	10°363377	9°681740	20 108	10°318260	10°045117	20 20	9°954883	20	20					
30	42			9°636754	21 92	10°363246	9°681901	21 113	10°318099	10°045147	21 21	9°954853	18	30					
41	44			9°636886	22 96	10°363114	9°682063	22 119	10°317937	10°045177	22 22	9°954823	16	19					
30	46			9°637017	23 101	10°362983	9°682225	23 124	10°317775	10°045208	23 23	9°954792	14	30					
42	48			9°637148	24 105	10°362852	9°682387	24 130	10°317613	10°045238	24 24	9°954762	12	18					
30	50			9°637280	25 110	10°362720	9°682548	25 135	10°317452	10°045268	25 25	9°954732	10	30					
43	52			9°637411	26 114	10°362589	9°682710	26 140	10°317290	10°045299	26 26	9°954701	8	17					
30	54			9°637542	27 119	10°362458	9°682871	27 146	10°317129	10°045329	27 27	9°954671	6	30					
44	56			9°637673	28 123	10°362327	9°683033	28 151	10°316967	10°045359	28 28	9°954640	4	16					
30	58			9°637804	29 127	10°362196	9°683194	29 157	10°316806	10°045390	29 29	9°954610	2	30					
45	60			9°637935	30 132	10°362065	9°683356	30 162	10°316644	10°045421	30 30	9°954579	27	15					
30	2			9°638066	1 4	10°361934	9°683517	1 5	10°316483	10°045451	1 1	9°954549	56	30					
46	4			9°638197	2 9	10°361803	9°683679	2 11	10°316321	10°045482	2 2	9°954518	56	14					
30	6			9°638328	3 13	10°361672	9°683840	3 16	10°316160	10°045512	3 3	9°954488	54	30					
47	8			9°638459	4 17	10°361541	9°684001	4 21	10°315999	10°045543	4 4	9°954457	52	13					
30	10			9°638589	5 22	10°361411	9°684162	5 27	10°315838	10°045573	5 5	9°954427	50	30					
48	12			9°638720	6 26	10°361280	9°684324	6 32	10°315676	10°045604	6 6	9°954396	48	12					
30	14			9°638851	7 31	10°361149	9°684485	7 38	10°315515	10°045634	7 7	9°954366	46	30					
49	16			9°638981	8 35	10°361019	9°684646	8 43	10°315354	10°045665	8 8	9°954335	44	11					
30	18			9°639112	9 39	10°360888	9°684807	9 48	10°315193	10°045695	9 9	9°954305	42	30					
50	20			9°639242	10 43	10°360757	9°684968	10 54	10°315032	10°045726	10 10	9°954274	40	10					
30	22			9°639373	11 48	10°360627	9°685129	11 59	10°314871	10°045757	11 11	9°954243	38	30					
51	24			9°639503	12 52	10°360497	9°685290	12 64	10°314710	10°045787	12 12	9°954213	36	9					
30	26			9°639633	13 56	10°360367	9°685451	13 70	10°314549	10°045818	13 13	9°954182	34	30					
52	28			9°639764	14 61	10°360236	9°685612	14 75	10°314388	10°045848	14 14	9°954152	32	8					
30	30			9°639894	15 65	10°360106	9°685773	15 80	10°314227	10°045879	15 15	9°954121	30	30					
53	32			9°640024	16 69	10°359976	9°685934	16 86	10°314066	10°045910	16 16	9°954090	28	7					
30	34			9°640154	17 74	10°359846	9°686095	17 91	10°313905	10°045940	17 17	9°954060	26	30					
54	36			9°640284	18 78	10°359716	9°686255	18 96	10°313745	10°045971	18 18	9°954029	24	6					
30	38			9°640414	19 82	10°359586	9°686416	19 102	10°313584	10°046002	19 19	9°953998	22	30					
55	40			9°640544	20 87	10°359456	9°686577	20 107	10°313423	10°046032	20 20	9°953968	20	5					
30	42			9°640674	21 91	10°359326	9°686737	21 113	10°313263	10°046063	21 21	9°953937	18	30					
56	44			9°640804	22 95	10°359196	9°686898	22 118	10°313102	10°046094	22 22	9°953906	16	4					
30	46			9°640934	23 100	10°359066	9°687059	23 123	10°312941	10°046124	23 23	9°953876	14	30					
57	48			9°641064	24 104	10°358936	9°687219	24 129	10°312781	10°046155	24 24	9°953845	12	3					
30	50			9°641194	25 109	10°358806	9°687380	25 134	10°312620	10°046186	25 25	9°953814	10	30					
58	52			9°641324	26 113	10°358676	9°687540	26 139	10°312460	10°046217	26 27	9°953783	8	2					
30	54			9°641453	27 117	10°358547	9°687701	27 145	10°312299	10°046247	27 28	9°953753	6	30					
59	56			9°641583	28 122	10°358417	9°687861	28 150	10°312139	10°046278	28 29	9°953722	4	1					
30	58			9°641712	29 126	10°358288	9°688021	29 155	10°311979	10°046309	29 30	9°953691	2	30					
60	60			9°641842	30 130	10°358158	9°688182	30 161	10°311818	10°046340	30 31	9°953660	0	0					
°	'	''	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	'	''	m.	'	''	m.

LOG. SINES, COSINES, &c.

1 ^h 44 ^m												26°											
°	'	''	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	°	'	''	m.	Cosine	Parts	Secant	Parts	Tangent	Cotang.	Parts	
0	0	0	0	9°641842		10°358158	9°688182		10°311818	10°046340		0	0	0	0	9°953660	10°	10°	10°	10°	10°	10°	
30	2	0	0	9°641971	1" 4	10°358029	9°688342	1" 5	10°311658	10°046371	1" 1	30	2	0	0	9°953629	30	30	30	30	30	30	
1	4	0	0	9°642101	2 9	10°357899	9°688502	2 11	10°311498	10°046401	2 2	1	4	0	0	9°953599	54	59	54	59	54	59	
6	6	0	0	9°642230	3 13	10°357770	9°688663	3 16	10°311337	10°046432	3 3	6	6	0	0	9°953568	54	30	54	30	54	30	
2	8	0	0	9°642360	4 17	10°357640	9°688823	4 21	10°311177	10°046463	4 4	2	8	0	0	9°953537	32	58	32	58	32	58	
10	10	0	0	9°642489	5 21	10°357511	9°688983	5 27	10°311017	10°046494	5 5	10	10	0	0	9°953506	50	20	50	20	50	20	
3	12	0	0	9°642618	6 26	10°357382	9°689143	6 32	10°310857	10°046525	6 6	3	12	0	0	9°953475	48	57	48	57	48	57	
30	14	0	0	9°642747	7 30	10°357253	9°689303	7 37	10°310697	10°046556	7 7	30	14	0	0	9°953444	46	30	46	30	46	30	
4	16	0	0	9°642877	8 34	10°357123	9°689463	8 43	10°310537	10°046587	8 8	4	16	0	0	9°953413	44	56	44	56	44	56	
30	18	0	0	9°643006	9 39	10°356994	9°689623	9 48	10°310377	10°046618	9 9	30	18	0	0	9°953382	42	30	42	30	42	30	
5	20	0	0	9°643135	10 43	10°356865	9°689783	10 53	10°310217	10°046648	10 10	5	20	0	0	9°953352	40	55	40	55	40	55	
30	22	0	0	9°643264	11 47	10°356736	9°689943	11 59	10°310057	10°046679	11 11	30	22	0	0	9°953321	38	30	38	30	38	30	
6	24	0	0	9°643393	12 51	10°356607	9°690103	12 64	10°309897	10°046710	12 12	6	24	0	0	9°953290	36	54	36	54	36	54	
30	26	0	0	9°643522	13 56	10°356478	9°690263	13 69	10°309737	10°046741	13 13	30	26	0	0	9°953259	34	30	34	30	34	30	
7	28	0	0	9°643650	14 60	10°356350	9°690423	14 75	10°309577	10°046772	14 14	7	28	0	0	9°953228	32	53	32	53	32	53	
30	30	0	0	9°643779	15 64	10°356221	9°690582	15 80	10°309418	10°046803	15 15	30	30	0	0	9°953197	30	30	30	30	30	30	
8	32	0	0	9°643908	16 68	10°356092	9°690742	16 85	10°309258	10°046834	16 16	8	32	0	0	9°953166	28	52	28	52	28	52	
30	34	0	0	9°644037	17 73	10°355963	9°690902	17 91	10°309098	10°046865	17 18	30	34	0	0	9°953135	26	30	26	30	26	30	
9	36	0	0	9°644165	18 77	10°355833	9°691062	18 96	10°308938	10°046896	18 19	9	36	0	0	9°953104	24	51	24	51	24	51	
30	38	0	0	9°644294	19 82	10°355706	9°691221	19 101	10°308779	10°046927	19 20	30	38	0	0	9°953073	22	30	22	30	22	30	
10	40	0	0	9°644423	20 86	10°355577	9°691381	20 107	10°308619	10°046958	20 21	10	40	0	0	9°953042	20	50	20	50	20	50	
30	42	0	0	9°644551	21 90	10°355449	9°691540	21 112	10°308460	10°046989	21 22	30	42	0	0	9°953011	18	30	18	30	18	30	
11	44	0	0	9°644680	22 94	10°355320	9°691700	22 117	10°308300	10°047020	22 23	11	44	0	0	9°952980	16	49	16	49	16	49	
30	46	0	0	9°644808	23 99	10°355192	9°691859	23 123	10°308141	10°047051	23 24	30	46	0	0	9°952949	14	30	14	30	14	30	
12	48	0	0	9°644936	24 103	10°355064	9°692019	24 128	10°307982	10°047082	24 25	12	48	0	0	9°952918	12	48	12	48	12	48	
30	50	0	0	9°645065	25 107	10°354935	9°692178	25 133	10°307822	10°047112	25 26	30	50	0	0	9°952886	10	30	10	30	10	30	
13	52	0	0	9°645193	26 112	10°354807	9°692338	26 139	10°307662	10°047145	26 27	13	52	0	0	9°952855	8	47	13	47	13	47	
30	54	0	0	9°645321	27 116	10°354679	9°692497	27 144	10°307503	10°047176	27 28	30	54	0	0	9°952824	6	30	27	28	27	28	
14	56	0	0	9°645450	28 120	10°354550	9°692656	28 149	10°307344	10°047207	28 29	14	56	0	0	9°952793	4	46	28	29	28	29	
30	58	0	0	9°645578	29 124	10°354422	9°692816	29 155	10°307184	10°047238	29 30	30	58	0	0	9°952762	2	30	29	30	29	30	
15	00	0	0	9°645706	30 129	10°354294	9°692975	30 160	10°307025	10°047269	30 31	15	00	0	0	9°952731	2	45	30	31	30	31	
30	2	0	0	9°645834	1 4	10°354166	9°693134	1 5	10°306866	10°047300	1 1	30	2	0	0	9°952700	30	44	30	1	30	1	
16	4	0	0	9°645962	2 9	10°354038	9°693293	2 11	10°306707	10°047331	2 2	16	4	0	0	9°952669	28	30	16	4	16	4	
30	6	0	0	9°646090	3 13	10°353910	9°693453	3 16	10°306547	10°047363	3 3	30	6	0	0	9°952637	26	30	16	6	16	6	
17	8	0	0	9°646218	4 17	10°353782	9°693612	4 21	10°306388	10°047394	4 4	17	8	0	0	9°952606	24	43	17	8	17	8	
30	10	0	0	9°646346	5 21	10°353654	9°693771	5 27	10°306229	10°047425	5 5	30	10	0	0	9°952575	22	30	17	10	17	10	
18	12	0	0	9°646474	6 25	10°353526	9°693930	6 32	10°306070	10°047456	6 6	18	12	0	0	9°952544	20	42	18	12	18	12	
30	14	0	0	9°646601	7 30	10°353399	9°694089	7 37	10°305911	10°047488	7 7	30	14	0	0	9°952512	18	30	18	14	18	14	
19	16	0	0	9°646729	8 34	10°353271	9°694248	8 42	10°305752	10°047519	8 8	19	16	0	0	9°952481	16	41	19	16	19	16	
30	18	0	0	9°646857	9 39	10°353143	9°694407	9 48	10°305593	10°047550	9 9	30	18	0	0	9°952450	14	30	19	18	19	18	
20	20	0	0	9°646984	10 43	10°353016	9°694566	10 53	10°305434	10°047581	10 10	20	20	0	0	9°952419	12	40	20	20	20	20	
30	22	0	0	9°647112	11 47	10°352888	9°694724	11 59	10°305276	10°047613	11 11	30	22	0	0	9°952387	10	30	20	22	20	22	
21	24	0	0	9°647240	12 51	10°352760	9°694883	12 64	10°305117	10°047644	12 13	21	24	0	0	9°952356	8	39	21	24	21	24	
30	26	0	0	9°647367	13 56	10°352633	9°695042	13 69	10°304958	10°047675	13 14	30	26	0	0	9°952325	6	30	21	26	21	26	
22	28	0	0	9°647494	14 59	10°352506	9°695201	14 74	10°304799	10°047706	14 15	22	28	0	0	9°952294	4	38	22	28	22	28	
30	30	0	0	9°647622	15 64	10°352378	9°695360	15 79	10°304640	10°047738	15 16	30	30	0	0	9°952262	2	30	22	30	22	30	
23	32	0	0	9°647749	16 68	10°352251	9°695518	16 85	10°304482	10°047769	16 17	23	32	0	0	9°952231	2	37	23	32	23	32	
30	34	0	0	9°647877	17 73	10°352123	9°695677	17 91	10°304323	10°047800	17 18	30	34	0	0	9°952200	2	30	23	34	23	34	
24	36	0	0	9°648004	18 77	10°351996	9°695836	18 96	10°304164	10°047832	18 19	24	36	0	0	9°952168	2	36	24	36	24	36	
30	38	0	0	9°648131	19 82	10°351869	9°695994	19 101	10°304006	10°047863	19 20	30	38	0	0	9°952137	2	30	24	38	24	38	
25	40	0	0	9°648258	20 86	10°351742	9°696153	20 106	10°303847	10°047894	20 21	25	40	0	0	9°952106	2	35	25	40	25	40	
30	42	0	0	9°648385	21 90	10°351615	9°696311	21 111	10°303689	10°047926	21 22	30	42	0	0	9°952074	18	30	25	42	25	42	
26	44	0	0	9°648512	22 94	10°351488	9°696470	22 116	10°303530	10°047957	22 23	26	44	0	0	9°							

LOG. SINES, COSINES, &c.

1 ^h 46 ^m												26°											
''	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	''	''	m.	''	''	''	''	''	''	''	''	''
30	0	9°549527		10°350473	9°697736		10°302264	10°048209		9°951791	14	30											
30	2	9°549654	1"	10°350346	9°697894	1"	10°302106	10°048240	1"	9°951760	14	30											
31	4	9°549781	2	10°350219	9°698053	2	10°301947	10°048272	2	9°951728	14	28											
30	6	9°549907	3	10°350093	9°698211	3	10°301789	10°048303	3	9°951697	14	26											
32	8	9°550034	4	10°349966	9°698369	4	10°301631	10°048335	4	9°951665	14	24											
32	10	9°550160	5	10°349840	9°698527	5	10°301473	10°048366	5	9°951634	14	22											
33	12	9°550287	6	10°349713	9°698685	6	10°301315	10°048398	6	9°951602	14	20											
30	14	9°550413	7	10°349587	9°698843	7	10°301157	10°048430	7	9°951570	14	18											
34	16	9°550539	8	10°349461	9°699001	8	10°300999	10°048461	8	9°951539	14	16											
34	18	9°550666	9	10°349334	9°699159	9	10°300841	10°048493	9	9°951507	14	14											
36	20	9°550792	10	10°349208	9°699316	10	10°300684	10°048524	10	9°951476	14	12											
30	22	9°550918	11	10°349082	9°699474	11	10°300526	10°048556	11	9°951444	14	10											
36	24	9°551044	12	10°348956	9°699632	12	10°300368	10°048588	12	9°951412	14	8											
30	26	9°551171	13	10°348829	9°699790	13	10°300210	10°048619	13	9°951381	14	6											
37	28	9°551297	14	10°348703	9°699947	14	10°300053	10°048651	14	9°951349	14	4											
37	30	9°551423	15	10°348577	9°700105	15	10°299895	10°048683	15	9°951317	14	2											
38	32	9°551549	16	10°348451	9°700263	16	10°299737	10°048714	16	9°951286	14	0											
30	34	9°551675	17	10°348325	9°700420	17	10°299580	10°048746	17	9°951254	14	30											
30	36	9°551800	18	10°348200	9°700578	18	10°299422	10°048778	18	9°951222	14	28											
30	38	9°551926	19	10°348074	9°700736	19	10°299264	10°048809	19	9°951191	14	26											
40	40	9°552052	20	10°347948	9°700893	20	10°299107	10°048841	20	9°951159	14	24											
30	42	9°552178	21	10°347822	9°701051	21	10°298949	10°048873	21	9°951127	14	22											
41	44	9°552304	22	10°347696	9°701208	22	10°298792	10°048904	22	9°951096	14	20											
30	46	9°552429	23	10°347571	9°701365	23	10°298635	10°048936	23	9°951064	14	18											
42	48	9°552555	24	10°347445	9°701523	24	10°298477	10°048968	24	9°951032	14	16											
42	50	9°552680	25	10°347320	9°701680	25	10°298320	10°049000	25	9°951000	14	14											
43	52	9°552806	26	10°347194	9°701837	26	10°298163	10°049032	26	9°950968	14	12											
30	54	9°552931	27	10°347069	9°701995	27	10°298005	10°049063	27	9°950937	14	10											
44	56	9°553057	28	10°346943	9°702152	28	10°297848	10°049095	28	9°950905	14	8											
30	58	9°553182	29	10°346818	9°702309	29	10°297691	10°049127	29	9°950873	14	6											
46	60	9°553308	30	10°346692	9°702466	30	10°297534	10°049159	30	9°950841	14	4											
30	2	9°553433	1	10°346567	9°702623	1	10°297377	10°049191	1	9°950809	14	2											
48	4	9°553558	2	10°346442	9°702781	2	10°297219	10°049222	2	9°950778	14	0											
30	6	9°553683	3	10°346317	9°702938	3	10°297062	10°049254	3	9°950746	14	30											
47	8	9°553808	4	10°346192	9°703095	4	10°296905	10°049286	4	9°950714	14	28											
30	10	9°553934	5	10°346066	9°703252	5	10°296748	10°049318	5	9°950682	14	26											
48	12	9°554059	6	10°345941	9°703409	6	10°296591	10°049350	6	9°950650	14	24											
30	14	9°554184	7	10°345816	9°703566	7	10°296434	10°049382	7	9°950618	14	22											
40	16	9°554309	8	10°345691	9°703722	8	10°296278	10°049414	8	9°950586	14	20											
30	18	9°554434	9	10°345566	9°703879	9	10°296121	10°049446	9	9°950554	14	18											
50	20	9°554558	10	10°345442	9°704036	10	10°295964	10°049478	10	9°950522	14	16											
30	22	9°554683	11	10°345317	9°704193	11	10°295807	10°049510	11	9°950490	14	14											
51	24	9°554808	12	10°345192	9°704350	12	10°295650	10°049542	12	9°950458	14	12											
30	26	9°554933	13	10°345067	9°704506	13	10°295494	10°049574	13	9°950426	14	10											
52	28	9°555058	14	10°344942	9°704663	14	10°295337	10°049606	14	9°950394	14	8											
30	30	9°555182	15	10°344818	9°704820	15	10°295180	10°049638	15	9°950362	14	6											
53	32	9°555307	16	10°344693	9°704976	16	10°295024	10°049670	16	9°950330	14	4											
30	34	9°555431	17	10°344569	9°705133	17	10°294867	10°049702	17	9°950298	14	2											
54	36	9°555556	18	10°344444	9°705290	18	10°294710	10°049734	18	9°950266	14	0											
30	38	9°555680	19	10°344320	9°705446	19	10°294553	10°049766	19	9°950234	14	30											
55	40	9°555805	20	10°344195	9°705603	20	10°294397	10°049798	20	9°950202	14	28											
30	42	9°555929	21	10°344071	9°705759	21	10°294241	10°049830	21	9°950170	14	26											
56	44	9°556054	22	10°343946	9°705916	22	10°294084	10°049862	22	9°950138	14	24											
30	46	9°556178	23	10°343822	9°706072	23	10°293928	10°049894	23	9°950106	14	22											
57	48	9°556302	24	10°343698	9°706228	24	10°293772	10°049926	24	9°950074	14	20											
30	50	9°556426	25	10°343574	9°706385	25	10°293615	10°049958	25	9°950042	14	18											
58	52	9°556551	26	10°343449	9°706541	26	10°293459	10°049990	26	9°950010	14	16											
30	54	9°556675	27	10°343325	9°706697	27	10°293303	10°050022	27	9°949978	14	14											
59	56	9°556799	28	10°343201	9°706854	28	10°293146	10°050055	28	9°949946	14	12											
30	58	9°556923	29	10°343077	9°707010	29	10°292990	10°050087	29	9°949914	14	10											
60	60	9°557047	30	10°342953	9°707166	30	10°292834	10°050119	30	9°949882	14	8											
''	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	''	''	m.	''	''	''	''	''	''	''	''	''

LOG. SINES, COSINES, &c.

1° 48'				27°								
''	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	''
0	0	9°57047		10°342953	9°707166		10°292834	10°050119		9°949881	12	60
1	2	9°57171	1 4	10°342829	9°707322	1 5	10°292678	10°050151	1 1	9°949849	38	20
2	4	9°57295	2 8	10°342705	9°707478	2 10	10°292522	10°050184	2 2	9°949816	56	59
3	6	9°57418	3 12	10°342582	9°707634	3 16	10°292366	10°050216	3 3	9°949784	74	30
4	8	9°57542	4 16	10°342458	9°707790	4 21	10°292210	10°050248	4 4	9°949752	92	58
5	10	9°57666	5 21	10°342334	9°707946	5 26	10°292054	10°050280	5 5	9°949720	110	20
6	12	9°57790	6 25	10°342210	9°708102	6 31	10°291898	10°050312	6 6	9°949688	128	57
7	14	9°57913	7 29	10°342087	9°708258	7 36	10°291742	10°050345	7 8	9°949655	146	20
8	16	9°58037	8 33	10°341963	9°708414	8 42	10°291586	10°050377	8 9	9°949623	164	56
9	18	9°58161	9 37	10°341839	9°708570	9 47	10°291430	10°050409	9 10	9°949591	182	20
10	20	9°58284	10 41	10°341716	9°708726	10 52	10°291274	10°050442	10 11	9°949558	200	55
11	22	9°58408	11 45	10°341592	9°708882	11 57	10°291118	10°050474	11 12	9°949526	218	20
12	24	9°58531	12 49	10°341469	9°709037	12 62	10°290963	10°050506	12 13	9°949494	236	54
13	26	9°58655	13 53	10°341345	9°709193	13 67	10°290807	10°050538	13 14	9°949462	254	20
14	28	9°58778	14 57	10°341222	9°709349	14 73	10°290651	10°050571	14 15	9°949430	272	53
15	30	9°58901	15 62	10°341099	9°709504	15 78	10°290496	10°050603	15 16	9°949397	290	20
16	32	9°59025	16 66	10°340975	9°709660	16 83	10°290340	10°050636	16 17	9°949364	308	52
17	34	9°59148	17 70	10°340852	9°709816	17 88	10°290184	10°050668	17 18	9°949332	326	20
18	36	9°59271	18 74	10°340729	9°709971	18 93	10°290029	10°050700	18 19	9°949300	344	51
19	38	9°59394	19 78	10°340606	9°710127	19 99	10°289873	10°050733	19 21	9°949267	362	20
20	40	9°59517	20 82	10°340483	9°710282	20 104	10°289718	10°050765	20 22	9°949235	380	50
21	42	9°59640	21 86	10°340360	9°710438	21 109	10°289562	10°050798	21 23	9°949202	398	20
22	44	9°59763	22 90	10°340237	9°710593	22 114	10°289407	10°050830	22 24	9°949170	416	49
23	46	9°59886	23 95	10°340114	9°710749	23 119	10°289251	10°050862	23 25	9°949138	434	20
24	48	9°60009	24 99	10°339991	9°710904	24 125	10°289096	10°050895	24 26	9°949105	452	48
25	50	9°60132	25 103	10°339868	9°711059	25 130	10°288941	10°050927	25 27	9°949073	470	20
26	52	9°60255	26 107	10°339745	9°711215	26 135	10°288785	10°050960	26 28	9°949040	488	47
27	54	9°60378	27 111	10°339622	9°711370	27 140	10°288630	10°050992	27 29	9°949008	506	20
28	56	9°60501	28 115	10°339499	9°711525	28 145	10°288475	10°051025	28 30	9°948975	524	46
29	58	9°60624	29 119	10°339377	9°711681	29 151	10°288319	10°051057	29 31	9°948943	542	20
30	60	9°60746	30 123	10°339254	9°711836	30 156	10°288164	10°051090	30 32	9°948910	560	45
31	2	9°60869	1 4	10°339131	9°711991	1 5	10°288009	10°051122	1 1	9°948878	578	20
32	4	9°60991	2 8	10°339009	9°712146	2 10	10°287854	10°051155	2 2	9°948845	596	44
33	6	9°61114	3 12	10°338886	9°712301	3 15	10°287699	10°051188	3 3	9°948812	614	20
34	8	9°61236	4 16	10°338764	9°712456	4 21	10°287544	10°051220	4 4	9°948780	632	43
35	10	9°61359	5 20	10°338641	9°712611	5 26	10°287389	10°051253	5 5	9°948747	650	20
36	12	9°61481	6 24	10°338519	9°712766	6 31	10°287234	10°051285	6 7	9°948715	668	42
37	14	9°61603	7 28	10°338397	9°712921	7 36	10°287079	10°051318	7 8	9°948682	686	20
38	16	9°61726	8 33	10°338274	9°713076	8 41	10°286924	10°051350	8 9	9°948650	704	41
39	18	9°61848	9 37	10°338152	9°713231	9 46	10°286769	10°051383	9 10	9°948617	722	20
40	20	9°61970	10 41	10°338030	9°713386	10 52	10°286614	10°051416	10 11	9°948584	740	40
41	22	9°62092	11 45	10°337908	9°713541	11 57	10°286459	10°051448	11 12	9°948552	758	20
42	24	9°62214	12 49	10°337786	9°713696	12 62	10°286304	10°051481	12 13	9°948519	776	39
43	26	9°62337	13 53	10°337663	9°713850	13 67	10°286150	10°051514	13 14	9°948486	794	20
44	28	9°62459	14 57	10°337541	9°714005	14 72	10°285995	10°051546	14 15	9°948454	812	38
45	30	9°62581	15 61	10°337419	9°714160	15 77	10°285840	10°051579	15 16	9°948421	830	20
46	32	9°62703	16 65	10°337297	9°714314	16 83	10°285686	10°051612	16 17	9°948388	848	37
47	34	9°62825	17 69	10°337175	9°714469	17 88	10°285531	10°051645	17 18	9°948355	866	20
48	36	9°62948	18 73	10°337054	9°714624	18 93	10°285376	10°051677	18 19	9°948323	884	36
49	38	9°63070	19 77	10°336932	9°714778	19 98	10°285222	10°051710	19 21	9°948290	902	20
50	40	9°63192	20 81	10°336810	9°714933	20 103	10°285067	10°051743	20 22	9°948257	920	35
51	42	9°63314	21 85	10°336688	9°715087	21 108	10°284913	10°051776	21 23	9°948224	938	20
52	44	9°63437	22 89	10°336567	9°715242	22 114	10°284758	10°051808	22 24	9°948192	956	34
53	46	9°63559	23 94	10°336445	9°715396	23 119	10°284604	10°051841	23 25	9°948159	974	20
54	48	9°63681	24 98	10°336323	9°715551	24 124	10°284449	10°051874	24 26	9°948126	992	33
55	50	9°63798	25 102	10°336202	9°715705	25 129	10°284295	10°051907	25 27	9°948093	1010	20
56	52	9°63920	26 106	10°336080	9°715860	26 134	10°284140	10°051940	26 28	9°948060	1028	32
57	54	9°64041	27 110	10°335959	9°716014	27 139	10°283986	10°051972	27 29	9°948028	1046	20
58	56	9°64163	28 114	10°335837	9°716168	28 144	10°283832	10°052005	28 31	9°947995	1064	31
59	58	9°64284	29 118	10°335716	9°716322	29 150	10°283678	10°052038	29 32	9°947962	1082	20
60	60	9°64406	30 122	10°335594	9°716477	30 155	10°283523	10°052071	30 33	9°947929	1100	30
''	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	''

LOG. SINES, COSINES, &c.

1 ^h 50 ^m											
27°											
°	'	''	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts
30	0			9°664406		10°335594	9°716477		10°283523	10°052071	9°947929
30	1			9°664527	1"	10°335473	9°716631	1"	10°283369	10°052104	9°947896
30	2			9°664648	2	10°335352	9°716785	2	10°283215	10°052137	9°947863
31	4			9°664769	3	10°335231	9°716939	3	10°283061	10°052170	9°947830
32	8			9°664891	4	10°335109	9°717093	4	10°282907	10°052203	9°947797
33	10			9°665012	5	10°334988	9°717247	5	10°282753	10°052236	9°947764
33	12			9°665133	6	10°334867	9°717401	6	10°282599	10°052269	9°947731
34	14			9°665254	7	10°334746	9°717555	7	10°282445	10°052302	9°947698
34	16			9°665375	8	10°334625	9°717709	8	10°282291	10°052335	9°947665
35	18			9°665496	9	10°334504	9°717863	9	10°282137	10°052367	9°947633
35	20			9°665617	10	10°334383	9°718017	10	10°281983	10°052400	9°947600
36	22			9°665738	11	10°334262	9°718171	11	10°281829	10°052433	9°947567
36	24			9°665859	12	10°334141	9°718325	12	10°281675	10°052467	9°947533
36	26			9°665979	13	10°334021	9°718479	13	10°281521	10°052500	9°947500
37	28			9°666100	14	10°333900	9°718633	14	10°281367	10°052533	9°947467
37	30			9°666221	15	10°333779	9°718786	15	10°281214	10°052566	9°947434
38	32			9°666342	16	10°333658	9°718940	16	10°281060	10°052599	9°947401
38	34			9°666462	17	10°333537	9°719094	17	10°280906	10°052632	9°947368
39	36			9°666583	18	10°333417	9°719248	18	10°280752	10°052665	9°947335
39	38			9°666703	19	10°333297	9°719401	19	10°280599	10°052698	9°947302
40	40			9°666824	20	10°333176	9°719555	20	10°280445	10°052731	9°947269
40	42			9°666944	21	10°333056	9°719708	21	10°280292	10°052764	9°947236
41	44			9°667065	22	10°332935	9°719862	22	10°280138	10°052797	9°947203
41	46			9°667185	23	10°332815	9°720016	23	10°279984	10°052830	9°947170
42	48			9°667305	24	10°332695	9°720169	24	10°279831	10°052864	9°947136
42	50			9°667426	25	10°332574	9°720322	25	10°279678	10°052897	9°947103
43	52			9°667546	26	10°332454	9°720476	26	10°279524	10°052930	9°947070
43	54			9°667666	27	10°332334	9°720629	27	10°279371	10°052963	9°947037
44	56			9°667786	28	10°332214	9°720783	28	10°279217	10°052996	9°947004
44	58			9°667906	29	10°332094	9°720936	29	10°279064	10°053030	9°946970
45	59			9°668027	30	10°331973	9°721089	30	10°278911	10°053063	9°946937
46	0			9°668147	1	10°331853	9°721243	1	10°278757	10°053096	9°946904
46	1			9°668267	2	10°331733	9°721396	2	10°278604	10°053129	9°946871
47	3			9°668386	3	10°331614	9°721549	3	10°278451	10°053163	9°946838
47	5			9°668506	4	10°331494	9°721702	4	10°278298	10°053196	9°946804
48	7			9°668626	5	10°331374	9°721855	5	10°278145	10°053229	9°946771
48	9			9°668746	6	10°331254	9°722009	6	10°277991	10°053262	9°946738
48	11			9°668866	7	10°331134	9°722162	7	10°277838	10°053296	9°946704
49	13			9°668986	8	10°331014	9°722315	8	10°277685	10°053329	9°946671
49	15			9°669105	9	10°330895	9°722468	9	10°277532	10°053362	9°946638
50	17			9°669225	10	10°330775	9°722621	10	10°277379	10°053396	9°946604
50	19			9°669345	11	10°330655	9°722774	11	10°277226	10°053429	9°946571
51	21			9°669464	12	10°330535	9°722927	12	10°277073	10°053462	9°946538
51	23			9°669584	13	10°330416	9°723080	13	10°276920	10°053496	9°946504
52	25			9°669703	14	10°330297	9°723232	14	10°276768	10°053529	9°946471
52	27			9°669823	15	10°330177	9°723385	15	10°276615	10°053563	9°946437
53	29			9°669942	16	10°330058	9°723538	16	10°276462	10°053596	9°946404
53	31			9°670061	17	10°329939	9°723691	17	10°276309	10°053629	9°946371
54	33			9°670181	18	10°329819	9°723844	18	10°276156	10°053663	9°946337
54	35			9°670300	19	10°329700	9°723996	19	10°276004	10°053696	9°946304
55	37			9°670419	20	10°329581	9°724149	20	10°275851	10°053730	9°946270
55	39			9°670538	21	10°329462	9°724302	21	10°275698	10°053763	9°946237
56	41			9°670658	22	10°329342	9°724454	22	10°275546	10°053797	9°946203
56	43			9°670777	23	10°329223	9°724607	23	10°275393	10°053830	9°946170
57	45			9°670896	24	10°329104	9°724760	24	10°275240	10°053864	9°946136
57	47			9°671015	25	10°328985	9°724912	25	10°275088	10°053897	9°946103
58	49			9°671134	26	10°328866	9°725065	26	10°274935	10°053931	9°946069
58	51			9°671253	27	10°328747	9°725217	27	10°274783	10°053964	9°946036
59	53			9°671372	28	10°328628	9°725370	28	10°274630	10°053998	9°946002
59	55			9°671490	29	10°328510	9°725522	29	10°274478	10°054031	9°945969
60	57			9°671609	30	10°328391	9°725674	30	10°274326	10°054065	9°945935
°	'	''	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts

LOG. SINES, COSINES. &c.

1° 52'		28'										30'	
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	mm.	°	'
0	0	9°671609		10°328391	9°725674		10°274326	10°054065		9°945935	8	60	00
30	2	9°671728	1" 4	10°328272	9°725827	1" 5	10°274173	10°054099	1" 1	9°945901	38	30	30
1	4	9°671847	2 8	10°328153	9°725979	2 10	10°274021	10°054132	2 2	9°945868	36	59	30
30	6	9°671965	3 12	10°328035	9°726131	3 15	10°273869	10°054166	3 3	9°945834	34	30	30
2	8	9°672084	4 16	10°327916	9°726284	4 20	10°273716	10°054200	4 4	9°945800	32	58	30
30	10	9°672203	5 20	10°327797	9°726436	5 25	10°273564	10°054233	5 6	9°945767	30	30	30
3	12	9°672321	6 24	10°327679	9°726588	6 30	10°273412	10°054267	6 7	9°945733	28	57	30
30	14	9°672440	7 28	10°327560	9°726740	7 35	10°273260	10°054300	7 8	9°945700	26	30	30
4	16	9°672558	8 32	10°327442	9°726892	8 40	10°273108	10°054334	8 9	9°945666	41	56	30
30	18	9°672677	9 35	10°327323	9°727045	9 46	10°272955	10°054368	9 10	9°945632	42	30	30
5	20	9°672795	10 39	10°327205	9°727197	10 51	10°272803	10°054402	10 11	9°945598	40	55	30
30	22	9°672914	11 43	10°327086	9°727349	11 56	10°272651	10°054435	11 12	9°945565	38	30	30
6	24	9°673032	12 47	10°326968	9°727501	12 61	10°272499	10°054469	12 13	9°945531	36	54	30
30	26	9°673150	13 51	10°326850	9°727653	13 66	10°272347	10°054503	13 15	9°945497	34	30	30
7	28	9°673268	14 55	10°326732	9°727805	14 71	10°272195	10°054536	14 16	9°945464	32	53	30
30	30	9°673387	15 59	10°326613	9°727957	15 76	10°272043	10°054570	15 17	9°945430	30	30	30
8	32	9°673505	16 63	10°326495	9°728109	16 81	10°271891	10°054604	16 18	9°945396	28	52	30
30	34	9°673623	17 67	10°326377	9°728261	17 86	10°271739	10°054638	17 19	9°945362	26	30	30
9	36	9°673741	18 71	10°326259	9°728412	18 91	10°271588	10°054672	18 20	9°945328	24	51	30
30	38	9°673859	19 75	10°326141	9°728564	19 96	10°271436	10°054705	19 21	9°945295	22	30	30
10	40	9°673977	20 79	10°326023	9°728716	20 101	10°271284	10°054739	20 23	9°945261	20	50	30
30	42	9°674095	21 83	10°325905	9°728868	21 106	10°271132	10°054773	21 24	9°945227	18	30	30
11	44	9°674213	22 87	10°325787	9°729020	22 111	10°270980	10°054807	22 25	9°945193	16	49	30
30	46	9°674331	23 91	10°325669	9°729171	23 116	10°270828	10°054841	23 26	9°945159	14	30	30
12	48	9°674448	24 95	10°325552	9°729323	24 121	10°270677	10°054875	24 27	9°945125	12	48	30
30	50	9°674566	25 99	10°325434	9°729475	25 126	10°270525	10°054908	25 28	9°945092	10	30	30
13	52	9°674684	26 103	10°325316	9°729626	26 132	10°270374	10°054942	26 29	9°945058	8	47	30
30	54	9°674802	27 106	10°325198	9°729778	27 137	10°270222	10°054976	27 30	9°945024	6	30	30
14	56	9°674919	28 110	10°325081	9°729929	28 142	10°270071	10°055010	28 31	9°944990	4	46	30
30	58	9°675037	29 114	10°324963	9°730081	29 147	10°269919	10°055044	29 32	9°944956	2	30	30
15	60	9°675155	30 118	10°324845	9°730233	30 152	10°269767	10°055078	30 34	9°944922	7	45	30
30	2	9°675272	1 4	10°324728	9°730384	1 5	10°269616	10°055112	1 1	9°944888	38	30	30
16	4	9°675390	2 8	10°324610	9°730535	2 10	10°269465	10°055146	2 2	9°944854	36	44	30
30	6	9°675507	3 12	10°324493	9°730687	3 15	10°269313	10°055180	3 3	9°944820	34	30	30
17	8	9°675624	4 16	10°324376	9°730838	4 20	10°269162	10°055214	4 5	9°944786	32	43	30
30	10	9°675742	5 19	10°324258	9°730990	5 25	10°269010	10°055248	5 6	9°944752	30	30	30
18	12	9°675859	6 23	10°324141	9°731141	6 30	10°268859	10°055282	6 7	9°944718	28	42	30
30	14	9°675976	7 27	10°324024	9°731292	7 35	10°268708	10°055316	7 8	9°944684	26	30	30
19	16	9°676094	8 31	10°323906	9°731444	8 40	10°268556	10°055350	8 9	9°944650	41	41	30
30	18	9°676211	9 35	10°323789	9°731595	9 45	10°268405	10°055384	9 10	9°944616	42	30	30
20	20	9°676328	10 39	10°323672	9°731746	10 50	10°268254	10°055418	10 11	9°944582	40	40	30
30	22	9°676445	11 43	10°323555	9°731897	11 55	10°268103	10°055452	11 12	9°944548	38	30	30
21	24	9°676562	12 47	10°323438	9°732048	12 60	10°267952	10°055486	12 14	9°944514	36	30	30
30	26	9°676679	13 51	10°323321	9°732200	13 65	10°267800	10°055520	13 15	9°944480	34	30	30
22	28	9°676796	14 55	10°323204	9°732351	14 70	10°267649	10°055554	14 16	9°944446	32	38	30
30	30	9°676913	15 58	10°323087	9°732502	15 75	10°267498	10°055588	15 17	9°944412	30	30	30
23	32	9°677030	16 62	10°322970	9°732653	16 80	10°267347	10°055623	16 18	9°944377	28	37	30
30	34	9°677147	17 66	10°322853	9°732804	17 86	10°267196	10°055657	17 19	9°944343	26	30	30
24	36	9°677264	18 70	10°322736	9°732955	18 91	10°267045	10°055691	18 20	9°944309	24	36	30
30	38	9°677381	19 74	10°322619	9°733106	19 96	10°266894	10°055725	19 22	9°944275	22	30	30
25	40	9°677498	20 78	10°322502	9°733257	20 101	10°266743	10°055759	20 23	9°944241	20	35	30
30	42	9°677614	21 82	10°322386	9°733408	21 106	10°266592	10°055793	21 24	9°944207	18	30	30
26	44	9°677731	22 86	10°322269	9°733558	22 111	10°266441	10°055828	22 25	9°944172	16	34	30
30	46	9°677848	23 90	10°322152	9°733709	23 116	10°266291	10°055862	23 26	9°944138	14	30	30
27	48	9°677964	24 93	10°322036	9°733860	24 121	10°266140	10°055896	24 27	9°944104	12	33	30
30	50	9°678081	25 97	10°321919	9°734011	25 126	10°265989	10°055930	25 28	9°944070	10	30	30
28	52	9°678197	26 101	10°321803	9°734162	26 131	10°265838	10°055964	26 29	9°944036	8	32	30
30	54	9°678314	27 105	10°321686	9°734312	27 136	10°265688	10°055999	27 31	9°944001	6	30	30
29	56	9°678430	28 109	10°321570	9°734463	28 141	10°265537	10°056033	28 32	9°943967	4	31	30
30	58	9°678547	29 113	10°321453	9°734614	29 146	10°265386	10°056067	29 33	9°943933	2	30	30
30	60	9°678663	30 117	10°321337	9°734764	30 151	10°265236	10°056101	30 34	9°943899	0	30	30

LOG. SINES, COSINES, &c.

1 ^h 54 ^m												28 ^u											
°		Sine		Parts		Cosine		Tangent		Parts		Cotang.		Secant		Parts		Cosine		m.		°	
30	0	9°678663				10°321337		9°734764				10°265236		10°056101				9°943899				30	0
30	1	9°678779	1"	4		10°321221		9°734915	1"	5		10°265085		10°056136	1"	1		9°943864	58	20		30	1
31	0	9°678895	2	8		10°321105		9°735066	2	10		10°264934		10°056170	2	2		9°943830	56	29		31	0
31	1	9°679012	3	12		10°320988		9°735216	3	15		10°264784		10°056204	3	3		9°943796	54	38		31	1
32	0	9°679128	4	15		10°320872		9°735367	4	20		10°264633		10°056239	4	5		9°943761	52	28		32	0
32	1	9°679244	5	19		10°320756		9°735517	5	25		10°264483		10°056273	5	6		9°943727	50	20		32	1
33	0	9°679360	6	23		10°320640		9°735668	6	30		10°264332		10°056307	6	7		9°943693	48	27		33	0
33	1	9°679476	7	27		10°320524		9°735818	7	35		10°264182		10°056342	7	8		9°943658	46	30		33	1
34	0	9°679592	8	31		10°320408		9°735969	8	40		10°264031		10°056376	8	9		9°943624	44	26		34	0
34	1	9°679708	9	35		10°320292		9°736119	9	45		10°263881		10°056411	9	10		9°943589	42	30		34	1
35	0	9°679824	10	39		10°320176		9°736269	10	50		10°263731		10°056445	10	11		9°943555	40	25		35	0
35	1	9°679940	11	42		10°320060		9°736420	11	55		10°263580		10°056479	11	13		9°943521	38	30		35	1
36	0	9°680056	12	46		10°319944		9°736570	12	60		10°263430		10°056514	12	14		9°943486	36	24		36	0
36	1	9°680172	13	50		10°319828		9°736720	13	65		10°263280		10°056548	13	15		9°943452	34	30		36	1
37	0	9°680288	14	54		10°319712		9°736870	14	70		10°263130		10°056583	14	16		9°943417	32	23		37	0
37	1	9°680403	15	58		10°319597		9°737021	15	75		10°262979		10°056617	15	17		9°943383	30	30		37	1
38	0	9°680519	16	62		10°319481		9°737171	16	80		10°262829		10°056652	16	18		9°943348	28	22		38	0
38	1	9°680635	17	66		10°319365		9°737321	17	85		10°262679		10°056686	17	20		9°943314	26	30		38	1
39	0	9°680750	18	69		10°319250		9°737471	18	90		10°262529		10°056721	18	21		9°943279	24	21		39	0
39	1	9°680866	19	73		10°319134		9°737621	19	95		10°262379		10°056755	19	22		9°943245	22	30		39	1
40	0	9°680982	20	77		10°319018		9°737771	20	100		10°262229		10°056790	20	23		9°943210	20	20		40	0
40	1	9°681097	21	81		10°318903		9°737921	21	105		10°262079		10°056824	21	24		9°943176	18	30		40	1
41	0	9°681213	22	85		10°318787		9°738071	22	110		10°261929		10°056859	22	25		9°943141	16	19		41	0
41	1	9°681328	23	89		10°318672		9°738221	23	115		10°261779		10°056893	23	26		9°943107	14	20		41	1
42	0	9°681443	24	93		10°318557		9°738371	24	120		10°261629		10°056928	24	28		9°943072	12	18		42	0
42	1	9°681559	25	97		10°318441		9°738521	25	125		10°261479		10°056963	25	29		9°943037	10	30		42	1
43	0	9°681674	26	100		10°318326		9°738671	26	130		10°261329		10°056997	26	30		9°943003	8	17		43	0
43	1	9°681789	27	104		10°318211		9°738821	27	135		10°261179		10°057032	27	31		9°942968	6	30		43	1
44	0	9°681905	28	108		10°318095		9°738971	28	140		10°261029		10°057066	28	32		9°942934	4	16		44	0
44	1	9°682020	29	112		10°317980		9°739121	29	145		10°260879		10°057101	29	33		9°942899	2	30		44	1
45	0	9°682135	30	116		10°317865		9°739271	30	150		10°260729		10°057136	30	34		9°942864	0	16		45	0
45	1	9°682250	1	4		10°317750		9°739420	1	5		10°260580		10°057170	1	1		9°942830	58	30		45	1
46	0	9°682365	2	8		10°317635		9°739570	2	10		10°260430		10°057205	2	2		9°942795	56	14		46	0
46	1	9°682480	3	11		10°317520		9°739720	3	15		10°260280		10°057240	3	3		9°942760	54	30		46	1
47	0	9°682595	4	15		10°317405		9°739870	4	20		10°260130		10°057274	4	5		9°942726	52	13		47	0
47	1	9°682710	5	19		10°317290		9°740019	5	25		10°259981		10°057309	5	6		9°942691	50	30		47	1
48	0	9°682825	6	23		10°317175		9°740169	6	30		10°259831		10°057344	6	7		9°942656	48	12		48	0
48	1	9°682940	7	27		10°317060		9°740319	7	35		10°259681		10°057379	7	8		9°942621	46	30		48	1
49	0	9°683055	8	31		10°316945		9°740468	8	40		10°259532		10°057413	8	9		9°942587	44	11		49	0
49	1	9°683170	9	34		10°316830		9°740618	9	45		10°259382		10°057448	9	10		9°942552	42	30		49	1
50	0	9°683284	10	38		10°316716		9°740767	10	50		10°259233		10°057483	10	11		9°942517	40	10		50	0
50	1	9°683399	11	42		10°316601		9°740917	11	55		10°259083		10°057518	11	13		9°942482	38	30		50	1
51	0	9°683514	12	46		10°316486		9°741066	12	60		10°258934		10°057552	12	14		9°942448	36	9		51	0
51	1	9°683628	13	50		10°316372		9°741216	13	65		10°258784		10°057587	13	15		9°942413	34	30		51	1
52	0	9°683743	14	54		10°316257		9°741365	14	70		10°258635		10°057622	14	16		9°942378	32	8		52	0
52	1	9°683858	15	57		10°316142		9°741514	15	75		10°258486		10°057657	15	17		9°942343	30	30		52	1
53	0	9°683972	16	61		10°316028		9°741664	16	80		10°258336		10°057692	16	19		9°942308	28	7		53	0
53	1	9°684087	17	65		10°315913		9°741813	17	85		10°258187		10°057727	17	20		9°942273	26	30		53	1
54	0	9°684201	18	69		10°315799		9°741962	18	90		10°258038		10°057761	18	21		9°942239	24	6		54	0
54	1	9°684315	19	73		10°315685		9°742112	19	95		10°257888		10°057796	19	22		9°942204	22	30		54	1
55	0	9°684430	20	76		10°315570		9°742261	20	100		10°257739		10°057831	20	23		9°942169	20	5		55	0
55	1	9°684544	21	80		10°315456		9°742410	21	105		10°257590		10°057866	21	24		9°942134	18	30		55	1
56	0	9°684658	22	84		10°315342		9°742559	22	110		10°257441		10°057901	22	26		9°942099	16	4		56	0
56	1	9°684773	23	88		10°315227		9°742709	23	115		10°257291		10°057936	23	27		9°942064	14	30		56	1
57	0	9°684887	24	92		10°315113		9°742858	24	120		10°257142		10°057971	24	28		9°942029	12	3		57	0
57	1	9°685001	25	96		10°314999		9°743007	25	124		10°256993		10°058006	25	29		9°941994	10	30		57	1
58	0	9°685115	26	100		10°314885		9°743156	26	129		10°256844		10°058041	26	30		9°941959	8	2		58	0
58	1	9°685229	27	103		10°314771		9°743305	27	134		10°256695		10°058076	27	31		9°941924	6	30		58	1
59	0	9°685343	28	107		10°314657		9°743454	28	139		10°256546		10°058111	28	32		9°941889	4	1		59	0
59	1	9°685457	29	111		10°314543		9°743603	29	144		10°256397		10°058146	29	34		9°941854	2	30		59	1
60	0	9°685571	30	115		10°314429		9°743752	30	149		10°256248		10°058181	30	35		9°941819	0	0		60	0

LOG. SINES, COSINES, &c.

1° 56'		30°										40°	
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	°	'
0	0	9°685571		10°314429	9°743752	1	10°256248	10°058181	1	9°941819	60	0	0
30	1	9°685685	1"	10°314315	9°743901	2	10°256099	10°058216	1"	9°941784	56	30	1
30	2	9°685799	2	10°314201	9°744050	3	10°255950	10°058251	2	9°941749	52	30	2
30	3	9°685913	3	10°314087	9°744199	4	10°255801	10°058286	3	9°941714	48	30	3
30	4	9°686027	4	10°313973	9°744348	5	10°255652	10°058321	4	9°941679	44	30	4
30	5	9°686141	5	10°313859	9°744496	6	10°255504	10°058356	5	9°941644	40	30	5
30	6	9°686254	6	10°313746	9°744645	7	10°255355	10°058391	6	9°941609	36	30	6
30	7	9°686368	7	10°313632	9°744794	8	10°255206	10°058426	7	9°941574	32	30	7
30	8	9°686482	8	10°313518	9°744943	9	10°255057	10°058461	8	9°941539	28	30	8
30	9	9°686595	9	10°313405	9°745092	10	10°254908	10°058496	9	9°941504	24	30	9
30	10	9°686709	10	10°313291	9°745240	11	10°254760	10°058531	10	9°941469	20	30	10
30	11	9°686822	11	10°313178	9°745389	12	10°254611	10°058567	11	9°941433	16	30	11
30	12	9°686936	12	10°313064	9°745538	13	10°254462	10°058602	12	9°941398	12	30	12
30	13	9°687049	13	10°312951	9°745686	14	10°254314	10°058637	13	9°941363	8	30	13
30	14	9°687163	14	10°312837	9°745835	15	10°254165	10°058672	14	9°941328	4	30	14
30	15	9°687276	15	10°312724	9°745983	16	10°254017	10°058707	15	9°941293	0	30	15
30	16	9°687389	16	10°312611	9°746132	17	10°253868	10°058742	16	9°941258	36	30	16
30	17	9°687503	17	10°312497	9°746281	18	10°253719	10°058777	17	9°941222	32	30	17
30	18	9°687616	18	10°312384	9°746429	19	10°253571	10°058812	18	9°941187	28	30	18
30	19	9°687729	19	10°312271	9°746577	20	10°253423	10°058848	19	9°941152	24	30	19
30	20	9°687843	20	10°312157	9°746726	21	10°253274	10°058883	20	9°941117	20	30	20
30	21	9°687956	21	10°312044	9°746874	22	10°253126	10°058919	21	9°941081	16	30	21
30	22	9°688069	22	10°311931	9°747023	23	10°252977	10°058954	22	9°941046	12	30	22
30	23	9°688182	23	10°311818	9°747171	24	10°252829	10°058989	23	9°941011	8	30	23
30	24	9°688295	24	10°311705	9°747319	25	10°252681	10°059025	24	9°940975	4	30	24
30	25	9°688408	25	10°311592	9°747468	26	10°252532	10°059060	25	9°940940	0	30	25
30	26	9°688521	26	10°311479	9°747616	27	10°252384	10°059095	26	9°940905	36	30	26
30	27	9°688634	27	10°311366	9°747764	28	10°252236	10°059130	27	9°940870	32	30	27
30	28	9°688747	28	10°311253	9°747913	29	10°252087	10°059166	28	9°940834	28	30	28
30	29	9°688860	29	10°311140	9°748061	30	10°251939	10°059201	29	9°940799	24	30	29
30	30	9°688972	30	10°311027	9°748209	31	10°251791	10°059237	30	9°940763	20	30	30
30	1	9°689085	1	10°310915	9°748357	32	10°251643	10°059272	31	9°940728	16	30	1
30	2	9°689198	2	10°310802	9°748505	33	10°251495	10°059307	32	9°940693	12	30	2
30	3	9°689311	3	10°310689	9°748653	34	10°251347	10°059343	33	9°940658	8	30	3
30	4	9°689423	4	10°310577	9°748801	35	10°251199	10°059378	34	9°940622	4	30	4
30	5	9°689536	5	10°310464	9°748949	36	10°251051	10°059414	35	9°940586	0	30	5
30	6	9°689648	6	10°310352	9°749097	37	10°250903	10°059449	36	9°940551	36	30	6
30	7	9°689761	7	10°310239	9°749245	38	10°250755	10°059484	37	9°940516	32	30	7
30	8	9°689873	8	10°310127	9°749393	39	10°250607	10°059520	38	9°940480	28	30	8
30	9	9°689986	9	10°310014	9°749541	40	10°250459	10°059555	39	9°940445	24	30	9
30	10	9°690098	10	10°309902	9°749689	41	10°250311	10°059591	40	9°940409	20	30	10
30	11	9°690211	11	10°309789	9°749837	42	10°250163	10°059626	41	9°940374	16	30	11
30	12	9°690323	12	10°309677	9°749985	43	10°250015	10°059662	42	9°940338	12	30	12
30	13	9°690435	13	10°309565	9°750133	44	10°249867	10°059697	43	9°940303	8	30	13
30	14	9°690548	14	10°309452	9°750281	45	10°249719	10°059733	44	9°940267	4	30	14
30	15	9°690660	15	10°309340	9°750428	46	10°249572	10°059769	45	9°940231	0	30	15
30	16	9°690772	16	10°309228	9°750576	47	10°249424	10°059804	46	9°940196	36	30	16
30	17	9°690884	17	10°309116	9°750724	48	10°249276	10°059840	47	9°940160	32	30	17
30	18	9°690996	18	10°309004	9°750872	49	10°249128	10°059875	48	9°940125	28	30	18
30	19	9°691108	19	10°308892	9°751019	50	10°248981	10°059911	49	9°940089	24	30	19
30	20	9°691220	20	10°308780	9°751167	51	10°248833	10°059946	50	9°940054	20	30	20
30	21	9°691332	21	10°308668	9°751315	52	10°248685	10°059982	51	9°940018	16	30	21
30	22	9°691444	22	10°308556	9°751462	53	10°248538	10°060018	52	9°939982	12	30	22
30	23	9°691556	23	10°308444	9°751610	54	10°248390	10°060053	53	9°939947	8	30	23
30	24	9°691668	24	10°308332	9°751757	55	10°248243	10°060089	54	9°939911	4	30	24
30	25	9°691780	25	10°308220	9°751905	56	10°248095	10°060125	55	9°939875	0	30	25
30	26	9°691892	26	10°308108	9°752052	57	10°247948	10°060160	56	9°939840	36	30	26
30	27	9°692004	27	10°307996	9°752200	58	10°247800	10°060196	57	9°939804	32	30	27
30	28	9°692115	28	10°307885	9°752347	59	10°247653	10°060232	58	9°939768	28	30	28
30	29	9°692227	29	10°307773	9°752495	60	10°247505	10°060267	59	9°939733	24	30	29
30	30	9°692339	30	10°307661	9°752642	61	10°247358	10°060303	60	9°939697	20	30	30
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	°	'

29°

4^b U^m

LOG. SINES, COSINES, &c.														
2 ^h 0 ^m							30°							
°	'	Sine	Parts	Cosec.	Tangent		Parts	Cotang.	Secant	Parts	Cosine	°	'	
0	0	9°698970		10°301030	9°761439		10°238561	10°062469	5°937531	60	60	0	0	
0	1	9°699090	1"	10°300921	9°761585	1"	10°238415	10°062506	5°937494	59	59	0	1	
1	0	9°699189	2	7	10°300811	9°761731	2	10	10°238269	10°062542	58	58	1	0
1	1	9°699298	3	11	10°300702	9°761877	3	15	10°238123	10°062579	57	57	1	1
2	0	9°699407	4	14	10°300593	9°762023	4	19	10°237977	10°062615	56	56	2	0
2	1	9°699517	5	18	10°300483	9°762168	5	24	10°237832	10°062652	55	55	2	1
3	0	9°699626	6	22	10°300374	9°762314	6	29	10°237686	10°062688	54	54	3	0
3	1	9°699735	7	25	10°300265	9°762460	7	34	10°237540	10°062725	53	53	3	1
4	0	9°699844	8	29	10°300156	9°762606	8	39	10°237394	10°062762	52	52	4	0
4	1	9°699953	9	33	10°300047	9°762751	9	44	10°237249	10°062798	51	51	4	1
5	0	9°700062	10	36	10°299938	9°762897	10	48	10°237103	10°062835	50	50	5	0
5	1	9°700171	11	40	10°299829	9°763043	11	53	10°236957	10°062871	49	49	5	1
6	0	9°700280	12	44	10°299720	9°763188	12	58	10°236812	10°062908	48	48	6	0
6	1	9°700389	13	47	10°299611	9°763334	13	63	10°236666	10°062944	47	47	6	1
7	0	9°700498	14	51	10°299502	9°763479	14	68	10°236521	10°062981	46	46	7	0
7	1	9°700607	15	54	10°299393	9°763625	15	73	10°236375	10°063018	45	45	7	1
8	0	9°700716	16	58	10°299284	9°763770	16	78	10°236230	10°063054	44	44	8	0
8	1	9°700825	17	62	10°299175	9°763916	17	82	10°236084	10°063091	43	43	8	1
9	0	9°700933	18	65	10°299066	9°764061	18	87	10°235939	10°063128	42	42	9	0
9	1	9°701042	19	69	10°298958	9°764207	19	92	10°235793	10°063164	41	41	9	1
10	0	9°701151	20	72	10°298849	9°764352	20	97	10°235648	10°063201	40	40	10	0
10	1	9°701259	21	76	10°298741	9°764497	21	102	10°235503	10°063238	39	39	10	1
11	0	9°701368	22	80	10°298632	9°764643	22	107	10°235357	10°063275	38	38	11	0
11	1	9°701477	23	83	10°298523	9°764788	23	112	10°235212	10°063311	37	37	11	1
12	0	9°701585	24	87	10°298415	9°764933	24	116	10°235067	10°063348	36	36	12	0
12	1	9°701694	25	91	10°298306	9°765079	25	121	10°234921	10°063385	35	35	12	1
13	0	9°701802	26	94	10°298198	9°765224	26	126	10°234776	10°063422	34	34	13	0
13	1	9°701911	27	98	10°298089	9°765369	27	131	10°234631	10°063458	33	33	13	1
14	0	9°702019	28	101	10°297981	9°765514	28	136	10°234486	10°063495	32	32	14	0
14	1	9°702127	29	105	10°297873	9°765660	29	141	10°234340	10°063532	31	31	14	1
15	0	9°702236	30	109	10°297764	9°765805	30	145	10°234195	10°063569	30	30	15	0
15	1	9°702344	1	4	10°297656	9°765950	1	5	10°234050	10°063606	29	29	15	1
16	0	9°702452	2	7	10°297548	9°766095	2	10	10°233905	10°063643	28	28	16	0
16	1	9°702561	3	11	10°297439	9°766240	3	14	10°233760	10°063680	27	27	16	1
17	0	9°702669	4	14	10°297331	9°766385	4	19	10°233615	10°063716	26	26	17	0
17	1	9°702777	5	18	10°297222	9°766530	5	24	10°233470	10°063753	25	25	17	1
18	0	9°702885	6	22	10°297115	9°766675	6	29	10°233325	10°063790	24	24	18	0
18	1	9°702993	7	25	10°297007	9°766820	7	34	10°233180	10°063827	23	23	18	1
19	0	9°703101	8	29	10°296899	9°766965	8	39	10°233035	10°063864	22	22	19	0
19	1	9°703209	9	32	10°296791	9°767110	9	43	10°232890	10°063901	21	21	19	1
20	0	9°703317	10	36	10°296683	9°767255	10	48	10°232745	10°063938	20	20	20	0
20	1	9°703425	11	39	10°296575	9°767400	11	53	10°232600	10°063975	19	19	20	1
21	0	9°703533	12	43	10°296467	9°767545	12	58	10°232455	10°064012	18	18	21	0
21	1	9°703641	13	47	10°296359	9°767690	13	63	10°232310	10°064049	17	17	21	1
22	0	9°703749	14	50	10°296251	9°767834	14	68	10°232166	10°064086	16	16	22	0
22	1	9°703856	15	54	10°296144	9°767979	15	72	10°232021	10°064123	15	15	22	1
23	0	9°703964	16	57	10°296036	9°768124	16	77	10°231876	10°064160	14	14	23	0
23	1	9°704072	17	61	10°295928	9°768269	17	82	10°231731	10°064197	13	13	23	1
24	0	9°704179	18	64	10°295821	9°768414	18	87	10°231586	10°064234	12	12	24	0
24	1	9°704287	19	68	10°295713	9°768558	19	92	10°231442	10°064271	11	11	24	1
25	0	9°704395	20	72	10°295605	9°768703	20	97	10°231297	10°064308	10	10	25	0
25	1	9°704502	21	75	10°295498	9°768848	21	101	10°231152	10°064345	9	9	25	1
26	0	9°704610	22	79	10°295390	9°768992	22	106	10°231008	10°064382	8	8	26	0
26	1	9°704717	23	83	10°295283	9°769137	23	111	10°230863	10°064419	7	7	26	1
27	0	9°704825	24	86	10°295175	9°769281	24	116	10°230719	10°064457	6	6	27	0
27	1	9°704932	25	90	10°295068	9°769426	25	121	10°230574	10°064494	5	5	27	1
28	0	9°705040	26	93	10°294960	9°769571	26	126	10°230429	10°064531	4	4	28	0
28	1	9°705147	27	97	10°294853	9°769715	27	130	10°230285	10°064568	3	3	28	1
29	0	9°705254	28	100	10°294746	9°769860	28	135	10°230140	10°064605	2	2	29	0
29	1	9°705362	29	104	10°294638	9°770004	29	140	10°229996	10°064642	1	1	29	1
30	0	9°705469	30	108	10°294531	9°770148	30	145	10°229852	10°064680	0	0	30	0
°	'	Cosine	Parts	Secant	Cotang.		Parts	Tangent	Cosec.	Parts	Sine	°	'	
59°														
3 ^h 58 ^m														

LOG. SINES, COSINES, &c.

2 ^h 2 ^m		30°											
°	'	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	'
30	0	8	9°705469		10°294531	9°770148		10°229852	10°064680		9°935320	58	30
30	1	2	9°705576	1" 4	10°294424	9°770293	1" 5	10°229707	10°064717	1" 1	9°935283	58	30
31	4	4	9°705683	2 7	10°294317	9°770437	2 10	10°229563	10°064754	2 2	9°935246	58	29
31	5	8	9°705790	3 11	10°294210	9°770582	3 14	10°229418	10°064791	3 4	9°935209	58	30
32	8	8	9°705898	4 14	10°294102	9°770726	4 19	10°229274	10°064829	4 5	9°935171	58	28
32	10	10	9°706005	5 18	10°293995	9°770870	5 24	10°229130	10°064866	5 6	9°935134	58	30
33	12	12	9°706112	6 21	10°293888	9°771015	6 29	10°228985	10°064903	6 7	9°935097	58	27
33	14	14	9°706219	7 25	10°293781	9°771159	7 34	10°228841	10°064940	7 9	9°935060	58	30
34	16	16	9°706326	8 28	10°293674	9°771303	8 38	10°228697	10°064978	8 10	9°935022	41	26
34	18	18	9°706433	9 32	10°293567	9°771448	9 43	10°228552	10°065015	9 11	9°934985	42	30
35	20	20	9°706539	10 36	10°293461	9°771592	10 48	10°228408	10°065052	10 12	9°934948	40	26
35	22	22	9°706646	11 39	10°293354	9°771736	11 53	10°228264	10°065090	11 14	9°934910	38	30
36	24	24	9°706753	12 43	10°293247	9°771880	12 58	10°228120	10°065127	12 15	9°934873	36	24
36	26	26	9°706860	13 46	10°293140	9°772024	13 62	10°227976	10°065164	13 16	9°934836	34	30
37	28	28	9°706967	14 50	10°293033	9°772168	14 67	10°227832	10°065202	14 17	9°934798	32	23
37	30	30	9°707073	15 53	10°292927	9°772312	15 72	10°227688	10°065239	15 19	9°934761	30	30
38	32	32	9°707180	16 57	10°292820	9°772457	16 77	10°227543	10°065277	16 20	9°934723	28	23
38	34	34	9°707287	17 61	10°292713	9°772601	17 82	10°227399	10°065314	17 21	9°934686	26	30
39	36	36	9°707393	18 64	10°292607	9°772745	18 86	10°227255	10°065351	18 22	9°934649	24	21
39	38	38	9°707500	19 68	10°292500	9°772889	19 91	10°227111	10°065389	19 24	9°934611	22	30
40	40	40	9°707606	20 71	10°292394	9°773033	20 96	10°226967	10°065426	20 25	9°934574	20	20
40	42	42	9°707713	21 75	10°292287	9°773177	21 101	10°226823	10°065464	21 26	9°934536	18	30
41	44	44	9°707819	22 78	10°292181	9°773321	22 106	10°226679	10°065501	22 27	9°934499	16	19
41	46	46	9°707926	23 82	10°292074	9°773465	23 110	10°226535	10°065539	23 29	9°934461	14	30
42	48	48	9°708032	24 85	10°291968	9°773608	24 115	10°226392	10°065576	24 30	9°934424	12	18
42	50	50	9°708139	25 89	10°291861	9°773752	25 120	10°226248	10°065614	25 31	9°934386	10	30
43	52	52	9°708245	26 92	10°291755	9°773896	26 125	10°226104	10°065651	26 32	9°934349	8	17
43	54	54	9°708351	27 96	10°291649	9°774040	27 130	10°225960	10°065689	27 34	9°934311	6	30
44	56	56	9°708458	28 99	10°291542	9°774184	28 134	10°225816	10°065726	28 35	9°934274	4	16
44	58	58	9°708564	29 103	10°291436	9°774328	29 139	10°225672	10°065764	29 36	9°934236	2	30
45	30	30	9°708670	30 107	10°291330	9°774471	30 144	10°225529	10°065801	30 37	9°934199	0	15
45	32	32	9°708776	1 4	10°291224	9°774615	1 5	10°225385	10°065839	1 1	9°934161	58	30
46	34	34	9°708882	2 7	10°291118	9°774759	2 10	10°225241	10°065877	2 3	9°934123	56	14
46	36	36	9°708988	3 11	10°291012	9°774902	3 14	10°225098	10°065914	3 4	9°934086	54	30
47	38	38	9°709094	4 14	10°290906	9°775046	4 19	10°224954	10°065952	4 5	9°934048	52	13
47	40	40	9°709200	5 18	10°290800	9°775190	5 24	10°224810	10°065989	5 6	9°934011	50	30
48	42	42	9°709306	6 21	10°290694	9°775333	6 29	10°224667	10°066027	6 8	9°933973	48	12
48	44	44	9°709412	7 25	10°290588	9°775477	7 32	10°224523	10°066065	7 9	9°933935	46	30
49	46	46	9°709518	8 28	10°290482	9°775621	8 38	10°224379	10°066102	8 10	9°933898	44	11
49	48	48	9°709624	9 32	10°290376	9°775764	9 43	10°224235	10°066140	9 11	9°933860	42	30
50	50	50	9°709730	10 35	10°290270	9°775908	10 48	10°224092	10°066178	10 13	9°933822	40	10
50	52	52	9°709836	11 39	10°290164	9°776051	11 53	10°223949	10°066216	11 14	9°933784	38	30
51	54	54	9°709941	12 42	10°290059	9°776195	12 57	10°223805	10°066253	12 15	9°933747	36	9
51	56	56	9°710047	13 46	10°289953	9°776338	13 62	10°223662	10°066291	13 16	9°933709	34	30
52	58	58	9°710153	14 49	10°289847	9°776482	14 67	10°223518	10°066329	14 18	9°933671	32	8
52	30	30	9°710259	15 53	10°289741	9°776625	15 72	10°223375	10°066367	15 19	9°933633	30	30
53	32	32	9°710364	16 56	10°289636	9°776768	16 76	10°223232	10°066404	16 20	9°933596	28	7
53	34	34	9°710470	17 60	10°289530	9°776912	17 81	10°223088	10°066442	17 21	9°933558	26	30
54	36	36	9°710575	18 63	10°289425	9°777055	18 86	10°222945	10°066480	18 23	9°933520	24	6
54	38	38	9°710681	19 67	10°289319	9°777199	19 91	10°222801	10°066518	19 24	9°933482	22	30
55	40	40	9°710786	20 70	10°289214	9°777342	20 96	10°222658	10°066555	20 25	9°933445	20	5
55	42	42	9°710892	21 74	10°289108	9°777485	21 100	10°222515	10°066593	21 26	9°933407	18	30
56	44	44	9°710997	22 77	10°289003	9°777628	22 105	10°222372	10°066631	22 28	9°933369	16	4
56	46	46	9°711103	23 81	10°288897	9°777772	23 110	10°222228	10°066669	23 29	9°933331	14	30
57	48	48	9°711208	24 85	10°288792	9°777915	24 115	10°222084	10°066707	24 30	9°933293	12	3
57	50	50	9°711313	25 88	10°288687	9°778058	25 119	10°221942	10°066745	25 32	9°933255	10	30
58	52	52	9°711419	26 92	10°288581	9°778201	26 124	10°221799	10°066783	26 33	9°933217	8	2
58	54	54	9°711524	27 95	10°288476	9°778344	27 129	10°221656	10°066821	27 34	9°933179	6	30
59	56	56	9°711629	28 99	10°288371	9°778488	28 134	10°221512	10°066859	28 35	9°933141	4	1
59	58	58	9°711734	29 102	10°288266	9°778631	29 139	10°221369	10°066896	29 37	9°933104	2	30
60	0	0	9°711839	30 106	10°288161	9°778774	30 143	10°221226	10°066934	30 38	9°933066	0	0
°	'	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	'
59°													3 ^h 56 ^m

LOG. SINES, COSINES, &c.

2 ^d 4 ^m		31°											
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'
0	0	9°7'11839		10°288161	9°778774	1°	10°221226	10°066934	1°	9°933066	86	50	
30	2	9°7'11944	3	10°288056	9°778917	5	10°221083	10°066972	1°	9°933028	58	30	
1	4	9°7'12050	7	10°287950	9°779060	10	10°220940	10°067010	2	9°932990	56	59	
30	6	9°7'12155	10	10°287845	9°779203	14	10°220797	10°067048	3	9°932952	54	30	
2	8	9°7'12260	14	10°287740	9°779346	19	10°220654	10°067086	4	9°932914	52	58	
30	10	9°7'12365	17	10°287635	9°779489	24	10°220511	10°067124	5	9°932876	50	30	
3	12	9°7'12469	21	10°287531	9°779632	29	10°220368	10°067162	6	9°932838	48	57	
30	14	9°7'12574	24	10°287426	9°779775	33	10°220225	10°067200	7	9°932800	46	30	
4	16	9°7'12679	28	10°287321	9°779918	38	10°220082	10°067238	8	9°932762	44	56	
30	18	9°7'12784	31	10°287216	9°780061	43	10°219939	10°067276	9	9°932724	42	30	
5	20	9°7'12889	35	10°287111	9°780203	48	10°219797	10°067315	10	9°932685	40	55	
30	22	9°7'12994	38	10°287006	9°780346	52	10°219654	10°067353	11	9°932647	38	30	
6	24	9°7'13098	42	10°286902	9°780489	57	10°219511	10°067391	12	9°932609	36	54	
30	26	9°7'13203	45	10°286797	9°780632	62	10°219368	10°067429	13	9°932571	34	30	
7	28	9°7'13308	49	10°286692	9°780775	67	10°219225	10°067467	14	9°932533	32	53	
30	30	9°7'13412	52	10°286588	9°780917	71	10°219083	10°067505	15	9°932495	30	30	
8	32	9°7'13517	56	10°286483	9°781060	76	10°218940	10°067543	16	9°932457	28	52	
30	34	9°7'13621	59	10°286379	9°781203	81	10°218797	10°067581	17	9°932419	26	30	
9	36	9°7'13726	63	10°286274	9°781346	86	10°218654	10°067620	18	9°932380	24	51	
30	38	9°7'13831	66	10°286169	9°781488	90	10°218512	10°067658	19	9°932342	22	30	
10	40	9°7'13935	70	10°286065	9°781631	95	10°218369	10°067696	20	9°932304	20	50	
30	42	9°7'14039	73	10°285961	9°781774	100	10°218226	10°067734	21	9°932266	18	30	
11	44	9°7'14144	77	10°285856	9°781916	105	10°218084	10°067772	22	9°932228	16	49	
30	46	9°7'14248	80	10°285752	9°782059	109	10°217941	10°067811	23	9°932189	14	30	
12	48	9°7'14352	84	10°285648	9°782201	114	10°217799	10°067849	24	9°932151	12	48	
30	50	9°7'14457	87	10°285543	9°782344	119	10°217656	10°067887	25	9°932113	10	30	
13	52	9°7'14561	91	10°285439	9°782486	124	10°217514	10°067925	26	9°932075	8	47	
30	54	9°7'14665	94	10°285335	9°782629	129	10°217371	10°067964	27	9°932037	6	30	
14	56	9°7'14769	98	10°285231	9°782771	133	10°217229	10°068002	28	9°931998	4	46	
30	58	9°7'14873	101	10°285127	9°782914	138	10°217086	10°068040	29	9°931960	2	30	
15	0	9°7'14978	105	10°285022	9°783056	143	10°216944	10°068079	30	9°931921	0	45	
30	2	9°7'15082	1	10°284918	9°783199	15	10°216801	10°068117	1	9°931883	58	30	
16	4	9°7'15186	7	10°284814	9°783341	20	10°216659	10°068155	2	9°931845	56	44	
30	6	9°7'15290	10	10°284710	9°783483	24	10°216517	10°068194	3	9°931806	54	30	
17	8	9°7'15394	14	10°284606	9°783626	29	10°216374	10°068232	4	9°931768	52	43	
30	10	9°7'15498	17	10°284502	9°783768	34	10°216232	10°068270	5	9°931730	50	30	
18	12	9°7'15602	21	10°284398	9°783910	39	10°216090	10°068309	6	9°931691	48	42	
30	14	9°7'15705	24	10°284295	9°784053	43	10°215947	10°068347	7	9°931653	46	30	
19	16	9°7'15809	28	10°284191	9°784195	48	10°215805	10°068386	8	9°931614	44	41	
30	18	9°7'15913	31	10°284087	9°784337	53	10°215663	10°068424	9	9°931576	42	30	
20	20	9°7'16017	35	10°283983	9°784479	57	10°215521	10°068463	10	9°931537	40	40	
30	22	9°7'16121	38	10°283879	9°784622	62	10°215378	10°068501	11	9°931499	38	30	
21	24	9°7'16224	42	10°283776	9°784764	67	10°215236	10°068540	12	9°931460	36	30	
30	26	9°7'16328	45	10°283672	9°784906	71	10°215094	10°068578	13	9°931422	34	30	
22	28	9°7'16432	49	10°283568	9°785048	76	10°214952	10°068617	14	9°931383	32	30	
30	30	9°7'16535	52	10°283465	9°785190	81	10°214810	10°068655	15	9°931345	30	30	
23	32	9°7'16639	56	10°283361	9°785332	86	10°214668	10°068694	16	9°931306	28	37	
30	34	9°7'16742	59	10°283258	9°785474	90	10°214526	10°068732	17	9°931268	26	30	
24	36	9°7'16846	63	10°283154	9°785616	95	10°214384	10°068771	18	9°931229	24	36	
30	38	9°7'16949	66	10°283051	9°785758	100	10°214242	10°068809	19	9°931191	22	30	
25	40	9°7'17053	69	10°282947	9°785900	105	10°214100	10°068848	20	9°931152	20	35	
30	42	9°7'17156	72	10°282844	9°786042	110	10°213958	10°068886	21	9°931114	18	30	
26	44	9°7'17259	76	10°282741	9°786184	114	10°213816	10°068925	22	9°931075	16	34	
30	46	9°7'17363	79	10°282637	9°786326	119	10°213674	10°068964	23	9°931036	14	30	
27	48	9°7'17466	83	10°282534	9°786468	124	10°213532	10°069002	24	9°930998	12	33	
30	50	9°7'17569	86	10°282431	9°786610	129	10°213390	10°069041	25	9°930959	10	30	
28	52	9°7'17673	90	10°282327	9°786752	133	10°213248	10°069079	26	9°930921	8	32	
30	54	9°7'17776	93	10°282224	9°786894	138	10°213106	10°069118	27	9°930882	6	30	
29	56	9°7'17879	97	10°282121	9°787036	143	10°212964	10°069157	28	9°930843	4	31	
30	58	9°7'17982	100	10°282018	9°787178	147	10°212822	10°069196	29	9°930804	2	30	
30	0	9°7'18085	104	10°281915	9°787319	152	10°212681	10°069234	30	9°930766	0	30	
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	Parts	°	'

LOG. SINES, COSINES, &c.

2° 6'				31°							
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	°
30	0	9°7'18085		10°281915	9°787319		10°212681	10°069234		9°930766	30
30	2	9°7'18188	1" 3	10°281812	9°787461	1" 5	10°212539	10°069273	1" 1	9°930727	28
31	4	9°7'18291	2 7	10°281709	9°787603	2 9	10°212397	10°069312	2 3	9°930688	26
30	6	9°7'18394	3 10	10°281606	9°787745	3 14	10°212255	10°069350	3 4	9°930650	24
32	8	9°7'18497	4 14	10°281503	9°787886	4 19	10°212114	10°069389	4 5	9°930611	22
30	10	9°7'18600	5 17	10°281400	9°788028	5 24	10°211972	10°069428	5 6	9°930572	20
33	12	9°7'18703	6 20	10°281297	9°788170	6 28	10°211830	10°069467	6 8	9°930533	18
30	14	9°7'18806	7 24	10°281194	9°788311	7 33	10°211689	10°069506	7 9	9°930495	16
34	16	9°7'18909	8 27	10°281091	9°788453	8 38	10°211547	10°069544	8 10	9°930456	14
30	18	9°7'19011	9 31	10°280989	9°788595	9 42	10°211405	10°069583	9 12	9°930417	12
35	20	9°7'19114	10 34	10°280886	9°788736	10 47	10°211264	10°069622	10 13	9°930378	10
30	22	9°7'19217	11 38	10°280783	9°788878	11 52	10°211122	10°069661	11 14	9°930339	8
36	24	9°7'19320	12 41	10°280680	9°789019	12 57	10°210981	10°069700	12 16	9°930300	6
30	26	9°7'19422	13 44	10°280578	9°789161	13 61	10°210839	10°069739	13 17	9°930262	4
37	28	9°7'19525	14 48	10°280475	9°789302	14 66	10°210698	10°069777	14 18	9°930223	2
30	30	9°7'19627	15 51	10°280372	9°789444	15 71	10°210556	10°069816	15 20	9°930184	0
38	32	9°7'19730	16 55	10°280270	9°789585	16 75	10°210415	10°069855	16 21	9°930145	28
30	34	9°7'19833	17 58	10°280167	9°789727	17 80	10°210273	10°069894	17 22	9°930106	26
30	36	9°7'19935	18 62	10°280065	9°789868	18 85	10°210132	10°069933	18 23	9°930067	24
30	38	9°7'20038	19 65	10°279962	9°790009	19 89	10°209991	10°069972	19 25	9°930028	22
40	40	9°7'20140	20 68	10°279860	9°790151	20 94	10°209849	10°070011	20 26	9°929989	20
30	42	9°7'20242	21 72	10°279758	9°790292	21 99	10°209708	10°070050	21 27	9°929950	18
41	44	9°7'20345	22 75	10°279655	9°790434	22 104	10°209566	10°070089	22 29	9°929911	16
30	46	9°7'20447	23 79	10°279553	9°790575	23 108	10°209425	10°070128	23 30	9°929872	14
42	48	9°7'20549	24 82	10°279451	9°790716	24 113	10°209284	10°070167	24 31	9°929833	12
30	50	9°7'20652	25 86	10°279348	9°790857	25 118	10°209143	10°070206	25 32	9°929794	10
43	52	9°7'20754	26 89	10°279246	9°790999	26 123	10°209001	10°070245	26 34	9°929755	8
30	54	9°7'20856	27 92	10°279144	9°791140	27 127	10°208860	10°070284	27 35	9°929716	6
44	56	9°7'20958	28 96	10°279042	9°791281	28 132	10°208719	10°070323	28 36	9°929677	4
30	58	9°7'21060	29 99	10°278940	9°791422	29 137	10°208578	10°070362	29 38	9°929638	2
45	0	9°7'21162	30 103	10°278838	9°791563	30 141	10°208437	10°070401	30 39	9°929599	0
30	2	9°7'21264	1 3	10°278736	9°791705	1 5	10°208295	10°070440	1 1	9°929560	28
46	4	9°7'21366	2 7	10°278634	9°791846	2 9	10°208154	10°070479	2 3	9°929521	26
30	6	9°7'21468	3 10	10°278532	9°791987	3 14	10°208013	10°070518	3 4	9°929482	24
47	8	9°7'21570	4 14	10°278430	9°792128	4 19	10°207872	10°070558	4 5	9°929443	22
30	10	9°7'21672	5 17	10°278328	9°792269	5 23	10°207731	10°070597	5 6	9°929403	20
48	12	9°7'21774	6 20	10°278226	9°792410	6 28	10°207590	10°070636	6 8	9°929364	18
30	14	9°7'21876	7 24	10°278124	9°792551	7 33	10°207449	10°070675	7 9	9°929325	16
49	16	9°7'21978	8 27	10°278022	9°792692	8 38	10°207308	10°070714	8 10	9°929286	14
30	18	9°7'22080	9 31	10°277920	9°792833	9 42	10°207167	10°070754	9 12	9°929247	12
50	20	9°7'22181	10 34	10°277819	9°792974	10 47	10°207026	10°070793	10 13	9°929207	10
30	22	9°7'22283	11 37	10°277717	9°793115	11 52	10°206885	10°070832	11 14	9°929168	8
51	24	9°7'22385	12 41	10°277615	9°793256	12 56	10°206744	10°070871	12 16	9°929129	6
30	26	9°7'22487	13 44	10°277513	9°793397	13 61	10°206603	10°070910	13 17	9°929090	4
52	28	9°7'22588	14 48	10°277412	9°793538	14 66	10°206462	10°070950	14 18	9°929050	2
30	30	9°7'22690	15 51	10°277310	9°793679	15 70	10°206321	10°070989	15 20	9°929011	0
53	32	9°7'22791	16 55	10°277209	9°793819	16 75	10°206181	10°071028	16 21	9°928972	28
30	34	9°7'22893	17 58	10°277107	9°793960	17 80	10°206040	10°071068	17 22	9°928933	26
54	36	9°7'22994	18 62	10°277006	9°794101	18 84	10°205899	10°071107	18 24	9°928893	24
30	38	9°7'23096	19 64	10°276904	9°794242	19 89	10°205758	10°071146	19 25	9°928854	22
55	40	9°7'23197	20 68	10°276803	9°794383	20 94	10°205617	10°071185	20 26	9°928815	20
30	42	9°7'23299	21 71	10°276701	9°794523	21 98	10°205477	10°071225	21 28	9°928775	18
56	44	9°7'23400	22 75	10°276600	9°794664	22 103	10°205336	10°071264	22 29	9°928736	16
30	46	9°7'23501	23 78	10°276499	9°794805	23 108	10°205195	10°071304	23 30	9°928696	14
57	48	9°7'23603	24 82	10°276397	9°794946	24 113	10°205054	10°071343	24 31	9°928657	12
30	50	9°7'23704	25 85	10°276296	9°795086	25 117	10°204914	10°071382	25 33	9°928618	10
58	52	9°7'23805	26 89	10°276195	9°795227	26 122	10°204773	10°071422	26 34	9°928578	8
30	54	9°7'23906	27 92	10°276094	9°795367	27 127	10°204633	10°071461	27 35	9°928539	6
59	56	9°7'24007	28 95	10°275993	9°795508	28 131	10°204492	10°071501	28 37	9°928499	4
30	58	9°7'24109	29 98	10°275891	9°795649	29 136	10°204351	10°071540	29 38	9°928460	2
60	0	9°7'24210	30 102	10°275790	9°795789	30 141	10°204211	10°071580	30 39	9°928420	0
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	°

58°

31 52"

LOG. SINES, COSINES, &c.

2° 8'		32°										32°	
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'
0	0	9°724210		10°275790	9°795789		10°204211	10°071580		9°928420	62	00	00
20	2	9°724311	1" 3	10°275689	9°795930	5	10°204070	10°071619	1" 1	9°928381	30	20	20
1	4	9°724412	2 7	10°275588	9°796070	2 9	10°203930	10°071658	2 3	9°928342	36	40	40
30	6	9°724513	3 10	10°275487	9°796211	3 14	10°203789	10°071698	3 4	9°928302	42	60	60
2	8	9°724614	4 13	10°275386	9°796351	4 19	10°203649	10°071737	4 5	9°928263	48	80	80
30	10	9°724715	5 17	10°275285	9°796494	5 23	10°203508	10°071777	5 7	9°928223	54	00	00
3	12	9°724816	6 20	10°275184	9°796632	6 28	10°203368	10°071817	6 8	9°928183	60	20	20
30	14	9°724917	7 23	10°275083	9°796773	7 33	10°203227	10°071856	7 9	9°928144	66	40	40
4	16	9°725017	8 27	10°274983	9°796913	8 37	10°203087	10°071896	8 11	9°928104	72	60	60
30	18	9°725118	9 30	10°274882	9°797053	9 42	10°202947	10°071935	9 12	9°928065	78	80	80
5	20	9°725219	10 34	10°274781	9°797194	10 47	10°202806	10°071975	10 13	9°928025	84	00	00
20	22	9°725320	11 37	10°274680	9°797334	11 51	10°202666	10°072015	11 15	9°927986	90	20	20
4	24	9°725420	12 40	10°274580	9°797475	12 56	10°202526	10°072054	12 16	9°927946	96	40	40
20	26	9°725521	13 44	10°274479	9°797615	13 61	10°202385	10°072094	13 17	9°927906	102	60	60
7	28	9°725622	14 47	10°274378	9°797755	14 65	10°202245	10°072133	14 18	9°927867	108	80	80
30	30	9°725722	15 50	10°274278	9°797895	15 70	10°202105	10°072173	15 20	9°927827	114	00	00
8	32	9°725823	16 54	10°274177	9°798036	16 75	10°201964	10°072213	16 21	9°927787	120	20	20
30	34	9°725923	17 57	10°274076	9°798176	17 79	10°201824	10°072252	17 22	9°927748	126	40	40
9	36	9°726024	18 61	10°273976	9°798316	18 84	10°201684	10°072292	18 24	9°927708	132	60	60
30	38	9°726124	19 64	10°273875	9°798456	19 89	10°201544	10°072332	19 25	9°927668	138	80	80
10	40	9°726225	20 67	10°273775	9°798596	20 93	10°201404	10°072371	20 26	9°927629	144	00	00
20	42	9°726325	21 70	10°273675	9°798737	21 98	10°201264	10°072411	21 28	9°927589	150	20	20
11	44	9°726426	22 74	10°273574	9°798877	22 103	10°201123	10°072451	22 29	9°927549	156	40	40
20	46	9°726526	23 77	10°273474	9°799017	23 107	10°200983	10°072491	23 30	9°927509	162	60	60
12	48	9°726626	24 80	10°273374	9°799157	24 112	10°200843	10°072530	24 32	9°927470	168	80	80
30	50	9°726727	25 84	10°273273	9°799297	25 117	10°200703	10°072570	25 33	9°927430	174	00	00
13	52	9°726827	26 87	10°273173	9°799437	26 122	10°200563	10°072610	26 34	9°927390	180	20	20
30	54	9°726927	27 90	10°273073	9°799577	27 126	10°200423	10°072650	27 36	9°927350	186	40	40
14	56	9°727027	28 94	10°272973	9°799717	28 131	10°200283	10°072690	28 37	9°927310	192	60	60
30	58	9°727128	29 97	10°272873	9°799857	29 136	10°200143	10°072730	29 38	9°927270	198	80	80
15	0	9°727228	30 101	10°272773	9°799997	30 140	10°200003	10°072769	30 40	9°927231	204	00	00
20	2	9°727328	1 3	10°272672	9°800137	1 5	10°199863	10°072809	1 1	9°927191	210	20	20
16	4	9°727428	2 7	10°272572	9°800277	2 9	10°199723	10°072849	2 3	9°927151	216	40	40
30	6	9°727528	3 10	10°272472	9°800417	3 14	10°199583	10°072889	3 4	9°927111	222	60	60
17	8	9°727628	4 13	10°272372	9°800557	4 19	10°199443	10°072929	4 5	9°927071	228	80	80
30	10	9°727728	5 17	10°272272	9°800697	5 23	10°199303	10°072969	5 7	9°927031	234	00	00
18	12	9°727828	6 20	10°272172	9°800836	6 28	10°199164	10°073009	6 8	9°926991	240	20	20
30	14	9°727928	7 23	10°272072	9°800976	7 33	10°199024	10°073049	7 9	9°926951	246	40	40
19	16	9°728027	8 27	10°271972	9°801116	8 37	10°198884	10°073089	8 11	9°926911	252	60	60
30	18	9°728127	9 30	10°271873	9°801256	9 42	10°198744	10°073129	9 12	9°926871	258	80	80
20	20	9°728227	10 33	10°271773	9°801396	10 46	10°198604	10°073169	10 13	9°926831	264	00	00
21	22	9°728327	11 37	10°271673	9°801535	11 51	10°198465	10°073209	11 15	9°926791	270	20	20
30	24	9°728427	12 40	10°271573	9°801675	12 56	10°198325	10°073249	12 16	9°926751	276	40	40
22	26	9°728526	13 43	10°271474	9°801815	13 60	10°198185	10°073289	13 17	9°926711	282	60	60
30	28	9°728626	14 47	10°271374	9°801955	14 65	10°198045	10°073329	14 19	9°926671	288	80	80
23	30	9°728726	15 50	10°271274	9°802094	15 70	10°197906	10°073369	15 20	9°926631	294	00	00
24	32	9°728825	16 53	10°271175	9°802234	16 74	10°197766	10°073409	16 21	9°926591	300	20	20
30	34	9°728925	17 56	10°271075	9°802374	17 79	10°197626	10°073449	17 23	9°926551	306	40	40
25	36	9°729024	18 59	10°270976	9°802513	18 84	10°197487	10°073489	18 24	9°926511	312	60	60
30	38	9°729124	19 63	10°270876	9°802653	19 88	10°197347	10°073529	19 25	9°926471	318	80	80
26	40	9°729223	20 66	10°270777	9°802792	20 93	10°197208	10°073569	20 27	9°926431	324	00	00
27	42	9°729323	21 70	10°270677	9°802932	21 98	10°197068	10°073609	21 28	9°926391	330	20	20
30	44	9°729423	22 73	10°270578	9°803072	22 102	10°196928	10°073649	22 29	9°926351	336	40	40
28	46	9°729522	23 76	10°270478	9°803211	23 107	10°196789	10°073689	23 31	9°926311	342	60	60
30	48	9°729621	24 80	10°270379	9°803351	24 112	10°196649	10°073729	24 32	9°926271	348	80	80
29	50	9°729720	25 83	10°270280	9°803490	25 116	10°196510	10°073770	25 33	9°926230	354	00	00
30	52	9°729820	26 86	10°270180	9°803630	26 121	10°196370	10°073810	26 35	9°926190	360	20	20
31	54	9°729919	27 90	10°270081	9°803769	27 126	10°196231	10°073850	27 36	9°926150	366	40	40
32	56	9°730017	28 93	10°269982	9°803909	28 130	10°196091	10°073890	28 38	9°926110	372	60	60
33	58	9°730117	29 96	10°269883	9°804048	29 135	10°195952	10°073931	29 39	9°926069	378	80	80
34	0	9°730217	30 100	10°269784	9°804187	30 139	10°195813	10°073971	30 40	9°926029	384	00	00
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	Parts	°	'

LOG. SINES, COSINES, &c.

2° 10'				32°									
°	'	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	'
30	0	9	9°730217		10°269783	9°804187		10°195813	10°073971		9°926029	80	30
30	1	9	9°730316	1" 3	10°269684	9°804327	1" 5	10°195673	10°074011	1" 1	9°925989	81	29
31	4	9	9°730415	3 7	10°269585	9°804466	3 9	10°195534	10°074051	2 3	9°925949	82	28
31	5	9	9°730514	3 10	10°269486	9°804605	3 14	10°195395	10°074092	3 4	9°925908	83	27
32	8	9	9°730613	4 13	10°269387	9°804745	4 19	10°195255	10°074132	4 5	9°925868	84	26
32	10	9	9°730712	5 16	10°269288	9°804884	5 23	10°195116	10°074172	5 7	9°925828	85	25
33	12	9	9°730811	6 20	10°269189	9°805023	6 28	10°194977	10°074212	6 8	9°925788	86	24
33	14	9	9°730910	7 23	10°269090	9°805163	7 32	10°194837	10°074253	7 9	9°925747	87	23
34	16	9	9°731009	8 26	10°268991	9°805302	8 37	10°194698	10°074293	8 11	9°925707	88	22
34	18	9	9°731108	9 30	10°268892	9°805441	9 42	10°194559	10°074333	9 12	9°925667	89	21
35	20	9	9°731206	10 33	10°268794	9°805580	10 46	10°194420	10°074374	10 13	9°925626	90	20
35	22	9	9°731305	11 36	10°268695	9°805719	11 51	10°194281	10°074414	11 15	9°925586	91	19
36	24	9	9°731404	12 40	10°268596	9°805859	12 56	10°194141	10°074455	12 16	9°925545	92	18
36	26	9	9°731503	13 43	10°268497	9°805998	13 60	10°194002	10°074495	13 18	9°925505	93	17
37	28	9	9°731602	14 46	10°268398	9°806137	14 65	10°193863	10°074535	14 19	9°925465	94	16
37	30	9	9°731700	15 49	10°268299	9°806276	15 70	10°193724	10°074576	15 20	9°925424	95	15
38	32	9	9°731799	16 53	10°268201	9°806415	16 74	10°193585	10°074616	16 22	9°925384	96	14
38	34	9	9°731897	17 56	10°268102	9°806554	17 79	10°193446	10°074657	17 23	9°925343	97	13
39	36	9	9°731996	18 59	10°268004	9°806693	18 83	10°193307	10°074697	18 24	9°925303	98	12
39	38	9	9°732095	19 63	10°267905	9°806832	19 88	10°193168	10°074738	19 26	9°925262	99	11
40	40	9	9°732193	20 66	10°267807	9°806971	20 93	10°193029	10°074778	20 27	9°925222	100	10
40	42	9	9°732292	21 69	10°267708	9°807110	21 97	10°192890	10°074819	21 28	9°925181	101	9
41	44	9	9°732390	22 73	10°267610	9°807249	22 102	10°192751	10°074859	22 30	9°925141	102	8
41	46	9	9°732489	23 76	10°267511	9°807388	23 107	10°192612	10°074900	23 31	9°925100	103	7
42	48	9	9°732587	24 79	10°267413	9°807527	24 111	10°192473	10°074940	24 32	9°925060	104	6
42	50	9	9°732685	25 82	10°267315	9°807666	25 116	10°192334	10°074981	25 34	9°925019	105	5
43	52	9	9°732784	26 86	10°267216	9°807805	26 121	10°192195	10°075021	26 35	9°924979	106	4
43	54	9	9°732882	27 89	10°267118	9°807944	27 125	10°192056	10°075062	27 36	9°924938	107	3
44	56	9	9°732980	28 92	10°267020	9°808083	28 130	10°191917	10°075103	28 38	9°924897	108	2
44	58	9	9°733079	29 95	10°266921	9°808222	29 134	10°191778	10°075143	29 39	9°924857	109	1
45	22	9	9°733177	30 99	10°266823	9°808361	30 139	10°191639	10°075184	30 40	9°924816	110	0
45	24	9	9°733275	1 3	10°266725	9°808499	1 5	10°191501	10°075224	1 1	9°924776	111	29
46	4	9	9°733373	2 6	10°266627	9°808638	2 9	10°191362	10°075265	2 3	9°924735	112	28
46	6	9	9°733471	3 10	10°266529	9°808777	3 14	10°191223	10°075306	3 4	9°924694	113	27
47	8	9	9°733569	4 13	10°266431	9°808916	4 18	10°191084	10°075346	4 5	9°924654	114	26
47	10	9	9°733667	5 16	10°266333	9°809055	5 23	10°190945	10°075387	5 7	9°924613	115	25
48	12	9	9°733765	6 20	10°266235	9°809193	6 28	10°190807	10°075428	6 8	9°924572	116	24
48	14	9	9°733863	7 23	10°266137	9°809332	7 32	10°190668	10°075469	7 10	9°924531	117	23
49	16	9	9°733961	8 26	10°266039	9°809471	8 37	10°190529	10°075509	8 11	9°924491	118	22
49	18	9	9°734059	9 29	10°265941	9°809609	9 42	10°190391	10°075550	9 12	9°924450	119	21
50	20	9	9°734157	10 33	10°265843	9°809748	10 46	10°190252	10°075591	10 14	9°924409	120	20
50	22	9	9°734255	11 36	10°265745	9°809887	11 51	10°190113	10°075632	11 15	9°924368	121	19
51	24	9	9°734353	12 39	10°265647	9°810025	12 55	10°189975	10°075672	12 16	9°924328	122	18
51	26	9	9°734451	13 42	10°265549	9°810164	13 60	10°189836	10°075713	13 18	9°924287	123	17
52	28	9	9°734549	14 46	10°265451	9°810302	14 65	10°189698	10°075754	14 19	9°924246	124	16
52	30	9	9°734646	15 49	10°265354	9°810441	15 69	10°189559	10°075795	15 20	9°924205	125	15
53	32	9	9°734744	16 52	10°265256	9°810580	16 74	10°189420	10°075836	16 22	9°924164	126	14
53	34	9	9°734842	17 55	10°265158	9°810718	17 79	10°189282	10°075876	17 23	9°924124	127	13
54	36	9	9°734939	18 59	10°265060	9°810857	18 83	10°189143	10°075917	18 24	9°924083	128	12
54	38	9	9°735037	19 62	10°264963	9°810995	19 88	10°189005	10°075958	19 26	9°924042	129	11
55	40	9	9°735135	20 65	10°264865	9°811134	20 92	10°188868	10°075999	20 27	9°924001	130	10
55	42	9	9°735232	21 68	10°264768	9°811272	21 97	10°188729	10°076040	21 29	9°923960	131	9
56	44	9	9°735330	22 72	10°264670	9°811410	22 102	10°188590	10°076081	22 30	9°923919	132	8
56	46	9	9°735427	23 75	10°264573	9°811549	23 106	10°188451	10°076122	23 31	9°923878	133	7
57	48	9	9°735525	24 78	10°264475	9°811687	24 111	10°188313	10°076163	24 33	9°923837	134	6
57	50	9	9°735622	25 82	10°264378	9°811826	25 116	10°188174	10°076204	25 34	9°923796	135	5
58	52	9	9°735719	26 85	10°264281	9°811964	26 120	10°188036	10°076245	26 35	9°923755	136	4
58	54	9	9°735817	27 88	10°264183	9°812102	27 125	10°187898	10°076286	27 37	9°923714	137	3
59	56	9	9°735914	28 91	10°264086	9°812241	28 129	10°187759	10°076327	28 38	9°923673	138	2
59	58	9	9°736011	29 95	10°263989	9°812379	29 134	10°187621	10°076368	29 39	9°923632	139	1
60	22	9	9°736109	30 98	10°263891	9°812517	30 139	10°187483	10°076409	30 41	9°923591	140	0
°	'	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	'
												57°	8h 48m

LOG. SINES, COSINES, &c.

2° 12'		33°											
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'
0	0	9°736109		10°263891	9°812517		10°187483	10°076409		9°923591		60	0
30	2	9°736206	1° 3	10°263794	9°812656	1° 5	10°187344	10°076450	1° 1	9°923550	38	30	2
1	4	9°736303	2 6	10°263697	9°812794	2 9	10°187206	10°076491	2 3	9°923509	66	59	4
30	6	9°736400	3 10	10°263600	9°812932	3 14	10°187068	10°076532	3 4	9°923468	94	30	6
2	8	9°736498	4 13	10°263502	9°813070	4 18	10°186930	10°076573	4 5	9°923427	122	58	8
30	10	9°736595	5 16	10°263405	9°813209	5 23	10°186791	10°076614	5 7	9°923386	150	20	10
3	12	9°736692	6 19	10°263308	9°813347	6 28	10°186653	10°076655	6 8	9°923345	178	47	12
30	14	9°736789	7 23	10°263211	9°813485	7 32	10°186515	10°076696	7 10	9°923304	206	30	14
4	16	9°736886	8 26	10°263114	9°813623	8 37	10°186377	10°076737	8 11	9°923263	234	56	16
30	18	9°736983	9 29	10°263017	9°813761	9 41	10°186239	10°076778	9 12	9°923222	262	30	18
5	20	9°737080	10 32	10°262920	9°813899	10 46	10°186101	10°076819	10 14	9°923181	290	55	20
20	22	9°737177	11 36	10°262823	9°814037	11 51	10°185963	10°076861	11 15	9°923139	318	30	22
6	24	9°737274	12 39	10°262726	9°814176	12 55	10°185824	10°076902	12 17	9°923098	346	54	24
30	26	9°737371	13 42	10°262629	9°814314	13 60	10°185686	10°076943	13 18	9°923057	374	30	26
7	28	9°737467	14 45	10°262532	9°814452	14 64	10°185548	10°076984	14 19	9°923016	402	53	28
30	30	9°737564	15 48	10°262436	9°814590	15 69	10°185410	10°077025	15 21	9°922975	430	30	30
8	32	9°737661	16 51	10°262339	9°814728	16 74	10°185272	10°077067	16 22	9°922933	458	52	32
30	34	9°737758	17 55	10°262242	9°814866	17 78	10°185134	10°077108	17 23	9°922892	486	30	34
9	36	9°737855	18 58	10°262145	9°815004	18 83	10°184996	10°077149	18 25	9°922851	514	51	36
30	38	9°737951	19 61	10°262049	9°815142	19 87	10°184858	10°077190	19 26	9°922810	542	30	38
10	40	9°738048	20 64	10°261952	9°815280	20 92	10°184720	10°077232	20 27	9°922768	570	50	40
30	42	9°738145	21 68	10°261855	9°815417	21 97	10°184583	10°077273	21 29	9°922727	598	30	42
11	44	9°738241	22 71	10°261759	9°815555	22 101	10°184445	10°077314	22 30	9°922686	626	49	44
30	46	9°738338	23 74	10°261662	9°815693	23 106	10°184307	10°077356	23 32	9°922644	654	30	46
12	48	9°738434	24 77	10°261566	9°815831	24 110	10°184169	10°077397	24 33	9°922603	682	48	48
30	50	9°738531	25 81	10°261469	9°815969	25 115	10°184031	10°077438	25 34	9°922562	710	30	50
13	52	9°738627	26 84	10°261373	9°816107	26 120	10°183893	10°077480	26 36	9°922520	738	47	52
30	54	9°738724	27 87	10°261276	9°816245	27 124	10°183755	10°077521	27 37	9°922479	766	30	54
14	56	9°738820	28 90	10°261180	9°816382	28 129	10°183618	10°077562	28 38	9°922438	794	46	56
30	58	9°738917	29 94	10°261083	9°816520	29 133	10°183480	10°077604	29 40	9°922396	822	30	58
15	60	9°739013	30 97	10°260987	9°816658	30 138	10°183342	10°077645	30 41	9°922355	850	45	60
30	2	9°739109	1 3	10°260891	9°816796	1 5	10°183204	10°077687	1 1	9°922313	878	30	2
16	4	9°739206	2 6	10°260794	9°816933	2 9	10°183067	10°077728	2 3	9°922272	906	44	4
30	6	9°739302	3 10	10°260698	9°817071	3 14	10°182929	10°077769	3 4	9°922231	934	30	6
17	8	9°739398	4 13	10°260602	9°817209	4 18	10°182791	10°077811	4 6	9°922189	962	43	8
30	10	9°739494	5 16	10°260506	9°817347	5 23	10°182653	10°077852	5 7	9°922148	990	30	10
18	12	9°739590	6 19	10°260410	9°817484	6 27	10°182516	10°077894	6 8	9°922106	1018	42	12
30	14	9°739687	7 22	10°260313	9°817622	7 32	10°182378	10°077935	7 10	9°922065	1046	30	14
19	16	9°739783	8 26	10°260217	9°817759	8 37	10°182241	10°077977	8 11	9°922023	1074	41	16
30	18	9°739879	9 29	10°260121	9°817897	9 41	10°182103	10°078018	9 13	9°921982	1102	30	18
20	20	9°739975	10 32	10°260025	9°818035	10 46	10°181965	10°078060	10 14	9°921940	1130	40	20
30	22	9°740071	11 35	10°259929	9°818172	11 50	10°181828	10°078101	11 15	9°921899	1158	30	22
21	24	9°740167	12 38	10°259833	9°818310	12 55	10°181690	10°078143	12 17	9°921857	1186	39	24
30	26	9°740263	13 42	10°259737	9°818447	13 60	10°181553	10°078185	13 18	9°921815	1214	30	26
22	28	9°740359	14 45	10°259641	9°818585	14 64	10°181415	10°078226	14 19	9°921774	1242	38	28
30	30	9°740455	15 48	10°259545	9°818722	15 69	10°181278	10°078268	15 21	9°921732	1270	30	30
23	32	9°740550	16 51	10°259450	9°818860	16 73	10°181140	10°078309	16 22	9°921691	1298	57	32
30	34	9°740646	17 55	10°259354	9°818997	17 78	10°181003	10°078351	17 24	9°921649	1326	30	34
24	36	9°740742	18 57	10°259258	9°819135	18 82	10°180865	10°078393	18 25	9°921607	1354	36	36
30	38	9°740838	19 61	10°259162	9°819272	19 87	10°180728	10°078434	19 26	9°921566	1382	30	38
25	40	9°740934	20 64	10°259066	9°819410	20 92	10°180590	10°078476	20 28	9°921524	1410	30	40
30	42	9°741029	21 67	10°258971	9°819547	21 96	10°180453	10°078518	21 29	9°921482	1438	30	42
26	44	9°741125	22 70	10°258875	9°819684	22 101	10°180316	10°078559	22 31	9°921441	1466	34	44
30	46	9°741221	23 74	10°258779	9°819822	23 105	10°180178	10°078601	23 32	9°921399	1494	30	46
27	48	9°741316	24 77	10°258684	9°819959	24 110	10°180041	10°078643	24 33	9°921357	1522	33	48
30	50	9°741412	25 80	10°258588	9°820096	25 114	10°179904	10°078685	25 35	9°921315	1550	30	50
28	52	9°741508	26 83	10°258492	9°820234	26 119	10°179766	10°078726	26 36	9°921274	1578	32	52
30	54	9°741603	27 86	10°258397	9°820371	27 124	10°179629	10°078768	27 38	9°921232	1606	30	54
29	56	9°741699	28 89	10°258301	9°820508	28 128	10°179492	10°078810	28 39	9°921190	1634	31	56
30	58	9°741794	29 93	10°258206	9°820646	29 133	10°179354	10°078852	29 40	9°921148	1662	30	58
30	60	9°741889	30 96	10°258111	9°820783	30 137	10°179217	10°078893	30 42	9°921107	1690	30	60
27	0											31	0
27		Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	Parts	27	0

TABLE 68

805

LOG. SINES, COSINES, &c.

2 ^h 14 ^m					33°				
°	'	''	'''	'''	°	'	''	'''	'''
Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	'''
30	8	9° 74' 1889	10° 258111	9° 820783	10° 179217	10° 078493	9° 921107	30	30
30	2	9° 74' 1985	10° 258015	9° 820920	10° 179080	10° 078935	9° 921065	30	30
31	4	9° 74' 2080	10° 257920	9° 821057	10° 178943	10° 078977	9° 921023	30	29
30	6	9° 74' 2176	10° 257824	9° 821195	10° 178805	10° 079019	9° 920981	30	30
32	8	9° 74' 2271	10° 257729	9° 821332	10° 178668	10° 079061	9° 920939	30	28
30	10	9° 74' 2366	10° 257634	9° 821469	10° 178531	10° 079103	9° 920897	30	30
33	12	9° 74' 2462	10° 257538	9° 821606	10° 178394	10° 079144	9° 920856	30	27
30	14	9° 74' 2557	10° 257443	9° 821743	10° 178257	10° 079186	9° 920814	30	30
34	16	9° 74' 2652	10° 257348	9° 821880	10° 178120	10° 079228	9° 920772	30	26
30	18	9° 74' 2747	10° 257253	9° 822017	10° 177983	10° 079270	9° 920730	30	30
35	20	9° 74' 2842	10° 257158	9° 822154	10° 177846	10° 079312	9° 920688	30	25
30	22	9° 74' 2937	10° 257063	9° 822292	10° 177708	10° 079354	9° 920646	30	30
30	24	9° 74' 3033	10° 256967	9° 822429	10° 177571	10° 079396	9° 920604	30	24
30	26	9° 74' 3128	10° 256872	9° 822566	10° 177434	10° 079438	9° 920562	30	30
37	28	9° 74' 3223	10° 256777	9° 822703	10° 177297	10° 079480	9° 920520	30	23
30	30	9° 74' 3318	10° 256682	9° 822840	10° 177160	10° 079522	9° 920478	30	30
32	32	9° 74' 3413	10° 256587	9° 822977	10° 177023	10° 079564	9° 920436	30	22
30	34	9° 74' 3508	10° 256492	9° 823114	10° 176886	10° 079606	9° 920394	30	30
30	36	9° 74' 3602	10° 256398	9° 823251	10° 176749	10° 079648	9° 920352	30	21
30	38	9° 74' 3697	10° 256303	9° 823388	10° 176613	10° 079690	9° 920310	30	30
40	40	9° 74' 3792	10° 256208	9° 823524	10° 176476	10° 079732	9° 920268	30	20
30	42	9° 74' 3887	10° 256113	9° 823661	10° 176339	10° 079774	9° 920226	30	30
41	44	9° 74' 3982	10° 256018	9° 823798	10° 176202	10° 079816	9° 920184	30	19
30	46	9° 74' 4077	10° 255923	9° 823935	10° 176065	10° 079859	9° 920142	30	30
42	48	9° 74' 4171	10° 255829	9° 824072	10° 175928	10° 079901	9° 920099	30	18
30	50	9° 74' 4266	10° 255734	9° 824209	10° 175791	10° 079943	9° 920057	30	30
43	52	9° 74' 4361	10° 255639	9° 824345	10° 175655	10° 079985	9° 920015	30	17
30	54	9° 74' 4455	10° 255545	9° 824482	10° 175518	10° 080027	9° 919973	30	30
44	56	9° 74' 4550	10° 255450	9° 824619	10° 175381	10° 080069	9° 919931	30	16
30	58	9° 74' 4644	10° 255356	9° 824756	10° 175244	10° 080111	9° 919889	30	30
46	60	9° 74' 4739	10° 255261	9° 824893	10° 175107	10° 080153	9° 919846	30	15
30	2	9° 74' 4833	10° 255167	9° 825029	10° 174971	10° 080196	9° 919804	30	30
46	4	9° 74' 4928	10° 255072	9° 825166	10° 174834	10° 080238	9° 919762	30	14
30	6	9° 74' 5022	10° 254978	9° 825303	10° 174697	10° 080280	9° 919720	30	30
47	8	9° 74' 5117	10° 254883	9° 825439	10° 174561	10° 080323	9° 919677	30	13
30	10	9° 74' 5211	10° 254789	9° 825576	10° 174424	10° 080365	9° 919635	30	30
48	12	9° 74' 5306	10° 254694	9° 825713	10° 174287	10° 080407	9° 919593	30	12
30	14	9° 74' 5400	10° 254600	9° 825849	10° 174151	10° 080449	9° 919551	30	30
49	16	9° 74' 5494	10° 254506	9° 825986	10° 174014	10° 080492	9° 919508	30	11
30	18	9° 74' 5589	10° 254411	9° 826123	10° 173877	10° 080534	9° 919466	30	30
50	20	9° 74' 5683	10° 254317	9° 826259	10° 173741	10° 080576	9° 919424	30	10
30	22	9° 74' 5777	10° 254223	9° 826396	10° 173604	10° 080619	9° 919381	30	30
51	24	9° 74' 5871	10° 254129	9° 826532	10° 173468	10° 080661	9° 919339	30	9
30	26	9° 74' 5965	10° 254035	9° 826669	10° 173331	10° 080703	9° 919297	30	30
52	28	9° 74' 6060	10° 253940	9° 826805	10° 173195	10° 080746	9° 919254	30	8
30	30	9° 74' 6154	10° 253846	9° 826942	10° 173058	10° 080788	9° 919212	30	30
53	32	9° 74' 6248	10° 253752	9° 827078	10° 172922	10° 080831	9° 919169	30	7
30	34	9° 74' 6342	10° 253658	9° 827215	10° 172785	10° 080873	9° 919127	30	30
54	36	9° 74' 6436	10° 253564	9° 827351	10° 172649	10° 080915	9° 919085	30	6
30	38	9° 74' 6530	10° 253470	9° 827488	10° 172512	10° 080958	9° 919042	30	30
55	40	9° 74' 6624	10° 253376	9° 827624	10° 172376	10° 081000	9° 919000	30	5
30	42	9° 74' 6718	10° 253282	9° 827761	10° 172239	10° 081043	9° 918957	30	30
56	44	9° 74' 6812	10° 253188	9° 827897	10° 172103	10° 081085	9° 918915	30	4
30	46	9° 74' 6905	10° 253095	9° 828033	10° 171967	10° 081128	9° 918872	30	30
57	48	9° 74' 6999	10° 253001	9° 828170	10° 171830	10° 081170	9° 918830	30	3
30	50	9° 74' 7093	10° 252907	9° 828306	10° 171694	10° 081213	9° 918787	30	30
58	52	9° 74' 7187	10° 252813	9° 828442	10° 171558	10° 081255	9° 918745	30	2
30	54	9° 74' 7281	10° 252719	9° 828579	10° 171421	10° 081298	9° 918702	30	30
59	56	9° 74' 7374	10° 252626	9° 828715	10° 171285	10° 081341	9° 918659	30	1
30	58	9° 74' 7468	10° 252532	9° 828851	10° 171149	10° 081383	9° 918617	30	30
60	60	9° 74' 7562	10° 252438	9° 828987	10° 171013	10° 081426	9° 918574	30	0
°	'	'''	'''	'''	°	'	'''	'''	'''
Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	'''
56°					3 ^h 44 ^m				

LOG. SINES, COSINES, &c.

2 ^h 20 ^m		35°										3 ^h 30 ^m	
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'
0	0	9°758591		10°241409	9°845227		10°154773	10°086635		9°913365		60	0
0	1	9°758681	1' 3	10°241319	9°845361	1" 4	10°154639	10°086680	1" 1	9°913320	30	60	1
1	0	9°758772	2 6	10°241228	9°845496	2 9	10°154504	10°086724	2 3	9°913276	30	59	2
1	1	9°758862	3 9	10°241138	9°845630	3 13	10°154370	10°086768	3 4	9°913232	30	58	3
2	0	9°758952	4 12	10°241048	9°845764	4 18	10°154236	10°086813	4 6	9°913187	30	57	4
2	1	9°759042	5 15	10°240958	9°845899	5 22	10°154101	10°086857	5 7	9°913143	30	56	5
3	0	9°759132	6 18	10°240868	9°846033	6 27	10°153967	10°086901	6 9	9°913099	40	55	6
3	1	9°759222	7 21	10°240778	9°846168	7 31	10°153832	10°086945	7 10	9°913055	40	54	7
4	0	9°759312	8 24	10°240688	9°846302	8 36	10°153698	10°086990	8 12	9°913011	40	53	8
4	1	9°759402	9 27	10°240598	9°846436	9 40	10°153564	10°087034	9 13	9°912966	40	52	9
5	0	9°759492	10 30	10°240508	9°846570	10 45	10°153430	10°087078	10 15	9°912922	40	51	10
5	1	9°759582	11 33	10°240418	9°846705	11 49	10°153295	10°087123	11 16	9°912877	40	50	11
6	0	9°759672	12 36	10°240328	9°846839	12 54	10°153161	10°087167	12 18	9°912833	40	49	12
6	1	9°759762	13 39	10°240238	9°846973	13 58	10°153027	10°087212	13 19	9°912788	40	48	13
7	0	9°759852	14 42	10°240148	9°847108	14 63	10°152892	10°087256	14 21	9°912744	40	47	14
7	1	9°759941	15 45	10°240059	9°847242	15 67	10°152758	10°087300	15 22	9°912700	40	46	15
8	0	9°760031	16 48	10°239969	9°847376	16 72	10°152624	10°087345	16 24	9°912655	40	45	16
8	1	9°760121	17 51	10°239879	9°847510	17 76	10°152490	10°087389	17 25	9°912611	40	44	17
9	0	9°760211	18 54	10°239789	9°847644	18 80	10°152356	10°087434	18 27	9°912566	40	43	18
9	1	9°760300	19 57	10°239700	9°847779	19 85	10°152221	10°087478	19 28	9°912522	40	42	19
10	0	9°760390	20 60	10°239610	9°847913	20 89	10°152087	10°087523	20 30	9°912477	40	41	20
10	1	9°760480	21 63	10°239520	9°848047	21 94	10°151953	10°087567	21 31	9°912433	40	40	21
11	0	9°760569	22 66	10°239431	9°848181	22 98	10°151819	10°087612	22 33	9°912388	40	39	22
11	1	9°760659	23 69	10°239341	9°848315	23 103	10°151685	10°087656	23 34	9°912344	40	38	23
12	0	9°760748	24 72	10°239252	9°848449	24 107	10°151551	10°087701	24 36	9°912299	40	37	24
12	1	9°760838	25 75	10°239162	9°848583	25 112	10°151417	10°087746	25 37	9°912255	40	36	25
13	0	9°760927	26 78	10°239073	9°848717	26 116	10°151283	10°087790	26 38	9°912210	40	35	26
13	1	9°761017	27 81	10°238983	9°848851	27 121	10°151149	10°087835	27 40	9°912165	40	34	27
14	0	9°761106	28 84	10°238894	9°848986	28 125	10°151014	10°087879	28 41	9°912121	40	33	28
14	1	9°761196	29 87	10°238804	9°849120	29 130	10°150880	10°087924	29 43	9°912076	40	32	29
15	0	9°761285	30 90	10°238715	9°849254	30 134	10°150746	10°087969	30 44	9°912031	40	31	30
15	1	9°761374	1 3	10°238626	9°849388	1 4	10°150612	10°088013	1 1	9°911987	40	30	31
16	0	9°761464	2 6	10°238536	9°849522	2 9	10°150478	10°088058	2 3	9°911942	40	29	32
16	1	9°761553	3 9	10°238447	9°849656	3 13	10°150344	10°088103	3 4	9°911897	40	28	33
17	0	9°761642	4 12	10°238358	9°849790	4 18	10°150210	10°088147	4 6	9°911853	40	27	34
17	1	9°761732	5 15	10°238268	9°849924	5 22	10°150076	10°088192	5 7	9°911808	40	26	35
18	0	9°761821	6 18	10°238179	9°850057	6 27	10°149943	10°088237	6 9	9°911763	40	25	36
18	1	9°761910	7 21	10°238090	9°850191	7 31	10°149809	10°088281	7 10	9°911719	40	24	37
19	0	9°761999	8 24	10°238001	9°850325	8 36	10°149675	10°088326	8 12	9°911674	40	23	38
19	1	9°762088	9 27	10°237912	9°850459	9 40	10°149541	10°088371	9 13	9°911629	40	22	39
20	0	9°762177	10 30	10°237823	9°850593	10 45	10°149407	10°088416	10 15	9°911584	40	21	40
20	1	9°762267	11 33	10°237733	9°850727	11 49	10°149273	10°088460	11 16	9°911540	40	20	41
21	0	9°762356	12 36	10°237644	9°850861	12 54	10°149139	10°088505	12 18	9°911495	40	19	42
21	1	9°762445	13 39	10°237555	9°850995	13 58	10°149005	10°088550	13 19	9°911450	40	18	43
22	0	9°762534	14 42	10°237466	9°851129	14 63	10°148871	10°088595	14 21	9°911405	40	17	44
22	1	9°762623	15 45	10°237377	9°851263	15 67	10°148738	10°088640	15 22	9°911360	40	16	45
23	0	9°762712	16 48	10°237288	9°851396	16 72	10°148604	10°088685	16 24	9°911315	40	15	46
23	1	9°762801	17 51	10°237199	9°851530	17 76	10°148470	10°088729	17 25	9°911271	40	14	47
24	0	9°762889	18 54	10°237111	9°851664	18 80	10°148336	10°088774	18 27	9°911226	40	13	48
24	1	9°762978	19 57	10°237022	9°851797	19 85	10°148203	10°088819	19 28	9°911181	40	12	49
25	0	9°763067	20 60	10°236933	9°851931	20 89	10°148069	10°088864	20 30	9°911136	40	11	50
25	1	9°763156	21 63	10°236844	9°852065	21 94	10°147935	10°088909	21 31	9°911091	40	10	51
26	0	9°763245	22 66	10°236755	9°852199	22 98	10°147801	10°088954	22 33	9°911046	40	9	52
26	1	9°763333	23 69	10°236666	9°852332	23 103	10°147668	10°088999	23 34	9°911001	40	8	53
27	0	9°763422	24 72	10°236578	9°852466	24 107	10°147534	10°089044	24 36	9°910956	40	7	54
27	1	9°763511	25 75	10°236489	9°852600	25 112	10°147400	10°089089	25 37	9°910911	40	6	55
28	0	9°763600	26 78	10°236400	9°852733	26 116	10°147267	10°089134	26 38	9°910866	40	5	56
28	1	9°763688	27 81	10°236312	9°852867	27 121	10°147133	10°089179	27 40	9°910821	40	4	57
29	0	9°763777	28 84	10°236223	9°853001	28 125	10°146999	10°089224	28 41	9°910776	40	3	58
29	1	9°763865	29 87	10°236135	9°853134	29 129	10°146866	10°089269	29 43	9°910731	40	2	59
30	0	9°763954	30 90	10°236046	9°853268	30 134	10°146732	10°089314	30 45	9°910686	40	1	60
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	Parts	°	'

LOG. SINES, COSINES, &c.

2 ^h 26 ^m		36°											
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'
30	0	9°774388		10°225612	9°869209		10°130791	10°094821		9°905179	28	30	
30	2	9°774473	1" 3	10°225527	9°869341	1" 4	10°130659	10°094868	1" 2	9°905132	59	29	30
31	4	9°774558	2 6	10°225442	9°869473	2 9	10°130527	10°094915	2 3	9°905085	56	28	30
30	6	9°774644	3 8	10°225356	9°869605	3 13	10°130395	10°094962	3 5	9°905038	54	28	30
32	8	9°774729	4 11	10°225271	9°869737	4 18	10°130263	10°095008	4 6	9°904992	52	28	30
30	10	9°774814	5 14	10°225186	9°869869	5 22	10°130131	10°095055	5 8	9°904945	50	28	30
33	12	9°774899	6 17	10°225101	9°870001	6 26	10°129999	10°095102	6 9	9°904898	48	27	30
30	14	9°774985	7 20	10°225015	9°870133	7 31	10°129867	10°095149	7 11	9°904851	46	26	30
34	16	9°775070	8 23	10°224930	9°870265	8 35	10°129735	10°095196	8 13	9°904804	44	26	30
30	18	9°775155	9 25	10°224845	9°870397	9 40	10°129603	10°095243	9 14	9°904757	42	26	30
35	20	9°775240	10 28	10°224760	9°870529	10 44	10°129471	10°095289	10 16	9°904711	40	25	30
30	22	9°775325	11 31	10°224675	9°870661	11 48	10°129339	10°095336	11 17	9°904664	38	25	30
36	24	9°775410	12 34	10°224590	9°870793	12 53	10°129207	10°095383	12 19	9°904617	36	24	30
30	26	9°775495	13 37	10°224505	9°870925	13 57	10°129075	10°095430	13 20	9°904570	34	24	30
37	28	9°775580	14 40	10°224420	9°871057	14 62	10°128943	10°095477	14 22	9°904523	32	23	30
30	30	9°775665	15 42	10°224335	9°871189	15 66	10°128811	10°095524	15 24	9°904476	30	23	30
38	32	9°775750	16 45	10°224250	9°871321	16 70	10°128679	10°095571	16 25	9°904429	28	22	30
30	34	9°775835	17 48	10°224165	9°871453	17 75	10°128547	10°095618	17 27	9°904382	26	22	30
30	36	9°775920	18 51	10°224080	9°871585	18 79	10°128415	10°095665	18 28	9°904335	24	21	30
30	38	9°776005	19 54	10°223995	9°871717	19 84	10°128283	10°095712	19 30	9°904288	22	20	30
40	40	9°776090	20 57	10°223910	9°871849	20 88	10°128151	10°095759	20 31	9°904241	20	20	30
30	42	9°776175	21 59	10°223825	9°871980	21 92	10°128020	10°095806	21 33	9°904194	18	20	30
11	44	9°776259	22 62	10°223741	9°872112	22 97	10°127888	10°095853	22 34	9°904147	16	19	30
30	46	9°776344	23 65	10°223656	9°872244	23 101	10°127756	10°095900	23 36	9°904100	14	20	30
42	48	9°776429	24 68	10°223571	9°872376	24 106	10°127624	10°095947	24 38	9°904053	12	18	30
30	50	9°776514	25 71	10°223486	9°872508	25 110	10°127492	10°095994	25 39	9°904006	10	20	30
43	52	9°776598	26 74	10°223402	9°872640	26 114	10°127360	10°096041	26 41	9°903959	8	17	30
30	54	9°776683	27 76	10°223317	9°872771	27 119	10°127228	10°096088	27 42	9°903912	6	16	30
44	56	9°776768	28 79	10°223232	9°872903	28 123	10°127097	10°096136	28 44	9°903864	4	16	30
30	58	9°776852	29 82	10°223148	9°873035	29 128	10°126965	10°096183	29 46	9°903817	2	15	30
45	59	9°776937	30 85	10°223063	9°873167	30 132	10°126833	10°096230	30 47	9°903770	33	15	30
30	2	9°777021	1 3	10°222979	9°873299	1 4	10°126701	10°096277	1 2	9°903723	36	20	30
46	4	9°777106	2 6	10°222894	9°873430	2 9	10°126570	10°096324	2 3	9°903676	56	14	30
30	6	9°777191	3 8	10°222809	9°873562	3 13	10°126438	10°096371	3 5	9°903629	54	20	30
47	8	9°777275	4 11	10°222725	9°873694	4 18	10°126306	10°096419	4 6	9°903581	52	13	30
30	10	9°777359	5 14	10°222641	9°873825	5 22	10°126175	10°096466	5 8	9°903534	50	20	30
48	12	9°777444	6 17	10°222556	9°873957	6 26	10°126043	10°096513	6 9	9°903487	48	12	30
30	14	9°777528	7 20	10°222472	9°874089	7 31	10°125911	10°096560	7 11	9°903440	46	20	30
49	16	9°777613	8 23	10°222387	9°874220	8 35	10°125780	10°096608	8 13	9°903392	44	11	30
30	18	9°777697	9 25	10°222303	9°874352	9 40	10°125648	10°096655	9 14	9°903345	42	20	30
50	20	9°777781	10 28	10°222219	9°874484	10 44	10°125516	10°096702	10 16	9°903298	40	10	30
30	22	9°777866	11 31	10°222134	9°874615	11 48	10°125385	10°096750	11 17	9°903250	38	20	30
51	24	9°777950	12 34	10°222050	9°874747	12 53	10°125253	10°096797	12 19	9°903203	36	9	30
30	26	9°778034	13 37	10°221966	9°874879	13 57	10°125121	10°096844	13 21	9°903156	34	20	30
52	28	9°778119	14 40	10°221881	9°875010	14 61	10°124990	10°096892	14 22	9°903108	32	8	30
30	30	9°778203	15 42	10°221797	9°875142	15 66	10°124858	10°096939	15 24	9°903061	30	20	30
53	32	9°778287	16 45	10°221713	9°875273	16 70	10°124727	10°096986	16 25	9°903014	28	7	30
30	34	9°778371	17 48	10°221629	9°875405	17 75	10°124595	10°097034	17 27	9°902966	26	20	30
54	36	9°778455	18 51	10°221545	9°875537	18 79	10°124463	10°097081	18 28	9°902919	24	6	30
30	38	9°778539	19 54	10°221461	9°875668	19 83	10°124332	10°097129	19 30	9°902871	22	30	30
55	40	9°778624	20 57	10°221376	9°875800	20 88	10°124200	10°097176	20 32	9°902824	20	5	30
30	42	9°778708	21 59	10°221292	9°875931	21 92	10°124069	10°097224	21 33	9°902776	18	20	30
56	44	9°778792	22 62	10°221208	9°876063	22 97	10°123937	10°097271	22 35	9°902729	16	4	30
30	46	9°778876	23 65	10°221124	9°876194	23 101	10°123806	10°097319	23 36	9°902681	14	20	30
57	48	9°778960	24 68	10°221040	9°876326	24 105	10°123674	10°097366	24 38	9°902634	12	3	30
30	50	9°779044	25 70	10°220956	9°876457	25 110	10°123543	10°097414	25 39	9°902586	10	20	30
58	52	9°779128	26 73	10°220872	9°876589	26 114	10°123411	10°097461	26 41	9°902539	8	2	30
30	54	9°779211	27 76	10°220789	9°876720	27 119	10°123280	10°097509	27 43	9°902491	6	20	30
59	56	9°779295	28 79	10°220705	9°876852	28 123	10°123148	10°097556	28 44	9°902444	4	1	30
30	58	9°779379	29 82	10°220621	9°876983	29 127	10°123017	10°097604	29 46	9°902396	2	20	30
60	59	9°779463	30 85	10°220537	9°877114	30 132	10°122886	10°097651	30 47	9°902349	0	0	30
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	Parts	°	'

LOG. SINES, COSINES, &c.

2 ^h 24 ^m		37°											
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'
0	0	9°779463		10°220537	9°877114	1	10°122286	10°097651	1°2	9°902349	32	60	
30	2	9°779547	1°3	10°220453	9°877246	4	10°122754	10°097600	2	9°902301	30	30	
1	4	9°779631	2	10°220369	9°877377	9	10°123263	10°097747	3	9°902253	28	50	
30	6	9°779714	3	10°220286	9°877509	13	10°123791	10°097794	5	9°902206	26	30	
2	8	9°779798	4	10°220202	9°877640	17	10°124360	10°097842	6	9°902158	24	68	
30	10	9°779882	5	10°220118	9°877771	22	10°124929	10°097890	8	9°902110	22	30	
3	12	9°779966	6	10°220034	9°877903	26	10°125497	10°097937	10	9°902063	20	67	
30	14	9°780049	7	10°219951	9°878034	31	10°126066	10°097985	12	9°902015	18	20	
4	16	9°780133	8	10°219867	9°878165	35	10°126635	10°098033	14	9°901967	16	66	
30	18	9°780216	9	10°219784	9°878297	39	10°127203	10°098080	16	9°901920	14	20	
5	20	9°780300	10	10°219700	9°878428	44	10°127772	10°098128	18	9°901872	12	56	
30	22	9°780384	11	10°219616	9°878559	48	10°128341	10°098176	20	9°901824	10	20	
6	24	9°780467	12	10°219533	9°878691	52	10°128909	10°098224	22	9°901776	8	54	
30	26	9°780551	13	10°219449	9°878822	57	10°129478	10°098271	24	9°901729	6	20	
7	28	9°780634	14	10°219366	9°878953	61	10°130047	10°098319	26	9°901681	4	53	
30	30	9°780718	15	10°219282	9°879085	66	10°130615	10°098367	28	9°901633	2	20	
8	32	9°780801	16	10°219199	9°879216	70	10°131184	10°098415	30	9°901585		62	
30	34	9°780884	17	10°219116	9°879347	74	10°131753	10°098463	32	9°901537		20	
9	36	9°780968	18	10°219032	9°879478	79	10°132322	10°098510	34	9°901490		51	
30	38	9°781051	19	10°218949	9°879609	83	10°132891	10°098558	36	9°901442		20	
10	40	9°781134	20	10°218866	9°879741	87	10°133460	10°098606	38	9°901394		50	
30	42	9°781218	21	10°218782	9°879872	92	10°134029	10°098654	40	9°901346		30	
11	44	9°781301	22	10°218699	9°880003	96	10°134598	10°098702	42	9°901298		49	
30	46	9°781384	23	10°218616	9°880134	101	10°135167	10°098750	44	9°901250		14	
12	48	9°781468	24	10°218532	9°880265	105	10°135735	10°098798	46	9°901202		48	
30	50	9°781551	25	10°218449	9°880397	109	10°136304	10°098846	48	9°901154		10	
13	52	9°781634	26	10°218366	9°880528	114	10°136873	10°098894	50	9°901106		47	
30	54	9°781717	27	10°218283	9°880659	118	10°137442	10°098942	52	9°901058		20	
14	56	9°781800	28	10°218200	9°880790	122	10°138011	10°098990	54	9°901010		46	
30	58	9°781883	29	10°218117	9°880921	127	10°138580	10°099038	56	9°900962		2	
15	60	9°781966	30	10°218034	9°881052	131	10°139149	10°099086	58	9°900914		45	
30	2	9°782049	1	10°217951	9°881183	1	10°139718	10°099134	1	9°900866		38	
16	4	9°782132	2	10°217868	9°881314	9	10°140287	10°099182	3	9°900818		36	
30	6	9°782215	3	10°217785	9°881445	13	10°140856	10°099230	5	9°900770		54	
17	8	9°782298	4	10°217702	9°881577	17	10°141425	10°099278	7	9°900722		32	
30	10	9°782381	5	10°217619	9°881708	22	10°141994	10°099326	9	9°900674		30	
18	12	9°782464	6	10°217536	9°881839	26	10°142563	10°099374	11	9°900626		48	
30	14	9°782547	7	10°217453	9°881970	31	10°143132	10°099422	13	9°900578		46	
19	16	9°782630	8	10°217370	9°882101	35	10°143701	10°099470	15	9°900530		41	
30	18	9°782713	9	10°217287	9°882232	39	10°144270	10°099519	17	9°900482		42	
20	20	9°782796	10	10°217204	9°882363	44	10°144839	10°099567	19	9°900434		40	
30	22	9°782879	11	10°217121	9°882494	48	10°145408	10°099615	21	9°900386		38	
21	24	9°782961	12	10°217039	9°882625	52	10°145977	10°099663	23	9°900338		39	
30	26	9°783044	13	10°216956	9°882756	57	10°146546	10°099711	25	9°900290		34	
22	28	9°783127	14	10°216873	9°882887	61	10°147115	10°099759	27	9°900242		32	
30	30	9°783210	15	10°216790	9°883018	65	10°147684	10°099807	29	9°900194		30	
23	32	9°783292	16	10°216708	9°883148	70	10°148253	10°099855	31	9°900146		37	
30	34	9°783375	17	10°216625	9°883279	74	10°148822	10°099903	33	9°900098		20	
24	36	9°783458	18	10°216542	9°883410	78	10°149391	10°099951	35	9°900050		36	
30	38	9°783540	19	10°216460	9°883541	83	10°149960	10°100000	37	9°900002		22	
25	40	9°783623	20	10°216377	9°883672	87	10°150529	10°100049	39	9°900000		35	
30	42	9°783706	21	10°216295	9°883803	92	10°151098	10°100098	41	9°900000		18	
26	44	9°783788	22	10°216212	9°883934	96	10°151667	10°100146	43	9°900000		16	
30	46	9°783870	23	10°216130	9°884065	101	10°152236	10°100194	45	9°900000		14	
27	48	9°783953	24	10°216047	9°884196	105	10°152805	10°100243	47	9°900000		12	
30	50	9°784035	25	10°215965	9°884326	109	10°153374	10°100291	49	9°900000		10	
28	52	9°784118	26	10°215882	9°884457	113	10°153943	10°100340	51	9°900000		8	
30	54	9°784200	27	10°215800	9°884588	118	10°154512	10°100388	53	9°900000		6	
29	56	9°784282	28	10°215718	9°884719	122	10°155081	10°100436	55	9°900000		4	
30	58	9°784365	29	10°215635	9°884850	127	10°155650	10°100485	57	9°900000		2	
30	60	9°784447	30	10°215553	9°884980	131	10°156219	10°100533	59	9°900000		0	
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	Parts	°	'

LOG. SINES, COSINES, &c.

2° 32'		38°											
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'
		Parts	Parts	Parts	Parts	Parts	Parts	Parts	Parts	Parts	Parts		
0	0	9°789342		10°210658	9°892810	1	10°107190	10°103468	1	9°896532	28	60	
0	1	9°789443	1 3	10°210577	9°892940	2	10°107060	10°103517	2	9°896483	28	59	
1	4	9°789504	2 5	10°210496	9°893070	3	10°106930	10°103567	3	9°896433	28	58	
2	8	9°789584	3 8	10°210416	9°893200	4	10°106800	10°103616	4	9°896384	28	57	
3	12	9°789665	4 11	10°210335	9°893331	5	10°106669	10°103665	5	9°896335	28	56	
4	16	9°789746	5 13	10°210254	9°893461	6	10°106539	10°103715	6	9°896285	28	55	
5	20	9°789827	6 16	10°210173	9°893591	7	10°106409	10°103764	7	9°896236	28	54	
6	24	9°789907	7 19	10°210093	9°893721	8	10°106279	10°103814	8	9°896186	28	53	
7	28	9°789988	8 21	10°210012	9°893851	9	10°106149	10°103863	9	9°896137	28	52	
8	32	9°790069	9 24	10°209931	9°893981	10	10°106019	10°103913	10	9°896087	28	51	
9	36	9°790149	10 27	10°209851	9°894111	11	10°105889	10°103962	11	9°896038	28	50	
10	40	9°790230	11 29	10°209770	9°894241	12	10°105759	10°104012	12	9°895988	28	49	
11	44	9°790310	12 32	10°209690	9°894371	13	10°105628	10°104061	13	9°895939	28	48	
12	48	9°790391	13 35	10°209609	9°894502	14	10°105498	10°104111	14	9°895889	28	47	
13	52	9°790471	14 37	10°209529	9°894632	15	10°105368	10°104160	15	9°895839	28	46	
14	56	9°790552	15 40	10°209448	9°894762	16	10°105238	10°104210	16	9°895789	28	45	
15	0	9°790632	16 43	10°209368	9°894892	17	10°105108	10°104259	17	9°895739	28	44	
16	4	9°790713	17 46	10°209287	9°895022	18	10°104978	10°104309	18	9°895689	28	43	
17	8	9°790793	18 48	10°209207	9°895152	19	10°104848	10°104359	19	9°895639	28	42	
18	12	9°790874	19 51	10°209126	9°895282	20	10°104718	10°104408	20	9°895589	28	41	
19	16	9°790954	20 54	10°209046	9°895412	21	10°104588	10°104458	21	9°895539	28	40	
20	20	9°791034	21 56	10°208966	9°895542	22	10°104458	10°104507	22	9°895489	28	39	
21	24	9°791115	22 59	10°208885	9°895672	23	10°104328	10°104557	23	9°895439	28	38	
22	28	9°791195	23 62	10°208805	9°895802	24	10°104198	10°104607	24	9°895389	28	37	
23	32	9°791275	24 65	10°208725	9°895932	25	10°104068	10°104657	25	9°895339	28	36	
24	36	9°791356	25 67	10°208644	9°896062	26	10°103938	10°104706	26	9°895289	28	35	
25	40	9°791436	26 70	10°208564	9°896192	27	10°103808	10°104756	27	9°895239	28	34	
26	44	9°791516	27 72	10°208484	9°896322	28	10°103678	10°104806	28	9°895189	28	33	
27	48	9°791596	28 75	10°208404	9°896452	29	10°103548	10°104855	29	9°895139	28	32	
28	52	9°791677	29 78	10°208324	9°896582	30	10°103418	10°104905	30	9°895089	28	31	
29	56	9°791757	30 80	10°208243	9°896712	31	10°103288	10°104955	31	9°895039	28	30	
30	0	9°791837	1 3	10°208163	9°896842	32	10°103158	10°105005	32	9°894989	28	29	
31	4	9°791917	2 5	10°208083	9°896972	33	10°103028	10°105055	33	9°894939	28	28	
32	8	9°791997	3 8	10°208003	9°897102	34	10°102898	10°105105	34	9°894889	28	27	
33	12	9°792077	4 11	10°207923	9°897232	35	10°102768	10°105155	35	9°894839	28	26	
34	16	9°792157	5 13	10°207843	9°897362	36	10°102638	10°105205	36	9°894789	28	25	
35	20	9°792237	6 16	10°207763	9°897492	37	10°102508	10°105255	37	9°894739	28	24	
36	24	9°792317	7 19	10°207683	9°897622	38	10°102378	10°105305	38	9°894689	28	23	
37	28	9°792397	8 21	10°207603	9°897752	39	10°102248	10°105355	39	9°894639	28	22	
38	32	9°792477	9 24	10°207523	9°897882	40	10°102118	10°105405	40	9°894589	28	21	
39	36	9°792557	10 27	10°207443	9°898012	41	10°101988	10°105455	41	9°894539	28	20	
40	40	9°792636	11 30	10°207364	9°898142	42	10°101858	10°105505	42	9°894489	28	19	
41	44	9°792716	12 32	10°207284	9°898272	43	10°101728	10°105555	43	9°894439	28	18	
42	48	9°792796	13 35	10°207204	9°898402	44	10°101600	10°105605	44	9°894389	28	17	
43	52	9°792876	14 37	10°207124	9°898532	45	10°101470	10°105655	45	9°894339	28	16	
44	56	9°792956	15 40	10°207044	9°898662	46	10°101341	10°105705	46	9°894289	28	15	
45	0	9°793035	16 43	10°206965	9°898792	47	10°101211	10°105755	47	9°894239	28	14	
46	4	9°793115	17 46	10°206885	9°898922	48	10°101081	10°105805	48	9°894189	28	13	
47	8	9°793195	18 48	10°206805	9°899052	49	10°100951	10°105855	49	9°894139	28	12	
48	12	9°793275	19 51	10°206725	9°899182	50	10°100822	10°105905	50	9°894089	28	11	
49	16	9°793354	20 54	10°206646	9°899312	51	10°100692	10°105955	51	9°894039	28	10	
50	20	9°793434	21 56	10°206566	9°899442	52	10°100562	10°106005	52	9°893989	28	9	
51	24	9°793514	22 59	10°206486	9°899572	53	10°100432	10°106055	53	9°893939	28	8	
52	28	9°793593	23 62	10°206407	9°899702	54	10°100303	10°106105	54	9°893889	28	7	
53	32	9°793673	24 65	10°206327	9°899832	55	10°100173	10°106155	55	9°893839	28	6	
54	36	9°793752	25 67	10°206248	9°899962	56	10°100043	10°106205	56	9°893789	28	5	
55	40	9°793832	26 70	10°206168	9°900092	57	10°099913	10°106255	57	9°893739	28	4	
56	44	9°793911	27 72	10°206089	9°900222	58	10°099784	10°106305	58	9°893689	28	3	
57	48	9°793991	28 75	10°206009	9°900352	59	10°099654	10°106355	59	9°893639	28	2	
58	52	9°794070	29 78	10°205930	9°900482	60	10°099524	10°106405	60	9°893589	28	1	
59	56	9°794150	30 80	10°205850	9°900612	61	10°099395	10°106455	61	9°893539	28	0	
60	0					62			62				

TABLE 68

817

LOG. SINES, COSINES, &c.

2 ^h 38 ^m										39°									
''	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	''	''	m.	''				
30	0	9°803511		10°196489	9°916104		10°883866	10°112594		9°887406	22	30							
30	2	9°803587	1° 3	10°196413	9°916233	1° 4	10°883767	10°112668	1° 2	9°887354	38	30							
31	4	9°803664	2 5	10°195336	9°916362	2 9	10°883638	10°112698	2 3	9°887302	54	29							
30	6	9°803740	3 8	10°196260	9°916491	3 13	10°883510	10°112750	3 5	9°887250	54	30							
32	8	9°803817	4 10	10°196183	9°916619	4 17	10°883381	10°112802	4 7	9°887198	52	28							
30	10	9°803893	5 13	10°196107	9°916748	5 21	10°883252	10°112854	5 9	9°887146	50	30							
33	12	9°803970	6 15	10°196030	9°916877	6 26	10°883123	10°112907	6 10	9°887093	48	27							
30	14	9°804046	7 18	10°195954	9°917005	7 30	10°882995	10°112959	7 12	9°887041	40	30							
34	16	9°804123	8 20	10°195877	9°917134	8 34	10°882866	10°113011	8 14	9°886989	41	26							
30	18	9°804199	9 23	10°195801	9°917262	9 39	10°882738	10°113063	9 16	9°886937	42	30							
35	20	9°804276	10 25	10°195724	9°917391	10 43	10°882609	10°113115	10 17	9°886885	40	25							
30	22	9°804352	11 28	10°195648	9°917520	11 47	10°882480	10°113168	11 19	9°886832	38	30							
36	24	9°804428	12 30	10°195572	9°917648	12 51	10°882352	10°113220	12 21	9°886780	36	24							
30	26	9°804505	13 33	10°195495	9°917777	13 56	10°882223	10°113272	13 23	9°886728	34	30							
37	28	9°804581	14 35	10°195419	9°917906	14 60	10°882094	10°113324	14 24	9°886676	32	23							
30	30	9°804657	15 38	10°195343	9°918034	15 64	10°881966	10°113377	15 26	9°886623	30	30							
38	32	9°804734	16 40	10°195266	9°918163	16 69	10°881837	10°113429	16 28	9°886571	28	22							
30	34	9°804810	17 43	10°195190	9°918291	17 73	10°881709	10°113481	17 30	9°886519	26	30							
39	36	9°804886	18 46	10°195114	9°918420	18 77	10°881580	10°113534	18 31	9°886466	24	21							
30	38	9°804962	19 48	10°195038	9°918548	19 81	10°881452	10°113586	19 33	9°886414	22	30							
40	40	9°805039	20 51	10°194961	9°918677	20 80	10°881323	10°113638	20 35	9°886362	20	20							
30	42	9°805115	21 53	10°194885	9°918805	21 90	10°881195	10°113691	21 37	9°886309	18	30							
41	44	9°805191	22 56	10°194809	9°918934	22 94	10°881066	10°113743	22 38	9°886257	16	19							
30	46	9°805267	23 58	10°194733	9°919063	23 99	10°880937	10°113796	23 40	9°886204	14	30							
42	48	9°805343	24 61	10°194657	9°919191	24 103	10°880809	10°113848	24 42	9°886152	12	18							
30	50	9°805419	25 63	10°194581	9°919320	25 107	10°880680	10°113901	25 44	9°886099	10	30							
43	52	9°805495	26 66	10°194505	9°919448	26 111	10°880552	10°113953	26 45	9°886047	8	17							
30	54	9°805571	27 68	10°194429	9°919577	27 116	10°880423	10°114005	27 47	9°885995	6	30							
44	56	9°805647	28 71	10°194353	9°919705	28 120	10°880295	10°114058	28 49	9°885942	4	16							
30	58	9°805723	29 73	10°194277	9°919834	29 124	10°880166	10°114110	29 50	9°885890	2	30							
45	59	9°805799	30 76	10°194201	9°919962	30 129	10°880038	10°114163	30 52	9°885837	21	15							
30	2	9°805875	1 3	10°194125	9°920091	1 4	10°879909	10°114216	1 2	9°885784	38	30							
46	4	9°805951	2 5	10°194049	9°920219	2 9	10°879781	10°114268	2 4	9°885732	56	14							
30	6	9°806027	3 8	10°193973	9°920348	3 13	10°879652	10°114321	3 5	9°885679	54	30							
47	8	9°806103	4 10	10°193897	9°920476	4 17	10°879524	10°114373	4 7	9°885627	52	13							
30	10	9°806179	5 13	10°193821	9°920604	5 21	10°879396	10°114426	5 9	9°885574	50	30							
48	12	9°806254	6 15	10°193746	9°920733	6 26	10°879267	10°114478	6 11	9°885522	48	12							
30	14	9°806330	7 18	10°193670	9°920861	7 30	10°879139	10°114531	7 12	9°885469	46	30							
49	16	9°806406	8 20	10°193594	9°920990	8 34	10°879010	10°114584	8 14	9°885416	44	11							
30	18	9°806482	9 23	10°193518	9°921118	9 39	10°878882	10°114636	9 16	9°885364	42	30							
50	20	9°806557	10 25	10°193443	9°921247	10 43	10°878753	10°114689	10 18	9°885311	40	10							
30	22	9°806633	11 28	10°193367	9°921375	11 47	10°878625	10°114742	11 20	9°885258	38	30							
51	24	9°806709	12 30	10°193291	9°921503	12 51	10°878497	10°114795	12 21	9°885205	36	9							
30	26	9°806785	13 33	10°193215	9°921632	13 56	10°878368	10°114847	13 23	9°885153	34	30							
52	28	9°806860	14 35	10°193140	9°921760	14 60	10°878240	10°114900	14 25	9°885100	32	8							
30	30	9°806936	15 38	10°193064	9°921889	15 64	10°878111	10°114953	15 26	9°885047	30	30							
53	32	9°807011	16 40	10°192989	9°922017	16 68	10°877983	10°115006	16 28	9°884994	28	7							
30	34	9°807087	17 43	10°192913	9°922145	17 73	10°877855	10°115058	17 30	9°884942	26	30							
54	36	9°807163	18 45	10°192837	9°922274	18 77	10°877726	10°115111	18 32	9°884889	24	6							
30	38	9°807238	19 48	10°192762	9°922402	19 81	10°877598	10°115164	19 33	9°884836	22	30							
55	40	9°807314	20 50	10°192686	9°922530	20 86	10°877470	10°115217	20 35	9°884783	20	5							
30	42	9°807389	21 53	10°192611	9°922659	21 90	10°877341	10°115270	21 37	9°884730	18	30							
56	44	9°807465	22 55	10°192535	9°922787	22 94	10°877213	10°115323	22 39	9°884677	16	4							
30	46	9°807540	23 58	10°192460	9°922915	23 98	10°877085	10°115375	23 40	9°884625	14	30							
57	48	9°807615	24 60	10°192385	9°923044	24 103	10°876956	10°115428	24 42	9°884572	12	3							
30	50	9°807691	25 63	10°192309	9°923172	25 107	10°876828	10°115481	25 44	9°884519	10	30							
58	52	9°807766	26 65	10°192234	9°923300	26 111	10°876700	10°115534	26 46	9°884466	8	2							
30	54	9°807842	27 68	10°192158	9°923429	27 116	10°876571	10°115587	27 48	9°884413	6	30							
59	56	9°807917	28 70	10°192083	9°923557	28 120	10°876443	10°115640	28 49	9°884360	4	1							
30	58	9°807992	29 73	10°192008	9°923685	29 124	10°876315	10°115693	29 51	9°884307	2	30							
(H)	60	9°808067	30 76	10°191933	9°923814	30 128	10°876186	10°115746	30 53	9°884254	0	0							
''	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	''							

50°

34

LOG. SINES, COSINES, &c.

2° 42'		40°											
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	mm.	°	'
30	0	9°8'12544		10°187456	9°931499		10°068501	10°118954		9°881046	10	30	0
30	2	9°8'12618	1" 2	10°187382	9°931627	1" 4	10°068373	10°119008	1" 2	9°880992	58	30	2
31	4	9°8'12692	2 5	10°187308	9°931755	2 9	10°068245	10°119062	2 4	9°880938	50	30	4
30	6	9°8'12766	3 7	10°187234	9°931883	3 13	10°068117	10°119116	3 5	9°880884	54	30	6
32	8	9°8'12840	4 10	10°187160	9°932010	4 17	10°067990	10°119170	4 7	9°880830	52	30	8
30	10	9°8'12914	5 12	10°187086	9°932138	5 21	10°067862	10°119224	5 9	9°880776	50	30	10
33	12	9°8'12988	6 15	10°187012	9°932266	6 26	10°067734	10°119278	6 11	9°880722	48	30	12
30	14	9°8'13062	7 17	10°186938	9°932394	7 30	10°067606	10°119332	7 13	9°880668	46	30	14
34	16	9°8'13135	8 20	10°186865	9°932522	8 34	10°067478	10°119387	8 14	9°880613	44	30	16
30	18	9°8'13209	9 22	10°186791	9°932650	9 38	10°067350	10°119441	9 16	9°880559	42	30	18
35	20	9°8'13283	10 24	10°186717	9°932778	10 43	10°067222	10°119495	10 18	9°880505	40	30	20
30	22	9°8'13357	11 27	10°186643	9°932906	11 47	10°067094	10°119549	11 20	9°880451	38	30	22
36	24	9°8'13430	12 29	10°186570	9°933033	12 51	10°066966	10°119603	12 22	9°880397	36	30	24
30	26	9°8'13504	13 32	10°186496	9°933161	13 55	10°066839	10°119657	13 24	9°880343	34	30	26
37	28	9°8'13578	14 34	10°186422	9°933289	14 60	10°066711	10°119711	14 25	9°880289	32	30	28
30	30	9°8'13651	15 37	10°186349	9°933417	15 64	10°066583	10°119766	15 27	9°880234	30	30	30
38	32	9°8'13725	16 39	10°186275	9°933545	16 68	10°066455	10°119820	16 29	9°880180	28	30	32
30	34	9°8'13799	17 42	10°186201	9°933672	17 72	10°066328	10°119874	17 31	9°880126	26	30	34
39	36	9°8'13872	18 44	10°186128	9°933800	18 77	10°066200	10°119928	18 32	9°880072	24	30	36
30	38	9°8'13946	19 47	10°186054	9°933928	19 81	10°066072	10°119982	19 34	9°880018	22	30	38
40	40	9°8'14019	20 49	10°185981	9°934056	20 85	10°065944	10°120037	20 36	9°879963	20	30	40
30	42	9°8'14093	21 51	10°185907	9°934184	21 89	10°065816	10°120091	21 38	9°879909	18	30	42
41	44	9°8'14166	22 54	10°185834	9°934311	22 94	10°065689	10°120145	22 40	9°879855	16	30	44
30	46	9°8'14240	23 56	10°185760	9°934439	23 98	10°065561	10°120200	23 42	9°879800	14	30	46
42	48	9°8'14313	24 59	10°185687	9°934567	24 102	10°065433	10°120254	24 43	9°879746	12	30	48
30	50	9°8'14387	25 61	10°185613	9°934695	25 106	10°065305	10°120308	25 45	9°879692	10	30	50
43	52	9°8'14460	26 64	10°185540	9°934822	26 111	10°065178	10°120363	26 47	9°879637	8	30	52
30	54	9°8'14533	27 66	10°185467	9°934950	27 115	10°065050	10°120417	27 49	9°879583	6	30	54
44	56	9°8'14607	28 69	10°185393	9°935078	28 119	10°064922	10°120471	28 51	9°879529	4	30	56
30	58	9°8'14680	29 71	10°185320	9°935206	29 124	10°064794	10°120526	29 52	9°879474	2	30	58
45	60	9°8'14753	30 74	10°185247	9°935333	30 128	10°064667	10°120580	30 54	9°879420	0	30	60
30	2	9°8'14827	1 2	10°185173	9°935461	1 4	10°064539	10°120635	1 2	9°879365	58	30	2
46	4	9°8'14900	2 5	10°185100	9°935589	2 9	10°064411	10°120689	2 4	9°879311	56	30	4
30	6	9°8'14973	3 7	10°185027	9°935717	3 13	10°064283	10°120743	3 5	9°879257	54	30	6
47	8	9°8'15046	4 10	10°184954	9°935844	4 17	10°064156	10°120798	4 7	9°879202	52	30	8
30	10	9°8'15120	5 12	10°184880	9°935972	5 21	10°064028	10°120852	5 9	9°879148	50	30	10
48	12	9°8'15193	6 15	10°184807	9°936100	6 26	10°063900	10°120907	6 11	9°879093	48	30	12
30	14	9°8'15266	7 17	10°184734	9°936227	7 30	10°063773	10°120961	7 13	9°879039	46	30	14
49	16	9°8'15339	8 20	10°184661	9°936355	8 34	10°063645	10°121016	8 15	9°878984	44	30	16
30	18	9°8'15412	9 22	10°184588	9°936483	9 38	10°063517	10°121071	9 16	9°878929	42	30	18
50	20	9°8'15485	10 24	10°184515	9°936611	10 43	10°063389	10°121125	10 18	9°878875	40	30	20
30	22	9°8'15558	11 27	10°184442	9°936738	11 47	10°063262	10°121180	11 20	9°878820	38	30	22
51	24	9°8'15632	12 29	10°184368	9°936866	12 51	10°063134	10°121234	12 22	9°878766	36	30	24
30	26	9°8'15705	13 32	10°184295	9°936994	13 55	10°063006	10°121289	13 24	9°878711	34	30	26
52	28	9°8'15778	14 34	10°184222	9°937121	14 60	10°062879	10°121344	14 25	9°878656	32	30	28
30	30	9°8'15851	15 36	10°184149	9°937249	15 64	10°062751	10°121398	15 27	9°878602	30	30	30
53	32	9°8'15924	16 39	10°184076	9°937377	16 68	10°062623	10°121453	16 29	9°878547	28	30	32
30	34	9°8'15996	17 41	10°184004	9°937504	17 72	10°062496	10°121508	17 31	9°878492	26	30	34
54	36	9°8'16069	18 44	10°183931	9°937632	18 77	10°062368	10°121562	18 33	9°878438	24	30	36
30	38	9°8'16142	19 46	10°183858	9°937759	19 81	10°062241	10°121617	19 35	9°878383	22	30	38
55	40	9°8'16215	20 49	10°183785	9°937887	20 85	10°062113	10°121672	20 36	9°878328	20	30	40
30	42	9°8'16288	21 51	10°183712	9°938015	21 89	10°061985	10°121727	21 38	9°878273	18	30	42
56	44	9°8'16361	22 54	10°183639	9°938142	22 94	10°061858	10°121781	22 40	9°878219	16	30	44
30	46	9°8'16434	23 56	10°183566	9°938270	23 98	10°061730	10°121836	23 42	9°878164	14	30	46
57	48	9°8'16507	24 59	10°183493	9°938398	24 102	10°061602	10°121891	24 44	9°878109	12	30	48
30	50	9°8'16579	25 61	10°183421	9°938525	25 106	10°061475	10°121946	25 46	9°878054	10	30	50
58	52	9°8'16652	26 63	10°183348	9°938653	26 111	10°061347	10°122001	26 47	9°877999	8	30	52
30	54	9°8'16725	27 66	10°183275	9°938780	27 115	10°061220	10°122055	27 49	9°877945	6	30	54
59	56	9°8'16798	28 68	10°183202	9°938908	28 119	10°061092	10°122110	28 51	9°877890	4	30	56
30	58	9°8'16870	29 70	10°183130	9°939035	29 123	10°060965	10°122165	29 53	9°877835	2	30	58
60	60	9°8'16943	30 73	10°183057	9°939163	30 128	10°060837	10°122220	30 55	9°877780	0	30	60
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	mm.	°	'

LOG. SINES, COSINES, &c.											
24°						41°					
°	'	mm.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine
0	0		9°816943		10°183057	9°939163		10°060837	10°122220		9°877780
30	1		9°817016	1' 2	10°182984	9°939291	1" 4	10°060709	10°122275	1" 2	9°877725
1	4		9°817088	2 5	10°182912	9°939418	2 8	10°060582	10°122330	2 4	9°877670
30	6		9°817161	3 7	10°182839	9°939546	3 13	10°060454	10°122385	3 5	9°877615
3	8		9°817233	4 10	10°182767	9°939673	4 17	10°060327	10°122440	4 7	9°877560
30	10		9°817306	5 12	10°182694	9°939801	5 21	10°060199	10°122495	5 9	9°877505
3	12		9°817379	6 14	10°182621	9°939928	6 25	10°060072	10°122550	6 11	9°877450
30	14		9°817451	7 17	10°182549	9°940056	7 30	10°059944	10°122605	7 13	9°877395
4	16		9°817524	8 19	10°182476	9°940183	8 34	10°059817	10°122660	8 15	9°877340
30	18		9°817596	9 22	10°182404	9°940311	9 38	10°059689	10°122715	9 16	9°877285
5	20		9°817668	10 24	10°182332	9°940439	10 42	10°059561	10°122770	10 18	9°877230
30	22		9°817741	11 27	10°182259	9°940566	11 47	10°059434	10°122825	11 20	9°877175
6	24		9°817813	12 29	10°182187	9°940694	12 51	10°059306	10°122880	12 22	9°877120
30	26		9°817886	13 32	10°182114	9°940821	13 55	10°059179	10°122935	13 24	9°877065
7	28		9°817958	14 34	10°182042	9°940949	14 59	10°059051	10°122990	14 26	9°877010
30	30		9°818030	15 36	10°181970	9°941076	15 64	10°058924	10°123045	15 27	9°876954
8	32		9°818103	16 39	10°181897	9°941204	16 68	10°058796	10°123101	16 29	9°876899
30	34		9°818175	17 41	10°181825	9°941331	17 72	10°058669	10°123156	17 31	9°876844
9	36		9°818247	18 43	10°181753	9°941459	18 76	10°058541	10°123211	18 33	9°876789
30	38		9°818320	19 46	10°181680	9°941586	19 81	10°058414	10°123266	19 35	9°876734
10	40		9°818392	20 48	10°181608	9°941713	20 85	10°058287	10°123322	20 37	9°876678
30	42		9°818464	21 51	10°181536	9°941841	21 89	10°058159	10°123377	21 38	9°876623
11	44		9°818536	22 53	10°181464	9°941968	22 93	10°058032	10°123432	22 40	9°876568
30	46		9°818609	23 56	10°181391	9°942096	23 98	10°057904	10°123487	23 42	9°876513
12	48		9°818681	24 58	10°181319	9°942223	24 102	10°057777	10°123543	24 44	9°876457
30	50		9°818753	25 61	10°181247	9°942351	25 106	10°057649	10°123598	25 46	9°876402
13	52		9°818825	26 63	10°181175	9°942478	26 110	10°057522	10°123653	26 48	9°876347
30	54		9°818897	27 65	10°181103	9°942606	27 115	10°057394	10°123709	27 49	9°876291
14	56		9°818969	28 68	10°181031	9°942733	28 119	10°057267	10°123764	28 51	9°876236
30	58		9°819041	29 70	10°180959	9°942861	29 123	10°057139	10°123819	29 53	9°876181
15	60		9°819113	30 72	10°180887	9°942988	30 127	10°057012	10°123875	30 55	9°876125
30	2		9°819185	1 2	10°180815	9°943115	1 4	10°056885	10°123930	1 2	9°876070
16	4		9°819257	2 5	10°180743	9°943243	2 8	10°056757	10°123986	2 4	9°876014
30	6		9°819329	3 7	10°180671	9°943370	3 13	10°056630	10°124041	3 6	9°875959
17	8		9°819401	4 10	10°180599	9°943498	4 17	10°056502	10°124096	4 7	9°875904
30	10		9°819473	5 12	10°180527	9°943625	5 21	10°056375	10°124152	5 9	9°875848
18	12		9°819545	6 14	10°180455	9°943752	6 25	10°056248	10°124207	6 11	9°875793
30	14		9°819617	7 17	10°180383	9°943880	7 30	10°056120	10°124263	7 13	9°875737
19	16		9°819689	8 19	10°180311	9°944007	8 34	10°055993	10°124318	8 15	9°875682
30	18		9°819761	9 22	10°180239	9°944135	9 38	10°055865	10°124374	9 17	9°875626
20	20		9°819832	10 24	10°180168	9°944262	10 42	10°055738	10°124429	10 19	9°875571
30	22		9°819904	11 26	10°180096	9°944389	11 47	10°055611	10°124485	11 20	9°875515
21	24		9°819976	12 29	10°180024	9°944517	12 51	10°055483	10°124541	12 22	9°875459
30	26		9°820048	13 31	10°179952	9°944644	13 55	10°055356	10°124596	13 24	9°875404
22	28		9°820120	14 34	10°179880	9°944771	14 59	10°055229	10°124652	14 26	9°875348
30	30		9°820191	15 36	10°179809	9°944899	15 64	10°055101	10°124707	15 28	9°875293
23	32		9°820263	16 38	10°179737	9°945026	16 68	10°054974	10°124763	16 30	9°875237
30	34		9°820335	17 41	10°179665	9°945153	17 72	10°054847	10°124819	17 31	9°875181
24	36		9°820406	18 43	10°179594	9°945281	18 76	10°054719	10°124874	18 33	9°875126
30	38		9°820478	19 46	10°179522	9°945408	19 81	10°054592	10°124930	19 35	9°875070
25	40		9°820550	20 48	10°179450	9°945535	20 85	10°054465	10°124986	20 37	9°875014
30	42		9°820621	21 50	10°179379	9°945663	21 89	10°054337	10°125042	21 39	9°874958
26	44		9°820693	22 53	10°179307	9°945790	22 93	10°054210	10°125097	22 41	9°874903
30	46		9°820764	23 55	10°179236	9°945917	23 98	10°054083	10°125153	23 43	9°874847
27	48		9°820836	24 57	10°179164	9°946045	24 102	10°053955	10°125209	24 45	9°874791
30	50		9°820907	25 60	10°179093	9°946172	25 106	10°053828	10°125265	25 46	9°874735
28	52		9°820979	26 62	10°179021	9°946300	26 110	10°053701	10°125320	26 48	9°874679
30	54		9°821050	27 65	10°178950	9°946427	27 115	10°053573	10°125376	27 50	9°874624
29	56		9°821122	28 67	10°178878	9°946554	28 119	10°053446	10°125432	28 52	9°874568
30	58		9°821193	29 69	10°178807	9°946681	29 123	10°053319	10°125488	29 54	9°874512
30	60		9°821265	30 72	10°178735	9°946808	30 127	10°053192	10°125544	30 56	9°874456
°	'	mm.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine

LOG. SINES, COSINES, &c.

48°				41°				
°	'	m.	Parts	°	'	m.	Parts	
Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	
Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	
30	0	9'8211265	10'178735	9'946808	10'053192	10'125544	9'874456	30
30	2	9'821336	10'178664	9'946936	10'053064	10'125600	9'874400	30
31	4	9'821407	10'178593	9'947063	10'052937	10'125656	9'874344	30
30	6	9'821479	10'178521	9'947190	10'052810	10'125712	9'874288	30
32	8	9'821550	10'178450	9'947318	10'052682	10'125768	9'874232	30
30	10	9'821621	10'178379	9'947445	10'052555	10'125823	9'874177	30
33	12	9'821693	10'178307	9'947572	10'052428	10'125879	9'874121	30
30	14	9'821764	10'178236	9'947699	10'052301	10'125935	9'874065	30
34	16	9'821835	10'178165	9'947827	10'052173	10'125991	9'874009	30
30	18	9'821906	10'178094	9'947954	10'052046	10'126047	9'873953	30
35	20	9'821977	10'178023	9'948081	10'051919	10'126104	9'873896	30
30	22	9'822049	10'177951	9'948208	10'051792	10'126160	9'873840	30
36	24	9'822120	10'177880	9'948335	10'051665	10'126216	9'873784	30
30	26	9'822191	10'177809	9'948463	10'051537	10'126272	9'873728	30
37	28	9'822262	10'177738	9'948590	10'051410	10'126328	9'873672	30
30	30	9'822333	10'177667	9'948717	10'051283	10'126384	9'873616	30
38	32	9'822404	10'177596	9'948844	10'051156	10'126440	9'873560	30
30	34	9'822475	10'177525	9'948972	10'051028	10'126496	9'873504	30
39	36	9'822546	10'177454	9'949099	10'050901	10'126552	9'873448	30
30	38	9'822617	10'177383	9'949226	10'050774	10'126609	9'873392	30
40	40	9'822688	10'177312	9'949353	10'050647	10'126665	9'873336	30
30	42	9'822759	10'177241	9'949480	10'050520	10'126721	9'873280	30
41	44	9'822830	10'177170	9'949608	10'050392	10'126777	9'873224	30
30	46	9'822901	10'177099	9'949735	10'050265	10'126833	9'873168	30
42	48	9'822972	10'177028	9'949862	10'050138	10'126889	9'873112	30
30	50	9'823043	10'176957	9'949989	10'050011	10'126946	9'873056	30
43	52	9'823114	10'176886	9'950116	10'049884	10'127002	9'872999	30
30	54	9'823185	10'176815	9'950243	10'049757	10'127059	9'872943	30
44	56	9'823255	10'176745	9'950371	10'049629	10'127115	9'872887	30
30	58	9'823326	10'176674	9'950498	10'049502	10'127171	9'872831	30
45	60	9'823397	10'176603	9'950625	10'049375	10'127228	9'872775	30
30	2	9'823468	10'176532	9'950752	10'049248	10'127284	9'872719	30
46	4	9'823539	10'176461	9'950879	10'049121	10'127341	9'872663	30
30	6	9'823609	10'176391	9'951006	10'048994	10'127397	9'872607	30
47	8	9'823680	10'176320	9'951133	10'048867	10'127453	9'872551	30
30	10	9'823751	10'176249	9'951261	10'048739	10'127510	9'872495	30
48	12	9'823822	10'176178	9'951388	10'048612	10'127566	9'872439	30
30	14	9'823892	10'176107	9'951515	10'048485	10'127623	9'872383	30
49	16	9'823963	10'176037	9'951642	10'048358	10'127679	9'872327	30
30	18	9'824033	10'175966	9'951769	10'048231	10'127736	9'872271	30
50	20	9'824104	10'175896	9'951896	10'048104	10'127792	9'872215	30
30	22	9'824174	10'175826	9'952023	10'047977	10'127849	9'872159	30
51	24	9'824245	10'175755	9'952150	10'047850	10'127905	9'872103	30
30	26	9'824315	10'175685	9'952277	10'047723	10'127962	9'872047	30
52	28	9'824386	10'175614	9'952405	10'047595	10'128019	9'871991	30
30	30	9'824456	10'175544	9'952532	10'047468	10'128075	9'871935	30
53	32	9'824527	10'175473	9'952659	10'047341	10'128132	9'871879	30
30	34	9'824597	10'175403	9'952786	10'047214	10'128189	9'871823	30
54	36	9'824668	10'175332	9'952913	10'047087	10'128245	9'871767	30
30	38	9'824738	10'175262	9'953040	10'046960	10'128302	9'871711	30
55	40	9'824808	10'175192	9'953167	10'046833	10'128359	9'871655	30
30	42	9'824879	10'175121	9'953294	10'046706	10'128415	9'871599	30
56	44	9'824949	10'175051	9'953421	10'046579	10'128472	9'871543	30
30	46	9'825019	10'174981	9'953548	10'046452	10'128529	9'871487	30
57	48	9'825090	10'174910	9'953675	10'046325	10'128586	9'871431	30
30	50	9'825160	10'174840	9'953802	10'046198	10'128642	9'871375	30
58	52	9'825230	10'174770	9'953929	10'046071	10'128699	9'871319	30
30	54	9'825300	10'174700	9'954056	10'045944	10'128756	9'871263	30
59	56	9'825371	10'174629	9'954183	10'045817	10'128813	9'871207	30
30	58	9'825441	10'174559	9'954310	10'045690	10'128870	9'871151	30
60	60	9'825511	10'174489	9'954437	10'045563	10'128927	9'871095	30
°	'	m.	Parts	°	'	m.	Parts	
Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	

48°

3° 12'

LOG. SINES, COSINES, &c.													
24 48"							42°						
°	'	''	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	''	°
0	0	0	9°825511		10°174489	9°954437		10°045563	10°128927		9°871073	1.2	60
30	2	0	9°825581	1° 2	10°174419	9°954564	1° 4	10°045436	10°128983	1° 2	9°871017	50	30
1	4	0	9°825651	2 5	10°174349	9°954691	2 8	10°045309	10°129040	2 4	9°870960	56	59
30	6	0	9°825721	3 7	10°174279	9°954819	3 13	10°045181	10°129097	3 6	9°870903	51	30
1	8	0	9°825791	4 9	10°174209	9°954946	4 17	10°045054	10°129154	4 8	9°870846	52	58
30	10	0	9°825861	5 12	10°174139	9°955073	5 21	10°044927	10°129211	5 10	9°870789	54	30
3	12	0	9°825931	6 14	10°174069	9°955200	6 25	10°044800	10°129268	6 11	9°870732	46	67
30	14	0	9°826001	7 16	10°173999	9°955327	7 30	10°044673	10°129325	7 13	9°870675	46	30
4	16	0	9°826071	8 19	10°173929	9°955454	8 34	10°044546	10°129382	8 15	9°870618	44	56
30	18	0	9°826141	9 21	10°173859	9°955581	9 38	10°044419	10°129439	9 17	9°870561	42	30
5	20	0	9°826211	10 23	10°173789	9°955708	10 42	10°044292	10°129496	10 19	9°870504	40	55
30	22	0	9°826281	11 26	10°173719	9°955835	11 47	10°044165	10°129553	11 21	9°870447	38	30
6	24	0	9°826351	12 28	10°173649	9°955961	12 51	10°044039	10°129610	12 23	9°870390	30	54
30	26	0	9°826421	13 30	10°173579	9°956088	13 55	10°043912	10°129667	13 25	9°870333	31	30
7	28	0	9°826491	14 33	10°173509	9°956215	14 59	10°043785	10°129724	14 27	9°870276	32	53
30	30	0	9°826561	15 35	10°173439	9°956342	15 63	10°043658	10°129782	15 29	9°870218	30	30
8	32	0	9°826631	16 37	10°173369	9°956469	16 68	10°043531	10°129839	16 30	9°870161	28	52
30	34	0	9°826701	17 40	10°173299	9°956596	17 72	10°043404	10°129896	17 32	9°870104	26	30
9	36	0	9°826771	18 42	10°173230	9°956723	18 76	10°043277	10°129953	18 34	9°870047	24	51
30	38	0	9°826841	19 44	10°173160	9°956850	19 80	10°043150	10°130010	19 36	9°869990	22	30
10	40	0	9°826911	20 47	10°173090	9°956977	20 85	10°043023	10°130067	20 38	9°869933	20	50
30	42	0	9°826981	21 49	10°173020	9°957104	21 89	10°042896	10°130125	21 40	9°869875	18	30
11	44	0	9°827049	22 51	10°172951	9°957231	22 93	10°042769	10°130182	22 42	9°869818	16	49
30	46	0	9°827119	23 54	10°172881	9°957358	23 97	10°042642	10°130239	23 44	9°869761	14	30
12	48	0	9°827189	24 56	10°172811	9°957485	24 102	10°042515	10°130296	24 46	9°869704	12	48
30	50	0	9°827258	25 58	10°172742	9°957612	25 106	10°042388	10°130354	25 48	9°869646	10	30
13	52	0	9°827328	26 61	10°172672	9°957739	26 110	10°042261	10°130411	26 49	9°869589	8	47
30	54	0	9°827398	27 63	10°172602	9°957866	27 114	10°042134	10°130468	27 51	9°869532	6	30
14	56	0	9°827467	28 65	10°172533	9°957993	28 118	10°042007	10°130526	28 53	9°869474	4	46
30	58	0	9°827537	29 68	10°172463	9°958120	29 123	10°041880	10°130583	29 55	9°869417	2	30
15	60	0	9°827606	30 70	10°172394	9°958247	30 127	10°041753	10°130640	30 57	9°869360	1.2	45
30	2	0	9°827676	1 2	10°172324	9°958373	1 4	10°041627	10°130698	1 2	9°869302	58	30
16	4	0	9°827745	2 5	10°172255	9°958500	2 8	10°041500	10°130755	2 4	9°869245	56	44
30	6	0	9°827815	3 7	10°172185	9°958627	3 13	10°041373	10°130812	3 6	9°869188	54	30
17	8	0	9°827884	4 9	10°172116	9°958754	4 17	10°041246	10°130870	4 8	9°869130	52	43
30	10	0	9°827954	5 12	10°172046	9°958881	5 21	10°041119	10°130927	5 10	9°869073	50	30
18	12	0	9°828023	6 14	10°171977	9°959008	6 25	10°040992	10°130985	6 12	9°869015	48	42
30	14	0	9°828093	7 16	10°171907	9°959135	7 30	10°040865	10°131042	7 13	9°868958	46	30
19	16	0	9°828162	8 19	10°171838	9°959262	8 34	10°040738	10°131100	8 15	9°868900	44	41
30	18	0	9°828231	9 21	10°171769	9°959389	9 38	10°040611	10°131157	9 17	9°868843	42	30
20	20	0	9°828301	10 23	10°171699	9°959516	10 42	10°040484	10°131215	10 19	9°868785	40	40
30	22	0	9°828370	11 26	10°171630	9°959642	11 47	10°040358	10°131272	11 21	9°868728	38	30
21	24	0	9°828439	12 28	10°171561	9°959769	12 51	10°040231	10°131330	12 23	9°868670	36	30
30	26	0	9°828509	13 30	10°171491	9°959896	13 55	10°040104	10°131388	13 25	9°868612	34	30
22	28	0	9°828578	14 33	10°171422	9°960023	14 59	10°039977	10°131445	14 27	9°868555	32	38
30	30	0	9°828647	15 35	10°171353	9°960150	15 63	10°039850	10°131503	15 29	9°868497	30	30
23	32	0	9°828716	16 37	10°171284	9°960277	16 68	10°039723	10°131560	16 31	9°868440	28	37
30	34	0	9°828786	17 40	10°171214	9°960404	17 72	10°039596	10°131618	17 32	9°868382	26	30
24	36	0	9°828855	18 42	10°171145	9°960530	18 76	10°039470	10°131676	18 35	9°868324	24	36
30	38	0	9°828924	19 44	10°171076	9°960657	19 80	10°039343	10°131733	19 36	9°868267	22	30
25	40	0	9°828993	20 46	10°171007	9°960784	20 85	10°039216	10°131791	20 38	9°868209	20	35
30	42	0	9°829062	21 49	10°170938	9°960911	21 89	10°039089	10°131849	21 40	9°868151	18	30
26	44	0	9°829131	22 51	10°170869	9°961038	22 93	10°038962	10°131907	22 42	9°868093	16	34
30	46	0	9°829200	23 54	10°170800	9°961165	23 97	10°038835	10°131964	23 44	9°868036	14	30
27	48	0	9°829269	24 56	10°170731	9°961292	24 102	10°038708	10°132022	24 46	9°867978	12	33
30	50	0	9°829338	25 58	10°170662	9°961418	25 106	10°038582	10°132080	25 48	9°867920	10	30
28	52	0	9°829407	26 60	10°170593	9°961545	26 110	10°038455	10°132138	26 50	9°867862	8	32
30	54	0	9°829476	27 62	10°170524	9°961672	27 114	10°038328	10°132196	27 52	9°867804	6	30
29	56	0	9°829545	28 65	10°170455	9°961799	28 118	10°038201	10°132253	28 54	9°867747	4	31
30	58	0	9°829614	29 67	10°170386	9°961926	29 123	10°038074	10°132311	29 56	9°867689	2	30
30	60	0	9°829683	30 69	10°170317	9°962052	30 127	10°037948	10°132369	30 58	9°867631	0	30
°	'	''	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	''	°

LOG. SINES, COSINES, &c.

2 ^h 50 ^m		42°											
//	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	//	
30	0	9°829683		10°170317	9°902052		10°037948	10°132369		9°867631	10	30	
30	2	9°829752	1° 2	10°170248	9°902179	1° 4	10°037821	10°132427	1° 2	9°867573	98	30	
31	4	9°829821	2 5	10°170179	9°902306	2 8	10°037694	10°132485	2 4	9°867515	96	29	
30	6	9°829890	3 7	10°170110	9°902433	3 13	10°037567	10°132543	3 6	9°867457	94	30	
32	8	9°829959	4 9	10°170041	9°902560	4 17	10°037440	10°132601	4 8	9°867399	92	28	
30	10	9°830028	5 12	10°169972	9°902686	5 21	10°037314	10°132659	5 10	9°867341	90	30	
33	12	9°830097	6 14	10°169903	9°902813	6 25	10°037187	10°132717	6 12	9°867283	88	27	
30	14	9°830165	7 16	10°169835	9°902940	7 30	10°037060	10°132775	7 14	9°867225	86	30	
34	16	9°830234	8 19	10°169766	9°903067	8 34	10°036933	10°132833	8 15	9°867167	84	26	
30	18	9°830303	9 21	10°169697	9°903194	9 38	10°036806	10°132891	9 17	9°867109	82	30	
35	20	9°830372	10 23	10°169628	9°903320	10 42	10°036680	10°132949	10 19	9°867051	80	26	
30	22	9°830440	11 25	10°169560	9°903447	11 46	10°036553	10°133007	11 21	9°866993	78	30	
36	24	9°830509	12 27	10°169491	9°903574	12 51	10°036426	10°133065	12 23	9°866935	76	24	
30	26	9°830578	13 30	10°169422	9°903701	13 55	10°036299	10°133123	13 25	9°866877	74	30	
37	28	9°830646	14 32	10°169354	9°903828	14 59	10°036172	10°133181	14 27	9°866819	72	23	
30	30	9°830715	15 34	10°169285	9°903954	15 63	10°036046	10°133239	15 29	9°866761	70	30	
38	32	9°830784	16 36	10°169216	9°904081	16 68	10°035919	10°133297	16 31	9°866703	68	22	
30	34	9°830852	17 39	10°169148	9°904208	17 72	10°035792	10°133355	17 33	9°866645	66	30	
39	36	9°830921	18 41	10°169079	9°904335	18 76	10°035665	10°133414	18 35	9°866586	64	21	
30	38	9°830989	19 43	10°169011	9°904461	19 80	10°035539	10°133472	19 37	9°866528	62	30	
40	40	9°831058	20 46	10°168942	9°904588	20 84	10°035412	10°133530	20 39	9°866470	60	20	
30	42	9°831127	21 48	10°168873	9°904715	21 89	10°035285	10°133588	21 41	9°866412	58	30	
41	44	9°831195	22 50	10°168805	9°904842	22 93	10°035158	10°133647	22 43	9°866353	56	19	
30	46	9°831263	23 52	10°168736	9°904968	23 97	10°035032	10°133705	23 44	9°866295	54	30	
42	48	9°831332	24 55	10°168668	9°905095	24 101	10°034905	10°133763	24 46	9°866237	52	18	
30	50	9°831400	25 57	10°168600	9°905222	25 105	10°034778	10°133821	25 48	9°866179	50	30	
43	52	9°831469	26 59	10°168531	9°905349	26 110	10°034651	10°133880	26 50	9°866120	48	17	
30	54	9°831537	27 62	10°168463	9°905475	27 114	10°034525	10°133938	27 52	9°866062	46	30	
44	56	9°831606	28 64	10°168394	9°905602	28 118	10°034398	10°133996	28 54	9°866004	44	16	
30	58	9°831674	29 66	10°168326	9°905729	29 122	10°034271	10°134055	29 56	9°865945	42	30	
45	51	9°831742	30 69	10°168258	9°905855	30 127	10°034145	10°134113	30 58	9°865887	2	15	
30	2	9°831811	1 2	10°168189	9°905982	1 4	10°034018	10°134172	1 2	9°865828	58	30	
46	4	9°831879	2 5	10°168121	9°906109	2 8	10°033891	10°134230	2 4	9°865770	56	14	
30	6	9°831947	3 7	10°168053	9°906236	3 13	10°033764	10°134288	3 6	9°865712	54	30	
47	8	9°832015	4 9	10°167985	9°906362	4 17	10°033638	10°134347	4 8	9°865653	52	13	
30	10	9°832084	5 12	10°167916	9°906489	5 21	10°033511	10°134405	5 10	9°865595	50	30	
48	12	9°832152	6 14	10°167848	9°906616	6 25	10°033384	10°134464	6 12	9°865536	48	12	
30	14	9°832220	7 16	10°167780	9°906742	7 30	10°033258	10°134522	7 14	9°865478	46	30	
49	16	9°832288	8 19	10°167712	9°906869	8 34	10°033131	10°134581	8 16	9°865419	44	11	
30	18	9°832356	9 21	10°167643	9°906996	9 38	10°033004	10°134639	9 18	9°865361	42	30	
50	20	9°832424	10 23	10°167575	9°907123	10 42	10°032877	10°134698	10 20	9°865302	40	10	
30	22	9°832493	11 25	10°167507	9°907249	11 46	10°032751	10°134756	11 21	9°865244	38	30	
51	24	9°832561	12 27	10°167439	9°907376	12 51	10°032624	10°134815	12 23	9°865185	36	9	
30	26	9°832629	13 30	10°167371	9°907503	13 55	10°032497	10°134874	13 25	9°865126	34	30	
52	28	9°832697	14 32	10°167303	9°907629	14 59	10°032371	10°134932	14 27	9°865068	32	8	
30	30	9°832765	15 34	10°167235	9°907756	15 63	10°032244	10°134991	15 29	9°865009	30	30	
53	32	9°832833	16 36	10°167167	9°907883	16 68	10°032117	10°135050	16 31	9°864950	28	7	
30	34	9°832901	17 39	10°167099	9°908009	17 72	10°031991	10°135108	17 33	9°864892	26	30	
54	36	9°832969	18 41	10°167031	9°908136	18 76	10°031864	10°135167	18 35	9°864833	24	6	
30	38	9°833037	19 43	10°166963	9°908263	19 80	10°031737	10°135226	19 37	9°864774	22	30	
55	40	9°833105	20 45	10°166895	9°908389	20 84	10°031611	10°135284	20 39	9°864716	20	5	
30	42	9°833173	21 48	10°166827	9°908516	21 89	10°031484	10°135343	21 41	9°864657	18	30	
56	44	9°833241	22 50	10°166759	9°908643	22 93	10°031357	10°135402	22 43	9°864598	16	4	
30	46	9°833309	23 52	10°166691	9°908769	23 97	10°031231	10°135461	23 45	9°864539	14	30	
57	48	9°833377	24 55	10°166623	9°908896	24 101	10°031104	10°135519	24 47	9°864481	12	3	
30	50	9°833444	25 57	10°166556	9°909023	25 106	10°030977	10°135578	25 49	9°864422	10	30	
58	52	9°833512	26 59	10°166488	9°909149	26 110	10°030851	10°135637	26 51	9°864363	8	2	
30	54	9°833580	27 61	10°166420	9°909276	27 114	10°030724	10°135696	27 53	9°864304	6	30	
59	56	9°833648	28 64	10°166352	9°909403	28 118	10°030597	10°135755	28 55	9°864245	4	1	
30	58	9°833716	29 66	10°166284	9°909529	29 122	10°030471	10°135814	29 57	9°864186	2	30	
60	51	9°833783	30 68	10°166217	9°909656	30 127	10°030344	10°135873	30 59	9°864127	0	0	
//	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	//	

LOG. SINES, COSINES, &c.											
2° 52'						43°					
'''	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m. '''
0	0	9°833783		10°166217	9°969656		10°030344	10°135873		9°864127	0 68
1	2	9°833851	1 2	10°166149	9°969783	1 4	10°030217	10°135931	1 2	9°864069	20 30
30	4	9°833919	3 4	10°166081	9°969909	3 8	10°030091	10°135990	3 4	9°864010	50 50
30	6	9°833986	5 7	10°166014	9°970036	5 13	10°029964	10°136049	5 6	9°863951	51 30
2	8	9°834054	8 9	10°165946	9°970162	8 17	10°029838	10°136108	8 8	9°863892	52 58
30	10	9°834122	10 11	10°165878	9°970289	10 21	10°029711	10°136167	10 10	9°863833	53 50
3	12	9°834189	12 13	10°165811	9°970416	12 25	10°029584	10°136226	12 12	9°863774	54 57
30	14	9°834257	14 16	10°165743	9°970542	14 30	10°029458	10°136285	14 14	9°863715	55 30
4	16	9°834325	16 18	10°165675	9°970669	16 34	10°029331	10°136344	16 16	9°863656	56 30
30	18	9°834392	18 20	10°165608	9°970796	18 38	10°029204	10°136403	18 18	9°863597	57 30
5	20	9°834460	20 22	10°165540	9°970922	20 42	10°029078	10°136462	20 20	9°863538	58 55
30	22	9°834527	22 25	10°165473	9°971049	22 46	10°028951	10°136522	22 22	9°863478	59 30
0	24	9°834595	24 27	10°165405	9°971175	24 51	10°028825	10°136581	24 24	9°863419	59 54
30	26	9°834662	26 29	10°165338	9°971302	26 55	10°028698	10°136640	26 26	9°863360	30 30
7	28	9°834730	28 31	10°165270	9°971429	28 59	10°028571	10°136699	28 28	9°863301	32 53
30	30	9°834797	30 34	10°165203	9°971555	30 63	10°028445	10°136758	30 30	9°863242	33 30
8	32	9°834865	32 36	10°165135	9°971682	32 68	10°028318	10°136817	32 32	9°863183	34 52
30	34	9°834932	34 38	10°165068	9°971808	34 72	10°028192	10°136876	34 34	9°863124	35 30
9	36	9°834999	36 41	10°165001	9°971935	36 76	10°028065	10°136936	36 36	9°863064	36 51
30	38	9°835067	38 43	10°164933	9°972062	38 80	10°027938	10°136995	38 38	9°863005	37 30
10	40	9°835134	40 45	10°164866	9°972188	40 84	10°027812	10°137054	40 40	9°862946	38 50
30	42	9°835201	42 47	10°164799	9°972315	42 89	10°027685	10°137113	42 42	9°862887	39 30
11	44	9°835269	44 49	10°164731	9°972441	44 93	10°027559	10°137173	44 44	9°862827	40 49
30	46	9°835336	46 51	10°164664	9°972568	46 97	10°027432	10°137232	46 46	9°862768	41 30
12	48	9°835403	48 54	10°164597	9°972695	48 101	10°027305	10°137291	48 48	9°862709	42 48
30	50	9°835471	50 56	10°164529	9°972821	50 105	10°027179	10°137350	50 50	9°862650	43 30
13	52	9°835538	52 58	10°164462	9°972948	52 110	10°027052	10°137410	52 52	9°862590	44 47
30	54	9°835605	54 61	10°164395	9°973074	54 114	10°026926	10°137469	54 54	9°862531	45 30
14	56	9°835672	56 63	10°164328	9°973201	56 118	10°026799	10°137529	56 56	9°862472	46 46
30	58	9°835739	58 65	10°164261	9°973327	58 122	10°026673	10°137588	58 58	9°862412	47 30
15	60	9°835807	60 68	10°164193	9°973454	60 126	10°026546	10°137647	60 59	9°862353	48 45
30	62	9°835874	62 70	10°164126	9°973581	62 130	10°026419	10°137707	62 62	9°862293	49 30
16	64	9°835941	64 72	10°164059	9°973707	64 134	10°026293	10°137766	64 64	9°862234	50 44
30	66	9°836008	66 74	10°163992	9°973834	66 138	10°026166	10°137826	66 66	9°862175	51 30
17	68	9°836075	68 76	10°163925	9°973960	68 142	10°026040	10°137885	68 68	9°862115	52 43
30	70	9°836142	70 78	10°163858	9°974087	70 146	10°025913	10°137945	70 70	9°862055	53 30
18	72	9°836209	72 80	10°163791	9°974213	72 150	10°025787	10°138004	72 72	9°861996	54 42
30	74	9°836276	74 82	10°163724	9°974340	74 154	10°025660	10°138064	74 74	9°861936	55 30
19	76	9°836343	76 84	10°163657	9°974466	76 158	10°025534	10°138123	76 76	9°861877	56 41
30	78	9°836410	78 86	10°163590	9°974593	78 162	10°025407	10°138183	78 78	9°861817	57 30
20	80	9°836477	80 88	10°163523	9°974720	80 166	10°025280	10°138242	80 80	9°861758	58 40
30	82	9°836544	82 90	10°163456	9°974846	82 170	10°025154	10°138302	82 82	9°861698	59 30
21	84	9°836611	84 92	10°163389	9°974973	84 174	10°025027	10°138362	84 84	9°861638	60 39
30	86	9°836678	86 94	10°163322	9°975099	86 178	10°024901	10°138421	86 86	9°861579	61 30
22	88	9°836745	88 96	10°163255	9°975226	88 182	10°024774	10°138481	88 88	9°861519	62 38
30	90	9°836812	90 98	10°163188	9°975352	90 186	10°024648	10°138541	90 90	9°861459	63 30
23	92	9°836878	92 100	10°163122	9°975479	92 190	10°024521	10°138600	92 92	9°861399	64 37
30	94	9°836945	94 102	10°163055	9°975605	94 194	10°024395	10°138660	94 94	9°861339	65 30
24	96	9°837012	96 104	10°162988	9°975732	96 198	10°024268	10°138720	96 96	9°861279	66 36
30	98	9°837079	98 106	10°162921	9°975858	98 202	10°024142	10°138779	98 98	9°861219	67 35
25	100	9°837146	100 108	10°162854	9°975985	100 206	10°024015	10°138839	100 100	9°861159	68 35
30	102	9°837212	102 110	10°162788	9°976111	102 210	10°023889	10°138899	102 102	9°861099	69 30
26	104	9°837279	104 112	10°162721	9°976238	104 214	10°023762	10°138959	104 104	9°861039	70 34
30	106	9°837346	106 114	10°162654	9°976364	106 218	10°023636	10°139019	106 106	9°860979	71 30
27	108	9°837412	108 116	10°162588	9°976491	108 222	10°023509	10°139078	108 108	9°860919	72 33
30	110	9°837479	110 118	10°162521	9°976617	110 226	10°023383	10°139138	110 110	9°860859	73 30
28	112	9°837546	112 120	10°162454	9°976744	112 230	10°023256	10°139198	112 112	9°860799	74 32
30	114	9°837612	114 122	10°162388	9°976870	114 234	10°023130	10°139258	114 114	9°860739	75 30
29	116	9°837679	116 124	10°162321	9°976997	116 238	10°023003	10°139318	116 116	9°860679	76 31
30	118	9°837746	118 126	10°162254	9°977123	118 242	10°022877	10°139378	118 118	9°860619	77 30
30	120	9°837812	120 128	10°162188	9°977250	120 246	10°022750	10°139438	120 120	9°860559	78 30
'''	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m. '''

LOG. SINES, COSINES, &c.

2 ^h 54 ^m		43°										44°	
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	°	'
30	0	9°837812		10°162188	9°977250		10°022750	10°139438		9°860562	6	30	0
30	2	9°837879	1" 2	10°162121	9°977377	1" 4	10°022623	10°139498	1" 2	9°860502	38	30	2
31	4	9°837945	2 4	10°162055	9°977503	2 8	10°022497	10°139558	2 4	9°860442	56	29	4
30	6	9°838012	3 7	10°161988	9°977630	3 13	10°022370	10°139618	3 6	9°860382	34	30	6
32	8	9°838078	4 9	10°161922	9°977756	4 17	10°022244	10°139678	4 8	9°860322	52	28	8
30	10	9°838145	5 11	10°161855	9°977882	5 21	10°022118	10°139738	5 10	9°860262	50	30	10
33	12	9°838211	6 13	10°161789	9°978009	6 25	10°021991	10°139798	6 12	9°860202	48	27	12
30	14	9°838278	7 15	10°161722	9°978135	7 30	10°021865	10°139858	7 14	9°860142	46	30	14
34	16	9°838344	8 17	10°161656	9°978262	8 34	10°021738	10°139918	8 16	9°860082	44	26	16
30	18	9°838410	9 20	10°161590	9°978388	9 38	10°021612	10°139978	9 18	9°860022	42	30	18
35	20	9°838477	10 22	10°161523	9°978515	10 42	10°021485	10°140038	10 20	9°859962	40	25	20
30	22	9°838543	11 24	10°161457	9°978641	11 46	10°021359	10°140098	11 22	9°859902	38	30	22
36	24	9°838610	12 27	10°161390	9°978768	12 51	10°021232	10°140158	12 24	9°859842	36	24	24
30	26	9°838676	13 29	10°161324	9°978894	13 55	10°021106	10°140219	13 26	9°859781	34	30	26
37	28	9°838742	14 31	10°161258	9°979021	14 59	10°020979	10°140279	14 28	9°859721	32	23	28
30	30	9°838808	15 33	10°161192	9°979147	15 63	10°020853	10°140339	15 30	9°859661	30	30	30
38	32	9°838875	16 35	10°161125	9°979274	16 67	10°020726	10°140399	16 32	9°859601	28	22	32
30	34	9°838941	17 37	10°161059	9°979400	17 72	10°020600	10°140459	17 34	9°859541	26	30	34
39	36	9°839007	18 40	10°160993	9°979527	18 76	10°020473	10°140520	18 36	9°859480	24	21	36
30	38	9°839073	19 42	10°160927	9°979653	19 80	10°020347	10°140580	19 38	9°859420	22	30	38
40	40	9°839140	20 44	10°160860	9°979780	20 84	10°020220	10°140640	20 40	9°859360	20	20	40
30	42	9°839206	21 46	10°160794	9°979906	21 89	10°020094	10°140700	21 42	9°859300	19	30	42
41	44	9°839272	22 48	10°160728	9°980033	22 93	10°019967	10°140761	22 44	9°859239	17	19	44
30	46	9°839338	23 51	10°160662	9°980159	23 97	10°019841	10°140821	23 46	9°859179	16	30	46
42	48	9°839404	24 53	10°160596	9°980286	24 101	10°019714	10°140881	24 48	9°859119	14	18	48
30	50	9°839470	25 55	10°160530	9°980412	25 105	10°019588	10°140942	25 50	9°859058	10	30	50
43	52	9°839536	26 57	10°160464	9°980538	26 110	10°019462	10°141002	26 52	9°858998	8	17	52
30	54	9°839602	27 60	10°160398	9°980665	27 114	10°019335	10°141063	27 54	9°858937	6	30	54
44	56	9°839668	28 62	10°160332	9°980791	28 118	10°019209	10°141123	28 56	9°858877	4	16	56
30	58	9°839734	29 64	10°160266	9°980918	29 122	10°019082	10°141183	29 58	9°858817	2	30	58
45	58	9°839800	30 66	10°160200	9°981044	30 126	10°018956	10°141244	30 60	9°858756	5	15	58
30	2	9°839866	1 2	10°160134	9°981171	1 4	10°018829	10°141304	1 2	9°858696	56	30	2
46	4	9°839932	2 4	10°160068	9°981297	2 8	10°018703	10°141365	2 4	9°858635	54	14	4
30	6	9°839998	3 7	10°160002	9°981424	3 13	10°018576	10°141425	3 6	9°858575	52	30	6
47	8	9°840064	4 9	10°159936	9°981550	4 17	10°018450	10°141486	4 8	9°858514	50	13	8
30	10	9°840130	5 11	10°159870	9°981677	5 21	10°018323	10°141546	5 10	9°858454	50	30	10
48	12	9°840196	6 13	10°159804	9°981803	6 25	10°018197	10°141607	6 12	9°858393	48	12	12
30	14	9°840262	7 15	10°159738	9°981929	7 29	10°018071	10°141668	7 14	9°858332	46	30	14
49	16	9°840328	8 17	10°159672	9°982056	8 34	10°017944	10°141728	8 16	9°858272	44	11	16
30	18	9°840393	9 20	10°159607	9°982182	9 38	10°017818	10°141789	9 18	9°858211	42	30	18
50	20	9°840459	10 22	10°159541	9°982309	10 42	10°017691	10°141849	10 20	9°858151	40	10	20
30	22	9°840525	11 24	10°159475	9°982435	11 46	10°017565	10°141910	11 22	9°858090	38	30	22
51	24	9°840591	12 26	10°159409	9°982562	12 51	10°017438	10°141971	12 24	9°858029	36	9	24
30	26	9°840657	13 29	10°159343	9°982688	13 55	10°017312	10°142032	13 26	9°857968	34	30	26
52	28	9°840722	14 31	10°159278	9°982814	14 59	10°017186	10°142092	14 28	9°857908	32	8	28
30	30	9°840788	15 33	10°159212	9°982941	15 63	10°017059	10°142153	15 30	9°857847	30	30	30
53	32	9°840854	16 35	10°159146	9°983067	16 67	10°016933	10°142214	16 32	9°857786	28	7	32
30	34	9°840919	17 37	10°159081	9°983194	17 72	10°016806	10°142274	17 34	9°857726	26	30	34
54	36	9°840985	18 39	10°159015	9°983320	18 76	10°016680	10°142335	18 36	9°857665	24	6	36
30	38	9°841051	19 42	10°158949	9°983447	19 80	10°016553	10°142396	19 38	9°857604	22	30	38
55	40	9°841116	20 44	10°158884	9°983573	20 84	10°016427	10°142457	20 40	9°857543	20	5	40
30	42	9°841182	21 46	10°158818	9°983699	21 88	10°016301	10°142518	21 42	9°857482	18	30	42
56	44	9°841247	22 48	10°158753	9°983826	22 93	10°016174	10°142578	22 44	9°857422	16	4	44
30	46	9°841313	23 51	10°158687	9°983952	23 97	10°016048	10°142639	23 46	9°857361	14	30	46
57	48	9°841378	24 53	10°158622	9°984079	24 101	10°015921	10°142700	24 48	9°857300	12	3	48
30	50	9°841444	25 55	10°158556	9°984205	25 105	10°015795	10°142761	25 51	9°857239	10	30	50
58	52	9°841509	26 57	10°158491	9°984331	26 109	10°015668	10°142822	26 53	9°857178	8	2	52
30	54	9°841575	27 59	10°158425	9°984458	27 114	10°015542	10°142883	27 55	9°857117	6	30	54
59	56	9°841640	28 61	10°158360	9°984584	28 118	10°015416	10°142944	28 57	9°857056	4	1	56
30	58	9°841706	29 64	10°158294	9°984711	29 122	10°015290	10°143005	29 59	9°856995	2	30	58
60	58	9°841771	30 66	10°158229	9°984837	30 126	10°015163	10°143066	30 61	9°856934	0	0	58
°	'	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	°	'

LOG. SINES, COSINES, &c.

2 ^h 56 ^m			44°												
°	'	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	Parts	°	'		
0	0	9.841771		10.158229	9.984837		10.015163	10.143066		9.856934		60	0		
30	2	9.841837	1" 2	10.158163	9.984904	1" 4	10.015036	10.143127	1" 2	9.856873	1" 2	59	30		
1	4	9.841902	3 4	10.158098	9.985090	2 8	10.014910	10.143188	2 4	9.856812	2 4	58	30		
30	6	9.841967	3 7	10.158033	9.985216	3 13	10.014784	10.143249	3 6	9.856751	3 6	57	30		
2	8	9.842033	4 9	10.157967	9.985343	4 17	10.014657	10.143310	4 8	9.856690	4 8	56	30		
30	10	9.842098	5 11	10.157902	9.985469	5 21	10.014531	10.143371	5 10	9.856629	5 10	55	30		
3	12	9.842163	6 13	10.157837	9.985596	6 25	10.014404	10.143432	6 12	9.856568	6 12	54	30		
30	14	9.842229	7 15	10.157771	9.985722	7 29	10.014278	10.143493	7 14	9.856507	7 14	53	30		
4	16	9.842294	8 17	10.157706	9.985848	8 34	10.014152	10.143554	8 16	9.856446	8 16	52	30		
30	18	9.842359	9 20	10.157641	9.985975	9 38	10.014025	10.143616	9 18	9.856384	9 18	51	30		
5	20	9.842424	10 22	10.157576	9.986101	10 42	10.013899	10.143677	10 20	9.856323	10 20	50	30		
30	22	9.842490	11 24	10.157510	9.986228	11 46	10.013772	10.143738	11 22	9.856262	11 22	49	30		
6	24	9.842555	12 26	10.157445	9.986354	12 51	10.013646	10.143799	12 24	9.856201	12 24	48	30		
30	26	9.842620	13 28	10.157380	9.986480	13 55	10.013520	10.143860	13 27	9.856140	13 27	47	30		
7	28	9.842685	14 30	10.157315	9.986607	14 59	10.013393	10.143922	14 29	9.856078	14 29	46	30		
30	30	9.842750	15 33	10.157250	9.986733	16 63	10.013267	10.143983	15 31	9.856017	15 31	45	30		
8	32	9.842815	16 35	10.157185	9.986860	16 67	10.013140	10.144044	16 33	9.855956	16 33	44	30		
30	34	9.842880	17 37	10.157120	9.986986	17 72	10.013014	10.144106	17 35	9.855895	17 35	43	30		
9	36	9.842946	18 39	10.157054	9.987112	18 76	10.012888	10.144167	18 37	9.855833	18 37	42	30		
30	38	9.843011	19 41	10.156989	9.987239	19 80	10.012761	10.144228	19 39	9.855772	19 39	41	30		
10	40	9.843076	20 43	10.156924	9.987365	20 84	10.012635	10.144289	20 41	9.855711	20 41	40	30		
30	42	9.843141	21 46	10.156859	9.987491	21 88	10.012509	10.144351	21 43	9.855649	21 43	39	30		
11	44	9.843206	22 48	10.156794	9.987618	22 93	10.012382	10.144412	22 45	9.855588	22 45	38	30		
30	46	9.843271	23 50	10.156729	9.987744	23 97	10.012256	10.144474	23 47	9.855526	23 47	37	30		
12	48	9.843336	24 52	10.156664	9.987871	24 101	10.012129	10.144535	24 49	9.855465	24 49	36	30		
30	50	9.843401	25 54	10.156599	9.987997	25 105	10.012003	10.144596	25 51	9.855404	25 51	35	30		
13	52	9.843466	26 56	10.156534	9.988123	26 109	10.011877	10.144658	26 53	9.855342	26 53	34	30		
30	54	9.843530	27 59	10.156470	9.988250	27 114	10.011750	10.144719	27 55	9.855281	27 55	33	30		
14	56	9.843595	28 61	10.156405	9.988376	28 118	10.011624	10.144781	28 57	9.855219	28 57	32	30		
30	58	9.843660	29 63	10.156340	9.988503	29 122	10.011497	10.144842	29 59	9.855158	29 59	31	30		
15	57	9.843725	30 65	10.156275	9.988629	30 126	10.011371	10.144904	30 61	9.855096	30 61	30	30		
30	2	9.843790	1 2	10.156210	9.988755	1 4	10.011245	10.144965	1 2	9.855035	1 2	29	30		
16	4	9.843855	2 4	10.156145	9.988882	2 8	10.011118	10.145027	2 4	9.854973	2 4	28	30		
30	6	9.843919	3 6	10.156081	9.989008	3 13	10.010992	10.145089	3 6	9.854911	3 6	27	30		
17	8	9.843984	4 9	10.156016	9.989134	4 17	10.010866	10.145150	4 8	9.854850	4 8	26	30		
30	10	9.844049	5 11	10.155951	9.989261	5 21	10.010739	10.145212	5 10	9.854788	5 10	25	30		
18	12	9.844114	6 13	10.155886	9.989387	6 25	10.010613	10.145273	6 12	9.854727	6 12	24	30		
30	14	9.844178	7 15	10.155822	9.989513	7 29	10.010487	10.145335	7 14	9.854665	7 14	23	30		
19	16	9.844243	8 17	10.155757	9.989640	8 34	10.010360	10.145397	8 16	9.854603	8 16	22	30		
30	18	9.844308	9 19	10.155692	9.989766	9 38	10.010234	10.145458	9 19	9.854542	9 19	21	30		
20	20	9.844372	10 21	10.155628	9.989893	10 42	10.010107	10.145520	10 21	9.854480	10 21	20	30		
30	22	9.844437	11 24	10.155563	9.990019	11 46	10.009981	10.145582	11 23	9.854418	11 23	19	30		
21	24	9.844502	12 26	10.155498	9.990145	12 51	10.009855	10.145644	12 25	9.854356	12 25	18	30		
30	26	9.844566	13 28	10.155434	9.990272	13 55	10.009728	10.145705	13 27	9.854295	13 27	17	30		
22	28	9.844631	14 30	10.155369	9.990398	14 59	10.009602	10.145767	14 29	9.854233	14 29	16	30		
30	30	9.844696	15 32	10.155304	9.990524	15 63	10.009476	10.145829	15 31	9.854171	15 31	15	30		
23	32	9.844760	16 34	10.155240	9.990651	16 67	10.009349	10.145891	16 33	9.854109	16 33	14	30		
30	34	9.844825	17 37	10.155175	9.990777	17 72	10.009223	10.145953	17 35	9.854047	17 35	13	30		
24	36	9.844889	18 39	10.155111	9.990903	18 76	10.009097	10.146014	18 37	9.853986	18 37	12	30		
30	38	9.844954	19 41	10.155046	9.991030	19 80	10.008970	10.146076	19 39	9.853924	19 39	11	30		
25	40	9.845018	20 43	10.154982	9.991156	20 84	10.008844	10.146138	20 41	9.853862	20 41	10	30		
30	42	9.845083	21 45	10.154917	9.991283	21 88	10.008717	10.146200	21 43	9.853800	21 43	9	30		
26	44	9.845147	22 47	10.154853	9.991409	22 93	10.008591	10.146262	22 45	9.853738	22 45	8	30		
30	46	9.845211	23 49	10.154789	9.991535	23 97	10.008465	10.146324	23 47	9.853676	23 47	7	30		
27	48	9.845276	24 52	10.154724	9.991662	24 101	10.008338	10.146386	24 49	9.853614	24 49	6	30		
30	50	9.845340	25 54	10.154660	9.991788	25 105	10.008212	10.146448	25 51	9.853552	25 51	5	30		
28	52	9.845405	26 56	10.154595	9.991914	26 109	10.008086	10.146510	26 54	9.853490	26 54	4	30		
30	54	9.845469	27 58	10.154531	9.992041	27 114	10.007959	10.146572	27 56	9.853428	27 56	3	30		
29	56	9.845533	28 60	10.154467	9.992167	28 118	10.007833	10.146634	28 58	9.853366	28 58	2	30		
30	58	9.845598	29 62	10.154402	9.992293	29 122	10.007707	10.146696	29 60	9.853304	29 60	1	30		
30	59	9.845662	30 64	10.154338	9.992420	30 126	10.007580	10.146758	30 62	9.853242	30 62	0	30		
°	'	Cosine	Parts	Secant	Cotang.	Tangent	Cosec.	Parts	Sine	Parts	°	'			

45°

3^h 2^m

LOG. SINES, COSINES, &c.

2 1/2 58"				44°				45°				3 1/2 (m)			
"	m.	Sine	Parts	Cosec.	Tangent	Parts	Cotang.	Secant	Parts	Cosine	m.	"	m.	"	
30	1	9°84566a		10°154338	9°992420		10°007580	10°146758		9°853242	2	30		30	
30	2	9°845726	1" 2	10°154274	9°992546	1" 4	10°007454	10°146820	1" 2	9°853180	58	30		30	
31	4	9°845790	2 4	10°154210	9°992672	2 8	10°007328	10°146882	2 4	9°853116	56	29		30	
31	6	9°845855	3 6	10°154145	9°992799	3 13	10°007201	10°146944	3 6	9°853056	54	30		30	
32	8	9°845919	4 8	10°154081	9°992925	4 17	10°007075	10°147006	4 8	9°852994	52	28		30	
32	10	9°845983	5 10	10°154017	9°993051	5 21	10°006949	10°147069	5 10	9°852931	50	30		30	
33	12	9°846047	6 13	10°153953	9°993178	6 25	10°006822	10°147131	6 12	9°852869	48	27		30	
33	14	9°846111	7 15	10°153889	9°993304	7 29	10°006696	10°147193	7 15	9°852807	46	30		30	
34	16	9°846175	8 17	10°153825	9°993430	8 34	10°006570	10°147255	8 17	9°852745	44	26		30	
34	18	9°846240	9 19	10°153760	9°993557	9 38	10°006443	10°147317	9 19	9°852683	42	30		30	
35	20	9°846304	10 21	10°153696	9°993683	10 42	10°006317	10°147380	10 21	9°852620	40	25		30	
35	22	9°846368	11 23	10°153632	9°993810	11 46	10°006190	10°147442	11 23	9°852558	38	30		30	
36	24	9°846432	12 26	10°153568	9°993936	12 51	10°006064	10°147504	12 25	9°852496	36	24		30	
36	26	9°846496	13 28	10°153504	9°994062	13 55	10°005938	10°147566	13 27	9°852434	34	30		30	
37	28	9°846560	14 30	10°153440	9°994189	14 59	10°005811	10°147629	14 29	9°852371	32	23		30	
37	30	9°846624	15 32	10°153376	9°994315	15 63	10°005685	10°147691	15 31	9°852309	30	30		30	
38	32	9°846688	16 34	10°153312	9°994441	16 67	10°005559	10°147753	16 33	9°852247	28	22		30	
38	34	9°846752	17 36	10°153248	9°994568	17 72	10°005432	10°147816	17 35	9°852184	26	30		30	
39	36	9°846816	18 38	10°153184	9°994694	18 76	10°005306	10°147878	18 37	9°852122	24	21		30	
39	38	9°846880	19 40	10°153120	9°994820	19 80	10°005180	10°147941	19 40	9°852059	22	30		30	
40	40	9°846944	20 42	10°153056	9°994947	20 84	10°005053	10°148003	20 42	9°851997	20	20		30	
40	42	9°847008	21 45	10°152992	9°995073	21 88	10°004927	10°148066	21 44	9°851934	18	30		30	
41	44	9°847071	22 47	10°152929	9°995199	22 93	10°004801	10°148128	22 46	9°851872	16	19		30	
41	46	9°847135	23 49	10°152865	9°995326	23 97	10°004674	10°148190	23 48	9°851810	14	30		30	
42	48	9°847199	24 51	10°152801	9°995452	24 101	10°004548	10°148253	24 50	9°851747	12	18		30	
42	50	9°847263	25 53	10°152737	9°995579	25 105	10°004422	10°148315	25 52	9°851685	10	30		30	
43	52	9°847327	26 55	10°152673	9°995705	26 109	10°004295	10°148378	26 54	9°851622	8	17		30	
43	54	9°847391	27 58	10°152609	9°995831	27 114	10°004169	10°148441	27 56	9°851559	6	30		30	
44	56	9°847454	28 60	10°152546	9°995957	28 118	10°004043	10°148503	28 58	9°851497	4	16		30	
44	58	9°847518	29 62	10°152482	9°996084	29 122	10°003916	10°148566	29 60	9°851434	2	30		30	
45	59	9°847582	30 64	10°152418	9°996210	30 126	10°003790	10°148628	30 62	9°851372	2	15		30	
45	2	9°847646	1 2	10°152354	9°996336	1 4	10°003664	10°148691	1 2	9°851309	38	30		30	
46	4	9°847709	2 4	10°152291	9°996463	2 8	10°003537	10°148754	2 4	9°851246	36	14		30	
46	6	9°847773	3 6	10°152227	9°996589	3 13	10°003411	10°148816	3 6	9°851184	34	30		30	
47	8	9°847836	4 8	10°152164	9°996715	4 17	10°003285	10°148879	4 8	9°851121	32	13		30	
47	10	9°847900	5 11	10°152100	9°996842	5 21	10°003158	10°148942	5 10	9°851058	30	30		30	
48	12	9°847964	6 13	10°152036	9°996968	6 25	10°003032	10°149004	6 13	9°850996	48	12		30	
48	14	9°848027	7 15	10°151973	9°997094	7 29	10°002906	10°149067	7 15	9°850933	46	30		30	
49	16	9°848091	8 17	10°151909	9°997221	8 34	10°002779	10°149130	8 17	9°850870	44	11		30	
49	18	9°848155	9 19	10°151845	9°997347	9 38	10°002653	10°149193	9 19	9°850807	42	30		30	
50	20	9°848218	10 21	10°151782	9°997473	10 42	10°002527	10°149255	10 21	9°850745	40	10		30	
50	22	9°848282	11 23	10°151718	9°997600	11 46	10°002400	10°149318	11 23	9°850682	38	30		30	
51	24	9°848345	12 25	10°151655	9°997726	12 51	10°002274	10°149381	12 25	9°850619	36	30		30	
51	26	9°848409	13 28	10°151591	9°997852	13 55	10°002148	10°149444	13 27	9°850556	34	30		30	
52	28	9°848472	14 30	10°151528	9°997979	14 59	10°002021	10°149507	14 29	9°850493	32	8		30	
52	30	9°848535	15 32	10°151465	9°998105	15 63	10°001895	10°149570	15 31	9°850430	30	30		30	
53	32	9°848599	16 34	10°151401	9°998231	16 67	10°001769	10°149632	16 34	9°850368	28	7		30	
53	34	9°848662	17 36	10°151338	9°998358	17 72	10°001642	10°149695	17 36	9°850305	26	30		30	
54	36	9°848726	18 38	10°151274	9°998484	18 76	10°001516	10°149758	18 38	9°850242	24	6		30	
54	38	9°848789	19 40	10°151211	9°998610	19 80	10°001390	10°149821	19 40	9°850179	22	30		30	
55	40	9°848852	20 43	10°151148	9°998737	20 84	10°001263	10°149884	20 42	9°850116	20	5		30	
55	42	9°848916	21 45	10°151084	9°998863	21 88	10°001137	10°149947	21 44	9°850053	18	30		30	
56	44	9°848979	22 47	10°151021	9°998989	22 93	10°001011	10°150010	22 46	9°849990	16	4		30	
56	46	9°849042	23 49	10°150958	9°999116	23 97	10°000884	10°150073	23 48	9°849927	14	30		30	
57	48	9°849106	24 51	10°150894	9°999242	24 101	10°000758	10°150136	24 50	9°849864	12	3		30	
57	50	9°849169	25 53	10°150831	9°999368	25 105	10°000632	10°150199	25 52	9°849801	10	30		30	
58	52	9°849232	26 55	10°150768	9°999495	26 109	10°000505	10°150262	26 54	9°849738	8	2		30	
58	54	9°849295	27 57	10°150705	9°999621	27 114	10°000379	10°150326	27 56	9°849674	6	30		30	
59	56	9°849359	28 60	10°150641	9°999747	28 118	10°000253	10°150389	28 59	9°849611	4	1		30	
59	58	9°849422	29 62	10°150578	9°999874	29 122	10°000126	10°150452	29 61	9°849548	2	30		30	
60	60	9°849485	30 64	10°150515	10°000000	30 126	10°000000	10°150515	30 63	9°849485	0	0		30	
"	m.	Cosine	Parts	Secant	Cotang.	Parts	Tangent	Cosec.	Parts	Sine	m.	"	m.	"	
45°														3 1/2 (m)	

LOG. OF THE SQUARE OF THE SINE*
OF HALF THE ARC.

	0°				1°				2°				a.
	0'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'		
	0 ^h 0 ^m	0 ^h 1 ^m	0 ^h 2 ^m	0 ^h 3 ^m	0 ^h 4 ^m	0 ^h 5 ^m	0 ^h 6 ^m	0 ^h 7 ^m	0 ^h 8 ^m	0 ^h 9 ^m	0 ^h 10 ^m		
0° 0'		4.67757	27963	6.181	5.88168	0.7550	2.3385	3.6774	4.8371	5.8600	6.7751	0	
15	1.12127	4.69193	28684	6.162	5.88530	0.7839	2.3626	3.6980	4.8552	5.8761	6.7895	1	
30	1.72333	4.70605	29399	6.141	5.88889	0.8127	2.3866	3.7136	4.8732	5.8921	6.8040	2	
45	2.07552	4.71995	30108	6.617	5.89247	0.8414	2.4106	3.7392	4.8912	5.9081	6.8184	3	
1° 0'	2.32539	4.73363	30811	6.509	5.89604	0.8700	2.4345	3.7597	4.9092	5.9241	6.8328	4	
15	2.51921	4.74710	31509	6.561	5.89959	0.8985	2.4583	3.7802	4.9271	5.9401	6.8471	5	
30	2.67757	4.76036	32201	6.602	5.90313	0.9270	2.4821	3.8006	4.9450	5.9560	6.8615	6	
45	2.81147	4.77342	32888	6.649	5.90665	0.9553	2.5058	3.8209	4.9628	5.9719	6.8758	7	
2° 0'	2.92745	4.78629	33569	6.695	5.91016	0.9836	2.5294	3.8412	4.9807	5.9878	6.8901	8	
15	3.02976	4.79897	34245	6.741	5.91366	1.0117	2.5530	3.8615	4.9984	6.0036	6.9044	9	
30	3.12127	4.81147	34916	6.787	5.91714	1.0398	2.5765	3.8817	5.0162	6.0194	6.9186	10	
45	3.20406	4.82379	35581	6.833	5.92061	1.0677	2.5999	3.9019	5.0339	6.0352	6.9328	11	
3° 0'	3.27963	4.83594	36242	6.878	5.92406	1.0956	2.6233	3.9220	5.0516	6.0509	6.9470	12	
15	3.34916	4.84792	36897	6.923	5.92750	1.1234	2.6466	3.9421	5.0692	6.0666	6.9612	13	
30	3.41353	4.85973	37548	6.968	5.93093	1.1511	2.6699	3.9622	5.0868	6.0823	6.9754	14	
45	3.47345	4.87139	38194	7.013	5.93434	1.1787	2.6931	3.9821	5.1044	6.0980	6.9895	15	
4° 0'	3.52951	4.88290	38835	7.058	5.93773	1.2063	2.7162	4.0021	5.1219	6.1136	7.0036	16	
15	3.58217	4.89425	39471	7.103	5.94113	1.2337	2.7393	4.0220	5.1394	6.1292	7.0177	17	
30	3.63182	4.90546	40103	7.146	5.94450	1.2611	2.7623	4.0418	5.1568	6.1448	7.0318	18	
45	3.67878	4.91653	40730	7.189	5.94786	1.2883	2.7852	4.0616	5.1743	6.1604	7.0458	19	
5° 0'	3.72333	4.92745	41352	7.232	5.95121	1.3155	2.8081	4.0814	5.1916	6.1759	7.0598	20	
15	3.76571	4.93824	41971	7.276	5.95454	1.3426	2.8309	4.1011	5.2090	6.1914	7.0738	21	
30	3.80612	4.94890	42584	7.319	5.95786	1.3696	2.8537	4.1208	5.2263	6.2068	7.0878	22	
45	3.84473	4.95943	43194	7.362	5.96117	1.3966	2.8764	4.1404	5.2436	6.2223	7.1017	23	
6° 0'	3.88169	4.96983	43799	7.405	5.96447	1.4234	2.8991	4.1600	5.2608	6.2377	7.1157	24	
15	3.91715	4.98011	44400	7.447	5.96775	1.4502	2.9217	4.1795	5.2780	6.2531	7.1296	25	
30	3.95122	4.99027	44997	7.490	5.97102	1.4769	2.9442	4.1990	5.2952	6.2684	7.1435	26	
45	3.98400	5.00031	45590	7.532	5.97428	1.5035	2.9667	4.2185	5.3124	6.2838	7.1573	27	
7° 0'	4.01559	5.01024	46179	7.573	5.97753	1.5300	2.9891	4.2379	5.3295	6.2991	7.1712	28	
15	4.04607	5.02005	46764	7.616	5.98076	1.5564	3.0114	4.2573	5.3466	6.3143	7.1850	29	
30	4.07551	5.02976	47345	7.657	5.98399	1.5828	3.0337	4.2766	5.3636	6.3296	7.1988	30	
45	4.10400	5.03935	47922	7.698	5.98720	1.6091	3.0560	4.2959	5.3806	6.3448	7.2125	31	
8° 0'	4.13157	5.04885	48495	7.739	5.99040	1.6353	3.0781	4.3151	5.3976	6.3600	7.2263	32	
15	4.15830	5.05824	49065	7.782	5.99358	1.6614	3.1003	4.3343	5.4146	6.3752	7.2400	33	
30	4.18423	5.06753	49631	7.824	5.99676	1.6874	3.1223	4.3534	5.4315	6.3903	7.2537	34	
45	4.20941	5.07672	50193	7.866	5.99992	1.7134	3.1444	4.3726	5.4484	6.4054	7.2674	35	
9° 0'	4.23388	5.08581	50752	7.907	6.00308	1.7393	3.1663	4.3916	5.4652	6.4205	7.2811	36	
15	4.25768	5.09481	51307	7.948	6.00622	1.7651	3.1882	4.4106	5.4820	6.4356	7.2947	37	
30	4.28084	5.10372	51858	7.988	6.00935	1.7908	3.2101	4.4296	5.4988	6.4506	7.3084	38	
45	4.30340	5.11254	52406	8.021	6.01247	1.8165	3.2319	4.4486	5.5156	6.4656	7.3220	39	
10° 0'	4.32539	5.12127	52951	8.061	6.01557	1.8421	3.2536	4.4675	5.5323	6.4806	7.3355	40	
15	4.34684	5.12991	53492	8.100	6.01867	1.8676	3.2753	4.4863	5.5490	6.4956	7.3491	41	
30	4.36777	5.13847	54030	8.139	6.02176	1.8930	3.2969	4.5052	5.5656	6.5105	7.3626	42	
45	4.38821	5.14694	54564	8.178	6.02483	1.9184	3.3185	4.5239	5.5822	6.5254	7.3761	43	
11° 0'	4.40818	5.15534	55095	8.217	6.02789	1.9437	3.3400	4.5427	5.5988	6.5403	7.3896	44	
15	4.42770	5.16365	55623	8.256	6.03095	1.9689	3.3615	4.5614	5.6154	6.5552	7.4031	45	
30	4.44679	5.17188	56148	8.294	6.03399	1.9940	3.3829	4.5800	5.6319	6.5700	7.4166	46	
45	4.46547	5.18004	56670	8.333	6.03702	2.0191	3.4043	4.5986	5.6484	6.5848	7.4300	47	
12° 0'	4.48375	5.18812	57189	8.371	6.04004	2.0441	3.4256	4.6172	5.6649	6.5996	7.4434	48	
15	4.50166	5.19612	57704	8.409	6.04305	2.0690	3.4469	4.6358	5.6813	6.6144	7.4568	49	
30	4.51921	5.20406	58216	8.447	6.04605	2.0938	3.4681	4.6543	5.6977	6.6291	7.4702	50	
45	4.53641	5.21192	58726	8.484	6.04904	2.1186	3.4892	4.6727	5.7141	6.6438	7.4835	51	
13° 0'	4.55328	5.21971	59232	8.522	6.05202	2.1433	3.5103	4.6911	5.7304	6.6585	7.4969	52	
15	4.56982	5.22743	59736	8.559	6.05499	2.1680	3.5314	4.7095	5.7467	6.6731	7.5102	53	
30	4.58600	5.23508	60236	8.596	6.05795	2.1925	3.5524	4.7279	5.7630	6.6878	7.5235	54	
45	4.60200	5.24267	60734	8.634	6.06090	2.2170	3.5734	4.7462	5.7792	6.7024	7.5367	55	
14° 0'	4.61765	5.25019	61229	8.670	6.06384	2.2415	3.5943	4.7644	5.7955	6.7170	7.5500	56	
15	4.63302	5.25764	61721	8.707	6.06677	2.2658	3.6151	4.7826	5.8117	6.7315	7.5632	57	
30	4.64813	5.26503	62211	8.744	6.06969	2.2901	3.6359	4.8008	5.8278	6.7461	7.5764	58	
45	4.66298	5.27236	62697	8.780	6.07260	2.3144	3.6567	4.8190	5.8439	6.7606	7.5896	59	

* Same as log. haversine of Inman's Tables.

LOG. SINE SQUARE

		2°					3°					4°					5°							
		45'		0'		15'		30'		45'		0'		15'		30'		45'		0'		15'		
		0' 11m	0' 12m	0' 13m	0' 14m	0' 15m	0' 16m	0' 17m	0' 18m	0' 19m	0' 20m	0' 21m	s.											
0	0'	6'	6'	6'	7"	7"	7"	7"	7"	7"	7"	7"	0											
	15	76028	83584	90535	6'96970	02960	08564	13827	18790	23483	27936	32171	0											
	30	76159	83704	90646	6'97073	03057	08654	13912	18870	23559	28008	32240	1											
	45	76290	83825	90757	6'97176	03153	08745	13997	18950	23635	28080	32309	2											
	1	76421	83945	90868	6'97279	03249	08835	14082	19030	23711	28153	32377	3											
1	0'	76552	84065	90979	6'97382	03345	08925	14167	19111	23787	28225	32446	4											
	15	76683	84185	91089	6'97485	03441	09015	14252	19191	23863	28297	32515	5											
	30	76814	84304	91200	6'97588	03537	09105	14337	19271	23939	28369	32583	6											
	45	76944	84424	91310	6'97690	03633	09195	14421	19350	24015	28441	32652	7											
	2	77074	84543	91421	6'97793	03729	09284	14506	19430	24090	28513	32720	8											
2	0'	77204	84663	91531	6'97895	03824	09374	14590	19510	24166	28584	32789	9											
	15	77334	84782	91641	6'97997	03920	09464	14674	19590	24241	28656	32857	10											
	30	77463	84900	91751	6'98099	04015	09553	14759	19669	24317	28728	32925	11											
	45	77592	85019	91860	6'98201	04110	09642	14843	19749	24392	28800	32994	12											
	3	77722	85138	91970	6'98303	04205	09732	14927	19828	24468	28871	33062	13											
3	0'	77851	85256	92079	6'98405	04300	09821	15011	19908	24543	28943	33130	14											
	15	77979	85374	92189	6'98506	04395	09910	15095	19987	24618	29014	33198	15											
	30	78108	85492	92298	6'98608	04490	09999	15179	20066	24693	29086	33266	16											
	45	78236	85610	92407	6'98709	04585	10088	15262	20145	24768	29157	33334	17											
	4	78364	85728	92516	6'98811	04680	10177	15346	20225	24843	29228	33402	18											
4	0'	78492	85846	92624	6'98912	04774	10265	15430	20304	24918	29299	33470	19											
	15	78620	85963	92733	6'99013	04869	10354	15513	20383	24993	29371	33538	20											
	30	78748	86080	92841	6'99114	04963	10443	15597	20461	25068	29442	33606	21											
	45	78875	86197	92950	6'99214	05057	10531	15680	20540	25143	29513	33673	22											
	5	79002	86314	93058	6'99315	05151	10619	15763	20619	25217	29584	33741	23											
5	0'	79129	86431	93166	6'99416	05245	10708	15846	20698	25292	29655	33809	24											
	15	79256	86548	93274	6'99516	05339	10796	15930	20776	25366	29726	33876	25											
	30	79383	86664	93382	6'99616	05433	10884	16013	20855	25441	29797	33944	26											
	45	79509	86781	93489	6'99717	05527	10972	16096	20933	25515	29867	34011	27											
	6	79636	86897	93597	6'99817	05620	11060	16178	21012	25590	29938	34079	28											
6	0'	79762	87013	93704	6'99917	05714	11148	16261	21090	25664	30009	34146	29											
	15	79888	87129	93812	7'00017	05807	11235	16344	21168	25738	30079	34213	30											
	30	80014	87244	93919	7'00116	05901	11323	16427	21246	25812	30150	34281	31											
	45	80139	87360	94026	7'00216	05994	11411	16509	21325	25886	30220	34348	32											
	7	80265	87475	94133	7'00315	06087	11498	16592	21403	25960	30291	34415	33											
7	0'	80390	87591	94239	7'00415	06180	11586	16674	21481	26034	30361	34482	34											
	15	80515	87706	94346	7'00514	06273	11673	16756	21558	26108	30431	34549	35											
	30	80640	87821	94453	7'00613	06366	11760	16839	21636	26182	30501	34616	36											
	45	80764	87935	94559	7'00712	06458	11847	16921	21714	26256	30572	34683	37											
	8	80889	88050	94665	7'00811	06551	11934	17003	21792	26330	30642	34750	38											
8	0'	81013	88165	94771	7'00910	06643	12021	17085	21869	26403	30712	34817	39											
	15	81137	88279	94877	7'01009	06736	12108	17167	21947	26477	30782	34884	40											
	30	81261	88393	94983	7'01107	06828	12195	17249	22024	26550	30852	34950	41											
	45	81385	88507	95089	7'01206	06920	12282	17331	22102	26624	30922	35017	42											
	9	81509	88621	95194	7'01304	07013	12368	17412	22179	26697	30992	35084	43											
9	0'	81632	88735	95300	7'01403	07105	12455	17494	22256	26771	31062	35150	44											
	15	81756	88848	95405	7'01501	07196	12541	17575	22333	26844	31131	35217	45											
	30	81879	88962	95510	7'01599	07288	12627	17657	22411	26917	31201	35283	46											
	45	82002	89075	95615	7'01697	07380	12714	17738	22488	26990	31271	35350	47											
	10	82124	89188	95720	7'01795	07472	12800	17820	22565	27063	31340	35416	48											
10	0'	82247	89301	95825	7'01892	07563	12886	17901	22642	27137	31410	35482	49											
	15	82369	89414	95930	7'01990	07655	12972	17982	22719	27210	31479	35549	50											
	30	82492	89527	96034	7'02088	07746	13058	18063	22795	27282	31549	35615	51											
	45	82613	89639	96139	7'02185	07837	13144	18144	22872	27355	31618	35681	52											
	11	82735	89752	96243	7'02282	07928	13229	18225	22949	27428	31687	35747	53											
11	0'	82857	89864	96347	7'02379	08019	13315	18306	23025	27501	31757	35813	54											
	15	82979	89976	96451	7'02476	08110	13401	18387	23102	27573	31826	35879	55											
	30	83100	90088	96555	7'02573	08201	13486	18468	23178	27646	31895	35945	56											
	45	83221	90200	96659	7'02670	08292	13572	18548	23255	27719	31964	36011	57											
	12	83342	90312	96763	7'02767	08383	13657	18629	23331	27791	32033	36077	58											
12	0'	83463	90423	96865	7'02864	08473	13742	18709	23407	27864	32102	36143	59											
	15	83584	90535	96968	7'02961	08564	13827	18790	23483	27936	32171	36208	60											
	30	83704	90646	97071	7'03058	08654	13912	18870	23559	28008	32240	36273	61											
	45	83825	90757	97174	7'03155	08745	13997	18950	23635	28080	32309	36338	62											
	13	83945	90868	97277	7'03252	08835	14082	19030	23711	28153	32377	36403	63											

TABLE 69

LOG. SINE SQUARE														
		5°		6°				7°				8°		N.
		30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'		
		0° 22'	0° 23'	0° 24'	0° 25'	0° 26'	0° 27'	0° 28'	0° 29'	0° 30'	0° 31'	0° 32'		
0	0	36209	40067	43760	47302	50706	53980	57135	60179	63120	65964	68717	0	
	15	36274	40129	43820	47360	50761	54034	57187	60229	63168	66011	68762	1	
	30	36340	40193	43880	47418	50817	54087	57238	60279	63216	66057	68807	2	
	45	36406	40255	43941	47476	50872	54141	57290	60329	63266	66103	68852	3	
1	0	36471	40318	44001	47533	50928	54194	57341	60378	63312	66150	68897	4	
	15	36537	40380	44061	47591	50983	54247	57393	60428	63360	66196	68942	5	
	30	36602	40443	44121	47649	51039	54301	57444	60478	63408	66243	68987	6	
	45	36668	40506	44181	47707	51094	54354	57496	60527	63456	66289	69032	7	
2	0	36733	40568	44241	47764	51149	54407	57547	60577	63504	66336	69077	8	
	15	36798	40631	44301	47821	51205	54461	57598	60627	63552	66382	69122	9	
	30	36864	40693	44361	47879	51260	54514	57650	60676	63600	66429	69167	10	
	45	36929	40756	44420	47936	51315	54567	57701	60726	63648	66475	69212	11	
3	0	36994	40818	44480	47994	51370	54620	57752	60775	63696	66521	69257	12	
	15	37059	40880	44540	48051	51426	54673	57804	60825	63744	66568	69302	13	
	30	37124	40943	44600	48109	51481	54727	57855	60874	63792	66614	69347	14	
	45	37189	41005	44659	48166	51536	54780	57906	60924	63839	66660	69392	15	
4	0	37254	41067	44719	48223	51591	54833	57957	60973	63887	66704	69437	16	
	15	37319	41129	44779	48280	51646	54886	58008	61022	63935	66753	69481	17	
	30	37384	41191	44838	48337	51701	54939	58060	61072	63983	66799	69526	18	
	45	37449	41253	44898	48395	51756	54992	58111	61121	64030	66845	69571	19	
	30	37514	41315	44957	48452	51811	55045	58162	61170	64078	66891	69616	20	
	45	37579	41377	45016	48509	51866	55097	58213	61220	64126	66937	69660	21	
	30	37643	41439	45076	48566	51921	55150	58264	61269	64173	66983	69705	22	
	45	37708	41501	45135	48623	51975	55203	58315	61318	64221	67029	69750	23	
6	0	37772	41563	45194	48680	52030	55256	58366	61367	64269	67075	69794	24	
	15	37837	41625	45254	48737	52085	55308	58416	61417	64316	67121	69839	25	
	30	37902	41686	45313	48794	52140	55361	58467	61466	64364	67167	69883	26	
	45	37966	41748	45372	48850	52194	55414	58518	61515	64411	67213	69928	27	
7	0	38030	41810	45431	48907	52249	55467	58569	61564	64458	67259	69972	28	
	15	38095	41871	45490	48964	52304	55519	58620	61613	64506	67305	70017	29	
	30	38159	41933	45549	49021	52358	55572	58670	61662	64553	67351	70061	30	
	45	38223	41994	45608	49077	52413	55624	58721	61711	64601	67397	70106	31	
8	0	38288	42056	45667	49134	52467	55677	58772	61760	64648	67443	70150	32	
	15	38352	42117	45726	49191	52522	55729	58823	61809	64695	67489	70195	33	
	30	38416	42179	45785	49247	52576	55782	58873	61858	64743	67535	70239	34	
	45	38480	42240	45844	49304	52631	55834	58924	61907	64790	67580	70283	35	
9	0	38544	42301	45903	49360	52685	55887	58974	61955	64837	67626	70328	36	
	15	38608	42363	45962	49417	52739	55939	59025	62004	64885	67672	70372	37	
	30	38672	42424	46020	49473	52794	55992	59075	62053	64932	67717	70416	38	
	45	38736	42485	46079	49530	52848	56044	59126	62102	64979	67763	70461	39	
	30	38800	42546	46138	49586	52902	56096	59176	62151	65026	67809	70505	40	
	45	38863	42607	46196	49642	52956	56148	59227	62200	65073	67854	70549	41	
	30	38927	42668	46255	49699	53011	56201	59277	62248	65120	67900	70593	42	
	45	38991	42729	46313	49755	53065	56253	59327	62297	65167	67946	70637	43	
11	0	39054	42790	46372	49811	53119	56305	59378	62345	65214	67991	70682	44	
	15	39118	42851	46430	49867	53173	56357	59428	62394	65261	68037	70726	45	
	30	39182	42912	46489	49923	53227	56409	59478	62442	65308	68082	70770	46	
	45	39245	42973	46547	49979	53281	56461	59529	62491	65355	68128	70814	47	
12	0	39309	43034	46605	50036	53335	56513	59579	62540	65402	68173	70858	48	
	15	39372	43095	46664	50092	53389	56565	59629	62588	65449	68219	70902	49	
	30	39435	43155	46722	50148	53443	56617	59679	62636	65496	68264	70946	50	
	45	39499	43216	46780	50204	53497	56669	59729	62685	65543	68309	70990	51	
13	0	39562	43277	46838	50259	53550	56721	59779	62733	65590	68355	71034	52	
	15	39625	43337	46896	50315	53604	56773	59829	62782	65637	68400	71078	53	
	30	39688	43398	46955	50371	53658	56825	59879	62830	65683	68445	71122	54	
	45	39751	43458	47013	50427	53712	56876	59929	62878	65730	68491	71166	55	
14	0	39815	43519	47071	50483	53765	56928	59979	62927	65777	68536	71210	56	
	15	39878	43579	47129	50539	53819	56980	60029	62975	65824	68581	71254	57	
	30	39941	43639	47187	50594	53873	57032	60079	63023	65870	68627	71298	58	
	45	40004	43700	47245	50650	53926	57083	60129	63071	65917	68672	71341	59	
Sec. 1° 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'														
D. 64. Parts 4 9 13 17 21 26 30 34 38 43 47 51 55 60 64														
D. 45. Parts 3 6 9 12 15 18 21 24 27 30 33 36 39 42 45														

TABLE 69

881

LOG. SINE SQUARE

	8°				9°				10°				N.
	15'	30'	45'		0'	15'	30'	45'	0'	15'	30'	45'	
	0° 33'	0° 34'	0° 35'	0° 36'	0° 37'	0° 38'	0° 39'	0° 40'	0° 41'	0° 42'	0° 43'		
0° 0'	71385	73974	76487	78929	81303	83615	85866	88059	90198	92286	94324	0	
15	71429	74016	76528	78969	81342	83653	85903	88095	90234	92320	94357	1	
30	71473	74059	76569	79009	81382	83691	85940	88131	90269	92354	94391	2	
45	71516	74101	76610	79049	81421	83729	85977	88167	90304	92389	94424	3	
1 0	71560	74143	76652	79089	81459	83767	86014	88203	90339	92423	94458	4	
15	71604	74186	76693	79129	81498	83804	86050	88239	90374	92457	94491	5	
30	71648	74228	76734	79169	81537	83842	86087	88276	90409	92492	94525	6	
45	71691	74271	76775	79209	81576	83880	86124	88312	90445	92526	94558	7	
2 0	71735	74313	76816	79249	81615	83918	86161	88348	90480	92560	94592	8	
15	71778	74355	76857	79289	81654	83956	86198	88383	90515	92595	94625	9	
30	71822	74398	76898	79329	81693	83994	86235	88419	90550	92629	94659	10	
45	71866	74440	76940	79369	81732	84032	86272	88455	90585	92663	94692	11	
3 0	71909	74482	76981	79409	81771	84070	86309	88491	90620	92697	94726	12	
15	71953	74524	77022	79449	81810	84107	86346	88527	90655	92731	94759	13	
30	71996	74567	77063	79489	81848	84145	86382	88563	90690	92766	94792	14	
45	72040	74609	77104	79529	81887	84183	86419	88599	90725	92800	94826	15	
4 0	72083	74651	77145	79568	81926	84221	86456	88635	90760	92834	94859	16	
15	72126	74693	77186	79608	81965	84258	86493	88671	90795	92868	94892	17	
30	72170	74735	77227	79648	82003	84296	86530	88707	90830	92902	94926	18	
45	72213	74777	77267	79688	82042	84334	86566	88742	90865	92936	94959	19	
5 0	72257	74819	77308	79728	82081	84372	86603	88778	90900	92970	94992	20	
15	72300	74861	77349	79767	82119	84409	86640	88814	90935	93005	95026	21	
30	72343	74904	77390	79807	82158	84447	86676	88850	90970	93039	95059	22	
45	72387	74946	77431	79847	82197	84484	86713	88885	91005	93073	95092	23	
6 0	72430	74988	77472	79886	82235	84522	86750	88921	91039	93107	95126	24	
15	72473	75030	77513	79926	82274	84560	86786	88957	91074	93141	95159	25	
30	72516	75072	77553	79966	82313	84597	86823	88993	91109	93175	95192	26	
45	72560	75114	77594	80005	82351	84635	86860	89028	91144	93209	95225	27	
7 0	72603	75155	77635	80045	82390	84672	86896	89064	91179	93243	95259	28	
15	72646	75197	77676	80085	82428	84710	86933	89100	91214	93277	95292	29	
30	72689	75239	77716	80124	82467	84747	86969	89135	91248	93311	95325	30	
45	72732	75281	77757	80164	82505	84785	87006	89171	91283	93345	95358	31	
8 0	72775	75323	77798	80203	82544	84822	87042	89207	91318	93379	95391	32	
15	72818	75365	77838	80243	82582	84860	87079	89242	91353	93413	95424	33	
30	72861	75407	77879	80282	82621	84897	87115	89278	91387	93447	95458	34	
45	72904	75448	77920	80322	82659	84935	87152	89314	91422	93480	95491	35	
9 0	72947	75490	77960	80361	82698	84972	87188	89349	91457	93514	95524	36	
15	72990	75532	78001	80401	82736	85010	87225	89385	91492	93548	95557	37	
30	73033	75574	78041	80440	82774	85047	87261	89420	91526	93582	95590	38	
45	73076	75615	78082	80480	82813	85084	87298	89456	91561	93616	95623	39	
10 0	73119	75657	78122	80519	82851	85122	87334	89491	91596	93650	95656	40	
15	73162	75699	78163	80558	82889	85159	87371	89527	91630	93684	95689	41	
30	73205	75740	78203	80598	82928	85196	87407	89562	91665	93717	95722	42	
45	73248	75782	78244	80637	82966	85234	87443	89598	91699	93751	95755	43	
11 0	73291	75824	78284	80677	83004	85271	87480	89633	91734	93785	95788	44	
15	73334	75865	78325	80716	83043	85308	87516	89668	91769	93819	95821	45	
30	73377	75907	78365	80755	83081	85346	87552	89704	91803	93852	95854	46	
45	73419	75948	78405	80794	83119	85383	87589	89740	91838	93886	95887	47	
12 0	73462	75990	78446	80834	83157	85420	87625	89775	91872	93920	95920	48	
15	73505	76031	78486	80873	83196	85457	87661	89810	91907	93954	95953	49	
30	73548	76073	78526	80912	83234	85494	87697	89846	91941	93987	95986	50	
45	73590	76114	78567	80951	83272	85532	87734	89881	91976	94021	96019	51	
13 0	73633	76156	78607	80991	83310	85569	87770	89916	92010	94055	96052	52	
15	73676	76197	78647	81030	83348	85606	87806	89952	92045	94088	96085	53	
30	73718	76239	78688	81069	83386	85643	87842	89987	92079	94122	96118	54	
45	73761	76280	78728	81108	83424	85680	87878	90022	92114	94156	96150	55	
14 0	73803	76321	78768	81147	83462	85717	87915	90057	92148	94189	96183	56	
15	73846	76363	78808	81186	83501	85754	87951	90093	92183	94223	96216	57	
30	73889	76404	78848	81225	83539	85791	87987	90128	92217	94257	96249	58	
45	73931	76445	78889	81264	83577	85829	88023	90163	92251	94290	96282	59	

Sec. 1° 2° 3° 4° 5° 6° 7° 8° 9° 10° 11° 12° 13° 14° 15°

D. 44 Parts 3 6 9 11 14 17 20 23 26 29 32 34 37 40 43

D. 33 Parts 2 4 7 9 11 13 15 18 20 23 24 26 29 31 33

TABLE 69

LOG. SINE SQUARE														
		11°				12°				13°				
		14'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	
		0h 44m	0h 45m	0h 46m	0h 47m	0h 48m	0h 49m	0h 50m	0h 51m	0h 52m	0h 53m	0h 54m	0h 55m	
0	0	79	80	81	82	83	84	85	86	87	88	89	90	0
1	0	65146	7982604	01638	20248	38469	56312	73792	90922	07717	24190	40352	56514	0
1	15	63474	7982925	01945	20555	38770	56606	74080	91205	07995	24462	40619	56821	1
1	30	61801	7983245	02259	20862	39070	56900	74368	91487	08272	24734	40886	57123	2
1	45	60129	7983565	02572	21168	39370	57194	74656	91770	08549	25006	41152	57425	3
1	0	64457	7983886	02886	21475	39670	57488	74944	92052	08826	25277	41419	57726	4
1	15	64784	7984206	03199	21781	39970	57782	75232	92334	09102	25549	41685	58027	5
1	30	65111	7984526	03512	22087	40270	58076	75520	92617	09379	25820	41952	58328	6
1	45	65439	7984846	03825	22394	40570	58370	75808	92899	09655	26091	42218	58629	7
2	0	65766	7985166	04137	22700	40870	58663	76095	93181	09932	26363	42484	58930	8
2	15	66093	7985485	04450	23006	41169	58957	76383	93463	10209	26634	42750	59231	9
2	30	66420	7985805	04763	23312	41469	59250	76670	93744	10485	26905	43016	59532	10
2	45	66746	7986124	05075	23617	41768	59543	76958	94026	10761	27176	43282	59833	11
3	0	67073	7986443	05388	23923	42067	59836	77245	94308	11037	27447	43557	60134	12
3	15	67399	7986762	05701	24229	42367	60129	77532	94589	11314	27718	43814	60435	13
3	30	67726	7987082	06012	24534	42666	60422	77819	94871	11590	27989	44080	60736	14
3	45	68052	7987400	06324	24839	42965	60715	78106	95152	11865	28259	44345	61037	15
4	0	68378	7987719	06636	25145	43264	61008	78393	95433	12141	28530	44611	61338	16
4	15	68704	7988038	06947	25450	43562	61301	78680	95714	12417	28800	44876	61639	17
4	30	69030	7988357	07259	25755	43861	61593	78967	95995	12693	29071	45142	61940	18
4	45	69355	7988675	07571	26060	44159	61886	79253	96276	12968	29341	45407	62241	19
5	0	69681	7988994	07882	26365	44458	62178	79540	96557	13244	29611	45672	62542	20
5	15	70006	7989312	08193	26669	44756	62470	79826	96838	13519	29882	45937	62843	21
5														

LOG. SINE SQUARE

	13°					14°					15°					16°					n.		
	45'		0'		15'		30'		45'		0'		15'		30'		45'		0'			15'	
	0° 58'	0° 59'	1° 00'	1° 01'	1° 02'	1° 03'	1° 04'	1° 05'	1° 06'	1° 07'	1° 08'	1° 09'	1° 10'	1° 11'	1° 12'	1° 13'	1° 14'	1° 15'	1° 16'	1° 17'		1° 18'	
0° 0'	8.1	8.1	8.1	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	
15	56215	71788	187085	02112	16879	31395	45669	59708	73519	87111	00488	0											
30	56477	72046	187337	02360	17123	31635	45905	59940	73748	87373	00710	1											
45	56738	72303	187590	02608	17367	31875	46141	60172	73976	87560	00913	2											
1 0	57000	72560	187842	02856	17611	32115	46376	60404	74204	87784	01152	3											
15	57262	72817	188095	03104	17854	32354	46612	60636	74432	88009	01373	4											
30	57524	73074	188347	03352	18098	32594	46848	60867	74660	88233	01594	5											
45	57785	73331	188599	03600	18342	32833	47083	61099	74888	88458	01815	6											
2 0	58046	73588	188851	03848	18585	33073	47319	61313	75116	88682	02035	7											
15	58308	73844	189104	04095	18829	33312	47554	61562	75344	88906	02256	8											
30	58569	74101	189356	04343	19072	33552	47790	61794	75572	89131	02477	9											
45	58830	74357	189608	04591	19316	33791	48025	62025	75800	89355	02698	10											
3 0	59091	74614	189859	04838	19559	34030	48260	62257	76027	89579	02918	11											
15	59352	74870	190111	05086	19802	34269	48495	62488	76255	89803	03139	12											
30	59613	75126	190363	05333	20045	34508	48730	62719	76483	90027	03359	13											
45	59874	75382	190615	05580	20288	34747	48965	62951	76710	90251	03580	14											
4 0	60135	75639	190866	05827	20531	34986	49200	63182	76937	90475	03800	15											
15	60396	75895	191118	06074	20774	35225	49435	63413	77165	90699	04021	16											
30	60656	76150	191369	06322	21017	35464	49670	63643	77392	90922	04241	17											
45	60917	76406	191620	06569	21263	35703	49905	63875	77620	91146	04461	18											
5 0	61177	76662	191872	06816	21503	35941	50140	64106	77847	91370	04681	19											
15	61438	76918	192123	07062	21745	36180	50374	64337	78074														

	Sec.	1'	2'	3'	4'	5'	6'	7'	8'	9'	10'	11'	12'	13'	14'	15'
D. 260.	Parts	17	35	52	69	87	104	121	139	156	173	191	208	225	243	260
D. 220.	Parts	15	29	44	59	73	88	103	117	132	147	161	176	191	206	220

LOG. SINE SQUARE

	16°		17°				18°				19°	s.
	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'	
	1 ^h 6 ^m	1 ^h 7 ^m	1 ^h 8 ^m	1 ^h 9 ^m	1 ^h 10 ^m	1 ^h 11 ^m	1 ^h 12 ^m	1 ^h 13 ^m	1 ^h 14 ^m	1 ^h 15 ^m	1 ^h 16 ^m	
0	8.3	8.3	8.3	8.3	8.3	8.3	8.	8.4	8.4	8.4	8.4	0
15	13659	26629	39404	51990	64392	76615	388665	00546	12262	23818	35218	1
30	13877	26844	39615	52198	64597	76817	388864	00742	12456	24009	35407	2
45	14095	27058	39827	52406	64802	77020	389064	00939	12650	24201	35596	3
1	14312	27272	40038	52614	65007	77222	389263	01135	12843	24392	35784	4
15	14530	27487	40249	52822	65212	77424	389462	01332	13037	24583	35973	5
30	14748	27701	40460	53030	65417	77626	389661	01528	13231	24774	36161	6
45	14965	27915	40671	53238	65622	77828	389860	01724	13425	24965	36350	7
2	15182	28129	40882	53446	65827	78030	390059	01921	13618	25156	36538	8
15	15400	28344	41093	53654	66032	78232	390259	02117	13812	25347	36727	9
30	15617	28558	41304	53862	66237	78434	390458	02313	14005	25538	36915	10
45	15835	28772	41515	54070	66441	78635	390657	02510	14199	25729	37104	11
3	16052	28986	41726	54277	66646	78837	390855	02706	14392	25920	37292	12
15	16269	29200	41936	54485	66851	79039	391054	02902	14586	26110	37480	13
30	16486	29413	42147	54692	67055	79241	391252	03098	14779	26301	37668	14
45	16703	29627	42358	54900	67260	79442	391452	03294	14972	26492	37857	15
4	16920	29841	42568	55107	67464	79644	391651	03490	15166	26683	38045	16
15	17137	30055	42779	55315	67669	79845	391849	03686	15359	26873	38233	17
30	17354	30268	42989	55522	67873	80047	392048	03882	15552	27064	38421	18
45	17571	30482	43200	55730	68077	80248	392247	04077	15745	27254	38609	19
5	17788	30695	43410	55937	68282	80450	392445	04273	15938	27445	38797	20
15	18004	30909	43620	56144	68486	80651	392644	04469	16131	27635	38985	21
30	18221	31122	43830	56351	68690	80852	392842	04665	16324	27826	39173	22
45	18438	31336	44041	56558	68894	81053	393040	04860	16518	28016	39360	23
6	18654	31549	44251	56765	69098	81255	393239	05056	16710	28206	39548	24
15	18871	31762	44461	56973	69302	81456	393437	05252	16903	28397	39736	25
30	19087	31975	44671	57179	69506	81657	393635	05447	17096	28587	39924	26
45	19304	32189	44881	57386	69710	81858	393834	05643	17289	28777	40111	27
7	19520	32402	45091	57593	69914	82059	394032	05838	17482	28967	40299	28
15	19736	32615	45301	57800	70118	82260	394230	06033	17674	29157	40486	29
30	19953	32828	45511	58007	70322	82461	394428	06229	17867	29347	40674	30
8	20169	33041	45720	58214	70526	82661	394626	06424	18060	29537	40862	31
15	20385	33254	45930	58420	70729	82862	394824	06619	18252	29727	41049	32
30	20601	33466	46140	58627	70933	83063	395022	06814	18445	29917	41236	33
45	20817	33679	46349	58833	71137	83264	395220	07009	18637	30107	41424	34
9	21033	33892	46559	59040	71340	83464	395418	07205	18830	30297	41611	35
15	21249	34105	46768	59246	71544	83665	395615	07400	19022	30487	41798	36
30	21465	34317	46978	59453	71747	83866	395813	07595	19214	30677	41986	37
45	21681	34530	47187	59659	71950	84066	396011	07790	19407	30866	42173	38
10	21897	34743	47397	59866	72154	84267	396209	07985	19599	31056	42360	39
15	22112	34955	47606	60072	72357	84467	396406	08179	19791	31246	42547	40
20	22328	35167	47815	60278	72560	84667	396604	08374	19983	31435	42734	41
25	22543	35379	48025	60484	72764	84868	396801	08569	20176	31625	42921	42
30	22759	35592	48234	60690	72967	85068	396999	08764	20368	31814	43108	43
35	22974	35804	48443	60896	73170	85268	397196	08959	20560	32004	43295	44
40	23190	36016	48652	61102	73373	85468	397394	09153	20752	32193	43482	45
45	23405	36228	48861	61308	73576	85668	397591	09348	20944	32383	43669	46
11	23620	36440	49070	61514	73779	85869	397788	09542	21136	32572	43856	47
15	23836	36652	49279	61720	73982	86069	397985	09737	21328	32761	44043	48
20	24051	36864	49488	61926	74185	86269	398183	09931	21519	32951	44229	49
25	24266	37076	49696	62132	74387	86469	398380	10126	21711	33140	44416	50
30	24481	37288	49905	62338	74590	86668	398577	10320	21903	33329	44603	51
35	24696	37500	50114	62543	74793	86868	398774	10515	22095	33518	44789	52
40	24911	37712	50323	62749	74996	87068	398971	10709	22286	33707	44976	53
45	25126	37924	50531	62954	75198	87268	399168	10903	22478	33896	45163	54
12	25341	38135	50740	63160	75401	87468	399365	11097	22669	34085	45349	55
15	25556	38347	50948	63365	75603	87667	399562	11292	22861	34274	45535	56
20	25771	38558	51157	63571	75806	87867	399759	11486	23053	34463	45722	57
25	25985	38770	51365	63776	76008	88066	399955	11680	23244	34652	45908	58
30	26200	38981	51573	63981	76211	88266	400152	11874	23435	34841	46095	59
35	26415	39193	51782	64187	76413	88465	400349	12068	23627	35030	46281	60

Dec. 1. 218. Parts 14 29 43 58 72 86 101 115 130 144 158 173 187 202 216
 D. 187. Parts 12 25 37 50 62 75 87 100 112 125 137 150 162 175 187

LOG. SINE SQUARE

		19°			20°				21°				s.
		15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	
		1° 17'	1° 18'	1° 19'	1° 20'	1° 21'	1° 22'	1° 23'	1° 24'	1° 25'	1° 26'	1° 27'	
0	0	8.4	8.4	8.4	8.4	8.5	8.5	8.5	8.5	8.5	8.5	8.5	0
15	0	46653	57752	68706	79340	490089	00564	10979	21266	31429	41470	51392	1
30	0	46839	57938	68887	79520	490196	00739	11151	21436	31597	41636	51556	2
45	0	47026	58119	69068	79699	490373	00914	11324	21607	31765	41802	51720	3
1	0	47212	58303	69250	79878	490550	01088	11496	21777	31934	41968	51885	4
15	0	47398	58486	69431	80057	490726	01263	11669	21947	32102	42135	52049	5
30	0	47584	58670	69612	80235	490903	01437	11841	22118	32270	42301	52213	6
45	0	47770	58853	69793	80414	491080	01612	12013	22288	32438	42467	52377	7
2	0	47956	59037	69975	80593	491256	01786	12186	22458	32606	42633	52542	8
15	0	48142	59220	70156	80772	491433	01961	12358	22628	32774	42799	52706	9
30	0	48327	59404	70337	80951	491609	02135	12530	22798	32942	42965	52870	10
45	0	48513	59587	70518	81130	491786	02309	12702	22968	33111	43131	53034	11
3	0	48699	59771	70699	81308	491962	02483	12874	23138	33278	43297	53198	12
15	0	48885	59954	70880	81487	492139	02658	13047	23308	33446	43463	53362	13
30	0	49070	60137	71061	81666	492315	02832	13219	23478	33614	43629	53526	14
45	0	49256	60320	71241	81844	492492	03006	13391	23648	33782	43795	53690	15
4	0	49442	60504	71422	82023	492668	03180	13563	23818	33950	43961	53854	16
15	0	49627	60687	71603	82201	492844	03354	13735	23988	34118	44127	54018	17
30	0	49813	60870	71784	82380	493021	03528	13906	24158	34286	44293	54182	18
45	0	49998	61053	71964	82558	493197	03702	14078	24328	34454	44459	54346	19
5	0	50184	61236	72145	82737	493373	03876	14250	24498	34621	44624	54509	20
15	0	50369	61419	72326	82915	493549	04050	14422	24667	34789	44790	54673	21
30	0	50554	61602	72506	83093	493725	04224	14594	24837	34957	44956	54837	22
45	0	50740	61785	72687	83272	493901	04398	14766	25007	35124	45121	55001	23
6	0	50925	61968	72868	83450	494077	04572	14937	25176	35292	45287	55164	24
15	0	51110	62150	73048	83628	494253	04746	15109	25346	35459	45453	55328	25
30	0	51295	62333	73228	83806	494429	04919	15281	25515	35627	45618	55491	26
45	0	51480	62516	73409	83985	494605	05093	15452	25685	35795	45784	55655	27
7	0	51666	62699	73589	84163	494781	05267	15624	25854	35962	45949	55819	28
15	0	51851	62881	73769	84341	494957	05441	15795	26024	36129	46115	55982	29
30	0	52036	63064	73950	84519	495133	05614	15967	26193	36297	46280	56146	30
45	0	52221	63247	74130	84697	495308	05788	16138	26363	36464	46445	56309	31
8	0	52406	63429	74310	84875	495484	05961	16310	26532	36631	46611	56472	32
15	0	52591	63612	74490	85053	495660	06135	16481	26701	36799	46776	56636	33
30	0	52775	63794	74671	85231	495835	06308	16652	26871	36966	46941	56799	34
45	0	52960	63976	74851	85408	496011	06482	16824	27040	37133	47107	56963	35
9	0	53145	64160	75031	85586	496187	06655	16995	27209	37300	47272	57126	36
15	0	53330	64341	75211	85764	496362	06829	17166	27378	37468	47437	57289	37
30	0	53515	64524	75391	85942	496538	07002	17338	27548	37635	47602	57452	38
45	0	53699	64706	75571	86119	496713	07175	17509	27717	37802	47767	57615	39
10	0	53884	64888	75751	86297	496889	07349	17680	27886	37969	47932	57779	40
15	0	54068	65070	75930	86475	497064	07522	17851	28055	38136	48097	57942	41
30	0	54253	65252	76110	86652	497239	07695	18022	28224	38303	48262	58105	42
45	0	54437	65434	76290	86830	497415	07868	18193	28393	38470	48427	58268	43
1	0	54622	65617	76470	87007	497590	08041	18364	28562	38637	48592	58431	44
15	0	54806	65799	76649	87185	497765	08214	18535	28731	38804	48757	58594	45
30	0	54991	65981	76829	87362	497941	08387	18706	28899	38971	48922	58757	46
45	0	55175	66162	77009	87540	498116	08560	18877	29068	39137	49087	58920	47
12	0	55359	66344	77188	87717	498291	08733	19048	29237	39304	49252	59083	48
15	0	55544	66526	77368	87894	498466	08906	19219	29406	39471	49417	59246	49
30	0	55728	66708	77547	88072	498641	09079	19390	29575	39638	49581	59408	50
45	0	55912	66890	77727	88249	498816	09252	19560	29743	39804	49746	59571	51
13	0	56096	67072	77906	88426	498991	09425	19731	29912	39971	49911	59734	52
15	0	56280	67253	78086	88603	499166	09598	19902	30081	40138	50076	59897	53
30	0	56464	67435	78265	88780	499341	09771	20072	30249	40304	50240	60059	54
45	0	56648	67617	78444	88958	499516	09944	20243	30418	40471	50405	60222	55
11	0	56832	67798	78624	89135	499691	10116	20414	30586	40637	50569	60385	56
15	0	57016	67980	78803	89312	499866	10289	20584	30755	40804	50734	60548	57
30	0	57200	68161	78982	89489	500040	10461	20755	30923	40970	50898	60710	58
45	0	57384	68343	79161	89666	500215	10634	20925	31092	41137	51063	60873	59
					89842	500390	10807	21096	31260	41303	51227	61035	60

Sec. 1° 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 188. Parts 12 25 37 49 62 74 85 99 111 123 136 148 160 173 185
D. 164. Parts 11 22 33 44 55 66 76 87 98 109 120 131 142 153 164

		22°				23°				24°			a.
		0'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	
		1-28=	1-29=	1-30=	1-31=	1-32=	1-33=	1-34=	1-35=	1-36=	1-37=	1-38=	
		8.5	8.5	8.5	8.5	8.	8.6	8.6	8.6	8.6	8.6	8.6	
0	0	61198	70890	80471	89944	599311	08573	17734	26795	35758	44625	53399	0
15	15	61360	71051	80630	90101	599466	08726	17885	26945	35906	44772	53545	1
30	30	61523	71211	80789	90258	599621	08880	18037	27095	36055	44919	53690	2
45	45	61685	71372	80948	90415	599776	09033	18189	27245	36203	45066	53836	3
1	0	61847	71532	81106	90572	599931	09187	18341	27395	36352	45213	53981	4
15	15	62010	71693	81265	90729	600086	09340	18492	27545	36500	45360	54126	5
30	30	62172	71853	81424	90886	600242	09494	18644	27695	36649	45507	54272	6
45	45	62334	72014	81582	91042	600397	09647	18796	27845	36797	45654	54417	7
2	0	62497	72174	81741	91199	600552	09800	18947	27995	36946	45801	54562	8
15	15	62659	72334	81899	91356	600707	09954	19099	28145	37094	45947	54707	9
30	30	62821	72495	82058	91512	600862	10107	19251	28295	37242	46094	54853	10
45	45	62983	72655	82216	91669	601016	10260	19402	28445	37391	46241	54998	11
3	0	63145	72815	82375	91826	601171	10413	19554	28595	37539	46388	55143	12
15	15	63307	72975	82533	91982	601326	10566	19705	28745	37687	46534	55288	13
30	30	63469	73136	82691	92139	601481	10720	19857	28895	37835	46681	55433	14
45	45	63631	73296	82850	92296	601636	10873	20008	29044	37984	46828	55578	15
4	0	63793	73456	83008	92452	601791	11026	20160	29194	38132	46974	55723	16
15	15	63955	73616	83166	92609	601945	11179	20311	29344	38280	47121	55868	17
30	30	64117	73776	83325	92765	602100	11332	20462	29494	38428	47267	56014	18
45	45	64279	73936	83483	92922	602255	11485	20614	29643	38576	47414	56159	19
5	0	64441	74096	83641	93078	602410	11638	20765	29793	38724	47560	56304	20
15	15	64603	74256	83799	93234	602564	11791	20916	29943	38872	47707	56448	21
30	30	64765	74416	83957	93391	602719	11944	21067	30092	39020	47853	56593	22
45	45	64926	74576	84115	93547	602873	12096	21219	30242	39168	48000	56738	23
6	0	65088	74736	84273	93703	603028	12249	21370	30391	39316	48146	56883	24
15	15	65250	74896	84431	93860	603182	12402	21521	30541	39464	48293	57028	25
30	30	65412	75056	84589	94016	603337	12555	21672	30690	39612	48439	57173	26
45	45	65573	75215	84747	94172	603491	12708	21823	30840	39760	48585	57318	27
7	0	65735	75375	84905	94328	603646	12861	21974	30989	39908	48731	57462	28
15	15	65896	75535	85063	94484	603800	13013	22125	31139	40056	48878	57607	29
30	30	66058	75695	85221	94641	603955	13166	22276	31288	40203	49024	57752	30
45	45	66219	75854	85379	94797	604109	13319	22427	31438	40351	49170	57896	31
8	0	66381	76014	85537	94953	604263	13471	22578	31587	40499	49316	58041	32
15	15	66542	76173	85695	95109	604418	13624	22729	31736	40647	49463	58186	33
30	30	66704	76333	85853	95265	604572	13776	22880	31886	40794	49609	58330	34
45	45	66865	76493	86010	95421	604726	13929	23031	32035	40942	49755	58475	35
9	0	67027	76652	86168	95577	604880	14081	23182	32184	41090	49901	58620	36
15	15	67188	76812	86326	95732	605035	14234	23333	32333	41237	50047	58764	37
30	30	67349	76971	86483	95888	605189	14386	23484	32482	41385	50193	58909	38
45	45	67510	77130	86641	96044	605343	14539	23634	32632	41532	50339	59053	39
10	0	67672	77290	86799	96200	605497	14691	23785	32781	41680	50485	59198	40
15	15	67833	77449	86956	96356	605651	14844	23936	32930	41828	50631	59342	41
30	30	67994	77609	87114	96512	605805	14996	24087	33079	41975	50777	59486	42
45	45	68155	77768	87271	96667	605959	15148	24237	33228	42123	50923	59631	43
11	0	68316	77927	87429	96823	606113	15301	24388	33377	42270	51069	59775	44
15	15	68477	78086	87586	96979	606267	15453	24539	33526	42417	51215	59919	45
30	30	68639	78246	87743	97134	606421	15605	24689	33675	42565	51360	60064	46
45	45	68800	78405	87901	97290	606575	15757	24840	33824	42712	51506	60208	47
12	0	68961	78564	88058	97446	606729	15910	24990	33973	42859	51652	60352	48
15	15	69122	78723	88216	97601	606883	16062	25141	34122	43007	51798	60496	49
30	30	69282	78882	88373	97757	607036	16214	25291	34271	43154	51943	60641	50
45	45	69443	79041	88530	97912	607190	16366	25442	34419	43301	52089	60785	51
13	0	69604	79200	88687	98068	607344	16518	25592	34568	43449	52235	60929	52
15	15	69765	79359	88845	98223	607498	16670	25742	34717	43596	52380	61073	53
30	30	69926	79518	89002	98379	607651	16822	25893	34866	43743	52526	61217	54
45	45	70087	79677	89159	98534	607805	16974	26043	35015	43890	52672	61361	55
14	0	70247	79836	89316	98689	607959	17126	26194	35163	44037	52817	61505	56
15	15	70408	79995	89473	98845	608112	17278	26344	35312	44184	52963	61649	57
30	30	70569	80154	89630	99000	608266	17430	26494	35461	44331	53108	61793	58
45	45	70729	80313	89787	99155	608419	17582	26644	35609	44478	53254	61937	59

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 162 Parts 11 22 32 43 54 65 76 86 97 108 119 130 140 151 162
D. 145 Parts 10 19 29 39 48 58 68 77 87 97 106 116 126 135 145

LOG. SINE SQUARE

	24°					25°					26°					27°					s.	
	45'		0'		15'		30'		45'		0'		15'		30'		45'		0'			
	1° 39'	1° 40'	1° 41'	1° 42'	1° 43'	1° 44'	1° 45'	1° 46'	1° 47'	1° 48'	1° 49'	1° 50'	1° 51'	1° 52'	1° 53'	1° 54'	1° 55'	1° 56'	1° 57'	1° 58'		
0° 0'	62081	70674	79177	87595	95927	04176	12343	20431	28439	36371	44226	0									0	
15	62225	70816	79318	87734	96065	04313	12479	20565	28572	36502	44356	1									1	
30	62369	70958	79459	87974	96203	04450	12614	20699	28705	36634	44486	2									2	
45	62513	71101	79600	88013	96341	04586	12750	20833	28838	36765	44617	3									3	
1 0	62657	71243	79741	88153	96479	04723	12885	20967	28970	36896	44747	4									4	
15	62801	71385	79882	88292	96618	04860	13020	21101	29103	37028	44877	5									5	
30	62945	71528	80023	88432	96756	04996	13156	21235	29236	37159	45007	6									6	
45	63088	71670	80164	88571	96894	05133	13291	21369	29368	37291	45137	7									7	
2 0	63232	71812	80305	88710	97032	05270	13426	21503	29501	37422	45268	8									8	
15	63376	71955	80445	88850	97170	05406	13562	21637	29634	37554	45398	9									9	
30	63520	72097	80586	88989	97308	05543	13697	21771	29766	37685	45528	10									10	
45	63663	72239	80727	89129	97445	05679	13832	21905	29899	37816	45658	11									11	
3 0	63807	72381	80868	89268	97583	05816	13967	22039	30032	37948	45788	12									12	
15	63951	72523	81008	89407	97721	05952	14102	22173	30164	38079	45918	13									13	
30	64094	72666	81149	89546	97859	06089	14238	22306	30297	38210	46048	14									14	
45	64238	72808	81290	89686	97997	06225	14373	22440	30429	38341	46178	15									15	
4 0	64381	72950	81430	89825	98135	06362	14508	22574	30562	38473	46308	16									16	
15	64525	73092	81571	89964	98273	06498	14643	22708	30694	38604	46437	17									17	
30	64668	73234	81711	90103	98410	06635	14778	22841	30827	38735	46568	18									18	
45	64812	73376	81852	90242	98548	06771	14913	22975	30959	38866	46698	19									19	
5 0	64955	73518	81993	90381	98686	06908	15048	23109	31092	38997	46828	20									20	
15	65099	73660	82133	90520	98823	07044	15183	23242	31224	39128	46958	21									21	
30	65242	73802	82274	90660	98961	07180	15318	23376	31356	39259	47087	22									22	
45	65386	73944	82414	90799	99099	07316	15453	23510	31489	39391	47217	23									23	
6 0	65529	74086	82555	90938	99237	07453	15588	23643	31621	39522	47347	24									24	
15	65672	74227	82695	91077	99374	07589	15723	23777	31753	39653	47477	25									25	
30	65816	74369	82835	91216	99512	07725	15858	23911	31886	39784	47607	26									26	
45	65959	74511	82976	91355	99649	07861	15993	24044	32018	39915	47736	27									27	
7 0	66102	74653	83116	91493	99787	07998	16127	24178	32150	40046	47866	28									28	
15	66245	74795	83256	91632	99924	08134	16262	24311	32282	40177	47996	29									29	
30	66389	74936	83397	91771	100062	08270	16397	24445	32414	40308	48126	30									30	
45	66532	75078	83537	91910	100199	08406	16532	24578	32547	40438	48255	31									31	
8 0	66675	75220	83677	92049	100337	08542	16667	24712	32679	40569	48385	32									32	
15	66818	75361	83817	92188	100474	08678	16801	24845	32811	40700	48515	33									33	
30	66961	75503	83958	92327	100612	08814	16936	24978	32943	40831	48644	34									34	
45	67104	75645	84098	92465	100749	08950	17071	25112	33075	40962	48774	35									35	
9 0	67247	75786	84238	92604	100886	09086	17205	25245	33207	41093	48903	36									36	
15	67390	75928	84378	92743	101024	09222	17340	25378	33339	41224	49033	37									37	
30	67533	76069	84518	92881	101161	09358	17475	25512	33471	41354	49162	38									38	
45	67676	76211	84658	93020	101298	09494	17609	25645	33603	41485	49292	39									39	
11 0	67819	76352	84798	93159	101436	09630	17744	25778	33735	41616	49421	40									40	
15	67962	76494	84938	93297	101573	09766	17878	25912	33867	41747	49551	41									41	
30	68105	76635	85078	93436	101710	09902	18013	26045	33999	41877	49680	42									42	
45	68248	76777	85218	93575	101847	10038	18147	26178	34131	42008	49810	43									43	
1 0	68391	76918	85358	93713	101984	10173	18282	26311	34263	42138	49939	44									44	
15	68534	77060	85498	93852	102121	10309	18416	26444	34395	42269	50068	45									45	
30	68677	77201	85638	93990	102259	10445	18551	26578	34527	42400	50198	46									46	
45	68819	77342	85778	94129	102396	10581	18685	26711	34659	42530	50327	47									47	
12 0	68962	77484	85918	94267	102533	10716	18820	26844	34790	42661	50457	48									48	
15	69105	77625	86058	94406	102670	10852	18954	26977	34922	42791	50586	49									49	
30	69248	77766	86198	94544	102807	10988	19088	27110	35054	42922	50715	50									50	
45	69390	77907	86337	94682	102944	11123	19223	27243	35186	43052	50844	51									51	
13 0	69533	78049	86477	94821	103081	11259	19357	27376	35317	43183	50974	52									52	
15	69676	78190	86617	94959	103218	11395	19491	27509	35449	43313	51103	53									53	
30	69818	78331	86757	95097	103355	11530	19626	27642	35581	43444	51232	54									54	
45	69961	78472	86896	95236	103492	11666	19760	27775	35712	43574	51361	55									55	
14 0	70103	78613	87036	95374	103629	11801	19894	27908	35844	43705	51490	56									56	
15	70246	78754	87176	95512	103765	11937	20028	28041	35976	43835	51619	57									57	
30	70389	78895	87315	95651	103902	12073	20162	28174	36107	43965	51749	58									58	
45	70531	79036	87455	95789	104039	12208	20297	28306	36239	44096	51878	59									59	

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 143. Parts 9 19 28 38 48 57 67 76 86 95 105 114 123 133 143

D. 130. Parts 9 17 26 35 43 52 61 69 78 87 95 104 113 121 130

TABLE 69

LOG. SINE SQUARE													
	27°		28°				29°				30°		a.
	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'		
	1° 30'	1° 51'	1° 52'	1° 53'	1° 54'	1° 55'	1° 56'	1° 57'	1° 58'	1° 59'	2° 0'		
0	8.7	8.7	8.7	8.7	8.7	8.7	8.	8-8	8-8	8-8	8-8	8-8	
15	53007	59715	67350	74910	82411	89839	797199	04494	11723	18839	25992	32992	0
30	52136	59842	67477	75041	82536	89962	797321	04615	11843	19008	26110	33110	1
45	52265	59970	67604	75167	82660	90085	797443	04736	11963	19127	26228	33228	2
1	52394	60098	67730	75292	82784	90208	797566	04857	12083	19246	26343	33343	3
2	52523	60226	67857	75417	82909	90332	797688	04978	12203	19365	26464	33464	4
3	52652	60354	67983	75543	83033	90455	797810	05099	12323	19484	26582	33582	5
4	52781	60481	68110	75668	83157	90578	797932	05220	12443	19602	26699	33699	6
5	52910	60609	68237	75794	83281	90701	798054	05341	12563	19721	26817	33817	7
6	53039	60737	68363	75919	83406	90824	798176	05461	12683	19840	26935	33935	8
7	53168	60864	68490	76044	83530	90947	798298	05582	12802	19959	27053	34053	9
8	53296	60992	68616	76170	83654	91070	798420	05703	12922	20078	27170	34170	10
9	53425	61120	68743	76295	83778	91193	798542	05824	13042	20196	27288	34288	11
10	53554	61247	68869	76420	83902	91316	798663	05945	13162	20315	27406	34406	12
11	53683	61375	68995	76545	84026	91439	798785	06066	13281	20434	27523	34523	13
12	53812	61503	69122	76671	84150	91562	798907	06186	13401	20552	27641	34641	14
13	53941	61630	69248	76796	84275	91685	799029	06307	13521	20671	27759	34759	15
14	54069	61758	69375	76921	84399	91808	799151	06428	13641	20790	27876	34876	16
15	54198	61885	69501	77046	84523	91931	799273	06549	13760	20908	27994	34994	17
16	54327	62013	69627	77172	84647	92054	799395	06669	13880	21027	28111	35111	18
17	54455	62140	69754	77297	84771	92177	799516	06790	13999	21145	28229	35229	19
18	54584	62268	69880	77422	84895	92300	799638	06911	14119	21264	28346	35346	20
19	54713	62395	70006	77547	85019	92423	799760	07031	14239	21382	28464	35464	21
20	54841	62523	70132	77672	85143	92545	799882	07152	14358	21501	28581	35581	22
21	54970	62650	70259	77797	85266	9266							

LOG. SINE SQUARE

		30°				31°				32°				33°	
		18'	30'	45'	0'	18'	30'	45'	0'	18'	30'	45'	0'		
		2 ^h 1 ^m	2 ^h 2 ^m	2 ^h 3 ^m	2 ^h 4 ^m	2 ^h 5 ^m	2 ^h 6 ^m	2 ^h 7 ^m	2 ^h 8 ^m	2 ^h 9 ^m	2 ^h 10 ^m	2 ^h 11 ^m	2 ^h 12 ^m		
0	0	883	884	46936	53798	0602	67349	74040	0676	87258	893785	0261	06684	0	
1	0	3034	0015	47050	53911	0715	67461	74151	0786	87367	893894	0368	06790	1	
2	0	3151	0130	47050	53911	0715	67461	74151	0786	87367	893894	0368	06790	2	
3	0	3268	0246	47165	54025	0828	67573	74262	0896	87476	894002	0476	06897	3	
4	0	3384	0362	47280	54139	0941	67685	74373	1006	87585	894110	0583	07003	4	
5	0	3501	0478	47395	54253	1053	67797	74484	1117	87694	894219	0690	07110	5	
6	0	3618	0594	47510	54367	1166	67909	74595	1227	87804	894327	0798	07217	6	
7	0	3735	0709	47624	54481	1279	68021	74706	1337	87913	894435	0905	07323	7	
8	0	3851	0825	47739	54594	1392	68133	74817	1447	88022	894544	1013	07430	8	
9	0	3968	0941	47854	54708	1505	68245	74928	1557	88131	894652	1120	07536	9	
10	0	4085	1056	47968	54822	1618	68356	75039	1667	88240	894760	1227	07643	0	
11	0	4201	1172	48083	54936	1730	68468	75150	1777	88349	894868	1335	07749	11	
12	0	4318	1288	48198	55049	1843	68580	75261	1887	88458	894976	1442	07856	12	
13	0	4435	1404	48313	55163	1956	68692	75372	1997	88567	895085	1549	07962	13	
14	0	4551	1519	48427	55277	2069	68804	75483	2107	88676	895193	1657	08068	14	
15	0	4668	1635	48542	55390	2181	68915	75594	2217	88786	895301	1764	08175	15	
16	0	4785	1750	48657	55504	2294	69027	75704	2327	88895	895409	1871	08281	16	
17	0	4901	1866	48771	55618	2407	69139	75815	2436	89004	895517	1978	08388	17	
18	0	5018	1982	48886	55731	2519	69251	75926	2566	89113	895625	2086	08494	18	
19	0	5134	2097	49000	55845	2632	69362	76037	2666	89222	895734	2193	08600	19	
20	0	5251	2213	49115	55959	2745	69474	76148	2766	89330	895842	2300	08707	20	
21	0	5367	2328	49229	56072	2857	69586	76258	2876	89439	895950	2407	08813	21	
22	0	5484	2444	49344	56186	2970	69697	76369	2986	89548	896058	2514	08919	22	
23	0	5600	2559	49458	56299	3082	69809	76480	3096	89657	896166	2622	09026	23	
24	0	5717	2675	49573	56413	3195	69921	76590	3205	89766	896274	2729	09132	24	
25	0	5833	2790	49687	56526	3308	70032	76701	3315	89875	896382	2836	09238	25	
26	0	5950	2905	49802	56640	3420	70144	76812	3425	89984	896490	2943	09345	26	
27	0	6066	3021	49916	56753	3533	70255	76923	3535	90093	896598	3050	09451	27	
28	0	6183	3136	50031	56867	3645	70367	77033	3644	90202	896706	3157	09557	28	
29	0	6299	3251	50145	56980	3758	70479	77144	3754	90311	896814	3264	09663	29	
30	0	6415	3367	50259	57094	3870	70590	77254	3864	90419	896922	3371	09770	30	
31	0	6532	3482	50374	57207	3983	70702	77365	3974	90528	897030	3479	09876	31	
32	0	6648	3598	50488	57320	4095	70813	77476	4083	90637	897137	3586	09982	32	
33	0	6764	3713	50603	57434	4207	70925	77586	4193	90746	897245	3693	10088	33	
34	0	6881	3828	50717	57547	4320	71036	77697	4303	90854	897353	3800	10194	34	
35	0	6997	3944	50831	57660	4432	71148	77807	4412	90963	897461	3907	10301	35	
36	0	7113	4059	50945	57774	4545	71259	77918	4522	91072	897569	4014	10407	36	
37	0	7230	4174	51060	57887	4657	71370	78028	4632	91181	897677	4121	10513	37	
38	0	7346	4289	51174	58000	4769	71482	78139	4741	91289	897785	4228	10619	38	
39	0	7462	4405	51288	58114	4882	71593	78249	4851	91398	897892	4334	10725	39	
40	0	7578	4520	51403	58227	4994	71705	78360	4960	91507	898000	4441	10831	40	
41	0	7694	4635	51517	58340	5106	71816	78470	5070	91615	898108	4548	10937	41	
42	0	7811	4750	51631	58453	5219	71927	78581	5179	91724	898216	4655	11043	42	
43	0	7927	4865	51745	58567	5331	72039	78691	5289	91833	898324	4762	11149	43	
44	0	8043	4981	51859	58680	5443	72150	78802	5398	91941	898431	4869	11255	44	
45	0	8159	5096	51973	58793	5555	72261	78912	5508	92050	898539	4976	11361	45	
46	0	8275	5211	52088	58906	5668	72373	79022	5617	92158	898647	5083	11467	46	
47	0	8391	5326	52202	59019	5780	72484	79133	5727	92267	898754	5190	11573	47	
48	0	8507	5441	52316	59132	5892	72595	79243	5836	92376	898862	5296	11679	48	
49	0	8623	5556	52430	59246	6004	72706	79353	5946	92484	898970	5403	11785	49	
50	0	8739	5671	52544	59359	6116	72818	79464	6055	92593	899077	5510	11891	50	
51	0	8855	5786	52658	59472	6227	72929	79574	6164	92701	899185	5617	11997	51	
52	0	8971	5901	52772	59585	6341	73040	79684	6274	92810	899293	5723	12103	52	
53	0	9087	6016	52886	59698	6453	73151	79795	6383	92918	899400	5830	12209	53	
54	0	9203	6131	53000	59811	6565	73262	79905	6492	93027	899508	5937	12315	54	
55	0	9319	6246	53114	59924	6677	73374	80015	6602	93135	899615	6044	12421	55	
56	0	9435	6361	53228	60037	6789	73485	80125	6711	93244	899723	6150	12526	56	
57	0	9551	6476	53342	60150	6901	73596	80235	6821	93352	899831	6257	12632	57	
58	0	9667	6591	53456	60263	7013	73707	80346	6930	93460	899938	6364	12738	58	
59	0	9783	6706	53570	60376	7125	73818	80456	7039	93569	900046	6470	12844	59	
60	0	9899	6821	53684	60489	7237	73929	80566	7148	93677	900153	6577	12950	60	

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 116. Parts 8 15 23 31 39 46 54 62 68 77 85 93 100 108 116

D. 106. Parts 7 14 21 29 36 43 49 56 63 71 78 85 92 99 106

LOG. SINE SQUARE

		36°				37°				38°				
		0'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'		
		24°	25°	26°	27°	28°	29°	30°	31°	32°	33°	34°	s.	
0	8'9	8'9	8'9		9'0	9'0	9'0	9'0	9'0	9'0	9'0	9'0		
	79965	85775	91543	8'997269	02953	08596	14198	19761	25284	30768	36213	0		
	80062	85872	91639	8'997364	03047	08690	14291	19853	25375	30859	36304	1		
	80159	85968	91735	8'997459	03142	08783	14384	19946	25467	30950	36394	2		
	80256	86065	91830	8'997554	03236	08877	14477	20038	25559	31041	36485	3		
1	80353	86161	91926	8'997649	03330	08971	14570	20130	25651	31132	36575	4		
	80451	86258	92022	8'997744	03425	09064	14663	20223	25742	31223	36665	5		
	80548	86354	92118	8'997839	03519	09158	14757	20315	25834	31314	36756	6		
	80645	86450	92213	8'997934	03613	09252	14849	20407	25926	31405	36846	7		
	80742	86547	92309	8'998029	03708	09345	14942	20500	26017	31496	36936	8		
2	80839	86643	92405	8'998124	03802	09439	15035	20592	26109	31587	37027	9		
	80936	86740	92500	8'998219	03896	09532	15128	20684	26201	31678	37117	10		
	81033	86836	92596	8'998314	03990	09626	15221	20776	26292	31769	37207	11		
	81130	86932	92692	8'998409	04085	09720	15314	20869	26384	31860	37298	12		
	81227	87029	92787	8'998504	04179	09813	15407	20961	26475	31951	37388	13		
3	81324	87125	92883	8'998599	04273	09907	15500	21053	26567	32042	37478	14		
	81421	87221	92978	8'998694	04367	10000	15593	21145	26658	32133	37569	15		
	81518	87318	93074	8'998789	04461	10094	15686	21237	26750	32224	37659	16		
	81615	87414	93170	8'998883	04556	10187	15778	21330	26842	32315	37749	17		
	81712	87510	93265	8'998978	04650	10281	15871	21422	26933	32405	37839	18		
4	81809	87606	93361	8'999073	04744	10374	15964	21514	27025	32496	37930	19		
	81906	87703	93456	8'999168	04838	10468	16057	21606	27116	32587	38020	20		
	82003	87799	93552	8'999263	04933	10561	16150	21698	27208	32678	38110	21		
	82100	87895	93647	8'999358	05027	10654	16243	21791	27299	32769	38200	22		
	82197	87991	93743	8'999453	05121	10748	16335	21883	27391	32860	38291	23		
6	82294	88088	93838	8'999547	05215	10842	16428	21975	27482	32951	38381	24		
	82391	88184	93934	8'999642	05309	10935	16521	22067	27574	33041	38471	25		
	82488	88280	94029	8'999737	05403	11029	16614	22159	27665	33132	38561	26		
	82585	88376	94125	8'999832	05497	11122	16706	22251	27756	33223	38651	27		
	82682	88472	94220	8'999927	05591	11215	16799	22343	27848	33314	38741	28		
7	82779	88568	94316	9'000021	05685	11309	16893	22435	27939	33405	38832	29		
	82875	88665	94411	9'000116	05780	11402	16985	22527	28031	33495	38922	30		
	82972	88761	94507	9'000211	05874	11496	17077	22619	28122	33586	39012	31		
	83069	88857	94602	9'000305	05968	11589	17170	22711	28213	33677	39102	32		
	83166	88953	94697	9'000400	06062	11682	17263	22803	28305	33768	39192	33		
8	83263	89049	94793	9'000495	06156	11776	17355	22895	28396	33858	39282	34		
	83359	89145	94888	9'000590	06250	11869	17448	22987	28488	33949	39372	35		
	83456	89241	94984	9'000684	06344	11962	17541	23079	28579	34040	39462	36		
	83553	89337	95079	9'000779	06438	12055	17633	23171	28670	34130	39552	37		
	83650	89433	95174	9'000874	06532	12149	17726	23263	28762	34221	39642	38		
9	83746	89529	95269	9'000968	06625	12242	17819	23355	28853	34312	39732	39		
	83843	89625	95365	9'001063	06719	12335	17911	23447	28944	34402	39822	40		
	83940	89721	95460	9'001157	06813	12429	18004	23539	29035	34493	39912	41		
	84037	89817	95555	9'001252	06907	12522	18096	23631	29127	34584	40002	42		
	84133	89913	95651	9'001347	07001	12615	18189	23723	29218	34674	40092	43		
11	84230	90009	95746	9'001441	07095	12708	18281	23815	29309	34765	40182	44		
	84327	90105	95841	9'001536	07189	12802	18374	23907	29400	34855	40272	45		
	84423	90201	95937	9'001630	07283	12895	18467	23999	29492	34946	40362	46		
	84520	90297	96032	9'001725	07377	12988	18559	24091	29583	35037	40452	47		
	84617	90393	96127	9'001819	07471	13081	18652	24182	29674	35127	40542	48		
12	84713	90489	96222	9'001914	07564	13174	18744	24274	29765	35218	40632	49		
	84810	90585	96317	9'002008	07658	13267	18837	24366	29856	35308	40722	50		
	84906	90681	96413	9'002103	07752	13361	18929	24458	29948	35399	40812	51		
	85003	90777	96508	9'002197	07846	13454	19021	24550	30039	35489	40902	52		
	85100	90872	96603	9'002292	07940	13547	19114	24642	30130	35580	40992	53		
20	85196	90968	96698	9'002386	08033	13640	19206	24733	30221	35670	41082	54		
	85293	91064	96793	9'002481	08127	13733	19299	24825	30312	35761	41171	55		
	85389	91160	96888	9'002575	08221	13826	19391	24917	30403	35851	41261	56		
	85486	91256	96983	9'002670	08315	13919	19484	25009	30495	35942	41351	57		
	85582	91352	97079	9'002764	08408	14012	19576	25100	30586	36032	41441	58		
30	85679	91447	97174	9'002858	08502	14105	19668	25192	30677	36123	41531	59		

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 97. Parts 6 13 19 26 32 39 45 52 58 65 71 78 84 91 97

D. 90. Parts 6 12 18 24 30 36 42 48 54 60 66 72 78 84 90

		LOG. SINE SQUARE																		
		38°				39°					40°					41°			S.	
		48'		0'		18'		36'		48'		0'		18'		45'		0'		
		24 36"	24 36"	24 36"	24 36"	24 36"	24 36"	24 36"	24 36"	24 36"	24 36"	24 36"	24 36"	24 36"	24 36"	24 36"	24 36"	24 36"	24 36"	
0	0	9'0	9'0	9'0	9'0	9'0	9'0	9'0	9'0	9'0	9'0	9'0	9'0	9'0	9'0	9'0	9'0	9'0	9'0	0
1	0	41621	46991	52323	57619	62879	68103	73292	78446	83565	88651	93702	98736	103748	108728	113675	118589	123469	128315	1
2	0	41710	47080	52412	57707	62967	68190	73378	78532	83650	88735	93786	98819	103829	108815	113767	118685	123564	128410	2
3	0	41800	47169	52500	57795	63054	68277	73465	78617	83735	88819	93870	98904	103994	108979	113937	118865	123744	128590	3
4	0	41890	47258	52589	57883	63141	68364	73551	78703	83820	88904	93954	98988	104078	109063	114020	118957	123836	128682	4
5	0	41980	47347	52677	57971	63229	68450	73637	78788	83905	88988	94038	99072	104162	109147	114104	119041	123920	128768	5
6	0	42070	47436	52766	58059	63316	68537	73723	78874	83990	89073	94122	99157	104205	109190	114147	119084	124009	128816	6
7	0	42159	47525	52855	58147	63403	68624	73809	78960	84075	89157	94205	99242	104289	109274	114220	119157	124098	128904	7
8	0	42249	47615	52943	58235	63491	68710	73895	79045	84160	89242	94289	99326	104373	109358	114267	119204	124187	129012	8
9	0	42339	47704	53032	58323	63578	68797	73981	79131	84245	89326	94373	99360	104460	109445	114305	119242	124276	129100	9
10	0	42428	47793	53120	58411	63665	68884	74067	79216	84330	89410	94457	99444	104549	109534	114343	119280	124365	129188	10
11	0	42518	47882	53208	58499	63752	68971	74154	79302	84415	89495	94541	99528	104638	109619	114381	119317	124454	129276	11
12	0	42608	47971	53297	58586	63840	69057	74240	79387	84500	89579	94625	99612	104725	109707	114419	119354	124543	129364	12
13	0	42698	48060	53385	58674	63927	69144	74326	79473	84585	89664	94708	99699	104812	109794	114457	119391	124632	129452	13
14	0	42787	48149	53474	58762	64014	69231	74412	79558	84670	89748	94792	99784	104899	109881	114495	119428	124721	129540	14
15	0	42877	48238	53562	58850	64101	69317	74498	79644	84755	89832	94876	99869	104986	109968	114533	119465	124810	129628	15
16	0	42967	48327	53651	58938	64189	69404	74584	79729	84840	89917	94960	99954	105073	110055	114571	119502	124899	129716	16
17	0	43056	48416	53739	59025	64276	69490	74670	79815	84925	90001	95044	100031	105160	110142	114609	119539	124988	129804	17
18	0	43146	48505	53828	59113	64363	69577	74756	79900	85010	90085	95127	100117	105249	110229	114647	119576	125077	129892	18
19	0	43236	48594	53916	59201	64450	69664	74842	79985	85094	90170	95211	100204	105338	110316	114685	119613	125166	129980	19
20	0	43325	48683	54004	59289	64537	69750	74928	80071	85179	90254	95295	100291	105427	110403	114723	119650	125255	130068	20
21	0	43415	48772	54093	59377	64625	69837	75014	80156	85264	90338	95379	100378	105516	110490	114761	119687	125344	130156	21
22	0	43504	48861	54181	59464	64712	69923	75100	80242	85349	90422	95462	100465	105605	110577	114799	119724	125433	130244	22
23	0	43594	48950	54269	59552	64799	70010	75186	80327	85434	90507	95546	100552	105694	110664	114837	119761	125522	130332	23
24	0	43684	49039	54358	59640	64886	70107	75272	80412	85519	90591	95630	100639	105783	110751	114875	119798	125611	130420	24
25	0	43773	49128	54446	59728	64973	70183	75358	80498	85603	90675	95713	100726	105872	110838	114913	119835	125700	130508	25
26	0	43863	49217	54534	59815	65060	70270	75444	80583	85688	90759	95797	100812	105961	110925	114951	119872	125789	130596	26
27	0	43952	49306	54623	59903	65147	70356	75530	80669	85773	90844	95881	100900	106050	111012	114989	119909	125878	130684	27
28	0	44042	49395	54711	59991	65234	70443	75616	80754	85858	90928	95964	100987	106139	111099	115027	119946	125967	130772	28
29	0	44131	49484	54799	60079	65322	70529	75702	80839	85943	91012	96043	101074	106228	111186	115065	119983	126056	130860	29
30	0	44221	49573	54888	60166	65409	70616	75787	80925	86027	91096	96132	101161	106317	111273	115103	120020	126145	130948	30
31	0	44310	49662	54976	60254	65496	70702	75873	81010	86112	91181	96215	101249	106406	111360	115141	120057	126234	131036	31
32	0	44400	49750	55064	60341	65583	70789	75959	81095	86197	91265	96299	101337	106495	111447	115179	120094	126323	131124	32
33	0	44489	49839	55152	60429	65670	70875	76045	81181	86282	91349	96383	101425	106584	111534	115217	120131	126412	131212	33
34	0	44579	49928	55241	60517	65757	70961	76131	81266	86366	91433	96466	101513	106673	111621	115255	120168	126501	131300	34
35	0	44668	50017	55329	60604	65844	71048	76217	81351	86451	91517	96550	101601	106762	111708	115293	120205	126590	131388	35
36	0	44758	50106	55417	60692	65931	71134	76303	81436	86536	91601	96633	101689	106851	111795	115331	120242	126679	131476	36
37	0	44847	50195	55505	60780	66018	71221	76389	81522	86621	91685	96717	101777	106940	111882	115369	120279	126768	131564	37
38	0	44936	50283	55593	60867	66105	71307	76474	81607	86705	91770	96801	101865	107029	111969	115407	120316	126857	131652	38
39	0	45026	50372	55682	60955	66192	71394	76560	81693	86790	91854	96884	101953	107117	112056	115445	120353	126946	131740	39
40	0	45115	50461	55770	61042	66279	71480	76646	81778	86875	91938	96968	102041	107205	112143	115483	120390	127035	131828	40
41	0	45205	50550	55858	61130	66366	71566	76732	81863	86959	92022	97051	102129	107293	112230	115521	120427	127124	131916	41
42	0	45294	50639	55946	61218	66453	71653	76818	81948	87044	92106	97135	102217	107381	112317	115559	120464	127213	132004	42
43	0	45383	50727	56034	61305	66540	71739	76903	82033	87128	92190	97218	102305	107469	112404	115597	120501	127302	132092	43
44	0	45473	50816	56122	61393	66627	71826	76989	82118	87213	92274	97302	102393	107557	112491	115635	120538	127391	132180	44
45	0	45562	50905	56210	61480	66714	71912	77075	82203	87298	92358	97385	102481	107645	112578	115673	120575	127480	132268	45
46	0	45652	50994	56299	61568	66801	71998	77161	82289	87382	92442	97472	102569	107733	112665	115711	120612	127569	132356	46
47	0	45741	51082	56387	61655	66888	72085	77247	82374	87467	92526	97559	102657	107821	112752	115749	120649	127658	132444	47
48	0	45830	51171	56475	61743	66974	72171	77332	82459	87552	92610	97646	102745	107909	112839	115787	120686	127747	132532	48
49	0	45920	51260	56563	61830	67061	72257	77418	82544	87636	92694	97731	102833	107997	112926	115825	120723	127836	132620	49
50	0	46009	51348	56651	61918	67148	72343	77504	82629	87721	92778	97818	102921	108085	113013	115863	120760	127925	132708	50
51	0	46098	51437	56739	62005	67235	72430	77589	82714	87805	92862	97904	103009	108173	113100	115901	120797	128014	132796	51
52	0	46187	51526	56827	62093	67322	72516	77675	82800	87890	92946	97990	103097	108261	113187	115939	120834	128103	132884	52
53	0	46277	51614	56915	62180	67409	72602	77761	82885	87975	93030	98075	103185	108349	113274	115977	120871	128192	132972	53
54	0	46366	51703	57003																

TABLE 60

843

LOG. SINE SQUARE

	41°		42°				43°				44°		s.
	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'		
	2° 40"	2° 47"	2° 48"	2° 40"	2° 50"	2° 51"	2° 52"	2° 53"	2° 54"	2° 55"	2° 56"		
0 0	9' 098720	9' 103706	9' 108658	9' 113579	9' 118468	9' 123325	9' 128151	9' 132946	9' 137711	9' 142446	9' 147151	0	1
15	098804	037788	087411	13661	18549	23405	28231	33026	37790	42524	47229	1	2
30	098887	038711	08823	13742	18630	23486	28311	33105	37869	42603	47307	2	3
45	098970	03954	08905	13824	18711	23567	28391	33185	37948	42682	47385	3	4
1 0	099054	04037	08987	13906	18792	23647	28471	33265	38028	42760	47463	4	5
15	099137	04120	09070	13987	18873	23728	28552	33344	38107	42839	47542	5	6
30	099220	04202	09152	14069	18955	23809	28632	33424	38186	42918	47620	6	7
45	099304	04285	09234	14151	19036	23889	28712	33504	38265	42996	47698	7	8
2 0	099387	04368	09316	14232	19117	23970	28792	33583	38344	43075	47776	8	9
15	099470	04451	09398	14314	19198	24051	28872	33663	38423	43153	47854	9	10
30	099553	04533	09481	14396	19279	24131	28952	33742	38502	43232	47935	10	11
45	099637	04616	09563	14477	19360	24212	29032	33822	38581	43311	48010	11	12
3 0	099720	04699	09645	14559	19441	24292	29112	33902	38660	43389	48088	12	13
15	099803	04781	09727	14641	19523	24373	29192	33981	38739	43468	48166	13	14
30	099886	04864	09809	14722	19604	24454	29272	34061	38818	43546	48244	14	15
45	099970	04947	09891	14804	19685	24534	29353	34140	38898	43625	48322	15	16
4 0	100053	05030	09974	14886	19766	24615	29433	34220	38977	43703	48401	16	17
15	100136	05112	10055	14967	19847	24695	29513	34299	39056	43782	48479	17	18
30	100219	05195	10138	15049	19928	24776	29593	34379	39135	43860	48557	18	19
45	100303	05277	10220	15130	20009	24856	29673	34458	39214	43939	48635	19	20
5 0	100386	05360	10302	15212	20090	24937	29753	34538	39293	44018	48713	20	21
15	100469	05443	10384	15293	20171	25017	29833	34617	39372	44096	48791	21	22
30	100552	05525	10466	15375	20252	25098	29913	34697	39451	44174	48869	22	23
45	100635	05608	10548	15457	20333	25178	29993	34776	39530	44253	48947	23	24
6 0	100718	05691	10630	15538	20414	25259	30073	34856	39609	44331	49025	24	25
15	100801	05773	10712	15620	20495	25339	30153	34935	39688	44410	49102	25	26
30	100885	05856	10794	15701	20576	25420	30233	35015	39766	44488	49180	26	27
45	100968	05938	10877	15783	20657	25500	30313	35094	39845	44567	49258	27	28
7 0	101051	06021	10959	15864	20738	25581	30393	35174	39924	44645	49336	28	29
15	101134	06103	11041	15946	20819	25661	30472	35253	40003	44724	49414	29	30
30	101217	06186	11123	16027	20900	25742	30552	35332	40082	44802	49492	30	31
45	101300	06269	11205	16109	20981	25822	30632	35412	40161	44880	49570	31	32
8 0	101383	06351	11287	16190	21062	25902	30712	35491	40240	44959	49648	32	33
15	101466	06434	11369	16272	21143	25983	30792	35571	40319	45037	49726	33	34
30	101549	06516	11451	16353	21224	26063	30872	35650	40398	45116	49804	34	35
45	101632	06599	11533	16434	21305	26144	30952	35729	40477	45194	49882	35	36
9 0	101715	06681	11614	16516	21385	26224	31032	35809	40556	45272	49960	36	37
15	101798	06764	11696	16597	21466	26305	31112	35888	40634	45351	50038	37	38
30	101881	06846	11778	16679	21547	26385	31191	35967	40713	45429	50115	38	39
45	101964	06929	11860	16760	21628	26465	31271	36047	40792	45507	50193	39	40
10 0	102047	07011	11942	16841	21709	26546	31351	36126	40871	45586	50271	40	41
15	102130	07093	12024	16923	21790	26626	31431	36205	40950	45664	50349	41	42
30	102213	07176	12106	17004	21871	26706	31511	36285	41029	45742	50427	42	43
45	102296	07258	12188	17086	21952	26787	31591	36364	41107	45821	50505	43	44
11 0	102379	07341	12270	17167	22033	26867	31670	36443	41186	45899	50582	44	45
15	102462	07423	12352	17248	22113	26947	31750	36523	41265	45977	50660	45	46
30	102545	07506	12434	17330	22194	27028	31830	36602	41344	46056	50738	46	47
45	102628	07588	12515	17411	22275	27108	31910	36681	41423	46134	50816	47	48
12 0	102711	07670	12597	17492	22356	27188	31990	36761	41501	46212	50894	48	49
15	102794	07753	12679	17574	22437	27268	32069	36840	41580	46290	50971	49	50
30	102877	07835	12761	17655	22517	27349	32149	36919	41659	46369	51049	50	51
45	102960	07917	12843	17736	22598	27429	32229	36998	41738	46447	51127	51	52
13 0	103043	08000	12925	17818	22679	27509	32309	37077	41816	46525	51205	52	53
15	103126	08082	13006	17899	22759	27589	32388	37157	41895	46603	51282	53	54
30	103209	08164	13088	17980	22840	27670	32468	37236	41974	46682	51360	54	55
45	103291	08247	13170	18061	22921	27750	32548	37315	42052	46760	51438	55	56
14 0	103374	08329	13252	18143	23002	27830	32627	37394	42131	46838	51516	56	57
15	103457	08411	13334	18224	23083	27910	32707	37474	42210	46916	51593	57	58
30	103540	08494	13415	18305	23163	27990	32787	37553	42288	46994	51671	58	59
45	103623	08576	13497	18386	23244	28071	32867	37632	42367	47073	51749	59	60

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 83. Parts 5 11 16 22 28 33 39 44 50 55 61 66 72 77 83
11. 78. Parts 5 10 16 21 26 31 36 42 47 52 57 62 68 73 78

LOG. SINE SQUARE

	44°			45°				46°				47°	L
	18'	20'	45'	0'	18'	20'	45'	0'	15'	30'	45'	0'	
	2° 57'	2° 58'	2° 59'	3° 0'	3° 1'	3° 2'	3° 3'	3° 4'	3° 5'	3° 6'	3° 7'	3° 8'	
0 0	9'1	9'1	9'1	9'1	9'17	9'17	9'1	9'18	9'1	9'19	9'	9'20	0
15	51826	56473	61090	65679	0240	4773	79278	3756	88207	2631	197028	1399	1
30	51904	56550	61167	65756	0316	4848	79353	3830	88281	2704	197101	1472	2
45	51982	56627	61244	65832	0392	4924	79428	3905	88355	2778	197174	1545	3
1 0	52059	56704	61320	65908	0467	4999	79503	3979	88429	2851	197247	1617	4
15	52137	56781	61397	65984	0543	5074	79578	4054	88503	2925	197320	1690	5
30	52215	56859	61474	66060	0619	5149	79652	4128	88576	2998	197393	1762	6
45	52292	56936	61550	66137	0695	5225	79727	4202	88650	3072	197466	1835	7
2 0	52370	57013	61627	66213	0770	5300	79802	4277	88724	3145	197539	1908	8
15	52448	57090	61704	66289	0846	5375	79877	4351	88798	3219	197613	1980	9
30	52525	57167	61780	66365	0922	5450	79952	4425	88872	3292	197686	2053	10
45	52603	57244	61857	66441	0998	5526	80026	4500	88946	3366	197759	2125	11
3 0	52680	57321	61934	66518	1073	5601	80101	4574	89020	3439	197832	2198	12
15	52758	57399	62010	66594	1149	5676	80176	4648	89094	3512	197905	2270	13
30	52836	57476	62087	66670	1225	5751	80251	4723	89168	3586	197977	2343	14
45	52913	57553	62164	66746	1300	5827	80325	4797	89241	3659	198050	2416	15
4 0	52991	57630	62240	66822	1376	5902	80400	4871	89315	3733	198123	2488	16
15	53068	57707	62317	66898	1452	5977	80475	4946	89389	3806	198196	2561	17
30	53146	57784	62393	66974	1527	6052	80550	5020	89463	3879	198269	2633	18
45	53223	57861	62470	67051	1603	6127	80624	5094	89537	3953	198342	2706	19
5 0	53301	57938	62547	67127	1679	6203	80699	5168	89611	4026	198415	2778	20
15	53378	58015	62623	67203	1754	6278	80774	5243	89684	4100	198488	2851	21
30	53456	58092	62700	67279	1830	6353	80849	5317	89758	4173	198561	2923	22
45	53533	58169	62776	67355	1905	6428	80923	5391	89832	4246	198634	2996	23
6 0	53611	58246	62853	67431	1981	6503	80998	5465	89906	4320	198707	3068	24
15	53688	58323	62929	67507	2057	6578	81073	5540	89980	4393	198780	3141	25
30	53766	58400	63006	67583	2132	6653	81147	5614	90053	4466	198853	3213	26
45	53843	58477	63082	67659	2208	6729	81222	5688	90127	4540	198926	3285	27
7 0	53921	58554	63159	67735	2283	6804	81297	5762	90201	4613	198998	3358	28
15	53998	58631	63235	67811	2359	6879	81371	5836	90275	4686	199071	3430	29
30	54076	58708	63312	67887	2435	6954	81446	5911	90348	4759	199144	3503	30
8 0	54153	58785	63388	67963	2510	7029	81521	5985	90422	4833	199217	3575	31
15	54231	58862	63465	68039	2586	7104	81595	6059	90496	4906	199290	3648	32
30	54308	58939	63541	68115	2661	7179	81670	6133	90570	4979	199363	3720	33
45	54385	59016	63618	68191	2737	7254	81744	6207	90643	5053	199436	3792	34
9 0	54463	59093	63694	68267	2812	7329	81819	6281	90717	5126	199508	3865	35
15	54540	59170	63771	68343	2888	7404	81894	6356	90791	5199	199581	3937	36
30	54618	59247	63847	68419	2963	7479	81968	6430	90864	5272	199654	4010	37
45	54695	59324	63924	68495	3039	7554	82043	6504	90938	5346	199727	4082	38
10 0	54772	59401	64000	68571	3114	7629	82117	6578	91012	5419	199800	4154	39
15	54850	59477	64076	68647	3190	7704	82192	6652	91085	5492	199872	4227	40
30	54927	59554	64153	68723	3265	7779	82266	6726	91159	5565	199945	4299	41
45	55005	59631	64229	68799	3341	7854	82341	6800	91233	5639	200018	4371	42
11 0	55082	59708	64306	68875	3416	7929	82416	6874	91306	5712	200091	4444	43
15	55159	59785	64382	68951	3491	8004	82490	6948	91380	5785	200164	4516	44
30	55237	59862	64458	69027	3567	8079	82565	7023	91454	5858	200237	4588	45
45	55314	59939	64535	69103	3642	8154	82639	7097	91527	5931	200309	4661	46
12 0	55391	60015	64611	69178	3718	8229	82714	7171	91601	6004	200382	4733	47
15	55468	60092	64687	69254	3793	8304	82788	7245	91674	6078	200455	4805	48
30	55546	60169	64764	69330	3869	8379	82863	7319	91748	6151	200527	4878	49
45	55623	60246	64840	69406	3944	8454	82937	7393	91822	6224	200600	4950	50
13 0	55700	60323	64916	69482	4019	8529	83012	7467	91895	6297	200673	5022	51
15	55778	60399	64993	69558	4095	8604	83086	7541	91969	6370	200745	5094	52
30	55855	60476	65069	69634	4170	8679	83161	7615	92042	6443	200818	5167	53
45	55932	60553	65145	69709	4246	8754	83235	7689	92116	6517	200891	5239	54
14 0	56009	60630	65222	69785	4321	8829	83309	7763	92190	6590	200963	5311	55
15	56087	60707	65298	69861	4396	8904	83384	7837	92263	6663	201036	5383	56
30	56164	60783	65374	69937	4472	8979	83458	7911	92337	6736	201109	5456	57
45	56241	60860	65450	70013	4547	9054	83533	7985	92410	6809	201181	5528	58
15 0	56318	60937	65527	70089	4622	9128	83607	8059	92484	6882	201254	5600	59
30	56396	61014	65603	70164	4698	9203	83682	8133	92557	6955	201327	5672	60

D. 78. Parts 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15
D. 72. Parts 5 10 14 19 24 29 34 38 43 48 53 58 62 67 72

TABLE 69

LOG. SINE SQUARE

	47°			48°				49°				s.
	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	
	3 ^d 9 ^m	3 ^d 10 ^m	3 ^d 11 ^m	3 ^d 12 ^m	3 ^d 13 ^m	3 ^d 14 ^m	3 ^d 15 ^m	3 ^d 16 ^m	3 ^d 17 ^m	3 ^d 18 ^m	3 ^d 19 ^m	
0	9'2	9'2	9'2	9'2	9'2	9'2	9'2	9'2	9'2	9'2	9'2	0
15	05745	10064	14358	18627	22870	27089	31284	35454	39600	43722	47821	1
30	05817	10136	14429	18698	22941	27159	31353	35523	39669	43791	47889	2
45	05889	10207	14501	18768	23011	27229	31423	35593	39738	43859	47957	3
1	05961	10279	14572	18839	23082	27300	31493	35662	39807	43928	48025	4
15	06033	10351	14643	18910	23152	27370	31562	35731	39876	43996	48094	5
30	06105	10423	14715	18981	23223	27440	31632	35800	39944	44065	48162	6
45	06178	10494	14786	19052	23293	27510	31702	35870	40013	44133	48230	7
2	06250	10566	14857	19123	23364	27580	31772	35939	40082	44202	48298	8
15	06322	10638	14929	19194	23434	27650	31841	36008	40151	44270	48366	9
30	06394	10710	15000	19265	23505	27720	31911	36077	40220	44339	48434	10
45	06466	10781	15071	19336	23575	27790	31980	36147	40289	44407	48502	11
3	06538	10853	15142	19406	23646	27860	32050	36216	40358	44476	48570	12
15	06610	10925	15214	19477	23716	27930	32120	36285	40426	44544	48638	13
30	06682	10996	15285	19548	23786	28000	32189	36354	40495	44612	48706	14
45	06755	11068	15356	19619	23857	28070	32259	36423	40564	44681	48774	15
4	06827	11140	15427	19690	23927	28140	32329	36493	40632	44749	48842	16
15	06899	11211	15499	19761	23998	28210	32398	36562	40701	44818	48910	17
30	06971	11283	15570	19831	24068	28280	32468	36631	40770	44886	48978	18
45	07043	11355	15641	19902	24139	28350	32537	36700	40839	44954	49046	19
5	07115	11426	15712	19973	24209	28420	32607	36769	40908	45023	49114	20
15	07187	11498	15784	20044	24279	28490	32676	36839	40977	45091	49182	21
30	07259	11570	15855	20115	24350	28560	32746	36908	41046	45160	49250	22
45	07331	11641	15926	20186	24420	28630	32816	36977	41114	45228	49318	23
6	07403	11713	15997	20256	24491	28700	32885	37046	41183	45296	49386	24
15	07475	11785	16068	20327	24561	28770	32955	37115	41252	45365	49454	25
30	07547	11856	16140	20398	24631	28840	33024	37184	41321	45433	49522	26
45	07619	11928	16211	20469	24702	28910	33094	37254	41390	45501	49590	27
7	07691	11999	16282	20539	24772	28980	33163	37323	41458	45570	49658	28
15	07763	12071	16353	20610	24842	29050	33232	37392	41527	45638	49726	29
30	07835	12142	16424	20681	24913	29120	33302	37461	41595	45706	49794	30
45	07907	12214	16495	20752	24983	29190	33372	37530	41664	45775	49862	31
8	07979	12286	16566	20822	25053	29259	33441	37599	41733	45843	49930	32
15	08051	12357	16638	20893	25123	29329	33511	37668	41802	45911	49998	33
30	08123	12429	16709	20964	25194	29399	33580	37737	41870	45980	50065	34
45	08195	12500	16780	21034	25264	29469	33650	37806	41939	46048	50133	35
9	08267	12572	16851	21105	25334	29539	33719	37875	42008	46116	50201	36
15	08339	12643	16922	21176	25405	29609	33789	37944	42076	46184	50269	37
30	08411	12715	16993	21246	25475	29679	33858	38013	42145	46253	50337	38
45	08483	12786	17064	21317	25545	29749	33928	38083	42214	46321	50405	39
10	08555	12858	17135	21388	25615	29818	33997	38152	42282	46389	50473	40
15	08627	12929	17206	21459	25686	29888	34067	38221	42351	46457	50541	41
30	08699	13001	17278	21529	25756	29958	34136	38290	42420	46526	50608	42
45	08771	13072	17349	21600	25826	30028	34205	38359	42488	46594	50676	43
11	08843	13144	17420	21670	25896	30098	34275	38428	42557	46662	50744	44
15	08915	13215	17491	21741	25967	30168	34344	38497	42625	46730	50812	45
30	08987	13287	17562	21812	26037	30237	34414	38566	42694	46798	50880	46
45	09058	13358	17633	21882	26107	30307	34483	38635	42763	46867	50948	47
12	09130	13430	17704	21953	26177	30377	34552	38704	42831	46935	51015	48
15	09202	13501	17775	22024	26247	30447	34621	38773	42900	47003	51083	49
30	09274	13573	17846	22094	26318	30517	34691	38842	42968	47071	51151	50
45	09346	13644	17917	22165	26388	30586	34761	38911	43037	47140	51219	51
13	09418	13715	17988	22235	26458	30656	34830	38980	43106	47208	51287	52
15	09490	13787	18059	22306	26528	30726	34899	39049	43174	47276	51354	53
30	09561	13858	18130	22376	26598	30796	34968	39118	43243	47344	51422	54
45	09633	13930	18201	22447	26668	30865	35037	39187	43311	47412	51490	55
14	09705	14001	18272	22518	26739	30935	35107	39255	43380	47480	51558	56
15	09777	14072	18343	22588	26809	31005	35177	39324	43448	47549	51626	57
30	09849	14144	18414	22659	26879	31075	35246	39393	43517	47617	51693	58
45	09920	14215	18485	22729	26949	31144	35315	39462	43585	47685	51761	59
15	09992	14287	18556	22800	27019	31214	35385	39531	43654	47753	51829	60

Rec. 1° 2° 3° 4° 5° 6° 7° 8° 9° 10° 11° 12° 13° 14° 15°

D. 72. Parts 5 10 14 19 24 29 34 38 43 48 53 58 62 67 72

D. 88. Parts 4 9 13 18 23 27 31 36 40 45 50 54 59 63 68

TABLE 69

LOG. SINE SQUARE													
	50°				51°				52°				S.
	0	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'		
	3° 30'	3° 21'	3° 22'	3° 23'	3° 24'	3° 25'	3° 26'	3° 27'	3° 28'	3° 29'	3° 30'		
0	92	92	92	92	92	92	92	92	92	92	92	92	0
1	51897	55949	59978	63985	67969	71930	75870	79788	83684	87558	91412	95246	1
2	51904	56016	60045	64051	68035	71996	75936	79853	83749	87623	91476	95310	2
3	52032	56133	60162	64168	68150	72062	76001	79918	83813	87687	91540	95374	3
4	52100	56199	60217	64214	68187	72128	76067	79983	83878	87752	91604	95438	4
5	52167	56218	60246	64251	68234	72194	76132	80048	83943	87817	91668	95499	5
6	52235	56285	60313	64318	68300	72260	76197	80113	84008	87880	91732	95560	6
7	52303	56353	60380	64384	68366	72325	76263	80178	84072	87945	91796	95621	7
8	52360	56420	60447	64451	68432	72391	76328	80244	84138	88009	91860	95682	8
9	52428	56487	60514	64517	68498	72457	76394	80309	84202	88073	91924	95743	9
10	52506	56555	60580	64584	68564	72523	76459	80374	84266	88138	91988	95804	10
11	52573	56622	60647	64650	68631	72589	76525	80439	84331	88202	92053	95865	11
12	52641	56689	60714	64717	68697	72654	76590	80504	84396	88266	92116	95926	12
13	52709	56756	60781	64783	68764	72720	76655	80569	84461	88331	92180	95987	13
14	52776	56824	60848	64850	68829	72786	76721	80634	84525	88395	92244	96048	14
15	52844	56891	60915	64916	68895	72852	76786	80699	84590	88459	92308	96109	15
16	52912	56958	60982	64983	68961	72917	76852	80764	84655	88524	92372	96170	16
17	52979	57025	61049	65049	69027	72983	76917	80829	84719	88588	92436	96231	17
18	53047	57093	61116	65116	69094	73049	76982	80894	84784	88652	92500	96292	18
19	53115	57160	61182	65182	69160	73115	77048	80959	84849	88717	92564	96353	19
20	53182	57227	61249	65249	69226	73180	77113	81024	84913	88781	92627	96414	20
21	53250	57294	61316	65315	69292	73246	77178	81089	84978	88845	92691	96475	21
22	53317	57362	61383	65382	69358	73312	77244	81154	85042	88909	92755	96536	22
23	53385	57429	61450	65448	69424	73378	77309	81219	85107	88974	92819	96597	23
24	53453	57496	61517	65515	69490	73443	77374	81284	85172	8			

LOG. SINE SQUARE

	58°				59°				60°				61°	
	15'	30'	45'		0'	15'	30'	45'	0'	15'	30'	45'	0'	
	3 ^h 54 ^m	3 ^h 54 ^m	3 ^h 55 ^m	3 ^h 56 ^m	3 ^h 57 ^m	3 ^h 58 ^m	3 ^h 59 ^m	4 ^h 0 ^m	4 ^h 1 ^m	4 ^h 2 ^m	4 ^h 3 ^m	4 ^h 3 ^m	4 ^h 4 ^m	s.
0 0	9'3	9'3	9'3	9'3	9'3	9'39	9'39	9'	9'40	9'40	9'4	9'41	9'41	0
15	74552	77945	81320	84678	88018	91342	94649	397940	1214	4471	07713	0938	0	1
30	74609	78001	81376	84733	88074	91398	94704	397995	1268	4526	07767	0991	1	2
45	74666	78057	81432	84789	88130	91453	94759	398049	1323	4580	07820	1045	2	3
1 0	74722	78114	81488	84845	88185	91508	94814	398104	1377	4634	07874	1099	3	4
15	74779	78170	81544	84901	88241	91563	94869	398159	1432	4688	07928	1152	4	5
30	74836	78227	81600	84957	88296	91619	94924	398213	1486	4742	07982	1206	5	6
45	74892	78283	81656	85012	88351	91674	94979	398268	1540	4796	08036	1259	6	7
2 0	74949	78339	81712	85068	88407	91729	95034	398323	1595	4850	08090	1313	7	8
15	75006	78396	81768	85124	88463	91784	95089	398377	1649	4905	08144	1367	8	9
30	75062	78452	81825	85180	88518	91839	95144	398432	1704	4959	08197	1420	9	10
45	75119	78508	81881	85236	88574	91895	95199	398487	1758	5013	08251	1474	10	11
3 0	75176	78565	81937	85291	88629	91950	95254	398541	1812	5067	08305	1527	11	12
15	75232	78621	81993	85347	88685	92005	95309	398596	1867	5121	08359	1581	12	13
30	75289	78677	82049	85403	88740	92060	95364	398651	1921	5175	08413	1634	13	14
45	75345	78734	82105	85459	88796	92116	95419	398705	1975	5229	08467	1688	14	15
4 0	75402	78790	82161	85514	88851	92171	95474	398760	2030	5283	08520	1741	15	16
15	75459	78846	82217	85570	88906	92226	95529	398814	2084	5337	08574	1795	16	17
30	75515	78903	82273	85626	88962	92281	95583	398869	2139	5391	08628	1849	17	18
45	75572	78959	82329	85681	89017	92336	95638	398924	2193	5446	08682	1902	18	19
5 0	75628	79015	82385	85737	89073	92391	95693	398979	2247	5500	08736	1956	19	20
15	75685	79072	82441	85793	89128	92447	95748	399033	2302	5554	08789	2009	20	21
30	75742	79128	82497	85849	89184	92502	95803	399088	2356	5608	08843	2063	21	22
45	75798	79184	82553	85905	89239	92557	95858	399142	2410	5662	08897	2116	22	23
6 0	75855	79240	82609	85960	89295	92612	95913	399197	2465	5716	08951	2170	23	24
15	75911	79297	82665	86016	89350	92667	95968	399252	2519	5770	09005	2223	24	25
30	75968	79353	82721	86072	89406	92722	96023	399306	2573	5824	09058	2277	25	26
45	76024	79409	82777	86127	89461	92778	96077	399361	2628	5878	09112	2330	26	27
7 0	76081	79466	82833	86183	89516	92833	96132	399415	2682	5932	09166	2384	27	28
15	76138	79522	82889	86239	89572	92888	96187	399470	2736	5986	09220	2437	28	29
30	76194	79578	82945	86294	89627	92943	96242	399524	2790	6040	09273	2491	29	30
45	76251	79634	83001	86350	89683	92998	96297	399579	2845	6094	09327	2544	30	31
8 0	76307	79691	83057	86406	89738	93053	96352	399633	2899	6148	09381	2598	31	32
15	76364	79747	83113	86461	89793	93108	96406	399688	2953	6202	09435	2651	32	33
30	76420	79803	83169	86517	89849	93163	96461	399742	3008	6256	09488	2705	33	34
45	76477	79859	83225	86573	89904	93218	96516	399797	3062	6310	09542	2758	34	35
9 0	76533	79916	83281	86629	89959	93274	96571	399852	3116	6364	09596	2812	35	36
15	76590	79972	83337	86684	90015	93329	96626	399906	3170	6418	09650	2865	36	37
30	76646	80028	83392	86740	90070	93384	96681	399961	3225	6472	09703	2919	37	38
45	76703	80084	83448	86795	90125	93439	96735	400015	3279	6526	09757	2972	38	39
10 0	76759	80140	83504	86851	90181	93494	96790	400070	3333	6580	09811	3025	39	40
15	76816	80197	83560	86907	90236	93549	96845	400124	3387	6634	09864	3079	40	41
30	76872	80253	83616	86962	90292	93604	96900	400179	3442	6688	09918	3132	41	42
45	76929	80309	83672	87018	90347	93659	96955	400233	3496	6742	09972	3186	42	43
11 0	76985	80365	83728	87074	90402	93714	97009	400288	3550	6796	10026	3239	43	44
15	77042	80421	83784	87129	90458	93769	97064	400342	3604	6850	10079	3293	44	45
30	77098	80478	83840	87185	90513	93824	97119	400397	3659	6904	10133	3346	45	46
45	77155	80534	83896	87240	90568	93879	97174	400451	3713	6958	10187	3399	46	47
12 0	77211	80590	83952	87296	90624	93934	97228	400506	3767	7012	10240	3453	47	48
15	77268	80646	84007	87351	90679	93989	97283	400560	3821	7066	10294	3506	48	49
30	77324	80702	84063	87407	90734	94045	97338	400615	3875	7120	10348	3560	49	50
45	77380	80758	84119	87463	90790	94100	97393	400669	3930	7174	10401	3613	50	51
13 0	77437	80815	84175	87518	90845	94155	97447	400724	3984	7228	10455	3666	51	52
15	77493	80871	84231	87574	90900	94210	97502	400778	4038	7281	10509	3719	52	53
30	77550	80927	84287	87630	90956	94265	97557	400833	4092	7335	10562	3773	53	54
45	77606	80983	84343	87685	91011	94320	97612	400887	4146	7389	10616	3827	54	55
14 0	77663	81039	84398	87741	91066	94375	97666	400942	4201	7443	10670	3880	55	56
15	77719	81095	84454	87796	91121	94430	97721	400996	4255	7497	10723	3933	56	57
30	77775	81151	84510	87852	91177	94485	97776	401051	4309	7551	10777	3987	57	58
45	77832	81208	84566	87907	91232	94540	97831	401105	4363	7605	10830	4040	58	59
50	77888	81264	84622	87962	91287	94595	97885	401159	4417	7659	10884	4093	59	60

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 57. Parts 4 8 11 15 19 23 27 30 34 38 42 46 49 53 57

D. 54. Parts 3 7 10 14 18 21 24 28 32 36 39 42 46 49 54

LOG. SINE SQUARE

		61°			62°				63°				64°	
		18'	20'	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'	
		4 8	4 0	4 7	4 8	4 9	4 10	4 11	4 12	4 13	4 14	4 15	4 16	
0	0	9'41	9'4	9'42	9'42	9'42	9'4	9'43	9'4	9'4	9'4	9'4	9'4	0
15	0	4147	17340	0517	3679	6825	29955	3070	36170	39255	42325	45379	48419	1
30	0	4200	17393	0570	3731	6877	30007	3122	36222	39306	42376	45430	48470	2
45	0	4253	17446	0623	3784	6929	30059	3174	36273	39358	42427	45481	48520	3
1	0	4307	17499	0676	3836	6982	30111	3226	36325	39409	42478	45532	48571	4
15	0	4360	17552	0728	3889	7034	30163	3277	36376	39460	42529	45583	48622	5
30	0	4413	17605	0781	3941	7086	30215	3329	36428	39511	42580	45633	48672	6
45	0	4467	17658	0834	3994	7138	30267	3381	36479	39563	42631	45684	48723	7
2	0	4520	17711	0887	4046	7191	30319	3433	36531	39614	42682	45735	48773	8
15	0	4573	17764	0940	4099	7243	30371	3484	36582	39665	42733	45786	48824	9
30	0	4627	17817	0992	4152	7295	30423	3536	36634	39716	42784	45836	48874	10
45	0	4680	17870	1045	4204	7347	30475	3588	36685	39768	42835	45887	48925	11
3	0	4733	17924	1098	4257	7400	30527	3640	36737	39819	42886	45938	48975	12
15	0	4787	17977	1151	4309	7452	30579	3691	36788	39870	42937	45989	49026	13
30	0	4840	18030	1203	4362	7504	30631	3743	36840	39921	42988	46039	49076	14
45	0	4893	18083	1256	4414	7556	30683	3795	36891	39973	43039	46090	49127	15
1	0	4946	18136	1309	4467	7609	30735	3847	36943	40024	43090	46141	49177	16
15	0	5000	18189	1362	4519	7661	30787	3898	36994	40075	43141	46192	49228	17
30	0	5053	18242	1414	4572	7713	30839	3950	37046	40126	43192	46242	49278	18
45	0	5106	18295	1467	4624	7765	30891	4002	37097	40177	43243	46293	49329	19
5	0	5160	18348	1520	4677	7817	30943	4054	37149	40229	43294	46344	49379	20
15	0	5213	18401	1573	4729	7870	30995	4105	37200	40280	43345	46394	49430	21
30	0	5266	18454	1625	4782	7922	31047	4157	37252	40331	43396	46445	49480	22
45	0	5319	18507	1678	4834	7974	31099	4209	37303	40382	43446	46496	49530	23
6	0	5373	18560	1731	4886	8026	31151	4260	37354	40433	43497	46546	49581	24
15	0	5426	18613	1784	4939	8079	31203	4312	37406	40485	43548	46597	49632	25
30	0	5479	18666	1836	4991	8131	31255	4364	37457	40536	43599	46648	49682	26
45	0	5532	18718	1889	5044	8183	31307	4415	37509	40587	43650	46699	49732	27
1	0	5586	18771	1942	5096	8235	31359	4467	37560	40638	43701	46749	49783	28
15	0	5639	18824	1994	5149	8287	31411	4519	37611	40689	43752	46800	49833	29
30	0	5692	18877	2047	5201	8340	31463	4570	37663	40741	43803	46851	49883	30
45	0	5745	18930	2100	5254	8392	31515	4622	37714	40791	43854	46901	49934	31
8	0	5798	18983	2152	5306	8444	31567	4674	37766	40843	43905	46952	49984	32
15	0	5852	19036	2205	5358	8496	31618	4725	37817	40894	43956	47003	50035	33
30	0	5905	19089	2258	5411	8548	31670	4777	37869	40945	44007	47053	50085	34
45	0	5958	19142	2311	5463	8600	31722	4829	37920	40996	44057	47104	50136	35
9	0	6011	19195	2363	5516	8653	31774	4880	37971	41047	44108	47155	50186	36
15	0	6064	19248	2416	5568	8705	31826	4932	38023	41099	44159	47205	50236	37
30	0	6118	19301	2469	5621	8757	31878	4984	38074	41150	44210	47256	50287	38
45	0	6171	19354	2521	5673	8809	31930	5035	38125	41201	44261	47306	50337	39
10	0	6224	19407	2574	5725	8861	31982	5087	38177	41252	44312	47357	50388	40
15	0	6277	19460	2627	5778	8913	32034	5139	38228	41303	44363	47408	50438	41
30	0	6330	19513	2679	5830	8966	32085	5190	38280	41354	44414	47458	50488	42
45	0	6384	19566	2732	5882	9018	32137	5242	38331	41405	44465	47509	50539	43
11	0	6437	19618	2784	5935	9070	32189	5293	38382	41456	44515	47560	50589	44
15	0	6490	19671	2837	5987	9122	32241	5345	38434	41507	44566	47610	50639	45
30	0	6543	19724	2890	6040	9174	32293	5397	38485	41559	44617	47661	50690	46
45	0	6596	19777	2942	6092	9226	32345	5448	38536	41610	44668	47711	50740	47
12	0	6649	19830	2995	6144	9278	32397	5500	38588	41661	44719	47762	50790	48
15	0	6702	19883	3048	6197	9330	32449	5551	38639	41712	44770	47813	50841	49
30	0	6756	19936	3100	6249	9382	32500	5603	38691	41763	44821	47863	50891	50
45	0	6809	19989	3153	6301	9434	32552	5655	38742	41814	44871	47914	50941	51
13	0	6862	20042	3205	6354	9487	32604	5706	38793	41865	44922	47964	50992	52
15	0	6915	20094	3258	6406	9539	32656	5758	38844	41916	44973	48015	51042	53
30	0	6968	20147	3311	6458	9591	32708	5809	38896	41967	45024	48065	51092	54
45	0	7021	20200	3363	6511	9643	32759	5861	38947	42018	45075	48116	51143	55
14	0	7074	20253	3416	6563	9695	32811	5912	38998	42069	45125	48167	51193	56
15	0	7127	20306	3468	6615	9747	32863	5964	39050	42120	45176	48217	51243	57
30	0	7181	20359	3521	6668	9799	32915	6016	39101	42172	45227	48268	51294	58
45	0	7234	20411	3573	6720	9851	32967	6067	39152	42223	45278	48318	51344	59
15	0	7287	20464	3626	6772	9903	33018	6119	39204	42274	45329	48369	51394	60

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 53. Parts 3 7 11 14 18 21 25 28 32 35 39 42 46 49 53

D. 50. Parts 3 7 10 13 17 20 23 27 30 33 37 40 43 47 50

LOG. SINE SQUARE

		64°			65°				66°				s.
		15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	
		4 ^h 17 ^m	4 ^h 18 ^m	4 ^h 19 ^m	4 ^h 20 ^m	4 ^h 21 ^m	4 ^h 22 ^m	4 ^h 23 ^m	4 ^h 24 ^m	4 ^h 25 ^m	4 ^h 26 ^m	4 ^h 27 ^m	
		9'4	9'4	9'4	9'4	9'4	9'4	9'4	9'4	9'4	9'4	9'4	
0	0	51445	54455	57451	60433	63400	66353	69293	72218	75128	78026	80909	0
	15	51495	54505	57501	60483	63450	66403	69341	72266	75177	78074	80957	1
	30	51546	54555	57551	60532	63499	66452	69390	72315	75225	78122	81005	2
	45	51596	54605	57601	60582	63548	66501	69439	72363	75274	78170	81053	3
1	0	51646	54655	57651	60631	63598	66550	69488	72412	75322	78218	81101	4
	15	51696	54706	57700	60681	63647	66599	69537	72461	75371	78267	81149	5
	30	51746	54756	57750	60730	63696	66648	69586	72509	75419	78315	81197	6
	45	51797	54806	57800	60780	63746	66697	69635	72558	75467	78363	81245	7
2	0	51847	54856	57850	60829	63795	66746	69683	72606	75516	78411	81293	8
	15	51897	54906	57900	60879	63844	66795	69732	72655	75564	78459	81341	9
3	0	51947	54956	57949	60929	63894	66844	69781	72704	75612	78507	81388	10
	15	51998	55006	57999	60978	63943	66893	69830	72752	75661	78555	81436	11
	30	52048	55056	58049	61028	63992	66942	69879	72801	75709	78604	81484	12
	45	52098	55106	58099	61077	64041	66992	69927	72849	75757	78652	81532	13
4	0	52148	55156	58148	61127	64091	67041	69976	72898	75806	78700	81580	14
	15	52199	55206	58198	61176	64140	67090	70025	72947	75854	78748	81628	15
	30	52249	55256	58248	61226	64189	67139	70074	72995	75902	78796	81676	16
	45	52299	55306	58298	61275	64239	67188	70123	73044	75951	78844	81724	17
5	0	52349	55356	58347	61325	64288	67237	70171	73092	75999	78892	81771	18
	15	52400	55406	58397	61374	64337	67286	70220	73141	76047	78940	81819	19
6	0	52450	55456	58447	61424	64386	67335	70269	73189	76096	78988	81867	20
	15	52500	55506	58497	61473	64436	67384	70318	73238	76144	79036	81915	21
	30	52550	55556	58546	61523	64485	67433	70366	73286	76192	79085	81963	22
	45	52600	55605	58596	61572	64534	67482	70415	73335	76241	79133	82011	23
7	0	52651	55655	58646	61622	64583	67531	70464	73384	76289	79181	82059	24
	15	52701	55705	58695	61671	64633	67580	70513	73432	76337	79229	82107	25
	30	52751	55755	58745	61721	64682	67629	70562	73481	76386	79277	82154	26
	45	52801	55805	58795	61770	64731	67678	70610	73529	76434	79325	82202	27
8	0	52851	55855	58845	61820	64780	67727	70659	73578	76482	79373	82250	28
	15	52902	55905	58894	61869	64830	67776	70708	73626	76531	79421	82298	29
9	0	52952	55955	58944	61918	64879	67825	70757	73675	76579	79469	82346	30
	15	53002	56005	58994	61968	64928	67874	70806	73723	76627	79517	82394	31
	30	53052	56055	59043	62017	64977	67923	70854	73772	76675	79565	82441	32
	45	53102	56105	59093	62067	65026	67972	70903	73820	76724	79613	82489	33
10	0	53152	56155	59143	62116	65076	68021	70952	73869	76772	79661	82537	34
	15	53202	56205	59192	62166	65125	68070	71000	73917	76820	79709	82585	35
	30	53252	56255	59242	62215	65174	68119	71049	73966	76869	79758	82633	36
	45	53303	56305	59292	62265	65223	68168	71098	74014	76917	79806	82680	37
11	0	53353	56354	59341	62314	65272	68217	71147	74063	76965	79854	82728	38
	15	53403	56404	59391	62363	65322	68265	71195	74111	77013	79902	82776	39
12	0	53453	56454	59441	62413	65371	68314	71244	74160	77062	79950	82824	40
	15	53503	56504	59490	62462	65420	68363	71293	74208	77110	79998	82872	41
	30	53554	56554	59540	62512	65469	68412	71342	74257	77158	80046	82919	42
	45	53604	56604	59590	62561	65518	68461	71390	74305	77206	80094	82967	43
13	0	53654	56654	59639	62610	65567	68510	71439	74354	77254	80142	83015	44
	15	53704	56704	59689	62660	65617	68559	71488	74402	77303	80190	83063	45
	30	53754	56754	59739	62709	65666	68608	71536	74451	77351	80238	83110	46
	45	53804	56803	59788	62759	65715	68657	71585	74499	77399	80286	83158	47
14	0	53854	56853	59838	62808	65764	68706	71634	74547	77447	80334	83206	48
	15	53904	56903	59887	62857	65813	68755	71682	74596	77496	80382	83254	49
15	0	53954	56953	59937	62907	65862	68804	71731	74644	77544	80430	83302	50
	15	54005	57003	59987	62956	65911	68853	71780	74693	77592	80478	83349	51
	30	54055	57053	60036	63006	65960	68901	71828	74741	77640	80526	83397	52
	45	54105	57103	60086	63055	66010	68950	71877	74790	77688	80573	83445	53
16	0	54155	57152	60135	63104	66059	68999	71926	74838	77737	80621	83493	54
	15	54205	57202	60185	63154	66108	69048	71974	74886	77785	80669	83540	55
	30	54255	57252	60235	63203	66157	69097	72023	74935	77833	80717	83588	56
	45	54305	57302	60284	63252	66206	69146	72072	74983	77881	80765	83636	57
17	0	54355	57352	60334	63302	66255	69195	72120	75032	77929	80813	83684	58
	15	54405	57402	60383	63351	66304	69244	72169	75080	77978	80861	83731	59

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 50. Parts 3 7 10 13 17 20 23 27 30 33 37 40 43 47 50

D. 48. Parts 3 6 10 13 16 19 22 26 29 32 35 38 42 45 48

TABLE 69

LOG. SINE SQUARE													
	67°				68°				69°				a.
	0'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'		
	4 28"	4 29"	4 30"	4 31"	4 32"	4 33"	4 34"	4 35"	4 36"	4 37"	4 38"		
0	9'4	9'4	9'4	9'4	9'4	9'	9'5	9'5	9'5	9'5	9'5	0	
15	83779	86635	89478	92307	95123	97926	00716	03492	06256	09007	11745	1	
30	83827	86683	89525	92354	95170	97973	00762	03539	06302	09053	11790	2	
45	83874	86730	89572	92401	95217	98019	00809	03585	06348	09098	11836	3	
1	83922	86778	89620	92448	95264	98066	00855	03631	06394	09144	11881	4	
15	83970	86825	89667	92495	95311	98112	00901	03677	06440	09190	11927	5	
30	84017	86873	89714	92542	95357	98159	00948	03723	06486	09235	11972	6	
45	84065	86920	89761	92589	95404	98206	00994	03769	06532	09281	12018	7	
2	84113	86968	89809	92636	95451	98252	01040	03815	06578	09327	12065	8	
15	84161	87015	89856	92683	95498	98299	01087	03862	06624	09373	12109	9	
30	84208	87062	89903	92730	95545	98345	01133	03908	06669	09418	12154	10	
45	84256	87110	89950	92778	95591	98392	01179	03954	06715	09464	12200	11	
3	84304	87157	90008	92825	95638	98438	01226	04000	06761	09510	12245	12	
15	84351	87205	90055	92871	95685	98485	01272	04046	06807	09555	12291	13	
30	84399	87252	90092	92919	95732	98532	01318	04092	06853	09601	12336	14	
45	84447	87300	90139	92966	95778	98578	01365	04138	06899	09647	12382	15	
1	84494	87347	90186	93012	95825	98625	01411	04184	06945	09692	12427	16	
15	84542	87395	90234	93059	95872	98671	01457	04231	06991	09738	12473	17	
30	84590	87442	90281	93106	95919	98718	01504	04277	07037	09784	12518	18	
45	84637	87489	90328	93153	95965	98764	01550	04323	07083	09830	12564	19	
2	84685	87537	90375	93200	96012	98811	01596	04369	07128	09875	12609	20	
15	84733	87584	90423	93247	96059	98857	01643	04415	07174	09921	12655	21	
30	84780	87632	90470	93294	96106	98904	01689	04461	07220	09967	12700	22	
45	84828	87679	90517	93341	96152	98951	01735	04507	07266	10012	12745	23	
3	84875	87726	90564	93388	96199	98997	01782	04553	07312	10058	12791	24	
15	84923	87774	90611	93435	96246	99044	01828	04599	07358	10103	12836	25	
30	84971	87821	90658	93482	96293	99090	01874	04645	07404	10149	12882	26	
45	85018	87869	90706	93529	96339	99137	01921	04692	07450	10195	12927	27	
1	85066	87916	90753	93576	96386	99183	01967	04738	07495	10240	12973	28	
15	85114	87963	90800	93623	96433	99230	02013	04784	07541	10286	13018	29	
30	85161	88011	90848	93670	96480	99276	02059	04830	07587	10332	13064	30	
45	85209	88058	90894	93717	96526	99323	02106	04876	07633	10377	13109	31	
3	85256	88106	90941	93764	96573	99369	02152	04922	07679	10423	13154	32	
15	85304	88153	90989	93811	96620	99416	02198	04968	07725	10469	13200	33	
30	85352	88200	91036	93858	96666	99462	02245	05014	07771	10514	13245	34	
45	85399	88248	91083	93905	96713	99509	02291	05060	07816	10560	13291	35	
1	85447	88295	91130	93952	96760	99555	02337	05106	07862	10606	13336	36	
15	85494	88342	91177	93998	96807	99601	02383	05152	07908	10651	13381	37	
30	85542	88390	91224	94045	96853	99648	02430	05198	07954	10697	13427	38	
45	85589	88437	91271	94092	96900	99694	02476	05244	08000	10742	13472	39	
2	85637	88485	91318	94139	96947	99741	02522	05290	08045	10788	13518	40	
15	85685	88532	91366	94186	96993	99787	02568	05336	08091	10833	13563	41	
30	85732	88579	91413	94233	97040	99834	02615	05382	08137	10879	13608	42	
45	85780	88627	91460	94280	97087	99880	02661	05428	08183	10925	13654	43	
3	85827	88674	91507	94327	97133	99927	02707	05474	08229	10970	13699	44	
15	85875	88721	91554	94374	97180	99973	02753	05520	08274	11016	13744	45	
30	85922	88769	91601	94421	97227	500020	02799	05566	08320	11061	13790	46	
45	85970	88816	91648	94467	97273	500066	02846	05612	08366	11107	13835	47	
1	86017	88863	91695	94514	97320	500112	02892	05658	08412	11153	13881	48	
15	86065	88910	91742	94561	97367	500159	02938	05704	08458	11198	13926	49	
30	86113	88958	91790	94608	97413	500205	02984	05750	08503	11244	13971	50	
45	86160	89005	91837	94655	97460	500252	03030	05796	08549	11289	14017	51	
3	86208	89052	91884	94702	97507	500298	03077	05842	08595	11335	14062	52	
15	86255	89100	91931	94749	97553	500345	03123	05888	08641	11380	14107	53	
30	86303	89147	91978	94795	97600	500391	03169	05934	08687	11426	14153	54	
45	86350	89194	92025	94842	97646	500437	03215	05980	08732	11471	14198	55	
1	86398	89242	92072	94889	97693	500484	03261	06026	08778	11517	14243	56	
15	86445	89289	92119	94936	97740	500530	03308	06072	08824	11563	14289	57	
30	86493	89336	92166	94983	97786	500577	03354	06118	08870	11608	14334	58	
45	86540	89383	92213	95030	97833	500623	03400	06164	08915	11654	14379	59	
2	86588	89431	92260	95077	97879	500669	03446	06210	08961	11699	14425	60	
Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'													
D. 48. Parts 3 6 10 13 16 19 22 26 29 32 35 38 42 45 48													
D. 48. Parts 3 6 9 12 15 18 21 25 28 31 34 37 40 43 46													

LOG. SINE SQUARE

	69°												n.
	70°				71°				72°				
	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'	15'		
	4° 30'	4° 40'	4° 41'	4° 42'	4° 43'	4° 44'	4° 45'	4° 46'	4° 47'	4° 48'	4° 49'		
0 0	9'5	9'5	9'5	9'5	9'5	9'5	9'5	9'5	9'5	9'5	9'5	0	
15	14470	17183	19883	22570	25245	27908	30559	33197	35823	38437	41040	1	
30	14515	17228	19927	22615	25290	27952	30603	33241	35867	38481	41083	2	
45	14561	17273	19972	22659	25334	27997	30647	33285	35910	38524	41126	3	
1 0	14606	17318	20017	22704	25379	28041	30691	33329	35954	38568	41169	4	
15	14651	17363	20062	22749	25423	28085	30735	33372	35998	38611	41213	5	
30	14696	17408	20107	22794	25468	28129	30779	33416	36041	38655	41256	6	
45	14742	17453	20152	22838	25512	28174	30823	33460	36085	38698	41299	7	
2 0	14787	17498	20197	22883	25557	28218	30867	33504	36129	38742	41342	8	
15	14832	17543	20242	22928	25601	28262	30911	33548	36172	38785	41386	9	
30	14878	17588	20287	22972	25645	28306	30955	33592	36216	38828	41429	10	
45	14923	17633	20331	23017	25690	28351	30999	33635	36260	38872	41472	11	
3 0	14968	17678	20376	23062	25734	28395	31043	33679	36303	38915	41515	12	
15	15014	17724	20421	23106	25779	28439	31087	33723	36347	38959	41559	13	
30	15059	17769	20466	23151	25823	28483	31131	33767	36391	39002	41602	14	
45	15104	17814	20511	23195	25868	28528	31175	33811	36434	39046	41645	15	
4 0	15149	17859	20556	23240	25912	28572	31219	33854	36478	39089	41688	16	
15	15195	17904	20600	23285	25957	28616	31263	33898	36521	39132	41731	17	
30	15240	17949	20645	23329	26001	28660	31307	33942	36565	39176	41775	18	
45	15285	17994	20690	23374	26045	28704	31351	33986	36609	39219	41818	19	
5 0	15330	18039	20735	23419	26090	28749	31395	34030	36652	39263	41861	20	
15	15376	18084	20780	23463	26134	28793	31439	34074	36696	39306	41904	21	
30	15421	18129	20825	23508	26179	28837	31483	34117	36740	39349	41948	22	
45	15466	18174	20869	23552	26223	28881	31527	34161	36783	39393	41991	23	
6 0	15511	18219	20914	23597	26267	28926	31571	34205	36827	39436	42034	24	
15	15557	18264	20959	23642	26312	28970	31615	34249	36870	39480	42077	25	
30	15602	18309	21004	23686	26356	29014	31659	34293	36914	39523	42120	26	
45	15647	18354	21049	23731	26401	29058	31703	34336	36957	39566	42164	27	
7 0	15692	18399	21094	23775	26445	29102	31747	34380	37001	39610	42207	28	
15	15737	18444	21138	23820	26489	29146	31791	34424	37045	39653	42250	29	
30	15783	18489	21183	23865	26534	29191	31835	34468	37088	39697	42293	30	
45	15828	18534	21228	23909	26578	29235	31879	34511	37132	39740	42336	31	
8 0	15873	18579	21273	23954	26623	29279	31923	34555	37175	39783	42379	32	
15	15918	18624	21317	23998	26667	29323	31967	34599	37219	39827	42423	33	
30	15963	18669	21362	24043	26711	29367	32011	34643	37262	39870	42466	34	
45	16009	18714	21407	24087	26756	29411	32055	34687	37306	39913	42509	35	
9 0	16054	18759	21452	24132	26800	29456	32099	34730	37350	39957	42552	36	
15	16099	18804	21497	24177	26844	29500	32143	34774	37393	40000	42595	37	
30	16144	18849	21541	24221	26889	29544	32187	34818	37437	40043	42638	38	
45	16189	18894	21586	24266	26933	29588	32231	34862	37480	40087	42681	39	
10 0	16235	18939	21631	24310	26977	29632	32275	34905	37524	40130	42725	40	
15	16280	18984	21676	24355	27022	29676	32319	34949	37567	40173	42768	41	
30	16325	19029	21720	24400	27066	29721	32363	34993	37611	40217	42811	42	
45	16370	19074	21765	24444	27110	29765	32407	35037	37654	40260	42854	43	
11 0	16415	19119	21810	24489	27155	29809	32451	35080	37698	40304	42897	44	
15	16460	19164	21855	24533	27199	29853	32495	35124	37741	40347	42940	45	
30	16506	19209	21899	24578	27244	29897	32538	35168	37785	40390	42983	46	
45	16551	19254	21944	24622	27288	29941	32582	35211	37828	40434	43027	47	
12 0	16596	19299	21989	24667	27332	29985	32626	35255	37872	40477	43070	48	
15	16641	19344	22034	24711	27376	30029	32670	35299	37915	40520	43113	49	
30	16686	19389	22078	24756	27421	30074	32714	35343	37959	40563	43156	50	
45	16731	19433	22123	24800	27465	30118	32758	35386	38002	40607	43199	51	
13 0	16777	19478	22168	24845	27509	30162	32802	35430	38046	40650	43242	52	
15	16822	19523	22213	24889	27554	30206	32846	35474	38089	40693	43285	53	
30	16867	19568	22257	24934	27598	30250	32890	35517	38133	40737	43328	54	
45	16912	19613	22302	24978	27642	30294	32934	35561	38176	40780	43371	55	
14 0	16957	19658	22347	25023	27687	30338	32978	35605	38220	40823	43414	56	
15	17002	19703	22391	25067	27731	30382	33021	35648	38263	40866	43458	57	
30	17047	19748	22436	25112	27775	30426	33065	35692	38307	40910	43501	58	
45	17092	19793	22481	25156	27819	30470	33109	35736	38350	40953	43544	59	
15	17137	19838	22525	25201	27864	30514	33153	35779	38394	40996	43587	60	

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 43. Parts 3 6 9 12 15 18 21 24 27 30 33 36 39 42 45

D. 43. Parts 3 6 9 12 14 17 20 23 26 29 32 35 37 40 43

LOG. SINE SQUARE

	75°			76°			77°			n.		
	15'	30'	45'	0'	15'	30'	45'	5'	15'	30'	45'	
	h 1m	h 2m	h 3m	h 4m	h 5m	h 6m	h 7m	h 8m	h 9m	h 10m	h 11m	
0	9'5	9'5	9'5	9'5	9'5	9'5	9'5	9'5	9'5	9'5	9'5	0
15	71358	73811	76253	78684	81104	83513	85911	88299	90676	93042	95398	1
30	71399	73852	76294	78724	81144	83553	85951	88339	90716	93082	95437	2
45	71440	73893	76334	78765	81185	83593	85991	88379	90755	93121	95476	3
1 0	71481	73933	76375	78805	81225	83633	86031	88418	90795	93161	95516	4
15	71522	73974	76415	78846	81265	83673	86071	88458	90834	93200	95555	5
30	71563	74015	76456	78886	81305	83713	86111	88498	90874	93239	95594	6
45	71604	74056	76497	78926	81345	83753	86151	88537	90913	93279	95633	7
2 0	71645	74097	76537	78967	81386	83793	86191	88577	90953	93318	95672	8
15	71686	74137	76578	79007	81426	83834	86230	88616	90992	93357	95712	9
30	71727	74178	76618	79048	81466	83874	86270	88656	91032	93397	95751	10
45	71768	74219	76659	79088	81506	83914	86310	88696	91071	93436	95790	11
3 0	71809	74260	76700	79128	81546	83954	86350	88736	91111	93475	95829	12
15	71850	74300	76740	79169	81587	83994	86390	88775	91150	93514	95868	13
30	71891	74341	76781	79209	81627	84034	86430	88815	91190	93554	95907	14
45	71932	74382	76821	79250	81667	84074	86470	88855	91229	93593	95946	15
4 0	71973	74423	76862	79290	81707	84114	86509	88894	91269	93632	95986	16
15	72013	74463	76902	79330	81747	84154	86549	88934	91308	93672	96025	17
30	72054	74504	76943	79371	81788	84194	86589	88974	91348	93711	96064	18
45	72095	74545	76983	79411	81828	84234	86629	89013	91387	93750	96103	19
5 0	72136	74586	77024	79451	81868	84274	86669	89053	91427	93790	96142	20
15	72177	74626	77065	79492	81908	84314	86709	89093	91466	93829	96181	21
30	72218	74667	77105	79532	81948	84354	86748	89132	91506	93868	96220	22
45	72259	74708	77146	79573	81989	84394	86788	89172	91545	93907	96259	23
6 0	72300	74748	77186	79613	82029	84434	86828	89212	91584	93947	96298	24
15	72341	74789	77227	79653	82069	84474	86868	89251	91624	93986	96338	25
30	72382	74830	77267	79694	82109	84514	86908	89291	91663	94025	96377	26
45	72423	74871	77308	79734	82149	84554	86947	89330	91703	94065	96416	27
7 0	72463	74911	77348	79774	82189	84594	86987	89370	91742	94104	96455	28
15	72504	74952	77389	79815	82230	84634	87027	89410	91782	94143	96494	29
30	72545	74993	77429	79855	82270	84674	87067	89449	91821	94182	96533	30
45	72586	75033	77470	79895	82310	84714	87107	89489	91861	94222	96572	31
8 0	72627	75074	77510	79936	82350	84754	87146	89529	91900	94261	96611	32
15	72668	75115	77551	79976	82390	84794	87186	89568	91939	94300	96650	33
30	72709	75156	77591	80016	82430	84834	87226	89608	91979	94339	96689	34
45	72750	75196	77632	80057	82470	84874	87266	89647	92018	94379	96729	35
9 0	72791	75237	77672	80097	82511	84913	87306	89687	92058	94418	96768	36
15	72831	75277	77713	80137	82551	84953	87345	89727	92097	94457	96807	37
30	72872	75318	77754	80178	82591	84993	87385	89766	92137	94496	96846	38
45	72913	75359	77794	80218	82631	85033	87425	89806	92176	94536	96885	39
10 0	72954	75400	77834	80258	82671	85073	87465	89845	92215	94575	96924	40
15	72995	75440	77875	80298	82711	85113	87504	89885	92255	94614	96963	41
30	73036	75481	77915	80339	82751	85153	87544	89925	92294	94653	97002	42
45	73076	75522	77956	80379	82791	85193	87584	89964	92334	94693	97041	43
11 0	73117	75562	77996	80419	82832	85233	87624	90004	92373	94732	97080	44
15	73158	75603	78037	80460	82872	85273	87663	90043	92412	94771	97119	45
30	73199	75644	78077	80500	82912	85313	87703	90083	92452	94810	97158	46
45	73240	75684	78118	80540	82952	85353	87743	90122	92491	94850	97197	47
12 0	73281	75725	78158	80581	82992	85393	87783	90162	92531	94889	97236	48
15	73321	75766	78199	80621	83032	85433	87822	90202	92570	94928	97275	49
30	73362	75806	78239	80661	83072	85473	87862	90241	92609	94967	97314	50
45	73403	75847	78279	80701	83112	85513	87902	90281	92649	95006	97353	51
13 0	73444	75887	78320	80742	83152	85552	87942	90320	92688	95046	97392	52
15	73485	75928	78360	80782	83193	85592	87981	90360	92728	95085	97432	53
30	73526	75969	78401	80822	83233	85632	88021	90399	92767	95124	97471	54
45	73566	76009	78441	80862	83273	85672	88061	90439	92806	95163	97510	55
14 0	73607	76050	78482	80903	83313	85712	88101	90478	92846	95202	97549	56
15	73648	76091	78522	80943	83353	85752	88140	90518	92885	95242	97588	57
30	73689	76131	78563	80983	83393	85792	88180	90558	92924	95281	97627	58
45	73730	76172	78603	81023	83433	85832	88220	90597	92964	95320	97666	59
15	73770	76212	78644	81064	83473	85872	88259	90637	93003	95359	97705	60

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 41. Parts 3 5 8 11 14 16 19 22 24 27 30 33 35 38 41

D. 39. Parts 3 5 8 10 13 15 18 21 23 26 29 31 33 36 39

LOG. SINE SQUARE

		78°				79°				80°			a.
		0'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	
		5 ^h 12 ^m	5 ^h 13 ^m	5 ^h 14 ^m	5 ^h 15 ^m	5 ^h 16 ^m	5 ^h 17 ^m	5 ^h 18 ^m	5 ^h 19 ^m	5 ^h 20 ^m	5 ^h 21 ^m	5 ^h 22 ^m	
0	0	977744	00078	02403	04717	07021	09315	11598	13872	16135	18388	20632	0
1	0	977783	00117	02442	04756	07059	09353	11636	13909	16173	18426	20669	1
2	0	977822	00156	02480	04794	07098	09391	11674	13947	16210	18463	20706	2
3	0	977861	00195	02519	04833	07136	09429	11712	13985	16248	18501	20744	3
4	0	977900	00234	02558	04871	07174	09467	11750	14023	16285	18538	20781	4
5	0	977939	00273	02596	04910	07213	09505	11788	14061	16323	18576	20818	5
6	0	977978	00311	02635	04948	07251	09544	11826	14098	16361	18613	20855	6
7	0	978017	00350	02674	04986	07289	09582	11864	14136	16398	18651	20893	7
8	0	978056	00389	02712	05025	07327	09620	11902	14174	16436	18688	20930	8
9	0	978095	00428	02751	05063	07366	09658	11940	14212	16474	18725	20967	9
10	0	978133	00467	02789	05102	07404	09696	11978	14250	16511	18763	21005	10
11	0	978171	00505	02828	05140	07442	09734	12016	14287	16549	18800	21042	11
12	0	978210	00544	02867	05179	07481	09772	12054	14325	16586	18838	21079	12
13	0	978249	00583	02905	05217	07519	09810	12092	14363	16624	18875	21116	13
14	0	978288	00622	02944	05256	07557	09848	12130	14401	16662	18913	21154	14
15	0	978327	00661	02982	05294	07595	09886	12168	14438	16699	18950	21191	15
16	0	978367	00699	03021	05332	07634	09925	12205	14476	16737	18987	21228	16
17	0	978406	00738	03060	05371	07672	09963	12243	14514	16774	19025	21266	17
18	0	978445	00777	03098	05409	07710	10001	12281	14552	16812	19062	21303	18
19	0	978484	00816	03137	05448	07748	10039	12319	14589	16850	19100	21340	19
20	0	978523	00854	03175	05486	07787	10077	12357	14627	16887	19137	21377	20
21	0	978562	00893	03214	05525	07825	10115	12395	14665	16925	19175	21415	21
22	0	978601	00932	03253	05563	07863	10153	12433	14703	16962	19212	21452	22
23	0	978640	00971	03291	05602	07901	10191	12471	14740	17000	19249	21489	23
24	0	978679	01009	03330	05640	07940	10229	12509	14778	17037	19287	21526	24
25	0	978718	01048	03368	05678	07978	10267	12547	14816	17075	19324	21564	25
26	0	978757	01087	03407	05717	08016	10305	12585	14854	17113	19362	21601	26
27	0	978796	01126	03446	05755	08054	10343	12622	14891	17150	19399	21638	27
28	0	978834	01164	03484	05794	08093	10381	12660	14929	17188	19436	21675	28
29	0	978873	01203	03523	05832	08131	10419	12698	14967	17225	19474	21712	29
30	0	978912	01242	03561	05870	08169	10458	12736	15005	17263	19511	21749	30
31	0	978951	01281	03600	05909	08207	10496	12774	15042	17300	19549	21787	31
32	0	978990	01319	03638	05947	08246	10534	12812	15080	17338	19586	21824	32
33	0	979029	01358	03677	05986	08284	10572	12850	15118	17376	19623	21861	33
34	0	979068	01397	03716	06024	08322	10610	12888	15155	17413	19661	21899	34
35	0	979107	01436	03754	06062	08360	10648	12926	15193	17451	19698	21936	35
36	0	979146	01474	03793	06101	08398	10686	12963	15231	17488	19736	21973	36
37	0	979185	01513	03831	06139	08437	10724	13001	15269	17526	19773	22010	37
38	0	979224	01552	03870	06177	08475	10762	13039	15306	17563	19810	22047	38
39	0	979262	01591	03908	06216	08513	10800	13077	15344	17601	19848	22085	39
40	0	979301	01629	03947	06254	08551	10838	13115	15383	17638	19885	22122	40
41	0	979340	01668	03986	06293	08589	10876	13153	15421	17676	19922	22159	41
42	0	979379	01707	04024	06331	08628	10914	13191	15457	17713	19960	22196	42
43	0	979418	01745	04063	06369	08666	10952	13229	15495	17751	19997	22233	43
44	0	979457	01784	04101	06408	08704	10990	13266	15532	17788	20034	22271	44
45	0	979496	01823	04140	06446	08742	11028	13304	15570	17826	20072	22308	45
46	0	979535	01861	04178	06484	08780	11066	13342	15608	17863	20109	22345	46
47	0	979574	01900	04217	06523	08819	11104	13380	15645	17901	20146	22382	47
48	0	979612	01939	04255	06561	08857	11142	13418	15683	17938	20184	22419	48
49	0	979651	01978	04294	06599	08895	11180	13456	15721	17976	20221	22456	49
50	0	979690	02016	04332	06638	08933	11218	13493	15758	18013	20258	22494	50
51	0	979729	02055	04371	06676	08971	11256	13531	15796	18051	20296	22531	51
52	0	979768	02094	04409	06714	09009	11294	13569	15834	18088	20333	22568	52
53	0	979807	02132	04448	06753	09048	11332	13607	15871	18126	20371	22605	53
54	0	979846	02171	04486	06791	09086	11370	13645	15909	18163	20408	22642	54
55	0	979884	02210	04525	06829	09124	11408	13683	15947	18201	20445	22679	55
56	0	979923	02248	04563	06868	09162	11446	13720	15984	18238	20482	22717	56
57	0	979962	02287	04602	06906	09200	11484	13758	16022	18276	20520	22754	57
58	0	600001	02326	04640	06944	09238	11522	13796	16060	18313	20557	22791	58
59	0	600040	02364	04679	06983	09277	11560	13834	16097	18351	20594	22828	59

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 30. Parts 3 5 8 10 13 15 18 21 23 26 29 31 33 36 39

D. 37. Parts 2 5 7 10 12 15 17 20 22 25 27 29 32 34 37

LOG. SINE SQUARE													
	83°		84°				85°				86°		c.
	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'		
	83 34"	83 35"	84 36"	84 37"	84 38"	84 39"	85 40"	85 41"	85 42"	85 43"	85 44"		
0	9'6	9'6	9'6	9'6	9'6	9'6	9'6	9'6	9'6	9'6	9'6		
1	46794	48913	51022	53122	55212	57294	59367	61430	63485	65530	67567	0	
2	46829	48948	51057	53157	55247	57329	59401	61464	63519	65564	67601	1	
3	46865	48983	51092	53192	55282	57363	59436	61499	63553	65598	67634	2	
4	46900	49018	51127	53226	55317	57398	59470	61533	63587	65632	67668	3	
5	46936	49053	51162	53261	55352	57433	59504	61567	63621	65666	67702	4	
6	46971	49089	51197	53296	55386	57467	59539	61602	63655	65700	67736	5	
7	47006	49124	51232	53331	55421	57502	59573	61636	63690	65734	67770	6	
8	47042	49159	51267	53366	55456	57536	59608	61670	63724	65768	67804	7	
9	47077	49194	51302	53401	55491	57571	59642	61705	63758	65802	67837	8	
10	47113	49230	51337	53436	55525	57606	59677	61739	63792	65836	67871	9	
11	47148	49265	51372	53471	55560	57640	59711	61773	63826	65870	67905	10	
12	47183	49300	51407	53506	55595	57675	59746	61807	63860	65904	67939	11	
13	47219	49335	51442	53541	55630	57709	59780	61842	63894	65938	67973	12	
14	47254	49370	51478	53575	55664	57744	59815	61876	63929	65972	68007	13	
15	47289	49406	51513	53610	55699	57779	59849	61910	63963	66006	68041	14	
16	47325	49441	51548	53645	55734	57813	59883	61945	63997	66040	68074	15	
17	47360	49476	51583	53680	55768	57848	59918	61979	64031	66074	68108	16	
18	47395	49511	51618	53715	55803	57882	59952	62013	64065	66108	68142	17	
19	47431	49546	51653	53750	55838	57917	59987	62047	64099	66142	68176	18	
20	47466	49582	51688	53785	55873	57951	60021	62082	64133	66176	68210	19	
21	47501	49617	51723	53820	55907	57986	60055	62116	64167	66210	68243	20	
22	47537	49652	51758	53855	55942	58021	60090	62150	64201	66244	68277	21	
23	47572	49687	51793	53889	55977	58055	60124	62184	64236	66278	68311	22	
24	47607	49722	51828	53924	56012	58090	60159	62219	64270	66312	68345	23	
25	47643	49757	51862	53959	56046	58124	60193	62253	64304	66346	68379	24	
26	47678	49793	51898	53994	56081	58159	60228	62287	64338	66380	68413	25	
27	47713	49828	51933	54029	56116	58193	60262	62321	64372	66414	68446	26	
28	47749	49863	51968	54064	56150	58228	60296	62356	64406	66448	68480	27	
29	47784	49898	52003	54099	56185	58262	60331	62390	64440	66482	68514	28	
30	47819	49933	52038	54133	56220	58297	60365	62424	64474	66516	68548	29	
31	47854	49968	52073	54168	56254	58332	60400	62458	64508	66550	68582	30	
32	47890	50003	52108	54203	56289	58366	60434	62493	64543	66584	68615	31	
33	47925	50039	52143	54238	56324	58401	60468	62527	64577	66617	68649	32	
34	47960	50074	52178	54273	56359	58435	60503	62561	64611	66651	68683	33	
35	47996	50109	52213	54308	56393	58470	60537	62595	64645	66685	68717	34	
36	48031	50144	52248	54343	56428	58504	60571	62630	64679	66719	68751	35	
37	48066	50179	52283	54377	56463	58539	60606	62664	64713	66753	68784	36	
38	48102	50214	52318	54412	56497	58573	60640	62698	64747	66787	68818	37	
39	48137	50249	52353	54447	56532	58608	60675	62732	64781	66821	68852	38	
40	48172	50285	52388	54482	56567	58642	60709	62767	64815	66855	68886	39	
41	48207	50320	52423	54517	56601	58677	60743	62801	64849	66889	68919	40	
42	48243	50355	52458	54551	56636	58711	60778	62835	64883	66923	68953	41	
43	48278	50390	52493	54586	56671	58746	60812	62869	64917	66957	68987	42	
44	48313	50425	52528	54621	56705	58780	60846	62903	64951	66991	69021	43	
45	48349	50460	52563	54656	56740	58815	60881	62938	64985	67024	69054	44	
46	48384	50495	52598	54691	56775	58849	60915	62972	65020	67058	69088	45	
47	48419	50530	52633	54725	56809	58884	60949	63006	65054	67092	69122	46	
48	48454	50566	52668	54760	56844	58918	60984	63040	65088	67126	69156	47	
49	48490	50601	52702	54795	56879	58953	61018	63074	65122	67160	69189	48	
50	48525	50636	52737	54830	56913	58987	61053	63109	65156	67194	69223	49	
51	48560	50671	52772	54865	56948	59022	61087	63143	65190	67228	69257	50	
52	48595	50706	52807	54900	56982	59056	61121	63177	65224	67262	69291	51	
53	48631	50741	52842	54934	57017	59091	61156	63211	65258	67296	69324	52	
54	48666	50776	52877	54969	57052	59125	61190	63245	65292	67329	69358	53	
55	48701	50811	52912	55004	57086	59160	61224	63280	65326	67363	69392	54	
56	48736	50846	52947	55039	57121	59194	61259	63314	65360	67397	69426	55	
57	48772	50881	52982	55073	57156	59229	61293	63348	65394	67431	69459	56	
58	48807	50917	53017	55108	57190	59263	61327	63382	65428	67465	69493	57	
59	48842	50952	53052	55143	57225	59298	61362	63416	65462	67499	69527	58	
60	48877	50987	53087	55178	57260	59332	61396	63450	65496	67533	69561	59	

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
 D. 35. Parts 2 5 7 9 12 14 16 19 21 23 26 28 30 33 35

LOG. SINE SQUARE

	86°			87°				88°				s.
	18'	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	
	s. 48m	s. 46m	s. 47m	s. 48m	s. 49m	s. 50m	s. 51m	s. 52m	s. 53m	s. 54m	s. 55m	
0	0	9'6	9'6	9'6	9'6	9'6	9'6	9'6	9'6	9'6	9'6	0
1	0	69594	71613	73623	75624	77617	79601	81576	83543	85501	87450	1
2	0	69628	71647	73657	75658	77650	79634	81609	83575	85533	87482	2
3	0	69662	71680	73690	75691	77683	79667	81642	83608	85566	87515	3
4	0	69695	71714	73723	75724	77716	79700	81674	83641	85598	87547	4
5	0	69729	71747	73757	75757	77749	79733	81707	83673	85631	87580	5
6	0	69763	71781	73790	75791	77783	79766	81740	83706	85663	87612	6
7	0	69797	71815	73824	75824	77816	79799	81773	83739	85696	87644	7
8	0	69830	71848	73857	75857	77849	79832	81806	83771	85728	87677	8
9	0	69864	71882	73890	75891	77882	79865	81839	83804	85761	87709	9
10	0	69898	71915	73924	75924	77915	79898	81872	83837	85794	87742	10
11	0	69931	71949	73957	75957	77948	79930	81904	83869	85826	87774	11
12	0	69965	71982	73991	75990	77981	79963	81937	83902	85859	87806	12
13	0	69999	72016	74024	76024	78014	79996	81970	83935	85891	87839	13
14	0	70032	72049	74058	76057	78047	80029	83903	85859	87871	87871	14
15	0	70066	72083	74091	76090	78081	80062	82036	84000	85956	87904	15
16	0	70100	72116	74124	76123	78114	80095	82068	84033	85989	87936	16
17	0	70133	72150	74158	76157	78147	80128	82101	84065	86021	87968	17
18	0	70167	72184	74191	76190	78180	80161	82134	84098	86054	88001	18
19	0	70201	72217	74224	76223	78213	80194	82167	84131	86086	88033	19
20	0	70234	72251	74258	76256	78246	80227	82200	84163	86119	88066	20
21	0	70268	72284	74291	76290	78279	80260	82232	84196	86151	88098	21
22	0	70302	72318	74325	76323	78312	80293	82265	84229	86214	88130	22
23	0	70336	72351	74358	76356	78345	80326	82298	84261	86216	88163	23
24	0	70369	72385	74391	76389	78378	80359	82331	84294	86249	88195	24
25	0	70403	72418	74425	76422	78411	80392	82364	84327	86281	88227	25
26	0	70437	72452	74458	76456	78445	80425	82396	84359	86314	88260	26
27	0	70470	72485	74491	76489	78478	80458	82429	84392	86346	88292	27
28	0	70504	72519	74525	76522	78511	80491	82462	84425	86379	88325	28
29	0	70538	72552	74558	76555	78544	80524	82495	84457	86411	88357	29
30	0	70571	72586	74592	76589	78577	80557	82528	84490	86444	88389	30
31	0	70605	72619	74625	76622	78610	80589	82560	84523	86476	88422	31
32	0	70638	72653	74658	76655	78643	80622	82593	84555	86509	88454	32
33	0	70672	72686	74692	76688	78676	80655	82626	84588	86541	88486	33
34	0	70706	72720	74725	76721	78709	80688	82659	84620	86574	88519	34
35	0	70739	72753	74758	76755	78742	80721	82691	84653	86606	88551	35
36	0	70773	72787	74792	76788	78775	80754	82724	84686	86639	88583	36
37	0	70807	72820	74825	76821	78808	80787	82757	84718	86671	88616	37
38	0	70840	72854	74858	76854	78841	80820	82790	84751	86704	88648	38
39	0	70874	72887	74892	76887	78874	80853	82822	84784	86736	88680	39
40	0	70908	72921	74925	76920	78907	80886	82855	84816	86769	88713	40
41	0	70941	72954	74958	76954	78940	80919	82888	84849	86801	88745	41
42	0	70975	72988	74992	76987	78974	80951	82921	84881	86834	88777	42
43	0	71008	73021	75025	77020	79007	80984	82953	84914	86866	88810	43
44	0	71042	73054	75058	77053	79040	81017	82986	84947	86899	88842	44
45	0	71076	73088	75092	77086	79073	81050	83019	84979	86931	88874	45
46	0	71109	73121	75125	77120	79106	81083	83052	85012	86963	88907	46
47	0	71143	73155	75158	77153	79139	81116	83084	85044	86996	88939	47
48	0	71176	73188	75192	77186	79172	81149	83117	85077	87028	88971	48
49	0	71210	73222	75225	77219	79205	81182	83150	85110	87061	89003	49
50	0	71244	73255	75258	77252	79238	81214	83183	85142	87093	89036	50
51	0	71277	73289	75291	77285	79271	81247	83215	85175	87126	89068	51
52	0	71311	73322	75325	77319	79304	81280	83248	85207	87158	89100	52
53	0	71344	73356	75358	77352	79337	81313	83281	85240	87191	89133	53
54	0	71378	73389	75391	77385	79370	81346	83313	85273	87223	89165	54
55	0	71412	73423	75425	77418	79403	81379	83346	85305	87255	89197	55
56	0	71445	73456	75458	77451	79436	81412	83379	85338	87288	89230	56
57	0	71479	73489	75491	77484	79469	81445	83412	85370	87320	89262	57
58	0	71512	73523	75525	77518	79502	81477	83444	85403	87353	89294	58
59	0	71546	73556	75558	77551	79535	81510	83477	85435	87385	89326	59
60	0	71580	73590	75591	77584	79568	81543	83510	85468	87417	89359	60

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
 D. 33. Parts 2 4 7 9 11 13 15 18 20 22 24 26 29 31 33

LOG. SINE SQUARE

		89°				90°				91°			S.
		0'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	
		89° 0'	89° 15'	89° 30'	89° 45'	90° 0'	90° 15'	90° 30'	90° 45'	91° 0'	91° 15'	91° 30'	
0	0	9'6	9'6	9'6	9'6	9'	9'7	9'7	9'7	9'7	9'7	9'7	0
1	0	91324	93248	95163	97071	698970	00861	02743	04618	06484	08342	10192	1
2	0	91356	93280	95195	97103	699002	00892	02775	04649	06515	08373	10223	2
3	0	91388	93312	95227	97134	699033	00924	02806	04680	06546	08404	10254	3
4	0	91420	93344	95259	97166	699065	00955	02837	04711	06577	08435	10285	4
5	0	91452	93376	95291	97198	699096	00987	02869	04743	06608	08466	10315	5
6	0	91484	93408	95323	97229	699128	01018	02900	04774	06639	08497	10346	6
7	0	91516	93440	95355	97261	699159	01049	02931	04805	06670	08528	10377	7
8	0	91548	93472	95386	97293	699191	01081	02963	04836	06701	08558	10408	8
9	0	91581	93504	95418	97325	699223	01112	02994	04867	06732	08589	10439	9
10	0	91613	93536	95450	97356	699254	01144	03025	04898	06763	08620	10469	10
11	0	91645	93568	95482	97388	699286	01175	03056	04929	06794	08651	10500	11
12	0	91677	93600	95514	97420	699317	01207	03088	04961	06825	08682	10531	12
13	0	91709	93632	95546	97451	699349	01238	03119	04992	06856	08713	10561	13
14	0	91741	93664	95577	97483	699380	01269	03150	05023	06887	08744	10592	14
15	0	91773	93695	95609	97515	699412	01301	03182	05054	06918	08775	10623	15
16	0	91805	93727	95641	97546	699443	01332	03213	05085	06949	08805	10653	16
17	0	91838	93759	95673	97578	699475	01364	03244	05116	06980	08836	10684	17
18	0	91870	93791	95705	97610	699506	01395	03275	05147	07011	08867	10715	18
19	0	91902	93823	95737	97641	699538	01426	03307	05179	07042	08898	10746	19
20	0	91933	93855	95768	97673	699570	01458	03338	05210	07073	08929	10776	20
21	0	91966	93887	95800	97705	699601	01489	03369	05241	07104	08960	10807	21
22	0	91998	93919	95832	97737	699633	01521	03400	05272	07135	08991	10838	22
23	0	92030	93951	95864	97768	699664	01552	03432	05303	07166	09021	10869	23
24	0	92062	93983	95896	97800	699696	01583	03463	05334	07197	09052	10899	24
25	0	92094	94015	95927	97831	699727	01615	03494	05365	07228	09083	10930	25
26	0	92126	94047	95959	97863	699759	01646	03525	05396	07259	09114	10961	26
27	0	92158	94079	95991	97895	699790	01678	03557	05428	07290	09145	10991	27
28	0	92190	94111	96023	97926	699822	01709	03588	05459	07321	09176	11022	28
29	0	92222	94143	96055	97958	699853	01740	03619	05490	07352	09207	11053	29
30	0	92255	94175	96086	97990	699885	01772	03650	05521	07383	09237	11083	30
31	0	92287	94207	96118	98021	699916	01803	03682	05552	07414	09268	11114	31
32	0	92319	94239	96150	98053	699948	01834	03713	05583	07445	09299	11145	32
33	0	92351	94270	96182	98085	699979	01866	03744	05614	07476	09330	11176	33
34	0	92383	94302	96214	98116	700011	01897	03775	05645	07507	09361	11206	34
35	0	92415	94334	96245	98148	700042	01929	03807	05676	07538	09392	11237	35
36	0	92447	94366	96277	98180	700074	01960	03838	05707	07569	09422	11268	36
37	0	92479	94398	96309	98211	700105	01991	03869	05739	07600	09453	11298	37
38	0	92511	94430	96341	98243	700137	02023	03900	05770	07631	09484	11329	38
39	0	92543	94462	96372	98275	700168	02054	03932	05801	07662	09515	11360	39
40	0	92575	94494	96404	98306	700200	02085	03963	05832	07693	09546	11390	40
41	0	92607	94526	96436	98338	700231	02117	03994	05863	07724	09576	11421	41
42	0	92639	94558	96468	98370	700263	02148	04025	05894	07755	09607	11452	42
43	0	92671	94590	96499	98401	700294	02179	04056	05925	07786	09638	11483	43
44	0	92703	94621	96531	98433	700326	02211	04088	05956	07817	09669	11513	44
45	0	92735	94653	96563	98464	700357	02242	04119	05987	07847	09700	11544	45
46	0	92767	94685	96595	98496	700389	02274	04150	06018	07878	09731	11574	46
47	0	92800	94717	96627	98528	700420	02305	04181	06049	07909	09761	11605	47
48	0	92832	94749	96658	98559	700452	02336	04212	06080	07940	09792	11636	48
49	0	92864	94781	96690	98591	700483	02368	04244	06112	07971	09823	11666	49
50	0	92896	94813	96722	98622	700515	02399	04275	06143	08002	09854	11697	50
51	0	92928	94845	96754	98654	700546	02430	04306	06174	08033	09884	11728	51
52	0	92960	94877	96785	98686	700578	02462	04337	06205	08064	09915	11758	52
53	0	92992	94909	96817	98717	700609	02493	04368	06236	08095	09946	11789	53
54	0	93024	94940	96849	98749	700641	02524	04400	06267	08126	09977	11820	54
55	0	93056	94972	96881	98780	700672	02556	04431	06298	08157	10008	11850	55
56	0	93088	95004	96912	98812	700702	02587	04462	06329	08188	10038	11881	56
57	0	93120	95036	96944	98844	700735	02618	04493	06360	08219	10069	11912	57
58	0	93152	95068	96976	98875	700766	02649	04524	06391	08249	10100	11942	58
59	0	93184	95100	97007	98907	700798	02681	04556	06422	08280	10131	11973	59
60	0	93216	95132	97039	98938	700829	02712	04587	06453	08311	10161	12004	60

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 32. Parts 2 4 6 9 11 13 15 17 19 21 23 26 28 30 32

TABLE 69

861

LOG. SINE SQUARE

	LOG. SINE SQUARE												S.	
	91°		92°				93°				94°			
	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'	15'			
	0-7	0-8	0-9	0-10	0-11	0-12	0-13	0-14	0-15	0-16	0-17			
0 0	9'7	9'7	9'7	9'7	9'7	9'7	9'7	9'7	9'7	9'7	9'7	9'7	0	
15	12034	13868	15694	17512	19322	21124	22919	24705	26484	28255	30018	1		
30	12065	13899	15725	17542	19352	21154	22949	24735	26514	28284	30047	2		
45	12095	13929	15755	17573	19382	21184	22978	24765	26543	28314	30077	3		
1 0	12126	13960	15785	17603	19412	21214	23008	24794	26573	28343	30106	4		
15	12157	13990	15816	17633	19443	21244	23038	24824	26602	28373	30135	5		
30	12187	14021	15846	17663	19473	21274	23068	24854	26632	28402	30165	6		
45	12218	14051	15876	17693	19503	21304	23098	24883	26661	28432	30194	7		
2 0	12249	14082	15907	17724	19533	21334	23128	24913	26691	28461	30223	8		
15	12279	14112	15937	17754	19563	21364	23157	24943	26721	28490	30253	9		
30	12310	14142	15967	17784	19593	21394	23187	24973	26750	28520	30282	10		
45	12340	14173	15998	17814	19623	21424	23217	25002	26780	28549	30311	11		
3 0	12371	14203	16028	17845	19653	21454	23247	25032	26809	28579	30341	12		
15	12402	14234	16058	17875	19683	21484	23277	25062	26839	28608	30370	13		
30	12432	14264	16089	17905	19713	21514	23306	25091	26868	28638	30399	14		
45	12463	14295	16119	17935	19743	21544	23336	25121	26898	28667	30428	15		
4 0	12493	14325	16149	17965	19773	21574	23366	25151	26927	28696	30458	16		
15	12524	14356	16180	17996	19804	21604	23396	25180	26957	28726	30487	17		
30	12555	14386	16210	18026	19834	21634	23426	25210	26987	28755	30516	18		
45	12585	14417	16240	18056	19864	21664	23455	25240	27016	28785	30546	19		
5 0	12616	14447	16271	18086	19894	21693	23485	25270	27046	28814	30575	20		
15	12646	14478	16301	18116	19924	21723	23515	25299	27075	28843	30604	21		
30	12677	14508	16331	18147	19954	21753	23545	25329	27105	28873	30633	22		
45	12708	14539	16362	18177	19984	21783	23575	25358	27134	28902	30663	23		
6 0	12738	14569	16392	18207	20014	21813	23604	25388	27164	28932	30692	24		
15	12769	14599	16422	18237	20044	21843	23634	25418	27193	28961	30721	25		
30	12799	14630	16453	18267	20074	21873	23664	25447	27223	28990	30751	26		
45	12830	14660	16483	18297	20104	21903	23694	25477	27252	29020	30780	27		
7 0	12860	14691	16513	18328	20134	21933	23724	25507	27282	29049	30809	28		
15	12891	14721	16544	18358	20164	21963	23753	25536	27311	29079	30838	29		
30	12922	14752	16574	18388	20194	21993	23783	25566	27341	29108	30868	30		
45	12952	14782	16604	18418	20224	22023	23813	25596	27370	29137	30897	31		
8 0	12983	14813	16634	18448	20254	22052	23843	25625	27400	29167	30926	32		
15	13013	14843	16665	18479	20284	22082	23872	25655	27429	29196	30955	33		
30	13044	14873	16695	18509	20314	22112	23902	25685	27459	29226	30985	34		
45	13074	14904	16725	18539	20344	22142	23932	25714	27488	29255	31014	35		
9 0	13105	14934	16756	18569	20374	22172	23962	25744	27518	29284	31043	36		
15	13136	14965	16786	18599	20405	22202	23992	25773	27547	29314	31072	37		
30	13166	14995	16816	18629	20435	22232	24021	25803	27577	29343	31102	38		
45	13197	15026	16846	18659	20465	22262	24051	25833	27606	29373	31131	39		
10 0	13227	15056	16877	18690	20495	22292	24081	25862	27636	29402	31160	40		
15	13258	15086	16907	18720	20525	22322	24111	25892	27665	29431	31189	41		
30	13288	15117	16937	18750	20555	22351	24140	25922	27695	29461	31219	42		
45	13319	15147	16967	18780	20585	22381	24170	25951	27724	29490	31248	43		
11 0	13349	15178	16998	18810	20615	22411	24200	25981	27754	29519	31277	44		
15	13380	15208	17028	18840	20645	22441	24230	26010	27783	29549	31306	45		
30	13411	15238	17058	18870	20675	22471	24259	26040	27813	29578	31335	46		
45	13441	15269	17089	18901	20705	22501	24289	26070	27842	29607	31365	47		
12 0	13472	15299	17119	18931	20735	22531	24319	26099	27872	29637	31394	48		
15	13502	15330	17149	18961	20765	22560	24349	26129	27901	29666	31423	49		
30	13533	15360	17179	18991	20795	22590	24378	26158	27931	29695	31452	50		
45	13563	15390	17210	19021	20825	22620	24408	26188	27960	29725	31482	51		
13 0	13594	15421	17240	19051	20855	22650	24438	26218	27990	29754	31511	52		
15	13624	15451	17270	19081	20885	22680	24468	26247	28019	29783	31540	53		
30	13655	15481	17300	19111	20915	22710	24497	26277	28049	29813	31569	54		
45	13685	15512	17331	19141	20945	22740	24527	26306	28078	29842	31598	55		
14 0	13716	15542	17361	19171	20975	22769	24557	26336	28108	29871	31628	56		
15	13746	15573	17391	19202	21004	22799	24586	26366	28137	29901	31657	57		
30	13777	15603	17421	19232	21034	22829	24616	26395	28166	29930	31686	58		
45	13807	15633	17452	19262	21064	22859	24646	26425	28196	29959	31715	59		
15	13833	15664	17482	19292	21094	22889	24676	26454	28225	29989	31744	60		

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D 30. Parts 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30

LOG. SINE SQUARE													
	94°		95°				96°				97°		S.
	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'		
	0° 15'	0° 19'	0° 20'	0° 21'	0° 22'	0° 23'	0° 24'	0° 25'	0° 26'	0° 27'	0° 28'		
0	0	9'7	9'7	9'7	9'7	9'7	9'7	9'7	9'7	9'7	9'7	0	
1	0	31774	33521	35262	36994	38719	40437	42147	43849	45544	47232	48912	1
2	0	31803	33551	35291	37023	38748	40465	42175	43878	45573	47260	48940	2
3	0	31832	33580	35320	37052	38777	40494	42204	43906	45601	47288	48968	3
4	0	31861	33609	35349	37081	38805	40523	42232	43934	45629	47316	48996	4
5	0	31890	33638	35377	37110	38834	40551	42261	43963	45657	47344	49024	5
6	0	31920	33667	35406	37138	38863	40580	42289	43991	45685	47372	49052	6
7	0	31949	33696	35435	37167	38892	40608	42317	44019	45713	47400	49080	7
8	0	31978	33725	35464	37196	38920	40637	42346	44048	45742	47428	49108	8
9	0	32007	33754	35493	37225	38949	40665	42374	44076	45770	47456	49136	9
10	0	32036	33783	35522	37254	38978	40694	42403	44104	45798	47485	49164	10
11	0	32066	33812	35551	37282	39006	40722	42431	44132	45826	47513	49192	11
12	0	32095	33841	35580	37311	39035	40751	42460	44161	45854	47541	49219	12
13	0	32124	33870	35609	37340	39063	40780	42488	44189	45883	47569	49247	13
14	0	32153	33899	35638	37369	39092	40808	42516	44217	45911	47597	49275	14
15	0	32182	33928	35667	37397	39121	40837	42545	44246	45939	47625	49303	15
16	0	32211	33957	35696	37426	39149	40865	42573	44274	45967	47653	49331	16
17	0	32241	33986	35724	37455	39178	40894	42602	44302	45995	47681	49359	17
18	0	32270	34015	35753	37484	39207	40922	42630	44330	46023	47709	49387	18
19	0	32299	34044	35782	37513	39235	40951	42658	44359	46051	47737	49415	19
20	0	32328	34073	35811	37541	39264	40979	42687	44387	46080	47765	49443	20
21	0	32357	34102	35840	37570	39293	41008	42715	44415	46108	47793	49471	21
22	0	32386	34131	35869	37599	39321	41036	42744	44443	46136	47821	49499	22
23	0	32415	34160	35898	37628	39350	41065	42772	44472	46164	47849	49526	23
24	0	32444	34189	35927	37656	39379	41093	42800	44500	46192	47877	49554	24
25	0	32474	34218	35956	37685	39407	41122	42829	44528	46220	47905	49582	25
26	0	32503	34248	35985	37714	39436	41150	42857	44557	46249	47933	49610	26
27	0	32532	34277	36013	37743	39465	41179	42885	44585	46277	47961	49638	27
28	0	32561	34306	36042	37772	39493	41207	42914	44613	46305	47989	49666	28
29	0	32590	34335	36071	37800	39522	41236	42942	44641	46333	48017	49694	29
30	0	32619	34364	36100	37829	39551	41264	42971	44670	46361	48045	49722	30
31	0	32649	34394	36129	37858	39579	41293	42999	44698	46389	48073	49750	31
32	0	32678	34422	36158	37887	39608	41321	43027	44726	46417	48101	49778	32
33	0	32707	34451	36187	37915	39636	41350	43056	44754	46445	48129	49805	33
34	0	32736	34479	36216	37944	39665	41378	43084	44783	46473	48157	49833	34
35	0	32765	34509	36244	37973	39694	41407	43112	44811	46502	48185	49861	35
36	0	32794	34537	36273	38002	39722	41435	43141	44839	46530	48213	49889	36
37	0	32823	34567	36302	38030	39751	41464	43169	44867	46558	48241	49917	37
38	0	32852	34596	36331	38059	39779	41492	43198	44896	46586	48269	49945	38
39	0	32882	34625	36360	38088	39808	41521	43226	44924	46614	48297	49973	39
40	0	32911	34654	36389	38117	39837	41549	43254	44952	46642	48325	50000	40
41	0	32940	34682	36418	38145	39865	41578	43283	44980	46670	48353	50028	41
42	0	32969	34711	36447	38174	39894	41606	43311	45009	46698	48381	50056	42
43	0	32998	34740	36475	38203	39922	41635	43339	45037	46727	48409	50084	43
44	0	33027	34769	36504	38231	39951	41663	43368	45065	46755	48437	50112	44
45	0	33056	34798	36533	38260	39980	41692	43396	45093	46783	48465	50140	45
46	0	33085	34827	36562	38289	40008	41720	43424	45121	46811	48493	50168	46
47	0	33114	34856	36591	38318	40037	41749	43453	45150	46839	48521	50195	47
48	0	33143	34885	36620	38346	40065	41777	43481	45178	46867	48549	50223	48
49	0	33172	34914	36648	38375	40094	41805	43509	45206	46895	48577	50251	49
50	0	33202	34943	36677	38404	40123	41834	43538	45234	46923	48605	50279	50
51	0	33231	34972	36706	38432	40151	41862	43566	45262	46951	48633	50307	51
52	0	33260	35001	36735	38461	40180	41891	43594	45291	46979	48661	50335	52
53	0	33289	35030	36764	38490	40208	41919	43623	45319	47007	48689	50362	53
54	0	33318	35059	36793	38519	40237	41948	43651	45347	47036	48717	50390	54
55	0	33347	35088	36822	38547	40266	41976	43679	45375	47064	48745	50418	55
56	0	33376	35117	36850	38576	40294	42005	43703	45403	47093	48773	50446	56
57	0	33405	35146	36879	38605	40323	42033	43732	45432	47120	48800	50474	57
58	0	33434	35175	36908	38633	40351	42062	43764	45460	47148	48828	50502	58
59	0	33463	35204	36937	38662	40380	42090	43793	45488	47176	48856	50530	59
60	0	33492	35233	36966	38691	40408	42118	43821	45516	47204	48884	50557	60

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 28. Parts 2 4 6 7 9 11 13 15 17 19 20 22 24 26 28

LOG. SINE SQUARE

	97°			98°				99°				S.
	15'	20'	45'	0'	15'	30'	45'	0'	15'	30'	45'	
	0° 29'	0° 30'	0° 31'	0° 32'	0° 33'	0° 34'	0° 35'	0° 36'	0° 37'	0° 38'	0° 39'	
0	9'7	9'7	9'7	9'7	9'7	9'7	9'7	9'7	9'7	9'7	9'7	0
1	50585	52251	53909	55560	57203	58840	60469	62091	63706	65314	66914	1
2	50613	52278	53936	55587	57231	58867	60496	62118	63733	65340	66941	2
3	50641	52306	53964	55615	57258	58894	60523	62145	63760	65367	66968	3
4	50669	52334	53991	55642	57285	58921	60550	62172	63786	65394	66994	4
5	50696	52361	54019	55670	57313	58949	60577	62199	63813	65421	67021	5
6	50724	52389	54047	55697	57340	58976	60604	62226	63840	65447	67047	6
7	50752	52417	54074	55724	57367	59003	60631	62253	63867	65474	67074	7
8	50780	52444	54102	55752	57395	59030	60659	62280	63894	65501	67101	8
9	50808	52472	54129	55779	57422	59057	60686	62307	63921	65527	67127	9
10	50835	52500	54157	55807	57449	59085	60713	62334	63948	65554	67154	10
11	50863	52527	54184	55834	57477	59112	60740	62361	63974	65581	67180	11
12	50891	52555	54212	55862	57504	59139	60767	62388	64001	65608	67207	12
13	50919	52583	54240	55889	57531	59166	60794	62415	64028	65634	67234	13
14	50947	52611	54267	55916	57558	59193	60821	62442	64055	65661	67260	14
15	50974	52638	54295	55944	57586	59221	60848	62468	64082	65688	67287	15
16	51002	52666	54322	55971	57613	59248	60875	62495	64108	65714	67313	16
17	51030	52694	54350	55999	57640	59275	60902	62522	64135	65741	67340	17
18	51058	52721	54377	56026	57668	59302	60929	62549	64162	65768	67367	18
19	51085	52749	54405	56054	57695	59329	60956	62576	64189	65795	67393	19
20	51113	52776	54432	56081	57722	59356	60983	62603	64216	65821	67420	20
21	51141	52804	54460	56108	57750	59384	61010	62630	64243	65848	67446	21
22	51169	52832	54487	56136	57777	59411	61038	62657	64269	65875	67473	22
23	51197	52859	54515	56163	57804	59438	61065	62684	64296	65901	67499	23
24	51224	52887	54543	56191	57831	59465	61092	62711	64323	65928	67526	24
25	51252	52915	54570	56218	57859	59492	61119	62738	64350	65955	67553	25
26	51280	52942	54598	56245	57886	59519	61146	62765	64377	65981	67579	26
27	51308	52970	54625	56273	57913	59547	61173	62792	64403	66008	67606	27
28	51335	52998	54653	56300	57941	59574	61200	62819	64430	66035	67632	28
29	51363	53025	54680	56328	57968	59601	61227	62845	64457	66061	67659	29
30	51391	53053	54708	56355	57995	59628	61254	62872	64484	66088	67685	30
31	51419	53081	54735	56382	58022	59655	61281	62899	64511	66115	67712	31
32	51447	53108	54763	56410	58050	59682	61308	62926	64537	66141	67739	32
33	51474	53136	54790	56437	58077	59710	61335	62953	64564	66168	67765	33
34	51502	53164	54818	56465	58104	59737	61362	62980	64591	66195	67792	34
35	51530	53191	54845	56492	58131	59764	61389	63007	64618	66221	67818	35
36	51558	53219	54873	56519	58159	59791	61416	63034	64645	66248	67845	36
37	51585	53246	54900	56547	58186	59818	61443	63061	64671	66275	67871	37
38	51613	53274	54928	56574	58213	59845	61470	63088	64698	66302	67898	38
39	51641	53302	54955	56602	58241	59872	61497	63115	64725	66328	67924	39
40	51669	53329	54983	56629	58268	59900	61524	63141	64752	66355	67951	40
41	51696	53357	55010	56656	58295	59927	61551	63168	64778	66382	67977	41
42	51724	53385	55038	56684	58322	59954	61578	63195	64805	66408	68004	42
43	51752	53412	55065	56711	58350	59981	61605	63222	64832	66435	68031	43
44	51779	53440	55093	56738	58377	60008	61632	63249	64859	66462	68057	44
45	51807	53467	55120	56766	58404	60035	61659	63276	64886	66488	68084	45
46	51835	53495	55148	56793	58431	60062	61686	63303	64912	66515	68110	46
47	51863	53523	55175	56820	58459	60089	61713	63330	64939	66541	68137	47
48	51890	53550	55203	56848	58486	60117	61740	63357	64966	66568	68163	48
49	51918	53578	55230	56875	58513	60144	61767	63384	64993	66595	68190	49
50	51946	53605	55258	56903	58540	60171	61794	63410	65019	66621	68216	50
51	51974	53633	55285	56930	58568	60198	61821	63437	65046	66648	68243	51
52	52001	53661	55312	56957	58595	60225	61848	63464	65073	66675	68269	52
53	52029	53688	55340	56985	58622	60252	61875	63491	65100	66701	68296	53
54	52057	53716	55367	57012	58649	60279	61902	63518	65126	66728	68322	54
55	52084	53743	55395	57039	58676	60306	61929	63545	65153	66755	68349	55
56	52112	53771	55422	57067	58704	60333	61956	63572	65180	66781	68375	56
57	52140	53799	55450	57094	58731	60361	61983	63599	65207	66808	68402	57
58	52167	53826	55477	57121	58758	60388	62010	63625	65234	66834	68428	58
59	52195	53854	55505	57149	58785	60415	62037	63652	65260	66861	68455	59
60	52223	53881	55532	57176	58813	60442	62064	63679	65287	66888	68481	60

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 27. Parts 2 4 5 7 9 11 13 14 16 18 20 22 23 27

LOG. SINE SQUARE													
	100°				101°				102°				n.
	0'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'		
	6° 40'	6° 41'	6° 42'	6° 43'	6° 44'	6° 45'	6° 46'	6° 47'	6° 48'	6° 49'	6° 50'		
0	9.7	9.7	9.7	9.7	9.7	9.7	9.7	9.7	9.7	9.7	9.7	0	
15	68508	70094	71674	73246	74812	76371	77922	79467	81005	82536	84061	1	
30	68534	70121	71700	73273	74838	76397	77948	79493	81031	82562	84086	2	
45	68561	70147	71726	73299	74864	76423	77974	79519	81056	82587	84111	3	
1	68587	70174	71753	73325	74890	76448	78000	79544	81082	82613	84137	4	
15	68614	70200	71779	73351	74916	76474	78026	79570	81107	82638	84162	5	
30	68640	70226	71805	73377	74942	76500	78051	79596	81133	82664	84187	6	
45	68667	70253	71832	73403	74968	76526	78077	79621	81159	82689	84212	7	
2	68693	70279	71858	73430	74994	76552	78103	79647	81184	82714	84238	8	
15	68720	70305	71884	73456	75020	76578	78129	79673	81210	82740	84263	9	
30	68746	70332	71910	73482	75046	76604	78155	79698	81235	82765	84289	10	
45	68773	70358	71936	73508	75072	76630	78180	79724	81261	82791	84314	11	
3	68799	70385	71963	73534	75098	76656	78206	79750	81286	82816	84339	12	
15	68826	70411	71989	73560	75124	76682	78232	79775	81312	82842	84365	13	
30	68852	70437	72015	73586	75150	76707	78258	79801	81338	82867	84390	14	
45	68879	70464	72042	73612	75176	76733	78284	79827	81363	82893	84415	15	
4	68905	70490	72068	73639	75202	76759	78309	79852	81389	82918	84441	16	
15	68932	70516	72094	73665	75228	76785	78335	79878	81414	82943	84466	17	
30	68958	70543	72120	73691	75254	76811	78361	79904	81440	82969	84491	18	
45	68985	70569	72146	73717	75280	76837	78387	79929	81465	82994	84516	19	
5	69011	70595	72173	73743	75306	76863	78412	79955	81491	83020	84542	20	
15	69038	70622	72199	73769	75332	76889	78438	79981	81516	83045	84567	21	
30	69064	70648	72225	73795	75358	76915	78464	80006	81542	83071	84592	22	
45	69090	70674	72251	73821	75384	76940	78490	80032	81567	83096	84618	23	
6	69117	70701	72278	73847	75410	76966	78515	80058	81593	83121	84643	24	
15	69143	70727	72304	73874	75436	76992	78541	80083	81618	83147	84668	25	
30	69170	70753	72330	73900	75462	77018	78567	80109	81644	83172	84694	26	
45	69196	70780	72356	73926	75488	77044	78593	80134	81669	83198	84719	27	
7	69223	70806	72382	73952	75514	77070	78618	80160	81695	83223	84744	28	
15	69249	70832	72409	73978	75540	77096	78644	80186	81721	83248	84770	29	
30	69276	70859	72435	74004	75566	77122	78670	80211	81746	83274	84795	30	
45	69302	70885	72461	74030	75592	77147	78696	80237	81772	83299	84820	31	
8	69329	70911	72487	74056	75618	77173	78721	80263	81797	83325	84845	32	
15	69355	70938	72514	74082	75644	77199	78747	80288	81823	83350	84871	33	
30	69381	70964	72540	74108	75670	77225	78773	80314	81848	83375	84896	34	
45	69408	70990	72566	74135	75696	77251	78799	80340	81874	83401	84921	35	
9	69434	71017	72592	74161	75722	77277	78824	80365	81899	83426	84947	36	
15	69461	71043	72618	74187	75748	77303	78850	80391	81925	83452	84972	37	
30	69487	71069	72645	74213	75774	77328	78876	80416	81950	83477	84997	38	
45	69514	71096	72671	74239	75800	77354	78902	80442	81976	83502	85022	39	
10	69540	71122	72697	74265	75826	77380	78927	80468	82001	83528	85048	40	
15	69566	71148	72723	74291	75852	77406	78953	80493	82027	83553	85073	41	
30	69593	71175	72749	74317	75878	77432	78979	80519	82052	83579	85098	42	
45	69619	71201	72775	74343	75904	77458	79005	80544	82078	83604	85123	43	
11	69646	71227	72802	74369	75930	77483	79030	80570	82103	83629	85149	44	
15	69672	71253	72828	74395	75956	77509	79056	80596	82129	83655	85174	45	
30	69698	71280	72854	74421	75982	77535	79082	80621	82154	83680	85199	46	
45	69725	71306	72880	74447	76008	77561	79107	80647	82180	83705	85224	47	
12	69751	71332	72906	74473	76034	77587	79133	80672	82205	83731	85250	48	
15	69778	71359	72933	74500	76060	77613	79159	80698	82231	83756	85275	49	
30	69804	71385	72959	74526	76085	77638	79184	80724	82256	83782	85300	50	
45	69831	71411	72985	74552	76111	77664	79210	80749	82282	83807	85326	51	
13	69857	71437	73011	74578	76137	77690	79236	80775	82307	83832	85351	52	
15	69883	71464	73037	74604	76163	77716	79262	80799	82333	83858	85376	53	
30	69910	71490	73063	74630	76189	77742	79287	80826	82358	83883	85401	54	
45	69936	71516	73090	74656	76215	77768	79313	80852	82384	83908	85427	55	
14	69962	71543	73116	74682	76241	77793	79339	80877	82409	83934	85452	56	
15	69989	71569	73142	74708	76267	77819	79364	80903	82434	83959	85477	57	
30	70015	71595	73168	74734	76293	77845	79390	80928	82460	83985	85502	58	
45	70042	71621	73194	74760	76319	77871	79416	80954	82485	84010	85528	59	
50	70068	71648	73220	74786	76345	77897	79442	80980	82511	84035	85553	60	

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 26. Parts 2 3 5 7 9 10 12 14 15 17 19 21 22 24 26

LOG. SINE SQUARE

	LOG. SINE SQUARE												s.	
	102°		103°				104°				105°			
	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'	15'			
	6 ^h 51 ^m	6 ^h 52 ^m	6 ^h 53 ^m	6 ^h 54 ^m	6 ^h 55 ^m	6 ^h 56 ^m	6 ^h 57 ^m	6 ^h 58 ^m	6 ^h 59 ^m	7 ^h 0 ^m	7 ^h 1 ^m			
0 0	9'7	9'7	9'7	9'7	9'7	9'7	9'7	9'7	9'7	9'	9'8		0	
15	85578	87089	88593	90090	91580	93064	94541	96012	97476	98933	00384		1	
30	85603	87114	88618	90115	91605	93089	94566	96036	97500	98958	00408		2	
45	85628	87139	88643	90140	91630	93114	94591	96061	97525	98982	00432		3	
1 0	85654	87164	88668	90165	91655	93138	94615	96085	97549	99006	00456		4	
15	85679	87189	88693	90189	91680	93163	94640	96110	97573	99030	00481		5	
30	85704	87214	88718	90214	91704	93188	94664	96134	97598	99054	00505		6	
45	85729	87239	88743	90239	91729	93212	94689	96159	97622	99079	00529		7	
2 0	85755	87265	88768	90264	91754	93237	94713	96183	97646	99103	00553		8	
15	85780	87290	88793	90289	91779	93262	94738	96208	97671	99127	00577		9	
30	85805	87315	88818	90314	91803	93286	94762	96232	97695	99151	00601		10	
45	85830	87340	88843	90339	91828	93311	94787	96256	97719	99176	00625		11	
3 0	85855	87365	88868	90364	91853	93336	94812	96281	97744	99200	00649		12	
15	85881	87390	88893	90389	91878	93360	94836	96305	97768	99224	00673		13	
30	85906	87415	88918	90413	91902	93385	94861	96330	97792	99248	00698		14	
45	85931	87440	88943	90438	91927	93410	94885	96354	97817	99272	00722		15	
4 0	85956	87465	88968	90463	91952	93434	94910	96379	97841	99297	00746		16	
15	85982	87490	88993	90488	91977	93459	94934	96403	97865	99321	00770		17	
30	86007	87516	89018	90513	92002	93483	94959	96427	97889	99345	00794		18	
45	86032	87541	89043	90538	92026	93508	94983	96452	97914	99369	00818		19	
5 0	86057	87566	89068	90563	92051	93533	95008	96476	97938	99393	00842		20	
15	86082	87591	89093	90587	92076	93557	95032	96501	97962	99418	00866		21	
30	86108	87616	89117	90612	92101	93582	95057	96525	97987	99442	00890		22	
45	86133	87641	89142	90637	92125	93607	95081	96549	98011	99466	00914		23	
6 0	86158	87666	89167	90662	92150	93631	95106	96574	98035	99490	00938		24	
15	86183	87691	89192	90687	92175	93656	95130	96598	98060	99514	00963		25	
30	86208	87716	89217	90712	92200	93681	95155	96623	98084	99539	00987		26	
45	86233	87741	89242	90737	92224	93705	95180	96647	98108	99563	01011		27	
7 0	86259	87766	89267	90761	92249	93730	95204	96672	98133	99587	01035		28	
15	86284	87791	89292	90786	92274	93754	95229	96696	98157	99611	01059		29	
30	86309	87816	89317	90811	92299	93779	95253	96720	98181	99635	01083		30	
45	86334	87842	89342	90836	92323	93804	95278	96745	98205	99660	01107		31	
8 0	86359	87866	89367	90861	92348	93828	95302	96769	98230	99684	01131		32	
15	86385	87892	89392	90886	92373	93853	95327	96794	98254	99708	01155		33	
30	86410	87917	89417	90911	92397	93878	95351	96818	98278	99732	01179		34	
45	86435	87942	89442	90935	92422	93902	95376	96842	98303	99756	01203		35	
9 0	86460	87967	89467	90960	92447	93927	95400	96867	98327	99780	01227		36	
15	86485	87992	89491	90985	92472	93951	95425	96891	98351	99805	01251		37	
30	86510	88017	89517	91010	92496	93976	95449	96916	98375	99829	01275		38	
45	86536	88042	89542	91035	92521	94001	95474	96940	98400	99853	01299		39	
10 0	86561	88067	89567	91060	92546	94025	95498	96964	98424	99877	01324		40	
15	86586	88092	89592	91084	92570	94050	95523	96989	98448	99901	01348		41	
30	86611	88117	89617	91109	92595	94074	95547	97013	98473	99925	01372		42	
45	86636	88142	89642	91134	92620	94099	95572	97038	98497	99949	01396		43	
11 0	86661	88167	89666	91159	92644	94124	95596	97062	98521	99974	01420		44	
15	86687	88192	89691	91184	92669	94148	95620	97086	98545	99998	01444		45	
30	86712	88217	89716	91208	92694	94173	95645	97111	98570	80022	01468		46	
45	86737	88242	89741	91233	92719	94197	95669	97135	98594	80046	01492		47	
12 0	86762	88267	89766	91258	92743	94222	95694	97159	98618	80070	01516		48	
15	86787	88292	89791	91283	92768	94247	95718	97184	98642	80094	01540		49	
30	86812	88317	89816	91308	92793	94271	95743	97208	98667	80119	01564		50	
45	86837	88342	89841	91333	92817	94296	95767	97232	98691	80143	01588		51	
13 0	86863	88368	89866	91357	92842	94320	95792	97257	98715	80167	01612		52	
15	86888	88393	89891	91382	92867	94345	95816	97281	98739	80191	01636		53	
30	86913	88418	89916	91407	92891	94369	95841	97306	98764	80215	01660		54	
45	86938	88443	89940	91432	92916	94394	95865	97330	98788	80239	01684		55	
14 0	86963	88468	89965	91457	92941	94419	95890	97354	98812	80263	01708		56	
15	86988	88493	89990	91481	92966	94443	95914	97379	98836	80287	01732		57	
30	87013	88518	90015	91506	92990	94468	95939	97403	98861	80312	01756		58	
45	87038	88543	90040	91531	93015	94492	95963	97427	98885	80336	01780		59	
15 0	87064	88568	90065	91556	93040	94517	95988	97452	98909	80360	01804		60	

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 25. Parts 2 3 5 7 8 10 12 13 15 17 18 20 22 23 25

LOG. SINE SQUARE														
	105°		106°				107°				108°		a.	
	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'	15'		
	7 2	7 3	7 4	7 5	7 6	7 7	7 8	7 9	7 10	7 11	7 12	7 13		
0	9 80	9 80	9 80	9 80	9 80	9 8	9 8	9 8	9 8	9 8	9 8	9 8	0	
10	18 52	3266	4697	6122	7540	8952	10357	11756	13149	14535	15915	17289	1	
20	18 52	3290	4721	6146	7564	8975	10381	11780	13172	14558	15938	17312	2	
30	18 76	3314	4745	6169	7587	8999	10404	11803	13195	14581	15961	17335	3	
40	19 00	3338	4769	6193	7611	9022	10427	11826	13219	14604	15984	17357	4	
50	19 24	3362	4792	6217	7634	9046	10451	11849	13242	14628	16007	17380	5	
60	19 48	3385	4816	6240	7658	9069	10474	11873	13265	14651	16030	17403	6	
70	19 72	3409	4840	6264	7682	9093	10498	11896	13288	14674	16054	17426	7	
80	19 96	3433	4864	6288	7705	9116	10521	11919	13311	14697	16077	17449	8	
90	20 20	3457	4887	6311	7729	9140	10544	11942	13334	14720	16100	17472	9	
100	20 44	3481	4911	6335	7752	9163	10568	11966	13357	14743	16123	17494	10	
110	20 68	3505	4935	6359	7776	9187	10591	11989	13381	14766	16146	17517	11	
120	20 92	3529	4959	6383	7800	9210	10614	12012	13404	14789	16169	17540	12	
130	21 16	3553	4983	6406	7823	9234	10638	12035	13427	14812	16191	17563	13	
140	21 40	3577	5006	6430	7847	9257	10661	12059	13450	14835	16214	17586	14	
150	21 64	3601	5030	6453	7870	9281	10684	12082	13473	14858	16237	17608	15	
160	21 88	3624	5054	6477	7894	9304	10708	12105	13496	14881	16260	17631	16	
170	22 12	3648	5078	6501	7917	9327	10731	12128	13519	14904	16283	17654	17	
180	22 36	3672	5102	6524	7941	9351	10754	12152	13543	14927	16306	17677	18	
190	22 60	3696	5125	6548	7964	9374	10778	12175	13566	14950	16329	17700	19	
200	22 84	3720	5149	6572	7988	9398	10801	12198	13589	14973	16352	17722	20	
210	23 08	3744	5173	6595	8012	9421	10824	12221	13612	14996	16375	17745	21	
220	23 32	3768	5197	6619	8035	9445	10848	12245	13635	15019	16398	17768	22	
230	23 56	3792	5220	6643	8059	9468	10871	12268	13658	15042	16420	17791	23	
240	24 20	3815	5244	6666	8082	9492	10894	12291	13681	15065	16443	17814	24	
250	24 44	3839	5268	6690	8106	9515	10918	12314	13704	15088	16466	17837	25	
260	24 68	3863	5292	6714	8129	9538	10941	12337	13727	15111	16489	17859	26	
270	24 92	3887	5315	6737	8153	9562	10964	12361	13751	15134	16512	17882	27	
280	25 16	3911	5339	6761	8176	9585	10988	12384	13774	15157	16534	17905	28	
290	25 40	3935	5363	6785	8200	9609	11011	12407	13797	15180	16557	17928	29	
300	25 64	3959	5387	6808	8223	9632	11034	12430	13820	15203	16580	17951	30	
310	25 88	3982	5410	6832	8247	9656	11058	12453	13843	15226	16603	17973	31	
320	26 12	4006	5434	6856	8270	9679	11081	12477	13866	15249	16626	17996	32	
330	26 36	4030	5458	6879	8294	9702	11104	12500	13889	15272	16649	18019	33	
340	26 60	4054	5482	6903	8318	9726	11127	12523	13912	15295	16671	18042	34	
350	26 84	4078	5505	6926	8341	9749	11151	12546	13935	15318	16694	18064	35	
360	26 08	4102	5529	6950	8365	9773	11174	12570	13958	15341	16717	18087	36	
370	26 32	4125	5553	6974	8388	9796	11198	12593	13982	15364	16740	18110	37	
380	26 56	4149	5577	6997	8412	9819	11221	12616	14005	15387	16763	18133	38	
390	27 20	4173	5600	7021	8435	9843	11244	12639	14028	15410	16786	18156	39	
400	27 44	4197	5624	7045	8459	9866	11267	12662	14051	15433	16809	18178	40	
410	27 68	4221	5648	7068	8482	9890	11291	12686	14074	15456	16832	18201	41	
420	27 92	4245	5672	7092	8506	9913	11314	12709	14097	15479	16854	18224	42	
430	28 16	4269	5695	7115	8529	9936	11337	12732	14120	15502	16877	18247	43	
440	28 40	4293	5719	7139	8553	9960	11361	12755	14143	15525	16900	18269	44	
450	28 64	4316	5743	7163	8576	9983	11384	12778	14166	15548	16923	18292	45	
460	28 88	4340	5766	7186	8600	10007	11407	12801	14189	15571	16946	18315	46	
470	29 12	4364	5790	7210	8623	10030	11431	12825	14212	15594	16969	18338	47	
480	29 36	4388	5814	7233	8647	10053	11454	12848	14235	15617	16992	18360	48	
490	29 60	4411	5837	7257	8670	10077	11477	12871	14259	15640	17015	18383	49	
500	29 84	4435	5861	7281	8694	10100	11500	12894	14282	15663	17037	18406	50	
510	30 08	4459	5885	7304	8717	10124	11524	12917	14305	15686	17060	18429	51	
520	30 32	4483	5909	7328	8741	10147	11547	12941	14328	15709	17083	18452	52	
530	30 56	4507	5932	7351	8764	10170	11570	12964	14351	15732	17106	18474	53	
540	30 80	4531	5956	7375	8788	10194	11594	12987	14374	15755	17129	18497	54	
550	31 04	4554	5980	7399	8811	10217	11617	13010	14397	15778	17152	18520	55	
560	31 28	4578	6003	7422	8835	10241	11641	13033	14420	15801	17175	18543	56	
570	31 52	4602	6027	7446	8858	10264	11663	13056	14443	15823	17198	18565	57	
580	31 76	4626	6051	7469	8882	10287	11687	13079	14466	15846	17220	18588	58	
590	32 00	4650	6075	7493	8905	10311	11710	13103	14489	15869	17243	18611	59	
600	32 24	4673	6098	7517	8929	10334	11733	13126	14512	15892	17266	18633	60	

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 24. Parts 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24

LOG. SINE SQUARE														
	111°			112°				113°				e.		
	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'			
	7 ^h 25 ^m	7 ^h 26 ^m	7 ^h 27 ^m	7 ^h 28 ^m	7 ^h 29 ^m	7 ^h 30 ^m	7 ^h 31 ^m	7 ^h 32 ^m	7 ^h 33 ^m	7 ^h 34 ^m	7 ^h 35 ^m			
0	9.8	9.8	9.8	9.8	9.8	9.8	9.8	9.8	9.8	9.8	9.8	0		
0	33287	34580	35867	37148	38424	39693	40956	42213	43464	44710	45949	0		
15	33308	34601	35889	37170	38445	39714	40977	42234	43485	44730	45970	1		
30	33330	34623	35910	37191	38466	39735	40998	42255	43506	44751	45990	2		
45	33352	34644	35931	37212	38487	39756	41019	42276	43527	44772	46011	3		
1	33373	34666	35953	37234	38508	39777	41040	42297	43548	44793	46032	4		
15	33395	34687	35974	37255	38530	39798	41061	42318	43568	44813	46052	5		
30	33416	34709	35996	37276	38551	39819	41082	42339	43589	44834	46073	6		
45	33438	34730	36017	37297	38572	39840	41103	42359	43610	44855	46093	7		
2	33460	34752	36038	37319	38593	39861	41124	42380	43631	44875	46114	8		
15	33481	34773	36060	37340	38614	39883	41145	42401	43652	44896	46135	9		
3	33503	34795	36081	37361	38636	39904	41166	42422	43672	44917	46155	10		
45	33524	34816	36103	37383	38657	39925	41187	42443	43693	44937	46176	11		
3	33546	34838	36124	37404	38678	39946	41208	42464	43714	44958	46196	12		
15	33568	34859	36145	37425	38699	39967	41229	42485	43735	44979	46217	13		
30	33589	34881	36167	37446	38720	39988	41250	42506	43756	45000	46238	14		
45	33611	34902	36188	37468	38741	40009	41271	42526	43776	45020	46258	15		
4	33632	34924	36209	37489	38763	40030	41292	42547	43797	45041	46279	16		
15	33654	34945	36231	37510	38784	40051	41313	42568	43818	45062	46299	17		
30	33675	34967	36252	37532	38805	40072	41334	42589	43839	45082	46320	18		
45	33697	34988	36274	37553	38826	40093	41355	42610	43859	45103	46341	19		
5	33718	35010	36295	37574	38847	40114	41376	42631	43880	45124	46361	20		
15	33740	35031	36316	37595	38868	40136	41397	42652	43901	45144	46382	21		
30	33762	35053	36338	37617	38890	40157	41418	42673	43922	45165	46402	22		
45	33783	35074	36359	37638	38911	40178	41439	42693	43942	45186	46423	23		
6	33805	35096	36380	37659	38932	40199	41460	42714	43963	45206	46443	24		
15	33826	35117	36402	37680	38953	40220	41481	42735	43984	45227	46464	25		
30	33848	35138	36423	37702	38974	40241	41502	42756	44005	45248	46484	26		
45	33869	35160	36444	37723	38995	40262	41522	42777	44026	45268	46505	27		
7	33891	35181	36466	37744	39017	40283	41543	42798	44046	45289	46526	28		
15	33913	35203	36487	37766	39038	40304	41564	42819	44067	45310	46546	29		
3	33934	35224	36509	37787	39059	40325	41585	42839	44088	45330	46567	30		
45	33956	35246	36530	37808	39080	40346	41606	42860	44109	45351	46587	31		
8	33977	35267	36551	37829	39101	40367	41627	42881	44129	45372	46608	32		
15	33999	35289	36573	37851	39122	40388	41648	42902	44150	45392	46628	33		
30	34020	35310	36594	37872	39143	40409	41669	42923	44171	45413	46649	34		
45	34042	35332	36615	37893	39165	40430	41690	42944	44192	45434	46670	35		
9	34063	35353	36637	37914	39186	40451	41711	42965	44212	45454	46690	36		
15	34085	35375	36658	37935	39207	40472	41732	42986	44233	45475	46711	37		
30	34107	35396	36679	37957	39228	40493	41753	43006	44254	45495	46731	38		
45	34128	35417	36701	37978	39249	40515	41774	43027	44275	45516	46752	39		
10	34150	35439	36722	37999	39270	40536	41795	43048	44295	45537	46772	40		
15	34171	35460	36743	38020	39292	40557	41816	43069	44316	45557	46793	41		
30	34193	35482	36765	38042	39313	40578	41837	43090	44337	45578	46814	42		
45	34214	35503	36786	38063	39334	40599	41858	43111	44358	45599	46834	43		
11	34236	35525	36807	38084	39355	40620	41878	43131	44378	45619	46854	44		
15	34257	35546	36829	38105	39376	40641	41900	43152	44399	45640	46875	45		
30	34279	35567	36850	38127	39397	40662	41920	43173	44420	45661	46895	46		
45	34300	35589	36871	38148	39418	40683	41941	43194	44441	45681	46916	47		
12	34322	35610	36893	38169	39439	40704	41962	43215	44461	45702	46937	48		
15	34343	35632	36914	38190	39460	40725	41983	43235	44482	45722	46957	49		
3	34365	35653	36935	38211	39482	40746	42004	43256	44503	45743	46978	50		
45	34386	35675	36957	38233	39513	40767	42025	43277	44523	45764	46998	51		
13	34408	35696	36978	38254	39524	40788	42046	43298	44544	45784	47019	52		
15	34429	35717	36999	38275	39545	40809	42067	43319	44565	45805	47039	53		
30	34451	35739	37021	38296	39566	40830	42088	43340	44586	45826	47060	54		
45	34472	35760	37042	38318	39587	40851	42109	43360	44606	45846	47080	55		
14	34494	35782	37063	38339	39608	40872	42130	43381	44627	45867	47101	56		
15	34515	35803	37084	38360	39629	40893	42150	43402	44648	45887	47121	57		
30	34537	35824	37106	38381	39651	40914	42171	43423	44668	45908	47142	58		
45	34558	35846	37127	38402	39672	40933	42192	43444	44689	45929	47162	59		
Sec. 1° 2° 3° 4° 5° 6° 7° 8° 9° 10° 11° 12° 13° 14° 15°														
D. 21. Parts 1 3 4 6 7 8 10 11 13 14 15 17 18 20 21														

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 21. Parts 1 3 4 6 7 8 10 11 13 14 15 17 18 20 21

LOG. SINE SQUARE

	114°				115°				116°			s.
	0'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	
	7h 30m	7h 37m	7h 38m	7h 39m	7h 40m	7h 41m	7h 42m	7h 43m	7h 44m	7h 45m	7h 46m	
0 0	9.8	9.8	9.8	9.8	9.8	9.8	9.8	9.8	9.8	9.8	9.8	0
10	47183	48410	49632	50848	52058	53263	54461	55654	56841	58022	59198	1
20	47203	48431	49653	50868	52078	53283	54481	55674	56861	58042	59217	2
30	47224	48451	49673	50889	52099	53303	54501	55694	56880	58061	59237	3
40	47244	48472	49693	50909	52119	53323	54521	55713	56900	58081	59257	4
1 0	47265	48492	49713	50929	52139	53343	54541	55733	56920	58101	59276	5
15	47285	48512	49734	50949	52159	53363	54561	55753	56940	58120	59295	6
30	47306	48533	49754	50969	52179	53383	54581	55773	56959	58140	59315	7
45	47326	48553	49774	50990	52199	53403	54601	55793	56979	58160	59334	8
2 0	47347	48574	49795	51010	52219	53423	54621	55813	56999	58179	59354	9
15	47367	48594	49815	51030	52239	53443	54640	55832	57019	58199	59373	10
30	47388	48615	49835	51050	52260	53463	54660	55852	57038	58219	59393	11
45	47408	48635	49856	51071	52280	53483	54680	55872	57058	58238	59413	12
3 0	47429	48655	49876	51091	52300	53503	54700	55892	57078	58258	59432	13
15	47449	48676	49896	51111	52320	53523	54720	55912	57097	58277	59452	14
30	47470	48696	49917	51131	52340	53543	54740	55931	57117	58297	59471	15
45	47490	48716	49937	51151	52360	53563	54760	55951	57137	58317	59491	16
4 0	47511	48737	49957	51172	52380	53583	54780	55971	57157	58336	59510	17
15	47531	48757	49977	51192	52400	53603	54800	55991	57176	58356	59530	18
30	47552	48778	49998	51212	52420	53623	54820	56011	57196	58375	59549	19
45	47572	48798	50018	51232	52440	53643	54840	56030	57216	58395	59569	20
5 0	47593	48818	50038	51252	52460	53663	54860	56050	57235	58415	59588	21
15	47613	48839	50059	51272	52481	53683	54879	56070	57255	58434	59608	22
30	47634	48859	50079	51293	52501	53703	54899	56090	57275	58454	59627	23
45	47654	48879	50099	51313	52521	53723	54919	56110	57294	58473	59647	24
6 0	47675	48900	50119	51333	52541	53743	54939	56129	57314	58493	59666	25
15	47695	48920	50140	51353	52561	53763	54959	56149	57334	58513	59686	26
30	47715	48941	50160	51373	52581	53783	54979	56169	57354	58532	59705	27
45	47736	48961	50180	51393	52601	53803	54999	56189	57373	58552	59725	28
7 0	47756	48981	50200	51414	52621	53823	55019	56209	57393	58571	59744	29
15	47777	49002	50221	51434	52641	53843	55039	56228	57413	58591	59764	30
30	47797	49022	50241	51454	52661	53863	55058	56248	57432	58611	59783	31
45	47818	49042	50261	51474	52681	53883	55078	56268	57452	58630	59803	32
8 0	47838	49063	50282	51494	52701	53903	55098	56288	57472	58650	59822	33
15	47859	49083	50302	51515	52721	53923	55118	56308	57491	58669	59842	34
30	47879	49103	50322	51535	52742	53943	55138	56327	57511	58689	59861	35
45	47900	49124	50342	51555	52762	53963	55158	56347	57531	58709	59881	36
9 0	47920	49144	50363	51575	52782	53982	55178	56367	57550	58728	59900	37
15	47941	49165	50383	51595	52802	54002	55197	56387	57570	58748	59920	38
30	47961	49185	50403	51615	52822	54022	55217	56406	57590	58767	59939	39
45	47981	49205	50423	51635	52842	54042	55237	56426	57609	58787	59959	40
10 0	48002	49226	50444	51656	52862	54062	55257	56446	57629	58806	59978	41
15	48022	49246	50464	51676	52882	54082	55277	56466	57649	58826	59998	42
30	48043	49266	50484	51696	52902	54102	55297	56485	57668	58846	60017	43
45	48063	49287	50504	51716	52922	54122	55317	56505	57688	58865	60037	44
11 0	48084	49307	50525	51736	52942	54142	55336	56525	57708	58885	60056	45
15	48104	49327	50545	51756	52962	54162	55356	56545	57727	58904	60075	46
30	48125	49348	50565	51777	52982	54182	55376	56564	57747	58924	60095	47
45	48145	49368	50585	51797	53002	54202	55396	56584	57767	58944	60114	48
12 0	48166	49388	50605	51817	53022	54222	55416	56604	57786	58963	60134	49
15	48186	49409	50626	51837	53042	54242	55436	56624	57806	58983	60153	50
30	48207	49429	50646	51857	53062	54262	55455	56643	57826	59002	60173	51
45	48227	49449	50666	51877	53082	54282	55475	56663	57845	59022	60192	52
13 0	48247	49470	50686	51897	53102	54302	55495	56683	57865	59041	60211	53
15	48267	49490	50707	51918	53123	54322	55515	56703	57885	59061	60231	54
30	48288	49510	50727	51938	53143	54342	55535	56722	57904	59080	60251	55
45	48308	49531	50747	51958	53163	54362	55555	56742	57924	59100	60270	56
14 0	48329	49551	50767	51978	53183	54381	55575	56762	57944	59120	60290	57
15	48349	49571	50788	51998	53203	54401	55594	56782	57963	59139	60309	58
30	48370	49592	50808	52018	53223	54421	55614	56801	57983	59159	60328	59
45	48390	49612	50828	52038	53243	54441	55634	56821	58003	59178	60348	60

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 20. Parts 1 3 4 5 7 8 9 11 12 13 15 16 17 19 20

871

LOG. SINE SQUARE														
	119°		120°				121°				122°		s.	
	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'	15'		
	7° 59'	7° 59'	8° 0'	8° 1'	8° 2'	8° 3'	8° 4'	8° 5'	8° 6'	8° 7'	8° 8'	8° 9'		
0° 0'	72862	73964	75061	76153	77238	78319	79394	80463	81527	82585	83639	84686	0	
15	72881	73983	75080	76171	77256	78337	79411	80481	81545	82603	83656	84704	1	
30	72899	74001	75098	76189	77274	78355	79429	80499	81562	82621	83674	84721	2	
45	72917	74019	75116	76207	77293	78373	79447	80516	81580	82638	83691	84738	3	
1° 0'	72936	74033	75134	76225	77311	78391	79465	80534	81598	82656	83709	84756	4	
15	72954	74056	75152	76243	77329	78408	79483	80552	81615	82673	83726	84773	5	
30	72973	74074	75171	76261	77347	78426	79501	80570	81633	82691	83744	84791	6	
45	72991	74093	75189	76280	77365	78444	79519	80587	81651	82709	83761	84808	7	
2° 0'	73009	74111	75207	76298	77383	78462	79536	80605	81668	82726	83778	84826	8	
15	73028	74129	75225	76316	77401	78480	79554	80623	81686	82744	83796	84843	9	
30	73046	74148	75244	76334	77419	78498	79572	80641	81704	82761	83813	84860	10	
45	73065	74166	75262	76352	77437	78516	79590	80658	81721	82779	83831	84878	11	
3° 0'	73083	74184	75280	76370	77455	78534	79608	80676	81739	82796	83848	84895	12	
15	73101	74202	75298	76389	77473	78552	79626	80694	81757	82814	83866	84913	13	
30	73120	74221	75316	76406	77491	78570	79644	80712	81774	82832	83882	84930	14	
45	73138	74239	75335	76425	77509	78588	79661	80729	81792	82849	83901	84947	15	
4° 0'	73157	74257	75353	76443	77527	78606	79679	80747	81810	82867	83918	84965	16	
15	73175	74276	75371	76461	77545	78624	79697	80765	81827	82884	83936	84982	17	
30	73193	74294	75389	76479	77563	78642	79715	80783	81845	82902	83953	84999	18	
45	73212	74312	75407	76497	77581	78660	79733	80800	81863	82920	83971	85017	19	
5° 0'	73230	74331	75426	76515	77599	78678	79751	80818	81880	82937	83988	85034	20	
15	73249	74349	75444	76533	77617	78696	79768	80836	81898	82955	84000	85052	21	
30	73267	74367	75462	76551	77635	78713	79786	80854	81916	82972	84023	85069	22	
45	73285	74386	75480	76569	77653	78731	79804	80871	81933	82990	84041	85086	23	
6° 0'	73304	74404	75498	76588	77671	78749	79822	80889	81951	83007	84058	85104	24	
15	73322	74422	75517	76606	77689	78767	79840	80907	81969	83025	84076	85121	25	
30	73340	74440	75534	76624	77707	78785	79858	80925	81986	83042	84093	85138	26	
45	73359	74459	75553	76642	77725	78803	79875	80942	82004	83060	84111	85156	27	
7° 0'	73377	74477	75571	76660	77743	78818	79893	80960	82022	83078	84128	85173	28	
15	73396	74495	75589	76678	77761	78839	79911	80978	82039	83095	84146	85191	29	
30	73414	74514	75608	76696	77779	78857	79929	80996	82057	83113	84163	85208	30	
45	73432	74532	75626	76714	77797	78875	79947	81013	82074	83130	84181	85255	31	
8° 0'	73451	74550	75644	76732	77815	78893	79965	81031	82092	83148	84198	85243	32	
15	73469	74568	75662	76750	77833	78911	79982	81049	82110	83165	84215	85260	33	
30	73487	74587	75680	76769	77851	78928	80000	81067	82127	83183	84233	85277	34	
45	73506	74605	75699	76787	77869	78946	80018	81084	82145	83200	84250	85295	35	
9° 0'	73524	74623	75717	76805	77887	78964	80036	81102	82163	83218	84268	85312	36	
15	73543	74641	75735	76823	77905	78982	80054	81120	82180	83235	84285	85330	37	
30	73561	74660	75753	76841	77922	79000	80071	81137	82198	83253	84303	85347	38	
45	73579	74678	75771	76859	77941	79018	80089	81155	82216	83271	84320	85364	39	
10° 0'	73598	74696	75789	76877	77959	79036	80107	81173	82233	83288	84338	85382	40	
15	73616	74715	75808	76895	77977	79054	80125	81191	82251	83306	84355	85399	41	
30	73634	74733	75826	76913	77995	79072	80143	81208	82268	83323	84372	85416	42	
45	73653	74751	75844	76931	78013	79089	80160	81226	82286	83341	84390	85434	43	
11° 0'	73671	74769	75862	76949	78031	79107	80178	81244	82304	83358	84407	85451	44	
15	73689	74788	75880	76967	78049	79125	80196	81261	82321	83376	84425	85468	45	
30	73708	74806	75898	76986	78067	79143	80214	81279	82339	83393	84442	85486	46	
45	73726	74824	75917	77004	78085	79161	80232	81297	82357	83411	84460	85503	47	
12° 0'	73744	74842	75935	77022	78103	79179	80249	81315	82374	83428	84477	85520	48	
15	73763	74861	75953	77040	78121	79197	80267	81332	82392	83446	84495	85538	49	
30	73781	74879	75971	77058	78139	79215	80285	81350	82409	83463	84512	85555	50	
45	73799	74897	75989	77076	78157	79233	80303	81368	82427	83481	84529	85572	51	
13° 0'	73818	74915	76007	77094	78175	79251	80321	81385	82445	83498	84547	85590	52	
15	73836	74934	76026	77112	78193	79268	80338	81403	82462	83516	84564	85607	53	
30	73854	74952	76044	77130	78211	79286	80356	81421	82480	83533	84582	85624	54	
45	73873	74970	76062	77148	78229	79304	80374	81438	82497	83551	84599	85642	55	
14° 0'	73891	74988	76080	77166	78247	79322	80392	81456	82515	83568	84617	85659	56	
15	73909	75007	76098	77184	78265	79340	80410	81474	82533	83586	84634	85677	57	
30	73928	75025	76116	77202	78283	79358	80427	81491	82550	83604	84651	85694	58	
45	73946	75043	76134	77220	78301	79376	80445	81509	82568	83621	84669	85711	59	
Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'														
D. 18. Parts 1 2 4 5 6 7 8 10 11 12 13 14 16 17 18														

LOG. SINE SQUARE															
		122°		123°				124°				125°			
		30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'			
		8° 10'	8° 11'	8° 12'	8° 13'	8° 14'	8° 15'	8° 16'	8° 17'	8° 18'	8° 19'	8° 20'			
0	0	9° 8'	9° 8'	9° 8'	9° 8'	9° 8'	9° 8'	9° 8'	9° 8'	9° 8'	9° 8'	9° 8'	0		
15	85729	86765	87797	88823	89844	90860	91870	92875	93874	94869	95858	1			
30	85746	86783	87814	88840	89861	90876	91887	92891	93891	94885	95874	2			
45	85763	86800	87831	88857	89878	90893	91903	92908	93908	94902	95891	3			
1	0	85781	86817	87848	88874	89895	90910	91920	92925	93924	94918	95907	4		
15	85798	86834	87866	88891	89912	90927	91937	92942	93941	94935	95924	5			
30	85815	86852	87883	88908	89929	90944	91954	92958	93957	94951	95940	6			
45	85832	86869	87900	88925	89946	90961	91971	92975	93974	94968	95956	7			
2	0	85850	86886	87917	88943	89963	90978	91987	92992	93991	94984	95973	8		
15	85867	86903	87934	88960	89980	90995	92004	93008	94007	95001	95989	9			
30	85884	86920	87951	88977	89997	91011	92021	93025	94024	95017	96006	10			
45	85902	86938	87968	88994	90014	91028	92038	93042	94040	95034	96022	11			
3	0	85919	86955	87986	89011	90031	91045	92054	93058	94057	95050	96039	12		
15	85936	86972	88003	89028	90048	91062	92071	93075	94074	95067	96055	13			
30	85954	86989	88020	89045	90065	91079	92088	93092	94090	95083	96071	14			
45	85971	87007	88037	89062	90081	91096	92105	93108	94107	95100	96088	15			
4	0	85988	87024	88054	89079	90098	91113	92122	93125	94123	95116	96104	16		
15	86006	87041	88071	89096	90115	91129	92138	93142	94140	95133	96121	17			
30	86023	87058	88088	89113	90132	91146	92155	93159	94157	95149	96137	18			
45	86040	87075	88105	89130	90149	91163	92172	93175	94173	95166	96154	19			
5	0	86057	87093	88123	89147	90166	91180	92189	93192	94190	95182	96170	20		
15	86075	87110	88140	89164	90183	91197	92205	93209	94206	95199	96186	21			
30	86092	87127	88157	89181	90200	91214	92222	93225	94223	95215	96203	22			
45	86109	87144	88174	89198	90217	91231	92239	93242	94240	95232	96219	23			
6	0	86127	87162	88191	89215	90234	91247	92256	93259	94256	95248	96236	24		
15	86144	87179	88208	89232	90251	91264	92272	93275	94273	95265	96252	25			
30	86161	87196	88225	89249	90268	91281	92289	93292	94289	95281	96268	26			
45	86178	87213	88242	89266	90285	91298	92306	93309	94306	95298	96285	27			
7	0	86196	87230	88259	89283	90302	91315	92323	93325	94322	95314	96301	28		
15	86213	87248	88277	89300	90319	91332	92339	93342	94339	95331	96318	29			
30	86230	87265	88294	89317	90336	91349	92356	93359	94356	95347	96334	30			
45	86248	87282	88311	89334	90352	91365	92373	93375	94372	95364	96350	31			
8	0	86265	87299	88328	89351	90369	91382	92390	93392	94389	95380	96367	32		
15	86282	87316	88345	89368	90386	91399	92407	93409	94405	95397	96383	33			
30	86299	87333	88362	89385	90403	91416	92423	93425	94422	95413	96400	34			
45	86317	87351	88379	89402	90420	91433	92440	93442	94439	95430	96416	35			
9	0	86334	87368	88396	89419	90437	91450	92457	93459	94455	95446	96432	36		
15	86351	87385	88413	89436	90454	91466	92473	93475	94472	95463	96449	37			
30	86368	87402	88430	89453	90471	91483	92490	93492	94488	95479	96465	38			
45	86386	87419	88447	89470	90488	91500	92507	93508	94505	95496	96482	39			
10	0	86403	87437	88465	89487	90505	91517	92524	93525	94521	95512	96498	40		
15	86420	87454	88482	89504	90522	91534	92540	93542	94538	95529	96514	41			
30	86438	87471	88499	89521	90539	91551	92557	93558	94554	95545	96531	42			
45	86455	87488	88516	89538	90555	91567	92574	93575	94571	95562	96547	43			
11	0	86472	87505	88533	89555	90572	91584	92591	93592	94587	95578	96563	44		
15	86489	87522	88550	89572	90589	91601	92607	93608	94604	95595	96580	45			
30	86507	87540	88567	89589	90606	91618	92624	93625	94621	95611	96596	46			
45	86524	87557	88584	89606	90623	91635	92641	93642	94637	95628	96613	47			
12	0	86541	87574	88601	89623	90640	91651	92657	93658	94654	95644	96629	48		
15	86558	87591	88618	89640	90657	91668	92674	93675	94670	95660	96645	49			
30	86576	87608	88635	89657	90674	91685	92691	93691	94687	95677	96662	50			
45	86593	87625	88652	89674	90691	91702	92708	93708	94703	95693	96678	51			
13	0	86610	87643	88670	89691	90708	91719	92724	93725	94720	95710	96694	52		
15	86627	87660	88687	89708	90724	91735	92741	93741	94736	95726	96711	53			
30	86645	87677	88704	89725	90741	91752	92758	93758	94753	95743	96727	54			
45	86662	87694	88721	89742	90758	91769	92775	93775	94770	95759	96744	55			
14	0	86679	87711	88738	89759	90775	91786	92791	93791	94786	95776	96760	56		
15	86696	87728	88755	89776	90792	91803	92808	93808	94803	95792	96776	57			
30	86714	87746	88772	89793	90809	91819	92825	93825	94819	95808	96793	58			
45	86731	87763	88789	89810	90826	91836	92841	93841	94835	95825	96809	59			
50	86748	87780	88806	89827	90843	91853	92858	93858	94852	95841	96825	60			
Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'															
D. 17. Parts 1 2 3 5 6 7 8 9 10 11 12 14 15 16 17															

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 17. Parts 1 2 3 5 6 7 8 9 10 11 12 14 15 16 17

LOG. SINE SQUARE

	125°			126°				127°				s.
	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	
	8° 21"	8° 22"	8° 23"	8° 24"	8° 26"	8° 28"	8° 27"	8° 28"	8° 29"	8° 30"	8° 31"	
0	9'8	9'8	9'8	9'	9'9	9'9	9'9	9'9	9'9	9'9	9'9	
0	96842	97820	98794	99762	00725	01682	02635	03582	04525	05462	06394	0
15	96858	97836	98810	99778	00741	01698	02651	03598	04540	05477	06409	1
30	96874	97853	98826	99794	00757	01714	02667	03614	04556	05493	06425	2
45	96891	97869	98842	99810	00773	01730	02682	03630	04572	05508	06440	3
1	96907	97885	98858	99826	00789	01746	02698	03645	04587	05524	06456	4
15	96923	97902	98874	99842	00805	01762	02714	03661	04603	05539	06471	5
30	96940	97918	98891	99858	00821	01778	02730	03677	04618	05555	06486	6
45	96956	97934	98907	99874	00837	01794	02746	03693	04634	05571	06502	7
2	96972	97950	98923	99890	00853	01810	02762	03708	04650	05586	06517	8
15	96985	97967	98939	99906	00869	01826	02777	03724	04665	05602	06533	9
30	97005	97983	98955	99923	00885	01842	02793	03740	04681	05617	06548	10
45	97021	97999	98971	99939	00901	01857	02809	03756	04697	05633	06564	11
3	97038	98015	98988	99955	00917	01873	02825	03771	04712	05648	06579	12
15	97054	98032	99004	99971	00933	01889	02841	03787	04728	05664	06595	13
30	97070	98048	99020	99987	00949	01905	02856	03803	04744	05679	06610	14
45	97087	98064	99036	99003	00965	01921	02872	03818	04759	05695	06626	15
4	97103	98080	99052	99019	00981	01937	02888	03834	04775	05711	06641	16
15	97119	98097	99068	99035	00997	01953	02904	03850	04791	05726	06657	17
30	97136	98113	99085	99051	01012	01969	02920	03866	04806	05742	06672	18
45	97152	98129	99101	99067	01028	01985	02935	03881	04822	05757	06688	19
5	97168	98145	99117	99083	01044	02001	02951	03897	04837	05773	06703	20
15	97185	98162	99133	99099	01060	02016	02967	03913	04853	05788	06719	21
30	97201	98178	99149	99115	01076	02032	02983	03928	04869	05804	06734	22
45	97217	98194	99165	99131	01092	02048	02999	03944	04884	05819	06749	23
6	97234	98210	99181	99147	01108	02064	03015	03960	04900	05835	06765	24
15	97250	98226	99198	99164	01124	02080	03030	03976	04916	05851	06780	25
30	97266	98243	99214	99180	01140	02096	03046	03991	04931	05866	06796	26
45	97283	98259	99230	99196	01156	02112	03062	04007	04947	05882	06811	27
7	97299	98275	99246	99212	01172	02128	03078	04023	04962	05897	06827	28
15	97315	98291	99262	99228	01188	02144	03094	04038	04978	05913	06842	29
30	97332	98307	99278	99244	01204	02159	03109	04054	04994	05928	06858	30
45	97348	98324	99294	99260	01220	02175	03125	04070	05009	05944	06873	31
8	97364	98340	99311	99276	01236	02191	03141	04086	05025	05959	06889	32
15	97380	98356	99327	99292	01252	02207	03157	04101	05041	05975	06904	33
30	97397	98372	99343	99308	01268	02223	03172	04117	05056	05990	06919	34
45	97413	98389	99359	99324	01284	02239	03188	04133	05072	06006	06935	35
9	97429	98405	99375	99340	01300	02255	03204	04148	05087	06021	06950	36
15	97446	98421	99391	99356	01316	02270	03220	04164	05103	06037	06966	37
30	97462	98437	99407	99372	01332	02286	03236	04180	05119	06052	06981	38
45	97478	98453	99424	99388	01348	02302	03251	04195	05134	06068	06997	39
10	97495	98470	99440	99404	01364	02318	03267	04211	05150	06083	07012	40
15	97511	98486	99456	99420	01380	02334	03283	04227	05165	06099	07027	41
30	97527	98502	99472	99436	01396	02350	03299	04242	05181	06115	07043	42
45	97543	98518	99488	99452	01412	02366	03314	04258	05197	06130	07058	43
11	97560	98535	99504	99468	01427	02381	03330	04274	05212	06146	07074	44
15	97576	98551	99520	99484	01443	02397	03346	04289	05228	06161	07089	45
30	97592	98567	99536	99500	01459	02413	03362	04305	05243	06177	07105	46
45	97609	98583	99552	99516	01475	02429	03377	04321	05259	06192	07120	47
12	97625	98599	99568	99532	01491	02445	03393	04337	05275	06208	07135	48
15	97641	98616	99585	99548	01507	02461	03409	04352	05290	06223	07151	49
30	97658	98632	99601	99565	01523	02477	03425	04368	05306	06239	07166	50
45	97674	98648	99617	99581	01539	02492	03441	04384	05321	06254	07182	51
13	97690	98664	99633	99597	01555	02508	03456	04399	05337	06270	07197	52
15	97706	98680	99649	99613	01571	02524	03472	04415	05353	06285	07213	53
30	97723	98697	99665	99629	01587	02540	03488	04431	05368	06301	07228	54
45	97739	98713	99681	99645	01603	02556	03504	04446	05384	06316	07243	55
14	97755	98729	99697	99661	01619	02572	03519	04462	05399	06332	07259	56
15	97771	98745	99713	99677	01635	02587	03535	04478	05415	06347	07274	57
30	97788	98761	99730	99693	01651	02603	03551	04493	05430	06363	07290	58
45	97804	98777	99746	99709	01666	02619	03567	04509	05446	06378	07305	59

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 16. Parts 1 2 3 4 5 6 7 8 9 11 12 13 14 15 16

LOG. SINE SQUARE													
	128°				199°				180°			A.	
	0'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'		
	8° 32'	8° 33'	8° 34'	8° 35'	8° 36'	8° 37'	8° 38'	8° 39'	8° 40'	8° 41'	8° 42'		
0	0	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	0	
	15	07320	08242	09159	10076	10992	11893	12774	13665	14551	15433	16309	1
	30	07336	08257	09174	10085	10992	11893	12789	13680	14566	15447	16323	2
	45	07351	08273	09189	10100	11007	11908	12804	13695	14581	15462	16338	3
1	0	07367	08288	09204	10116	11022	11923	12819	13710	14596	15476	16352	4
	15	07382	08303	09220	10131	11037	11938	12834	13724	14610	15491	16367	5
	30	07397	08319	09235	10146	11052	11953	12848	13739	14625	15506	16381	6
	45	07413	08334	09250	10161	11067	11968	12863	13754	14640	15520	16396	7
2	0	07428	08349	09265	10176	11082	11983	12878	13769	14654	15535	16411	8
	15	07444	08365	09280	10191	11097	11998	12893	13784	14669	15550	16425	9
	30	07459	08380	09296	10206	11112	12012	12908	13799	14684	15564	16440	10
3	0	07474	08395	09311	10222	11127	12027	12923	13813	14699	15579	16454	11
	15	07490	08410	09326	10237	11142	12042	12938	13828	14713	15594	16469	12
	30	07505	08426	09341	10252	11157	12057	12953	13843	14728	15608	16483	13
	45	07520	08441	09357	10267	11172	12072	12968	13858	14743	15623	16498	14
4	0	07536	08456	09372	10282	11187	12087	12982	13873	14757	15637	16512	15
	15	07551	08472	09387	10297	11202	12102	12997	13887	14772	15652	16527	16
	30	07567	08487	09402	10312	11217	12117	13002	13902	14787	15667	16541	17
	45	07582	08502	09417	10327	11232	12132	13017	13917	14801	15681	16556	18
5	0	07597	08518	09433	10343	11247	12147	13042	13932	14816	15696	16570	19
	15	07613	08533	09448	10358	11262	12162	13057	13946	14831	15710	16585	20
	30	07628	08548	09463	10373	11277	12177	13072	13961	14846	15725	16600	21
	45	07644	08563	09478	10388	11292	12192	13087	13976	14860	15740	16614	22
6	0	07659	08579	09493	10403	11308	12207	13101	13991	14875	15754	16629	23
	15	07674	08594	09509	10418	11323	12222	13116	14006	14890	15769	16643	24
	30	07690	08609	09524	10433	11338	12237	13131	14020	14904	15783	16658	25
	45	07705	08625	09539	10448	11353	12252	13146	14035	14919	15798	16672	26
7	0	07720	08640	09554	10464	11368	12267	13161	14049	14934	15813	16687	27
	15	07736	08655	09569	10479	11383	12282	13176	14065	14948	15827	16701	28
	30	07751	08670	09585	10494	11398	12297	13191	14079	14963	15842	16716	29
	45	07766	08686	09600	10509	11413	12312	13205	14094	14978	15857	16730	30
8	0	07782	08701	09615	10524	11428	12326	13220	14109	14993	15871	16745	31
	15	07797	08716	09630	10539	11443	12341	13235	14124	15007	15886	16759	32
	30	07813	08731	09645	10554	11458	12356	13250	14139	15022	15900	16774	33
	45	07828	08747	09661	10569	11473	12371	13265	14153	15037	15915	16788	34
9	0	07843	08762	09676	10584	11488	12386	13280	14168	15051	15930	16803	35
	15	07859	08777	09691	10599	11503	12401	13294	14183	15066	15944	16817	36
	30	07874	08793	09706	10615	11518	12416	13309	14198	15081	15959	16832	37
	45	07889	08808	09721	10630	11533	12431	13324	14212	15095	15973	16846	38
10	0	07906	08823	09736	10645	11548	12446	13339	14227	15110	15988	16861	39
	15	07920	08838	09752	10660	11563	12461	13354	14242	15125	16003	16875	40
	30	07935	08854	09767	10675	11578	12476	13369	14257	15139	16017	16890	41
	45	07951	08869	09782	10690	11593	12491	13383	14271	15154	16032	16904	42
11	0	07966	08884	09797	10705	11608	12506	13398	14286	15169	16046	16919	43
	15	07981	08899	09812	10720	11623	12521	13413	14301	15183	16061	16933	44
	30	07997	08915	09828	10735	11638	12535	13428	14316	15198	16075	16948	45
	45	08012	08930	09843	10750	11653	12550	13443	14330	15213	16090	16962	46
12	0	08027	08945	09858	10765	11668	12565	13458	14345	15227	16105	16977	47
	15	08043	08960	09873	10781	11683	12580	13472	14360	15242	16119	16991	48
	30	08058	08976	09888	10796	11698	12595	13487	14374	15257	16134	17006	49
	45	08073	08991	09903	10811	11713	12610	13502	14389	15271	16148	17020	50
13	0	08089	09006	09919	10826	11728	12625	13517	14404	15286	16163	17035	51
	15	08104	09021	09934	10841	11743	12640	13532	14419	15301	16178	17049	52
	30	08119	09037	09949	10856	11758	12655	13547	14433	15315	16192	17064	53
	45	08135	09052	09964	10871	11773	12670	13561	14448	15330	16207	17078	54
14	0	08150	09067	09979	10886	11788	12685	13576	14463	15345	16221	17093	55
	15	08165	09082	09994	10901	11803	12700	13591	14478	15359	16236	17107	56
	30	08181	09098	10009	10916	11818	12714	13606	14492	15374	16250	17122	57
	45	08196	09113	10025	10931	11833	12729	13621	14507	15389	16265	17136	58
15	0	08211	09128	10040	10946	11848	12744	13636	14522	15403	16279	17151	59
	15	08227	09143	10055	10961	11863	12759	13650	14537	15418	16294	17165	60

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 15. Parts 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15

LOG. SINE SQUARE

	130°		131°				132°				133°				N.
	48'		0'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	
	8° 43'	8° 44'	8° 45'	8° 46'	8° 47'	8° 48'	8° 49'	8° 50'	8° 51'	8° 52'	8° 53'	8° 54'	8° 55'	8° 56'	
0	0	9'9	17180	18046	18907	19763	20614	21460	22302	23138	23969	24794	25617	26437	0
1	0	15	17194	18060	18921	19777	20628	21474	22316	23152	23983	24809	25631	26451	1
2	0	30	17209	18075	18936	19791	20642	21488	22330	23166	23997	24823	25644	26464	2
3	0	45	17223	18089	18950	19806	20657	21502	22343	23179	24011	24837	25658	26483	3
4	0	15	17238	18103	18964	19820	20671	21516	22357	23193	24024	24850	25672	26502	4
5	0	30	17252	18118	18978	19834	20685	21531	22371	23207	24038	24864	25685	26517	5
6	0	45	17267	18132	18993	19848	20699	21545	22385	23221	24052	24878	25699	26531	6
7	0	15	17281	18147	19007	19863	20713	21559	22399	23235	24066	24892	25713	26547	7
8	0	30	17296	18161	19021	19877	20727	21573	22413	23249	24079	24905	25726	26562	8
9	0	45	17310	18175	19036	19891	20741	21587	22427	23263	24093	24919	25740	26577	9
10	0	30	17324	18190	19050	19905	20755	21601	22441	23277	24107	24933	25753	26593	10
11	0	45	17339	18204	19064	19919	20770	21615	22455	23291	24121	24947	25767	26607	11
12	0	15	17353	18218	19079	19934	20784	21629	22469	23304	24134	24960	25781	26621	12
13	0	30	17368	18233	19093	19948	20798	21643	22483	23318	24148	24974	25794	26635	13
14	0	45	17382	18247	19107	19962	20812	21657	22497	23332	24162	24988	25808	26649	14
15	0	15	17397	18262	19121	19976	20826	21671	22511	23346	24176	25001	25822	26663	15
16	0	30	17411	18276	19136	19990	20840	21685	22525	23360	24190	25015	25835	26677	16
17	0	45	17426	18290	19150	20005	20854	21699	22539	23374	24203	25029	25849	26691	17
18	0	15	17440	18305	19164	20019	20868	21713	22553	23388	24217	25043	25863	26705	18
19	0	30	17454	18319	19179	20033	20883	21727	22567	23402	24231	25056	25876	26719	19
20	0	45	17469	18333	19193	20047	20897	21741	22581	23415	24245	25070	25890	26733	20
21	0	15	17483	18348	19207	20061	20911	21755	22595	23429	24258	25084	25903	26747	21
22	0	30	17498	18362	19221	20076	20925	21769	22609	23443	24272	25097	25917	26761	22
23	0	45	17512	18377	19236	20090	20939	21783	22623	23457	24286	25111	25931	26775	23
24	0	15	17527	18391	19250	20104	20953	21797	22637	23471	24299	25125	25944	26789	24
25	0	30	17541	18405	19264	20118	20967	21811	22651	23485	24313	25138	25958	26803	25
26	0	45	17556	18419	19278	20132	20981	21825	22664	23499	24327	25152	25972	26817	26
27	0	15	17570	18434	19293	20147	20995	21839	22678	23512	24341	25166	25985	26831	27
28	0	30	17585	18448	19307	20161	21010	21853	22692	23526	24354	25180	25999	26845	28
29	0	45	17599	18463	19321	20175	21024	21868	22706	23540	24368	25193	26012	26859	29
30	0	15	17613	18477	19336	20189	21038	21882	22720	23554	24382	25207	26026	26873	30
31	0	30	17628	18491	19350	20203	21052	21896	22734	23568	24396	25221	26040	26887	31
32	0	45	17642	18506	19364	20218	21066	21910	22748	23582	24410	25234	26053	26901	32
33	0	15	17657	18520	19378	20232	21080	21924	22762	23596	24424	25248	26067	26915	33
34	0	30	17671	18534	19393	20246	21094	21938	22776	23609	24438	25262	26080	26929	34
35	0	45	17686	18549	19407	20260	21108	21952	22790	23623	24452	25275	26094	26943	35
36	0	15	17700	18563	19421	20274	21122	21966	22804	23637	24466	25289	26108	26957	36
37	0	30	17714	18577	19435	20288	21136	21980	22818	23651	24479	25303	26121	26971	37
38	0	45	17729	18592	19450	20303	21151	21994	22832	23665	24493	25316	26135	26985	38
39	0	15	17743	18606	19464	20317	21165	22008	22846	23679	24507	25330	26148	26999	39
40	0	30	17758	18620	19478	20331	21179	22022	22860	23693	24521	25344	26162	27013	40
41	0	45	17772	18635	19492	20345	21193	22036	22874	23707	24534	25357	26176	27027	41
42	0	15	17787	18649	19507	20359	21207	22050	22887	23721	24548	25371	26189	27041	42
43	0	30	17801	18663	19521	20373	21221	22064	22901	23735	24562	25385	26203	27055	43
44	0	45	17815	18678	19535	20388	21235	22078	22915	23749	24576	25398	26216	27068	44
45	0	15	17830	18692	19549	20402	21249	22092	22929	23762	24589	25412	26230	27082	45
46	0	30	17844	18706	19564	20416	21263	22106	22943	23776	24603	25426	26244	27096	46
47	0	45	17859	18721	19578	20430	21278	22120	22957	23790	24617	25439	26257	27109	47
48	0	15	17873	18735	19592	20444	21292	22134	22971	23804	24631	25453	26271	27123	48
49	0	30	17887	18749	19606	20458	21306	22148	22985	23818	24644	25467	26284	27137	49
50	0	45	17902	18764	19621	20473	21320	22162	22999	23831	24658	25480	26298	27151	50
51	0	15	17916	18778	19635	20487	21334	22176	23013	23845	24672	25494	26311	27165	51
52	0	30	17931	18792	19649	20501	21348	22190	23027	23859	24686	25508	26325	27179	52
53	0	45	17945	18807	19663	20515	21362	22204	23040	23873	24699	25521	26339	27193	53
54	0	15	17959	18821	19678	20529	21376	22218	23054	23886	24713	25535	26352	27207	54
55	0	30	17974	18835	19692	20543	21390	22232	23068	23900	24727	25549	26366	27221	55
56	0	45	17988	18850	19706	20558	21404	22246	23082	23914	24740	25562	26379	27235	56
57	0	15	18003	18864	19720	20572	21418	22260	23096	23928	24754	25576	26393	27249	57
58	0	30	18017	18878	19735	20586	21432	22274	23110	23942	24768	25590	26407	27263	58
59	0	45	18031	18893	19749	20600	21446	22288	23124	23955	24782	25603	26420	27277	59

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 14. Parts 1 2 3 4 5 6 7 8 9 10 11 12 13 14

LOG. SINE SQUARE														
	133°		134°				135°				136°		c.	
	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'			
	8 ^h 54 ^m	8 ^h 55 ^m	8 ^h 56 ^m	8 ^h 57 ^m	8 ^h 58 ^m	8 ^h 59 ^m	9 ^h 0 ^m	9 ^h 1 ^m	9 ^h 2 ^m	9 ^h 3 ^m	9 ^h 4 ^m			
0	9'9	7'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9		0	
15	26434	27245	28052	28854	29651	30443	31231	32013	32791	33564	34332		1	
30	26447	27259	28066	28867	29664	30457	31244	32026	32804	33576	34345		2	
45	26461	27272	28079	28881	29678	30470	31257	32039	32817	33589	34357		3	
1	26474	27286	28092	28894	29691	30483	31270	32052	32830	33602	34370		4	
15	26488	27299	28106	28907	29704	30496	31283	32065	32842	33615	34383		5	
30	26501	27313	28119	28921	29717	30509	31296	32078	32855	33628	34396		6	
45	26515	27326	28131	28934	29731	30522	31309	32091	32868	33641	34408		7	
2	26529	27340	28146	28947	29744	30535	31322	32104	32881	33653	34421		8	
15	26542	27353	28159	28961	29757	30549	31335	32117	32894	33666	34434		9	
30	26556	27367	28173	28974	29770	30562	31348	32130	32907	33679	34447		10	
45	26569	27380	28186	28987	29783	30575	31361	32143	32920	33692	34459		11	
3	26583	27394	28199	29000	29797	30588	31374	32156	32933	33705	34472		12	
15	26596	27407	28213	29014	29810	30601	31388	32169	32946	33718	34485		13	
30	26610	27421	28226	29027	29823	30614	31401	32182	32959	33730	34498		14	
45	26623	27434	28240	29040	29836	30627	31414	32195	32972	33743	34510		15	
4	26637	27448	28253	29054	29850	30641	31427	32208	32984	33756	34523		16	
15	26651	27461	28266	29067	29863	30654	31440	32221	32997	33769	34536		17	
30	26664	27474	28280	29080	29876	30667	31453	32234	33010	33782	34549		18	
45	26678	27488	28293	29094	29889	30680	31466	32247	33023	33795	34561		19	
5	26691	27501	28307	29107	29902	30693	31479	32260	33036	33807	34574		20	
15	26705	27515	28320	29120	29916	30706	31492	32273	33049	33820	34587		21	
30	26718	27528	28333	29134	29929	30719	31505	32286	33062	33833	34599		22	
45	26732	27542	28347	29147	29942	30733	31518	32299	33075	33846	34612		23	
6	26745	27555	28360	29160	29955	30746	31531	32312	33088	33859	34625		24	
15	26759	27569	28374	29173	29969	30759	31544	32325	33100	33871	34638		25	
30	26772	27582	28387	29187	29982	30772	31557	32338	33113	33884	34650		26	
45	26786	27596	28400	29200	29995	30785	31570	32351	33126	33897	34663		27	
7	26800	27609	28414	29213	30008	30798	31583	32364	33139	33910	34676		28	
15	26813	27622	28427	29227	30021	30811	31596	32377	33152	33923	34688		29	
30	26827	27636	28440	29240	30035	30825	31609	32390	33165	33936	34701		30	
45	26840	27649	28454	29253	30048	30838	31622	32403	33178	33948	34714		31	
8	26854	27663	28467	29266	30061	30851	31636	32416	33191	33961	34727		32	
15	26867	27676	28480	29280	30074	30864	31649	32429	33204	33974	34739		33	
30	26881	27690	28494	29293	30087	30877	31662	32441	33216	33987	34752		34	
45	26894	27703	28507	29306	30101	30890	31675	32454	33229	34000	34765		35	
9	26908	27716	28520	29320	30114	30903	31688	32467	33242	34012	34777		36	
15	26921	27730	28534	29333	30127	30916	31701	32480	33255	34025	34790		37	
30	26935	27743	28547	29346	30140	30929	31714	32493	33268	34038	34803		38	
45	26948	27757	28561	29359	30153	30943	31727	32506	33281	34051	34816		39	
10	26962	27770	28574	29373	30167	30956	31740	32519	33294	34063	34828		40	
15	26975	27784	28587	29386	30180	30969	31753	32532	33307	34076	34841		41	
30	26989	27797	28601	29399	30193	30982	31766	32545	33319	34089	34854		42	
45	27002	27811	28614	29413	30206	30995	31779	32558	33332	34102	34866		43	
11	27016	27824	28627	29426	30219	31008	31792	32571	33345	34115	34879		44	
15	27029	27837	28641	29439	30233	31021	31805	32584	33358	34127	34892		45	
30	27043	27851	28654	29452	30246	31034	31818	32597	33371	34140	34905		46	
45	27056	27864	28667	29466	30259	31047	31831	32610	33384	34153	34917		47	
12	27070	27878	28681	29479	30272	31060	31844	32623	33397	34166	34930		48	
15	27083	27891	28694	29492	30285	31074	31857	32636	33409	34178	34943		49	
30	27097	27905	28707	29505	30298	31087	31870	32649	33422	34191	34955		50	
45	27110	27918	28721	29519	30312	31100	31883	32662	33435	34204	34968		51	
13	27124	27931	28734	29532	30325	31113	31896	32674	33448	34217	34981		52	
15	27137	27945	28747	29545	30338	31126	31909	32687	33461	34230	34993		53	
30	27151	27958	28761	29558	30351	31139	31922	32700	33474	34242	35006		54	
45	27164	27972	28774	29572	30364	31152	31935	32713	33487	34255	35019		55	
14	27178	27985	28787	29585	30377	31165	31948	32726	33500	34268	35031		56	
15	27191	27999	28801	29598	30391	31178	31961	32739	33512	34281	35044		57	
30	27205	28012	28814	29611	30404	31191	31974	32752	33525	34293	35057		58	
45	27218	28025	28827	29625	30417	31204	31987	32765	33538	34306	35070		59	
50	27232	28039	28841	29638	30430	31218	32000	32778	33551	34319	35082		60	

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 13. Parts 1 2 3 4 5 6 7 8 9 10 10 11 12 13

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 13. Parts 1 2 3 4 5 6 7 8 9 10 11 12 13

LOG. SINE SQUARE

	136°			137°				138°				s.
	18'	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	
	9 ^h 5 ^m	9 ^h 6 ^m	9 ^h 7 ^m	9 ^h 8 ^m	9 ^h 9 ^m	9 ^h 10 ^m	9 ^h 11 ^m	9 ^h 12 ^m	9 ^h 13 ^m	9 ^h 14 ^m	9 ^h 15 ^m	
0	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	0
1	35095	35853	36607	37356	38100	38839	39574	40303	41029	41749	42464	1
2	35108	35866	36620	37368	38112	38851	39586	40316	41041	41761	42476	2
3	35120	35879	36632	37381	38125	38864	39598	40328	41053	41773	42488	3
4	35133	35891	36645	37393	38137	38876	39610	40340	41065	41785	42500	4
5	35146	35904	36657	37405	38149	38888	39622	40352	41077	41797	42512	5
6	35158	35916	36670	37418	38162	38901	39635	40364	41089	41809	42524	6
7	35171	35929	36682	37430	38174	38913	39647	40376	41101	41821	42536	7
8	35184	35942	36695	37443	38186	38925	39659	40388	41113	41833	42548	8
9	35196	35954	36707	37455	38199	38937	39671	40400	41125	41844	42559	9
10	35209	35967	36720	37468	38211	38950	39683	40413	41137	41856	42571	10
11	35222	35979	36732	37480	38223	38962	39696	40425	41149	41868	42583	11
12	35234	35992	36745	37493	38236	38974	39708	40437	41161	41880	42595	12
13	35247	36004	36757	37505	38248	38986	39720	40449	41173	41892	42607	13
14	35260	36017	36770	37517	38261	38999	39732	40461	41185	41904	42619	14
15	35272	36030	36782	37530	38273	39011	39744	40473	41197	41916	42631	15
16	35285	36042	36795	37542	38285	39023	39757	40485	41209	41928	42643	16
17	35298	36055	36807	37555	38297	39035	39769	40497	41221	41940	42654	17
18	35310	36067	36820	37567	38310	39048	39781	40509	41233	41952	42666	18
19	35323	36080	36832	37579	38322	39060	39793	40521	41245	41964	42678	19
20	35336	36092	36845	37592	38334	39072	39805	40534	41257	41976	42690	20
21	35348	36105	36857	37604	38347	39084	39817	40546	41269	41988	42702	21
22	35361	36118	36870	37617	38359	39097	39830	40558	41281	42000	42714	22
23	35373	36130	36882	37629	38371	39109	39842	40570	41293	42012	42726	23
24	35386	36143	36895	37642	38384	39121	39854	40582	41305	42024	42737	24
25	35399	36155	36907	37654	38396	39134	39866	40594	41317	42036	42749	25
26	35411	36168	36920	37666	38408	39146	39878	40606	41329	42048	42761	26
27	35424	36180	36932	37679	38421	39158	39890	40618	41341	42059	42773	27
28	35437	36193	36945	37691	38433	39170	39903	40630	41353	42071	42785	28
29	35449	36206	36957	37704	38445	39183	39915	40642	41365	42083	42797	29
30	35462	36218	36969	37716	38458	39195	39927	40654	41377	42095	42809	30
31	35475	36231	36982	37728	38470	39207	39939	40667	41389	42107	42820	31
32	35487	36243	36994	37741	38482	39219	39951	40679	41401	42119	42832	32
33	35500	36256	37007	37753	38495	39232	39963	40691	41413	42131	42844	33
34	35513	36268	37019	37766	38507	39244	39976	40703	41425	42143	42856	34
35	35525	36281	37032	37778	38519	39256	39988	40715	41437	42155	42868	35
36	35538	36294	37044	37790	38532	39268	40000	40727	41449	42167	42880	36
37	35551	36306	37057	37803	38544	39280	40012	40739	41461	42179	42891	37
38	35563	36319	37069	37815	38556	39293	40024	40751	41473	42191	42903	38
39	35576	36331	37082	37828	38569	39305	40036	40763	41485	42203	42915	39
40	35588	36344	37094	37840	38581	39317	40049	40775	41497	42214	42927	40
41	35601	36356	37107	37852	38593	39329	40061	40787	41509	42226	42939	41
42	35614	36369	37119	37865	38606	39342	40073	40799	41521	42238	42951	42
43	35626	36381	37132	37877	38618	39354	40085	40811	41533	42250	42963	43
44	35639	36394	37144	37890	38630	39366	40097	40824	41545	42262	42974	44
45	35652	36406	37157	37902	38642	39378	40109	40836	41557	42274	42986	45
46	35664	36419	37169	37914	38655	39390	40121	40848	41569	42286	42998	46
47	35677	36431	37181	37927	38667	39403	40134	40860	41581	42298	43010	47
48	35689	36444	37194	37939	38679	39415	40146	40872	41593	42310	43022	48
49	35702	36457	37206	37951	38692	39427	40158	40884	41605	42322	43033	49
50	35715	36469	37219	37964	38704	39439	40170	40896	41617	42334	43045	50
51	35727	36482	37231	37976	38716	39452	40182	40908	41629	42345	43057	51
52	35740	36494	37244	37989	38729	39464	40194	40920	41641	42357	43069	52
53	35753	36507	37256	38001	38741	39476	40206	40932	41653	42369	43081	53
54	35765	36519	37269	38013	38753	39488	40219	40944	41665	42381	43093	54
55	35778	36532	37281	38026	38765	39500	40231	40956	41677	42393	43104	55
56	35790	36544	37294	38038	38778	39513	40243	40968	41689	42405	43116	56
57	35803	36557	37306	38050	38790	39525	40255	40980	41701	42417	43128	57
58	35816	36569	37318	38063	38802	39537	40267	40992	41713	42429	43140	58
59	35828	36582	37331	38075	38815	39549	40279	41004	41725	42441	43152	59
60	35841	36594	37343	38087	38827	39561	40291	41016	41737	42452	43163	60

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14'
D. 12. Parts 1 2 2 3 4 5 6 6 7 8 9 10 11 12

TABLE 69

LOG. SINE SQUARE														
		139°				140°				141°				
		0'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'		
		9° 16'	9° 17'	9° 18'	9° 19'	9° 20'	9° 21'	9° 22'	9° 23'	9° 24'	9° 25'	9° 26'		
6	0	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	0	
15	0	43175	43181	44583	45280	45972	46659	47342	48020	48693	49362	50026	1	
30	0	43187	43193	44594	45291	45983	46670	47353	48031	48704	49373	50037	2	
45	0	43199	43205	44606	45303	45995	46682	47364	48042	48716	49384	50048	3	
1	0	43211	43217	44618	45314	46006	46693	47376	48054	48727	49395	50059	4	
15	0	43222	43228	44629	45326	46018	46705	47387	48065	48738	49406	50070	5	
30	0	43234	43240	44641	45337	46029	46716	47398	48076	48749	49417	50082	6	
45	0	43246	43252	44653	45349	46041	46727	47410	48087	48760	49428	50092	7	
2	0	43258	43264	44664	45361	46052	46739	47421	48099	48771	49439	50103	8	
15	0	43270	43276	44676	45372	46064	46750	47432	48110	48782	49451	50114	9	
30	0	43281	43287	44688	45384	46075	46762	47444	48121	48794	49462	50125	10	
45	0	43293	43299	44699	45395	46086	46773	47455	48132	48805	49473	50136	11	
3	0	43305	43311	44711	45407	46098	46785	47466	48144	48816	49484	50147	12	
15	0	43317	43323	44723	45418	46109	46796	47478	48155	48827	49495	50158	13	
30	0	43329	43335	44734	45429	46121	46807	47489	48166	48838	49506	50169	14	
45	0	43340	43346	44746	45441	46132	46819	47500	48177	48849	49517	50180	15	
4	0	43352	43358	44757	45453	46144	46830	47512	48189	48861	49528	50191	16	
15	0	43364	43370	44769	45465	46155	46842	47523	48200	48872	49539	50202	17	
30	0	43376	43382	44781	45476	46167	46853	47534	48211	48883	49550	50213	18	
45	0	43388	43394	44792	45488	46178	46864	47546	48222	48894	49561	50224	19	
5	0	43399	43405	44804	45499	46190	46876	47557	48233	48905	49573	50235	20	
15	0	43411	43417	44816	45511	46201	46887	47568	48245	48916	49584	50246	21	
30	0	43423	43429	44827	45522	46213	46898	47579	48256	48928	49595	50257	22	
45	0	43435	43441	44839	45534	46224	46910	47591	48267	48939	49606	50268	23	
6	0	43446	43452	44850	45545	46236	46921	47602	48278	48950	49617	50279	24	
15	0	43458	43464	44862	45557	46247	46933	47613	48290	48961	49628	50290	25	
30	0	43470	43476	44874	45569	46259	46944	47625	48301	48972	49639	50301	26	
45	0	43482	43488	44885	45580	46270	46955	47636	48312	48983	49650	50312	27	
7	0	43494	43498	44897	45592	46281	46967	47647	48323	48995	49661	50323	28	
15	0	43505	43509	44909	45603	46293	46978	47659	48335	49006	49672	50334	29	
30	0	43517	43521	44920	45615	46304	46990	47670	48346	49017	49684	50345	30	
45	0	43529	43533	44932	45626	46316	47001	47681	48357	49028	49694	50356	31	
8	0	43541	43544	44943	45638	46327	47012	47693	48368	49039	49705	50367	32	
15	0	43552	43556	44955	45649	46339	47024	47704	48379	49050	49716	50378	33	
30	0	43564	43568	44967	45661	46350	47035	47715	48391	49062	49728	50389	34	
45	0	43576	43579	44978	45672	46362	47046	47726	48402	49073	49739	50400	35	
9	0	43588	43591	44990	45684	46373	47058	47738	48413	49084	49750	50411	36	
15	0	43599	43603	45001	45695	46385	47069	47749	48424	49095	49761	50422	37	
30	0	43611	43614	45013	45707	46396	47081	47760	48436	49106	49772	50433	38	
45	0	43623	43626	45025	45718	46407	47092	47772	48447	49117	49783	50444	39	
10	0	43635	43638	45036	45730	46419	47103	47783	48458	49128	49794	50455	40	
15	0	43647	43650	45048	45741	46430	47115	47794	48469	49139	49805	50466	41	
30	0	43658	43661	45059	45753	46442	47126	47805	48480	49151	49816	50477	42	
45	0	43670	43673	45071	45765	46453	47137	47817	48492	49162	49827	50488	43	
11	0	43682	43685	45083	45776	46465	47149	47828	48503	49173	49838	50499	44	
15	0	43694	43696	45094	45788	46476	47160	47839	48514	49184	49849	50510	45	
30	0	43705	43708	45106	45799	46488	47171	47851	48525	49195	49860	50521	46	
45	0	43717	43719	45117	45811	46499	47183	47862	48536	49206	49871	50532	47	
12	0	43729	43731	45129	45822	46510	47194	47874	48548	49217	49882	50543	48	
15	0	43741	43743	45141	45834	46522	47206	47884	48559	49228	49893	50554	49	
30	0	43752	43754	45152	45845	46533	47217	47896	48570	49240	49904	50565	50	
45	0	43764	43766	45164	45857	46545	47228	47907	48581	49251	49916	50576	51	
13	0	43776	43778	45175	45868	46556	47240	47918	48592	49262	49927	50587	52	
15	0	43787	43789	45187	45880	46568	47251	47930	48604	49273	49938	50598	53	
30	0	43799	43801	45199	45891	46579	47262	47941	48615	49284	49949	50609	54	
45	0	43811	43813	45210	45903	46591	47274	47952	48626	49295	49960	50620	55	
14	0	43823	43825	45222	45914	46602	47285	47963	48637	49306	49971	50631	56	
15	0	43834	43836	45233	45926	46613	47296	47975	48648	49317	49982	50642	57	
30	0	43846	43848	45245	45937	46625	47308	47986	48660	49328	49993	50653	58	
45	0	43858	43860	45256	45949	46636	47319	47997	48671	49340	50004	50663	59	
15	0	43870	43871	45268	45960	46648	47330	48008	48682	49351	50015	50674	60	
Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'														
D. 11. Parts 1 1 2 3 4 4 5 6 7 7 8 9 9 10 11														

LOG. SINE SQUARE													
	144°		145°				146°				147°		a.
	20'	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'		
	9° 38'	9° 39'	9° 40'	9° 41'	9° 42'	9° 43'	9° 44'	9° 45'	9° 46'	9° 47'	9° 48'		
0	0	57635	58239	58839	59434	60025	60611	61193	61770	62342	62910	63474	0
	15	57645	58249	58849	59444	60035	60621	61202	61779	62352	62920	63483	1
	30	57655	58259	58859	59454	60044	60630	61212	61789	62361	62929	63493	2
	45	57665	58269	58869	59464	60054	60640	61222	61798	62371	62939	63502	3
1	0	57675	58279	58879	59474	60064	60650	61231	61808	62380	62948	63511	4
	15	57685	58289	58889	59484	60074	60660	61241	61818	62390	62957	63521	5
	30	57696	58299	58899	59493	60084	60669	61250	61827	62399	62967	63530	6
	45	57706	58309	58909	59503	60093	60679	61260	61837	62409	62976	63539	7
2	0	57716	58319	58919	59513	60103	60689	61270	61846	62418	62986	63549	8
	15	57726	58329	58929	59523	60113	60699	61279	61856	62428	62995	63558	9
3	0	57736	58340	58938	59533	60123	60708	61289	61865	62437	63005	63567	10
	15	57746	58350	58948	59543	60133	60718	61299	61875	62447	63014	63577	11
	30	57756	58360	58958	59553	60142	60728	61308	61885	62456	63023	63586	12
	45	57766	58370	58968	59563	60152	60737	61318	61894	62466	63033	63595	13
4	0	57776	58380	58978	59572	60162	60747	61328	61904	62475	63042	63605	14
	15	57786	58390	58988	59582	60172	60757	61337	61913	62485	63052	63614	15
	30	57797	58400	58998	59592	60182	60767	61347	61923	62494	63061	63623	16
	45	57807	58410	59008	59602	60191	60776	61357	61932	62504	63070	63633	17
5	0	57817	58420	59018	59612	60201	60786	61366	61942	62513	63080	63642	18
	15	57827	58430	59028	59622	60211	60796	61376	61951	62523	63089	63651	19
6	0	57837	58440	59038	59632	60221	60805	61385	61961	62532	63099	63661	20
	15	57847	58450	59048	59641	60230	60815	61395	61970	62542	63108	63670	21
	30	57857	58460	59058	59651	60240	60825	61405	61980	62551	63118	63679	22
	45	57867	58470	59068	59661	60250	60834	61414	61990	62561	63127	63689	23
7	0	57877	58480	59078	59671	60260	60844	61424	61999	62570	63136	63698	24
	15	57887	58490	59088	59681	60270	60854	61434	62009	62579	63146	63707	25
	30	57897	58500	59097	59691	60279	60864	61443	62018	62589	63155	63717	26
	45	57907	58510	59107	59701	60289	60873	61453	62028	62598	63165	63726	27
8	0	57917	58520	59117	59710	60299	60883	61462	62037	62608	63174	63735	28
	15	57928	58530	59127	59720	60309	60893	61472	62047	62617	63183	63745	29
9	0	57938	58540	59137	59730	60318	60902	61482	62057	62627	63193	63754	30
	15	57948	58550	59147	59740	60328	60912	61491	62066	62636	63202	63763	31
	30	57958	58560	59157	59750	60338	60922	61501	62076	62646	63211	63773	32
	45	57968	58570	59167	59760	60348	60931	61511	62085	62655	63221	63782	33
10	0	57978	58580	59177	59769	60357	60941	61520	62095	62665	63230	63791	34
	15	57988	58590	59187	59779	60367	60951	61530	62104	62674	63240	63801	35
	30	57998	58600	59197	59789	60377	60960	61539	62114	62684	63249	63810	36
	45	58008	58610	59207	59799	60387	60970	61549	62123	62693	63258	63819	37
11	0	58018	58620	59216	59809	60396	60980	61559	62133	62703	63268	63828	38
	15	58028	58630	59226	59819	60406	60990	61568	62142	62712	63277	63838	39
12	0	58038	58640	59236	59828	60416	60999	61578	62152	62721	63287	63847	40
	15	58048	58650	59246	59838	60426	61009	61587	62161	62731	63296	63856	41
	30	58058	58660	59256	59848	60436	61019	61597	62171	62740	63305	63866	42
	45	58068	58670	59266	59858	60445	61028	61607	62180	62750	63315	63875	43
13	0	58078	58680	59276	59868	60455	61038	61616	62190	62759	63324	63884	44
	15	58089	58690	59286	59878	60465	61048	61626	62200	62769	63333	63894	45
	30	58099	58700	59296	59887	60475	61057	61635	62209	62778	63343	63903	46
	45	58109	58709	59306	59897	60484	61067	61645	62219	62788	63352	63912	47
14	0	58119	58719	59315	59907	60494	61077	61655	62228	62797	63362	63922	48
	15	58129	58729	59325	59917	60504	61086	61664	62238	62807	63371	63931	49
15	0	58139	58739	59335	59927	60514	61096	61674	62247	62816	63380	63940	50
	15	58149	58749	59345	59937	60523	61106	61683	62257	62825	63390	63949	51
	30	58159	58759	59355	59946	60533	61115	61693	62266	62835	63399	63959	52
	45	58169	58769	59365	59956	60543	61125	61703	62276	62844	63408	63968	53
16	0	58179	58779	59375	59966	60553	61135	61712	62285	62854	63418	63977	54
	15	58189	58789	59385	59976	60562	61144	61722	62295	62863	63427	63987	55
	30	58199	58799	59395	59986	60572	61154	61731	62304	62873	63436	63996	56
	45	58209	58809	59405	59995	60582	61164	61741	62314	62882	63446	64005	57
17	0	58219	58819	59414	60005	60591	61173	61751	62323	62891	63455	64014	58
	15	58229	58829	59424	60015	60601	61183	61760	62333	62901	63465	64024	59

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 10. Parts 1 1 2 3 3 4 5 5 6 7 7 8 9 9 10

LOG. SINE SQUARE

	147°			148°				149°				s.
	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	
	9 ^h 49 ^m	9 ^h 50 ^m	9 ^h 51 ^m	9 ^h 52 ^m	9 ^h 53 ^m	9 ^h 54 ^m	9 ^h 55 ^m	9 ^h 56 ^m	9 ^h 57 ^m	9 ^h 58 ^m	9 ^h 59 ^m	
0	9' 9	9' 9	9' 9	9' 9	9' 9	9' 9	9' 9	9' 9	9' 9	9' 9	9' 9	0
15	64033	64588	65138	65683	66224	66761	67293	67821	68344	68863	69378	1
30	64042	64597	65147	65692	66233	66770	67302	67830	68353	68872	69386	2
45	64052	64606	65156	65701	66242	66779	67311	67839	68362	68880	69395	3
1	64061	64615	65165	65710	66251	66788	67320	67847	68370	68889	69403	4
15	64070	64624	65174	65719	66260	66797	67329	67856	68379	68898	69412	5
30	64079	64634	65183	65729	66269	66806	67337	67865	68388	68906	69420	6
45	64089	64643	65192	65738	66278	66814	67346	67874	68396	68915	69429	7
2	64099	64652	65202	65747	66287	66823	67355	67882	68405	68923	69437	8
15	64107	64661	65211	65756	66296	66832	67364	67891	68414	68932	69446	9
30	64116	64670	65220	65765	66305	66841	67373	67900	68423	68941	69454	10
45	64126	64680	65229	65774	66314	66850	67382	67909	68431	68949	69463	11
3	64135	64689	65238	65783	66323	66859	67390	67917	68440	68958	69471	12
15	64144	64698	65247	65792	66332	66868	67399	67926	68448	68966	69480	13
30	64154	64707	65256	65801	66341	66877	67408	67935	68457	68975	69488	14
45	64163	64716	65265	65810	66350	66886	67417	67943	68466	68984	69497	15
4	64172	64726	65274	65819	66359	66895	67426	67952	68474	68992	69506	16
15	64181	64735	65283	65828	66368	66903	67434	67961	68483	69001	69514	17
30	64191	64744	65293	65837	66377	66912	67443	67970	68492	69009	69523	18
45	64200	64753	65302	65846	66386	66921	67452	67978	68500	69018	69531	19
5	64209	64762	65311	65855	66395	66930	67461	67987	68509	69027	69540	20
15	64218	64771	65320	65864	66404	66939	67470	67996	68518	69035	69548	21
30	64228	64781	65329	65873	66413	66948	67479	68005	68526	69044	69557	22
45	64237	64790	65338	65882	66422	66957	67487	68013	68535	69052	69565	23
6	64246	64799	65347	65891	66431	66966	67496	68022	68544	69061	69574	24
15	64255	64808	65356	65900	66440	66974	67505	68031	68552	69069	69582	25
30	64265	64817	65365	65909	66449	66983	67514	68040	68561	69078	69591	26
45	64274	64827	65375	65918	66458	66992	67523	68048	68570	69087	69599	27
7	64283	64836	65384	65927	66466	67001	67531	68057	68578	69095	69608	28
15	64292	64845	65393	65936	66475	67010	67540	68066	68587	69104	69616	29
30	64302	64854	65402	65945	66484	67019	67549	68074	68596	69112	69625	30
45	64311	64863	65411	65954	66493	67028	67558	68083	68604	69121	69633	31
8	64320	64873	65420	65963	66502	67037	67567	68092	68613	69129	69642	32
15	64329	64882	65429	65972	66511	67045	67575	68101	68622	69138	69650	33
30	64339	64891	65438	65981	66520	67054	67584	68109	68630	69147	69659	34
45	64348	64900	65447	65990	66529	67063	67593	68118	68639	69155	69667	35
9	64357	64909	65456	65999	66538	67072	67602	68127	68648	69164	69676	36
15	64366	64918	65465	66008	66547	67081	67610	68136	68656	69172	69684	37
30	64375	64927	65474	66018	66556	67090	67619	68144	68665	69181	69693	38
45	64385	64936	65484	66027	66565	67099	67628	68153	68673	69189	69701	39
10	64394	64946	65493	66035	66574	67108	67637	68162	68682	69198	69710	40
15	64403	64955	65502	66044	66583	67116	67646	68170	68691	69206	69718	41
30	64413	64964	65511	66054	66592	67125	67654	68179	68699	69215	69727	42
45	64422	64973	65520	66063	66601	67134	67663	68188	68708	69224	69735	43
11	64431	64982	65529	66072	66609	67143	67672	68196	68717	69232	69744	44
15	64440	64991	65538	66081	66618	67152	67681	68205	68725	69241	69752	45
30	64449	65001	65547	66089	66627	67161	67690	68214	68734	69249	69760	46
45	64459	65010	65556	66098	66636	67169	67698	68223	68742	69258	69769	47
12	64468	65019	65565	66108	66645	67178	67707	68231	68751	69266	69777	48
15	64477	65028	65575	66117	66654	67187	67716	68240	68760	69275	69786	49
30	64486	65037	65584	66126	66663	67196	67725	68249	68768	69284	69794	50
45	64495	65046	65593	66135	66672	67205	67733	68257	68777	69292	69803	51
13	64505	65055	65602	66144	66681	67214	67742	68266	68786	69301	69811	52
15	64514	65065	65611	66153	66690	67223	67751	68275	68794	69309	69820	53
30	64523	65074	65620	66162	66699	67231	67760	68283	68803	69318	69828	54
45	64532	65083	65629	66170	66708	67240	67768	68292	68811	69326	69837	55
14	64542	65092	65638	66179	66717	67249	67777	68301	68820	69335	69845	56
15	64551	65101	65647	66188	66725	67258	67786	68310	68829	69343	69854	57
30	64560	65110	65656	66197	66734	67267	67795	68318	68837	69352	69862	58
45	64569	65119	65665	66206	66743	67276	67803	68327	68846	69360	69871	59
15	64578	65129	65674	66215	66752	67284	67812	68336	68855	69369	69879	60

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 9 Parts 1 1 2 2 3 4 4 5 5 6 7 7 8 8 9

LOG. SINE SQUARE														
		150°				151°				152°				
		0'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'		
		10 ⁰ 0=	10 ⁰ 1=	10 ⁰ 2=	10 ⁰ 3=	10 ⁰ 4=	10 ⁰ 5=	10 ⁰ 6=	10 ⁰ 7=	10 ⁰ 8=	10 ⁰ 9=	10 ⁰ 10=	1.	
0	0	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	0	
	15	69883	70393	70894	71391	71883	72371	72855	73334	73808	74279	74744	1	
	30	69896	70401	70902	71399	71891	72379	72863	73342	73816	74286	74752	2	
	45	69905	70410	70911	71408	71900	72387	72871	73349	73824	74294	74760	3	
	1	69913	70418	70919	71416	71908	72395	72879	73357	73832	74302	74768	4	
1	0	69921	70427	70927	71424	71916	72403	72887	73365	73840	74310	74775	5	
	15	69930	70435	70936	71432	71924	72411	72895	73373	73848	74318	74783	6	
	30	69938	70443	70944	71440	71932	72420	72903	73381	73855	74325	74791	7	
	45	69947	70452	70952	71449	71940	72428	72911	73389	73863	74333	74798	8	
2	0	69955	70460	70961	71457	71949	72436	72919	73397	73871	74341	74806	9	
	15	69964	70469	70969	71465	71957	72444	72927	73405	73879	74349	74814		
	30	69972	70477	70977	71473	71965	72452	72935	73413	73887	74356	74822	10	
	45	69981	70485	70986	71482	71973	72460	72943	73421	73895	74364	74829	11	
3	0	69989	70494	70994	71479	71981	72468	72951	73429	73903	74372	74837	12	
	15	69997	70502	71002	71497	71989	72476	72959	73437	73910	74380	74845	13	
	30	70006	70510	71010	71506	71997	72484	72967	73445	73918	74388	74852	14	
	45	70014	70519	71019	71514	72006	72492	72975	73453	73926	74395	74860	15	
4	0	70023	70527	71027	71522	72014	72500	72983	73461	73934	74403	74868	16	
	15	70031	70535	71035	71531	72022	72508	72991	73468	73942	74411	74876	17	
	30	70040	70544	71044	71539	72030	72516	72999	73476	73950	74419	74883	18	
	45	70048	70552	71052	71547	72038	72525	73007	73484	73958	74426	74891	19	
5	0	70057	70561	71060	71555	72046	72533	73015	73492	73965	74434	74899	20	
	15	70065	70569	71069	71564	72054	72541	73023	73500	73973	74442	74906	21	
	30	70073	70577	71077	71572	72063	72549	73031	73508	73981	74450	74914	22	
	45	70082	70586	71085	71580	72071	72557	73039	73516	73989	74458	74922	23	
6	0	70090	70594	71093	71588	72079	72565	73047	73524	73997	74465	74929	24	
	15	70099	70602	71102	71597	72087	72573	73055	73532	74005	74473	74937	25	
	30	70107	70611	71110	71605	72095	72581	73063	73540	74013	74481	74945	26	
	45	70116	70619	71118	71613	72103	72589	73071	73548	74020	74489	74953	27	
7	0	70124	70627	71126	71621	72111	72597	73079	73556	74028	74496	74960	28	
	15	70132	70636	71135	71629	72120	72605	73087	73563	74036	74504	74968	29	
	30	70141	70644	71143	71638	72128	72613	73095	73571	74044	74512	74976	30	
	45	70149	70653	71151	71646	72136	72621	73103	73579	74052	74520	74983	31	
8	0	70158	70661	71160	71654	72144	72629	73111	73587	74060	74528	74991	32	
	15	70166	70669	71168	71662	72152	72637	73119	73595	74067	74535	74999	33	
	30	70175	70678	71176	71670	72160	72645	73127	73603	74075	74543	75006	34	
	45	70183	70686	71184	71679	72168	72654	73135	73611	74083	74551	75014	35	
9	0	70191	70694	71193	71687	72176	72662	73143	73619	74091	74559	75022	36	
	15	70200	70703	71201	71695	72185	72670	73150	73627	74099	74566	75029	37	
	30	70208	70711	71209	71703	72193	72678	73158	73635	74107	74574	75037	38	
	45	70217	70719	71218	71711	72201	72686	73166	73643	74114	74582	75045	39	
10	0	70225	70728	71226	71720	72209	72694	73174	73650	74122	74590	75053	40	
	15	70233	70736	71234	71728	72217	72702	73182	73658	74130	74597	75060	41	
	30	70242	70744	71242	71736	72225	72710	73190	73666	74138	74605	75068	42	
	45	70250	70753	71251	71744	72233	72718	73198	73674	74146	74613	75076	43	
11	0	70259	70761	71259	71752	72241	72726	73206	73682	74154	74621	75083	44	
	15	70267	70769	71267	71761	72249	72734	73214	73690	74161	74628	75091	45	
	30	70276	70778	71275	71769	72258	72742	73222	73698	74169	74636	75099	46	
	45	70284	70786	71284	71777	72266	72750	73230	73706	74177	74644	75106	47	
12	0	70292	70794	71292	71785	72274	72758	73238	73714	74185	74652	75114	48	
	15	70301	70803	71300	71793	72282	72766	73246	73721	74193	74658	75122	49	
	30	70309	70811	71308	71801	72290	72774	73254	73729	74200	74667	75129	50	
	45	70318	70819	71317	71810	72298	72782	73262	73737	74208	74675	75137	51	
13	0	70326	70828	71325	71818	72306	72790	73270	73745	74216	74683	75145	52	
	15	70334	70836	71333	71826	72314	72798	73278	73753	74224	74690	75152	53	
	30	70343	70844	71341	71834	72322	72806	73286	73761	74232	74698	75160	54	
	45	70351	70853	71350	71842	72331	72814	73294	73769	74239	74706	75168	55	
14	0	70360	70861	71358	71851	72339	72823	73302	73777	74247	74713	75175	56	
	15	70368	70869	71366	71859	72347	72831	73310	73785	74255	74721	75183	57	
	30	70376	70878	71374	71867	72355	72839	73318	73792	74263	74729	75191	58	
	45	70385	70886	71383	71875	72363	72847	73326	73800	74271	74737	75198	59	
Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'														
D. R. Parts 1 1 2 2 3 3 4 4 5 5 6 6 7 7 8														

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 8. Parts 1 1 2 2 3 3 4 4 5 5 6 6 7 7 8

LOG. SINE SQUARE

		155°		156°				157°				158°		
		30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'		
		10°22'	10°23'	10°24'	10°25'	10°26'	10°27'	10°28'	10°29'	10°30'	10°31'	10°32'		
6	0	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9		
	15	79995	80404	80809	81209	81606	81998	82385	82769	83148	83523	83893	0	
	30	80001	80411	80816	81216	81612	82004	82392	82775	83154	83529	83899	1	
	45	80008	80417	80822	81223	81619	82011	82398	82782	83160	83535	83905	2	
	1	80015	80424	80829	81229	81625	82017	82405	82788	83167	83541	83912	3	
1	0	80022	80431	80836	81236	81632	82024	82411	82794	83173	83547	83918	4	
	15	80029	80438	80842	81243	81639	82030	82417	82801	83179	83554	83924	5	
	30	80036	80444	80849	81249	81645	82037	82424	82807	83186	83560	83930	6	
	45	80043	80451	80856	81256	81652	82043	82430	82813	83192	83566	83936	7	
	2	0	80049	80458	80862	81262	81658	82050	82437	82820	83198	83572	83942	8
2	15	80056	80465	80869	81269	81665	82056	82443	82826	83204	83579	83948	9	
	30	80063	80472	80876	81276	81671	82063	82450	82832	83211	83585	83954	10	
	45	80070	80478	80883	81282	81678	82069	82456	82839	83217	83591	83961	11	
	3	0	80077	80485	80889	81289	81684	82076	82462	82845	83223	83597	83967	12
	15	80084	80492	80896	81296	81691	82082	82469	82851	83229	83603	83973	13	
3	30	80090	80499	80903	81302	81698	82089	82475	82857	83236	83610	83979	14	
	45	80097	80505	80909	81309	81704	82095	82482	82864	83242	83616	83985	15	
	4	0	80104	80512	80916	81315	81711	82102	82488	82870	83248	83622	83991	16
	15	80111	80519	80923	81322	81717	82108	82494	82877	83254	83628	83997	17	
	30	80118	80526	80929	81329	81724	82114	82501	82883	83261	83634	84003	18	
4	45	80125	80533	80936	81335	81730	82121	82507	82889	83267	83640	84010	19	
	5	0	80131	80539	80943	81342	81737	82127	82514	82896	83273	83647	84016	20
	15	80138	80546	80949	81348	81743	82134	82520	82902	83280	83653	84022	21	
	30	80145	80553	80956	81355	81750	82140	82526	82908	83286	83659	84028	22	
	45	80152	80560	80963	81362	81756	82147	82533	82915	83292	83665	84034	23	
6	0	80159	80566	80970	81368	81763	82153	82539	82921	83298	83671	84040	24	
	15	80166	80573	80976	81375	81770	82160	82546	82927	83305	83678	84046	25	
	30	80172	80580	80983	81382	81776	82166	82552	82934	83311	83684	84052	26	
	45	80179	80587	80990	81388	81783	82173	82558	82940	83317	83690	84058	27	
	7	0	80186	80593	80996	81395	81789	82179	82565	82946	83323	83696	84065	28
7	15	80193	80600	81003	81401	81796	82186	82571	82953	83330	83702	84071	29	
	30	80200	80607	81010	81408	81802	82192	82578	82959	83336	83708	84077	30	
	45	80207	80614	81016	81415	81809	82199	82584	82965	83342	83715	84083	31	
	8	0	80213	80620	81023	81421	81815	82205	82590	82972	83348	83721	84089	32
	15	80220	80627	81030	81428	81822	82211	82597	82978	83355	83727	84095	33	
8	30	80227	80634	81036	81435	81828	82218	82603	82984	83361	83733	84101	34	
	45	80234	80641	81043	81441	81835	82224	82610	82990	83367	83739	84107	35	
	9	0	80241	80647	81050	81448	81841	82231	82616	82997	83373	83745	84113	36
	15	80247	80654	81056	81454	81848	82237	82622	83003	83379	83752	84119	37	
	30	80254	80661	81063	81461	81854	82244	82628	83009	83386	83758	84126	38	
9	45	80261	80668	81070	81468	81861	82250	82635	83016	83392	83764	84132	39	
	10	0	80268	80674	81076	81474	81867	82257	82641	83022	83398	83770	84138	40
	15	80275	80681	81083	81481	81874	82263	82648	83028	83404	83776	84144	41	
	30	80282	80688	81090	81487	81881	82270	82654	83035	83411	83782	84150	42	
	45	80288	80694	81096	81494	81887	82276	82661	83041	83417	83789	84156	43	
11	0	80295	80701	81103	81501	81894	82282	82667	83047	83423	83795	84162	44	
	15	80302	80708	81110	81507	81900	82289	82673	83054	83429	83801	84168	45	
	30	80309	80715	81116	81514	81907	82295	82680	83060	83436	83807	84174	46	
	45	80316	80721	81123	81520	81913	82302	82686	83066	83442	83813	84180	47	
	12	0	80322	80728	81130	81527	81920	82308	82692	83072	83448	83819	84186	48
12	15	80329	80735	81136	81533	81926	82315	82699	83079	83454	83826	84193	49	
	30	80336	80742	81143	81540	81933	82321	82705	83085	83460	83832	84199	50	
	45	80343	80748	81150	81547	81939	82328	82712	83091	83467	83838	84205	51	
	13	0	80349	80755	81156	81553	81946	82334	82718	83098	83473	83844	84211	52
	15	80356	80762	81163	81560	81952	82340	82724	83104	83479	83850	84217	53	
13	30	80363	80768	81169	81566	81959	82347	82731	83110	83485	83856	84223	54	
	45	80370	80775	81176	81573	81965	82353	82737	83116	83492	83862	84229	55	
	14	0	80377	80782	81183	81580	81972	82360	82743	83123	83498	83869	84235	56
	15	80383	80789	81189	81586	81978	82366	82750	83129	83504	83875	84241	57	
	30	80390	80795	81196	81593	81985	82373	82756	83135	83510	83881	84247	58	
14	45	80397	80802	81203	81599	81991	82379	82762	83142	83516	83887	84253	59	

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 7. Parts 0 1 2 3 4 5 6 7 8

LOG. SINE SQUARE

		158°			159°				160°				s.
		15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	
		10°33'	10°34'	10°35'	10°36'	10°37'	10°38'	10°39'	10°40'	10°41'	10°42'	10°43'	
		10°33'	10°34'	10°35'	10°36'	10°37'	10°38'	10°39'	10°40'	10°41'	10°42'	10°43'	
0	0	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	0
15	0	84259	84621	84979	85332	85681	86026	86367	86703	87035	87363	87686	1
30	0	84265	84627	84985	85338	85687	86032	86372	86709	87040	87368	87692	2
45	0	84271	84633	84991	85344	85693	86038	86378	86714	87046	87373	87697	3
1	0	84278	84639	84997	85350	85699	86043	86384	86720	87051	87379	87702	4
15	0	84284	84645	85003	85356	85704	86049	86389	86725	87057	87384	87708	5
30	0	84290	84651	85008	85361	85710	86055	86395	86731	87062	87390	87713	6
45	0	84296	84657	85014	85367	85716	86060	86400	86736	87068	87395	87718	7
2	0	84302	84663	85020	85373	85722	86066	86406	86742	87073	87401	87724	8
15	0	84308	84669	85026	85379	85728	86072	86412	86747	87079	87406	87729	9
30	0	84314	84675	85032	85385	85733	86077	86417	86753	87084	87411	87734	10
45	0	84320	84681	85038	85391	85739	86083	86423	86758	87090	87417	87740	11
1	15	84326	84687	85044	85397	85745	86089	86429	86764	87095	87422	87745	12
30	15	84332	84693	85050	85402	85751	86095	86434	86770	87101	87428	87751	13
45	15	84338	84699	85056	85408	85756	86100	86440	86775	87106	87433	87756	14
2	15	84344	84705	85062	85414	85762	86106	86445	86781	87112	87439	87761	15
15	15	84350	84711	85068	85420	85768	86112	86451	86786	87117	87444	87766	16
30	15	84356	84717	85074	85426	85774	86117	86457	86792	87123	87449	87772	17
45	15	84362	84723	85080	85432	85779	86123	86462	86797	87128	87455	87777	18
3	15	84368	84729	85085	85437	85785	86129	86468	86803	87134	87460	87782	19
45	15	84374	84735	85091	85443	85791	86134	86474	86808	87139	87466	87788	20
4	0	84380	84741	85097	85449	85797	86140	86479	86814	87145	87471	87793	21
15	0	84387	84747	85103	85455	85802	86146	86485	86820	87150	87476	87798	22
30	0	84393	84753	85109	85461	85808	86151	86490	86825	87156	87482	87804	23
45	0	84399	84759	85115	85467	85814	86157	86496	86831	87161	87487	87809	24
5	0	84405	84765	85121	85472	85819	86163	86502	86836	87167	87493	87814	25
15	0	84411	84771	85127	85478	85826	86168	86507	86842	87172	87498	87820	26
30	0	84417	84777	85133	85484	85831	86174	86513	86847	87177	87503	87825	27
45	0	84423	84783	85138	85490	85837	86180	86519	86853	87183	87509	87830	28
6	0	84429	84789	85144	85496	85843	86186	86524	86858	87188	87514	87836	29
15	0	84435	84795	85150	85502	85848	86191	86530	86864	87194	87520	87841	30
7	0	84441	84801	85156	85507	85854	86197	86535	86869	87199	87525	87846	31
15	0	84447	84807	85162	85513	85860	86203	86541	86875	87205	87530	87852	32
30	0	84453	84813	85168	85519	85866	86208	86546	86881	87210	87536	87857	33
45	0	84459	84818	85174	85525	85872	86214	86552	86886	87216	87541	87862	34
8	0	84465	84824	85180	85531	85877	86220	86558	86892	87221	87547	87867	35
15	0	84471	84830	85186	85536	85883	86225	86563	86897	87227	87552	87873	36
30	0	84477	84836	85191	85542	85889	86231	86569	86903	87232	87557	87878	37
45	0	84483	84842	85197	85548	85894	86237	86574	86908	87237	87563	87883	38
9	0	84489	84848	85203	85554	85900	86242	86580	86914	87243	87568	87889	39
15	0	84495	84854	85209	85560	85906	86248	86586	86919	87248	87573	87894	40
10	0	84501	84860	85215	85565	85912	86254	86591	86925	87254	87579	87899	41
15	0	84507	84866	85221	85571	85917	86259	86597	86930	87259	87584	87905	42
30	0	84513	84872	85227	85577	85923	86265	86602	86936	87265	87590	87910	43
45	0	84519	84878	85233	85583	85929	86271	86608	86941	87270	87595	87915	44
11	0	84525	84884	85238	85589	85935	86276	86614	86947	87276	87600	87921	45
15	0	84531	84890	85244	85594	85940	86282	86619	86952	87281	87606	87926	46
30	0	84537	84896	85250	85600	85946	86288	86625	86958	87286	87611	87931	47
45	0	84543	84902	85256	85606	85952	86293	86630	86963	87292	87616	87937	48
12	0	84549	84908	85262	85612	85958	86299	86636	86969	87297	87622	87942	49
15	0	84555	84914	85268	85618	85963	86305	86642	86974	87303	87627	87947	50
13	0	84561	84920	85274	85623	85969	86310	86647	86980	87308	87633	87953	51
15	0	84567	84926	85280	85629	85975	86316	86653	86985	87314	87638	87958	52
30	0	84573	84931	85285	85635	85980	86321	86658	86991	87319	87643	87963	53
45	0	84579	84937	85291	85641	85986	86327	86664	86996	87325	87649	87968	54
14	0	84585	84943	85297	85647	85992	86333	86669	87002	87330	87654	87974	55
15	0	84591	84949	85303	85652	85998	86338	86675	87007	87335	87659	87979	56
30	0	84597	84955	85309	85658	86003	86344	86681	87013	87341	87665	87985	57
45	0	84603	84961	85315	85664	86009	86350	86686	87018	87346	87670	87990	58
15	0	84609	84967	85321	85670	86015	86355	86692	87024	87352	87675	87995	59
45	0	84615	84973	85326	85676	86020	86361	86697	87029	87357	87681	88000	60

Sec. 1° 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
 D. 6. Parts 0 1 1 2 2 2 3 3 4 4 4 5 5 6 6

LOG. SINE SQUARE

		161°				162°				163°			2.
		0'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	
		10°44'	10°45'	10°46'	10°47'	10°48'	10°49'	10°50'	10°51'	10°52'	10°53'	10°54'	
0	0	88005	88320	88631	88938	89240	89538	89832	90121	90407	90688	90964	0
15	0	88011	88326	88636	88943	89245	89543	89836	90126	90411	90692	90969	1
30	0	88016	88331	88641	88948	89250	89548	89841	90131	90416	90697	90974	2
45	0	88021	88336	88647	88953	89255	89553	89846	90136	90421	90702	90978	3
1	0	88026	88341	88652	88958	89260	89558	89851	90140	90425	90706	90983	4
15	0	88032	88346	88657	88963	89265	89562	89856	90145	90430	90711	90987	5
30	0	88037	88352	88662	88968	89270	89567	89861	90150	90435	90715	90992	6
45	0	88042	88357	88667	88973	89275	89572	89866	90155	90439	90720	90996	7
2	0	88048	88362	88672	88978	89280	89577	89870	90159	90444	90725	91001	8
15	0	88053	88367	88677	88983	89285	89582	89875	90164	90449	90729	91006	9
30	0	88058	88372	88682	88988	89290	89587	89880	90169	90454	90734	91010	10
45	0	88063	88378	88688	88993	89295	89592	89885	90174	90458	90739	91015	11
3	0	88069	88383	88693	88998	89300	89597	89890	90179	90463	90743	91019	12
15	0	88074	88388	88698	89003	89305	89602	89895	90188	90468	90748	91024	13
30	0	88079	88393	88703	89008	89310	89607	89899	90188	90472	90753	91028	14
45	0	88085	88398	88708	89014	89315	89612	89904	90193	90477	90757	91033	15
4	0	88090	88404	88713	89019	89320	89617	89909	90198	90482	90762	91038	16
15	0	88095	88409	88718	89024	89325	89621	89914	90202	90487	90766	91042	17
30	0	88100	88414	88723	89029	89330	89626	89919	90207	90491	90771	91047	18
45	0	88106	88419	88729	89034	89335	89631	89924	90212	90496	90776	91051	19
5	0	88111	88424	88734	89039	89340	89636	89929	90217	90501	90780	91056	20
15	0	88116	88430	88739	89044	89345	89641	89933	90221	90505	90785	91060	21
30	0	88121	88435	88744	89049	89350	89646	89938	90226	90510	90790	91065	22
45	0	88127	88440	88749	89054	89355	89651	89943	90231	90515	90794	91069	23
6	0	88132	88445	88754	89059	89360	89656	89948	90236	90519	90799	91074	24
15	0	88137	88450	88759	89064	89365	89661	89953	90241	90524	90803	91079	25
30	0	88142	88456	88764	89069	89370	89666	89958	90245	90529	90808	91083	26
45	0	88148	88461	88769	89074	89375	89671	89962	90250	90533	90813	91088	27
7	0	88153	88466	88775	89079	89379	89675	89967	90255	90538	90817	91092	28
15	0	88158	88471	88780	89084	89384	89680	89972	90260	90543	90822	91097	29
30	0	88163	88476	88785	89089	89389	89685	89977	90264	90548	90827	91101	30
45	0	88169	88481	88790	89094	89394	89690	89982	90269	90552	90831	91106	31
8	0	88174	88487	88795	89099	89399	89695	89987	90274	90557	90836	91110	32
15	0	88179	88492	88800	89104	89404	89700	89991	90279	90562	90840	91115	33
30	0	88184	88497	88805	89109	89409	89705	89996	90283	90566	90845	91119	34
45	0	88190	88502	88810	89114	89414	89710	90001	90288	90571	90850	91124	35
9	0	88195	88507	88815	89119	89419	89715	90006	90293	90576	90854	91129	36
15	0	88200	88513	88821	89124	89424	89719	90011	90298	90580	90859	91133	37
30	0	88205	88518	88826	89129	89429	89724	90015	90302	90585	90863	91138	38
45	0	88211	88523	88831	89134	89434	89729	90020	90307	90590	90868	91142	39
10	0	88216	88528	88836	89140	89439	89734	90025	90312	90594	90873	91147	40
15	0	88221	88533	88841	89145	89444	89739	90030	90317	90599	90877	91151	41
30	0	88226	88538	88846	89150	89449	89744	90035	90321	90604	90882	91156	42
45	0	88232	88544	88851	89155	89454	89749	90040	90326	90608	90886	91160	43
11	0	88237	88549	88856	89160	89459	89754	90044	90331	90613	90891	91165	44
15	0	88242	88554	88861	89165	89464	89759	90049	90336	90618	90896	91169	45
30	0	88247	88559	88866	89170	89469	89763	90054	90340	90622	90900	91174	46
45	0	88252	88564	88871	89175	89474	89768	90059	90345	90627	90905	91178	47
12	0	88258	88569	88877	89180	89479	89773	90064	90350	90632	90909	91183	48
15	0	88263	88575	88882	89185	89484	89778	90068	90354	90636	90914	91187	49
30	0	88268	88580	88887	89190	89488	89783	90073	90359	90641	90919	91192	50
45	0	88273	88585	88892	89195	89493	89788	90078	90364	90646	90923	91196	51
13	0	88279	88590	88897	89200	89498	89793	90083	90369	90650	90928	91201	52
15	0	88284	88595	88902	89205	89503	89798	90088	90373	90655	90932	91205	53
30	0	88289	88600	88907	89210	89508	89802	90092	90378	90660	90937	91210	54
45	0	88294	88605	88912	89215	89513	89807	90097	90383	90664	90942	91214	55
14	0	88300	88611	88917	89220	89518	89812	90102	90388	90669	90946	91219	56
15	0	88305	88616	88922	89225	89523	89817	90107	90392	90674	90951	91224	57
30	0	88310	88621	88927	89230	89528	89822	90112	90397	90678	90955	91228	58
45	0	88315	88626	88933	89235	89533	89827	90116	90402	90683	90960	91233	59

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 5. Paris 0 1 1 2 2 2 3 3 3 3 4 4 4 5 5

LOG. SINE SQUARE

		163°					164°					165°					166°					s.
		48'	0'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	0'	15'						
10°55'	10°56'	10°57'	10°58'	10°59'	11°0'	11°1'	11°2'	11°3'	11°4'	11°5'	12°0'	12°1'	12°2'	12°3'	12°4'	12°5'						
0	0	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9						
	15	9'12.3	9'15.06	9'17.70	9'20.30	9'22.86	9'25.37	9'27.85	9'30.28	9'32.67	9'35.01	9'37.32	0	1								
	30	9'14.2	9'15.10	9'17.74	9'20.34	9'22.90	9'25.41	9'27.89	9'30.32	9'32.71	9'35.05	9'37.36	1	2								
	45	9'14.6	9'15.14	9'17.79	9'20.38	9'22.94	9'25.45	9'27.93	9'30.36	9'32.74	9'35.09	9'37.40	2	3								
	1	0	9'15.1	9'15.19	9'17.83	9'20.43	9'22.98	9'25.50	9'27.97	9'30.40	9'32.78	9'35.13	9'37.43	3	4							
1	0	9'15.5	9'15.23	9'17.87	9'20.47	9'23.02	9'25.54	9'28.01	9'30.44	9'32.82	9'35.17	9'37.47	4	5								
	15	9'12.60	9'15.28	9'17.92	9'20.51	9'23.07	9'25.58	9'28.05	9'30.48	9'32.86	9'35.21	9'37.51	5	6								
	30	9'12.64	9'15.32	9'17.96	9'20.56	9'23.11	9'25.62	9'28.09	9'30.52	9'32.90	9'35.25	9'37.55	6	7								
	45	9'12.69	9'15.37	9'18.00	9'20.60	9'23.15	9'25.66	9'28.13	9'30.56	9'32.94	9'35.28	9'37.59	7	8								
	2	0	9'12.73	9'15.41	9'18.05	9'20.64	9'23.19	9'25.70	9'28.17	9'30.60	9'32.98	9'35.32	9'37.62	8	9							
2	0	9'12.78	9'15.45	9'18.09	9'20.68	9'23.24	9'25.75	9'28.21	9'30.64	9'33.02	9'35.36	9'37.66	9	10								
	15	9'12.82	9'15.50	9'18.13	9'20.73	9'23.28	9'25.79	9'28.25	9'30.68	9'33.06	9'35.40	9'37.70	10	11								
	30	9'12.87	9'15.55	9'18.18	9'20.77	9'23.32	9'25.83	9'28.29	9'30.72	9'33.10	9'35.44	9'37.74	11	12								
	45	9'12.91	9'15.59	9'18.22	9'20.81	9'23.36	9'25.87	9'28.33	9'30.76	9'33.14	9'35.48	9'37.78	12	13								
	3	0	9'12.96	9'15.63	9'18.27	9'20.86	9'23.40	9'25.91	9'28.37	9'30.80	9'33.18	9'35.52	9'37.81	13	14							
3	0	9'13.00	9'15.68	9'18.31	9'20.90	9'23.45	9'25.95	9'28.42	9'30.84	9'33.22	9'35.56	9'37.85	14	15								
	15	9'13.05	9'15.72	9'18.35	9'20.94	9'23.49	9'25.99	9'28.46	9'30.88	9'33.26	9'35.59	9'37.89	15	16								
	30	9'13.09	9'15.76	9'18.40	9'20.98	9'23.53	9'26.04	9'28.50	9'30.92	9'33.30	9'35.63	9'37.93	16	17								
	45	9'13.14	9'15.81	9'18.44	9'21.03	9'23.57	9'26.08	9'28.54	9'30.96	9'33.34	9'35.67	9'37.97	17	18								
	4	0	9'13.18	9'15.85	9'18.48	9'21.07	9'23.61	9'26.12	9'28.58	9'31.00	9'33.38	9'35.71	9'38.00	18	19							
4	0	9'13.23	9'15.90	9'18.53	9'21.11	9'23.66	9'26.16	9'28.62	9'31.04	9'33.41	9'35.75	9'38.04	19	20								
	15	9'13.27	9'15.94	9'18.57	9'21.16	9'23.70	9'26.20	9'28.66	9'31.08	9'33.45	9'35.79	9'38.08	20	21								
	30	9'13.32	9'15.98	9'18.61	9'21.20	9'23.74	9'26.24	9'28.70	9'31.12	9'33.49	9'35.83	9'38.12	21	22								
	45	9'13.36	9'16.03	9'18.66	9'21.24	9'23.78	9'26.28	9'28.74	9'31.16	9'33.53	9'35.86	9'38.15	22	23								
	5	0	9'13.41	9'16.07	9'18.70	9'21.28	9'23.82	9'26.32	9'28.78	9'31.20	9'33.57	9'35.90	9'38.19	23	24							
5	0	9'13.45	9'16.12	9'18.74	9'21.33	9'23.87	9'26.37	9'28.82	9'31.24	9'33.61	9'35.94	9'38.23	24	25								
	15	9'13.50	9'16.16	9'18.79	9'21.37	9'23.91	9'26.41	9'28.86	9'31.28	9'33.65	9'35.98	9'38.27	25	26								
	30	9'13.54	9'16.21	9'18.83	9'21.41	9'23.95	9'26.45	9'28.90	9'31.32	9'33.69	9'36.02	9'38.31	26	27								
	45	9'13.59	9'16.25	9'18.87	9'21.45	9'23.99	9'26.49	9'28.94	9'31.36	9'33.73	9'36.06	9'38.34	27	28								
	6	0	9'13.63	9'16.29	9'18.92	9'21.50	9'24.03	9'26.53	9'28.98	9'31.40	9'33.77	9'36.09	9'38.38	28	29							
6	0	9'13.67	9'16.34	9'18.96	9'21.54	9'24.08	9'26.57	9'29.03	9'31.44	9'33.81	9'36.13	9'38.42	29	30								
	15	9'13.72	9'16.38	9'19.00	9'21.58	9'24.12	9'26.61	9'29.07	9'31.48	9'33.85	9'36.17	9'38.46	30	31								
	30	9'13.76	9'16.43	9'19.05	9'21.63	9'24.16	9'26.65	9'29.11	9'31.52	9'33.89	9'36.21	9'38.49	31	32								
	45	9'13.81	9'16.47	9'19.09	9'21.67	9'24.20	9'26.70	9'29.15	9'31.56	9'33.92	9'36.25	9'38.53	32	33								
	7	0	9'13.85	9'16.51	9'19.13	9'21.71	9'24.24	9'26.74	9'29.19	9'31.60	9'33.96	9'36.29	9'38.57	33	34							
7	0	9'13.90	9'16.56	9'19.18	9'21.75	9'24.29	9'26.78	9'29.23	9'31.64	9'34.00	9'36.33	9'38.61	34	35								
	15	9'13.94	9'16.60	9'19.22	9'21.80	9'24.33	9'26.82	9'29.27	9'31.68	9'34.04	9'36.36	9'38.65	35	36								
	30	9'13.99	9'16.65	9'19.26	9'21.84	9'24.37	9'26.86	9'29.31	9'31.72	9'34.08	9'36.40	9'38.68	36	37								
	45	9'14.03	9'16.69	9'19.30	9'21.88	9'24.41	9'26.90	9'29.35	9'31.76	9'34.12	9'36.44	9'38.72	37	38								
	8	0	9'14.08	9'16.73	9'19.35	9'21.92	9'24.45	9'26.94	9'29.39	9'31.79	9'34.16	9'36.48	9'38.76	38	39							
8	0	9'14.12	9'16.78	9'19.39	9'21.97	9'24.49	9'26.98	9'29.43	9'31.83	9'34.20	9'36.52	9'38.80	39	40								
	15	9'14.17	9'16.82	9'19.44	9'22.01	9'24.54	9'27.03	9'29.47	9'31.87	9'34.24	9'36.56	9'38.83	40	41								
	30	9'14.21	9'16.87	9'19.48	9'22.05	9'24.58	9'27.07	9'29.51	9'31.91	9'34.27	9'36.59	9'38.87	41	42								
	45	9'14.25	9'16.91	9'19.52	9'22.09	9'24.62	9'27.11	9'29.55	9'31.95	9'34.31	9'36.63	9'38.91	42	43								
	9	0	9'14.30	9'16.95	9'19.56	9'22.14	9'24.66	9'27.15	9'29.59	9'31.99	9'34.35	9'36.67	9'38.95	43	44							
9	0	9'14.34	9'17.00	9'19.61	9'22.18	9'24.70	9'27.19	9'29.63	9'32.03	9'34.39	9'36.71	9'38.98	44	45								
	15	9'14.39	9'17.04	9'19.65	9'22.22	9'24.75	9'27.23	9'29.67	9'32.07	9'34.43	9'36.75	9'39.02	45	46								
	30	9'14.43	9'17.09	9'19.69	9'22.26	9'24.79	9'27.27	9'29.71	9'32.11	9'34.47	9'36.79	9'39.06	46	47								
	45	9'14.48	9'17.13	9'19.74	9'22.30	9'24.83	9'27.31	9'29.75	9'32.15	9'34.51	9'36.82	9'39.10	47	48								
	10	0	9'14.52	9'17.17	9'19.78	9'22.35	9'24.87	9'27.35	9'29.79	9'32.19	9'34.55	9'36.86	9'39.13	48	49							
10	0	9'14.57	9'17.22	9'19.82	9'22.39	9'24.91	9'27.39	9'29.83	9'32.23	9'34.59	9'36.90	9'39.17	49	50								
	15	9'14.61	9'17.26	9'19.87	9'22.43	9'24.95	9'27.44	9'29.87	9'32.27	9'34.63	9'36.94	9'39.21	50	51								
	30	9'14.66	9'17.30	9'19.91	9'22.47	9'25.00	9'27.48	9'29.91	9'32.31	9'34.66	9'36.98	9'39.25	51	52								
	45	9'14.70	9'17.35	9'19.95	9'22.52	9'25.04	9'27.52	9'29.95	9'32.35	9'34.70	9'37.02	9'39.28	52	53								
	11	0	9'14.74	9'17.39	9'20.00	9'22.56	9'25.08	9'27.56	9'29.99	9'32.39	9'34.74	9'37.05	9'39.32	53	54							
11	0	9'14.79	9'17.43	9'20.04	9'22.60	9'25.12	9'27.60	9'30.03	9'32.43	9'34.78	9'37.09	9'39.36	54	55								
	15	9'14.83	9'17.48	9'20.08	9'22.64	9'25.16	9'27.64	9'30.08	9'32.47	9'34.82	9'37.13	9'39.40	55	56								
	30	9'14.88	9'17.52	9'20.13	9'22.69	9'25.20	9'27.68	9'30.12	9'32.51	9'34.86	9'37.17	9'39.43	56	57								
	45	9'14.92	9'17.57	9'20.17	9'22.73	9'25.25	9'27.72	9'30.16	9'32.55	9'34.90	9'37.21	9'39.47	57	58								
	12	0	9'14.97	9'17.61	9'20.21	9'22.77	9'25.29	9'27.76	9'30.20	9'32.59	9'34.94	9'37.24	9'39.51	58	59							
12	0	9'15.01	9'17.65	9'20.25	9'22.81	9'25.33	9'27.80	9'30.24	9'32.63	9'34.98	9'37.28	9'39.55	59	60								
	15	9'15.06	9'17.70	9'20.30	9'22.86	9'25.38	9'27.85	9'30.29	9'32.68	9'35.03	9'37.33	9'39.60	60	61								
	30	9'15.11	9'17.75	9'20.35	9'22.91	9'25.43	9'27.90	9'30.34	9'32.73	9'35.08	9'37.38	9'39.65	61	62								
	45	9'15.16	9'17.80	9'20.40	9'22.96	9'25.48	9'27.95	9'30.39	9'32.78	9'35.13	9'37.43	9'39.70	62	63								
	13	0	9'15.21	9'17.85	9'20.45	9'23.01	9'25.53	9'28.00	9'30.44	9'32.83	9'35.18	9'37.48	9'39.75	63	64							

LOG. SINE SQUARE													
	166°		167°				168°				169°		s.
	30'	48'	0'	15'	30'	45'	0'	15'	30'	45'	0'		
	11° 6'	11° 7'	11° 8'	11° 9'	11° 10'	11° 11'	11° 12'	11° 13'	11° 14'	11° 15'	11° 16'		
0	9' 93958	9' 94181	9' 94399	9' 94612	9' 94822	9' 95027	9' 95229	9' 95426	9' 95619	9' 95807	9' 95992	0	
15	93962	94184	94402	94616	94825	95031	95232	95429	95622	95811	95995	1	
30	93966	94188	94406	94619	94829	95034	95235	95432	95625	95814	95998	2	
45	93970	94192	94409	94623	94832	95038	95239	95436	95628	95817	96001	3	
1	93973	94195	94413	94626	94836	95041	95242	95439	95631	95820	96004	4	
15	93977	94199	94417	94630	94839	95044	95245	95442	95635	95823	96007	5	
30	93981	94202	94420	94633	94843	95048	95248	95445	95638	95826	96010	6	
45	93984	94206	94424	94637	94846	95051	95252	95448	95641	95829	96015	7	
2	93988	94210	94427	94641	94850	95054	95255	95452	95644	95832	96016	8	
15	93992	94213	94431	94644	94853	95058	95259	95455	95647	95835	96019	9	
30	93996	94217	94434	94648	94856	95061	95262	95458	95650	95838	96022	10	
45	93999	94221	94438	94651	94860	95065	95263	95461	95654	95842	96025	11	
3	94003	94224	94442	94655	94863	95068	95268	95465	95657	95845	96028	12	
15	94007	94228	94445	94658	94867	95071	95272	95468	95660	95848	96031	13	
30	94011	94232	94449	94662	94870	95075	95275	95471	95663	95851	96034	14	
45	94014	94235	94452	94665	94874	95078	95278	95474	95666	95854	96037	15	
4	94018	94239	94456	94669	94877	95081	95282	95478	95669	95857	96040	16	
15	94022	94243	94460	94672	94881	95085	95285	95481	95673	95860	96043	17	
30	94025	94246	94463	94676	94884	95088	95288	95484	95676	95863	96047	18	
45	94029	94250	94467	94679	94887	95092	95292	95487	95679	95866	96050	19	
5	94033	94254	94470	94683	94891	95095	95295	95491	95682	95869	96053	20	
15	94037	94257	94474	94686	94894	95098	95298	95494	95685	95872	96056	21	
30	94040	94261	94477	94690	94898	95102	95301	95497	95688	95876	96059	22	
45	94044	94265	94481	94693	94901	95105	95305	95500	95692	95879	96062	23	
6	94048	94268	94485	94697	94905	95108	95308	95503	95695	95882	96065	24	
15	94051	94272	94488	94700	94908	95112	95311	95507	95698	95885	96068	25	
30	94055	94275	94492	94704	94911	95115	95315	95510	95701	95888	96071	26	
45	94059	94279	94495	94707	94915	95118	95318	95513	95704	95891	96074	27	
7	94063	94283	94499	94711	94918	95122	95321	95516	95707	95894	96077	28	
15	94066	94286	94502	94714	94922	95125	95324	95520	95710	95897	96080	29	
30	94070	94290	94506	94718	94925	95129	95328	95523	95714	95900	96083	30	
45	94074	94294	94510	94721	94929	95132	95331	95526	95717	95903	96086	31	
8	94077	94297	94513	94725	94932	95135	95334	95529	95720	95906	96089	32	
15	94081	94301	94517	94728	94935	95139	95338	95532	95723	95909	96092	33	
30	94085	94305	94520	94732	94939	95142	95341	95536	95726	95912	96095	34	
45	94088	94308	94524	94735	94942	95145	95344	95539	95729	95916	96098	35	
9	94092	94312	94527	94739	94946	95149	95347	95542	95732	95919	96101	36	
15	94096	94315	94531	94742	94949	95152	95351	95545	95736	95922	96104	37	
30	94100	94319	94535	94746	94953	95155	95354	95548	95739	95925	96107	38	
45	94103	94323	94538	94749	94956	95159	95357	95552	95742	95928	96110	39	
10	94107	94326	94542	94752	94959	95162	95361	95555	95745	95931	96113	40	
15	94111	94330	94545	94756	94963	95165	95364	95558	95748	95934	96116	41	
30	94114	94334	94549	94759	94966	95169	95367	95561	95751	95937	96119	42	
45	94118	94337	94552	94763	94970	95172	95370	95564	95754	95940	96122	43	
11	94122	94341	94556	94766	94973	95175	95374	95568	95757	95943	96125	44	
15	94125	94344	94559	94770	94976	95179	95377	95571	95761	95946	96128	45	
30	94129	94348	94563	94773	94980	95182	95380	95574	95764	95949	96131	46	
45	94133	94352	94566	94777	94983	95185	95383	95577	95767	95952	96134	47	
12	94136	94355	94570	94780	94987	95189	95387	95580	95770	95955	96137	48	
15	94140	94359	94573	94784	94991	95192	95390	95584	95773	95958	96140	49	
30	94144	94362	94577	94787	94993	95195	95393	95587	95776	95961	96143	50	
45	94147	94366	94581	94791	94997	95199	95396	95590	95779	95965	96146	51	
13	94151	94370	94584	94794	95000	95202	95400	95593	95782	95968	96149	52	
15	94155	94373	94588	94798	95004	95205	95403	95596	95786	95971	96152	53	
30	94158	94377	94591	94801	95007	95209	95406	95600	95789	95974	96154	54	
45	94162	94381	94595	94805	95010	95212	95410	95603	95792	95977	96157	55	
14	94166	94384	94598	94808	95014	95215	95413	95606	95795	95980	96160	56	
15	94170	94388	94602	94812	95017	95219	95416	95609	95798	95983	96163	57	
30	94173	94391	94605	94815	95021	95222	95419	95612	95801	95986	96166	58	
45	94177	94395	94609	94819	95024	95225	95423	95615	95805	95989	96169	59	

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 3 Parts 0 0 1 1 1 1 1 2 2 2 2 2 3 3 3

LOG. SINE SQUARE

	169°			170°				171°				N.
	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'	
	11°17'	11°18'	11°19'	11°20'	11°21'	11°22'	11°23'	11°24'	11°25'	11°26'	11°27'	
0	9' 96172	9' 96349	9' 96521	9' 96688	9' 96852	9' 97012	9' 97167	9' 97318	9' 97465	9' 97608	9' 97747	0
1	0 96175	0 96351	0 96523	0 96691	0 96855	0 97014	0 97170	0 97321	0 97468	0 97611	0 97749	1
2	0 96178	0 96354	0 96526	0 96694	0 96858	0 97017	0 97172	0 97323	0 97470	0 97613	0 97752	2
3	0 96181	0 96357	0 96529	0 96697	0 96860	0 97020	0 97175	0 97326	0 97473	0 97615	0 97754	3
4	0 96184	0 96360	0 96532	0 96699	0 96863	0 97022	0 97177	0 97328	0 97475	0 97618	0 97756	4
5	0 96187	0 96363	0 96535	0 96702	0 96866	0 97025	0 97180	0 97331	0 97477	0 97620	0 97758	5
6	0 96190	0 96366	0 96538	0 96705	0 96868	0 97027	0 97182	0 97333	0 97480	0 97622	0 97761	6
7	0 96193	0 96369	0 96540	0 96708	0 96871	0 97030	0 97185	0 97336	0 97482	0 97625	0 97763	7
8	0 96196	0 96372	0 96543	0 96711	0 96874	0 97033	0 97187	0 97338	0 97485	0 97627	0 97765	8
9	0 96199	0 96375	0 96546	0 96713	0 96876	0 97035	0 97190	0 97341	0 97487	0 97629	0 97767	9
10	0 96202	0 96377	0 96549	0 96716	0 96879	0 97038	0 97193	0 97343	0 97489	0 97632	0 97770	10
11	0 96205	0 96380	0 96552	0 96719	0 96882	0 97040	0 97195	0 97346	0 97492	0 97634	0 97772	11
12	0 96208	0 96383	0 96554	0 96722	0 96884	0 97043	0 97198	0 97348	0 97494	0 97636	0 97774	12
13	0 96211	0 96386	0 96557	0 96724	0 96887	0 97046	0 97200	0 97351	0 97497	0 97639	0 97776	13
14	0 96214	0 96389	0 96560	0 96727	0 96890	0 97048	0 97203	0 97353	0 97499	0 97641	0 97779	14
15	0 96217	0 96392	0 96563	0 96730	0 96892	0 97051	0 97205	0 97355	0 97501	0 97643	0 97781	15
16	0 96220	0 96395	0 96566	0 96733	0 96895	0 97054	0 97208	0 97358	0 97504	0 97646	0 97783	16
17	0 96223	0 96398	0 96569	0 96735	0 96898	0 97056	0 97210	0 97360	0 97506	0 97648	0 97786	17
18	0 96226	0 96401	0 96571	0 96738	0 96900	0 97059	0 97213	0 97363	0 97509	0 97650	0 97788	18
19	0 96229	0 96403	0 96574	0 96741	0 96903	0 97061	0 97215	0 97365	0 97511	0 97653	0 97790	19
20	0 96232	0 96406	0 96577	0 96743	0 96906	0 97064	0 97218	0 97368	0 97513	0 97655	0 97792	20
21	0 96234	0 96409	0 96580	0 96746	0 96908	0 97067	0 97220	0 97370	0 97516	0 97657	0 97795	21
22	0 96237	0 96412	0 96583	0 96749	0 96911	0 97069	0 97223	0 97373	0 97518	0 97660	0 97797	22
23	0 96240	0 96415	0 96585	0 96752	0 96914	0 97072	0 97226	0 97375	0 97521	0 97662	0 97799	23
24	0 96243	0 96418	0 96588	0 96754	0 96916	0 97074	0 97228	0 97378	0 97523	0 97664	0 97801	24
25	0 96246	0 96421	0 96591	0 96757	0 96919	0 97077	0 97231	0 97380	0 97525	0 97667	0 97804	25
26	0 96249	0 96424	0 96593	0 96760	0 96922	0 97079	0 97233	0 97383	0 97528	0 97669	0 97806	26
27	0 96252	0 96426	0 96597	0 96763	0 96924	0 97082	0 97236	0 97385	0 97530	0 97671	0 97808	27
28	0 96255	0 96429	0 96599	0 96765	0 96927	0 97085	0 97238	0 97387	0 97532	0 97673	0 97810	28
29	0 96258	0 96432	0 96602	0 96768	0 96930	0 97087	0 97241	0 97390	0 97535	0 97676	0 97813	29
30	0 96261	0 96435	0 96605	0 96771	0 96932	0 97090	0 97243	0 97392	0 97537	0 97678	0 97815	30
31	0 96264	0 96438	0 96608	0 96774	0 96935	0 97092	0 97246	0 97395	0 97540	0 97680	0 97817	31
32	0 96267	0 96441	0 96611	0 96776	0 96938	0 97095	0 97248	0 97397	0 97542	0 97683	0 97819	32
33	0 96270	0 96444	0 96613	0 96779	0 96940	0 97098	0 97251	0 97400	0 97544	0 97685	0 97822	33
34	0 96273	0 96447	0 96616	0 96782	0 96943	0 97100	0 97253	0 97402	0 97547	0 97687	0 97824	34
35	0 96276	0 96449	0 96619	0 96784	0 96946	0 97103	0 97256	0 97405	0 97549	0 97690	0 97826	35
36	0 96279	0 96452	0 96622	0 96787	0 96948	0 97105	0 97258	0 97407	0 97552	0 97692	0 97828	36
37	0 96281	0 96455	0 96625	0 96790	0 96951	0 97108	0 97261	0 97409	0 97554	0 97694	0 97830	37
38	0 96284	0 96458	0 96627	0 96792	0 96954	0 97111	0 97263	0 97412	0 97556	0 97697	0 97833	38
39	0 96287	0 96461	0 96630	0 96795	0 96956	0 97113	0 97266	0 97414	0 97559	0 97699	0 97835	39
40	0 96290	0 96464	0 96633	0 96798	0 96959	0 97116	0 97268	0 97417	0 97561	0 97701	0 97837	40
41	0 96293	0 96467	0 96636	0 96801	0 96962	0 97118	0 97271	0 97419	0 97563	0 97703	0 97839	41
42	0 96296	0 96469	0 96638	0 96803	0 96964	0 97121	0 97273	0 97422	0 97566	0 97706	0 97842	42
43	0 96299	0 96472	0 96641	0 96806	0 96967	0 97124	0 97276	0 97424	0 97568	0 97708	0 97844	43
44	0 96302	0 96475	0 96644	0 96809	0 96970	0 97126	0 97278	0 97426	0 97570	0 97710	0 97846	44
45	0 96305	0 96478	0 96647	0 96812	0 96972	0 97129	0 97281	0 97429	0 97573	0 97713	0 97848	45
46	0 96308	0 96481	0 96650	0 96814	0 96975	0 97131	0 97283	0 97431	0 97575	0 97715	0 97850	46
47	0 96311	0 96484	0 96652	0 96817	0 96978	0 97134	0 97286	0 97434	0 97578	0 97717	0 97853	47
48	0 96314	0 96487	0 96655	0 96820	0 96980	0 97136	0 97288	0 97436	0 97580	0 97719	0 97855	48
49	0 96317	0 96489	0 96658	0 96822	0 96983	0 97139	0 97291	0 97439	0 97582	0 97722	0 97857	49
50	0 96319	0 96492	0 96661	0 96825	0 96985	0 97141	0 97293	0 97441	0 97585	0 97724	0 97859	50
51	0 96322	0 96495	0 96664	0 96828	0 96988	0 97144	0 97296	0 97444	0 97587	0 97726	0 97862	51
52	0 96325	0 96498	0 96666	0 96831	0 96991	0 97147	0 97298	0 97446	0 97589	0 97729	0 97864	52
53	0 96328	0 96501	0 96669	0 96833	0 96993	0 97149	0 97301	0 97448	0 97592	0 97731	0 97866	53
54	0 96331	0 96504	0 96672	0 96836	0 96996	0 97152	0 97303	0 97451	0 97594	0 97733	0 97868	54
55	0 96334	0 96506	0 96675	0 96839	0 96999	0 97154	0 97306	0 97453	0 97596	0 97736	0 97870	55
56	0 96337	0 96509	0 96677	0 96841	0 97001	0 97157	0 97308	0 97455	0 97599	0 97738	0 97873	56
57	0 96340	0 96512	0 96680	0 96844	0 97004	0 97159	0 97311	0 97458	0 97601	0 97740	0 97875	57
58	0 96343	0 96515	0 96683	0 96847	0 97006	0 97162	0 97313	0 97460	0 97603	0 97742	0 97877	58
59	0 96346	0 96518	0 96686	0 96849	0 97009	0 97165	0 97316	0 97463	0 97606	0 97745	0 97879	59

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'
D. 2. Parts 0 0 1 1 1 1 1 2 2 2 2 2 3 3 3

LOG. SINE SQUARE

		172°				173°				174°			s.
		0'	15'	30'	45'	0'	15'	30'	45'	0'	15'	30'	
		11°28'	11°29'	11°30'	11°31'	11°32'	11°33'	11°34'	11°35'	11°36'	11°37'	11°38'	
0	0	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	0
	15	97882	98013	98138	98260	98378	98492	98602	98707	98809	98906	98999	1
	30	97884	98014	98140	98262	98380	98494	98604	98709	98810	98908	99001	2
	45	97886	98016	98142	98264	98382	98496	98605	98711	98812	98909	99002	3
1	0	97888	98018	98144	98266	98384	98498	98607	98713	98814	98911	99004	4
	15	97890	98020	98146	98268	98386	98500	98609	98714	98815	98912	99005	5
	30	97893	98023	98149	98270	98388	98501	98611	98716	98817	98914	99007	6
	45	97895	98025	98151	98272	98390	98503	98613	98718	98819	98916	99008	7
2	0	97897	98027	98153	98274	98392	98505	98614	98719	98820	98917	99010	8
	15	97899	98029	98155	98276	98394	98507	98616	98721	98822	98919	99011	9
	30	97901	98031	98157	98278	98396	98509	98618	98723	98824	98920	99013	10
	45	97904	98033	98159	98280	98398	98511	98620	98725	98825	98922	99014	11
3	0	97906	98036	98161	98282	98400	98513	98621	98726	98827	98923	99016	12
	15	97908	98038	98163	98284	98402	98514	98623	98728	98829	98925	99017	13
	30	97910	98040	98165	98286	98403	98516	98625	98730	98831	98926	99019	14
	45	97912	98042	98167	98288	98405	98518	98627	98731	98832	98928	99020	15
4	0	97915	98044	98169	98290	98407	98520	98629	98733	98834	98930	99022	16
	15	97917	98046	98171	98292	98409	98522	98632	98735	98835	98931	99023	17
	30	97919	98048	98173	98294	98411	98524	98632	98736	98837	98932	99025	18
	45	97921	98050	98175	98296	98413	98526	98634	98738	98838	98934	99027	19
5	0	97923	98052	98177	98298	98415	98527	98636	98740	98840	98936	99028	20
	15	97926	98054	98179	98300	98417	98529	98637	98742	98842	98938	99029	21
	30	97928	98057	98181	98302	98419	98531	98639	98743	98843	98939	99031	22
	45	97930	98059	98183	98304	98421	98533	98641	98745	98845	98941	99032	23
6	0	97932	98061	98186	98306	98422	98535	98643	98747	98847	98942	99034	24
	15	97934	98063	98188	98308	98424	98537	98644	98749	98848	98944	99035	25
	30	97936	98065	98190	98310	98426	98539	98646	98750	98850	98945	99037	26
	45	97939	98067	98192	98312	98428	98540	98648	98752	98851	98947	99038	27
7	0	97941	98069	98194	98314	98430	98542	98650	98753	98853	98948	99040	28
	15	97943	98071	98196	98316	98432	98544	98652	98755	98855	98950	99041	29
	30	97945	98074	98198	98318	98434	98546	98653	98757	98856	98951	99043	30
	45	97947	98076	98200	98320	98436	98548	98655	98759	98858	98953	99044	31
8	0	97949	98078	98202	98322	98438	98549	98658	98760	98860	98955	99046	32
	15	97952	98080	98204	98324	98440	98551	98659	98762	98861	98956	99047	33
	30	97954	98082	98206	98326	98442	98553	98660	98764	98863	98958	99048	34
	45	97956	98084	98208	98328	98444	98555	98662	98765	98864	98959	99050	35
9	0	97958	98086	98210	98330	98445	98557	98664	98767	98866	98961	99052	36
	15	97960	98088	98212	98332	98447	98558	98666	98769	98868	98962	99053	37
	30	97962	98090	98214	98334	98449	98560	98667	98770	98870	98964	99054	38
	45	97965	98092	98216	98336	98451	98562	98669	98772	98871	98965	99056	39
10	0	97967	98094	98218	98338	98453	98564	98671	98774	98872	98967	99057	40
	15	97969	98097	98220	98340	98455	98566	98673	98775	98874	98969	99059	41
	30	97971	98099	98222	98342	98456	98568	98674	98777	98876	98970	99060	42
	45	97973	98101	98224	98344	98458	98569	98676	98779	98877	98972	99062	43
11	0	97975	98103	98226	98345	98460	98571	98678	98781	98879	98973	99063	44
	15	97977	98105	98228	98347	98462	98573	98680	98782	98881	98975	99065	45
	30	97980	98108	98230	98349	98464	98575	98681	98784	98882	98976	99066	46
	45	97982	98109	98232	98351	98466	98577	98683	98786	98884	98978	99068	47
12	0	97984	98111	98234	98353	98468	98579	98685	98787	98885	98979	99069	48
	15	97986	98113	98236	98355	98470	98580	98687	98789	98887	98981	99071	49
	30	97988	98115	98238	98357	98472	98582	98688	98791	98888	98982	99072	50
	45	97990	98117	98240	98359	98473	98584	98690	98792	98890	98984	99074	51
13	0	97993	98120	98242	98361	98475	98586	98692	98794	98892	98985	99075	52
	15	97995	98122	98244	98363	98477	98588	98694	98796	98893	98987	99076	53
	30	97997	98124	98246	98365	98479	98589	98695	98797	98895	98989	99078	54
	45	97999	98126	98248	98367	98481	98591	98697	98799	98896	98990	99079	55
14	0	98001	98128	98250	98369	98483	98593	98699	98800	98898	98992	99081	56
	15	98003	98130	98252	98371	98485	98595	98701	98802	98900	98993	99082	57
	30	98006	98132	98254	98373	98487	98596	98702	98804	98901	98995	99084	58
	45	98008	98134	98256	98375	98488	98598	98704	98805	98903	98996	99085	59
	50	98010	98136	98258	98376	98490	98600	98706	98807	98904	98998	99087	60

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

I. 2. Parts 0 0 0 1 1 1 1 1 1 1 1 2 2 2 2

TABLE 69

891

LOG. SINE SQUARE															
	174°				175°				176°				177°		s.
	45'		0'		15'		30'		45'		0'		15'		
	11430	11440	11441	11442	11443	11444	11445	11446	11447	11448	11449				
0	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	0	
	99088	99173	99254	99330	99402	99471	99535	99595	99651	99702	99750			1	
	99089	99174	99255	99331	99404	99472	99536	99596	99652	99703	99751			2	
	99091	99176	99256	99333	99405	99473	99537	99597	99653	99704	99752			3	
	99092	99177	99257	99334	99406	99474	99538	99598	99654	99705	99753			4	
1	99094	99178	99259	99335	99407	99475	99539	99599	99655	99706	99753			5	
	99095	99180	99260	99336	99408	99476	99540	99600	99656	99707	99754			6	
	99097	99181	99261	99337	99409	99477	99541	99601	99657	99708	99755			7	
	99098	99183	99263	99339	99411	99478	99542	99602	99658	99709	99756			8	
	99100	99184	99264	99340	99412	99479	99543	99603	99659	99710	99757			9	
2	99101	99185	99265	99341	99413	99481	99544	99604	99660	99711	99757			10	
	99103	99187	99267	99342	99414	99482	99545	99605	99661	99712	99758			11	
	99104	99188	99268	99344	99415	99483	99546	99606	99662	99713	99759			12	
	99105	99189	99269	99345	99416	99484	99547	99607	99663	99714	99760			13	
	99107	99191	99270	99346	99418	99485	99548	99608	99664	99715	99761			14	
3	99108	99192	99271	99347	99419	99486	99549	99609	99665	99716	99762			15	
	99110	99193	99273	99349	99420	99487	99550	99609	99666	99717	99763			16	
	99111	99195	99274	99350	99421	99488	99551	99610	99666	99718	99764			17	
	99113	99196	99276	99351	99422	99489	99552	99611	99667	99719	99765			18	
	99114	99197	99277	99352	99423	99490	99553	99612	99668	99720	99766			19	
4	99115	99199	99279	99353	99424	99491	99554	99613	99669	99721	99767			20	
	99117	99200	99280	99355	99426	99492	99555	99614	99670	99722	99768			21	
	99118	99202	99281	99356	99427	99494	99556	99615	99671	99723	99769			22	
	99120	99203	99282	99357	99428	99495	99557	99616	99672	99724	99770			23	
	99121	99204	99283	99358	99429	99496	99558	99617	99673	99725	99771			24	
5	99123	99206	99285	99360	99430	99497	99559	99618	99674	99726	99772			25	
	99124	99207	99286	99361	99431	99498	99560	99619	99675	99727	99773			26	
	99125	99208	99287	99362	99433	99499	99561	99620	99676	99728	99774			27	
	99127	99210	99288	99363	99434	99500	99562	99621	99677	99729	99775			28	
	99128	99211	99290	99364	99435	99501	99563	99622	99678	99730	99776			29	
6	99130	99212	99291	99366	99436	99502	99564	99623	99679	99731	99777			30	
	99131	99214	99292	99367	99437	99503	99565	99624	99680	99732	99778			31	
	99132	99215	99293	99368	99438	99504	99566	99625	99681	99733	99779			32	
	99134	99216	99295	99369	99439	99505	99567	99626	99682	99734	99780			33	
	99135	99218	99296	99370	99440	99506	99568	99627	99683	99735	99781			34	
7	99137	99219	99297	99371	99441	99507	99569	99628	99684	99736	99782			35	
	99139	99220	99298	99373	99443	99509	99570	99629	99685	99737	99783			36	
	99140	99222	99300	99374	99444	99510	99571	99630	99686	99738	99784			37	
	99141	99223	99301	99375	99445	99511	99572	99631	99687	99739	99785			38	
	99142	99224	99303	99376	99446	99512	99573	99632	99688	99740	99786			39	
8	99144	99226	99304	99378	99447	99513	99574	99633	99689	99741	99787			40	
	99145	99227	99305	99379	99448	99514	99575	99634	99690	99742	99788			41	
	99146	99228	99306	99380	99450	99515	99576	99635	99691	99743	99789			42	
	99148	99230	99308	99381	99451	99516	99577	99636	99692	99744	99790			43	
	99149	99231	99309	99382	99452	99517	99578	99637	99693	99745	99791			44	
9	99151	99232	99310	99384	99453	99518	99579	99638	99694	99746	99792			45	
	99152	99234	99311	99385	99454	99519	99580	99639	99695	99747	99793			46	
	99153	99235	99312	99386	99455	99520	99581	99640	99696	99748	99794			47	
	99155	99236	99314	99387	99456	99521	99582	99641	99697	99749	99795			48	
	99156	99238	99315	99388	99457	99522	99583	99642	99698	99750	99796			49	
10	99158	99239	99316	99389	99459	99523	99584	99643	99699	99751	99797			50	
	99159	99240	99318	99391	99460	99524	99585	99644	99700	99752	99798			51	
	99160	99242	99319	99392	99461	99525	99586	99645	99701	99753	99799			52	
	99162	99243	99320	99393	99462	99526	99587	99646	99702	99754	99800			53	
	99163	99244	99321	99394	99463	99527	99588	99647	99703	99755	99801			54	
11	99165	99246	99323	99395	99464	99529	99589	99648	99704	99756	99802			55	
	99166	99247	99324	99397	99465	99530	99590	99649	99705	99757	99803			56	
	99167	99248	99325	99398	99466	99531	99591	99650	99706	99758	99804			57	
	99169	99250	99326	99399	99467	99532	99592	99651	99707	99759	99805			58	
	99170	99251	99328	99400	99469	99533	99593	99652	99708	99760	99806			59	
12	99172	99252	99329	99401	99470	99534	99594	99654	99710	99761	99808			60	

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 1. Parts o o o o o o o i i i i i i i i

Sec. 1' 2' 3' 4' 5' 6' 7' 8' 9' 10' 11' 12' 13' 14' 15'

D. 1. Parts 0 0 0 0 0 0 0 1 1 1 1 1 1 1 1

LOG. SINE SQUARE													
	177°		178°				179°				L		
	30'	45'	0'	15'	30'	45'	0'	15'	30'	45'			
	11°50"	11°51"	11°52"	11°53"	11°54"	11°55"	11°56"	11°57"	11°58"	11°59"			
0	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'9	9'99998	0	
15	99793	99833	99868	99899	99926	99949	99967	99981	99992	9'99999	9'99998	1	
30	99794	99833	99868	99899	99926	99949	99967	99982	99992	9'99999	9'99998	2	
45	99795	99834	99869	99900	99927	99949	99968	99982	99992	9'99999	9'99998	3	
1	99796	99835	99870	99901	99927	99950	99968	99982	99992	9'99999	9'99998	4	
15	99797	99836	99870	99901	99928	99950	99968	99982	99992	9'99999	9'99998	5	
30	99797	99836	99871	99902	99928	99950	99969	99983	99993	9'99999	9'99998	6	
45	99798	99837	99871	99902	99928	99951	99969	99983	99993	9'99999	9'99998	7	
2	99799	99838	99872	99903	99929	99951	99969	99983	99993	9'99999	9'99998	8	
15	99799	99838	99873	99903	99929	99951	99969	99983	99993	9'99999	9'99998	9	
30	99800	99839	99873	99903	99930	99952	99970	99983	99993	9'99999	9'99998	10	
45	99801	99839	99874	99904	99930	99952	99970	99984	99993	9'99999	9'99998	11	
3	99801	99840	99874	99904	99930	99952	99970	99984	99993	9'99999	9'99998	12	
15	99802	99841	99875	99905	99931	99953	99970	99984	99993	9'99999	9'99998	13	
30	99803	99841	99875	99905	99931	99953	99971	99984	99994	9'99999	9'99998	14	
45	99804	99842	99876	99906	99932	99953	99971	99984	99994	9'99999	9'99998	15	
4	99804	99842	99876	99906	99932	99954	99971	99985	99994	9'99999	9'99998	16	
15	99805	99843	99877	99907	99932	99954	99971	99985	99994	9'99999	9'99998	17	
30	99806	99844	99877	99907	99933	99954	99972	99985	99994	9'99999	9'99998	18	
45	99806	99844	99878	99908	99933	99955	99972	99985	99994	9'99999	9'99998	19	
5	99807	99845	99878	99908	99934	99955	99972	99985	99994	9'99999	9'99998	20	
15	99808	99845	99879	99908	99934	99955	99972	99985	99994	9'99999	9'99998	21	
30	99808	99846	99880	99909	99934	99956	99973	99986	99994	9'99999	9'99998	22	
45	99809	99846	99880	99909	99935	99956	99973	99986	99994	9'99999	9'99998	23	
6	99810	99847	99881	99910	99935	99956	99973	99986	99995	9'99999	9'99998	24	
15	99810	99848	99881	99910	99936	99957	99973	99986	99995	9'99999	9'99998	25	
30	99811	99848	99882	99911	99936	99957	99974	99986	99995	9'99999	9'99998	26	
45	99811	99849	99882	99911	99936	99957	99974	99987	99995	9'99999	9'99998	27	
7	99812	99849	99883	99912	99937	99958	99974	99987	99995	9'99999	9'99998	28	
15	99813	99850	99883	99912	99937	99958	99974	99987	99995	9'99999	9'99998	29	
30	99813	99851	99884	99913	99937	99958	99975	99987	99995	9'99999	9'99998	30	
45	99814	99851	99884	99913	99938	99958	99975	99987	99995	9'99999	9'99998	31	
8	99815	99852	99885	99914	99938	99959	99975	99987	99996	9'99999	9'99998	32	
15	99815	99852	99885	99914	99939	99959	99975	99988	99996	9'99999	9'99998	33	
30	99816	99853	99886	99914	99939	99959	99976	99988	99996	9'99999	9'99998	34	
45	99817	99854	99886	99915	99939	99960	99976	99988	99996	10'00000	10'00000	35	
9	99817	99854	99887	99915	99940	99960	99976	99988	99996	10'00000	10'00000	36	
15	99818	99855	99887	99916	99940	99960	99976	99988	99996	10'00000	10'00000	37	
30	99819	99855	99888	99916	99940	99961	99977	99988	99996	10'00000	10'00000	38	
45	99819	99856	99888	99917	99941	99961	99977	99989	99996	10'00000	10'00000	39	
10	99820	99856	99889	99917	99941	99961	99977	99989	99996	10'00000	10'00000	40	
15	99821	99857	99889	99918	99942	99961	99977	99989	99996	10'00000	10'00000	41	
30	99821	99858	99890	99918	99942	99962	99977	99989	99996	10'00000	10'00000	42	
45	99822	99858	99890	99918	99942	99962	99978	99989	99997	10'00000	10'00000	43	
11	99822	99859	99891	99919	99943	99962	99978	99989	99997	10'00000	10'00000	44	
15	99823	99859	99891	99919	99943	99963	99978	99990	99997	10'00000	10'00000	45	
30	99824	99860	99892	99920	99943	99963	99978	99990	99997	10'00000	10'00000	46	
45	99824	99860	99892	99920	99944	99963	99979	99990	99997	10'00000	10'00000	47	
12	99825	99861	99893	99920	99944	99964	99979	99990	99997	10'00000	10'00000	48	
15	99826	99862	99893	99921	99944	99964	99979	99990	99997	10'00000	10'00000	49	
30	99826	99862	99894	99921	99945	99964	99979	99990	99997	10'00000	10'00000	50	
45	99827	99863	99894	99922	99945	99964	99979	99990	99997	10'00000	10'00000	51	
13	99827	99863	99895	99922	99946	99965	99980	99991	99997	10'00000	10'00000	52	
15	99828	99864	99895	99923	99946	99965	99980	99991	99997	10'00000	10'00000	53	
30	99829	99864	99896	99923	99946	99965	99980	99991	99997	10'00000	10'00000	54	
45	99829	99865	99896	99923	99947	99966	99980	99991	99998	10'00000	10'00000	55	
14	99830	99865	99897	99924	99947	99966	99981	99991	99998	10'00000	10'00000	56	
15	99831	99866	99897	99924	99947	99966	99981	99991	99998	10'00000	10'00000	57	
30	99831	99866	99898	99925	99948	99966	99981	99991	99998	10'00000	10'00000	58	
45	99832	99867	99898	99925	99948	99967	99981	99992	99998	10'00000	10'00000	59	

TABLE 70

LOGARITHMS
FOR COMPUTING THE REDUCTION TO THE MERIDIAN, AT SEA.
PART I. Latitude and Declination of the same name.

Lat.	DECLINATION.												Lat.
	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	
0°						1°359	1°279	1°212	1°153	1°101	1°055	1°012	0°
1							1°358	1°278	1°211	1°152	1°100	1°053	1
2								1°277	1°210	1°151	1°098	1°051	2
3								1°357	1°276	1°150	1°097	1°050	3
4									1°356	1°275	1°096	1°049	4
5	1°359									1°354	1°274	1°206	5
6	1°279	1°358									1°352	1°272	6
7	1°212	1°278	1°357									1°350	7
8	1°153	1°211	1°277	1°356									8
9	1°101	1°152	1°209	1°276	1°354								9
10	1°055	1°100	1°151	1°208	1°274	1°352							10
11	1°012	1°053	1°098	1°149	1°206	1°272	1°350						11
12	0°974	1°011	1°051	1°097	1°147	1°204	1°270	1°348					12
13	0°938	0°972	1°009	1°049	1°094	1°145	1°201	1°267	1°345				13
14	0°904	0°936	0°970	1°007	1°047	1°092	1°142	1°199	1°264	1°342			14
15	0°873	0°902	0°934	0°967	1°004	1°045	1°089	1°139	1°196	1°261	1°339		15
16	0°844	0°871	0°900	0°931	0°965	1°002	1°042	1°086	1°136	1°193	1°258	1°336	16
17	0°816	0°841	0°868	0°897	0°928	0°962	0°999	1°039	1°083	1°133	1°189	1°254	17
18	0°789	0°813	0°839	0°866	0°895	0°925	0°959	0°995	1°035	1°080	1°129	1°185	18
19	0°764	0°787	0°811	0°836	0°863	0°891	0°922	0°956	0°992	1°032	1°076	1°125	19
20	0°740	0°761	0°784	0°807	0°833	0°859	0°888	0°919	0°952	0°988	1°028	1°072	20
21	0°717	0°737	0°758	0°781	0°804	0°829	0°856	0°884	0°915	0°948	0°984	1°023	21
22	0°695	0°714	0°734	0°755	0°777	0°801	0°825	0°852	0°880	0°911	0°944	0°980	22
23	0°673	0°691	0°710	0°730	0°751	0°773	0°797	0°821	0°848	0°876	0°906	0°939	23
24	0°652	0°670	0°688	0°707	0°727	0°747	0°769	0°793	0°817	0°844	0°871	0°902	24
25	0°632	0°649	0°666	0°684	0°703	0°723	0°743	0°765	0°788	0°813	0°839	0°867	25
26	0°613	0°629	0°645	0°662	0°680	0°699	0°718	0°739	0°760	0°783	0°808	0°834	26
27	0°594	0°609	0°625	0°641	0°658	0°676	0°694	0°714	0°734	0°756	0°778	0°803	27
28	0°575	0°590	0°605	0°620	0°637	0°653	0°671	0°689	0°709	0°729	0°750	0°773	28
29	0°557	0°571	0°586	0°600	0°616	0°632	0°649	0°666	0°684	0°703	0°724	0°745	29
30	0°540	0°553	0°567	0°581	0°596	0°611	0°627	0°643	0°661	0°679	0°698	0°718	30
31	0°522	0°535	0°548	0°562	0°576	0°591	0°606	0°622	0°638	0°655	0°673	0°692	31
32	0°505	0°518	0°530	0°543	0°557	0°571	0°585	0°600	0°616	0°632	0°649	0°667	32
33	0°489	0°500	0°513	0°525	0°538	0°551	0°565	0°580	0°594	0°610	0°626	0°643	33
34	0°472	0°483	0°495	0°507	0°519	0°532	0°546	0°559	0°574	0°588	0°604	0°620	34
35	0°456	0°467	0°478	0°489	0°501	0°514	0°526	0°540	0°553	0°567	0°582	0°597	35
36	0°440	0°450	0°461	0°472	0°484	0°495	0°508	0°520	0°533	0°548	0°560	0°575	36
37	0°424	0°434	0°445	0°455	0°466	0°478	0°489	0°501	0°514	0°526	0°540	0°553	37
38	0°408	0°418	0°428	0°438	0°449	0°460	0°471	0°482	0°494	0°507	0°519	0°532	38
39	0°393	0°402	0°412	0°422	0°432	0°442	0°453	0°464	0°475	0°487	0°499	0°512	39
40	0°377	0°386	0°396	0°405	0°415	0°425	0°435	0°447	0°457	0°468	0°480	0°492	40
41	0°362	0°371	0°380	0°389	0°398	0°408	0°418	0°428	0°438	0°449	0°460	0°472	41
42	0°347	0°355	0°364	0°373	0°382	0°391	0°400	0°410	0°420	0°431	0°441	0°452	42
43	0°331	0°340	0°348	0°356	0°365	0°374	0°383	0°393	0°402	0°412	0°422	0°433	43
44	0°316	0°324	0°332	0°340	0°349	0°357	0°366	0°375	0°384	0°394	0°404	0°414	44
45	0°301	0°309	0°316	0°324	0°333	0°341	0°349	0°358	0°367	0°376	0°385	0°395	45
46	0°286	0°293	0°301	0°308	0°316	0°324	0°332	0°341	0°349	0°358	0°367	0°376	46
47	0°271	0°278	0°285	0°292	0°300	0°308	0°315	0°323	0°331	0°340	0°349	0°358	47
48	0°255	0°262	0°269	0°276	0°284	0°291	0°299	0°306	0°314	0°322	0°331	0°339	48
49	0°240	0°247	0°254	0°260	0°267	0°275	0°282	0°289	0°297	0°305	0°312	0°321	49
50	0°225	0°231	0°238	0°244	0°251	0°258	0°265	0°272	0°279	0°287	0°294	0°302	50
51	0°209	0°216	0°222	0°228	0°235	0°241	0°248	0°255	0°262	0°269	0°276	0°284	51
52	0°194	0°200	0°206	0°212	0°218	0°225	0°231	0°238	0°244	0°251	0°258	0°265	52
53	0°178	0°184	0°190	0°196	0°202	0°208	0°214	0°220	0°227	0°233	0°240	0°247	53
54	0°162	0°168	0°173	0°179	0°185	0°191	0°197	0°203	0°209	0°215	0°222	0°228	54
55	0°146	0°152	0°157	0°162	0°168	0°174	0°179	0°185	0°191	0°197	0°204	0°210	55
56	0°130	0°135	0°140	0°146	0°151	0°156	0°162	0°168	0°173	0°179	0°185	0°191	56
57	0°114	0°118	0°124	0°129	0°134	0°139	0°144	0°150	0°155	0°160	0°166	0°172	57
58	0°097	0°100	0°106	0°111	0°116	0°121	0°126	0°131	0°137	0°142	0°148	0°153	58
59	0°080	0°084	0°089	0°094	0°098	0°103	0°108	0°113	0°118	0°123	0°128	0°134	59
60	0°062	0°067	0°071	0°076	0°080	0°085	0°090	0°094	0°099	0°104	0°109	0°114	60
61	0°045	0°049	0°053	0°058	0°062	0°066	0°071	0°075	0°080	0°085	0°089	0°094	61
62	0°027	0°031	0°035	0°039	0°043	0°047	0°052	0°056	0°060	0°065	0°069	0°074	62

LOGARITHMS
FOR COMPUTING THE REDUCTION TO THE MERIDIAN, AT SEA.
PART I. Latitude and Declination of the same name.

Lat.	DECLINATION.												Lat.
	12°	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	
0°	0'974	0'938	0'904	0'873	0'844	0'816	0'789	0'764	0'740	0'717	0'695	0'673	0°
1	1'011	0'972	0'936	0'902	0'871	0'841	0'813	0'787	0'761	0'737	0'714	0'691	1
2	1'051	1'009	0'970	0'934	0'900	0'868	0'839	0'811	0'784	0'758	0'734	0'710	2
3	1'097	1'049	1'007	0'967	0'931	0'897	0'866	0'836	0'807	0'781	0'755	0'730	3
4	1'147	1'094	1'047	1'004	0'965	0'928	0'895	0'863	0'833	0'804	0'777	0'751	4
5	1'204	1'145	1'092	1'045	1'002	0'962	0'925	0'891	0'859	0'829	0'801	0'773	5
6	1'270	1'201	1'142	1'089	1'042	0'999	0'959	0'922	0'888	0'856	0'825	0'797	6
7	1'348	1'267	1'199	1'139	1'086	1'039	0'995	0'956	0'919	0'884	0'852	0'821	7
8		1'345	1'264	1'196	1'136	1'083	1'035	0'992	0'953	0'915	0'880	0'848	8
9			1'342	1'261	1'193	1'133	1'080	1'032	0'988	0'948	0'911	0'876	9
10				1'339	1'258	1'189	1'129	1'076	1'028	0'984	0'944	0'906	10
11					1'336		1'185	1'125	1'072	0'980	0'980	0'939	11
12						1'332	1'181	1'121	1'067	1'019	0'975	0'935	12
13							1'250	1'181	1'121	1'067	1'019	0'975	13
14							1'328	1'246	1'177	1'116	1'063	1'014	14
15								1'323	1'243	1'172	1'112	1'058	15
16									1'319	1'237	1'167	1'106	16
17	1'332									1'314		1'226	17
18	1'250	1'328									1'308		18
19	1'181	1'246	1'323									1'303	19
20	1'121	1'177	1'242	1'319									20
21	1'067	1'116	1'172	1'237	1'314								21
22	1'019	1'063	1'112	1'167	1'232	1'308							22
23	0'975	1'014	1'058	1'106	1'162	1'226	1'303						23
24	0'934	0'970	1'009	1'052	1'101	1'156	1'221	1'297					24
25	0'897	0'929	0'965	1'004	1'047	1'095	1'151	1'215	1'291				25
26	0'861	0'890	0'924	0'959	0'998	1'041	1'090	1'144	1'208	1'285			26
27	0'828	0'856	0'886	0'918	0'953	0'992	1'035	1'083	1'138	1'202	1'278		27
28	0'797	0'823	0'850	0'880	0'912	0'947	0'986	1'028	1'076	1'131	1'195	1'271	28
29	0'767	0'791	0'817	0'844	0'874	0'906	0'940	0'979	1'021	1'069	1'124	1'188	29
30	0'739	0'761	0'785	0'811	0'838	0'867	0'899	0'934	0'972	1'014	1'062	1'117	30
31	0'712	0'733	0'755	0'779	0'804	0'831	0'860	0'892	0'926	0'965	1'007	1'055	31
32	0'686	0'706	0'726	0'748	0'772	0'797	0'824	0'853	0'885	0'919	0'957	0'999	32
33	0'661	0'679	0'699	0'720	0'742	0'765	0'790	0'817	0'846	0'877	0'911	0'949	33
34	0'636	0'654	0'672	0'692	0'712	0'734	0'757	0'782	0'809	0'838	0'869	0'903	34
35	0'612	0'630	0'647	0'665	0'685	0'705	0'727	0'750	0'774	0'801	0'829	0'861	35
36	0'590	0'606	0'622	0'640	0'658	0'677	0'697	0'719	0'742	0'766	0'792	0'821	36
37	0'568	0'583	0'598	0'615	0'632	0'650	0'669	0'689	0'710	0'733	0'758	0'784	37
38	0'546	0'560	0'575	0'591	0'607	0'624	0'642	0'661	0'681	0'702	0'724	0'749	38
39	0'525	0'538	0'552	0'567	0'582	0'599	0'615	0'633	0'652	0'672	0'693	0'715	39
40	0'504	0'517	0'530	0'544	0'559	0'574	0'590	0'607	0'624	0'643	0'662	0'683	40
41	0'484	0'496	0'509	0'522	0'536	0'550	0'565	0'581	0'597	0'615	0'633	0'653	41
42	0'464	0'475	0'487	0'500	0'513	0'527	0'541	0'556	0'572	0'588	0'605	0'623	42
43	0'444	0'455	0'466	0'478	0'491	0'504	0'517	0'532	0'546	0'562	0'578	0'595	43
44	0'424	0'435	0'446	0'457	0'469	0'482	0'494	0'508	0'522	0'536	0'552	0'568	44
45	0'405	0'415	0'426	0'436	0'448	0'460	0'472	0'484	0'498	0'511	0'526	0'541	45
46	0'386	0'395	0'405	0'416	0'427	0'438	0'449	0'461	0'474	0'487	0'501	0'515	46
47	0'367	0'376	0'386	0'396	0'406	0'416	0'427	0'439	0'451	0'463	0'476	0'490	47
48	0'348	0'357	0'366	0'375	0'385	0'395	0'406	0'417	0'428	0'440	0'452	0'465	48
49	0'329	0'337	0'346	0'355	0'365	0'374	0'384	0'395	0'405	0'417	0'428	0'440	49
50	0'310	0'318	0'327	0'335	0'344	0'354	0'363	0'373	0'383	0'394	0'405	0'416	50
51	0'291	0'299	0'307	0'316	0'324	0'333	0'342	0'351	0'361	0'371	0'381	0'392	51
52	0'273	0'280	0'288	0'296	0'304	0'312	0'321	0'330	0'339	0'349	0'359	0'369	52
53	0'254	0'261	0'269	0'276	0'284	0'292	0'300	0'309	0'317	0'326	0'336	0'346	53
54	0'235	0'242	0'249	0'257	0'264	0'271	0'279	0'287	0'296	0'304	0'313	0'321	54
55	0'216	0'223	0'230	0'236	0'244	0'251	0'258	0'266	0'274	0'282	0'291	0'299	55
56	0'197	0'204	0'210	0'217	0'222	0'230	0'237	0'245	0'252	0'260	0'268	0'277	56
57	0'178	0'184	0'190	0'197	0'203	0'210	0'216	0'223	0'231	0'238	0'246	0'254	57
58	0'159	0'164	0'170	0'176	0'183	0'189	0'195	0'202	0'209	0'216	0'223	0'231	58
59	0'139	0'145	0'150	0'156	0'162	0'168	0'174	0'180	0'187	0'194	0'201	0'208	59
60	0'119	0'125	0'130	0'135	0'141	0'147	0'153	0'159	0'165	0'171	0'178	0'185	60
61	0'099	0'104	0'109	0'115	0'120	0'125	0'131	0'137	0'143	0'149	0'155	0'161	61
62	0'079	0'084	0'088	0'093	0'099	0'104	0'110	0'115	0'120	0'126	0'132	0'138	62

LOGARITHMS
FOR COMPUTING THE REDUCTION TO THE MERIDIAN, AT SEA.
PART I. Latitude and Declination of the same name.

Lat.	DECLINATION.													Lat.
	24°	25°	26°	27°	28°	29°	30°	31°	32°	33°	34°	35°		
0°	0.652	0.632	0.613	0.594	0.575	0.557	0.539	0.522	0.505	0.489	0.472	0.456	0°	
1	0.670	0.649	0.629	0.609	0.590	0.571	0.553	0.535	0.518	0.501	0.484	0.467	1	
2	0.688	0.666	0.645	0.625	0.605	0.586	0.567	0.548	0.530	0.513	0.496	0.478	2	
3	0.707	0.684	0.662	0.641	0.621	0.601	0.581	0.562	0.543	0.525	0.508	0.490	3	
4	0.727	0.703	0.680	0.658	0.637	0.616	0.596	0.576	0.557	0.538	0.520	0.502	4	
5	0.747	0.723	0.699	0.676	0.654	0.632	0.611	0.591	0.571	0.551	0.532	0.514	5	
6	0.769	0.743	0.718	0.694	0.671	0.649	0.627	0.606	0.585	0.565	0.545	0.526	6	
7	0.793	0.765	0.739	0.714	0.689	0.666	0.644	0.622	0.601	0.580	0.559	0.539	7	
8	0.817	0.788	0.760	0.734	0.709	0.684	0.661	0.638	0.616	0.595	0.574	0.553	8	
9	0.844	0.813	0.783	0.755	0.729	0.704	0.679	0.655	0.632	0.610	0.589	0.567	9	
10	0.872	0.839	0.808	0.778	0.750	0.724	0.698	0.673	0.649	0.626	0.604	0.582	10	
11	0.902	0.867	0.834	0.803	0.773	0.745	0.718	0.692	0.667	0.643	0.620	0.597	11	
12	0.935	0.897	0.862	0.829	0.797	0.767	0.739	0.712	0.686	0.661	0.637	0.613	12	
13	0.970	0.930	0.892	0.857	0.823	0.791	0.761	0.733	0.706	0.680	0.654	0.630	13	
14	1.010	0.965	0.924	0.886	0.850	0.817	0.785	0.755	0.726	0.699	0.673	0.647	14	
15	1.053	1.004	0.959	0.918	0.880	0.844	0.811	0.779	0.749	0.720	0.692	0.665	15	
16	1.101	1.047	0.998	0.953	0.911	0.874	0.838	0.804	0.772	0.742	0.713	0.685	16	
17	1.157	1.096	1.041	0.992	0.947	0.905	0.867	0.831	0.797	0.765	0.735	0.705	17	
18	1.222	1.151	1.089	1.035	0.986	0.940	0.898	0.860	0.824	0.790	0.758	0.727	18	
19	1.297	1.216	1.145	1.083	1.029	0.980	0.934	0.891	0.853	0.817	0.782	0.750	19	
20		1.291	1.210	1.138	1.076	1.022	0.973	0.927	0.884	0.846	0.809	0.774	20	
21			1.285	1.203	1.131	1.069	1.015	0.965	0.919	0.877	0.838	0.800	21	
22				1.278	1.196	1.124	1.061	1.007	0.957	0.911	0.868	0.829	22	
23					1.271	1.189	1.117	1.054	0.999	0.949	0.903	0.860	23	
24						1.264	1.182	1.109	1.046	0.991	0.941	0.894	24	
25							1.256	1.173	1.101	1.038	0.983	0.933	25	
26								1.248	1.165	1.092	1.029	0.974	26	
27									1.239	1.156	1.083	1.020	27	
28										1.230	1.147	1.074	28	
29	1.264										1.221	1.138	29	
30	1.112	1.256										1.212	30	
31	1.109	1.174	1.248										31	
32	1.046	1.101	1.166	1.239									32	
33	0.991	1.038	1.093	1.157	1.230								33	
34	0.941	0.983	1.030	1.084	1.147	1.221							34	
35	0.895	0.933	0.974	1.021	1.075	1.138	1.212						35	
36	0.852	0.886	0.924	0.965	1.012	1.065	1.128	1.202					36	
37	0.812	0.843	0.877	0.914	0.955	1.002	1.055	1.118	1.191				37	
38	0.775	0.803	0.834	0.867	0.904	0.945	0.992	1.045	1.107	1.181			38	
39	0.740	0.765	0.793	0.823	0.857	0.894	0.935	0.982	1.034	1.097	1.170		39	
40	0.706	0.730	0.755	0.783	0.814	0.847	0.883	0.924	0.970	1.023	1.086	1.158	40	
41	0.673	0.696	0.719	0.745	0.773	0.803	0.836	0.872	0.914	0.958	1.012	1.075	41	
42	0.642	0.663	0.685	0.709	0.734	0.762	0.792	0.825	0.861	0.901	0.947	1.000	42	
43	0.613	0.632	0.653	0.675	0.698	0.723	0.751	0.781	0.813	0.849	0.889	0.934	43	
44	0.585	0.602	0.621	0.642	0.664	0.687	0.712	0.739	0.769	0.801	0.837	0.877	44	
45	0.557	0.574	0.591	0.610	0.631	0.652	0.675	0.700	0.727	0.756	0.789	0.825	45	
46	0.530	0.546	0.562	0.580	0.599	0.619	0.640	0.663	0.687	0.714	0.744	0.776	46	
47	0.504	0.519	0.534	0.551	0.568	0.587	0.607	0.628	0.650	0.675	0.701	0.731	47	
48	0.478	0.492	0.507	0.522	0.539	0.556	0.575	0.594	0.615	0.637	0.662	0.688	48	
49	0.453	0.466	0.480	0.494	0.510	0.526	0.543	0.561	0.581	0.601	0.624	0.648	49	
50	0.428	0.440	0.453	0.467	0.482	0.497	0.513	0.530	0.548	0.567	0.588	0.610	50	
51	0.403	0.415	0.427	0.440	0.454	0.468	0.483	0.499	0.516	0.534	0.553	0.573	51	
52	0.379	0.390	0.402	0.414	0.427	0.440	0.454	0.469	0.485	0.501	0.519	0.538	52	
53	0.356	0.366	0.377	0.388	0.400	0.413	0.426	0.440	0.454	0.470	0.486	0.504	53	
54	0.332	0.342	0.352	0.363	0.374	0.386	0.398	0.411	0.425	0.439	0.455	0.471	54	
55	0.308	0.318	0.328	0.338	0.348	0.359	0.371	0.383	0.396	0.410	0.424	0.438	55	
56	0.285	0.294	0.303	0.313	0.322	0.333	0.344	0.356	0.368	0.380	0.394	0.408	56	
57	0.262	0.270	0.279	0.288	0.297	0.307	0.317	0.328	0.340	0.352	0.364	0.377	57	
58	0.238	0.246	0.254	0.263	0.272	0.281	0.291	0.301	0.312	0.323	0.335	0.347	58	
59	0.215	0.222	0.230	0.238	0.247	0.255	0.264	0.274	0.284	0.295	0.306	0.317	59	
60	0.191	0.198	0.205	0.213	0.221	0.230	0.238	0.247	0.257	0.267	0.277	0.288	60	
61	0.168	0.174	0.181	0.188	0.196	0.204	0.212	0.220	0.229	0.238	0.248	0.258	61	
62	0.144	0.150	0.157	0.164	0.171	0.178	0.186	0.194	0.202	0.211	0.220	0.229	62	

LOGARITHMS
FOR COMPUTING THE REDUCTION TO THE MERIDIAN, AT SEA.
PART II. Latitude and Declination of *contrary* Names.

DECLINATION.													Lat.
Lat.	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	
0°						1°359	1°279	1°212	1°153	1°101	1°055	1°012	0
1					1°360	1°280	1°213	1°154	1°102	1°056	1°014	0°975	1
2					1°281	1°213	1°155	1°103	1°057	1°015	0°976	0°941	2
3			1°360		1°213	1°155	1°104	1°058	1°016	0°977	0°942	0°909	3
4		1°360	1°280		1°213	1°155	1°104	1°058	1°016	0°978	0°943	0°910	4
5	1°359	1°280	1°213		1°155	1°104	1°058	1°016	0°978	0°943	0°910	0°880	5
6	1°279	1°213	1°155		1°104	1°058	1°016	0°979	0°943	0°911	0°880	0°852	6
7	1°212	1°154	1°103		1°058	1°016	0°978	0°943	0°911	0°881	0°851	0°825	7
8	1°153	1°102	1°057		1°016	0°978	0°943	0°911	0°881	0°852	0°825	0°800	8
9	1°101	1°056	1°015		0°977	0°943	0°910	0°880	0°852	0°825	0°800	0°776	9
10	1°055	1°014	0°976		0°942	0°910	0°880	0°852	0°825	0°800	0°776	0°754	10
11	1°012	0°975	0°941		0°909	0°879	0°851	0°825	0°800	0°776	0°754	0°732	11
12	0°974	0°939	0°907		0°878	0°850	0°824	0°799	0°775	0°753	0°732	0°711	12
13	0°938	0°906	0°876		0°849	0°823	0°798	0°775	0°752	0°731	0°711	0°691	13
14	0°904	0°875	0°847		0°821	0°797	0°774	0°751	0°730	0°710	0°691	0°672	14
15	0°873	0°846	0°820		0°795	0°772	0°750	0°729	0°709	0°690	0°671	0°653	15
16	0°844	0°818	0°794		0°771	0°749	0°728	0°708	0°689	0°670	0°653	0°635	16
17	0°816	0°792	0°769		0°747	0°726	0°706	0°687	0°669	0°651	0°634	0°617	17
18	0°789	0°767	0°745		0°724	0°705	0°686	0°668	0°650	0°633	0°617	0°601	18
19	0°764	0°743	0°722		0°703	0°684	0°666	0°648	0°632	0°615	0°600	0°584	19
20	0°740	0°720	0°700		0°682	0°664	0°646	0°630	0°614	0°598	0°583	0°568	20
21	0°717	0°698	0°679		0°661	0°644	0°628	0°612	0°596	0°581	0°567	0°553	21
22	0°695	0°676	0°659		0°642	0°625	0°609	0°594	0°579	0°565	0°551	0°537	22
23	0°673	0°656	0°639		0°623	0°607	0°592	0°577	0°563	0°549	0°535	0°522	23
24	0°652	0°636	0°621		0°604	0°589	0°575	0°560	0°547	0°533	0°520	0°508	24
25	0°632	0°616	0°601		0°586	0°572	0°558	0°544	0°531	0°518	0°505	0°493	25
26	0°613	0°598	0°583		0°569	0°555	0°541	0°528	0°515	0°503	0°491	0°479	26
27	0°594	0°579	0°565		0°551	0°538	0°525	0°512	0°500	0°488	0°476	0°465	27
28	0°575	0°561	0°548		0°535	0°522	0°509	0°497	0°485	0°473	0°462	0°451	28
29	0°557	0°544	0°531		0°518	0°506	0°494	0°482	0°470	0°459	0°448	0°437	29
30	0°540	0°527	0°514		0°502	0°490	0°478	0°467	0°456	0°445	0°434	0°425	30
31	0°522	0°510	0°498		0°486	0°474	0°463	0°452	0°442	0°431	0°421	0°411	31
32	0°505	0°493	0°482		0°470	0°459	0°448	0°438	0°427	0°417	0°407	0°397	32
33	0°489	0°477	0°466		0°455	0°444	0°434	0°423	0°413	0°403	0°394	0°384	33
34	0°472	0°461	0°450		0°440	0°429	0°419	0°409	0°399	0°390	0°380	0°371	34
35	0°456	0°445	0°435		0°424	0°414	0°405	0°395	0°386	0°376	0°367	0°358	35
36	0°440	0°429	0°419		0°410	0°400	0°390	0°381	0°372	0°363	0°354	0°345	36
37	0°424	0°414	0°404		0°395	0°385	0°376	0°367	0°358	0°350	0°341	0°333	37
38	0°408	0°399	0°389		0°380	0°371	0°362	0°353	0°345	0°336	0°328	0°320	38
39	0°393	0°384	0°374		0°365	0°357	0°348	0°340	0°331	0°323	0°315	0°307	39
40	0°377	0°368	0°360		0°351	0°342	0°334	0°326	0°318	0°310	0°302	0°294	40
41	0°362	0°353	0°345		0°336	0°328	0°320	0°312	0°304	0°297	0°289	0°282	41
42	0°347	0°338	0°330		0°322	0°314	0°306	0°299	0°291	0°284	0°276	0°269	42
43	0°331	0°323	0°315		0°308	0°300	0°292	0°285	0°278	0°270	0°263	0°256	43
44	0°316	0°308	0°301		0°293	0°286	0°279	0°271	0°264	0°257	0°250	0°243	44
45	0°301	0°294	0°286		0°279	0°272	0°265	0°258	0°251	0°244	0°237	0°231	45
46	0°286	0°279	0°271		0°264	0°257	0°251	0°244	0°237	0°231	0°224	0°218	46
47	0°271	0°264	0°257		0°250	0°243	0°237	0°230	0°224	0°217	0°211	0°205	47
48	0°255	0°249	0°242		0°235	0°229	0°223	0°216	0°210	0°204	0°198	0°191	48
49	0°240	0°234	0°227		0°221	0°215	0°208	0°202	0°196	0°190	0°184	0°178	49
50	0°225	0°219	0°212		0°206	0°200	0°194	0°188	0°182	0°176	0°171	0°165	50
51	0°209	0°203	0°197		0°191	0°185	0°180	0°174	0°168	0°163	0°157	0°151	51
52	0°194	0°188	0°182		0°176	0°171	0°165	0°160	0°154	0°149	0°143	0°138	52
53	0°178	0°172	0°167		0°161	0°156	0°150	0°145	0°140	0°134	0°129	0°124	53
54	0°162	0°157	0°151		0°146	0°141	0°136	0°130	0°125	0°120	0°115	0°110	54
55	0°146	0°141	0°136		0°131	0°125	0°120	0°115	0°110	0°105	0°101	0°096	55
56	0°130	0°125	0°120		0°115	0°110	0°105	0°100	0°095	0°091	0°086	0°081	56
57	0°114	0°109	0°104		0°099	0°094	0°090	0°085	0°080	0°076	0°071	0°066	57
58	0°097	0°092	0°087		0°083	0°078	0°074	0°069	0°065	0°060	0°056	0°051	58
59	0°080	0°075	0°071		0°066	0°062	0°058	0°053	0°049	0°045	0°040	0°036	59
60	0°062	0°058	0°054		0°050	0°045	0°041	0°037	0°033	0°029	0°024	0°020	60
61	0°045	0°041	0°036		0°032	0°028	0°024	0°020	0°016	0°012	0°008	0°004	61
62	0°027	0°023	0°019		0°015	0°011	0°007	0°003	9°999	9°995	9°992	9°988	62

TABLE 70

896

LOGARITHMS
FOR COMPUTING THE REDUCTION TO THE MERIDIAN, AT SEA
Part II. Latitude and Declination of *contrary* Names.

Lat.	DECLINATION.												Lat.
	12°	13°	14°	15°	16°	17°	18°	19°	20°	21°	22°	23°	
0°	0.974	0.938	0.904	0.873	0.844	0.816	0.789	0.764	0.740	0.717	0.695	0.673	0°
1	0.939	0.906	0.875	0.846	0.818	0.792	0.767	0.743	0.720	0.698	0.676	0.656	1
2	0.907	0.876	0.847	0.820	0.794	0.769	0.745	0.722	0.700	0.679	0.659	0.639	2
3	0.878	0.849	0.821	0.795	0.771	0.747	0.724	0.703	0.682	0.661	0.642	0.623	3
4	0.850	0.823	0.797	0.772	0.749	0.726	0.705	0.684	0.664	0.644	0.625	0.607	4
5	0.824	0.798	0.774	0.750	0.728	0.706	0.686	0.666	0.646	0.628	0.609	0.592	5
6	0.799	0.775	0.751	0.729	0.708	0.687	0.668	0.648	0.630	0.612	0.594	0.577	6
7	0.776	0.752	0.730	0.709	0.689	0.669	0.650	0.632	0.614	0.596	0.579	0.563	7
8	0.753	0.731	0.710	0.690	0.670	0.651	0.633	0.615	0.598	0.581	0.565	0.549	8
9	0.732	0.711	0.691	0.671	0.653	0.634	0.617	0.600	0.583	0.567	0.551	0.535	9
10	0.711	0.691	0.672	0.653	0.635	0.618	0.601	0.584	0.568	0.553	0.537	0.522	10
11	0.692	0.672	0.654	0.636	0.619	0.602	0.586	0.570	0.554	0.539	0.524	0.509	11
12	0.673	0.654	0.636	0.619	0.603	0.586	0.571	0.555	0.540	0.525	0.511	0.497	12
13	0.654	0.637	0.620	0.603	0.587	0.571	0.556	0.541	0.527	0.512	0.498	0.485	13
14	0.636	0.620	0.603	0.587	0.572	0.557	0.542	0.527	0.513	0.499	0.486	0.473	14
15	0.619	0.602	0.587	0.572	0.557	0.542	0.528	0.514	0.500	0.487	0.474	0.461	15
16	0.603	0.587	0.572	0.557	0.542	0.528	0.515	0.501	0.488	0.475	0.462	0.449	16
17	0.586	0.571	0.557	0.542	0.528	0.515	0.501	0.488	0.475	0.463	0.450	0.438	17
18	0.571	0.556	0.542	0.528	0.515	0.501	0.488	0.475	0.463	0.451	0.438	0.426	18
19	0.555	0.541	0.527	0.514	0.501	0.488	0.475	0.463	0.451	0.439	0.427	0.415	19
20	0.540	0.527	0.513	0.500	0.488	0.475	0.463	0.451	0.439	0.427	0.416	0.404	20
21	0.525	0.512	0.499	0.487	0.475	0.462	0.451	0.439	0.427	0.416	0.405	0.393	21
22	0.511	0.498	0.486	0.474	0.462	0.450	0.438	0.427	0.416	0.405	0.394	0.383	22
23	0.497	0.485	0.472	0.461	0.449	0.438	0.426	0.415	0.404	0.393	0.383	0.372	23
24	0.483	0.471	0.459	0.448	0.437	0.425	0.414	0.404	0.393	0.382	0.372	0.362	24
25	0.469	0.458	0.446	0.435	0.424	0.413	0.403	0.392	0.382	0.372	0.361	0.351	25
26	0.456	0.445	0.434	0.423	0.412	0.402	0.391	0.381	0.371	0.361	0.351	0.341	26
27	0.442	0.432	0.421	0.410	0.400	0.390	0.380	0.370	0.360	0.350	0.340	0.331	27
28	0.429	0.419	0.408	0.398	0.388	0.378	0.368	0.359	0.349	0.339	0.330	0.320	28
29	0.416	0.406	0.396	0.386	0.376	0.367	0.357	0.347	0.338	0.329	0.320	0.310	29
30	0.403	0.394	0.384	0.374	0.364	0.355	0.346	0.336	0.327	0.318	0.309	0.300	30
31	0.391	0.381	0.372	0.362	0.353	0.344	0.335	0.326	0.317	0.308	0.299	0.290	31
32	0.378	0.369	0.359	0.350	0.341	0.332	0.323	0.315	0.306	0.297	0.289	0.280	32
33	0.366	0.356	0.347	0.338	0.330	0.321	0.312	0.304	0.295	0.287	0.278	0.270	33
34	0.353	0.344	0.335	0.327	0.318	0.310	0.301	0.293	0.285	0.276	0.268	0.260	34
35	0.341	0.332	0.324	0.315	0.307	0.298	0.290	0.282	0.274	0.266	0.258	0.250	35
36	0.328	0.320	0.312	0.303	0.295	0.287	0.279	0.271	0.263	0.256	0.248	0.240	36
37	0.316	0.308	0.300	0.292	0.284	0.276	0.268	0.260	0.253	0.245	0.237	0.230	37
38	0.304	0.296	0.288	0.280	0.272	0.265	0.257	0.250	0.242	0.235	0.227	0.220	38
39	0.291	0.284	0.276	0.269	0.261	0.254	0.246	0.239	0.231	0.224	0.217	0.210	39
40	0.279	0.272	0.264	0.257	0.250	0.242	0.235	0.228	0.221	0.214	0.207	0.199	40
41	0.267	0.260	0.252	0.245	0.238	0.231	0.224	0.217	0.210	0.203	0.196	0.188	41
42	0.255	0.247	0.240	0.233	0.227	0.220	0.213	0.206	0.199	0.192	0.186	0.178	42
43	0.242	0.235	0.228	0.222	0.215	0.208	0.202	0.195	0.188	0.182	0.175	0.168	43
44	0.230	0.223	0.216	0.210	0.203	0.197	0.190	0.184	0.177	0.171	0.164	0.158	44
45	0.217	0.211	0.204	0.198	0.192	0.185	0.179	0.173	0.166	0.160	0.154	0.147	45
46	0.205	0.198	0.192	0.186	0.180	0.174	0.167	0.161	0.155	0.149	0.143	0.136	46
47	0.192	0.186	0.180	0.174	0.168	0.162	0.156	0.150	0.144	0.138	0.132	0.126	47
48	0.179	0.173	0.168	0.162	0.156	0.150	0.144	0.138	0.132	0.127	0.121	0.115	48
49	0.167	0.161	0.155	0.149	0.144	0.138	0.132	0.126	0.121	0.115	0.109	0.104	49
50	0.154	0.148	0.142	0.137	0.131	0.126	0.120	0.115	0.109	0.104	0.098	0.093	50
51	0.140	0.135	0.130	0.124	0.119	0.113	0.108	0.103	0.097	0.092	0.086	0.081	51
52	0.127	0.122	0.117	0.111	0.106	0.101	0.096	0.090	0.085	0.080	0.075	0.069	52
53	0.114	0.108	0.103	0.098	0.093	0.088	0.083	0.078	0.073	0.068	0.063	0.058	53
54	0.100	0.095	0.090	0.085	0.080	0.075	0.070	0.065	0.060	0.055	0.051	0.046	54
55	0.086	0.081	0.076	0.072	0.067	0.062	0.057	0.052	0.048	0.043	0.038	0.033	55
56	0.072	0.067	0.063	0.058	0.053	0.049	0.044	0.039	0.035	0.030	0.025	0.021	56
57	0.057	0.053	0.048	0.044	0.039	0.035	0.030	0.026	0.021	0.017	0.012	0.008	57
58	0.043	0.038	0.034	0.030	0.025	0.021	0.017	0.013	0.008	0.003	0.999	0.995	58
59	0.028	0.023	0.019	0.015	0.011	0.007	0.002	0.998	0.994	0.990	0.985	0.981	59
60	0.012	0.008	0.004	0.000	0.996	0.992	0.988	0.984	0.980	0.976	0.971	0.967	60
61	0.996	0.992	0.989	0.985	0.981	0.977	0.973	0.969	0.965	0.961	0.957	0.953	61
62	0.980	0.976	0.973	0.969	0.965	0.961	0.957	0.954	0.950	0.946	0.942	0.938	62

LOGARITHMS
FOR COMPUTING THE REDUCTION TO THE MERIDIAN, AT SEA.
PART II. Latitude and Declination of contrary Names.

Lat.	DECLINATION.												Lat.
	24°	25°	26°	27°	28°	29°	30°	31°	32°	33°	34°	35°	
0°	0.652	0.632	0.613	0.594	0.575	0.557	0.539	0.522	0.505	0.489	0.472	0.456	0°
1	0.636	0.617	0.598	0.579	0.561	0.544	0.526	0.510	0.493	0.477	0.461	0.445	1
2	0.620	0.601	0.583	0.565	0.548	0.531	0.514	0.498	0.482	0.466	0.450	0.435	2
3	0.605	0.587	0.569	0.551	0.535	0.518	0.502	0.486	0.470	0.455	0.439	0.424	3
4	0.589	0.572	0.555	0.538	0.522	0.506	0.490	0.474	0.459	0.444	0.429	0.414	4
5	0.574	0.558	0.541	0.525	0.509	0.494	0.478	0.463	0.448	0.433	0.419	0.404	5
6	0.560	0.544	0.528	0.512	0.497	0.482	0.467	0.452	0.437	0.423	0.409	0.395	6
7	0.546	0.531	0.515	0.500	0.485	0.470	0.456	0.441	0.427	0.413	0.399	0.385	7
8	0.533	0.518	0.503	0.488	0.473	0.459	0.445	0.431	0.417	0.404	0.390	0.376	8
9	0.520	0.506	0.491	0.476	0.462	0.448	0.434	0.421	0.407	0.394	0.380	0.367	9
10	0.507	0.493	0.479	0.465	0.451	0.437	0.424	0.411	0.397	0.384	0.371	0.358	10
11	0.495	0.481	0.467	0.453	0.440	0.426	0.413	0.401	0.387	0.375	0.362	0.349	11
12	0.483	0.469	0.455	0.442	0.429	0.416	0.403	0.391	0.378	0.366	0.353	0.341	12
13	0.471	0.457	0.444	0.431	0.418	0.406	0.393	0.381	0.368	0.356	0.344	0.332	13
14	0.459	0.446	0.433	0.421	0.408	0.396	0.384	0.372	0.359	0.347	0.335	0.323	14
15	0.448	0.435	0.422	0.410	0.398	0.386	0.374	0.362	0.349	0.338	0.326	0.315	15
16	0.436	0.424	0.412	0.400	0.388	0.376	0.364	0.353	0.341	0.330	0.318	0.307	16
17	0.425	0.413	0.402	0.390	0.378	0.366	0.355	0.344	0.332	0.321	0.309	0.298	17
18	0.414	0.403	0.391	0.380	0.368	0.357	0.346	0.335	0.323	0.312	0.301	0.290	18
19	0.404	0.392	0.381	0.370	0.358	0.347	0.336	0.326	0.314	0.303	0.292	0.282	19
20	0.393	0.382	0.371	0.360	0.349	0.338	0.327	0.317	0.306	0.295	0.284	0.274	20
21	0.383	0.371	0.361	0.350	0.339	0.329	0.318	0.308	0.297	0.286	0.276	0.266	21
22	0.372	0.361	0.351	0.340	0.330	0.320	0.309	0.299	0.288	0.278	0.268	0.258	22
23	0.362	0.351	0.341	0.330	0.320	0.310	0.300	0.289	0.279	0.270	0.260	0.250	23
24	0.351	0.341	0.331	0.321	0.311	0.301	0.291	0.281	0.271	0.262	0.252	0.242	24
25	0.341	0.331	0.321	0.311	0.301	0.292	0.282	0.272	0.262	0.253	0.243	0.234	25
26	0.331	0.322	0.312	0.302	0.292	0.283	0.273	0.264	0.254	0.245	0.235	0.226	26
27	0.321	0.312	0.302	0.292	0.283	0.274	0.264	0.256	0.246	0.237	0.227	0.218	27
28	0.311	0.302	0.292	0.283	0.274	0.265	0.256	0.248	0.238	0.229	0.219	0.210	28
29	0.301	0.292	0.282	0.274	0.265	0.256	0.247	0.239	0.229	0.221	0.211	0.202	29
30	0.291	0.282	0.273	0.265	0.256	0.247	0.238	0.230	0.221	0.213	0.204	0.195	30
31	0.281	0.272	0.263	0.255	0.246	0.238	0.229	0.221	0.212	0.204	0.196	0.187	31
32	0.271	0.263	0.254	0.246	0.237	0.229	0.221	0.213	0.204	0.196	0.187	0.179	32
33	0.261	0.253	0.245	0.237	0.228	0.220	0.212	0.204	0.195	0.187	0.179	0.171	33
34	0.252	0.244	0.236	0.228	0.220	0.212	0.203	0.195	0.187	0.179	0.171	0.163	34
35	0.242	0.234	0.226	0.218	0.210	0.203	0.194	0.186	0.178	0.170	0.162	0.155	35
36	0.232	0.225	0.217	0.209	0.201	0.194	0.186	0.178	0.170	0.162	0.154	0.147	36
37	0.222	0.215	0.207	0.199	0.191	0.184	0.176	0.169	0.161	0.153	0.145	0.138	37
38	0.212	0.205	0.197	0.190	0.182	0.175	0.167	0.160	0.152	0.145	0.137	0.130	38
39	0.202	0.195	0.187	0.180	0.173	0.166	0.158	0.152	0.143	0.136	0.129	0.122	39
40	0.192	0.185	0.178	0.171	0.164	0.157	0.150	0.143	0.135	0.128	0.121	0.114	40
41	0.182	0.175	0.168	0.162	0.155	0.148	0.141	0.134	0.127	0.120	0.113	0.106	41
42	0.172	0.165	0.158	0.152	0.145	0.138	0.131	0.125	0.118	0.111	0.104	0.097	42
43	0.161	0.155	0.148	0.142	0.135	0.129	0.122	0.116	0.109	0.102	0.095	0.088	43
44	0.151	0.144	0.138	0.132	0.126	0.119	0.113	0.106	0.100	0.093	0.086	0.079	44
45	0.141	0.134	0.128	0.122	0.116	0.110	0.103	0.097	0.090	0.084	0.077	0.071	45
46	0.131	0.124	0.118	0.112	0.106	0.100	0.094	0.087	0.081	0.074	0.068	0.062	46
47	0.120	0.114	0.108	0.102	0.096	0.090	0.084	0.078	0.071	0.065	0.058	0.053	47
48	0.109	0.103	0.098	0.092	0.086	0.080	0.074	0.068	0.062	0.056	0.049	0.043	48
49	0.098	0.092	0.087	0.082	0.075	0.070	0.064	0.058	0.052	0.046	0.040	0.034	49
50	0.087	0.081	0.076	0.071	0.064	0.059	0.054	0.048	0.042	0.036	0.030	0.024	50
51	0.076	0.070	0.064	0.060	0.054	0.049	0.043	0.037	0.032	0.026	0.020	0.014	51
52	0.064	0.059	0.053	0.048	0.043	0.038	0.032	0.027	0.021	0.016	0.010	0.004	52
53	0.052	0.048	0.042	0.037	0.031	0.027	0.021	0.016	0.010	0.005	0.000	9.994	53
54	0.040	0.036	0.031	0.026	0.020	0.015	0.010	0.005	9.999	9.994	9.989	9.984	54
55	0.028	0.024	0.019	0.014	0.009	0.003	9.998	9.994	9.988	9.983	9.978	9.973	55
56	0.016	0.011	0.006	0.002	9.997	9.992	9.987	9.982	9.977	9.972	9.967	9.962	56
57	0.003	9.999	9.994	9.990	9.985	9.980	9.975	9.970	9.965	9.961	9.955	9.951	57
58	9.990	9.986	9.981	9.977	9.973	9.968	9.963	9.958	9.953	9.949	9.944	9.939	58
59	9.977	9.973	9.968	9.964	9.960	9.956	9.950	9.946	9.941	9.937	9.932	9.927	59
60	9.963	9.959	9.955	9.951	9.946	9.943	9.937	9.933	9.928	9.924	9.920	9.915	60
61	9.948	9.945	9.941	9.937	9.932	9.929	9.924	9.920	9.915	9.911	9.907	9.902	61
62	9.934	9.930	9.926	9.923	9.918	9.914	9.910	9.906	9.902	9.898	9.894	9.889	62

LOGARITHMS FOR COMPUTING THE CORRECTION OF THE LATITUDE BY ACCOUNT.

PART I. Observations on the *same* side
both of the Meridian and of the Prime Vertical.

AZIMUTHS.													
	8°	10°	12°	14°	16°	18°	20°	22°	24°	26°	28°	30°	32°
12°	9°206												
14	9°316												
16	9°384	9°163											
18	9°430	9°238	9°035										
20	9°464	9°290	9°116	8°925									
22	9°490	9°329	9°172	9°010	8°829								
24	9°511	9°359	9°215	9°071	8°918	8°744							
26	9°528	9°383	9°248	9°116	8°981	8°836							
28	9°543	9°403	9°275	9°152	9°029	8°902	8°762						
30	9°555	9°419	9°297	9°182	9°068	8°953	8°831	8°695					
32	9°565	9°435	9°316	9°206	9°100	8°993	8°884	8°766					
34	9°575	9°446	9°332	9°227	9°126	9°027	8°926	8°821	8°707				
36	9°583	9°457	9°346	9°245	9°148	9°055	8°961	8°865	8°763	8°653			
38	9°590	9°467	9°359	9°260	9°168	9°079	8°991	8°901	8°809	8°711			
40	9°596	9°475	9°370	9°274	9°185	9°099	9°016	8°932	8°847	8°758	8°662		
42	9°602	9°483	9°379	9°286	9°200	9°118	9°038	8°959	8°879	8°797	8°710	8°617	
44	9°608	9°490	9°389	9°297	9°214	9°134	9°057	8°982	8°907	8°830	8°751	8°667	8°576
46	9°613	9°497	9°397	9°308	9°226	9°149	9°075	9°003	8°931	8°859	8°785	8°708	8°626
48	9°617	9°503	9°404	9°317	9°237	9°162	9°090	9°021	8°953	8°885	8°815	8°744	8°668
50	9°622	9°508	9°411	9°325	9°247	9°174	9°105	9°038	8°972	8°907	8°842	8°775	8°705
52	9°626	9°513	9°418	9°333	9°256	9°185	9°118	9°053	8°990	8°927	8°865	8°802	8°737
54	9°629	9°518	9°424	9°340	9°265	9°195	9°129	9°067	9°006	8°946	8°886	8°826	8°765
56	9°633	9°523	9°429	9°347	9°273	9°205	9°141	9°079	9°020	8°962	8°905	8°848	8°790
58	9°636	9°527	9°435	9°354	9°281	9°214	9°151	9°091	9°034	8°978	8°923	8°868	8°813
60	9°639	9°531	9°440	9°360	9°288	9°222	9°160	9°102	9°046	8°992	8°939	8°886	8°834
62	9°642	9°535	9°444	9°365	9°295	9°230	9°169	9°112	9°058	9°005	8°954	8°903	8°853
64	9°645	9°539	9°449	9°371	9°301	9°237	9°178	9°122	9°069	9°018	8°968	8°919	8°870
66	9°648	9°542	9°453	9°376	9°307	9°244	9°186	9°131	9°079	9°029	8°981	8°933	8°887
68	9°651	9°545	9°457	9°381	9°313	9°251	9°194	9°140	9°089	9°040	8°993	8°947	8°902
70	9°653	9°549	9°461	9°386	9°319	9°258	9°201	9°148	9°099	9°051	9°005	8°960	8°916
72	9°656	9°552	9°465	9°390	9°324	9°264	9°208	9°156	9°107	9°061	9°016	8°972	8°930
74	9°658	9°555	9°469	9°395	9°329	9°270	9°215	9°164	9°116	9°070	9°026	8°984	8°942
76	9°661	9°558	9°473	9°399	9°334	9°275	9°222	9°171	9°124	9°079	9°036	8°995	8°955
78	9°663	9°561	9°476	9°403	9°339	9°281	9°228	9°178	9°132	9°088	9°046	8°906	8°966
80	9°665	9°564	9°480	9°408	9°344	9°287	9°234	9°185	9°140	9°097	9°055	9°016	8°977
82	9°667	9°567	9°483	9°412	9°349	9°292	9°240	9°192	9°147	9°105	9°065	9°026	8°988
84	9°670	9°569	9°487	9°416	9°353	9°297	9°246	9°199	9°155	9°113	9°073	9°035	8°999
86	9°672	9°572	9°490	9°420	9°358	9°302	9°252	9°205	9°162	9°121	9°082	9°045	9°009
88	9°674	9°575	9°493	9°423	9°362	9°307	9°257	9°211	9°169	9°128	9°090	9°054	9°019
90	9°676	9°578	9°496	9°427	9°366	9°312	9°263	9°218	9°175	9°136	9°098	9°062	9°028
	36°	38°	40°	42°	44°	46°	48°	50°	52°	54°	56°	58°	60°
54°	8°637	8°567	8°492	8°408	8°314								
56	8°670	8°606	8°538	8°464	8°381	8°288							
58	8°700	8°640	8°577	8°510	8°437	8°356	8°264						
60	8°726	8°671	8°612	8°551	8°485	8°413	8°333	8°242					
62	8°750	8°698	8°643	8°587	8°526	8°461	8°391	8°312	8°221				
64	8°773	8°723	8°671	8°618	8°563	8°503	8°440	8°370	8°292				
66	8°793	8°745	8°697	8°647	8°595	8°540	8°482	8°419	8°350	8°273			
68	8°812	8°766	8°720	8°673	8°624	8°573	8°520	8°462	8°401	8°332	8°256		
70	8°829	8°786	8°742	8°697	8°651	8°603	8°553	8°501	8°444	8°383	8°316	8°240	
72	8°846	8°804	8°762	8°719	8°676	8°631	8°584	8°535	8°483	8°428	8°367	8°301	8°226
74	8°861	8°821	8°781	8°740	8°698	8°656	8°612	8°566	8°518	8°467	8°412	8°353	8°287
76	8°876	8°837	8°798	8°759	8°719	8°679	8°638	8°595	8°550	8°503	8°453	8°398	8°346
78	8°890	8°852	8°815	8°777	8°739	8°701	8°661	8°621	8°579	8°535	8°489	8°439	8°386
80	8°903	8°867	8°831	8°794	8°758	8°721	8°684	8°645	8°606	8°564	8°521	8°476	8°427
82	8°916	8°881	8°846	8°811	8°776	8°740	8°705	8°668	8°631	8°591	8°551	8°509	8°464
84	8°928	8°894	8°860	8°826	8°793	8°759	8°724	8°690	8°654	8°617	8°579	8°540	8°498
86	8°940	8°907	8°874	8°841	8°809	8°776	8°743	8°710	8°676	8°641	8°605	8°568	8°529
88	8°951	8°919	8°887	8°856	8°824	8°793	8°761	8°729	8°697	8°664	8°630	8°595	8°558
90	8°963	8°931	8°900	8°869	8°839	8°809	8°778	8°748	8°717	8°685	8°653	8°620	8°585

**LOGARITHMS
FOR COMPUTING THE CORRECTION OF THE LATITUDE BY ACCOUNT.**

**PART II. Observations on *different* sides
either of the Meridian or of the Prime Vertical.**

AZIMUTHS.													
	8°	10°	12°	14°	16°	18°	20°	22°	24°	26°	28°	30°	32°
8°	9°777												
10	9°911	9°879											
12	9°897	9°840	9°797										
14	9°870	9°810	9°764	9°728									
16	9°849	9°786	9°737	9°699	9°667								
18	9°832	9°766	9°715	9°674	9°641	9°613							
20	9°818	9°749	9°696	9°654	9°619	9°589	9°564						
22	9°806	9°735	9°680	9°636	9°599	9°568	9°542	9°519					
24	9°795	9°722	9°666	9°620	9°582	9°550	9°522	9°498	9°476				
26	9°786	9°712	9°654	9°606	9°567	9°534	9°505	9°480	9°457	9°437			
28	9°778	9°702	9°643	9°594	9°554	9°519	9°489	9°463	9°440	9°418	9°399		
30	9°771	9°693	9°633	9°583	9°542	9°506	9°475	9°448	9°424	9°402	9°382	9°364	
32	9°764	9°686	9°624	9°573	9°530	9°494	9°462	9°434	9°409	9°386	9°366	9°347	9°329
34	9°758	9°678	9°616	9°564	9°520	9°483	9°450	9°421	9°395	9°372	9°351	9°331	9°313
36	9°753	9°672	9°608	9°555	9°511	9°473	9°439	9°410	9°383	9°359	9°337	9°316	9°298
38	9°748	9°666	9°601	9°547	9°502	9°463	9°429	9°399	9°371	9°346	9°324	9°303	9°283
40	9°743	9°660	9°594	9°540	9°494	9°454	9°419	9°388	9°360	9°335	9°311	9°290	9°270
42	9°739	9°655	9°588	9°533	9°486	9°446	9°410	9°378	9°350	9°324	9°300	9°278	9°257
44	9°735	9°650	9°583	9°527	9°479	9°438	9°402	9°369	9°340	9°313	9°287	9°266	9°245
46	9°731	9°646	9°578	9°521	9°473	9°431	9°394	9°361	9°331	9°303	9°277	9°255	9°233
48	9°728	9°642	9°573	9°515	9°466	9°424	9°386	9°352	9°322	9°294	9°268	9°244	9°221
50	9°725	9°638	9°568	9°510	9°460	9°417	9°379	9°344	9°313	9°285	9°258	9°234	9°211
52	9°721	9°634	9°563	9°504	9°454	9°410	9°372	9°337	9°305	9°276	9°249	9°224	9°201
54	9°718	9°630	9°559	9°499	9°449	9°404	9°365	9°329	9°297	9°267	9°240	9°215	9°191
56	9°715	9°626	9°555	9°495	9°443	9°398	9°358	9°322	9°289	9°259	9°231	9°205	9°181
58	9°713	9°623	9°551	9°490	9°438	9°392	9°352	9°315	9°282	9°251	9°223	9°196	9°171
60	9°710	9°620	9°547	9°486	9°433	9°387	9°346	9°309	9°275	9°243	9°215	9°187	9°162
62	9°707	9°617	9°543	9°481	9°428	9°381	9°340	9°302	9°268	9°236	9°206	9°179	9°153
64	9°705	9°613	9°539	9°477	9°423	9°376	9°334	9°296	9°261	9°228	9°198	9°170	9°144
66	9°702	9°610	9°536	9°473	9°419	9°371	9°328	9°289	9°254	9°221	9°191	9°162	9°135
68	9°700	9°607	9°532	9°469	9°414	9°366	9°322	9°283	9°247	9°214	9°183	9°154	9°126
70	9°698	9°605	9°529	9°465	9°410	9°361	9°317	9°277	9°241	9°207	9°175	9°145	9°117
72	9°695	9°602	9°525	9°461	9°405	9°356	9°311	9°271	9°234	9°200	9°167	9°137	9°108
74	9°693	9°599	9°522	9°457	9°401	9°351	9°306	9°265	9°228	9°193	9°160	9°129	9°100
76	9°691	9°596	9°519	9°453	9°396	9°346	9°301	9°259	9°221	9°186	9°152	9°121	9°091
78	9°689	9°594	9°516	9°450	9°392	9°341	9°295	9°253	9°215	9°179	9°145	9°113	9°082
80	9°687	9°591	9°512	9°446	9°388	9°336	9°290	9°247	9°208	9°172	9°137	9°105	9°074
82	9°685	9°588	9°509	9°442	9°384	9°332	9°285	9°241	9°202	9°165	9°130	9°096	9°065
84	9°682	9°586	9°506	9°438	9°379	9°327	9°279	9°236	9°195	9°157	9°122	9°088	9°056
86	9°680	9°583	9°503	9°435	9°375	9°322	9°274	9°230	9°189	9°150	9°114	9°080	9°047
88	9°678	9°580	9°500	9°431	9°371	9°317	9°268	9°224	9°182	9°143	9°106	9°071	9°037
90	9°676	9°578	9°496	9°427	9°366	9°312	9°263	9°218	9°175	9°135	9°098	9°062	9°028
	36°	38°	40°	42°	44°	46°	48°	50°	52°	54°	56°	58°	60°
36	9°264												
38	9°248	9°232											
40	9°234	9°217	9°201										
42	9°220	9°202	9°186	9°171									
44	9°206	9°189	9°172	9°156	9°140								
46	9°193	9°175	9°158	9°141	9°125	9°110							
48	9°181	9°162	9°145	9°127	9°111	9°095	9°079						
50	9°169	9°150	9°132	9°114	9°097	9°080	9°064	9°049					
52	9°158	9°138	9°119	9°101	9°083	9°066	9°050	9°034	9°018				
54	9°147	9°126	9°107	9°088	9°070	9°052	9°035	9°019	9°002	8°986			
56	9°136	9°115	9°095	9°076	9°057	9°039	9°021	9°004	8°987	8°970	8°954		
58	9°125	9°104	9°083	9°063	9°044	9°025	9°007	8°989	8°972	8°955	8°938	8°921	
60	9°115	9°093	9°072	9°051	9°032	9°012	8°994	8°975	8°957	8°939	8°921	8°904	8°886
62	9°105	9°083	9°060	9°039	9°019	8°999	8°980	8°961	8°942	8°924	8°905	8°887	8°869
64	9°094	9°071	9°049	9°028	9°007	8°986	8°966	8°947	8°927	8°908	8°889	8°870	8°851
66	9°084	9°061	9°038	9°016	8°994	8°973	8°953	8°933	8°913	8°893	8°873	8°853	8°834
68	9°074	9°050	9°027	9°004	8°982	8°960	8°939	8°918	8°898	8°877	8°857	8°836	8°815

LOGARITHMS
FOR COMPUTING THE CORRECTION OF THE LATITUDE BY ACCOUNT
PART II. (continued.) Observations on *different* sides
either of the Meridian or of the Prime Vertical.

AZIMUTHS.

	36°	38°	40°	42°	44°	46°	48°	50°	52°	54°	56°	58°	60°	62°
70°	9°065	9°040	9°016	8°993	8°970	8°948	8°926	8°904	8°883	8°862	8°843	8°819	8°798	8°776
72	9°055	9°029	9°005	8°981	8°958	8°935	8°912	8°890	8°868	8°846	8°824	8°802	8°779	8°757
74	9°045	9°019	8°994	8°969	8°945	8°922	8°898	8°875	8°853	8°830	8°807	8°784	8°760	8°737
76	9°035	9°008	8°983	8°957	8°933	8°909	8°885	8°861	8°837	8°813	8°790	8°766	8°741	8°717
78	9°025	8°998	8°971	8°946	8°920	8°895	8°870	8°846	8°821	8°797	8°772	8°747	8°721	8°696
80	9°015	8°987	8°960	8°933	8°907	8°882	8°856	8°831	8°805	8°780	8°754	8°728	8°701	8°674
82	9°005	8°976	8°948	8°921	8°894	8°868	8°841	8°815	8°789	8°762	8°735	8°708	8°680	8°651
84	8°995	8°965	8°937	8°909	8°881	8°854	8°826	8°799	8°772	8°744	8°716	8°687	8°658	8°628
86	8°984	8°954	8°925	8°896	8°867	8°839	8°811	8°782	8°754	8°725	8°696	8°666	8°635	8°603
88	8°974	8°943	8°913	8°883	8°853	8°824	8°795	8°765	8°736	8°706	8°675	8°643	8°611	8°577
90	8°963	8°931	8°900	8°869	8°839	8°809	8°778	8°748	8°717	8°685	8°653	8°620	8°585	8°550

TABLE 72

LOGARITHMS
FOR COMPUTING THE EQUATION OF EQUAL ALTITUDES

Interval.	L g. A.	Log. B.	Interval.	Log. A.	Log. B.	Interval.	Log. A.	Log. B.
1° 30"	2°2725	2°2809	4° 30"	2°2499	2°3300	7° 30"	2°2032	2°4584
1 35	2°2722	2°2816	4 35	2°2489	2°3323	7 35	2°2015	2°4645
1 40	2°2719	2°2823	4 40	2°2479	2°3346	7 40	2°1998	2°4696
1 45	2°2715	2°2831	4 45	2°2469	2°3370	7 45	2°1980	2°4755
1 50	2°2711	2°2838	4 50	2°2459	2°3394	7 50	2°1963	2°4814
1 55	2°2707	2°2846	4 55	2°2449	2°3418	7 55	2°1945	2°4876
2 0	2°2703	2°2854	5 0	2°2438	2°3444	8 0	2°1928	2°4938
2 5	2°2699	2°2863	5 5	2°2428	2°3470	8 5	2°1910	2°5004
2 10	2°2695	2°2872	5 10	2°2417	2°3495	8 10	2°1892	2°5070
2 15	2°2690	2°2882	5 15	2°2406	2°3524	8 15	2°1874	2°5141
2 20	2°2685	2°2891	5 20	2°2394	2°3552	8 20	2°1855	2°5211
2 25	2°2680	2°2902	5 25	2°2383	2°3581	8 25	2°1836	2°5286
2 30	2°2675	2°2912	5 30	2°2371	2°3610	8 30	2°1817	2°5360
2 35	2°2669	2°2924	5 35	2°2359	2°3641	8 35	2°1798	2°5439
2 40	2°2664	2°2935	5 40	2°2347	2°3671	8 40	2°1778	2°5518
2 45	2°2658	2°2947	5 45	2°2334	2°3703	8 45	2°1758	2°5602
2 50	2°2652	2°2950	5 50	2°2322	2°3735	8 50	2°1738	2°5685
2 55	2°2646	2°2972	5 55	2°2309	2°3768	8 55	2°1718	2°5776
3 0	2°2641	2°2985	6 0	2°2297	2°3802	9 0	2°1697	2°5868
3 5	2°2634	2°2998	6 5	2°2283	2°3837	9 5	2°1677	2°5963
3 10	2°2628	2°3012	6 10	2°2271	2°3873	9 10	2°1656	2°6 63
3 15	2°2621	2°3027	6 15	2°2257	2°39 0	9 15	2°1635	2°6164
3 20	2°2614	2°3042	6 20	2°2244	2°3947	9 20	2°1613	2°6273
3 25	2°2607	2°3058	6 25	2°2230	2°3986	9 25	2°1592	2°6384
3 30	2°2600	2°3073	6 30	2°2216	2°4024	9 30	2°1570	2°6499
3 35	2°2592	2°3090	6 35	2°2202	2°4065	9 35	2°15 7	2°6619
3 40	2°2585	2°3106	6 40	2°2187	2°4106	9 40	2°1525	2°6744
3 45	2°2577	2°3124	6 45	2°2173	2°4149	9 45	2°1502	2°6874
3 50	2°2569	2°3141	6 50	2°2158	2°41 2	9 50	2°1480	2°7011
3 55	2°2561	2°3159	6 55	2°2143	2°4157	9 55	2°1457	2°7154
4 0	2°2553	2°3177	7 0	2°2127	2°4233	10 0	2°1433	2°7303
4 5	2°2544	2°3196	7 5	2°2112	2°4330	10 5	2°1409	2°7460
4 10	2°2536	2°3216	7 10	2°2096	2°4378	10 10	2°1386	2°7626
4 15	2°2527	2°3236	7 15	2°2080	2°4426	10 15	2°1361	2°7801
4 20	2°2518	2°3257	7 20	2°2064	2°4478	10 20	2°1337	2°7984
4 25	2°2509	2°3278	7 25	2°2048	2°4531	10 25	2°1312	2°8076

THE LOGARITHMIC DIFFERENCE
(Barometer, 30 inches. Fahrenheit's Thermometer, 80°.)

App. Alt.	Horizontal Parallax.										' of Par.	Corr. for ' of Par.						Cor. for ' of Alt.
	53	54	55	56	57	58	59	60	61	0'		1'	2'	3'	4'	5'	6'	
3 0	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	0	0	0	0	1	2	2	sub.
10	9841	9833	9825	9817	9809	9800	9792	9784	9776	9768	10	2	2	2	3	3	3	
20	9822	9814	9806	9797	9789	9780	9771	9763	9754	9746	20	3	3	3	4	4	4	
30	9804	9795	9786	9777	9769	9760	9751	9742	9732	9723	30	5	5	5	6	6	6	
40	9785	9776	9767	9758	9748	9739	9730	9720	9711	9701	40	6	7	7	8	8	8	
50	9767	9757	9747	9738	9728	9718	9709	9699	9689	9679	50	8	8	9	9	10	11	
4 0	9748	9738	9728	9718	9708	9698	9687	9677	9667	9656	0	0	0	0	1	2	2	11 1- 53
10	9729	9718	9708	9698	9687	9677	9666	9656	9645	9634	10	2	2	2	3	4	4	
20	9710	9699	9689	9678	9667	9656	9645	9634	9623	9613	20	4	4	4	5	6	6	
30	9691	9680	9669	9658	9646	9635	9624	9613	9601	9591	30	6	6	6	7	7	8	
40	9672	9660	9649	9637	9626	9614	9603	9591	9579	9569	40	8	8	9	9	10	10	
50	9653	9641	9629	9617	9605	9593	9581	9569	9557	9547	50	10	10	11	11	12	12	
5 0	9634	9622	9609	9597	9585	9572	9560	9547	9535	9523	0	0	0	1	1	2	2	2 4 6
10	9614	9602	9589	9576	9563	9551	9538	9525	9512	9500	10	2	3	3	3	4	4	
20	9595	9582	9569	9556	9543	9530	9516	9503	9490	9478	20	4	5	5	6	6	7	
30	9576	9562	9549	9535	9522	9509	9495	9481	9468	9454	30	7	7	8	8	9	9	
40	9557	9543	9529	9515	9501	9487	9474	9460	9446	9432	40	9	10	10	11	11	12	
50	9538	9523	9509	9495	9481	9466	9452	9438	9424	9409	50	12	13	13	14	14	15	
6 0	9518	9504	9489	9474	9460	9445	9431	9416	9401	9387	0	0	0	1	1	2	3	11.P 61'
10	9499	9484	9469	9454	9439	9424	9409	9394	9379	9364	10	3	3	4	4	5	5	
20	9480	9465	9449	9434	9418	9403	9388	9372	9357	9342	20	5	6	6	7	7	8	
30	9461	9445	9429	9413	9398	9382	9366	9350	9334	9319	30	8	8	9	10	10	11	
40	9441	9425	9409	9393	9377	9361	9345	9329	9312	9297	40	11	11	12	13	13	14	
50	9422	9406	9389	9373	9356	9340	9323	9307	9290	9274	50	14	15	15	16	16	17	
7 0	9403	9386	9369	9352	9335	9319	9301	9285	9268	9251	0	0	1	1	2	2	3	11.P 61'
10	9383	9366	9349	9332	9314	9297	9280	9263	9246	9229	10	3	3	4	5	5	6	
20	9364	9347	9329	9311	9294	9276	9258	9241	9223	9206	20	6	7	7	8	8	9	
30	9345	9327	9309	9291	9273	9255	9237	9219	9201	9183	30	9	10	10	11	12	12	
40	9326	9307	9289	9271	9252	9234	9216	9197	9179	9161	40	12	13	14	14	15	16	
50	9306	9288	9269	9250	9232	9213	9194	9175	9157	9138	50	16	16	17	18	18	19	
8 0	9287	9268	9249	9230	9211	9192	9173	9154	9134	9115	0	0	1	1	2	3	3	11.P 61'
10	9268	9248	9229	9209	9190	9170	9151	9132	9112	9093	10	3	4	5	5	6	7	
20	9249	9229	9209	9189	9169	9149	9130	9110	9090	9070	20	7	7	8	9	9	10	
30	9229	9209	9189	9169	9149	9128	9108	9088	9068	9048	30	10	11	12	12	13	14	
40	9210	9189	9169	9148	9128	9107	9087	9066	9046	9025	40	14	15	15	16	17	18	
50	9191	9170	9149	9128	9107	9086	9065	9044	9023	9002	50	18	19	19	20	21	21	
9 0	9172	9150	9129	9108	9086	9065	9044	9022	9001	8980	0	0	1	1	2	3	4	11.P 61'
10	9152	9131	9109	9087	9066	9044	9022	9001	8979	8957	10	4	4	5	6	6	7	
20	9133	9111	9089	9067	9045	9023	9001	8979	8957	8935	20	7	8	9	10	10	11	
30	9114	9091	9069	9047	9024	9002	8979	8957	8935	8912	30	11	12	13	14	14	15	
40	9095	9072	9049	9026	9004	8981	8958	8935	8912	8890	40	15	16	17	18	18	20	
50	9075	9052	9029	9006	8983	8960	8937	8913	8890	8868	50	20	20	21	22	23	23	

Sun's Alt. 5° 6° 7° 8° 14° 25° 34° 42° 51° 64° 90° | Star's Alt. 5° 6° 7° 8° 9° 11° 12° 14° 18° 30°
 Sub 17 13 11 9 7 9 11 13 15 17 18 | Sub. 15 11 9 7 5 4 3 2 1 0

The Logarithmic Difference is not given in this Table for altitudes less than 3°, because the lunar observation ought not to be employed with very low altitudes.

THE LOGARITHMIC DIFFERENCE
(Barometer, 30 inches. Fahrenheit's Thermometer, 50°.)

App. Alt.	Horizontal Parallax.										" of Par.	Corr. for " of Par. sub.						Corr. for " of Alt.
	53'	54'	55'	56'	57'	58'	59'	60'	61'	0'		2'	4'	6'	8'	10'		
10 0	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	0	0	1	2	3	4	sub.	
10 10	9037	9013	8989	8965	8941	8917	8894	8870	8846	10	4	5	6	7	8			
20 0	9018	8993	8969	8945	8921	8896	8872	8848	8824	20	8	9	10	11	12			
30 0	8998	8974	8949	8925	8900	8875	8851	8826	8802	30	12	13	14	15	16			
40 0	8979	8954	8929	8904	8879	8854	8830	8805	8780	40	17	18	19	20	21			
50 0	8960	8935	8909	8884	8859	8833	8808	8783	8758	50	21	22	23	24	25			
11 0	8941	8915	8889	8864	8838	8812	8787	8761	8735	0	0	1	2	3	4	H.P. 53'		
10 0	8922	8895	8869	8843	8817	8791	8765	8739	8713	10	4	5	6	7	8			
20 0	8903	8876	8850	8823	8797	8771	8744	8718	8691	20	9	10	11	12	13			
30 0	8883	8857	8830	8803	8776	8750	8723	8696	8669	30	13	14	15	16	17			
40 0	8864	8837	8810	8783	8756	8729	8702	8675	8647	40	18	19	20	21	22			
50 0	8845	8818	8790	8763	8735	8708	8680	8653	8625	50	23	24	25	26	27			
12 0	8826	8799	8771	8743	8715	8687	8659	8631	8604	0	0	1	2	3	4	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17		
10 0	8807	8779	8751	8723	8694	8666	8638	8610	8582	10	5	6	7	8	9			
20 0	8788	8760	8731	8703	8674	8645	8617	8588	8560	20	10	11	12	13	14			
30 0	8769	8740	8711	8682	8653	8624	8595	8566	8538	30	15	16	17	18	19			
40 0	8750	8721	8691	8662	8633	8603	8574	8545	8516	40	20	21	22	23	24			
50 0	8731	8701	8672	8642	8612	8582	8553	8523	8494	50	25	26	27	28	29			
13 0	8712	8682	8652	8622	8592	8562	8532	8502	8472	0	0	1	2	3	4	7 8 9 10 11 12 13 14 15 16 17		
10 0	8693	8662	8632	8601	8571	8541	8510	8480	8450	10	5	6	7	8	9			
20 0	8674	8643	8612	8581	8551	8520	8489	8458	8428	20	10	11	12	13	14			
30 0	8655	8624	8592	8561	8530	8499	8468	8437	8406	30	16	17	18	19	20			
40 0	8636	8604	8573	8541	8510	8478	8447	8416	8384	40	21	22	23	24	25			
50 0	8617	8585	8553	8521	8490	8458	8426	8394	8362	50	27	28	29	30	31			
14 0	8598	8566	8533	8501	8469	8437	8405	8373	8340	0	0	1	2	3	4	5 6 7 8 9 10 11 12 13 14 15 16 17		
10 0	8579	8546	8514	8481	8449	8416	8384	8351	8318	10	5	7	8	9	10			
20 0	8560	8527	8494	8461	8428	8395	8363	8330	8297	20	11	12	13	14	15			
30 0	8541	8508	8474	8441	8408	8375	8341	8308	8275	30	17	18	19	20	21			
40 0	8522	8489	8455	8421	8388	8354	8320	8287	8253	40	23	24	25	26	27			
50 0	8503	8469	8435	8401	8367	8333	8299	8266	8232	50	28	30	31	32	33			
15 0	8484	8450	8416	8381	8347	8313	8278	8244	8210	0	0	1	2	3	4	6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34		
10 0	8465	8431	8396	8361	8327	8292	8257	8223	8188	10	6	7	8	9	10			
20 0	8447	8412	8377	8342	8307	8271	8236	8201	8166	20	12	13	14	15	16			
30 0	8428	8392	8357	8322	8286	8251	8215	8180	8145	30	18	19	20	21	22			
40 0	8409	8373	8338	8302	8266	8230	8195	8159	8123	40	24	25	26	27	28			
50 0	8390	8354	8318	8282	8246	8210	8174	8138	8101	50	30	31	32	33	34			
16 0	8371	8335	8299	8262	8226	8189	8153	8116	8080	0	0	1	2	3	4	5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36		
10 0	8353	8316	8279	8242	8205	8169	8132	8095	8058	10	6	7	8	9	10			
20 0	8334	8297	8260	8222	8185	8148	8111	8074	8037	20	12	13	14	15	16			
30 0	8315	8278	8240	8203	8165	8128	8090	8053	8015	30	19	20	21	22	23			
40 0	8297	8259	8221	8183	8145	8107	8069	8031	7994	40	25	27	28	29	30			
50 0	8278	8240	8201	8163	8125	8087	8048	8010	7972	50	32	33	34	35	36			
17 0	8259	8221	8182	8143	8105	8066	8028	7989	7950	0	0	1	3	4	5	H.P. 61'		
10 0	8240	8201	8162	8124	8085	8046	8007	7968	7929	10	7	8	9	10	11			
20 0	8222	8183	8143	8104	8065	8025	7986	7947	7907	20	13	14	15	16	17			
30 0	8203	8164	8124	8084	8045	8005	7965	7926	7886	30	20	21	22	23	24			
40 0	8185	8145	8105	8065	8025	7985	7945	7905	7865	40	27	28	30	31	32			
50 0	8166	8126	8085	8045	8005	7964	7924	7884	7843	50	34	35	37	38	39			
18 0	8147	8107	8066	8025	7985	7944	7903	7863	7822	0	0	1	3	4	5	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40		
10 0	8129	8088	8047	8006	7965	7924	7882	7841	7800	10	7	8	10	11	12			
20 0	8110	8069	8027	7986	7945	7903	7862	7820	7779	20	14	15	17	18	19			
30 0	8092	8050	8008	7967	7925	7883	7841	7800	7758	30	21	22	24	25	27			
40 0	8073	8031	7989	7947	7905	7863	7821	7779	7736	40	28	30	31	32	34			
50 0	8055	8012	7970	7927	7885	7842	7800	7758	7715	50	36	37	39	40	41			
19 0	8036	7993	7950	7908	7865	7822	7779	7737	7694	0	0	1	3	4	6	7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44		
10 0	8018	7974	7931	7888	7845	7802	7759	7715	7672	10	7	9	10	12	13			
20 0	7999	7956	7912	7869	7825	7782	7738	7695	7651	20	15	16	17	19	20			
30 0	7981	7937	7893	7849	7805	7762	7718	7674	7630	30	22	24	25	27	28			
40 0	7962	7918	7874	7830	7786	7741	7697	7653	7609	40	30	31	33	34	36			
50 0	7944	7899	7855	7810	7766	7721	7677	7632	7588	50	37	39	40	42	43			
20 0	7926	7881	7836	7791	7746	7701	7656	7611	7567	0	0	1	3	4	6	7		

Sun's Alt. 5° 6° 7° 8° 14° 25° 34° 42° 51° 64° 90° | Star's Alt. 5° 6° 7° 8° 9° 10° 12° 14° 18° 30°
sub. 17 13 11 9 7 9 11 13 15 17 18 | sub. 15 11 9 7 5 4 3 2 1 0

THE LOGARITHMIC DIFFERENCE
(Barometer, 30 inches. Fahrenheit's Thermometer, 80°)

App. Alt.	Horizontal Parallax.										" of		Corr. for " of Par. sub						Corr. for Alt.
	53'	54'	55'	56'	57'	58'	59'	60'	61'	62'	Par.	0'	1'	2'	3'	4'	5'	6'	
20 0	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	0	0	1	3	4	6	8		
10	7907	7862	7817	7772	7726	7681	7636	7591	7545	7500	10	8	9	11	12	14	15		
20	7889	7843	7798	7752	7707	7661	7615	7570	7524	7478	20	15	17	18	20	21	23		
30	7871	7825	7779	7733	7687	7641	7595	7549	7503	7457	30	23	25	26	28	29	34		
40	7852	7806	7760	7714	7667	7621	7575	7529	7482	7436	40	31	33	34	36	37	39		
50	7834	7788	7741	7694	7648	7601	7554	7508	7461	7414	50	39	41	42	44	45	46		
60	7816	7769	7722	7674	7628	7581	7534	7487	7440	7393									
21 0	7798	7750	7703	7656	7608	7561	7514	7466	7419	7372	0	0	2	3	5	6	8		
10	7779	7732	7684	7636	7589	7541	7493	7446	7398	7350	10	8	9	11	12	14	16		H.P.
20	7761	7713	7665	7617	7569	7521	7473	7425	7377	7329	20	16	18	19	21	22	24		53'
30	7743	7695	7646	7598	7550	7501	7453	7405	7356	7308	30	24	26	27	29	30	32		
40	7725	7676	7628	7579	7530	7481	7433	7384	7336	7287	40	32	34	36	37	39	41		
50	7707	7658	7609	7560	7511	7462	7413	7364	7315	7266	50	41	42	44	46	47	48		
22 0	7689	7639	7590	7540	7491	7442	7392	7343	7294	7245	0	0	2	3	5	7	8		
10	7671	7621	7571	7521	7472	7422	7372	7323	7273	7224	10	8	10	12	13	15	17		
20	7653	7602	7552	7502	7452	7402	7352	7302	7252	7202	20	17	18	20	22	23	25		
30	7635	7584	7534	7483	7433	7383	7332	7282	7232	7182	30	25	27	28	30	32	34		
40	7617	7566	7515	7464	7414	7363	7312	7261	7211	7160	40	34	35	37	39	40	42		
50	7598	7547	7496	7445	7394	7343	7292	7241	7190	7139	50	42	44	45	48	49	50		
23 0	7581	7529	7478	7426	7375	7323	7272	7221	7169	7118	0	0	2	3	5	7	9		
10	7563	7511	7459	7407	7356	7304	7252	7200	7149	7097	10	9	10	12	14	15	17		
20	7545	7493	7441	7389	7336	7284	7232	7180	7128	7076	20	17	19	21	23	24	26		
30	7527	7474	7422	7370	7317	7265	7212	7160	7107	7055	30	26	28	30	31	33	35		
40	7509	7456	7403	7351	7298	7245	7192	7140	7087	7034	40	35	37	39	40	42	44		
50	7491	7438	7385	7332	7279	7226	7173	7119	7066	7013	50	44	46	48	50	51	53		
24 0	7473	7420	7366	7313	7259	7206	7153	7099	7046	6993	0	0	2	4	5	7	9		
10	7455	7402	7348	7294	7240	7187	7133	7079	7025	6971	10	9	11	13	14	16	18		
20	7438	7384	7330	7275	7221	7167	7113	7059	7005	6951	20	18	20	22	23	25	27		
30	7420	7365	7311	7257	7202	7148	7093	7039	6984	6930	30	27	29	31	33	34	36		
40	7402	7347	7293	7238	7183	7128	7074	7019	6964	6909	40	36	38	40	42	44	46		
50	7384	7329	7274	7219	7164	7109	7054	6999	6944	6889	50	46	48	49	51	53	55		
25 0	7367	7311	7256	7200	7145	7090	7034	6979	6923	6868	0	0	2	4	5	7	9		
10	7349	7293	7238	7182	7126	7070	7014	6959	6903	6848	10	9	11	13	15	17	19		
20	7331	7275	7219	7163	7107	7051	6995	6939	6883	6827	20	19	20	22	24	26	28		
30	7314	7258	7201	7145	7088	7032	6975	6919	6862	6806	30	28	30	32	34	36	38		
40	7296	7240	7183	7126	7069	7012	6956	6899	6842	6786	40	38	40	42	44	45	48		
50	7279	7222	7165	7107	7050	6993	6936	6879	6822	6765	50	48	49	51	53	55	57		
26 0	7261	7204	7146	7089	7031	6974	6916	6859	6802	6745	0	0	2	4	6	8	9		
10	7244	7186	7128	7070	7013	6955	6897	6839	6781	6724	10	9	12	14	15	17	19		
20	7226	7168	7110	7052	6994	6936	6878	6820	6762	6704	20	19	21	23	25	27	29		
30	7209	7150	7092	7034	6975	6917	6858	6800	6741	6683	30	29	31	33	35	37	39		
40	7191	7133	7074	7015	6956	6898	6839	6780	6721	6663	40	39	41	43	45	47	49		
50	7174	7115	7056	6997	6938	6878	6819	6760	6701	6642	50	49	51	53	55	57	59		
27 0	7156	7097	7038	6978	6919	6859	6800	6740	6681	6621	0	0	2	4	6	8	10		
10	7139	7079	7020	6960	6900	6840	6781	6721	6661	6601	10	10	12	14	16	18	20		
20	7122	7062	7002	6942	6882	6822	6761	6701	6641	6581	20	20	22	24	26	28	30		
30	7105	7044	6984	6923	6863	6803	6742	6682	6621	6561	30	30	32	34	36	38	40		
40	7087	7027	6966	6905	6844	6784	6723	6662	6602	6541	40	40	42	44	46	48	50		
50	7070	7009	6948	6887	6826	6765	6704	6643	6582	6521	50	51	53	55	57	59	61		
28 0	7051	6991	6930	6869	6807	6746	6684	6623	6562	6501	0	0	2	4	6	8	10		
10	7036	6974	6912	6851	6789	6727	6665	6604	6542	6481	10	10	12	14	16	18	21		
20	7018	6956	6894	6832	6770	6708	6646	6584	6522	6461	20	21	23	25	27	29	31		
30	7001	6939	6877	6814	6752	6690	6627	6565	6503	6441	30	31	33	35	37	39	42		
40	6984	6922	6859	6796	6734	6671	6608	6545	6483	6421	40	42	44	46	48	50	53		
50	6967	6904	6841	6778	6715	6651	6589	6526	6463	6401	50	52	55	57	59	61	63		
29 0	6950	6887	6823	6760	6697	6633	6570	6507	6443	6380	0	0	2	4	6	8	11		
10	6933	6869	6806	6742	6678	6615	6551	6488	6424	6361	10	11	13	15	17	19	21		
20	6916	6852	6788	6724	6660	6596	6532	6469	6405	6341	20	21	23	25	28	30	32		
30	6899	6835	6771	6706	6642	6578	6514	6449	6385	6321	30	32	34	36	39	41	43		
40	6882	6818	6753	6688	6624	6559	6495	6430	6366	6301	40	43	45	47	49	52	54		
50	6865	6800	6735	6671	6606	6541	6476	6411	6346	6281	50	54	56	58	60	63	65		

Sun's Alt. 5° 6° 7° 8° 14° 23° 34° 42° 51° 61° 80°

Star's Alt. 5° 6° 7° 8° 9° 11° 12° 14° 16° 30°

sub. 17 13 11 9 7 9 11 13 15 17 18

sub. 15 11 9 7 5 4 3 2 1 0

THE LOGARITHMIC DIFFERENCE
(Barometer, 30 inches. Fahrenheit's Thermometer, 60°.)

App. Alt.	Horizontal Parallax.										// of Par.	Corr. for // of Par. sub.						Corr. of Alt.			
	53'	54'	55'	56'	57'	58'	59'	60'	61'	0'		1'	2'	3'	4'	5'	6'		7'	8'	9'
30 0	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	0	0	2	4	6	9	11	H.P. 53'	1 2 3 4 5 6 7 8 9 10 11 12 13 14		
10	6848	6781	6718	6653	6588	6522	6457	6392	6327	10	11	13	15	17	20	22	24				
20	6831	6766	6700	6635	6569	6504	6439	6373	6308	20	22	24	26	29	31	33	35				
30	6815	6749	6683	6617	6551	6485	6420	6354	6288	30	33	35	37	40	42	44	46				
40	6798	6732	6665	6599	6533	6467	6401	6335	6269	40	44	46	49	51	53	56	58				
50	6781	6714	6648	6581	6515	6449	6382	6316	6249	50	56	58	60	62	64	66	68				
31 0	6764	6697	6630	6564	6497	6430	6363	6296	6230	0	0	2	4	7	9	11	H.P. 54'	1 2 3 4 5 6 7 8 9 10 11 12 13 14			
10	6747	6680	6613	6546	6479	6412	6344	6277	6210	10	11	13	16	18	20	23			25		
20	6731	6663	6596	6528	6461	6393	6326	6258	6191	20	23	25	27	29	32	34			36		
30	6714	6646	6579	6511	6443	6375	6307	6240	6172	30	34	36	38	41	43	46			48		
40	6697	6629	6561	6493	6425	6357	6289	6221	6153	40	46	48	50	52	55	57			59		
50	6681	6612	6544	6476	6407	6339	6270	6202	6134	50	57	59	62	64	66	68			71		
32 0	6664	6596	6527	6458	6389	6321	6252	6183	6115	0	0	2	5	7	9	11	H.P. 55'	1 2 3 4 5 6 7 8 9 10 11 12 13 14			
10	6648	6579	6510	6441	6372	6303	6234	6165	6096	10	11	14	16	18	21	23			25		
20	6631	6562	6493	6423	6354	6285	6215	6146	6077	20	23	25	28	30	32	35			37		
30	6615	6545	6475	6406	6336	6267	6197	6127	6058	30	35	37	40	42	44	47			49		
40	6598	6528	6458	6388	6318	6249	6179	6109	6039	40	47	49	52	54	56	59			61		
50	6582	6512	6441	6371	6301	6231	6160	6090	6020	50	59	61	63	66	68	71			73		
33 0	6565	6495	6424	6354	6283	6213	6142	6071	6001	0	0	2	5	7	9	12	H.P. 56'	1 2 3 4 5 6 7 8 9 10 11 12 13 14			
10	6549	6478	6407	6336	6265	6195	6124	6053	5982	10	12	14	17	19	21	24			26		
20	6533	6461	6390	6319	6248	6177	6106	6034	5963	20	24	26	29	31	33	36			38		
30	6516	6445	6373	6302	6230	6159	6087	6016	5944	30	36	38	41	43	45	48			50		
40	6500	6428	6356	6285	6213	6141	6069	5998	5926	40	48	50	53	55	58	60			62		
50	6484	6412	6340	6268	6195	6123	6051	5979	5907	50	60	63	65	68	70	72			74		
34 0	6468	6395	6323	6250	6178	6105	6033	5961	5888	0	0	2	5	7	9	12	H.P. 57'	1 2 3 4 5 6 7 8 9 10 11 12 13 14			
10	6451	6379	6306	6233	6160	6088	6015	5942	5869	10	12	15	17	19	22	24			26		
20	6435	6362	6289	6216	6143	6070	5997	5924	5851	20	24	27	29	32	34	37			39		
30	6419	6346	6273	6199	6126	6053	5979	5906	5833	30	37	39	42	44	47	49			51		
40	6403	6330	6256	6182	6109	6035	5961	5888	5814	40	49	52	54	57	59	62			64		
50	6387	6313	6239	6165	6091	6017	5943	5870	5796	50	62	64	67	69	72	74			76		
35 0	6371	6297	6223	6148	6074	6000	5926	5851	5777	0	0	2	5	7	10	12	H.P. 58'	1 2 3 4 5 6 7 8 9 10 11 12 13 14			
10	6355	6280	6206	6131	6057	5982	5908	5833	5759	10	12	15	17	20	22	25			27		
20	6339	6264	6189	6115	6040	5965	5890	5815	5740	20	25	27	30	32	35	38			40		
30	6323	6248	6173	6098	6023	5948	5872	5797	5722	30	38	40	43	45	48	50			52		
40	6307	6232	6156	6081	6006	5930	5855	5779	5704	40	50	53	55	58	61	63			65		
50	6292	6216	6140	6064	5989	5913	5837	5761	5686	50	63	66	68	71	74	76			78		
36 0	6276	6200	6124	6048	5971	5895	5819	5743	5667	0	0	2	5	8	10	13	H.P. 59'	1 2 3 4 5 6 7 8 9 10 11 12 13 14			
10	6260	6183	6107	6031	5954	5878	5802	5725	5649	10	13	16	18	20	23	26			28		
20	6244	6167	6091	6014	5938	5861	5784	5708	5631	20	26	28	31	33	36	39			41		
30	6228	6152	6075	5998	5921	5844	5767	5690	5613	30	39	41	44	46	49	52			54		
40	6213	6136	6058	5981	5904	5827	5749	5672	5595	40	52	54	57	59	62	65			67		
50	6197	6120	6042	5964	5887	5809	5732	5654	5577	50	65	67	70	73	75	78			80		
37 0	6181	6104	6026	5948	5870	5792	5714	5637	5559	0	0	3	5	8	10	13	H.P. 60'	1 2 3 4 5 6 7 8 9 10 11 12 13 14			
10	6166	6088	6009	5931	5853	5775	5697	5619	5541	10	13	16	18	21	23	26			28		
20	6150	6072	5993	5915	5837	5758	5680	5601	5523	20	26	29	31	34	37	39			41		
30	6135	6056	5977	5899	5820	5741	5662	5584	5505	30	39	42	45	47	50	53			55		
40	6119	6040	5961	5882	5803	5724	5645	5566	5487	40	53	56	58	61	63	66			68		
50	6104	6024	5945	5866	5787	5707	5628	5549	5469	50	66	69	72	74	77	79			81		
38 0	6088	6009	5929	5850	5770	5690	5611	5531	5452	0	0	3	5	8	11	13	H.P. 61'	1 2 3 4 5 6 7 8 9 10 11 12 13 14			
10	6073	5993	5913	5833	5753	5673	5594	5514	5434	10	13	16	19	21	24	27			29		
20	6058	5977	5897	5817	5737	5657	5577	5496	5416	20	27	29	32	35	37	40			42		
30	6042	5962	5881	5801	5721	5640	5560	5479	5399	30	40	43	46	48	51	54			56		
40	6027	5946	5866	5785	5704	5623	5543	5462	5381	40	54	57	59	62	65	68			70		
50	6012	5931	5850	5769	5688	5607	5526	5445	5364	50	68	70	73	76	79	81			83		
39 0	5997	5915	5834	5753	5671	5590	5509	5427	5346	0	0	3	5	8	11	14	H.P. 62'	1 2 3 4 5 6 7 8 9 10 11 12 13 14			
10	5981	5900	5818	5736	5655	5573	5492	5410	5328	10	14	16	19	22	25	27			29		
20	5966	5884	5802	5721	5639	5557	5475	5393	5311	20	27	30	33	36	38	41			43		
30	5951	5869	5787	5705	5622	5540	5458	5376	5294	30	41	44	47	49	52	55			57		
40	5936	5854	5771	5689	5606	5524	5441	5359	5277	40	55	58	61	63	66	69			71		
50	5921	5838	5756	5673	5590	5507	5425	5342	5259	50	69	72	75	77	80	82			84		
60	5906	5823	5740	5657	5574	5491	5408	5325	5242												
Sun's Alt. 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10° 11° 12° 13° 14° 15° 16° 17° 18° 19° 20°											Star's Alt. 0° 1° 2° 3° 4° 5° 6° 7° 8° 9° 10° 11° 12° 13° 14° 15° 16° 17° 18° 19° 20°										
sub. 17 13 11 9 7 5 4 3 2 1 0											sub. 15 11 9 7 5 4 3 2 1 0										

sun's Alt. 8° 6° 7° 8° 14° 26° 34° 42° 51° 64° 90° Star's Alt. 5° 6° 7° 8° 9° 11° 12° 14° 18° 30°
sub. 17 13 11 9 7 9 11 13 15 17 18 sub. 15 11 9 7 5 4 3 2 1 0

THE LOGARITHMIC DIFFERENCE
(Barometer, 30 inches. Fahrenheit's Thermometer, 50°.)

App. Alt.	Horizontal Parall.x.									" of Par.	Corr. for " of Par. sub.						Corr. for Alt.		
	53'	54'	55'	56'	57'	58'	59'	60'	61'		0"	2"	4"	6"	8"	10"			
40 0	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	0	0	3	6	8	11	14	sub.		
10	5891	5808	5724	5641	5558	5474	5391	5308	5225	10	14	17	19	22	25	28			
20	5876	5793	5709	5625	5542	5458	5375	5291	5207	20	28	31	34	36	39	42	H.P.		
30	5861	5777	5694	5610	5526	5442	5358	5274	5190	30	42	45	48	50	53	56	83'		
40	5847	5762	5678	5594	5510	5426	5342	5257	5173	40	56	59	62	65	68	71			
50	5832	5747	5663	5578	5494	5410	5325	5241	5156	50	71	73	76	79	82	84			
60	5817	5732	5647	5563	5478	5393	5309	5224	5139	60	84	86	88	90	92	94			
41 0	5802	5717	5632	5547	5462	5377	5292	5207	5122	0	0	3	6	8	11	14	1		
10	5787	5702	5617	5532	5446	5361	5276	5191	5105	10	14	17	20	23	26	28	3		
20	5773	5687	5602	5516	5431	5345	5260	5174	5089	20	28	31	34	37	40	43	4		
30	5758	5672	5587	5501	5415	5329	5243	5158	5072	30	43	46	49	51	54	57	5		
40	5744	5658	5571	5485	5399	5313	5227	5141	5055	40	57	60	63	66	69	72	6		
50	5729	5643	5556	5470	5384	5297	5211	5124	5038	50	72	75	78	81	83	86	7		
42 0	5714	5628	5541	5455	5368	5281	5195	5108	5021	0	0	3	6	9	11	14	10		
10	5700	5613	5526	5439	5352	5266	5179	5092	5005	10	14	17	20	23	26	29	11		
20	5686	5599	5511	5424	5337	5250	5163	5075	4988	20	29	32	35	38	41	44	13		
30	5671	5584	5496	5409	5322	5234	5147	5059	4972	30	44	47	49	52	55	58			
40	5657	5569	5482	5394	5306	5218	5131	5043	4955	40	58	61	64	67	70	73			
50	5643	5555	5467	5379	5291	5203	5115	5027	4939	50	73	76	79	82	85	87			
43 0	5628	5540	5452	5363	5275	5187	5099	5010	4922	0	0	3	6	9	12	15			
10	5614	5526	5437	5349	5260	5171	5083	4994	4906	10	15	18	21	24	26	30			
20	5600	5511	5422	5334	5245	5156	5067	4978	4890	20	30	32	35	38	41	45			
30	5586	5497	5408	5319	5230	5141	5051	4962	4873	30	45	47	50	53	56	60			
40	5572	5482	5393	5304	5214	5125	5036	4946	4857	40	60	63	65	68	71	75			
50	5558	5468	5378	5289	5199	5110	5020	4930	4841	50	75	78	81	84	87	89			
44 0	5544	5454	5364	5274	5184	5094	5004	4914	4825	0	0	3	6	9	12	15			
10	5530	5439	5349	5259	5169	5079	4989	4899	4809	10	15	18	21	24	27	30			
20	5516	5425	5335	5245	5154	5064	4973	4883	4793	20	30	33	36	39	42	45			
30	5502	5411	5320	5230	5139	5048	4957	4867	4777	30	45	48	51	54	57	61			
40	5488	5397	5306	5215	5124	5033	4942	4851	4760	40	61	64	67	70	73	76			
50	5474	5383	5292	5200	5109	5018	4927	4836	4744	50	76	79	82	85	88	90			
45 0	5460	5369	5277	5186	5094	5003	4911	4820	4728	0	0	3	6	9	12	15			
10	5446	5355	5263	5171	5080	4988	4896	4804	4713	10	15	18	21	24	27	31			
20	5433	5341	5249	5157	5065	4973	4881	4789	4697	20	31	34	37	40	43	46			
30	5419	5327	5235	5142	5050	4958	4866	4774	4681	30	46	49	52	55	58	62			
40	5405	5313	5220	5128	5035	4943	4851	4758	4666	40	62	65	68	71	74	77			
50	5392	5299	5206	5113	5021	4928	4835	4743	4650	50	77	80	83	87	90	92			
46 0	5378	5285	5192	5099	5006	4913	4820	4727	4634	0	0	3	6	9	12	15			
10	5365	5271	5178	5085	4992	4898	4805	4712	4619	10	15	19	22	25	28	31			
20	5351	5258	5164	5071	4977	4884	4790	4697	4603	20	31	34	37	40	44	47			
30	5338	5244	5150	5057	4963	4869	4775	4682	4588	30	47	50	53	56	59	63	H.P.		
40	5324	5230	5136	5042	4948	4854	4760	4666	4572	40	63	66	69	72	75	78	61		
50	5311	5217	5123	5028	4934	4840	4745	4651	4557	50	78	82	85	88	91	94			
47 0	5298	5203	5109	5014	4920	4825	4731	4636	4542	0	0	3	6	9	13	16	1		
10	5284	5190	5095	5000	4906	4811	4716	4621	4527	10	16	19	22	25	28	31	2		
20	5271	5176	5081	4986	4891	4796	4701	4606	4511	20	32	35	38	41	44	48	3		
30	5258	5163	5068	4972	4877	4782	4687	4592	4496	30	48	51	54	56	60	64	4		
40	5245	5149	5054	4959	4863	4768	4672	4577	4481	40	64	66	70	73	76	80	5		
50	5232	5136	5040	4945	4849	4753	4658	4562	4466	50	80	83	86	89	93	96	6		
48 0	5218	5123	5027	4931	4835	4739	4643	4547	4451	0	0	3	6	10	13	16	11		
10	5206	5109	5013	4917	4821	4725	4629	4533	4436	10	16	19	22	26	29	32	13		
20	5193	5096	5000	4903	4807	4711	4614	4518	4421	20	32	35	39	42	45	48	14		
30	5180	5083	4986	4890	4793	4696	4600	4503	4406	30	48	52	55	58	61	65			
40	5167	5070	4973	4876	4779	4682	4585	4488	4391	40	65	67	71	74	78	81			
50	5154	5057	4960	4862	4765	4668	4571	4474	4376	50	81	84	87	90	94	97			
49 0	5141	5044	4946	4849	4751	4654	4556	4459	4361	0	0	3	6	10	13	16			
10	5128	5031	4933	4835	4738	4640	4542	4444	4347	10	16	19	23	26	29	33			
20	5116	5018	4920	4822	4724	4626	4528	4430	4332	20	33	36	39	42	46	49			
30	5103	5005	4907	4809	4710	4612	4514	4416	4318	30	49	52	56	59	62	66			
40	5091	4992	4894	4795	4697	4598	4500	4402	4303	40	66	69	72	75	79	82			
50	5078	4979	4881	4782	4683	4585	4486	4387	4289	50	82	85	89	92	95	98			
Sum's Alt. 5° 6' 7' 8' 14' 25' 34' 42' 51' 64' 90'										Star's Alt. 5° 6' 7' 8' 9' 11' 12' 14' 15' 30'									
sub. 17 13 11 9 7 9 11 13 15 17 18										sub. 15 11 9 7 5 4 3 2 1 0									

TABLE 73

903

THE LOGARITHMIC DIFFERENCE
(Barometer, 30 inches. Fahrenheit's Thermometer, 50°.)

App. Alt.	Horizontal Parallax.										// of Par.	Corr. for // of Par. sub.						Cor. for // of Alt.
	53'	54'	55'	56'	57'	58'	59'	60'	61'	0'		2'	4'	6'	8'	10'		
50° 0	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	4274	0	0	3	7	10	13	16	
10	5053	4954	4855	4755	4656	4557	4458	4359	4260	10	16	20	23	26	30	33	36	sub.
20	5040	4941	4842	4742	4643	4544	4444	4345	4246	20	33	36	40	43	46	50	53	H.P.
30	5028	4928	4829	4729	4630	4530	4430	4331	4231	30	50	53	56	60	64	67	70	53'
40	5016	4916	4816	4716	4616	4516	4417	4317	4217	40	67	70	73	77	80	83	86	
50	5003	4903	4803	4703	4603	4503	4403	4303	4203	50	83	87	90	93	97	100		
51° 0	4991	4891	4790	4690	4590	4489	4389	4289	4188	0	0	3	7	10	13	17	20	1
10	4979	4878	4778	4677	4577	4476	4376	4275	4174	10	17	20	23	26	30	34	37	2
20	4967	4866	4765	4664	4564	4463	4362	4261	4160	20	34	37	40	43	47	50	54	3
30	4954	4853	4752	4651	4550	4449	4348	4247	4146	30	50	54	57	60	64	67	71	4
40	4942	4841	4740	4639	4537	4436	4335	4234	4133	40	67	71	74	78	81	84	88	5
50	4930	4829	4727	4626	4524	4423	4321	4220	4119	50	84	88	91	95	98	101		6
52° 0	4918	4816	4715	4613	4511	4410	4308	4206	4105	0	0	3	7	10	14	17	20	7
10	4906	4804	4702	4600	4499	4397	4295	4193	4091	10	17	20	24	27	31	34	37	8
20	4894	4792	4690	4588	4486	4384	4281	4179	4077	20	34	37	41	44	48	51	54	9
30	4882	4780	4678	4575	4473	4371	4268	4166	4064	30	51	54	58	61	65	68	71	
40	4871	4768	4665	4563	4460	4358	4255	4153	4050	40	68	72	75	79	82	86		
50	4859	4756	4653	4550	4448	4345	4242	4139	4036	50	86	89	93	96	99	102		H.P.
53° 0	4847	4744	4641	4538	4435	4332	4229	4126	4023	0	0	3	7	10	14	17	20	61'
10	4835	4732	4629	4526	4422	4319	4216	4113	4009	10	17	21	24	27	31	34	37	1
20	4824	4720	4617	4513	4410	4306	4203	4099	3996	20	34	39	41	45	48	52	55	2
30	4812	4708	4605	4501	4397	4294	4190	4086	3983	30	52	55	59	62	66	69	72	3
40	4800	4697	4593	4489	4385	4281	4177	4073	3969	40	69	73	76	80	83	87	90	4
50	4789	4685	4581	4476	4372	4268	4164	4060	3956	50	87	90	94	97	101	104	107	5
54° 0	4777	4673	4568	4464	4360	4255	4151	4047	3942	0	0	3	7	10	14	17	20	6
10	4766	4661	4557	4452	4348	4243	4139	4034	3930	10	17	21	24	28	31	35	38	7
20	4755	4650	4545	4440	4336	4231	4126	4021	3917	20	35	39	42	45	49	52	55	8
30	4743	4638	4533	4428	4324	4219	4114	4009	3904	30	52	56	59	63	66	70	73	9
40	4732	4627	4522	4417	4311	4206	4101	3996	3891	40	70	74	77	81	84	88		
50	4721	4615	4510	4405	4299	4194	4089	3983	3878	50	88	91	95	98	102	105		
55° 0	4709	4604	4498	4393	4287	4182	4076	3971	3865	0	0	3	7	11	14	18	21	H.P.
10	4698	4593	4487	4381	4275	4170	4064	3958	3852	10	18	21	25	28	32	35	38	53'
20	4687	4581	4475	4369	4263	4157	4051	3946	3840	20	35	39	42	46	49	53		
30	4676	4570	4464	4358	4251	4145	4039	3933	3827	30	53	57	61	64	67	71		
40	4665	4559	4452	4346	4240	4133	4027	3920	3814	40	71	74	78	82	85	89		
50	4654	4548	4441	4334	4228	4121	4014	3908	3801	50	89	92	96	99	103	106		
56° 0	4643	4536	4429	4323	4216	4109	4002	3895	3788	0	0	4	7	11	14	18	21	1
10	4632	4525	4418	4311	4204	4097	3990	3883	3776	10	18	21	25	28	32	36	39	2
20	4622	4514	4407	4300	4192	4085	3978	3871	3763	20	36	39	43	46	50	54	57	3
30	4611	4503	4396	4288	4181	4073	3966	3858	3751	30	54	57	61	64	68	72	75	4
40	4600	4492	4385	4277	4169	4062	3954	3846	3739	40	72	75	79	82	86	90	93	5
50	4589	4481	4373	4266	4158	4050	3942	3834	3726	50	90	93	97	101	104	108		6
57° 0	4578	4470	4362	4254	4146	4038	3930	3822	3714	0	0	4	7	11	14	18	21	7
10	4568	4460	4351	4243	4135	4027	3918	3810	3702	10	18	22	25	29	32	36	39	8
20	4558	4449	4341	4232	4124	4015	3907	3798	3690	20	36	40	43	47	51	54		9
30	4547	4439	4330	4221	4112	4004	3895	3786	3678	30	54	58	61	65	69	73		
40	4537	4428	4319	4210	4101	3992	3883	3774	3666	40	73	76	80	83	87	91		
50	4526	4417	4308	4199	4090	3981	3872	3763	3654	50	91	94	98	102	105	109		H.P.
58° 0	4516	4407	4297	4188	4079	3969	3860	3751	3642	0	0	4	7	11	15	18	21	61'
10	4506	4396	4287	4177	4068	3958	3849	3739	3630	10	18	22	25	29	33	37		1
20	4496	4386	4276	4166	4057	3947	3837	3728	3618	20	37	41	44	48	51	55		2
30	4485	4375	4266	4156	4046	3936	3826	3716	3606	30	55	59	62	66	70	73		3
40	4475	4365	4255	4145	4035	3925	3815	3705	3595	40	73	77	81	84	88	92		4
50	4465	4355	4244	4134	4024	3914	3803	3693	3583	50	92	95	99	103	107	110		5
59° 0	4455	4344	4234	4123	4013	3903	3792	3682	3571	0	0	4	7	11	15	18	21	6
10	4445	4334	4224	4113	4002	3892	3781	3670	3560	10	18	22	26	29	33	37		7
20	4435	4324	4213	4102	3992	3881	3770	3659	3548	20	37	41	44	48	52	55		8
30	4425	4314	4203	4092	3981	3870	3759	3648	3537	30	55	59	63	67	70	74		9
40	4415	4304	4193	4082	3970	3859	3748	3637	3526	40	74	78	81	85	89	93		
50	4405	4294	4182	4071	3960	3848	3737	3626	3514	50	94	98	100	104	108	111		

Sun's Alt. 5° 6° 7° 8° 14° 25° 34° 42° 51° 64° 90°
sub. 17 13 11 9 7 9 11 13 15 17 18

Star's Alt. 5° 6° 7° 8° 9° 11° 12° 14° 18° 30°
sub. 15 11 9 7 5 4 3 2 1 0

THE LOGARITHMIC DIFFERENCE
(Barometer, 30 inches. Fahrenheit's Thermometer, 50°.)

App. Alt.	Horizontal Parallax.										" of Par.	Corr. for " of Par. sub.						Corr. for " of Alt.				
	53	54	55	56	57	58	59	60	61	0'		2'	4'	6'	8'	10'						
70	0	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	0	0	4	8	12	16	20	sub				
	10	3902	3781	3660	3539	3418	3298	3177	3056	2935	10	20	24	28	32	36	40					
	20	3895	3774	3653	3532	3411	3290	3169	3049	2928	20	40	44	48	52	56	61					
	30	3889	3768	3647	3526	3404	3283	3162	3041	2920	30	61	65	69	73	77	81					
	40	3882	3761	3640	3519	3398	3276	3155	3034	2913	40	81	85	89	93	97	101					
71	0	3876	3755	3633	3512	3391	3269	3148	3027	2905	50	101	105	109	113	117	121					
	10	3869	3748	3626	3505	3384	3262	3141	3019	2898	0	0	4	8	12	16	20					
	20	3863	3741	3620	3498	3377	3255	3133	3012	2890	10	20	24	28	32	37	41					
	30	3857	3735	3613	3492	3370	3248	3127	3005	2883	20	41	45	49	53	57	61					
	40	3851	3729	3607	3485	3363	3242	3120	2998	2876	30	61	65	69	73	77	81					
72	0	3844	3722	3601	3479	3357	3235	3113	2991	2869	40	81	85	89	93	98	102					
	10	3838	3716	3594	3472	3350	3228	3106	2984	2862	50	102	106	110	114	118	122					
	20	3832	3710	3588	3466	3343	3221	3099	2977	2855	0	0	4	8	12	16	20					
	30	3826	3704	3581	3459	3337	3214	3092	2970	2848	10	20	24	28	33	37	41					
	40	3820	3698	3575	3453	3330	3208	3085	2963	2841	20	41	45	49	53	57	61					
73	0	3814	3692	3569	3447	3324	3202	3079	2957	2834	30	61	65	69	74	78	82					
	10	3808	3686	3563	3440	3318	3195	3073	2950	2827	40	82	86	90	94	98	102					
	20	3803	3680	3557	3434	3312	3189	3066	2943	2821	50	102	106	111	115	119	123					
	30	3797	3674	3551	3428	3305	3182	3060	2937	2814	0	0	4	8	12	16	20					
	40	3791	3668	3545	3422	3299	3176	3053	2930	2807	10	20	25	29	33	37	41					
74	0	3785	3662	3539	3416	3293	3170	3047	2924	2801	20	41	45	49	53	57	62					
	10	3780	3657	3533	3410	3287	3164	3041	2918	2794	30	62	66	70	74	78	82					
	20	3774	3651	3528	3404	3281	3158	3035	2911	2788	40	82	86	90	95	98	103					
	30	3769	3645	3522	3398	3275	3152	3028	2905	2782	50	103	107	111	115	119	123					
	40	3763	3640	3516	3393	3269	3146	3022	2899	2775	0	0	4	8	12	16	21					
75	0	3757	3634	3510	3387	3263	3140	3016	2892	2769	10	21	25	29	33	37	41					
	10	3752	3629	3505	3381	3258	3134	3010	2887	2763	20	41	45	49	54	58	62					
	20	3747	3623	3500	3376	3252	3128	3004	2881	2757	30	62	66	70	74	78	83					
	30	3742	3618	3494	3370	3246	3123	2999	2875	2751	40	83	87	91	95	99	103					
	40	3737	3613	3489	3365	3241	3117	2993	2869	2745	50	103	107	112	116	120	124					
76	0	3731	3607	3483	3359	3235	3111	2987	2863	2739	0	0	4	8	12	17	21					
	10	3726	3602	3478	3354	3230	3105	2981	2857	2733	10	21	25	29	33	37	41					
	20	3721	3597	3473	3349	3224	3100	2976	2852	2727	20	41	46	50	54	58	62					
	30	3716	3592	3468	3343	3219	3095	2970	2846	2722	30	62	66	70	75	79	83					
	40	3712	3587	3463	3338	3214	3089	2965	2841	2716	40	83	87	91	95	100	104					
77	0	3707	3582	3458	3333	3209	3084	2960	2835	2710	50	104	108	112	116	120	124					
	10	3702	3577	3453	3328	3203	3079	2954	2829	2705	0	0	4	8	12	17	21					
	20	3697	3572	3448	3323	3198	3073	2949	2824	2699	10	21	25	29	33	37	42					
	30	3692	3568	3443	3318	3193	3068	2944	2819	2694	20	42	46	50	54	58	62					
	40	3688	3563	3438	3313	3188	3063	2939	2814	2689	30	62	67	71	75	79	83					
78	0	3683	3558	3433	3308	3183	3058	2933	2808	2684	40	83	88	92	96	100	104					
	10	3679	3554	3429	3304	3178	3053	2928	2803	2678	50	104	108	113	117	121	125					
	20	3674	3549	3424	3299	3174	3048	2923	2798	2673	0	0	4	8	12	17	21					
	30	3669	3544	3419	3294	3169	3043	2918	2793	2668	10	21	25	29	33	38	42					
	40	3665	3540	3415	3289	3164	3039	2914	2788	2663	20	42	46	50	54	58	63					
79	0	3661	3536	3410	3285	3160	3034	2909	2783	2658	30	63	67	71	75	79	84					
	10	3657	3531	3406	3281	3155	3030	2904	2779	2653	40	84	88	92	96	100	105					
	20	3653	3527	3402	3276	3151	3025	2899	2774	2648	50	105	109	113	117	121	126					
	30	3648	3523	3397	3272	3146	3020	2895	2769	2644	0	0	4	8	13	17	21					
	40	3644	3519	3393	3267	3141	3016	2890	2764	2639	10	21	25	29	34	38	42					
80	0	3640	3515	3389	3263	3137	3012	2886	2760	2634	20	42	46	50	55	59	63					
	10	3636	3511	3385	3259	3133	3007	2881	2756	2630	30	63	67	71	76	80	84					
	20	3633	3507	3381	3255	3129	3003	2877	2751	2625	40	84	88	92	97	101	105					
	30	3629	3503	3377	3251	3125	2999	2873	2747	2621	50	105	109	113	118	122	126					
	40	3625	3499	3373	3247	3121	2995	2868	2742	2616	0	0	4	8	13	17	21					
81	0	3621	3495	3369	3243	3116	2990	2864	2738	2612	10	21	25	29	34	38	42					
	10	3617	3491	3365	3239	3113	2986	2860	2734	2608	20	42	46	50	55	59	63					
	20	3614	3488	3361	3235	3109	2982	2856	2730	2604	30	63	67	71	76	80	84					
	30	3610	3484	3358	3231	3105	2979	2852	2726	2600	40	84	88	93	97	101	105					
	40	3607	3480	3354	3228	3102	2975	2848	2722	2596	50	105	110	114	118	122	126					
Sun's Alt.	5°	6°	7°	8°	14°	28°	34°	42°	51°	64°	90°	Star's Alt. 5° 6° 7° 8° 9° 11° 12° 14° 18° 30°										
	sub.	17	13	11	9	7	9	11	13	15	17	18	sub.	15	11	5	7	3	4	3	2	1

Sun's Alt. 5° 6° 7° 8° 14° 28° 34° 42° 51° 64° 90°
sub. 17 13 11 9 7 9 11 13 15 17 18

Star's Alt. 5° 6° 7° 8° 9° 11° 12° 14° 18° 30°
sub. 15 11 5 7 3 4 3 2 1 0

TABLE 73

THE LOGARITHMIC DIFFERENCE																					
(Barometer, 30 inches. Fahrenheit's Thermometer, 50°.)																					
App. Alt.	Horizontal Parallax.										" of Par.	Corr. for " of Par. sub.						Corr. for Alt.			
	53'	54'	55'	56'	57'	58'	59'	60'	61'	0'		2'	4'	6'	8'	10'					
80 0	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	9'99	0						sub.				
	3600	3473	3347	3220	3094	2967	2840	2714	2587	10											
	3596	3470	3343	3217	3090	2963	2837	2710	2584	20											
	3593	3467	3340	3213	3087	2960	2833	2707	2580	30											
	3590	3463	3337	3210	3083	2956	2830	2703	2576	40											
81 0	3587	3460	3333	3206	3080	2953	2826	2699	2573	50						H.P. 53					
	3584	3457	3330	3203	3076	2949	2823	2696	2569	0											
	3580	3453	3327	3200	3073	2946	2819	2692	2565	10											
	3577	3451	3324	3197	3070	2943	2816	2689	2562	20											
	3575	3448	3321	3194	3067	2940	2813	2686	2559	30											
82 0	3572	3445	3318	3191	3063	2936	2809	2682	2555	40						10					
	3569	3442	3315	3188	3060	2933	2806	2679	2552	50											
	3566	3439	3312	3184	3057	2930	2803	2676	2549	0											
	3563	3436	3309	3181	3054	2927	2800	2673	2545	10											
	3561	3433	3306	3179	3052	2924	2797	2670	2542	20	0	4	8	13	17		21				
83 0	3558	3431	3303	3177	3049	2921	2794	2667	2539	30	21	25	29	34	38	43	20				
	3555	3428	3301	3173	3046	2919	2791	2664	2537	40	42	46	51	55	59	63					
	3553	3425	3298	3171	3043	2916	2788	2661	2534	50	63	68	72	76	80	84					
	3550	3423	3295	3168	3041	2913	2786	2658	2531	0	84	89	93	97	101	106					
	3548	3420	3293	3166	3038	2911	2783	2656	2528	10	106	110	114	118	123	127					
84 0	3546	3418	3291	3164	3036	2909	2781	2654	2526	20						93					
	3543	3416	3289	3162	3034	2907	2779	2652	2524	30											
	3541	3414	3286	3159	3031	2904	2776	2649	2521	40											
	3539	3411	3284	3156	3029	2901	2773	2646	2518	50											
	3537	3409	3282	3154	3027	2899	2771	2643	2516	0											
85 0	3535	3407	3279	3151	3024	2896	2768	2640	2513	10						H.P. 68					
	3533	3405	3277	3149	3022	2894	2766	2638	2511	20											
	3531	3403	3275	3147	3020	2892	2764	2636	2508	30											
	3529	3401	3273	3145	3018	2890	2762	2634	2506	40											
	3527	3399	3271	3143	3016	2888	2760	2632	2504	50											
86 0	3525	3397	3269	3141	3014	2886	2758	2630	2502	0						20					
	3523	3396	3268	3140	3013	2884	2756	2628	2500	10											
	3522	3394	3266	3138	3010	2882	2754	2626	2498	20											
	3520	3392	3264	3136	3007	2880	2752	2624	2496	30											
	3518	3391	3263	3134	3006	2878	2750	2621	2494	40											
87 0	3517	3389	3261	3133	3005	2877	2749	2620	2493	50						H.P. 68					
	3516	3388	3259	3131	3003	2875	2747	2619	2491	0											
	3514	3386	3258	3130	3002	2874	2746	2617	2489	10											
	3513	3385	3257	3128	3000	2872	2744	2616	2487	20											
	3511	3383	3255	3127	2999	2871	2743	2614	2486	30											
88 0	3510	3382	3253	3126	2998	2869	2741	2613	2485	40						20					
	3509	3381	3252	3124	2996	2868	2740	2612	2483	50											
	3508	3380	3251	3123	2995	2867	2739	2610	2482	0											
	3507	3379	3250	3122	2994	2866	2738	2609	2481	10	0	4	9	13	17		21				
	3506	3378	3250	3121	2993	2865	2736	2608	2480	20	21	25	30	34	38		43				
89 0	3505	3377	3249	3120	2992	2864	2735	2607	2479	30	43	47	52	56	60	64	20				
	3504	3376	3248	3119	2991	2863	2734	2606	2478	40	64	68	73	77	81	85					
	3503	3375	3247	3118	2990	2862	2733	2605	2477	50	85	90	94	98	102	107					
	3502	3374	3246	3117	2989	2861	2733	2604	2476	0	107	111	115	119	124	128					
	3501	3374	3245	3117	2989	2860	2732	2603	2475	10											
90 0	3501	3373	3244	3116	2988	2860	2731	2602	2474	20						H.P. 68					
	3500	3372	3244	3115	2987	2859	2731	2602	2474	30											
	3500	3372	3244	3115	2987	2858	2730	2601	2473	40											
	3499	3371	3243	3115	2986	2858	2729	2601	2473	50											
	3499	3371	3243	3114	2986	2858	2729	2600	2472	0											
91 0	3499	3371	3242	3114	2985	2857	2729	2600	2472	10						H.P. 68					
	3499	3370	3242	3113	2985	2857	2728	2600	2471	20											
	3498	3370	3242	3113	2985	2856	2728	2600	2471	30											
	3498	3370	3241	3113	2985	2856	2728	2600	2471	40											
	3498	3370	3241	3113	2984	2856	2727	2599	2470	50											
Sun's Alt. 5° 6° 7° 8° 9° 10° 11° 12° 13° 14° 15° 16° 17° 18° 19° 20°											Star's Alt. 5° 6° 7° 8° 9° 10° 11° 12° 13° 14° 15° 16° 17° 18° 19° 20°										
sub. 17 13 11 9 7 9 11 13 15 17 18											sub. 15 11 9 7 5 4 3 2 1 0										

PROPORTIONAL LOGARITHMS

ARC "	0° 0'	0° 1'	0° 2'	0° 3'	0° 4'	0° 5'	0° 6'	0° 7'	0° 8'	0° 9'	ARC "
0		2'5553	1'9542	1'7782	1'6532	1'5563	1'4771	1'4102	1'3522	1'3010	0
1	4'0334	2'2481	1'9506	1'7757	1'6514	1'5549	1'4759	1'4091	1'3513	1'3002	1
2	3'7324	2'2410	1'9471	1'7734	1'6496	1'5534	1'4747	1'4081	1'3504	1'2994	2
3	3'5563	2'2341	1'9435	1'7710	1'6478	1'5520	1'4735	1'4071	1'3495	1'2986	3
4	3'4314	2'2272	1'9400	1'7686	1'6460	1'5505	1'4723	1'4061	1'3486	1'2978	4
5	3'3345	2'2205	1'9365	1'7663	1'6443	1'5491	1'4711	1'4050	1'3477	1'2970	5
6	3'2553	2'2139	1'9331	1'7639	1'6425	1'5477	1'4699	1'4040	1'3468	1'2962	6
7	3'1883	2'2073	1'9296	1'7616	1'6407	1'5463	1'4688	1'4030	1'3459	1'2954	7
8	3'1303	2'2009	1'9262	1'7593	1'6390	1'5449	1'4676	1'4020	1'3450	1'2946	8
9	3'0792	2'1946	1'9228	1'7570	1'6372	1'5435	1'4664	1'4010	1'3441	1'2939	9
10	3'0334	2'1883	1'9195	1'7547	1'6355	1'5421	1'4652	1'4000	1'3432	1'2931	10
11	2'9900	2'1822	1'9162	1'7524	1'6337	1'5407	1'4640	1'3989	1'3423	1'2923	11
12	2'9542	2'1761	1'9128	1'7501	1'6320	1'5393	1'4629	1'3979	1'3415	1'2915	12
13	2'9195	2'1701	1'9096	1'7479	1'6303	1'5379	1'4617	1'3969	1'3406	1'2907	13
14	2'8873	2'1642	1'9063	1'7456	1'6286	1'5365	1'4605	1'3959	1'3397	1'2899	14
15	2'8573	2'1584	1'9031	1'7434	1'6269	1'5351	1'4594	1'3949	1'3388	1'2891	15
16	2'8293	2'1526	1'8999	1'7412	1'6252	1'5337	1'4582	1'3939	1'3379	1'2883	16
17	2'8030	2'1469	1'8967	1'7390	1'6235	1'5324	1'4571	1'3929	1'3371	1'2876	17
18	2'7782	2'1413	1'8935	1'7368	1'6218	1'5310	1'4559	1'3919	1'3362	1'2868	18
19	2'7547	2'1358	1'8904	1'7346	1'6201	1'5296	1'4548	1'3910	1'3353	1'2860	19
20	2'7324	2'1303	1'8873	1'7324	1'6184	1'5283	1'4536	1'3900	1'3344	1'2852	20
21	2'7112	2'1249	1'8842	1'7302	1'6168	1'5269	1'4525	1'3890	1'3336	1'2845	21
22	2'6910	2'1196	1'8811	1'7281	1'6151	1'5256	1'4514	1'3880	1'3327	1'2837	22
23	2'6717	2'1143	1'8781	1'7259	1'6135	1'5242	1'4502	1'3870	1'3319	1'2829	23
24	2'6532	2'1091	1'8751	1'7238	1'6118	1'5229	1'4491	1'3860	1'3310	1'2821	24
25	2'6355	2'1040	1'8721	1'7217	1'6102	1'5215	1'4480	1'3851	1'3301	1'2814	25
26	2'6184	2'0989	1'8691	1'7196	1'6085	1'5202	1'4468	1'3841	1'3293	1'2806	26
27	2'6021	2'0939	1'8661	1'7175	1'6069	1'5189	1'4457	1'3831	1'3284	1'2798	27
28	2'5863	2'0889	1'8632	1'7154	1'6053	1'5175	1'4446	1'3821	1'3276	1'2791	28
29	2'5710	2'0840	1'8602	1'7133	1'6037	1'5162	1'4435	1'3812	1'3267	1'2783	29
30	2'5563	2'0792	1'8573	1'7112	1'6021	1'5149	1'4424	1'3802	1'3259	1'2775	30
31	2'5421	2'0744	1'8544	1'7091	1'6004	1'5136	1'4412	1'3792	1'3250	1'2768	31
32	2'5283	2'0696	1'8516	1'7071	1'5988	1'5123	1'4401	1'3783	1'3241	1'2760	32
33	2'5149	2'0649	1'8487	1'7050	1'5973	1'5110	1'4390	1'3773	1'3233	1'2753	33
34	2'5019	2'0603	1'8459	1'7030	1'5957	1'5097	1'4379	1'3764	1'3225	1'2745	34
35	2'4894	2'0557	1'8431	1'7010	1'5941	1'5084	1'4368	1'3754	1'3216	1'2738	35
36	2'4771	2'0512	1'8403	1'6990	1'5925	1'5071	1'4357	1'3745	1'3208	1'2730	36
37	2'4652	2'0467	1'8375	1'6970	1'5909	1'5058	1'4346	1'3735	1'3199	1'2722	37
38	2'4536	2'0422	1'8348	1'6950	1'5894	1'5045	1'4335	1'3726	1'3191	1'2715	38
39	2'4424	2'0378	1'8320	1'6930	1'5878	1'5032	1'4325	1'3716	1'3183	1'2707	39
40	2'4314	2'0334	1'8293	1'6910	1'5863	1'5019	1'4314	1'3707	1'3174	1'2700	40
41	2'4206	2'0291	1'8266	1'6890	1'5847	1'5007	1'4303	1'3697	1'3166	1'2692	41
42	2'4102	2'0248	1'8239	1'6871	1'5832	1'4994	1'4292	1'3688	1'3158	1'2685	42
43	2'4000	2'0206	1'8212	1'6851	1'5816	1'4981	1'4281	1'3678	1'3149	1'2678	43
44	2'3900	2'0164	1'8186	1'6832	1'5801	1'4969	1'4270	1'3669	1'3141	1'2670	44
45	2'3802	2'0122	1'8159	1'6812	1'5786	1'4956	1'4260	1'3660	1'3133	1'2663	45
46	2'3707	2'0081	1'8133	1'6793	1'5771	1'4943	1'4249	1'3650	1'3124	1'2655	46
47	2'3613	2'0040	1'8107	1'6774	1'5755	1'4931	1'4238	1'3641	1'3116	1'2648	47
48	2'3522	2'0000	1'8081	1'6755	1'5740	1'4918	1'4228	1'3632	1'3108	1'2640	48
49	2'3432	1'9960	1'8055	1'6736	1'5725	1'4906	1'4217	1'3622	1'3100	1'2633	49
50	2'3345	1'9920	1'8030	1'6717	1'5710	1'4894	1'4206	1'3613	1'3091	1'2626	50
51	2'3259	1'9881	1'8004	1'6698	1'5695	1'4881	1'4196	1'3604	1'3083	1'2618	51
52	2'3174	1'9842	1'7979	1'6679	1'5680	1'4869	1'4185	1'3595	1'3075	1'2611	52
53	2'3091	1'9803	1'7954	1'6661	1'5666	1'4856	1'4175	1'3586	1'3067	1'2604	53
54	2'3010	1'9765	1'7929	1'6642	1'5651	1'4844	1'4164	1'3576	1'3059	1'2596	54
55	2'2931	1'9727	1'7904	1'6624	1'5636	1'4832	1'4154	1'3567	1'3051	1'2589	55
56	2'2852	1'9690	1'7879	1'6605	1'5621	1'4820	1'4143	1'3558	1'3043	1'2582	56
57	2'2775	1'9652	1'7855	1'6587	1'5607	1'4808	1'4133	1'3549	1'3034	1'2574	57
58	2'2700	1'9615	1'7830	1'6568	1'5592	1'4795	1'4122	1'3540	1'3026	1'2567	58
59	2'2626	1'9579	1'7806	1'6550	1'5577	1'4783	1'4112	1'3531	1'3018	1'2560	59
60	2'2553	1'9542	1'7782	1'6532	1'5563	1'4771	1'4102	1'3522	1'3010	1'2553	60

PROPORTIONAL LOGARITHMS													
sec. "	0° 10'	0° 11'	0° 12'	0° 13'	0° 14'	0° 15'	0° 16'	0° 17'	0° 18'	0° 19'	0° 20'	sec. "	
0	1'2553	1'2139	1'1761	1'1413	1'1091	1'0792	1'0512	1'0248	1'0000	9765	9542	0	
1	1'2545	1'2132	1'1755	1'1408	1'1086	1'0787	1'0507	1'0244	0'9996	9761	9539	1	
2	1'2538	1'2126	1'1749	1'1402	1'1081	1'0782	1'0502	1'0240	0'9992	9758	9535	2	
3	1'2531	1'2119	1'1743	1'1397	1'1076	1'0777	1'0498	1'0235	0'9988	9754	9532	3	
4	1'2524	1'2113	1'1737	1'1391	1'1071	1'0773	1'0493	1'0231	0'9984	9750	9528	4	
5	1'2517	1'2106	1'1731	1'1385	1'1066	1'0768	1'0489	1'0227	0'9980	9746	9524	5	
6	1'2510	1'2099	1'1725	1'1380	1'1061	1'0763	1'0484	1'0223	0'9976	9742	9521	6	
7	1'2502	1'2093	1'1719	1'1374	1'1055	1'0758	1'0480	1'0218	0'9972	9739	9517	7	
8	1'2495	1'2086	1'1713	1'1369	1'1050	1'0753	1'0475	1'0214	0'9968	9735	9514	8	
9	1'2488	1'2080	1'1707	1'1363	1'1045	1'0749	1'0471	1'0210	0'9964	9731	9510	9	
10	1'2481	1'2073	1'1701	1'1358	1'1040	1'0744	1'0467	1'0206	0'9960	9727	9506	10	
11	1'2474	1'2067	1'1695	1'1352	1'1035	1'0739	1'0462	1'0202	0'9956	9723	9503	11	
12	1'2467	1'2061	1'1689	1'1347	1'1030	1'0734	1'0458	1'0197	0'9952	9720	9499	12	
13	1'2460	1'2054	1'1683	1'1341	1'1025	1'0729	1'0453	1'0193	0'9948	9716	9496	13	
14	1'2453	1'2048	1'1677	1'1336	1'1020	1'0725	1'0449	1'0189	0'9944	9712	9492	14	
15	1'2445	1'2041	1'1671	1'1331	1'1015	1'0720	1'0444	1'0185	0'9940	9708	9488	15	
16	1'2438	1'2035	1'1665	1'1325	1'1009	1'0715	1'0440	1'0181	0'9936	9705	9485	16	
17	1'2431	1'2028	1'1660	1'1320	1'1004	1'0710	1'0435	1'0176	0'9932	9701	9481	17	
18	1'2424	1'2022	1'1654	1'1314	1'0999	1'0706	1'0431	1'0172	0'9928	9697	9478	18	
19	1'2417	1'2015	1'1648	1'1309	1'0994	1'0701	1'0426	1'0168	0'9924	9693	9474	19	
20	1'2410	1'2009	1'1642	1'1303	1'0989	1'0696	1'0422	1'0164	0'9920	9690	9471	20	
21	1'2403	1'2003	1'1636	1'1298	1'0984	1'0692	1'0418	1'0160	0'9916	9686	9467	21	
22	1'2396	1'1996	1'1630	1'1292	1'0979	1'0687	1'0413	1'0156	0'9912	9682	9464	22	
23	1'2389	1'1990	1'1624	1'1287	1'0974	1'0682	1'0409	1'0151	0'9908	9678	9460	23	
24	1'2382	1'1984	1'1619	1'1282	1'0969	1'0678	1'0404	1'0147	0'9905	9675	9456	24	
25	1'2375	1'1977	1'1613	1'1276	1'0964	1'0673	1'0400	1'0143	0'9901	9671	9453	25	
26	1'2368	1'1971	1'1607	1'1271	1'0959	1'0668	1'0395	1'0139	0'9897	9667	9449	26	
27	1'2362	1'1965	1'1601	1'1266	1'0954	1'0663	1'0391	1'0135	0'9893	9664	9446	27	
28	1'2355	1'1958	1'1595	1'1260	1'0949	1'0659	1'0387	1'0131	0'9889	9660	9442	28	
29	1'2348	1'1952	1'1589	1'1255	1'0944	1'0654	1'0382	1'0126	0'9885	9656	9439	29	
30	1'2341	1'1946	1'1584	1'1249	1'0939	1'0649	1'0378	1'0122	0'9881	9652	9435	30	
31	1'2334	1'1939	1'1578	1'1244	1'0934	1'0645	1'0373	1'0118	0'9877	9649	9432	31	
32	1'2327	1'1933	1'1572	1'1239	1'0929	1'0640	1'0369	1'0114	0'9873	9645	9428	32	
33	1'2320	1'1927	1'1566	1'1233	1'0924	1'0635	1'0365	1'0110	0'9869	9641	9425	33	
34	1'2313	1'1921	1'1560	1'1228	1'0919	1'0631	1'0360	1'0106	0'9865	9638	9421	34	
35	1'2306	1'1914	1'1555	1'1223	1'0914	1'0626	1'0356	1'0102	0'9861	9634	9418	35	
36	1'2300	1'1908	1'1549	1'1217	1'0909	1'0621	1'0352	1'0098	0'9858	9630	9414	36	
37	1'2293	1'1902	1'1543	1'1212	1'0904	1'0617	1'0347	1'0093	0'9854	9626	9410	37	
38	1'2286	1'1896	1'1537	1'1207	1'0899	1'0612	1'0343	1'0089	0'9850	9623	9407	38	
39	1'2279	1'1889	1'1532	1'1201	1'0894	1'0608	1'0339	1'0085	0'9846	9619	9404	39	
40	1'2272	1'1883	1'1526	1'1196	1'0889	1'0603	1'0334	1'0081	0'9842	9615	9400	40	
41	1'2266	1'1877	1'1520	1'1191	1'0884	1'0598	1'0330	1'0077	0'9838	9612	9396	41	
42	1'2259	1'1871	1'1515	1'1186	1'0880	1'0594	1'0326	1'0073	0'9834	9608	9393	42	
43	1'2252	1'1865	1'1509	1'1180	1'0875	1'0589	1'0321	1'0069	0'9830	9604	9389	43	
44	1'2245	1'1858	1'1503	1'1175	1'0870	1'0584	1'0317	1'0065	0'9827	9601	9386	44	
45	1'2239	1'1852	1'1498	1'1170	1'0865	1'0580	1'0313	1'0061	0'9823	9597	9383	45	
46	1'2232	1'1846	1'1492	1'1164	1'0860	1'0575	1'0308	1'0057	0'9819	9593	9379	46	
47	1'2225	1'1840	1'1486	1'1159	1'0855	1'0571	1'0304	1'0053	0'9815	9590	9376	47	
48	1'2218	1'1834	1'1481	1'1154	1'0850	1'0566	1'0300	1'0049	0'9811	9586	9372	48	
49	1'2212	1'1828	1'1475	1'1149	1'0845	1'0562	1'0295	1'0044	0'9807	9582	9369	49	
50	1'2205	1'1822	1'1469	1'1143	1'0840	1'0557	1'0291	1'0040	0'9803	9579	9365	50	
51	1'2198	1'1816	1'1464	1'1138	1'0835	1'0552	1'0287	1'0036	0'9800	9575	9362	51	
52	1'2192	1'1809	1'1458	1'1133	1'0831	1'0548	1'0282	1'0032	0'9796	9571	9358	52	
53	1'2185	1'1803	1'1452	1'1128	1'0826	1'0543	1'0278	1'0028	0'9792	9568	9355	53	
54	1'2178	1'1797	1'1447	1'1123	1'0821	1'0537	1'0274	1'0024	0'9788	9564	9351	54	
55	1'2172	1'1791	1'1441	1'1117	1'0816	1'0534	1'0270	1'0020	0'9784	9561	9348	55	
56	1'2165	1'1785	1'1436	1'1112	1'0811	1'0530	1'0265	1'0016	0'9780	9557	9344	56	
57	1'2159	1'1779	1'1430	1'1107	1'0806	1'0525	1'0261	1'0012	0'9777	9553	9341	57	
58	1'2152	1'1773	1'1424	1'1102	1'0801	1'0521	1'0257	1'0008	0'9773	9550	9337	58	
59	1'2145	1'1767	1'1419	1'1097	1'0797	1'0516	1'0252	1'0004	0'9769	9546	9334	59	
60	1'2139	1'1761	1'1413	1'1091	1'0792	1'0512	1'0248	1'0000	0'9765	9542	9331	60	

PROPORTIONAL LOGARITHMS

sec. //	^h _{0° 21'}	^h _{0° 22'}	^h _{0° 23'}	^h _{0° 24'}	^h _{0° 25'}	^h _{0° 26'}	^h _{0° 27'}	^h _{0° 28'}	^h _{0° 29'}	^h _{0° 30'}	^h _{0° 31'}	^h _{0° 32'}	sec. //
0	9331	9128	8935	8751	8573	8403	8239	8081	7929	7782	7639	7501	0
1	9327	9125	8932	8748	8570	8400	8236	8079	7926	7779	7637	7499	1
2	9324	9122	8929	8745	8567	8397	8234	8076	7924	7777	7634	7497	2
3	9320	9119	8926	8742	8565	8395	8231	8073	7921	7774	7632	7494	3
4	9317	9115	8923	8739	8562	8392	8228	8071	7919	7772	7630	7492	4
5	9313	9112	8920	8736	8559	8389	8226	8068	7916	7769	7627	7489	5
6	9310	9109	8917	8733	8556	8386	8223	8066	7914	7767	7625	7488	6
7	9306	9105	8913	8730	8553	8383	8220	8063	7911	7765	7623	7485	7
8	9303	9102	8910	8727	8550	8381	8218	8060	7909	7762	7620	7483	8
9	9300	9099	8907	8724	8547	8378	8215	8058	7906	7760	7618	7481	9
10	9296	9096	8904	8721	8544	8375	8212	8055	7904	7757	7616	7479	10
11	9293	9092	8901	8718	8542	8372	8210	8053	7901	7755	7613	7476	1
12	9289	9089	8898	8715	8539	8370	8207	8050	7899	7753	7611	7474	2
13	9286	9086	8895	8712	8536	8367	8204	8048	7896	7750	7609	7472	13
14	9283	9083	8892	8709	8533	8364	8202	8045	7894	7748	7606	7470	14
15	9279	9079	8888	8706	8530	8361	8199	8043	7891	7745	7604	7467	15
16	9276	9076	8885	8703	8527	8359	8196	8040	7889	7743	7602	7465	16
17	9272	9072	8882	8700	8524	8356	8194	8037	7886	7741	7600	7463	17
18	9269	9070	8879	8697	8522	8353	8191	8035	7884	7738	7597	7461	18
19	9265	9066	8876	8694	8519	8350	8188	8032	7882	7736	7595	7458	19
20	9262	9063	8873	8691	8516	8348	8186	8030	7879	7734	7593	7456	20
21	9259	9060	8870	8688	8513	8345	8183	8027	7877	7731	7590	7454	21
22	9255	9057	8867	8685	8510	8342	8180	8025	7874	7729	7588	7452	22
23	9252	9053	8864	8682	8507	8339	8178	8022	7872	7726	7586	7449	23
24	9249	9050	8861	8679	8504	8337	8175	8020	7869	7724	7583	7447	24
25	9245	9047	8857	8676	8501	8334	8173	8017	7867	7722	7581	7445	25
26	9242	9044	8854	8673	8499	8331	8170	8014	7864	7719	7579	7443	26
27	9238	9041	8851	8670	8496	8328	8167	8012	7862	7717	7577	7441	27
28	9235	9037	8848	8667	8493	8326	8165	8009	7859	7714	7574	7438	28
29	9232	9034	8845	8664	8490	8323	8162	8007	7857	7712	7572	7436	29
30	9228	9031	8842	8661	8487	8320	8159	8004	7855	7710	7570	7434	30
31	9225	9028	8839	8658	8484	8317	8157	8002	7852	7707	7567	7432	31
32	9222	9024	8836	8655	8482	8315	8154	7999	7850	7705	7565	7429	32
33	9218	9021	8833	8652	8479	8312	8152	7997	7847	7703	7563	7427	33
34	9215	9018	8830	8649	8476	8309	8149	7994	7845	7700	7560	7425	34
35	9211	9015	8827	8646	8473	8307	8146	7992	7842	7698	7558	7423	35
36	9208	9012	8824	8643	8470	8304	8144	7989	7840	7696	7556	7421	36
37	9205	9008	8820	8640	8467	8301	8141	7986	7837	7693	7554	7418	37
38	9201	9005	8817	8637	8465	8298	8138	7984	7835	7691	7551	7416	38
39	9198	9002	8814	8635	8462	8296	8136	7981	7832	7688	7549	7414	39
40	9195	8999	8811	8632	8459	8293	8133	7979	7830	7686	7547	7412	40
41	9191	8996	8808	8629	8456	8290	8130	7976	7828	7684	7544	7409	41
42	9188	8992	8805	8626	8453	8288	8128	7974	7825	7681	7542	7407	42
43	9185	8989	8802	8623	8451	8285	8125	7971	7823	7679	7540	7405	43
44	9181	8986	8799	8620	8448	8282	8123	7969	7820	7677	7538	7403	44
45	9178	8983	8796	8617	8445	8279	8120	7966	7818	7674	7535	7401	45
46	9175	8980	8793	8614	8442	8277	8117	7964	7815	7672	7533	7398	46
47	9171	8977	8790	8611	8439	8274	8115	7961	7813	7670	7531	7396	47
48	9168	8973	8787	8608	8437	8271	8112	7959	7811	7667	7528	7394	48
49	9165	8970	8784	8605	8434	8269	8110	7956	7808	7665	7526	7392	49
50	9161	8967	8781	8602	8431	8266	8107	7954	7806	7662	7524	7390	50
51	9158	8964	8778	8599	8428	8263	8104	7951	7803	7660	7522	7387	51
52	9155	8961	8775	8596	8425	8261	8102	7949	7801	7658	7519	7385	52
53	9152	8957	8772	8594	8422	8258	8099	7946	7798	7655	7517	7383	53
54	9148	8954	8769	8591	8420	8255	8097	7944	7796	7653	7515	7381	54
55	9145	8951	8766	8588	8417	8252	8094	7941	7794	7651	7513	7379	55
56	9142	8948	8763	8585	8414	8250	8091	7939	7791	7648	7510	7376	56
57	9138	8945	8760	8582	8411	8247	8089	7936	7789	7646	7508	7374	57
58	9135	8942	8757	8579	8409	8244	8086	7934	7786	7644	7506	7372	58
59	9132	8939	8754	8576	8406	8242	8084	7931	7784	7641	7503	7370	59
60	9128	8935	8751	8573	8403	8239	8081	7929	7782	7639	7501	7368	60

PROPORTIONAL LOGARITHMS

sec. "	0° 33'	0° 34'	0° 35'	0° 36'	0° 37'	0° 38'	0° 39'	0° 40'	0° 41'	0° 42'	0° 43'	0° 44'	sec. "
0	7368	7238	7112	6990	6871	6755	6642	6532	6425	6320	6218	6118	0
1	7365	7236	7110	6988	6869	6753	6640	6530	6423	6318	6216	6117	1
2	7363	7234	7108	6986	6867	6751	6638	6528	6421	6317	6215	6115	2
3	7361	7232	7106	6984	6865	6749	6637	6527	6420	6315	6213	6113	3
4	7359	7229	7104	6982	6863	6747	6635	6525	6418	6313	6211	6112	4
5	7357	7227	7102	6980	6861	6745	6633	6523	6416	6312	6210	6110	5
6	7354	7225	7100	6978	6859	6743	6631	6521	6414	6310	6208	6108	6
7	7352	7223	7098	6976	6857	6742	6629	6519	6412	6308	6206	6107	7
8	7350	7221	7095	6974	6855	6740	6627	6518	6411	6306	6205	6105	8
9	7348	7219	7093	6972	6853	6738	6625	6516	6409	6305	6203	6103	9
10	7346	7217	7091	6970	6851	6736	6624	6514	6407	6303	6201	6102	10
11	7343	7215	7089	6968	6849	6734	6622	6512	6405	6301	6200	6100	11
12	7341	7212	7087	6966	6847	6732	6620	6510	6404	6300	6198	6099	12
13	7339	7210	7085	6964	6845	6730	6618	6509	6402	6298	6196	6097	13
14	7337	7208	7083	6962	6843	6728	6616	6507	6400	6296	6194	6095	14
15	7335	7206	7081	6960	6841	6726	6614	6505	6398	6294	6193	6094	15
16	7333	7204	7079	6958	6839	6724	6612	6503	6397	6293	6191	6092	16
17	7330	7202	7077	6956	6837	6723	6611	6501	6395	6291	6189	6090	17
18	7328	7200	7075	6954	6836	6721	6609	6500	6393	6289	6188	6089	18
19	7326	7198	7073	6952	6834	6719	6607	6498	6391	6288	6186	6087	19
20	7324	7196	7071	6950	6832	6717	6605	6496	6390	6286	6184	6085	20
21	7322	7193	7069	6948	6830	6715	6603	6494	6388	6284	6183	6084	21
22	7320	7191	7067	6946	6828	6713	6601	6492	6386	6282	6181	6082	22
23	7317	7189	7065	6944	6826	6711	6600	6491	6384	6281	6179	6080	23
24	7315	7187	7063	6942	6824	6709	6598	6489	6383	6279	6178	6079	24
25	7313	7185	7061	6940	6822	6707	6596	6487	6381	6277	6176	6077	25
26	7311	7183	7059	6938	6820	6706	6594	6485	6379	6276	6174	6076	26
27	7309	7181	7057	6936	6818	6704	6592	6484	6377	6274	6173	6074	27
28	7307	7179	7054	6934	6816	6702	6590	6482	6376	6272	6171	6072	28
29	7304	7177	7052	6932	6814	6700	6589	6480	6374	6270	6169	6071	29
30	7302	7175	7050	6930	6812	6698	6587	6478	6372	6269	6168	6069	30
31	7300	7172	7048	6928	6810	6696	6585	6476	6370	6267	6166	6067	31
32	7298	7170	7046	6926	6809	6694	6583	6475	6369	6265	6164	6066	32
33	7296	7168	7044	6924	6807	6692	6581	6473	6367	6264	6163	6064	33
34	7294	7166	7042	6922	6805	6690	6579	6471	6365	6262	6161	6063	34
35	7291	7164	7040	6920	6803	6689	6578	6469	6363	6260	6159	6061	35
36	7289	7162	7038	6918	6801	6687	6576	6467	6362	6259	6158	6059	36
37	7287	7160	7036	6916	6799	6685	6574	6466	6360	6257	6156	6058	37
38	7285	7158	7034	6914	6797	6683	6572	6464	6358	6255	6154	6056	38
39	7283	7156	7032	6912	6795	6681	6570	6462	6357	6254	6153	6055	39
40	7281	7154	7030	6910	6793	6679	6568	6460	6355	6252	6151	6053	40
41	7279	7152	7028	6908	6791	6677	6567	6459	6353	6250	6150	6051	41
42	7276	7149	7026	6906	6789	6676	6565	6457	6351	6248	6148	6050	42
43	7274	7147	7024	6904	6787	6674	6563	6455	6350	6247	6146	6048	43
44	7272	7145	7022	6902	6785	6672	6561	6453	6348	6245	6145	6046	44
45	7270	7143	7020	6900	6784	6670	6559	6451	6346	6243	6143	6045	45
46	7268	7141	7018	6898	6782	6668	6557	6450	6344	6242	6141	6043	46
47	7266	7139	7016	6896	6780	6666	6556	6448	6343	6240	6140	6042	47
48	7264	7137	7014	6894	6778	6664	6554	6446	6341	6238	6138	6040	48
49	7261	7135	7012	6892	6776	6662	6552	6444	6339	6237	6136	6038	49
50	7259	7133	7010	6890	6774	6661	6550	6443	6338	6235	6135	6037	50
51	7257	7131	7008	6888	6772	6659	6548	6441	6336	6233	6133	6035	51
52	7255	7129	7006	6886	6770	6657	6547	6439	6334	6231	6131	6033	52
53	7253	7126	7004	6884	6768	6655	6545	6437	6332	6230	6130	6032	53
54	7251	7124	7002	6882	6766	6653	6543	6435	6331	6228	6128	6030	54
55	7249	7122	7000	6880	6764	6651	6541	6434	6329	6226	6126	6029	55
56	7246	7120	6998	6878	6762	6649	6539	6432	6327	6225	6125	6027	56
57	7244	7118	6996	6877	6761	6648	6538	6430	6325	6223	6123	6025	57
58	7242	7116	6994	6875	6759	6646	6536	6428	6324	6221	6121	6024	58
59	7240	7114	6992	6873	6757	6644	6534	6427	6322	6220	6120	6022	59
60	7238	7112	6990	6871	6755	6642	6532	6425	6320	6218	6118	6021	60

PROPORTIONAL LOGARITHMS

sec. //	0° 45'	0° 46'	0° 47'	0° 48'	0° 49'	0° 50'	0° 51'	0° 52'	0° 53'	0° 54'	0° 55'	0° 56'	sec. //
0	6021	5925	5832	5740	5651	5563	5477	5393	5310	5229	5149	5071	0
1	6019	5924	5830	5739	5649	5562	5476	5391	5309	5227	5148	5070	1
2	6017	5922	5829	5737	5648	5560	5474	5390	5307	5226	5146	5068	2
3	6016	5920	5827	5736	5646	5559	5473	5389	5306	5225	5145	5067	3
4	6014	5919	5826	5734	5645	5557	5471	5387	5304	5223	5144	5066	4
5	6013	5917	5824	5733	5643	5556	5470	5386	5303	5222	5142	5064	5
6	6011	5916	5823	5731	5642	5554	5469	5384	5302	5221	5141	5063	6
7	6009	5914	5821	5730	5640	5553	5467	5383	5300	5219	5140	5062	7
8	6008	5913	5819	5728	5639	5551	5466	5382	5299	5218	5139	5060	8
9	6006	5911	5818	5727	5637	5550	5464	5380	5298	5217	5137	5059	9
10	6004	5909	5816	5725	5636	5549	5463	5379	5296	5215	5136	5058	10
11	6003	5908	5815	5724	5634	5547	5461	5377	5295	5214	5135	5057	11
12	6001	5906	5813	5722	5633	5546	5460	5376	5294	5213	5133	5055	12
13	6000	5905	5812	5721	5632	5544	5459	5375	5292	5211	5132	5054	13
14	5998	5903	5810	5719	5630	5543	5457	5373	5291	5210	5131	5053	14
15	5997	5902	5809	5718	5629	5541	5456	5372	5290	5209	5129	5051	15
16	5995	5900	5807	5716	5627	5540	5454	5370	5288	5207	5128	5050	16
17	5993	5898	5806	5715	5626	5538	5453	5369	5287	5206	5127	5049	17
18	5992	5897	5804	5713	5624	5537	5452	5368	5285	5205	5125	5048	18
19	5990	5895	5803	5712	5623	5536	5450	5366	5284	5203	5124	5046	19
20	5988	5894	5801	5710	5621	5534	5449	5365	5283	5202	5123	5045	20
21	5987	5892	5800	5709	5620	5533	5447	5364	5281	5201	5122	5044	21
22	5985	5891	5798	5707	5618	5531	5446	5362	5280	5199	5120	5042	22
23	5984	5889	5796	5706	5617	5530	5444	5361	5279	5198	5119	5041	23
24	5982	5888	5795	5704	5615	5528	5443	5359	5277	5197	5118	5040	24
25	5981	5886	5793	5703	5614	5527	5442	5358	5276	5195	5116	5039	25
26	5979	5884	5792	5701	5612	5525	5440	5357	5275	5194	5115	5037	26
27	5977	5883	5790	5700	5611	5524	5439	5355	5273	5193	5114	5036	27
28	5976	5881	5789	5698	5610	5523	5437	5354	5272	5191	5112	5035	28
29	5974	5880	5787	5697	5608	5521	5436	5352	5270	5190	5111	5033	29
30	5973	5878	5786	5695	5607	5520	5435	5351	5269	5189	5110	5032	30
31	5971	5877	5784	5694	5605	5518	5433	5350	5268	5187	5108	5031	31
32	5969	5875	5783	5692	5604	5517	5432	5348	5266	5186	5107	5030	32
33	5966	5874	5781	5691	5602	5516	5430	5347	5265	5185	5106	5028	33
34	5966	5872	5780	5689	5601	5514	5429	5346	5264	5183	5105	5027	34
35	5965	5870	5778	5688	5599	5513	5428	5344	5262	5182	5103	5026	35
36	5963	5869	5777	5686	5598	5511	5426	5343	5261	5181	5102	5025	36
37	5961	5867	5775	5685	5596	5510	5425	5341	5260	5179	5101	5023	37
38	5960	5866	5774	5683	5595	5508	5423	5340	5258	5178	5099	5022	38
39	5958	5864	5772	5682	5594	5507	5422	5339	5257	5177	5098	5021	39
40	5957	5863	5771	5680	5592	5505	5421	5337	5256	5175	5097	5019	40
41	5955	5861	5769	5679	5591	5504	5419	5336	5254	5174	5095	5018	41
42	5954	5860	5768	5677	5589	5503	5418	5335	5253	5173	5094	5017	42
43	5952	5858	5766	5676	5588	5501	5416	5333	5252	5171	5093	5016	43
44	5950	5856	5764	5674	5586	5500	5415	5332	5250	5170	5092	5014	44
45	5949	5855	5763	5673	5585	5498	5414	5331	5249	5169	5090	5013	45
46	5947	5853	5761	5671	5583	5497	5412	5329	5248	5168	5089	5012	46
47	5946	5852	5760	5670	5582	5495	5411	5328	5246	5166	5088	5010	47
48	5944	5850	5758	5669	5580	5494	5409	5326	5245	5165	5086	5009	48
49	5942	5849	5757	5667	5579	5493	5408	5325	5244	5164	5085	5008	49
50	5941	5847	5755	5666	5577	5491	5407	5324	5242	5162	5084	5007	50
51	5939	5846	5754	5664	5576	5490	5405	5322	5241	5161	5082	5005	51
52	5938	5844	5752	5663	5575	5488	5404	5321	5239	5160	5081	5004	52
53	5936	5842	5751	5661	5573	5487	5402	5319	5238	5158	5080	5003	53
54	5935	5841	5749	5660	5572	5486	5401	5318	5237	5157	5079	5002	54
55	5933	5839	5748	5658	5570	5484	5400	5317	5235	5156	5077	5000	55
56	5931	5838	5746	5657	5569	5483	5398	5315	5234	5154	5076	4999	56
57	5930	5836	5745	5655	5567	5481	5397	5314	5233	5153	5075	4998	57
58	5928	5835	5743	5654	5566	5480	5395	5313	5231	5152	5073	4996	58
59	5927	5833	5742	5652	5564	5478	5394	5311	5230	5150	5072	4995	59
60	5925	5832	5740	5651	5563	5477	5393	5310	5229	5149	5071	4994	60

PROPORTIONAL LOGARITHMS

sec. //	1° 10'	1° 11'	1° 12'	1° 13'	1° 14'	1° 15'	1° 16'	1° 17'	1° 18'	1° 19'	1° 20'	1° 21'	sec. //
0	4108	4040	3979	3919	3860	3802	3745	3688	3632	3576	3522	3468	0
1	4101	4039	3978	3918	3859	3801	3744	3687	3631	3575	3521	3467	1
2	4100	4038	3977	3917	3858	3800	3743	3686	3630	3575	3520	3466	2
3	4099	4037	3976	3917	3857	3799	3742	3685	3629	3574	3519	3465	3
4	4098	4036	3975	3916	3856	3798	3741	3684	3628	3573	3518	3464	4
5	4097	4035	3974	3915	3855	3797	3740	3683	3627	3572	3517	3463	5
6	4096	4034	3973	3914	3855	3796	3739	3682	3626	3571	3516	3463	6
7	4094	4033	3972	3913	3854	3795	3738	3681	3625	3570	3515	3462	7
8	4093	4032	3971	3912	3853	3794	3737	3680	3624	3569	3514	3461	8
9	4092	4031	3970	3911	3852	3793	3736	3679	3623	3568	3514	3460	9
10	4091	4030	3969	3910	3851	3792	3735	3678	3622	3567	3513	3459	10
11	4090	4029	3968	3909	3850	3791	3734	3677	3621	3566	3512	3458	11
12	4089	4028	3967	3908	3849	3791	3733	3677	3621	3565	3511	3457	12
13	4088	4027	3966	3907	3848	3790	3732	3676	3620	3565	3510	3456	13
14	4087	4026	3965	3906	3847	3789	3731	3675	3619	3564	3509	3455	14
15	4086	4025	3964	3905	3846	3788	3730	3674	3618	3563	3508	3454	15
16	4085	4024	3963	3904	3845	3787	3729	3673	3617	3562	3507	3454	16
17	4084	4023	3962	3903	3844	3786	3728	3672	3616	3561	3506	3453	17
18	4083	4022	3961	3902	3843	3785	3727	3671	3615	3560	3505	3452	18
19	4082	4021	3960	3901	3842	3784	3726	3670	3614	3559	3505	3451	19
20	4081	4020	3959	3900	3841	3783	3726	3669	3613	3558	3504	3450	20
21	4080	4019	3958	3899	3840	3782	3725	3668	3612	3557	3503	3449	21
22	4079	4018	3957	3898	3839	3781	3724	3667	3611	3556	3502	3448	22
23	4078	4017	3956	3897	3838	3780	3723	3666	3610	3555	3501	3447	23
24	4077	4016	3955	3896	3837	3779	3722	3665	3610	3555	3500	3446	24
25	4076	4015	3954	3895	3836	3778	3721	3664	3609	3554	3499	3446	25
26	4075	4014	3953	3894	3835	3777	3720	3663	3608	3553	3498	3445	26
27	4074	4013	3952	3893	3834	3776	3719	3663	3607	3552	3497	3444	27
28	4073	4012	3951	3892	3833	3775	3718	3662	3606	3551	3496	3443	28
29	4072	4011	3950	3891	3832	3774	3717	3661	3605	3550	3496	3442	29
30	4071	4010	3949	3890	3831	3773	3716	3660	3604	3549	3495	3441	30
31	4070	4009	3948	3889	3830	3772	3715	3659	3603	3548	3494	3440	31
32	4069	4008	3947	3888	3829	3771	3714	3658	3602	3547	3493	3439	32
33	4068	4007	3946	3887	3828	3770	3713	3657	3601	3546	3492	3438	33
34	4067	4006	3945	3886	3827	3769	3712	3656	3600	3545	3491	3438	34
35	4066	4005	3944	3885	3826	3768	3711	3655	3599	3544	3490	3437	35
36	4065	4004	3943	3884	3825	3768	3710	3654	3598	3544	3489	3436	36
37	4064	4003	3942	3883	3824	3767	3709	3653	3597	3543	3488	3435	37
38	4063	4002	3941	3882	3823	3766	3708	3652	3597	3542	3488	3434	38
39	4062	4001	3940	3881	3822	3765	3708	3651	3596	3541	3487	3433	39
40	4061	4000	3939	3880	3821	3764	3707	3650	3595	3540	3486	3432	40
41	4060	3999	3938	3879	3820	3763	3706	3649	3594	3539	3485	3431	41
42	4059	3998	3937	3878	3820	3762	3705	3649	3593	3538	3484	3430	42
43	4057	3997	3936	3877	3819	3761	3704	3648	3592	3537	3483	3430	43
44	4056	3996	3935	3876	3818	3760	3703	3647	3591	3536	3482	3429	44
45	4055	3995	3934	3875	3817	3759	3702	3646	3590	3535	3481	3428	45
46	4054	3993	3933	3874	3816	3758	3701	3645	3589	3534	3480	3427	46
47	4053	3992	3932	3873	3815	3757	3700	3644	3588	3533	3479	3426	47
48	4052	3991	3931	3872	3814	3756	3699	3643	3587	3532	3479	3425	48
49	4051	3990	3930	3871	3813	3755	3698	3642	3586	3532	3478	3424	49
50	4050	3989	3929	3870	3812	3754	3697	3641	3586	3531	3477	3423	50
51	4049	3988	3928	3869	3811	3753	3696	3640	3585	3530	3476	3423	51
52	4048	3987	3927	3868	3810	3752	3695	3639	3584	3529	3475	3422	52
53	4047	3986	3926	3867	3809	3751	3694	3638	3583	3528	3474	3421	53
54	4046	3985	3925	3866	3808	3750	3693	3637	3582	3527	3473	3420	54
55	4045	3984	3924	3865	3807	3749	3692	3636	3581	3526	3472	3419	55
56	4044	3983	3923	3864	3806	3748	3691	3635	3580	3525	3471	3418	56
57	4043	3982	3922	3863	3805	3747	3691	3635	3579	3525	3471	3417	57
58	4042	3981	3921	3862	3804	3746	3690	3634	3578	3524	3470	3416	58
59	4041	3980	3920	3861	3803	3745	3689	3633	3577	3523	3469	3415	59
60	4040	3979	3919	3860	3802	3745	3688	3632	3576	3522	3468	3415	60

PROPORTIONAL LOGARITHMS													
sec. //	1° 22'	1° 23'	1° 24'	1° 25'	1° 26'	1° 27'	1° 28'	1° 29'	1° 30'	1° 31'	1° 32'	1° 33'	sec. //
0	3415	3362	3310	3259	3208	3158	3108	3059	3010	2962	2915	2868	0
1	3414	3361	3309	3258	3207	3157	3107	3058	3009	2961	2914	2867	1
2	3413	3360	3308	3257	3206	3156	3106	3057	3009	2961	2913	2866	2
3	3412	3359	3307	3256	3205	3155	3105	3056	3008	2960	2912	2865	3
4	3411	3358	3306	3255	3204	3154	3105	3056	3007	2959	2912	2865	4
5	3410	3358	3306	3254	3203	3153	3104	3055	3006	2958	2911	2864	5
6	3409	3357	3305	3253	3203	3153	3103	3054	3005	2958	2910	2863	6
7	3408	3356	3304	3253	3202	3152	3102	3053	3005	2957	2909	2862	7
8	3407	3355	3303	3252	3201	3151	3101	3052	3004	2956	2909	2862	8
9	3407	3354	3302	3251	3200	3150	3101	3052	3003	2955	2908	2861	9
10	3406	3353	3301	3250	3199	3149	3100	3051	3002	2954	2907	2860	10
11	3405	3352	3300	3249	3198	3148	3099	3050	3001	2954	2906	2859	11
12	3404	3351	3300	3248	3198	3148	3098	3049	3001	2953	2905	2859	12
13	3403	3351	3299	3247	3197	3147	3097	3048	3000	2952	2905	2858	13
14	3402	3350	3298	3247	3196	3146	3097	3047	2999	2951	2904	2857	14
15	3401	3349	3297	3246	3195	3145	3096	3047	2998	2950	2903	2856	15
16	3400	3348	3296	3245	3194	3144	3095	3046	2997	2950	2902	2855	16
17	3400	3347	3295	3244	3193	3143	3094	3045	2997	2949	2901	2855	17
18	3399	3346	3294	3243	3193	3143	3093	3044	2996	2948	2901	2854	18
19	3398	3345	3294	3242	3192	3142	3092	3043	2995	2947	2900	2853	19
20	3397	3344	3293	3241	3191	3141	3091	3043	2994	2946	2899	2852	20
21	3396	3344	3292	3241	3190	3140	3091	3042	2993	2946	2898	2852	21
22	3395	3343	3291	3240	3189	3139	3090	3041	2993	2945	2898	2851	22
23	3394	3342	3290	3239	3188	3138	3089	3040	2992	2944	2897	2850	23
24	3393	3341	3289	3238	3188	3138	3088	3039	2991	2943	2896	2849	24
25	3393	3340	3288	3237	3187	3137	3087	3038	2990	2942	2895	2848	25
26	3392	3339	3288	3236	3186	3136	3087	3038	2989	2942	2894	2848	26
27	3391	3338	3287	3236	3185	3135	3086	3037	2989	2941	2894	2847	27
28	3390	3338	3286	3235	3184	3134	3085	3036	2988	2940	2893	2846	28
29	3389	3337	3285	3234	3183	3133	3084	3035	2987	2939	2892	2845	29
30	3388	3336	3284	3233	3183	3133	3083	3034	2986	2939	2891	2845	30
31	3387	3335	3283	3232	3182	3132	3082	3034	2985	2938	2890	2844	31
32	3386	3334	3282	3231	3181	3131	3082	3033	2985	2937	2890	2843	32
33	3386	3333	3282	3231	3180	3130	3081	3032	2984	2936	2889	2842	33
34	3385	3332	3281	3230	3179	3129	3080	3031	2983	2935	2888	2841	34
35	3384	3331	3280	3229	3178	3128	3079	3030	2982	2935	2887	2841	35
36	3383	3331	3279	3228	3178	3128	3078	3030	2981	2934	2887	2840	36
37	3382	3330	3278	3227	3177	3127	3078	3029	2981	2933	2886	2839	37
38	3381	3329	3277	3226	3176	3126	3077	3028	2980	2932	2885	2838	38
39	3380	3328	3276	3225	3175	3125	3076	3027	2979	2931	2884	2838	39
40	3379	3327	3276	3225	3174	3124	3075	3026	2978	2931	2883	2837	40
41	3378	3326	3275	3224	3173	3124	3074	3026	2977	2930	2883	2836	41
42	3378	3325	3274	3223	3173	3123	3073	3025	2977	2929	2882	2835	42
43	3377	3325	3273	3222	3172	3122	3073	3024	2976	2928	2881	2835	43
44	3376	3324	3272	3221	3171	3121	3072	3023	2975	2927	2880	2834	44
45	3375	3323	3271	3220	3170	3120	3071	3022	2974	2927	2880	2833	45
46	3374	3322	3270	3219	3169	3119	3070	3022	2973	2926	2879	2832	46
47	3373	3321	3270	3219	3168	3119	3069	3021	2973	2925	2878	2831	47
48	3372	3320	3269	3218	3168	3118	3069	3020	2972	2924	2877	2831	48
49	3371	3319	3268	3217	3167	3117	3068	3019	2971	2923	2876	2830	49
50	3371	3319	3267	3216	3166	3116	3067	3018	2970	2923	2876	2829	50
51	3370	3318	3266	3215	3165	3115	3066	3018	2969	2922	2875	2828	51
52	3369	3317	3265	3214	3164	3114	3065	3017	2969	2921	2874	2828	52
53	3368	3316	3264	3214	3163	3114	3064	3016	2968	2920	2873	2827	53
54	3367	3315	3264	3213	3163	3113	3064	3015	2967	2920	2873	2826	54
55	3366	3314	3263	3212	3162	3112	3063	3014	2966	2919	2872	2825	55
56	3365	3313	3262	3211	3161	3111	3062	3013	2965	2918	2871	2824	56
57	3365	3313	3261	3210	3160	3110	3061	3013	2965	2917	2870	2824	57
58	3364	3312	3260	3209	3159	3109	3060	3012	2964	2916	2869	2823	58
59	3363	3311	3259	3209	3158	3109	3060	3011	2963	2916	2869	2822	59
60	3362	3310	3259	3208	3158	3108	3059	3010	2962	2915	2868	2821	60

PROPORTIONAL LOGARITHMS															
sec. "	1° 46'	1° 47'	1° 48'	1° 49'	1° 50'	1° 51'	1° 52'	1° 53'	1° 54'	1° 55'	1° 56'	1° 57'	sec. "		
0	2300	2259	2218	2178	2139	2099	2061	2022	1984	1946	1908	1871	0		
1	2299	2258	2218	2178	2138	2099	2060	2021	1983	1945	1907	1870	1		
2	2298	2257	2217	2177	2137	2098	2059	2021	1982	1944	1907	1870	2		
3	2298	2257	2216	2176	2137	2098	2059	2020	1982	1944	1906	1869	3		
4	2297	2256	2216	2176	2136	2097	2058	2019	1981	1943	1906	1868	4		
5	2296	2255	2215	2175	2135	2096	2057	2019	1980	1943	1905	1868	5		
6	2296	2255	2214	2174	2135	2096	2057	2018	1980	1942	1904	1867	6		
7	2295	2254	2214	2174	2134	2095	2056	2017	1979	1941	1904	1867	7		
8	2294	2253	2213	2173	2133	2094	2055	2017	1979	1941	1903	1866	8		
9	2294	2253	2212	2172	2133	2094	2055	2016	1978	1940	1903	1865	9		
10	2293	2252	2212	2172	2132	2093	2054	2016	1977	1939	1902	1865	10		
11	2292	2251	2211	2171	2132	2092	2053	2015	1977	1939	1901	1864	11		
12	2291	2251	2210	2170	2131	2092	2053	2014	1976	1938	1901	1863	12		
13	2291	2250	2210	2170	2130	2091	2052	2014	1975	1938	1900	1863	13		
14	2290	2249	2209	2169	2130	2090	2051	2013	1975	1937	1899	1862	14		
15	2289	2249	2208	2169	2129	2090	2051	2012	1974	1936	1899	1861	15		
16	2289	2248	2208	2168	2128	2089	2050	2012	1973	1936	1898	1861	16		
17	2288	2247	2207	2167	2128	2088	2050	2011	1973	1935	1898	1860	17		
18	2287	2247	2206	2167	2127	2088	2049	2010	1972	1934	1897	1860	18		
19	2287	2246	2206	2166	2126	2087	2048	2010	1972	1934	1896	1859	19		
20	2286	2245	2205	2165	2126	2086	2048	2009	1971	1933	1896	1858	20		
21	2285	2245	2204	2165	2125	2086	2047	2009	1970	1933	1895	1858	21		
22	2285	2244	2204	2164	2124	2085	2046	2008	1970	1932	1894	1857	22		
23	2284	2243	2203	2163	2124	2084	2046	2007	1969	1931	1894	1857	23		
24	2283	2243	2202	2163	2123	2084	2045	2007	1968	1931	1893	1856	24		
25	2283	2242	2202	2162	2122	2083	2044	2006	1968	1930	1893	1855	25		
26	2282	2241	2201	2161	2122	2083	2044	2005	1967	1929	1892	1855	26		
27	2281	2241	2200	2161	2121	2082	2043	2005	1967	1929	1891	1854	27		
28	2281	2240	2200	2160	2120	2081	2042	2004	1966	1928	1891	1854	28		
29	2280	2239	2199	2159	2120	2081	2042	2003	1965	1927	1890	1853	29		
30	2279	2239	2198	2159	2119	2080	2041	2003	1965	1927	1889	1852	30		
31	2279	2238	2198	2158	2118	2079	2041	2002	1964	1926	1889	1852	31		
32	2278	2237	2197	2157	2118	2079	2040	2001	1963	1926	1888	1851	32		
33	2277	2237	2196	2157	2117	2078	2039	2001	1963	1925	1888	1850	33		
34	2276	2236	2196	2156	2116	2077	2039	2000	1962	1924	1887	1850	34		
35	2276	2235	2195	2155	2116	2077	2038	2000	1961	1924	1886	1849	35		
36	2275	2235	2194	2155	2115	2076	2037	1999	1961	1923	1886	1849	36		
37	2274	2234	2194	2154	2114	2075	2037	1998	1960	1922	1885	1848	37		
38	2274	2233	2193	2153	2114	2075	2036	1998	1959	1922	1884	1847	38		
39	2273	2233	2192	2153	2113	2074	2035	1997	1959	1921	1884	1847	39		
40	2272	2232	2192	2152	2113	2073	2035	1996	1958	1921	1883	1846	40		
41	2272	2231	2191	2151	2112	2073	2034	1996	1957	1920	1883	1846	41		
42	2271	2231	2190	2151	2111	2072	2033	1995	1957	1919	1882	1845	42		
43	2270	2230	2190	2150	2111	2071	2033	1994	1956	1919	1881	1844	43		
44	2270	2229	2189	2149	2110	2071	2032	1994	1956	1918	1881	1844	44		
45	2269	2229	2188	2149	2109	2070	2032	1993	1955	1918	1880	1843	45		
46	2268	2228	2188	2148	2109	2070	2031	1993	1955	1917	1879	1842	46		
47	2268	2227	2187	2147	2108	2069	2030	1992	1954	1916	1879	1842	47		
48	2267	2227	2186	2147	2107	2068	2030	1991	1953	1916	1878	1841	48		
49	2266	2226	2186	2146	2107	2068	2029	1991	1953	1915	1878	1841	49		
50	2266	2225	2185	2145	2106	2067	2028	1990	1952	1914	1877	1840	50		
51	2265	2225	2184	2145	2105	2066	2028	1989	1951	1914	1876	1839	51		
52	2264	2224	2184	2144	2105	2066	2027	1989	1951	1913	1876	1839	52		
53	2264	2223	2183	2143	2104	2065	2026	1988	1950	1912	1875	1838	53		
54	2263	2223	2182	2143	2103	2064	2026	1987	1950	1912	1875	1838	54		
55	2262	2222	2182	2142	2103	2064	2025	1987	1949	1911	1874	1837	55		
56	2262	2221	2181	2141	2102	2063	2024	1986	1948	1911	1873	1836	56		
57	2261	2220	2180	2141	2101	2062	2024	1986	1948	1910	1873	1836	57		
58	2260	2220	2180	2140	2101	2062	2023	1985	1947	1909	1872	1835	58		
59	2260	2219	2179	2139	2100	2061	2023	1984	1946	1909	1871	1834	59		
60	2259	2218	2178	2139	2099	2061	2022	1984	1946	1908	1871	1834	60		

PROPORTIONAL LOGARITHMS

deg "	1° 58'	1° 59'	2° 0'	2° 1'	2° 2'	2° 3'	2° 4'	2° 5'	2° 6'	2° 7'	2° 8'	2° 9'	2° 10'	deg "
0	1834	1797	1761	1725	1689	1654	1619	1584	1549	1515	1481	1447	1413	0
1	1833	1797	1760	1724	1688	1653	1618	1583	1548	1514	1480	1446	1413	1
2	1833	1796	1760	1724	1688	1652	1617	1582	1548	1514	1479	1446	1412	2
3	1832	1795	1759	1723	1687	1652	1617	1582	1547	1513	1479	1445	1412	3
4	1831	1795	1758	1722	1687	1651	1616	1581	1547	1512	1478	1445	1411	4
5	1831	1794	1758	1722	1686	1651	1616	1581	1546	1512	1478	1444	1410	5
6	1830	1794	1757	1721	1686	1650	1615	1580	1546	1511	1477	1443	1410	6
7	1830	1793	1757	1721	1685	1650	1614	1580	1545	1511	1477	1443	1409	7
8	1829	1792	1756	1720	1684	1649	1614	1579	1544	1510	1476	1442	1409	8
9	1828	1792	1755	1719	1684	1648	1613	1578	1544	1510	1476	1442	1408	9
10	1828	1791	1755	1719	1683	1648	1613	1578	1543	1509	1475	1441	1408	10
11	1827	1791	1754	1718	1683	1647	1612	1577	1543	1508	1474	1441	1407	11
12	1827	1790	1754	1718	1682	1647	1612	1577	1542	1508	1474	1440	1407	12
13	1826	1789	1753	1717	1681	1646	1611	1576	1542	1507	1473	1440	1406	13
14	1825	1789	1752	1716	1681	1645	1610	1575	1541	1507	1473	1439	1405	14
15	1825	1788	1752	1716	1680	1645	1610	1575	1540	1506	1472	1438	1405	15
16	1824	1787	1751	1715	1680	1644	1609	1574	1540	1505	1472	1438	1404	16
17	1823	1787	1751	1715	1679	1644	1609	1574	1539	1505	1471	1437	1404	17
18	1823	1786	1750	1714	1678	1643	1608	1573	1539	1504	1470	1437	1403	18
19	1822	1786	1749	1713	1678	1642	1607	1573	1538	1504	1470	1436	1403	19
20	1822	1785	1749	1713	1677	1642	1607	1572	1538	1503	1469	1436	1402	20
21	1821	1785	1748	1712	1677	1641	1606	1571	1537	1503	1469	1435	1402	21
22	1820	1784	1748	1712	1676	1641	1606	1571	1536	1502	1468	1434	1401	22
23	1820	1783	1747	1711	1675	1640	1605	1570	1536	1502	1468	1434	1400	23
24	1819	1783	1746	1711	1675	1640	1605	1570	1535	1501	1467	1433	1400	24
25	1819	1782	1746	1710	1674	1639	1604	1569	1535	1500	1466	1433	1399	25
26	1818	1781	1745	1709	1674	1638	1603	1568	1534	1500	1466	1432	1399	26
27	1817	1781	1745	1709	1673	1638	1603	1568	1534	1499	1465	1432	1398	27
28	1817	1780	1744	1708	1673	1637	1602	1567	1533	1499	1465	1431	1398	28
29	1816	1780	1743	1708	1672	1637	1602	1567	1532	1498	1464	1431	1397	29
30	1816	1779	1743	1707	1671	1636	1601	1566	1532	1498	1464	1430	1397	30
31	1815	1778	1742	1706	1671	1635	1600	1566	1531	1497	1463	1429	1396	31
32	1814	1778	1742	1706	1670	1635	1600	1565	1531	1496	1463	1429	1395	32
33	1814	1777	1741	1705	1670	1634	1599	1565	1530	1496	1462	1428	1395	33
34	1813	1777	1740	1705	1669	1634	1599	1564	1529	1495	1461	1428	1394	34
35	1812	1776	1740	1704	1668	1633	1598	1563	1529	1495	1461	1427	1394	35
36	1812	1775	1739	1703	1668	1633	1598	1563	1528	1494	1460	1427	1393	36
37	1811	1775	1739	1703	1667	1632	1597	1562	1528	1494	1460	1426	1393	37
38	1811	1774	1738	1702	1667	1631	1596	1562	1527	1493	1459	1426	1392	38
39	1810	1774	1737	1702	1666	1631	1596	1561	1527	1493	1459	1425	1392	39
40	1809	1773	1737	1701	1665	1630	1595	1560	1526	1492	1458	1424	1391	40
41	1809	1772	1736	1700	1665	1630	1595	1560	1525	1491	1457	1424	1390	41
42	1808	1772	1736	1700	1664	1629	1594	1559	1525	1491	1457	1423	1390	42
43	1808	1771	1735	1699	1664	1628	1593	1558	1524	1490	1456	1423	1389	43
44	1807	1771	1734	1699	1663	1628	1593	1558	1524	1490	1456	1422	1389	44
45	1806	1770	1734	1698	1663	1627	1592	1558	1523	1489	1455	1422	1388	45
46	1806	1769	1733	1697	1662	1627	1592	1557	1523	1489	1455	1421	1388	46
47	1805	1769	1733	1697	1661	1626	1591	1556	1522	1488	1454	1420	1387	47
48	1805	1768	1732	1696	1661	1626	1591	1556	1522	1487	1454	1420	1387	48
49	1804	1768	1731	1696	1660	1625	1590	1555	1521	1487	1453	1419	1386	49
50	1803	1767	1731	1695	1660	1624	1589	1555	1520	1486	1452	1419	1386	50
51	1803	1766	1730	1694	1659	1624	1589	1554	1520	1486	1452	1418	1385	51
52	1802	1766	1730	1694	1658	1623	1588	1554	1519	1485	1451	1418	1384	52
53	1801	1765	1729	1693	1658	1623	1588	1553	1518	1485	1451	1417	1384	53
54	1801	1765	1728	1693	1657	1622	1587	1552	1518	1484	1450	1417	1383	54
55	1800	1764	1728	1692	1657	1621	1586	1552	1518	1483	1450	1416	1383	55
56	1800	1763	1727	1691	1656	1621	1586	1551	1517	1483	1449	1415	1382	56
57	1799	1763	1727	1691	1655	1620	1585	1551	1516	1482	1449	1415	1382	57
58	1798	1762	1726	1690	1655	1620	1585	1550	1516	1482	1448	1414	1381	58
59	1798	1761	1725	1690	1654	1619	1584	1550	1515	1481	1447	1414	1381	59
60	1797	1761	1725	1689	1654	1619	1584	1549	1515	1481	1447	1413	1380	60

TABLE 74

PROPORTIONAL LOGARITHMS													
sec. #	1° 11'	1° 12'	1° 13'	1° 14'	1° 15'	1° 16'	1° 17'	1° 18'	1° 19'	1° 20'	1° 21'	1° 22'	sec. #
0	1380	1347	1314	1282	1249	1217	1186	1154	1123	1091	1061	1030	0
1	1379	1346	1314	1281	1249	1217	1185	1153	1122	1091	1060	1029	1
2	1379	1346	1313	1281	1248	1216	1184	1153	1121	1090	1059	1029	2
3	1378	1345	1313	1280	1248	1216	1184	1152	1121	1090	1059	1028	3
4	1378	1345	1312	1279	1247	1215	1183	1152	1120	1089	1058	1028	4
5	1377	1344	1311	1279	1247	1215	1183	1151	1120	1089	1058	1027	5
6	1377	1344	1311	1278	1246	1214	1182	1151	1119	1088	1057	1027	6
7	1376	1343	1310	1278	1246	1214	1182	1150	1119	1088	1057	1026	7
8	1376	1343	1310	1277	1245	1213	1181	1150	1118	1087	1056	1026	8
9	1375	1342	1309	1277	1245	1213	1181	1149	1118	1087	1056	1025	9
10	1374	1341	1309	1276	1244	1212	1180	1149	1117	1086	1055	1025	10
11	1374	1341	1308	1276	1243	1211	1180	1148	1117	1086	1055	1024	11
12	1373	1340	1308	1275	1243	1211	1179	1148	1116	1085	1054	1024	12
13	1373	1340	1307	1275	1242	1210	1179	1147	1116	1085	1054	1023	13
14	1372	1339	1307	1274	1242	1210	1178	1147	1115	1084	1053	1023	14
15	1372	1339	1306	1274	1241	1209	1178	1146	1115	1084	1053	1022	15
16	1371	1338	1305	1273	1241	1209	1177	1146	1114	1083	1052	1022	16
17	1371	1338	1305	1272	1240	1208	1177	1145	1114	1083	1052	1021	17
18	1370	1337	1304	1272	1240	1208	1176	1145	1113	1082	1051	1021	18
19	1369	1337	1304	1271	1239	1207	1175	1144	1113	1082	1051	1020	19
20	1369	1336	1303	1271	1239	1207	1175	1143	1112	1081	1050	1020	20
21	1368	1335	1303	1270	1238	1206	1174	1143	1112	1081	1050	1019	21
22	1368	1335	1302	1270	1238	1206	1174	1142	1111	1080	1049	1019	22
23	1367	1334	1302	1269	1237	1205	1173	1142	1111	1080	1049	1018	23
24	1367	1334	1301	1269	1237	1205	1173	1141	1110	1079	1048	1018	24
25	1366	1333	1301	1268	1236	1204	1172	1141	1110	1079	1048	1017	25
26	1366	1333	1300	1268	1235	1203	1172	1140	1109	1078	1047	1017	26
27	1365	1332	1300	1267	1235	1203	1171	1140	1109	1078	1047	1016	27
28	1365	1332	1299	1267	1234	1202	1171	1139	1108	1077	1046	1016	28
29	1364	1331	1298	1266	1234	1202	1170	1139	1107	1076	1046	1015	29
30	1363	1331	1298	1266	1233	1201	1170	1138	1107	1076	1045	1015	30
31	1363	1330	1297	1265	1233	1201	1169	1138	1106	1075	1045	1014	31
32	1362	1329	1297	1264	1232	1200	1169	1137	1106	1075	1044	1014	32
33	1362	1329	1296	1264	1232	1200	1168	1137	1105	1074	1044	1013	33
34	1361	1328	1296	1263	1231	1199	1168	1136	1105	1074	1043	1013	34
35	1361	1328	1295	1263	1231	1199	1167	1136	1104	1073	1043	1012	35
36	1360	1327	1295	1262	1230	1198	1167	1135	1104	1073	1042	1012	36
37	1360	1327	1294	1262	1230	1198	1166	1135	1103	1072	1042	1011	37
38	1359	1326	1294	1261	1229	1197	1165	1134	1103	1072	1041	1010	38
39	1359	1326	1293	1261	1229	1197	1165	1134	1102	1071	1041	1010	39
40	1358	1325	1292	1260	1228	1196	1164	1133	1102	1071	1040	1009	40
41	1357	1325	1292	1260	1227	1196	1164	1132	1101	1070	1039	1009	41
42	1357	1324	1291	1259	1227	1195	1163	1132	1101	1070	1039	1008	42
43	1356	1323	1291	1258	1226	1194	1163	1131	1100	1069	1038	1008	43
44	1356	1323	1290	1258	1226	1194	1162	1131	1100	1069	1038	1007	44
45	1355	1322	1290	1257	1225	1193	1162	1130	1099	1068	1037	1007	45
46	1355	1322	1289	1257	1225	1193	1161	1130	1099	1068	1037	1006	46
47	1354	1321	1289	1256	1224	1192	1161	1129	1098	1067	1036	1006	47
48	1354	1321	1288	1256	1224	1192	1160	1129	1098	1067	1036	1005	48
49	1353	1320	1288	1255	1223	1191	1160	1128	1097	1066	1035	1005	49
50	1352	1320	1287	1255	1223	1191	1159	1128	1097	1066	1035	1004	50
51	1352	1319	1287	1254	1222	1190	1159	1127	1096	1065	1034	1004	51
52	1351	1319	1286	1254	1222	1190	1158	1127	1096	1065	1034	1003	52
53	1351	1318	1285	1253	1221	1189	1158	1126	1095	1064	1033	1003	53
54	1350	1317	1285	1253	1221	1189	1157	1126	1095	1064	1033	1002	54
55	1350	1317	1284	1252	1220	1188	1157	1125	1094	1063	1032	1002	55
56	1349	1316	1284	1251	1219	1188	1156	1125	1093	1063	1032	1001	56
57	1349	1316	1283	1251	1219	1187	1156	1124	1093	1062	1031	1001	57
58	1348	1315	1283	1250	1218	1187	1155	1124	1092	1062	1031	1000	58
59	1347	1315	1282	1250	1218	1186	1154	1123	1092	1061	1030	1000	59
60	1347	1314	1282	1249	1217	1186	1154	1123	1091	1061	1030	999	60

PROPORTIONAL LOGARITHMS

sec. "	2° 23'	2° 24'	2° 25'	2° 26'	2° 27'	2° 28'	2° 29'	2° 30'	2° 31'	2° 32'	2° 33'	2° 34'	sec. "
0	0999	0969	0939	0909	0880	0850	0821	0792	0763	0734	0706	0678	0
1	0999	0969	0939	0909	0879	0850	0820	0791	0762	0734	0705	0677	1
2	0998	0968	0938	0908	0879	0849	0820	0791	0762	0733	0705	0677	2
3	0998	0968	0938	0908	0878	0849	0819	0790	0762	0733	0704	0676	3
4	0997	0967	0937	0907	0878	0848	0819	0790	0761	0732	0704	0676	4
5	0997	0967	0937	0907	0877	0848	0818	0789	0761	0732	0703	0675	5
6	0996	0966	0936	0906	0877	0847	0818	0789	0760	0731	0703	0675	6
7	0996	0966	0936	0906	0876	0847	0817	0788	0760	0731	0702	0674	7
8	0995	0965	0935	0905	0876	0846	0817	0788	0759	0730	0702	0674	8
9	0995	0965	0935	0905	0875	0846	0816	0787	0759	0730	0702	0673	9
10	0994	0964	0934	0904	0875	0845	0816	0787	0758	0729	0701	0673	10
11	0994	0964	0934	0904	0874	0845	0815	0787	0758	0729	0701	0672	11
12	0993	0963	0933	0903	0874	0844	0815	0786	0757	0729	0700	0672	12
13	0993	0963	0933	0903	0873	0844	0815	0786	0757	0728	0700	0671	13
14	0992	0962	0932	0902	0873	0843	0814	0785	0756	0728	0699	0671	14
15	0992	0962	0932	0902	0872	0843	0814	0785	0756	0727	0699	0670	15
16	0991	0961	0931	0901	0872	0842	0813	0784	0755	0727	0698	0670	16
17	0991	0961	0931	0901	0871	0842	0813	0784	0755	0726	0698	0669	17
18	0990	0960	0930	0900	0871	0841	0812	0783	0754	0726	0697	0669	18
19	0990	0960	0930	0900	0870	0841	0812	0783	0754	0725	0697	0669	19
20	0989	0959	0929	0899	0870	0840	0811	0782	0753	0725	0696	0668	20
21	0989	0959	0929	0899	0869	0840	0811	0782	0753	0724	0696	0668	21
22	0988	0958	0928	0898	0869	0839	0810	0781	0752	0724	0695	0667	22
23	0988	0958	0928	0898	0868	0839	0810	0781	0752	0723	0695	0667	23
24	0987	0957	0927	0897	0868	0838	0809	0780	0751	0723	0694	0666	24
25	0987	0957	0927	0897	0867	0838	0809	0780	0751	0722	0694	0666	25
26	0986	0956	0926	0896	0867	0837	0808	0779	0750	0722	0693	0665	26
27	0986	0956	0926	0896	0866	0837	0808	0779	0750	0721	0693	0665	27
28	0985	0955	0925	0895	0866	0836	0807	0778	0750	0721	0693	0664	28
29	0985	0955	0925	0895	0865	0836	0807	0778	0749	0720	0692	0664	29
30	0984	0954	0924	0894	0865	0835	0806	0777	0749	0720	0692	0663	30
31	0984	0954	0924	0894	0864	0835	0806	0777	0748	0720	0691	0663	31
32	0983	0953	0923	0893	0864	0834	0805	0776	0748	0719	0691	0662	32
33	0983	0953	0923	0893	0863	0834	0805	0776	0747	0719	0690	0662	33
34	0982	0952	0922	0892	0863	0833	0804	0775	0747	0718	0690	0662	34
35	0982	0952	0922	0892	0862	0833	0804	0775	0746	0718	0689	0661	35
36	0981	0951	0921	0891	0862	0833	0803	0774	0746	0717	0689	0661	36
37	0981	0951	0921	0891	0861	0832	0803	0774	0745	0717	0688	0660	37
38	0980	0950	0920	0890	0861	0832	0802	0773	0745	0716	0688	0660	38
39	0980	0950	0920	0890	0860	0831	0802	0773	0744	0716	0687	0659	39
40	0979	0949	0919	0889	0860	0831	0801	0773	0744	0715	0687	0659	40
41	0979	0949	0919	0889	0859	0830	0801	0772	0743	0715	0686	0658	41
42	0978	0948	0918	0888	0859	0830	0801	0772	0743	0714	0686	0658	42
43	0978	0948	0918	0888	0858	0829	0800	0771	0742	0714	0685	0657	43
44	0977	0947	0917	0887	0858	0829	0800	0771	0742	0713	0685	0657	44
45	0977	0947	0917	0887	0857	0828	0799	0770	0741	0713	0685	0656	45
46	0976	0946	0916	0886	0857	0828	0799	0770	0741	0712	0684	0656	46
47	0976	0946	0916	0886	0856	0827	0798	0769	0740	0712	0684	0655	47
48	0975	0945	0915	0885	0856	0827	0798	0769	0740	0711	0683	0655	48
49	0975	0945	0915	0885	0855	0826	0797	0768	0739	0711	0683	0655	49
50	0974	0944	0914	0884	0855	0826	0797	0768	0739	0711	0682	0654	50
51	0974	0944	0914	0884	0855	0825	0796	0767	0739	0710	0682	0654	51
52	0973	0943	0913	0883	0854	0825	0796	0767	0738	0710	0681	0653	52
53	0973	0943	0913	0883	0854	0824	0795	0766	0737	0709	0681	0653	53
54	0972	0942	0912	0882	0853	0824	0795	0766	0737	0709	0680	0652	54
55	0972	0942	0912	0882	0853	0823	0794	0765	0737	0708	0680	0652	55
56	0971	0941	0911	0881	0852	0823	0794	0765	0736	0708	0679	0651	56
57	0971	0941	0911	0881	0852	0822	0793	0764	0736	0707	0679	0651	57
58	0970	0940	0910	0880	0851	0822	0793	0764	0735	0707	0678	0650	58
59	0970	0940	0910	0880	0851	0821	0792	0763	0735	0706	0678	0650	59
60	0969	0939	0909	0880	0850	0821	0792	0763	0734	0706	0678	0649	60

PROPORTIONAL LOGARITHMS															sec.
sec.	h 35'	h 36'	h 37'	h 38'	h 39'	h 40'	h 41'	h 42'	h 43'	h 44'	h 45'	h 46'	h 47'	h 48'	sec.
0	0649	0621	0594	0566	0539	0512	0484	0458	0431	0404	0378	0352	0	0	0
1	0649	0621	0593	0566	0538	0511	0484	0457	0430	0404	0377	0351	1	1	1
2	0648	0621	0593	0565	0538	0511	0484	0457	0430	0403	0377	0351	2	2	2
3	0648	0620	0592	0565	0537	0510	0483	0456	0430	0403	0377	0350	3	3	3
4	0648	0620	0592	0564	0537	0510	0483	0456	0429	0403	0376	0350	4	4	4
5	0647	0619	0591	0564	0536	0509	0482	0455	0429	0402	0376	0349	5	5	5
6	0647	0619	0591	0563	0536	0509	0482	0455	0428	0402	0375	0349	6	6	6
7	0646	0618	0590	0563	0535	0508	0481	0454	0427	0401	0374	0348	7	7	7
8	0646	0618	0590	0562	0535	0508	0481	0454	0427	0401	0374	0348	8	8	8
9	0645	0617	0590	0562	0535	0507	0480	0454	0427	0400	0374	0348	9	9	9
10	0645	0617	0589	0562	0534	0507	0480	0453	0426	0400	0373	0347	10	10	10
11	0644	0616	0589	0561	0534	0507	0479	0453	0426	0399	0373	0347	11	11	11
12	0644	0616	0588	0561	0533	0506	0479	0452	0426	0399	0373	0346	12	12	12
13	0643	0615	0588	0560	0533	0506	0479	0452	0425	0399	0372	0346	13	13	13
14	0643	0615	0587	0560	0532	0505	0478	0451	0425	0398	0372	0346	14	14	14
15	0642	0615	0587	0559	0532	0505	0478	0451	0424	0398	0371	0345	15	15	15
16	0642	0614	0586	0559	0531	0504	0477	0450	0424	0397	0371	0345	16	16	16
17	0641	0614	0586	0558	0531	0504	0477	0450	0423	0397	0370	0344	17	17	17
18	0641	0613	0585	0558	0531	0503	0476	0450	0423	0396	0370	0344	18	18	18
19	0641	0613	0585	0557	0530	0503	0476	0449	0422	0396	0370	0343	19	19	19
20	0640	0612	0584	0557	0530	0502	0475	0449	0422	0395	0369	0343	20	20	20
21	0640	0612	0584	0557	0529	0502	0475	0448	0422	0395	0369	0342	21	21	21
22	0639	0611	0584	0556	0529	0502	0475	0448	0421	0395	0368	0342	22	22	22
23	0639	0611	0583	0556	0528	0501	0474	0447	0421	0394	0368	0342	23	23	23
24	0638	0610	0583	0555	0528	0501	0474	0447	0420	0394	0367	0341	24	24	24
25	0638	0610	0582	0555	0527	0500	0473	0446	0420	0393	0367	0341	25	25	25
26	0637	0609	0582	0554	0527	0500	0473	0446	0419	0393	0366	0340	26	26	26
27	0637	0609	0581	0554	0526	0499	0472	0446	0419	0392	0366	0340	27	27	27
28	0636	0608	0581	0553	0526	0499	0472	0445	0418	0392	0366	0339	28	28	28
29	0636	0608	0580	0553	0526	0498	0471	0445	0418	0391	0365	0339	29	29	29
30	0635	0608	0580	0552	0525	0498	0471	0444	0418	0391	0365	0339	30	30	30
31	0635	0607	0579	0552	0525	0497	0471	0444	0417	0391	0364	0338	31	31	31
32	0634	0607	0579	0551	0524	0497	0470	0443	0417	0390	0364	0338	32	32	32
33	0634	0606	0579	0551	0524	0497	0470	0443	0416	0390	0363	0337	33	33	33
34	0634	0606	0578	0551	0523	0496	0469	0442	0416	0389	0363	0337	34	34	34
35	0633	0605	0578	0550	0523	0496	0469	0442	0415	0389	0363	0336	35	35	35
36	0633	0605	0577	0550	0522	0495	0468	0442	0415	0388	0362	0336	36	36	36
37	0632	0604	0577	0549	0522	0495	0468	0441	0414	0388	0362	0336	37	37	37
38	0632	0604	0576	0549	0521	0494	0467	0441	0414	0388	0361	0335	38	38	38
39	0631	0603	0576	0548	0521	0494	0467	0440	0414	0387	0361	0335	39	39	39
40	0631	0603	0575	0548	0521	0493	0466	0440	0413	0387	0360	0334	40	40	40
41	0630	0602	0575	0547	0520	0493	0466	0439	0413	0386	0360	0334	41	41	41
42	0630	0602	0574	0547	0520	0493	0466	0439	0412	0386	0359	0333	42	42	42
43	0629	0602	0574	0546	0519	0492	0465	0438	0412	0385	0359	0333	43	43	43
44	0629	0601	0573	0546	0519	0492	0465	0438	0411	0385	0359	0332	44	44	44
45	0628	0601	0573	0546	0518	0491	0464	0438	0411	0384	0358	0332	45	45	45
46	0628	0600	0573	0545	0518	0491	0464	0437	0410	0384	0358	0332	46	46	46
47	0627	0600	0572	0545	0517	0490	0463	0437	0410	0384	0357	0331	47	47	47
48	0627	0599	0572	0544	0517	0490	0463	0436	0410	0383	0357	0331	48	48	48
49	0627	0599	0571	0544	0516	0489	0462	0436	0409	0383	0356	0330	49	49	49
50	0626	0598	0571	0543	0516	0489	0462	0435	0409	0382	0356	0330	50	50	50
51	0626	0598	0570	0543	0516	0489	0462	0435	0408	0382	0356	0329	51	51	51
52	0625	0597	0570	0542	0515	0488	0461	0434	0408	0381	0355	0329	52	52	52
53	0625	0597	0569	0542	0515	0488	0461	0434	0407	0381	0355	0329	53	53	53
54	0624	0596	0569	0541	0514	0487	0460	0434	0407	0381	0354	0328	54	54	54
55	0624	0596	0568	0541	0513	0487	0460	0433	0406	0380	0354	0328	55	55	55
56	0623	0596	0568	0541	0513	0486	0459	0433	0406	0380	0353	0327	56	56	56
57	0623	0595	0568	0540	0513	0486	0459	0432	0405	0379	0353	0327	57	57	57
58	0622	0595	0567	0540	0512	0485	0458	0432	0405	0379	0352	0326	58	58	58
59	0622	0594	0567	0539	0512	0485	0458	0431	0405	0378	0352	0326	59	59	59
60	0621	0594	0566	0539	0512	0484	0458	0431	0404	0378	0352	0326	60	60	60

TABLE 74

923

PROPORTIONAL LOGARITHMS

sec.	47'	48'	49'	50'	51'	52'	53'	54'	55'	56'	57'	58'	59'	sec.
0	0326	0300	0274	0248	0223	0197	0172	0147	0122	0098	0073	0049	0024	0
1	0325	0299	0273	0248	0222	0197	0172	0147	0122	0097	0073	0048	0024	1
2	0325	0299	0273	0247	0222	0197	0171	0146	0121	0097	0072	0048	0023	2
3	0324	0298	0273	0247	0221	0196	0171	0146	0121	0096	0072	0047	0023	3
4	0324	0298	0272	0246	0221	0196	0171	0146	0121	0096	0071	0047	0023	4
5	0323	0297	0272	0246	0221	0195	0170	0145	0120	0096	0071	0046	0022	5
6	0323	0297	0271	0246	0220	0195	0170	0145	0120	0095	0071	0046	0022	6
7	0322	0297	0271	0245	0220	0194	0169	0144	0119	0095	0070	0046	0021	7
8	0322	0296	0270	0245	0219	0194	0169	0144	0119	0094	0070	0045	0021	8
9	0322	0296	0270	0244	0219	0194	0169	0143	0119	0094	0069	0045	0021	9
10	0321	0295	0270	0244	0218	0193	0168	0143	0118	0093	0069	0044	0020	10
11	0321	0295	0269	0244	0218	0193	0168	0143	0118	0093	0068	0044	0020	11
12	0320	0294	0269	0243	0218	0192	0167	0142	0117	0093	0068	0044	0019	12
13	0320	0294	0268	0243	0217	0192	0167	0142	0117	0092	0068	0043	0019	13
14	0319	0294	0268	0242	0217	0192	0166	0141	0117	0092	0067	0043	0018	14
15	0319	0293	0267	0242	0216	0191	0166	0141	0116	0092	0067	0042	0018	15
16	0319	0293	0267	0241	0216	0191	0166	0141	0116	0091	0066	0042	0018	16
17	0318	0292	0267	0241	0216	0190	0165	0140	0115	0091	0066	0042	0017	17
18	0318	0292	0266	0241	0215	0190	0165	0140	0115	0090	0066	0041	0017	18
19	0317	0291	0266	0240	0215	0189	0164	0139	0114	0090	0065	0041	0016	19
20	0317	0291	0265	0240	0214	0189	0164	0139	0114	0089	0065	0040	0016	20
21	0316	0291	0265	0239	0214	0189	0163	0139	0114	0089	0064	0040	0016	21
22	0316	0290	0264	0239	0213	0188	0163	0138	0113	0089	0064	0040	0015	22
23	0316	0290	0264	0238	0213	0188	0163	0138	0113	0088	0064	0039	0015	23
24	0315	0289	0264	0238	0213	0187	0162	0137	0112	0088	0063	0039	0015	24
25	0315	0289	0263	0238	0212	0187	0162	0137	0112	0087	0063	0038	0014	25
26	0314	0288	0263	0237	0212	0186	0161	0136	0112	0087	0062	0038	0014	26
27	0314	0288	0262	0237	0211	0186	0161	0136	0111	0087	0062	0038	0013	27
28	0313	0288	0262	0236	0211	0186	0161	0136	0111	0086	0062	0037	0013	28
29	0313	0287	0261	0236	0210	0185	0160	0135	0110	0086	0061	0037	0012	29
30	0313	0287	0261	0235	0210	0185	0160	0135	0110	0085	0061	0036	0012	30
31	0312	0286	0261	0235	0210	0184	0159	0134	0110	0085	0060	0036	0012	31
32	0312	0286	0260	0235	0209	0184	0159	0134	0109	0084	0060	0035	0011	32
33	0311	0285	0260	0234	0209	0184	0158	0134	0109	0084	0060	0035	0011	33
34	0311	0285	0259	0234	0208	0183	0158	0133	0108	0084	0059	0035	0010	34
35	0310	0285	0259	0233	0208	0183	0158	0133	0108	0083	0059	0034	0010	35
36	0310	0284	0258	0233	0208	0182	0157	0132	0107	0083	0058	0034	0010	36
37	0310	0284	0258	0232	0207	0182	0157	0132	0107	0082	0058	0033	0009	37
38	0309	0283	0258	0232	0207	0181	0156	0131	0107	0082	0057	0033	0009	38
39	0309	0283	0257	0232	0206	0181	0156	0131	0106	0082	0057	0033	0008	39
40	0308	0282	0257	0231	0206	0181	0156	0131	0106	0081	0057	0032	0008	40
41	0308	0282	0256	0231	0205	0180	0155	0130	0105	0081	0056	0032	0008	41
42	0307	0282	0256	0230	0205	0180	0155	0130	0105	0080	0056	0031	0007	42
43	0307	0281	0255	0230	0205	0179	0154	0129	0105	0080	0055	0031	0007	43
44	0306	0281	0255	0230	0204	0179	0154	0129	0104	0080	0055	0031	0006	44
45	0306	0280	0255	0229	0204	0179	0153	0129	0104	0079	0055	0030	0006	45
46	0306	0280	0254	0229	0203	0178	0153	0128	0103	0079	0054	0030	0006	46
47	0305	0279	0254	0228	0203	0178	0153	0128	0103	0078	0054	0029	0005	47
48	0305	0279	0253	0228	0202	0177	0152	0127	0103	0078	0053	0029	0005	48
49	0304	0279	0253	0227	0202	0177	0152	0127	0102	0077	0053	0029	0004	49
50	0304	0278	0252	0227	0202	0176	0151	0126	0102	0077	0053	0028	0004	50
51	0304	0278	0252	0227	0201	0176	0151	0126	0101	0077	0052	0028	0004	51
52	0303	0277	0252	0226	0201	0176	0151	0126	0101	0076	0052	0027	0003	52
53	0303	0277	0251	0226	0200	0175	0150	0125	0100	0076	0051	0027	0003	53
54	0302	0276	0251	0225	0200	0175	0150	0125	0100	0075	0051	0027	0002	54
55	0302	0276	0250	0225	0200	0174	0149	0124	0100	0075	0051	0026	0002	55
56	0301	0276	0250	0224	0199	0174	0149	0124	0099	0075	0050	0026	0002	56
57	0301	0275	0250	0224	0199	0174	0148	0124	0099	0074	0050	0025	0001	57
58	0300	0275	0249	0224	0198	0173	0148	0123	0098	0074	0049	0025	0001	58
59	0300	0274	0249	0223	0198	0173	0148	0123	0098	0073	0049	0025	0000	59
60	0300	0274	0248	0223	0197	0172	0147	0122	0098	0073	0049	0024	0000	60

ABBREVIATIONS ADOPTED IN THE ADMIRALTY CHARTS,
WITH EXPLANATORY NOTES.

GENERAL ABBREVIATIONS.

Anch ^o - Anchorage.	H.W. - High Water.	Obs ^a Spot Observation
B. - Bay.	H.W.F. & C. $\left\{ \begin{array}{l} \text{High Water.} \\ \text{Full \& Change.} \end{array} \right.$	Spot +
B. (near a buoy) Black.	I. - Island.	P. - Port.
Bat ^o - Battery.	I ^s - Islands.	P.D. - Position doubtful.
B ^a - Bank.	Kn. - Knots.	ful.
C. - Cape.	L. - Lake.	P ^a - Peak.
C.G. - Coast Guard.	Lat. - Latitude.	P ^a - Point.
Cath. - Cathedral.	Long. - Longitude.	R. - River.
Ch. - Church.	L ^t - Light.	R. (near a buoy) Red.
Chan. - Channel.	L ^t Alt. - " Alternating.	R ^a - Reef.
Cheq. Chequered.	L ^t F.Fl. - " Fixed and Flashing.	R ^a - Rock.
(near a buoy.)	L ^t F. - " Fixed.	S ^a - Sound.
Col ^a - Coloured.	L ^t Fl. - " Flashing.	sec. (near a light) Seconds.
Cr. - Creek.	L ^t Int. - " Intermittent.	Sh. - Shoal.
E.D. - Existence Doubtful.	L ^t Occ. - " Occulting.	Sp. - Springs.
Fl ^a L ^t - Floating Light.	L ^t Rev. - " Revolving.	Str. - Strait.
Fms. - Fathoms.	L.W. - Low Water.	Tel. - Telegraph.
Ft. - Feet or Foot.	m. (near a light) Nautical Mile.	Var ^a - Variation.
G. - Gulf.	Mag ^a - Magazine.	Vil. - Village.
G ^a - Groat.	Mag ^a - Magnetic.	vis. (near a light) Visible.
H. - Hour.	m.n. (near a light) Minutes.	V.S. (near a buoy) Vertical Stripes
H ^a - Head.	Mt. - Mountain.	W. (near a buoy) White.
Ho. - House.	Np. - Neaps.	W ^a Pl. - Watering Pl. ^{ce} .
H ^a - Harbour.		
M.S. (near a buoy) Horizontal Stripes.		

QUALITY OF THE BOTTOM.

b. - blue.	gn. - green.	rot. - rotten.
blk. - black.	grd. - ground.	s. - sand.
br. - brown.	gy. - gray.	sft. - soft.
brk. - broken.	h. - hard.	sh. - shells.
c. - coarse.	m. - mud.	spk. - speckled.
cl. - clay.	oy. - oysters.	st. - stones.
corl. - corall.	oz. - ooze.	stf. - stiff.
d. - dark.	pcb. - pebbles.	w. - white.
f. - fine.	pt. - pteropod.	w.l. - weed.
g. - gravel.	r. - rock.	y. - yellow.
gl. - glubigerina.		

All charts and plans are, where practicable, constructed upon the True Meridian, i.e. the East and the West marginal lines are drawn parallel to the True Meridian.

Soundings are reduced to mean Low Water of ordinary Spring tides, and are expressed in fathoms (of 6 feet) and fractions of a fathom, or in feet and fractions of a foot, each being denoted in the title of the Chart.

The underlined figures on the dry banks represent in feet or fathoms the depth of water over them at High Water, or the heights of the banks above Low Water. The method adopted is explained in the Title of the Chart. This dual system is being abolished, and in future all underlined figures will indicate feet above Low Water.

The Velocity of Tide is expressed in knots and fractions of a knot. The Period of the Tide being shown thus: 1st Qr., 2nd Qr., 3rd Qr., 4th Qr., for 1st, 2nd, 3rd, and 4th quarters.

The Rise of Tide is measured from the mean Low Water level of Ordinary Springs. The Range of Tide is measured from the Low Water of one tide to the High Water of the following tide. See Diagram on p. 344.

All heights are given in feet above High Water Ordinary Springs, and in places where there is no tide, above the level of the sea. [Exceptions to this general rule are stated on the title of the chart.]

All bearings, including the direction of winds and currents, are magnetic, except when otherwise expressed. Bearings of lights are given *as seen from seaward*, and not from the lights.

The natural scale, or the proportion which the Chart scale bears to the earth (obtained by reducing the number of feet in the minute of latitude to inches, and dividing the product by the scale), is represented thus $\frac{1}{12.5}$.

A cable's length is assumed to be equal to 100 fathoms; it is the 10th part of a sea mile.

Soundings upon Foreign Charts are expressed thus:—

Austrasian	(Faden) = 6.223	English feet, or 1.037	English fathoms
Chilian	(Metro) = 3.281	"	" 0.547 " "
Danish and Norwegian	(Favn) = 6.175	"	" 1.029 " "
Dutch (European)	(Vadem) = 5.575	"	" 0.929 " "
" (East Indian)	" = 5.905	"	" 0.984 " "
French	(Bra-se) = 5.329	"	" 0.888 " "
	(Mètre) = 3.281	"	" 0.547 " "
Italian	" = 3.281	"	" 0.547 " "
Japanese	(Fathom) = 6.000	"	" 1.000 " "
Portuguese	(Braça) = 6.004	"	" 1.000 " "
German	(Mètre) = 3.281	"	" 0.547 " "
Russian, Sashine or Fathom	(Сажень) = 6.000	"	" 1.000 " "
Spanish	(Braza) = 5.492	"	" 0.915 " "
Swedish	(Famn) = 5.843	"	" 0.974 " "
United States	(Fathom) = 6.000	"	" 1.000 " "

The Dutch *Elle*, the Spanish, Portuguese, and Italian *Metro*, and also the French *Mètre*, are identical.

CHARACTERISTICS MARKED AGAINST LIGHTS ON THE ADMIRALTY CHARTS.

F. Fixed. A continuous steady light.

FL. Flashing. Showing a single flash.

Gr. FL. Group flashing. Showing groups of two or more flashes in succession (not necessarily of the same colour), separated by eclipses.

F. & FL. Fixed and flashing. Fixed light varied by a single white or coloured flash, which may be preceded and followed by a short eclipse.

F. & Gr. FL. Fixed and group flashing. The same as the preceding, but with groups of flashes.

Rmv. Revolving. Light gradually increasing to full effect, then decreasing to eclipse. [At short distances and in clear weather a faint continuous light may be observed.]

Occ. Occulting. A steady light with, at regular intervals, one sudden and total eclipse.

Gr. Occ. Group occulting. A steady light with, at regular intervals, groups of two or more sudden and total eclipses.

The note attached to Revolving lights is in some cases applicable.

Alt. Alternating. Lights of different colours (generally red and white) alternately, without any intervening eclipse.

The distance the Lights are visible is calculated from a height of 15 feet above the sea at H.W. Lt.-vessels belonging to the Trinity House, London, are coloured red, have their Name painted on their sides, carry a Ball at each mast-head, fire a gun if a ship is standing into danger, and sound either a GONG or FOG HORN in foggy weather. A white Lt. is exhibited from the fore-mast of each Lt.-vessel, 6 feet above the rail, to show in which direction the vessel is riding.

When Lt.-vessels or other craft are placed to mark the position of wrecks, they will be distinguished by having their top-sides coloured green, and will exhibit, by day—Three balls from a yard, 20 feet above the sea; two placed vertically on the side that shipping may safely pass, and one on the other side. By night—Three fixed white Lts. similarly arranged, but the ordinary riding Lt. will not be shown. Mariners will thus know on sighting a wreck-marking vessel that she is so employed; and that they should pass on that side of her on which the two balls or two Lts. are shown.

GENERAL INDEX.

Numbers in index refer to the articles; unless prefixed by 'p.' when page is indicated.

A

ABERRATIONS adopted in Admiralty charts, p. 924, 925
Abbreviations, p. 10, note *
 in Table 10, explanation, p. 397
Abrolhos, no change of temper. of water on, 1038
Acceleration, Table 23, explan. p. 409
Achen, water off, p. 367
Acute, 86, p. 34
Adjusting screws, caution, 497
Adjusting compasses, 323
 Professor Airy on, 328
Adjustments of the sextant, 496
Admiralty ice chart, 1083
 charts, abbreviations adopted in, 924, 925
Adventure, H.M.S. p. 373, note
Age of tide, 919
 necessary for height, 935
Airy's projection of great circle on chart, 388
Alcates, log, p. 667, 373, note
Altitude, def. 306
 circles of, 427
 apparent and true, 493
 parallels of, 490
 changes of, 669
 correction of, p. 390
 observing the moon's, 540
 a star's, 541
 reduction of, for change of place, 661
 to an intermediate time, 660
 true to apparent, 667, 363
 to find the, p. 337
 on the merid. 668
 from the hour-angle, 666, &c.
 from the azimuth, 668, &c.
 on the prime vertical, 664, &c.
 and hour-angle, Table 29, explan. p. 411
 Tables 43, 44, explan. p. 415
 change of, to find, 669, &c.
 change of, at a given azimuth, 670, &c.
 Table 46, explan. p. 415
 do. and variation of do. p. 300
Altitudes, observing at sea, 487, 534
 do. when high, 535
 do. with hazy horizon or disc, 538
 with a shore horizon, 549, 550
 observing, on shore, 551
 manner of testing a set of, 556
 observed from opposite points of the horizon, 536, 541
 a set of, error of intervals, 558
 of stars, afford a check on the D.R. as also on a mistake in the sun's decl. 977
Ambiguous case, plane trigonometry, p. 50A
Amplitude, def. 446
 Table 59, explan. p. 419
 affected by refraction, 446
 corr. of Table 59A, explan. p. 420

Amplitude, observing, at sea, 385
 of a star is best observed at setting, 993
 the observation, not open to certain errors, 888
 to compute the, 887
Analogies or trigon. canons, 162
 rules for working by logs. 166
Analogy, 43
Anchor, angles for recovering a lost, 363
Angle, def. 81
 measure of, 83
 acute and obtuse, 86
 to lay off, at a point, 95
 at the sun or moon in a lunar, to find, p. 314, note †
Angles to measure and lay off, 104, 107
Animalcules colour the sea, p. 373, note †
Annatom, bearings required, p. 376, note
Annuaire des Mardres, p. 335, note *
Antarctic circle, 311
Aor, Pulo, p. 383
Apparent Altitude, 423
 dip, 305
 Table 30, explan. p. 411
 distance, 848 (3), and 850
 time, def. 474
 to convert into mean, 606
Approximate, note on term, p. 51
 are often preferable, p. 373, note
Approximate Doub. Alt., advantage of the method in practice, Pref. vi
 has been found convenient, p. 263, note
Approximate Lunar, principle, p. 302, note
 is near enough in general. 843, p. 306
 should be used as a check against error in the rigorous process, p. 304, note †
 affords the angles at both bodies, p. 314, note †
Arago, terrest. refr. 536
Arc, def. 80
 to convert into time, 570
 Table 17, explan. p. 408
 square of, to find, p. 418, Tab. 56
 is the limit of the sum of the chords, p. 130, note
 of sextant, to test, 498
Arctic circle, 311
Arithmetic complement, 63
 application of, 63
Arithmetical operations, by logs. p. 20, 64 to 72
Arlett, Lieut. p. 396
Arming, of the lead, 396
Arshens, p. 390 (10)
Artificial horizon, 517
 fluids proper for the purpose, 521
 Comm. Becher's, 522, p. 190
 bubble, not approved, p. 189, note †

Artificial horizon-top, p. 190, note*
 effect of the height of the eye, 559
 stand for, 519
Assumption, solution by, p. 51, note
Astronomical bearings, 903 : day, 480
Astronomy, Nautical Spherics applied to, p. 62A-64A
Athos, Mt. example, 394
Augmentation, Jsemid. 440
 Table 42, explan. p. 416
Australia dew, p. 368
Awaah, symbol of, p. 399 (1)
Axiom, 113
Axis, 181
Azimuth, def. 444 : how measured, 445
 to find, from the alt. 673
 from the hour-angle, 675
 from the hour-angle and alt. 676
 from change of alt. 677
 tables Burdwood and Davis, indispensable in iron ships, note on, p. 243
 tables, Davis star azimuth, p. 136, 242, 330

B

BAIRD & Roberts's Indian Tide Tables, p. 340, note
Barbary, coast, anchorage off, p. 374, note
Barometer, Fr. and Engl. Table 37, explan. p. 418
 ht. of, affects the tide, 929, note
Barrier ris. 1033
Bearings, compass, 223
 magnetic, 223
 true, 223
Bearing-plate, 318
Bearing, def. 301
 taking a, 301
 of land, by means of chron. 1016
Beaufort, Sir F., observation of index error, p. 182, note 3
 notation for wind and weather, 409
Becher, Comm., artificial horizon, 522, p. 190
Beechey, Adm., sextant, 501
 remarks on temperature of the sea, 1039 : see also p. 370
 his chronometers, p. 361, note †
Bégat, M. *Traité de Géodésie*, p. 181, note
Belcher, Sir E., remark on chronometers, p. 374, note
Bellinghousen, Adm., pp. 356-7, 374, note †
Bessel's refract. p. 401, note
Biot, M., mirage, p. 62, note
Birds indicate land, 1035
Bisect, a line, 98
 an arc, 100
Black Joke, p. 353, note *
Blackwood, Capt., 1033
Boat, horizon from, 538
Borda's circle, 507, &c.
Bottom, quality of, how expressed on charts, p. 924

Numbers in Index refer to the articles; unless prefixed by 'p,' when page is indicated.

Bowring, Mr. Lunars, p. 330, note
 Brackets, in Tab. 10, denote limits, &c.
 p. 389, No. 8
 Brasses, p. 330 (5), and p. 325
 Brasses, p. 381 (15)
 Breakers, 1041
 Burckhardt, tables, moon's semid. too
 small, p. 315 note
 Burdwood and Davis, azimuth tables,
 note, p. 242
 indispensable in iron ships, p. 242
 Burt's buoy and nipper, 402

O

OARLE's length, p. 325
 Calendar, necessity of arbitrary cor-
 rection, p. 170, note †
 Canon, raising the, 111
 Canons, constructing the, 163
 Carotest, 1058
 Case of a sextant, remark on, p. 188,
 note
 Centigrade therm. Table 36, expl. p.
 413
 Centimètre, Table 37, explan. p. 413
 Centre of a circle, to find, 102
 Changes of alt. 669
 Charts, p. 145, 146, note
 of small districts, 392
 Admiralty abbreviations adopted
 in, pp. 324, 325
 Chasing, p. 118, note †
 Chord, def. 80
 Chords, scale of, 106
 to construct, 109
 Chronometer, manner of fixing, 525
 position to be preserved, 526
 should be compared when moved,
 526; Chronometer Tables, p. 364
 to be wound up regularly, 537
 when stopped how to set a-going,
 537
 temperature chief cause of change
 of rate, 538
 recommended to be held in the
 hand while firing, p. 192, note †
 rating. *See Rating*, p. 293-297
 sea rates, p. 297
 Chronometers perform best at first,
 480
 agreement of, 521
 all in error, p. 361, note
 affected by thunder-storms, p.
 192, note
 supplying to ships generally, Pref.
 p. ix
 Chronometric differences, communi-
 cation of, p. 299
 Circle, def. 74
 to divide, 101
 to find centre of, 102
 to draw through three points, 108
 Circumference, 74
 Circummeridional alta. 705
 Civil day, 480
 time converted into astron. 480
 Clearness of water, 1033
 Closing a vessel, p. 118, note †
 Clump of trees, symbol, p. 399 (5)
 Coal depot, Table 11, p. 634; symbol,
 p. 401
 Cocoon-bur tree, importance of, p. 368
 (4)
 Colatitude, def. 185
 Coloured shades, 491
 error of, 499
 Combined alta., on the term, p. 255
 note *
 Common denominator, 9
 measure, p. 2, note
 Comparison of two watches, 564
 Compass, mariner's,
 antiquity of, 213
 azimuth, 214
 boxing, 212, p. 65
 Committee, Admiralty, 215
 Liverpool, 268

Compass, divisions of card, 212, p. 64
 examination of, 217
 liquid, 215
 points and degrees, 213
 to corr. for Var. & Dev. of, p. 160
 prismatic azimuth, 214
 Sir Wm. Thomson's, 216
 standard, 224
 total error of, 207, p. 324
 bearings, symbol for, p. 399 (3)
 Complement of an angle, 86
 Component signs (of symbols), p. 399
 Computation, 167 (3)
 Conjunction, 457
 Construction, 167
 Conversion of times, p. 198
 Cook, Captain, 1036, 1048
 Coral reefs, Navig. amongst, 1032
 Corollary, 114
 Correcting courses, for leeway, 418
 for variation, 321
 Correction of alt. p. 220
 the sun, p. 231
 the moon, p. 233
 a star or planet, p. 232
 for ship's change of place, 661
 for lapse of time, 669 to 672
 of Charts, caution, p. 145, note
 of the decl. &c. p. 246
 for 2d difference, 498
 of the long. by D.R. 966
 Coscant, def. 155
 to find, p. 578
 Cosine, def. 153
 to find, p. 578
 Cotangent, def. 154
 to find, p. 578
 Counting seconds, useful, 268
 Course, def. 197; D.R. 961
 how measured, 197
 by compass, 951
 to correct for Var. and Dev.
 221, p. 159
 by compass, for leeway, 418
 steered, 197
 shaping the, 940
 in a current, 942, p. 160
 on a great circle, 944
 when the long. is uncertain,
 1039
 to reduce course true, to course
 by compass, 231, p. 159
 Cross bearings, 266
 departure by, 266
 require variation to
 be known, 266
 Crossing mer. of 180°, pp. 354 and 406,
 note *
 Cross observation, by Borda's circle, 510
 Cube, 67
 Cube root, to extract by logs. 72
 Culmination, def. 454
 Current, how named, 290
 sometimes assumed, 1015
 drift of, computed, 291
 effect of, is always mixed up with
 local deviation, 298
 determination of, 1015, p. 160,
 180
 in shaping the course, p. 160
 Current sailing, p. 114
 charts, p. 145, note †

D

DAILY variations, Tables 21 and 21A,
 explan. p. 408, 409
 by Trav. Table, p. 379
 Damper, 1028, 1034
 Danger angle, 1033, pp. 143 and 366
 Danger discovered, 1061
 determination of, 1065
 transmitting account of, 1057
 duty of commanders respecting,
 1058
 in closing land, 1033, p. 366
 on ice, p. 368 (5)
 Danish feet, p. 280 (2)
 Darwin, Mr., p. 372, note

Date, change of, in crossing mer. of
 180° 971
 Dates, civil and astronomical, 480
 Dausmy, M., tides affected by barom.
 p. 240, note
 Davis and Burdwood, azimuth tables,
 note p. 242; star azimuth, p. 330
 Day and night equal, when sun on
 equator, 463
 lost or gained in going round the
 world, 970, note, p. 408, note
 Day's work, 418
 Dead reckoning, 208
 great importance of, 262
 keeping the, 964
 errors of the, 961, 966
 Decimals, p. 6
 omitting some places, 35
 reduction of, p. 8, 9
 Décimètre, Table 37
 Declination, def. 441; circles of, 441
 parallels of, 442
 Tables of, p. 430, p. 638
 corr., 579, 589, p. 308A, p. 224
 Deep sea lead, 328
 heaving the, 400
 Definitions in Navigation, 178-211
 in Nautical Astronomy, 419-482
 Spherics, p. 554, 564
 Degree, def. 75; of long. 194
 Degree of dependance, Pref. vii;
 principles, p. 52
 Degrees of lat. unequal in Mercator
 Chart, 579
 proportion of on Merc. Chart, 576
 Denominator, def. 2
 D'Entrecasteaux, 1035
 Departure, def. 200
 taking a, 347
 is secured up to the latest period,
 408
 and corresp. Diff. Long., Table
 3, expln. p. 251
 Departures, Chap. IV, p. 157
 by a bearing, 349
 by sound, 352
 by soundings, 373
 by two bearings and distance
 run, 350
 by alt. of a summit, 253
 by bearing and lat. or long. 374
 by cross bearings, 266
 by two angles, 363
 by two alta. of a summit, 361
 when in a line between two
 points, 372
 Depression, true, def. 205
 Table 9, explan. p. 347
 Description-symbols, p. 297
 Determinations of places, mode of
 indicating accuracy of, p. 296
 good do., marked ⊕ or noted to
 decimals, p. 296
 bad do., marked ⊖, p. 296
 Deviation of the compass, 222
 how determined, 224
 table, 225
 curve of, 226
 Napier's curve of, 229
 by straight line method, 230
 laws of its change, 246
 semicircular, 248
 quadrantal, 249
 constant, 250
 separation of parts, 251
 effect of electricity on, 254, p.
 101
 to correct courses and bearings
 for, 228, p. 159
 semicircular, to correct, 253-254
 quadrantal, to correct, 249
 coefficients of, 257
 Diagonal scale, 105
 Diameter of a circle, 78
 of the earth, 180
 apparent, of the sun and moon
 affected by refraction, p. 152,
 note †
 measuring do., p. 183 (2)

Numbers in Index refer to the articles; unless prefixed by 'p.' when page is indicated.

Difference of alt. to compute, 669
 is a test of observation, 556
 of azimuth required in a double
 altitude, 749
 of lat. def. 188
 how found, 189
 of long def. 194
 how found, 195
 determined by chron. 187, note
Diff. Long. and corres. dep. Table 4,
 p. 281
Dip, magnetic, discovery of, 232
 changes in, 232
 map showing, 232
Dip of the horizon, 208
 Table 30, explan. p. 411
 is variable, 207
 may be employed to the nearest
 min. only, p. 412
 accuracy necessary when the eye
 is low, 546
 of a shore horizon, Table 35, ex-
 plan. p. 418
 sector, p. 184, note †
Discoloured water, 1049
Distance, nautical term, def. 199
 error of, 960
 between two places, is least on a
 great circle, 336
 of the land in taking departures,
 349
 of sea horizon, Table 8, and p. 386
 methods of determining, Chap. IV.
 by sound, 382
 navigable Mercatorial, Table 12,
 explan. p. 406
Distance, by change of bearing, 350;
 Table 7, explan. p. 386
 by alt. of land, 353, 354
 by change of alt. 361
 of the celestial bodies is deter-
 mined by their parallax, 436
Distortion of charts, p. 146, note
Diurnal inequality, 928
Divide a line into equal parts, 99
 a circle into parts, 101
Division by logarithms, 66
Duckyards, a list of, p. 684
Dollond's circle, 516
Double altitude, 255
 Spherics applied to, p. 63A
 of the same body, p. 255
 short double alt. 750
 observations on same side, 729
Degr. of dependence, 730
 on different sides of meridian, 731
Degr. of dependence, 732
 when not known on which side
 of meridian, 728
 by stars or the moon, 734, &c.
 when one alt. is near the meri-
 dian, 787
 by the sun, 739
 by the moon, 743
 by a star, 741
 by a planet, 743
Degr. of dependence, 745
 when neither altitude is near the
 meridian, 746
 the simplest case, 750
 by the sun, 751
 by the moon, 755
 by a star, 753
 by a planet, 754
Degr. of dependence, 771
Ivory's method, 757
 correction of lat., p. 265 and
 Table 71, explan. p. 428
 of different bodies, 769
 one alt. near the merid. 761
 below the pole, 765
 observations not at the same
 instant, 764
 neither alt. near the merid. 746
 the general or rigorous process, 770
Degr. of dependence by any of
 these solutions, 771
 not necessary to correct for diff.
 long. made good, p. 364, note

Double rule of three, p. 15
Double sextant, general method of
 using, 504
D.R., abbrev. of dead reckoning, 203
Drift of a current, 290
Ducom, Cours d'Observations Nau-
tiques, p. 256, note
Du Petit Thouars, M., p. 196, note †,
 1038
D'Urville, M., voyage, 1035
Dutch feet, p. 280 (3)
 palms, p. 280 (4)

E

EARTH, how magnetised, 236
 figure and magnitude, 180
Eastline or Westing, 200
Eclipse, 456
Ecliptic, 459
Elevation of observer affects place of
 horizon, 206, 446 (3), 546
 affects refraction, p. 414, note
 effect of, on altitude, 559
 on time of rising and setting,
 638
 on amplitude, 446 (1), p. 526,
 note
Entire correction, 907, 961
Epacts, Table 14, explan. p. 407
Equal alts. 796
 at sea, 798; on shore, 808
 equation of, 797
 logs. for computing do., Table 72,
 explan. p. 428
Equal corr. for change of refract. 810
Equation of time, 476
 to reduce, 583, 584, p. 208 A
 table of, Table 62, explan. p. 421
Equator, def. 182
 days and nights equal on, 182
 celestial, 425
Equatorial instrument, p. 177, note
Equiangular triangles, 142
Equilateral, 87
Equinoctial, 182
Equinox, 463
Ericsson's lead, p. 153
Error, Total, of compass, 907, p. 334
Errors, effects of, in any computation.
See Degree of Dependence in this
case, p. 62
 of the D.R. p. 343
 of the time at sea, 973, 984
Establishment of the Port, vulgar, 921
 correct, 923
 is an interval, 937
Estimate angles, useful to be able to,
 492
Evolution, 70

F

FALCON, Captain, p. 108, note
Favos, p. 380 (1), and p. 825
Foejee Is. water clear, 1082-3
Feet, no. of in a sea mile, 186, p. 104,
 note, and Table 64A
 no. of, subtending 1', Table 9,
 explan. p. 387
 Danish, Dutch, &c., p. 380
Figure, useful to refer to, in the mind,
 167 (3)
 the, is the ground of the mathe-
 matical solution, p. 61 (3)
 shewing deduction of lat. from,
 mer. alt. 452
 shewing deduction of mean time
 from a star's hour-angle, 473
 shewing deduction of mean time
 from the sun's hour-angle, 478
 or digit, the last, 35
Figures of different tracks, 890
 used in tables, Pref. p. vii and
 viii
First meridians, 191 and p. 396

Fisher, remark on chronometers, p.
 191, note
 on observing the hazy disc of the
 sun, p. 194, note
 on lunar observ. p. 351, note
Fitzroy, Capt., additions to the sex-
 tant, 500
 remark on chrona. p. 192, note †
 chronometric measures, p. 261,
 note; see also p. 368
Fixed stars, p. 169, note *: principal,
 R.A. and declination of, Table
 63, explan. p. 421
 times of passing mer. Table 37
 explan. p. 410
Fleurieu, 1048
Flinders, 968, note
Fog or haze, observing in, 528, 539
 Fog-banks sometimes taken for land
 1044
Foreign charts, soundings how ex-
 pressed on, p. 925
 measures, p. 27-30
Forging ahead or astern, 968
Fractions, p. 1
 decimal, p. 6
 to convert vulgar into decimal, 32
 to convert decimal into vulgar, 34
French measures, p. 380, and Tables
 36, 37, explan. p. 413
Frigid zone, 211
Fuel, how symbolised. See b, p. 401

G

GAUTIER, observations of dip, 536
Geographical mile, p. 379; Table 64A
Geometry, defs. p. 21; problems, p. 24
Geometry, Theorems, p. 23
 George, Mr., sextant, 502
Gimbals, 217
Givry, M., remarks on refraction,
 p. 196, note
 on chronometers, p. 192, note †
Glasses, sand, 266
 should be often examined, 267
Globe, def. 90
 principle of rectifying, p. 161,
 note
Good Dead Reckoning, 962
Graham shoal, p. 365, note
Grant, Sir R., p. 249, note
Graves, Capt., p. 256, note
Great circle, def. 386, p. 56A
Great circle sailing, 336, p. 62A
 places on same side of equator
 337; do. on dif. do. 338
 includes the case of sailing on a
 meridian, 340
 gives the shortest distance, 336
 keeps the port directly ahead, 340
 projection on the chart, 386
 point of max. separ. in lat. 345
Alry's method of projecting, 388
Davis star azimuth tables, use of
 in projecting, p. 136
Godfray's chart and diagram, 389
Townson's diagram and table, 247
Greatest common measure, 8, note
Greek letters for stars, 568
Greenwich date, 481
 to find, without chron. 576
 by chron. 575
 refer to in crossing Pacific Ocean,
 pp. 354 and 406, notes
 M.T., correction of, for 2d diff. of
 lunar dist. Table 57, p. 419
Ground log, 265, note
Guépratte, 542, p. 178
Guns, sound of, from splitting of ice,
 1048
Gunter's scale not described in this
 work, Pref. vi

H

HACK watch, 564
Hall, Capt. B., index-error, pp. 182,
 356, note

Numbers in *Itaex* refer to the articles; unless prefixed by 'p', when page is indicated.

- Mall, Capt. D.,
observ. of the sea horizon, 536
observ. of planets, p. 556, note †
Hand lead, 399
Hartnup, Mr., p. 179, note
Heather on mathematical instru-
ments, p. 32, note
Heave of the sea, 961
Heeling error of compass, 256
how corrected, 256, p. 100
Height of eye, 305, 448 and 546
Height of land may be found by trial,
p. 388, note
is reckoned from H.W., p. 386
of tide, comput. of, 924
Herschel, Sir J., p. 169, note †
Hewitt, Capt., rating chron. at sea,
p. 294, note
High land, finding ship's dist. from,
355
by Lecky's tables, p. 143
alt. of, subject to variations, 207
High water, to find time of, roughly,
386, nearly, 388
Home, Sir E., 1034, p. 369
Horizon, sea, or visible, 304, Table 8
apparent places of, changes with
temperature, 208
from a boat, 358
place of do. in a fog, p. 191, note
is in the same state all round, 336
undulation of, indicates extror-
dinary refractions, p. 196, note*
refraction of, affected by shoals,
&c., p. 196, note*
rational, 431; distance of, p. 386
Horizontal parallax, 488, p. 165
of Moon, Planet, 588, Tables 40
and 48
Horn semicircle, or protractor, 108
useful in laying down points,
368
Horsburgh, pp. 351, 355, notes
instance of fallacious agreement
of lunar and chronom. p. 351,
note*
do. of erroneous lunar, p. 351,
note †
Hour-angle, def. 467
to find, from mean time, 609
of the sun, 609
by Spherics, p. 63A
Hour-angle, of the moon, 612
of a star, 611
from the alt. 612
from a doub. alt. p. 276,
note
from the azimuth, 616
from alt. and azim. 617
from changes of alt. near
the merid. 622
on passing the prime vertical, 618
Table 29, explan. p. 411
at rising and setting, 630
Hypothenuse, def. 39
made radius, p. 47 (3)
- I
- Ice, neighbourhood of, may be indi-
cated by temperature, 1049
chart, 1052
Ice islands, a danger, 1053
taken for land, 1045
danger of landing on, p. 368 (5)
decrease of wind near, 1052
drift of, 1053
blackness at night and in fog,
near, 1052
yields fresh water, but not always,
1054 (5), p. 369
Illusory appearances, 1043
Imbros, Mt., an example, 594
Index of a logarithm, 57
to print, 59
Index bar of a quadrant or sextant,
spring of, p. 152, note †
- Index error, 496
to measure, by the horizon,
496 (1)
by the sun, 496 (7)
Indian tides and tide tables, p. 340,
and note
Inspection, nature of, 167
Instruction réglementaire, &c., p. 192,
note †
Instruments of navigation, p. 63
nautical astron. p. 178
for drawing geometrical figures, 91
See Heather on p. 32
Interpolation, 50
note on mental, p. 215
for second differences, p. 214
Interval
of sid. T. to turn to M.T. 603
of M.T. to turn into S.T. 601
in a double alt. not to be cor-
rected for change of long. p.
364, note †
Inverse proportion, 53
Involution, 66
Iron, hard and soft, 227
magnetised by induction, 227
transient magnetism of, 227
permanent magnetism of, 227
used in adjusting compasses, 240
upright, 241
horizontal radially, 243
horizontal tangentially, 243
spheres, 243, p. 90
Flinders' bar, how used in adjust-
ing compasses, 247
Irradiation, 712
Islands, small, appearance different as
high and low water, 1060
Isosceles triangle, 87
Ivory's refract. p. 412, note
method of double alt. 757
- J
- JOHNSON, A. C., on Lat. and Long. 378A
Journal, ship's, 403 to 413
suggestions on, 413
ex. of man-of-war's, 413
Jupiter, planet, p. 170, note
R.A. and decl. to reduce, 595
observed by day, p. 354, note
long., by (satellites of), 578
- K
- KERGUELEN, Voyage, 1047
Kilometre, Table 37, explan. p. 413
King, Capt., p. 351, note
Knot, 260
Krusenstern, Admiral, p. 375
his Memoirs quoted, 1058
- L
- LA CAILLÉ, 542
Land, making the, 1029
when approaching, 1023
when to be set, 408
indications of, 1035
last point mentioned (Table 10),
position of given, p. 389
Latitude, def. 184
how deduced from the mer. alt. 452
is measured in miles, 186. See
Spheroidal Tables, 64A
diff. of, 188-9
is determined absolutely, 680
importance of, p. 243, note
reasons for introducing the sever-
al methods in this work, p. 243,
note
account, or dead reckoning, 354
errors of D.R. 964
in a double alt. p. 260, note
Finding by observation,
by Mer. alt. 681
of the sun, 682
of the moon, 693
of a star or a planet,
687
Latitude by Mer. alt.
Degr. of Dependence of this
method, 695
figures illustrating, p. 168
by Reduction to the meridian,
p. 249, p. 63A
by the sun, 699
by the moon, or star, or a pla-
net, 703
not near noon. See Double Alt.
p. 255, Degr. of Dependence, 704
by equal alts. near noon, 732
do. not near noon, 746
by Circummeridional alts.
by the sun, 706
by a star, pole star, or a planet,
713-717
by Double Altitude, p. 255
Degr. of Dependence, 730
by Alt. of the Pole Star, 717 and
p. 277
Latitudes and Longitudes of Places.
See Maritime Positions, Table 10
on transmitting corrections of,
1057
Lazarev, M., 547
Lead, 397, &c.; Massey's, 402
Degr. of descent of lead, 397
Lead-line, 399
when re-measured should be wet,
399, note
League, 199
Lecky's danger-angle tables, p. 143
Leeway, 303
to correct the course for, 418
should always be marked on the
log-board, 407
Leg of an angle, 81, p. 56A
Lighthouses, painted, p. 390, note
Lights, to make, p. 365, note
remarks on, pp. 403, 404
Lights, how shown on Admiralty
charts, p. 925
Limits of obs. and methods, p. 51
Log, ship's journal, 403 to 413, 351
heaving the, 229, 233; caution,
355
Massey's, 364; Walker's, p. 105
ground do, 265; attention to, 351
Log-line and lead-line, should be
wetted when measured, 363
line erroneous, 262
should be often examined, 263
Logarithm,
to find the, of a number, 38
to find the number corresponding
to, 59
to place the index, 38
Logarithmic difference, Table 73,
explanation, p. 428
to correct for bar. and therm.,
Table 73
to compute the, p. 429
Logarithmic sines, cosines, &c.
to half minutes, Table 68,
explanation, p. 424
derivation of these quantities,
from the log. sine, p. 425
sines to ten seconds, Table 67,
explan. p. 424
Logarithms, 56, &c.
arithmetical operations, by, 64, &c.
practical suggestions in using, 60
number of places to be used, 60
remarks on an abuse of, p. 214,
note
reasons for the number of places
given, Pref. viii
uses in trigonometry, 165
of numbers, Table 64, explan. p. 421
Log. sine, to convert into a propor-
tional log. p. 430
subtracting, use of log.
secant, &c., p. 45, note
square, Table 69; explan-
tion, p. 426, same as haversines
Longitude, def. 191
may be reckoned either E or W. 199

Numbers in Index refer to the articles; unless prefixed by 'p.' when page is indicated.

Longitude, how measured, 193
 diff. of, 194, 195
 is determined relatively only, 836
 by account or Dead Reckoning, 945
 is more correctly kept in low
 lat. 967
 correction by Table 1, p. 878A
 should be marked on chart for
 time of observation, 1007
 finding by observation, p. 297
 by chron. 827
 by lunar, p. 301
 by the moon's alt. 864
 to diminish the errors of this
 method, 866
 choice of results, 868
Degr. of Dependence, 869
 by an occultation
 of a star, 878
 of a planet, 878
Degr. of Dependence, 877
 by Jupiter's satellites, 878
 difference of, to d-terminis, 830
 particulars essential, 835
Longitudes of places, Table 10
 of first meridians, adopted on
 foreign charts, p. 395
 of secondary meridians, pp. 392-
 395
 telegraphic determination of,
 notes to, pp. 592-5
 by lunars and chron. mixed, no
 longer of value, p. 390
Loxodromic curve, p. 134, note †
Lubbock, Sir John, on tides, p. 335,
 note
Lunar distance, to correct, p. 308
 clearing the approx. methods,
 Pref. vii
 1st, inspection, 841
 2d, Logarithms, 844
 Rigorous method, 845
 special corrections of, 851
 elliptical disc, 852, and Table
 63, explan. p. 417
 spheroidal fig. of earth, 853
 inequality, of moon's motion, 856
 these corrections cannot all lie
 the same way, 859
 effect of error of 1' in, Table 58,
 explanation, p. 419
Lunar observation, determination of
 the long. by, 836
 in polar regions, 989
 Spherics applied to, p. 63A
 danger of trusting to one only,
 p. 351, note *
 mean of two not always correct,
 p. 351, note †
 by the sun, 847
 by a star or planet, 849
 finding the time at Greenwich,
 848
 computation of the alts. in, 863
Lunar tables, error of, 863
Lynn's Tables, p. 363, note

M

M and N. See *Spherical Trigonometry*
 Table 8, explan. p. 382
Maclear, Mr., long. of Madras, Pref. ix
Magnetic force, total, 233
 vertical, 233
 horizontal, 233
 horizontal, table of, 233, p. 53
 measuring, 234
 adjusting compasses by, 255, p. 98
 attraction, 235
 repulsion, 234
 induction, 235
Magnetism red and blue, 238
Magnets, used in adjusting compasses,
 239, 246
Magnetic bearings and courses, a no-
 tion for, p. 389
Magnitudes of the stars, p. 422, and
 note *

Making the land, 1029
Mantissa, p. 18, note
Maritime positions, arrangement, p.
 390, and Pref. viii
 heights given, p. 387, last par.
 abbreviations, p. 386
 given to 1', and tenths of 1', p. 388
 symbols denoting degree of pre-
 cision, p. 381
 do. description, p. 382
 secondary meridians, p. 391, &c.
 Table 10, explan. p. 387
Marquai's rulers, 91, note
Mars, R.A. and decl. to reduce, 594
 period, p. 189, note
Martin, Mr. K. B., observ. on refra-
 ction, 209
Maskelyne, Dr., p. 194, note
Massey's log, 284; lead, 403
Maximum separation, in lat., point of,
 345
Mean level of the sea, 920
Mean time, 475, p. 174
 how deduced from the motion of
 a star, 478 (4), p. 175
 how deduced from the motion of
 the sun, 478 (1)
 to convert into app. time, 636
 to convert into sid. time, 608,
 Table 23
Means, remarks on taking, 998, 1002-3
Measures, French and English, Tab. 37,
 p. 418
 foreign, reduction of, p. 379-381
*Mémoire sur l'Emploi des Chrono-
 mètres*, p. 192, note †
Mercator's Chart, 378, 379
 construction of, 391
 use, 380
 to find lat. and long. of a point
 on, 380
 to find the bearings between two
 places, 381
 to find the distance between two
 places (on the rhumb line), 382
 to find the ship's place on the
 chart by her course and dist. 384
 to lay off a point on the chart, 384
 projection of the voyage in a great
 circle, 386; Airy's, 388
 figures of different tracks upon,
 390
 charts of districts, 392
Mercator's sailing, 321
 is a perfect method, 321
 caution in high lat. 323
 selection of Mercator or Mid.
 lat. sailing, 330
Mercatorial Distances, Table 12, ex-
 planation, p. 406
Meridian, def. 183
 first, 191 and p. 395
 celestial, 436
 times of passing, p. 224
 of the sun, 623, &c.
 of the moon, 637
 of a star, 625, and Tables 27 and
 27A, explanation, p. 410
 sailing on a, is a case of great
 circle sailing, 340
 of 180°, crossing, pp. 354 and 406,
 notes
Meridian altitude is not the maximum
 alt., except of a star, p. 244,
 note †
 reduction to, 700; Tables for, 47,
 48, 49, and 50
 to find from decl. and lat. 663
Meridian distance. Hour Angle, 468
Meridians, secondary, Pref. x, 823, 825,
 and p. 388, 392
 denoted in Table 10 by small
 capitals, p. 388, par. 5
Meridional diff. lat. 322
Meridional parts, Table 6, explan. p. 375
 computation of, p. 386
 Methods of solution, 167
Mètre, Table 37 and p. 925
Middle latitude, 314

Middle lat. sailing, 312
 founded on par. sailing, 312
 has two cases, 313
 is not a correct method, 321
 may be made as correct as re-
 quired, in one case, 330
 is preferable to Mercator's sail-
 ing, in one case, 333
 estimation of error of, 331
 selection of, 330
 deduction of rules, 312
 old rule erroneous, p. 192, note
Milli-metre, Table 37, explan. p. 413
Minutes of arc, 75
 of Long. are not miles, p. 353
 note †
Moon, mean period of revolution or a
 lunation, p. 407, Table 14
 jointly with the sun produces the
 tides, 909
 age, to compute roughly, 932 (1)
 alt. remark in observing, 840
 to correct, 654
 correction of Table 39, explana-
 tion, p. 414
 long. found from, p. 319
 declination, to reduce, 589 and
 Table 22, explan. p. 409
 Right Ascension, to reduce, 591
 least and greatest variations of,
 591
 hor. parallax, to reduce, 588
 semidiameter, to reduce, 588
 too small, p. 315, note
 effect of error of her place, in a
 lunar, &c. 863
 merid. pass. to find, 637, and
 Table 28, explan. p. 410
 rising and setting, 637
 to allow for refraction and height
 of eye, 638

N

NADIR, def. 423
Names of places, differently given by
 different people, p. 389
Napier's curve for deviation of com-
 pass, 229
Napier's Lord, Rules for Spherics, p.
 57A
Natural sines, cosines, tangents, &c.
 Table 65, explan. p. 423
 scale on Admiralty Charts, p. 925
Navigating the ship, p. 347
Navigation, def. p. 56
 instruments of, p. 63
 of H.M. ships, Notes on, p. 376
Nautical Almanac, Hourly variation
 of elements in, 579-596
Nautical astronomy, pp. 62A-64A, 161
 instruments of, p. 178
Nautical Magazine, 1839
 discussion of longitudes in, Pref.
 p. viii, and p. 391
Nautical mile, 188, 199, p. 104, note,
 and Table 64A
Nearing the port, rate of, 288
Night observation, 541; should be
 practised, 977
Noon, obs. at, marked in log. 403

O

OBLIQUE angled plane triangles, 50A
Oblique circles, p. 56A
 Spherics, p. 58A-61A
Observations, on taking, with or with-
 out assistants, p. 201
 on a field of ice, 483

Numbers in Index refer to the articles; unless prefixed by 'p.' when page is indicated.

- Observer should take all parts of an observation himself, 563
should always be careful to observe accurately, 533
- Obtuse, 88, p. 34
- Oculitation, long, by, p. 322
- Olympus, Mt., example, difference of bearings on chart and globe, 594
- Orthography of names, p. 389
- Outer alt., the term, 723, 740 (3)
- Owen, Admiral Sir Edw. R., remark on double alts. p. 263, note
Adm. W. F. W., double alts. p. 366, note
the examples chiefly from his journals, Pref. vii
Captain R., remark on jumps of chron., p. 193, note
on changes of temperature on chron. 523, &c.
- P**
- PACIFIC OCEAN, change of day in crossing, pp. 354 and 406, notes
Pairing stars for lat. 716, 717
Pallurus, 218, p. 70
Palma, Dutch, p. 380 (4)
Paper, chart, distortion of, p. 146, note
Parallax in alt. 436
less as distance increases, 436
varies with the observer's lat. 437
of the sun, Table 34, expl. p. 413
of the planets, Table 48
of the stars, or annual, appreciable only in one or two cases, p. 169, note *
- Parallel circles, p. 55A
Parallel lines, 73, 93, 94, p. 22
Parallelism of the telescope in a sextant, 496 (3), Table 54
Parallelogram, 130
Parallel sailing, 301
may be used when the course is not due E. or W. 310
principles, 303-3
figure of track on the chart, 390
Parenthesis, in Table 10, use of, p. 389
Parry, Sir Edw., 536, 1052, p. 369
where wintered. See Table 10 (col. 141, 143, 144)
Passage of the meridian, p. 324
See Table 12, explan. p. 406
across Pacific Ocean, p. 354
round the world, pp. 354 and 406
Perpendicular, def. 88
methods of drawing, 96, 97
Personal equation, pp. 51, 54
Philips, voyage, 1046
Piedra, p. 380 (7)
Place of the ship is determined in two ways, 179
by Dead Reckoning, 984
by Observation, 974
remark on finding, 990
change of, how affects alts. 548
Places called by diff. names, p. 389
Plane chart, 392
Plane sailing, 271
Plane triangle, 87, note
Plane trigonometry, p. 44 to 51A
Planets enumerated, p. 169, note
observed best at twilight, 977
Pocket sextant, 486, George's, 503
Points of the compass, 76, 197
Polar angle, 770
circles, 311
distance, 448
Pole, 424
Pole-star, to find, 567
corr. of alt. Table 51, explan. p. 417
Port, rate of closing, 286
is kept right ahead on a great circle only, 340
Position of ship with respect to land, how determined, Chap. IV. pp. 137-143
on the chart, p. 361
on a line of bearing, 1006
- Position of ship, by two angles, 368 to 373
by altitude of high land, 353-366
by Lecky's tables, p. 143
Powers of numbers, 66, 67
of a telescope, 548
Practical geometry, p. 31
Pricking the ship off, 1004
Prime vertical, def. 428
time of passage
of the sun, 630
of the moon, 633
of a star or planet, 633
accurately, 634
altitude on the, 664
Problem, def. 73
Projections, properties of certain, 592
Proportion, direct, pp. 10, 11
inverse, p. 16
Proportional logarithms, Table 74, explanation, p. 429
remarks on, p. 430, note
Proportioning, in tables, p. 14, ex. 6, 7
Propositions of geometry, p. 33
of trigonometry, 168, p. 55A to 64A
- Q**
- QUADRANT, def. 79
the instrument, and sextant, 485
manner of observing with, 487
adjustments, 495
Quadrantal triangle, 56A, 56A
Quality of bottom, how shown on Admiralty charts, p. 924
Quicksilver horizon, 517
- R**
- RADIUS, 78, 164
of the trigonometrical tables is 1
log. of the, is 10, p. 48 (3 note)
Ramsey, Capt., pp. 353, 354, 406, note
Rate of chronom. 812
change of, detected on making the land, 830
Rate for less than 24^h, 832
See Chronometer
Rate of sailing, affected by various causes, 960
is estimated by seamen, nearly, p. 352, note
of current, 391
of nearing a port, 395
Rating the chronometer, 812
by observations on shore, 815, 825
by the absolute time, 816
by time signals, 818, and Table 13
by the longitude, 830
by intervals of time, 831
by diff. of long. 833
Ratio, 36
Reading off, 494
troublesome at night, 641
may be postponed, p. 188, note
Réaumur's therm. Table 36
Reduction of fractions, pp. 8, 9
of the astronomical elements to the Greenwich Date, 579-600
by hourly var. in *Nautical Almanac*, p. 208A
by proportional logs. 597
by special logs. 597
Reduction to the merid. 696
limits, Table 47, explan. p. 415
to compute at sea, circummeridional altitudes, 706
Tables 47, 48, 49, 50 and 70, explan. pp. 415 and 427
second do., Table 49, p. 416
value of, when 2d red. amounts to 1', Table 48, explan. p. 416
of lat. by obs. to geocentric latitude, Table 52, explan. p. 417
Reflecting circle, p. 185, note
use of, in observing two angles or altitudes, 514
Refraction, astronomical, 433
Table 31, explan. p. 412
varies with state of air, 433
- Refraction, corrections of, Table 32, 33, explanation, p. 412
is less for a depression, p. 222, note
tables of, adapted only to level of sea, p. 414, note
effect of, on figures of the sun and moon, 583
rising or setting in high lat. 633
on apparent amplitude, p. 167 (1)
lateral, 209
terrestrial, 207
Refreshments, how symbolised, r, p. 402
Rennell, pp. 353, 359, notes
Repeating reflecting circle, 506
noting the time in observations with, 506
effects of errors, 515
cross observation, 510
to observe two alts. 514
caution respecting the crooked handle, 507
Resolve, to, a distance made good in one direction upon another, 235
Results, combination of, 997
Retardation, Table 34, explan. p. 409
Revolving lights, note on the term, pp. 403, 404 note, and p. 923
Rhumb, def. 198; is not the direct course for the port, 340
Riddle, Mr., Long. of Madras, Pref. ix
Right angle, 84; right circles, p. 56A
Right ascension, def. 469; reduction of, p. 208A
to deduce from sidereal time, p. 208, 211, 421
Right Spherics, pp. 57A, 58A
Rising and setting, times of, p. 228
of the sun, 636, Table 36
of a star or planet, 637
effects of refract. and height of eye, 638
Roberts and Baird's Indian tide tables, p. 340, note
Rocks, whales taken for, 1046
Roof of artificial horizon should be reversed, 554
how to be placed, 519
to be used only when indispensable, 554
Roos, Sir John, p. 559, where wintered, Table 10 (col. 143)
Sir Jas. p. 183
Rollers, 1054
Rule of three, pp. 11, 16
Ruler, 91, to test a, 92
Rules, extent of the *rationale* admitted in this volume, Pref. xiv
involving many cases, are given in the form of tables, Pref. v.
- S**
- SABINE, Col., work quoted, p. 62, note *
on rating the chronometers, 823
Sailing directions, reference to, p. 347
Sailings, p. 106
to work by canons, 273
admit of two general cases, 270
See *Parallel*, *Mercator*, *Mid. Lat.*, *Great Circle*.
Saabes, p. 380 (11). (*Saïen*).
Saturn and satellites, p. 169, note
R.A. and decl. 596
Scales, common, 104
diagonal, 106
natural, p. 925
of chords, 106-7
to construct, 109
conversion of foreign thermometer, Table 86
Screens, or shades, in sextant, 491
eye ditto, useful, 491
Screws, caution respecting, 497
Sea, mean level of, 920
Seasons, reversed in south lat. 466
Sea rates of chronometers, p. 297
Sea-weed not a certain indication of land, 1038

Numbers in Index refer to articles; unless prefixed by 'p,' when page is indicated.

Secant, 155
to find, p. 425
Second of lat. is 101 ft. 186, Table 64A
Secondary meridians, Preface ix, 823, 825, and p. 388
are denoted in Table 10 by small capitals, p. 388
importance of establishing, p. 391
enumerated, Table at p. 393
take no symbols, p. 397
Second difference, 598, &c.
Table 25, explan. p. 400
of alt. 556
varies as the square of the interval, 558, p. 200, example
Seconds of time, useful to be able to count, 268; of arc, 75
Sector, 110. See Heather on mathematical instruments, p. 32, note
Semidircular horn protractor, for laying off angles, 108 and note
Semidiameter of the celestial bodies, 439
is less as the dist. is greater, 439
is greatest in the zenith, 440
Semimenstrual inequality, 924
for certain places, Table 15
Setting an object, 201
Sextant, 458-564, and p. 145
manner of using, 487
adjustments, 496
parallax of, p. 182, note
case or box for, p. 183, note *
methods of increasing efficiency, 400, p. 183, notes
caution against tormenting, p. 183, note
shades of, remark on using, 491
may produce errors, 499
Shallow water, variation of compass affected in, p. 72, and note
Ship, how magnetised, 244
magnetic forces of, 245
Ship's journal, p. 154-157
all matters relating to ship's place inserted, 413
Ship's change of place, how affects altitude, 548
Shoal patch, how symbolised, p. 399 (5)
Shore horizon, 549
Table 35, explan. p. 413
Short glass, 266
Sidereal day, 470
time, 471, p. 311, note, and Table 61
to convert into mean time, 607, Table 24; into Right Ascension, p. 309, 421
Sidereal time at noon, 477
to reduce, 585, Table 28
Sights, A.M. and P.M., should not be mixed, 816
Signals, time, Table 12, explan. p. 407
Signs and abbreviations, p. 10, note
or symbols, attached to places, p. 396
on Admiralty charts, p. 924
Signs of the Zodiac, 460
Similar triangles, 147
Sine, def. 152, 163, and p. 426
diff. of do. and arc, p. 385, note †
Small circle, 336, p. 180
Smyth, Adm. W. H., pp. 367, 373, note
Solar day varies, 476
Solstice, 464
Solutions, two classes admitted in this work, Pref. vi.
methods of, pp. 50-54
all in this work by inspection and logarithms, Pref. p. vi
by assumption, p. 51, note
Sound, velocity of, 563
affected by wind, 563
Sounding, Chap. VI, p. 151
in deep water, 401
instruments for, 402
omitting to sound, *inexcusable*, 1043
Sounding, Sir W. Thomson's machine for, 402, p. 153

Soundings, the only unequivocal sign of land, 1043
ship sometimes conducted by, by night or in fog 397
how symbolised in Table 10. *See* Depth, p. 401
on Admiralty charts, p. 924
Angles for verifying, 368
on foreign charts, how expressed, p. 925
Southing, an inefficient term, p. 341, note †
Sphere, def. 90, p. 55A
stereographic, projection of, p. 56A
sections of, p. 55A
Spherics, p. 55A to 64A
application to Nautical Astronomy, p. 62A-64A
circular parts, p. 56A
great circles, p. 55A
Napier's, Lord, rules in, p. 57A
oblique, p. 58A-61A
oblique circles, p. 56A
parallel circles, p. 56A
poles of circles, p. 55A
primitive circle, p. 56A
quadrantal triangle, p. 56A, 58A
right, p. 57A, 58A
circle, p. 56A
small circles, p. 55A
spherical angle, p. 56A
triangles, p. 56A
Spherical Traverse Table, Table 5, explan. p. 389
triangle, 386, p. 56A
Spheroidal Tables, 64A, explan. p. 433
Square, def. 135
Square of a number, 67, 68
to a small arc, p. 407 (explan. of Table 56)
Square root, to extract by logs, 71
Squares of certain numbers, given in Table 8, explan. p. 418
Standard compass, 224
Stars, fixed, note upon, p. 169
finding the, p. 203-205
list of principal, Table 63, p. 421
Astrum Tables, p. 184, 242, 330
magnitudes, p. 422, note
rise earlier every night, Table 37
how identified, 568
observing alt. of, at sea, 541
obs. in twilight, 977
times of merid. pass. Table 37, explan. p. 410
remark on the necessity of observing, 977, p. 349, note
Station-pointer, p. 143, note
Statute and geograph. miles, p. 379, and Table 64A (1)
Steam-vessels adapted to sounding in great depths, 401
dist. by log. too great, 963
Stores, places where obtained, p. 634, Table 11
Straight line, drawing, 91, 92
Stream of wind, advantage of working in, 299
Submarine volcanoes, p. 389
Subordinate computations, p. 205
Subtend, 83
feet subtending 1', Table 9, explan. p. 387
Sullivan, Comm., p. 362, note
Sumner's method, 1009-1014, p. 64A
Sun,
figure elongated, 209
jointly with the moon, produces tides, 910
dipping, p. 344 note
altitude, caution in observing, 490
to correct at sea, 647
accurately, 649
declination, Table 60, expl. p. 420
to reduce at sea, 679,
and Table 19, explan. p. 408
accurately, 580

Sun,
right ascension, Table 61, explan. p. 421
to reduce, 581, 582
parallax and semid. Table 34, explan. p. 418
semid. variation of, proves change of his distance, 439
rising and setting, time of, 636, Table 36
to allow for refraction and height of eye, 648, Table 38
difference of, at the base and summit of a mountain, 638
Supplement, 86
Surveying not treated in this work for reasons stated, Pref. x
Swedish feet, p. 381 (16)
Swell, how noted, 410
is marked in the log, 410
Swinging ship, 224
Symbols of determination, attached to places, p. 396
of description, pp. 396 and 924

T

TABLES, list of, p. xxii; remarks in taking quantities out, 50
to supply the place of *Nautical Almanac*, p. 430
principles of the arrangement stated, p. 377, note
danger-angle, *Lecky's*, p. 143
Tangent, def. 154
to find, p. 378
Telegraphic determinations of longitude, notes to pp. 392-396
Telescope of sextant, powers used, 543
remark in using, 542
raising or lowering alters brightness of image, p. 308, 4th par.
tubes may be scored or marked, 492, p. 180
error of parallelism, 495 (3), Table 54, explan. p. 418
Temperate zone, 311
Temperature of sea not a sure sign of land, 1038
may (?) indicate ice, 1038
may denote change of wind, 1039
alters apparent place of sea horizon, 308
Terrestrial refraction, 207
Theorems, 113-149
of geometry, p. 33-43
Theory, remarks on, Pref. xi
notice of the volume devoted to, Pref. xi
Thermometers, scales, Table 26, p. 413
Thomson, Sir W., compass, 216
sounding machine 402
Tide, age of, 919
current 917
height of the, 918
observations, p. 344
wave, 915
and half-tide, p. 408, note
Tides, p. 335
causes, 910
diurnal inequality of, 340
superior and inferior, 911
spring and neap, 912
highest, 918
causes of irregularities, 914
how noted on Admiralty chart, pp. 924, 925
proper treatment of the subject very difficult, Pref. x
Time, measures of, 470-480
to convert into arc, 570, Tables 17, 18; also 68 and 69
figures shewing manner of computing, p. 172, 174
accuracy of, at sea, 984
variation of, at sea, p. 336
change of, in voyage round the world, 970 and note, p. 406, note

Numbers in Index refer to articles; unless prefixed by 'p,' when page is indicated.

- Time, account of, most correctly kept in low lat. 973
to find by observation, p. 278
by alt. of the sun, 780
of the moon or a planet, 784
of a star, 783
choice of results, 787
by equal alts. p. 287
by change of alt. near the meridian, p. 288
from double alt. p. 289, note
Time-ball, 818, Table 12, explan. p. 407
Times, conversion of, p. 216
Toises, p. 280 (8)
Tormenting the sextant, caution against, p. 183, note
Torrid zone, 210
Total error of compass, 907, p. 234
Towson, Mr., Tables, p. 136, and note
do. for red. p. 416, note
Tracks, figures of different, 390
Traité de Géodésie, p. 151, note
Transit, def. 453
bearings, 1089, p. 376
Transit of Venus expeditions, determinations of longitude from, notes on pp. 392, 396
Traverse, to work a, 287
Traverse sailing, 386
Traverse Table 1, explan. p. 377
use of, in proportioning, p. 379
in right-angled triangles, p. 378
in reducing measures, p. 379, 380
in correcting longitude, p. 378A
Triangle, 87
Trigonometrical canon, 111
Trigonometry, terms of, pp. 44, 160-167
propositions of, p. 46
rules for use of, 163
spherical, p. 55A-64A; plane, 50A
Tropic, 210
Tropical year, 465, and note
Troughton's circle, p. 186, note
caution against tormenting the sextant, p. 183, note
True alt. to reduce to app. 687
course to reduce to compass, 225-230, p. 169
Tube, plain, of sextant, use of, 543
Twilight, 434
- U
UNITED STATES' exploring expedition, 209, 547, 1084
height of waves, 547
telegraphic determinations of longitude, notes to pp. 322-398
- V
VANCOUVER, p. 392
Varas, p. 381 (14)
Variation of time at sea, p. 354
of the compass, 219
change of, in England, 219, p. 71
chart of, 219, p. 71
affected by ground in shallow water, 220, and note
to find by amplitude, 884
azimuth, on the meridian, 890
from short double alt. 891
from equal altitudes, 897
on the prime vertical, 898
from altitude, 900
from time, 902
by astronomical bearing, 903
remarks on the term "Variation," 907
to correct courses and bearings for, 221, p. 159
Variations, daily and 12-hourly, Table 21, explan. p. 408
Venus, period, p. 169, note
observed by day, p. 356, note
inaccuracy in lunar dist. note, p. 311
declination, to reduce, 593
R.A. to reduce, 592
determinations from transit of, pp. 392-396
Vernier, 494
Versts, p. 369 (12)
Vertex of the great circle, 244
Vertical danger-angle, Lecky's tables, p. 143
Vessels, in a sea, acquire a tendency to move ahead or astern, 963
abandoned, 1063
- Vidal, Capt., Gulf of Guinea, pp. 192, 193, notes †
Views, should accompany hydrographic notices, 1060
Vrangel, Baron, 1034 (5), p. 369
Vulgar fractions, p. 1
- W
WALKER's taffrail log, p. 106, note
Water, procuring, p. 366
Waves, height of, 547, and note
Weather, notation of, 409
Weddell, voyage of, 1045
Westing, 300
Whales taken for rocks, 1046
Whewell, Dr., p. 324, note
Whole numbers, remark on working to, 35
Wickham, Capt., p. 356, note
Wilkes, Lieut., United States Navy, expedition of, quoted. 209, 547, 1054
Wind, figures denoting force of, 409
change of, sometimes denoted by temperature of the sea, 1039
strength of, affected by ice, 1059
Winds not treated in this work, Pref. x
Working to accuracy, remarks on, Pref. vi
Workman, *Navig. Improved*, p. 123, note
Wrangel, Baron, 1034 (5), p. 369
Wrecks, floating, 1053
- Y
YEAR, civil, 465
commencement of, p. 174, 171
note
- Z
ZERRA, H.M.S., p. 189, note
Zenith, def. 423
distance, 431
how named, 448
Zodiac, 460
Zone, 210, 211

LIST OF NAUTICAL WORKS

PUBLISHED BY

J. D. POTTER.

LIST OF NAUTICAL WORKS

PUBLISHED BY J. D. POTTER.

ADMIRALTY CHARTS.

On the Correction of Charts, Light Lists, and Sailing Directions; s. d.
and a Short History of the Hydrographic Department of the British Admiralty. *No charge.*

Official Catalogue of Charts and 22 Index Charts. *No charge.*

At Board of Trade inquiries reference is frequently made to the subject of charts and sailing directions. It is doubtful, however, if the general public has the remotest idea of the vast number of charts, plans and sailing directions which have been brought into existence by the cartographer. The making of charts is a never-ending task, for the simple reason that new dangers to navigation in the way of uncharted rocks and shoals are constantly being reported. Some conception of the amount of work done is afforded by the catalogue of Admiralty charts, plans and sailing directions issued by Mr. J. D. Potter, of 145, Minories, E.C. The volume, which is published by order of the Lords Commissioners of the Admiralty, consists of 260 pages, index charts, &c., and may be obtained gratis from Mr. Potter.--*Shipping Gazette and Lloyd's List*, May 7, 1909.

ALTITUDE TABLES.

Computed for Intervals of Four Minutes between the Parallels of Latitude 31° and 60° and Parallels of Declination 0° and 24°, designed for the Determination of the Position Line at all Hour Angles without Logarithmic Computation, by *Frederick Ball, M.A. (late Scholar of Exeter College, Oxford), Chaplain and Naval Instructor in His Majesty's Fleet* ... 15 0

Ditto, ditto, between the Parallels of Latitude 0° and 30° and Parallels of Declination 0° and 24° ... 15 0

Ditto, ditto, between the Parallels of Latitude 24° and 60° and Parallels of Declination 24° and 60° ... 15 0

Altitude and Azimuth Tables, for Facilitating the Determination of Lines of Position and Geographical Position at Sea. The simplest and readiest in solution. Spherical Traverse Tables for solving all problems of navigation. By *Lieut. Radler de Aquino (Brazilian Navy)*. All sights for position are worked out by the same method *without logarithms*, with hardly any calculation. All the other problems in navigation are easily and rapidly solved by inspection without interpolation. This work has received the favourable endorsement of the United States Hydrographic Office. Stereotyped Edition... 10 6

ARTIFICIAL HORIZON.

Description of an Artificial Horizon, invented by Capt. A. B. Becher, R.N., with examples of its application, afloat and ashore (1857) ... 1 0

List of Nautical Works published by J. D. POTTER.

AZIMUTHS.

s. d.

- Davis's Sun's True Bearing, or Azimuth Tables** (30° N. to 30° S.), by *J. E. and Percy L. H. Davis*. The only means of ensuring a correct course at sea is by the use of calculated or tabular azimuths, and the latter render the operation speedy and accurate. These tables, an addendum to those of Capt. Burdwood, R.N., which preceded them, have been in very general use since their publication. The instructions in several European languages for their use have proved of great service to foreign seamen ... 10 6
- Davis's Supplementary Azimuth Tables** (now published separately). The Time Azimuth Tables in general use do not often give azimuths near the meridian, which are in frequent demand for ex-meridian observations, but they will be found in this book, in addition to complete tables extending to latitude 64° ... 8 0
- Davis's Star Azimuth Tables**, computed for all latitudes between 60° North and 60° South, by *P. L. H. Davis*. This book has followed on the very general adoption of stellar observations as a means of navigation, and supplies the seaman with the same details regarding stars, as he can get from "Burdwood and Davis" when the sun is concerned. Some ingenious altitude marks are used for the first time in these tables which materially aid in the identification of any hastily observed star, as to which doubt may exist ... 10 6
- Short, Accurate, and Comprehensive Altitude-Azimuth Tables** to show the true bearing of the Sun, Moon, Planets, &c., for latitude 0° to 75° north or south; altitudes 0° to 75° ; and declination 30° north to 30° south; also the Approximate Ship Time, by *A. C. Johnson, R.N.* (Published by request) ... 3 6
- Time Azimuth Diagram**, by *Hugh Godfray, M.A.* ... 3 0
- Captain Weir's Azimuth Diagram** ... 1 6

BOATS.

- A Review of the New Methods of Lowering and Disconnecting Boats at Sea**, with a proposed Amendment (1857), by *Capt. Kynaston, R.N., C.B., &c.* ... 1 6

CHRONOMETERS.

- Davis's "Chronometer" Tables**; or, hour angles for selected altitudes between latitudes 0° and 50° , with variations for 1' in all elements, by *P. L. H. Davis*. Means of working a Sun "Chronometer" arithmetically have been for many years a desideratum, and have been published, in 1793, by Lalande; in 1827, by Lynn; and by Hommey, in 1863; but Mr. Davis, by the omission of useless or undesirable altitudes, and the inclusion of Variations in 1' of Altitude, Latitude, and Declination, has made a table of great practical utility. The book, as a substitute for or a check on logarithmic calculation, is almost a necessity, and is especially useful in latitudes less than 45° . A comparison has been made in actual work of the tabular results with those obtained in the ordinary way, showing practically identical results ... 10 6
- Notes on the Management of Chronometers and the Measurement of Meridian Distances**, by *Rear-Admiral Charles Shadwell, F.R.S.* (1861) ... 4 6

COLUMBUS.

- The Landfall of Columbus on his First Voyage to America**, with a Translation of The Baron Bonnefoux's History of his previous life, also a Chart showing his Track from the Landfall to Cuba, and an outline of his subsequent voyages (1856) ... 12 0

List of Nautical Works published by J. D. POTTER.

COMPASS.		s. d.
An Explanation of the Adjustment of Ships' Compasses , illustrated with numerous diagrams, by <i>Commander L. W. P. Chetwynd, R.N.</i>	2	0
Handbook to Beall's Compass Deviascope , by <i>Captain George Beall</i> , contains, in addition to a complete explanation of this well-known instrument, much information necessary to compass correction	1	6
Elementary Manual for the Deviations of the Compass in Iron Ships , intended for the use of Seamen of the Royal Navy and Mercantile Marine, and Navigation Schools, by <i>E. W. Creak, C.B., F.R.S., retired Captain, R.N.</i> ...	6	6
Practical Information on the Deviation of the Compass , for the use of Masters and Mates of Iron Ships, by <i>J. T. Towson, F.R.G.S.</i>	4	0
AND		
Supplement to the above ; being the Questions on the Deviation of the Compass issued by the Board of Trade for the Examination for Masters' and Extra Masters' Certificates, and Answers to the Questions, by <i>Capt. William Mayes, R.N.</i> ...	4	0
The Pocket Compass Corrector . Makes an error in applying variation and deviation almost impossible	2	0
The Binnacle Compass , Corrected by itself, or the Deviation found with one Compass by both methods, and the Corrections applied, by <i>Capt. A. B. Becher, R.N.</i> ..	1	0
The Storm Compass , or Seaman's Hurricane Companion, containing a familiar explanation of the Hurricane Theory, by <i>Capt. A. B. Becher, R.N.</i> , illustrated with Diagrams and Accounts of Hurricanes	1	6
Plain Deviation Curve Diagram , by <i>Captain J. C. Robinson</i>	0	6
COOKERY.		
Ship's Cook and Steward's Guide , containing Hints for Management, and Two Hundred and Fifty Recipes, by <i>James B. Wilson</i>	1	0
CRUISE.		
Cruise Round the World of the Flying Squadron, 1869-1870, under the command of <i>Rear-Admiral G. T. Phipps Hornby</i> (illustrated), and Chart showing its Track ...	21	0
CURRENTS (See Tides).		
DEVIATION (See Compass).		
DOUBLE ALTITUDES.		
A Method for finding the Latitude by the Simultaneous Altitudes of Two Stars , by <i>Capt. Burdwood, R.N.</i> (reprinted 1896)	1	0
EQUAL ALTITUDES.		
Tables for Facilitating the Method of Equal Altitudes , by <i>F. A. L. Kitchin, B.A., Naval Instructor, R.N.</i>	1	0
EX-MERIDIANS.		
Davis's Ex-Meridian Tables and Supplementary Azimuths , by <i>P.L.H. Davis</i> . This important work is now complete. It contains Calculated Reductions to the Meridian for hour angles less than 75° and altitudes lower than 84°, Declinations and Latitudes 34° and 64° N. and S. The use of the book is quite easy to anyone familiar with the Azimuth Tables. The Supplementary Azimuths, which accompany it, give bearings too near the meridian for inclusion in "Burdwood and Davis," which are now in great request for position lines and ex-meridian work	10	6
Tables for the Reduction of Ex-Meridian Altitudes , by <i>J. T. Towson, F.R.G.S.</i> ..	1	0
Ex-Meridian Diagram , by <i>F. A. L. Kitchin, B.A., Naval Instructor, R.N.</i>	1	0
GREAT CIRCLE SAILING.		
A Chart of South Latitudes , beyond 20 degrees, to facilitate the practice of Great Circle Sailing; with an accompanying diagram for the determination of the courses and distances, by <i>Hugh Godfray, M.A.</i>	3	0

List of Nautical Works published by J. D. POTTER.

HOUR ANGLES.

	s.	d.
Hour Angles of the Sun, Moon, and Stars, for Latitude and Declination 0°-80°, and Altitude 5°-64°, together with Short Methods of finding the Longitude by Chronometer; and the Latitude and Longitude by Two "Chronometers," by A. C. Johnson, R.N.	8	6

HYDROGRAPHICAL ENGINEERING.

An Essay on Hydrographical Engineering, as applicable to Floating Sea Barriers, Harbours, Batteries, Coast Defences, and Naval Fortifications, by Capt. Adderly Sleigh, K.T.S., F.R.S.L. (with Illustrations), (1859)	10	0
---	----	---

INTERPOLATION.

Notes on Interpolation, Mathematical and Practical, by Rear-Admiral C. Shadwell, F.R.S.	2	0
---	---	---

LATITUDE AND LONGITUDE.

On Finding the Latitude and Longitude in Cloudy Weather and at other Times, by A. C. Johnson, R.N. Greatly enlarged to 56 pages, with Appendix and Part II.	5	0
Short Tables and Rules for finding Latitude and Longitude, by Single and Double Altitudes, Pole Star, Lunars, &c., by A. C. Johnson, R.N.	3	0
Scales of Latitude from 5° to 60° proportional to a scale of Longitude, where $\frac{1}{2}$ in. = one mile, arranged to facilitate the finding of position from two Sumner lines, by R. E. Peake, A.M.I.C.E. per set	5	0
Charts to accompany above each	2	6
Tables showing the Length in Feet of a Degree, Minute, and Second of Latitude and Longitude, with the corresponding number of Statute Miles in each Degree of Latitude; and the number of Minutes of Latitude or Nautical Miles contained in a Degree of Longitude, under each Parallel of Latitude, by R. C. Carrington, F.R.G.S. (1868)	1	0

See also **Double Altitudes, Equal Altitudes, Ex-Meridians, Hour Angles, Lunars.**

LAW.

Admiralty Procedure against Merchant Ships and Cargoes, &c., in the High Court of Justice and in County Courts, showing the various matters as to which proceedings in Admiralty can be taken, and the mode of commencing action, &c., by R. G. M. Browne, the Admiralty Marshal (1889)	10	0
Handbook on the Law and Practice relating to Apprentices to the Mercantile Marine Service, by F. W. Gardner (of the Middle Temple)	1	6
The Statute Law of Merchant Shipping, comprised in an alphabetical Analysis, and a Summary of the unreppealed Merchant Shipping Acts, from 1821 to 1888, by R. G. M. Browne, the Admiralty Marshal (1889)	6	0

LIGHTS.

Lights in Lyrics, or a Glance at the Channel Lights as Piloting Marks, on a run from Scilly to the Nore, accompanied by a Parting Precept on Compass Deviation, addressed to all younger Mariners. With a view of the Caskets, Notes and Charts. (1859)	1	0
---	---	---

Davis's Requisite Tables (Logarithmic), by <i>P. L. H. Davis.</i> Tables of	a. d.
Logarithms to five places of decimals only, for practical use. The typography	
and arrangement of the book will render it suitable for habitual use, and it contains	
a table of Logarithmic and Natural Haversines specially designed for modern	
navigation	7 6
Davis's Five-Figure Logs and Anti-Logs, by <i>P. L. H. Davis.</i> Specially pre-	
pared for use in Actuarial and General Calculations. These tables are very legible	
and do not fatigue the eye in use.	5 0
Ditto ditto with Index Tabs... ..	6 0

Notes on the Reduction of Lunar Observations, Mathematical and Practical, by *Rear-Admiral C. Shadwell, F.R.S.* (1881) ... 4 6
See also Latitude and Longitude.

Tables of Mast-Head Angles, for five feet intervals, from 30 to 280 feet, and varying distances from a cable's length to four miles, with their application to Nautical Surveying; also the determination of distance by sound, with an example... .. 20

Foreign Measures and their English Values , compiled from Official Sources, by R. C. Carrington, F.R.G.S. (1864)	7 6
--	-----

A Voice from the Quarter-Deck on the State of our Mercantile Marine, by <i>Joseph Mayne</i> (Master Mariner) (1876)	1 0
An Address delivered to the Boys of the Training Ships "Chichester" and "Arethusa," by <i>G. M. Coshead</i> (1885)	0 4

Solectrics; a theory explaining the causes of Tempests, Seismic and Volcanic Disturbances, and how to calculate their time and place. Illustrated by over 100 di grams,	<i>by Alfred J. Cooper, Navigator, King's Medallist</i>	10 0
The Causes of Weather and Earthquakes (with four Diagrams),	<i>by Alfred J. Cooper (1902)</i>	2 0
Light as a Motive Power, a Series of Meteorological Essays (1875),	<i>by Lieut. R. H. Armit, R.N.</i>	15 0

Inman's Nautical Tables. A New Edition of this standard work, revised and brought thoroughly up to the present date, by the <i>Rev. William Hall, R.N.</i> , and containing all the aids to rapid fixing of position which are essential in modern Navigation	16	0
Lectures on Elementary Navigation , by <i>Rev. J. B. Harbord, M.A.</i> (<i>Retired Naval Instructor, R.N.; late Inspector of Naval Schools, Admiralty; Examiner in Navigation and Nautical Astronomy for the Department of Science and Art; Author of "Glossary of Navigation"</i>)	7	6
An Introduction to the Practice of Navigation and Nautical Astronomy , by <i>R. E. Hooppell, M.A., F.R.A.S.</i>	3	6
The Practice of Navigation and Nautical Astronomy , complete with tables, by <i>Lieut. Raper, R.N.</i>	16	0
Nautical Tables , by <i>Lieut. Raper, R.N.</i>	10	6
Navigation , intended for Self-Instruction up to the Second Mate's Examination, by <i>William Rou</i>	0	6

List of Nautical Works published by J. D. POTTER.

NAVIGATION—Continued.		s. d.
Practical Coastal Navigation , with numerous charts and diagrams, by <i>Count de Miremont</i>	4	0
Navigation Simplified , by a System of Teaching based on First Principles, for Officers (from 2nd Mate to Extra Master) in the Mercantile Marine and Yachtsmen. Illustrated by numerous diagrams, by <i>Captain P. Thompson, F.R.A.S., Younger Brother of the Trinity House, Senior Examiner of Masters and Mates, and Secretary to the Local Marine Board of London</i>	12	0
Examination Diagrams Simplified , for Navigation Students; illustrated by sixteen diagrams (including 5½ inch Boxwood Scale), by <i>Captain P. Thompson, F.R.A.S.</i>	2	6
Nautical Astronomy Made Easy , by <i>A. C. Johnson, R.N.</i> All the Rules being worked by a Small Table on One Page, designed to economise Time and Labour ...	3	0
REVERSIBLE TRANSIT INSTRUMENT.		
Notes on the use of the Portable Reversible Transit, and the Method of Calculation of the Observations , with diagrams and photographs, by <i>Capt. C. E. Monro, R.N.</i>	3	0
ROYAL NAVY.		
Chart of the Navy of Great Britain, from the Earliest Period of History , compiled from Historical publications, old records, Parliamentary returns, and other authorities, by <i>Frederick Perigal (of the Admiralty), 1860</i>	3	6
RULES OF THE ROAD.		
The Rules of the Road at Sea , comprising the Regulations for preventing collisions at Sea, 1897, and Rules in force in Harbours, Rivers, and Inland Waters; with explanatory notes and observations, by <i>H. Stuart Moore, of the Inner Temple and the Admiralty Court, Barrister-at-Law. (Third Edition)</i>	7	6
Diagrams, with Explanations, Illustrating the Rule of the Road for Sailing Ships , by <i>Capt. H. S. Blackburne</i>	2	0
SAILING DIRECTIONS.		
Yacht Cruising , illustrated with drawings and sketches, by <i>Claud Worth.</i> (This book consists partly of "logs" of cruises and partly of articles and notes on various matters connected with cruising)	7	6
Correct Magnetic Courses and Distances, from and to Various Ports round the British Isles , by <i>Arthur Underhill, LL.D., Commodore of the Royal Cruising Club, assisted by several Members of the Club. Second Edition</i>	2	0
Concise Navigating Directions for the River Thames , including all the Pools, Reaches, and Channels, from London Bridge to the South Foreland and Orfordness, and for the English Channel to Beachy Head; also for the Port of Dunkerque and the approaches to the Scheldt, by <i>Stephen Penny, Trinity Pilot, Gravesend</i> (illustrated by nineteen Charts)	7	6
East Coast Rivers. Charts and Sailing Directions for the Rivers Roach, Crouch, Blackwater, Colne, Stour, Orwell, Deben, Ore and Alde; together with General Charts from the Thames to Southwold , by <i>Lieut. S. V. S. C. Messum, R.N.</i>	5	0
The Pilot's Guide for the English Channel (with which is now incorporated "The Pilot's Handbook for the English Channel" by Staff Commander J. W. King, R.N.), comprising the South Coast of England, and general directions for the Navigation of the Channel; with numerous Charts and Plans of Harbours, edited by <i>H. D. Jenkins, F.R.G.S.</i>	7	6
A Chart of the Dutch Waterways , by <i>J. & A. B. Powell</i>	4	0
Notes on Cherbourg (Geographical and Historical description of, &c.), and Chart (1858), by <i>Commander Bedford Pim, R.N., F.R.G.S.</i>	1	0
From Calcutta to Bombay Coasting , being the Second Edition of the Handbook to the Ports on the Coast of India between Calcutta and Bombay, including Ceylon and the Maldivé and Laccadive Islands, with 11 Charts and 12 Photographs, by <i>Lieut. H. S. Brown, R.N.R., Port Officer, Marine Department, Madras Presidency.</i>	10	0

List of Nautical Works published by J. D. POTTER.

SAILING DIRECTIONS—Continued.

	s. d.
Winds and Currents of the Mediterranean , by <i>Capt. A. B. Becher, R.N.</i> , with remarks on its Navigation at different Seasons of the Year, compiled from various authorities, chiefly Spanish (1864)	3 0
Navigation of the Atlantic Ocean , by <i>Capt. A. B. Becher, R.N.</i> , with an account of the Winds, Weather and Currents found therein throughout the year (with Charts) (1892).	5 0
Navigation of the Indian Ocean, China and Australian Seas , by <i>Capt. A. B. Becher, R.N.</i> , with an account of the Winds, Weather, and Currents found therein throughout the year (with Charts) (1864)	5 0
Chart of the Sulina Branch of the Danube (European Commission of the Danube), surveyed by Robert Hansford, Surveyor of the Commission, under the direction of C. A. Hartley, Engineer in Chief (showing 45 nautical miles of the River from Sulina), size 10 ft. x 2 ft. 3 in. (1860)	20 0

SAIL-MAKING.

Remarks on Rigging Ships with Flat Surface Sails , by <i>Lieut. William Congalton, R.N.R.</i> (1865)	2 0
--	-----

SALVAGE.

Salvage Operations. The floating of H.M. Battleship "Howe." Illustrated by 23 plans and photographs, by <i>Rear-Admiral G. T. H. Boyes, late Flag-Captain H.M.S. "Anson"</i> (1900)	5 0
How Ships are Lost, and How to Save Life and Property at Sea (Illustrated), by <i>W. P. B. Manser</i> (1877)	1 0

SEAMANSHIP.

Under Square Sail , by <i>Capt. Withers</i> (1898)	2 0
Under the Red Ensign; or, "Going to Sea," by <i>Thomas Gray</i> (1892)	1 6

SEXTANTS.

Course and Position by Sextant Observations of two known Objects , by <i>Lt.-Col. English, late R.E.</i>	0 6
Captains' and Officers' Bridge or Poop Companion. Tables for finding the distance of an object at sea by inspection (without the use of pencil or paper), at the same time giving the distance the ship will go wide of the object before getting to it, and the course to steer to obtain a required distance. The above gives, with the aid of a compass only, the distance of a moving ship from any fixed object. By <i>A. Hütteroth</i>	2 6
Stars and Sextants. Star Distance Tables for facilitating the use of Lord Ellenborough's method of Correcting the Centring and Total Errors of Sextants at Sea, by <i>John Abner Sprigge, Wm. Fraser Doak, M.A., F.R.A.S., T. Charlton Hudson, B.A., F.R.A.S., of H.M. Nautical Almanac Office, Admiralty, and Arthur S. Cox, B.Sc., A.R.C.S.</i>	2 6

SHIPPING.

Historical Notes on Shipping , by <i>P. L. Isaac, M.I.N.A.</i> (1879)	1 0
---	-----

List of Nautical Works published by J. D. POTTER.

SIGNALS.

	s.	d.
Signal Cards—British System , with Plates, containing Instructions for Semaphore by Day , and with the Morse Code by Day or Night , together with the principal "Urgent" Light or Sound Signals, in accordance with the New Code. Also, Sheet of New Code Flags (34 Flags, coloured). Compiled by <i>J. Whitley Dixon</i> (<i>Retired Captain, Royal Navy</i>). (Size, $24\frac{1}{2} \times 19\frac{1}{2}$) 1 6		
Ditto ditto mounted on thick card 2 0		

SPEEDS.

Speed and Consumption of Steam-Ships , with Algebraic Formula for Economical Speed, and Rules for calculating the alterations in Draught and Trim corresponding to Changes in Displacement, and for using the Hydrometer to estimate those due to Differences in the Specific Gravity of the Water; for use in the Royal Navy and Mercantile Marine; by <i>J. F. Ruthven, Master Mariner, late Lieut. R.N.R., Assoc.Inst.N.A., M.R.U.S.I., Younger Brother of the Trinity House, F.R.G.S.</i> ... 2 0		
Speed Tables , for finding the distance run in a given time at a given speed, between the limits of 10 to 18 knots, by <i>J. D. Macpherson</i> (<i>Pacific Steam Navigation Co.</i>) ... 1 0		

STARS.

The Bearings of the Principal Bright Stars of greater declination than 23° north or 23° south; also those of the Moon and Planets when similarly situated, by <i>A. C. Johnson, R.N.</i> (Published by request) 8 0		
Pole-Star Latitude: a Method of Finding the Latitude from an Altitude of the Pole Star , by <i>Darnton Hutton</i> (<i>Master Mariner</i>), <i>B.A., M.Inst.C.E.</i> 1 0		
Position-Line Star Tables . A new and simple method of fixing ship's position by observations of stars near Meridian and Prime Vertical without logarithmic calculation, by <i>H. B. Goodwin, R.N.</i> 5 0		
Tables for Facilitating the Determination of the Latitude and Time at Sea by Observations of the Stars , by <i>Rear-Admiral C. Shadwell, F.R.S.</i> ... 2 6		
A Handbook for Star Double Altitudes , by <i>A. C. Johnson, R.N.</i> , with directions for selecting the Stars 2 6		

See also Sextants.

STABILITY.

A New Theory of the Stability of Ships , second edition, revised and enlarged, (with 28 diagrams), by <i>Alf. J. Cooper</i> (1899) 2 0		
--	--	--

SURVEYING.

Practical Nautical Surveying and the Handicraft of Navigation , by <i>Com. T. A. Hull, R.N.</i> 8 0		
Practical Observations on Surveying (on determining the Position of a Vessel when Sounding), by <i>Commander P. F. Shortland, R.N.</i> 1 0		

TIDES.

Moxly's Theory of the Tides , with numerous diagrams by <i>Capt. J. F. Ruthven, F.R.G.S.</i> ... 2 0		
Tide Charts of the English and Bristol Channels and entrance of the Thames , compiled from the Admiralty Tide Tables, by <i>Algernon Heber Percy</i> , late Lieut. Royal Navy 5 0		
The Direction and Rate of the Tidal Streams at every Hour, for 48 Localities between the Nore and Scilly Isles , compiled from Admiralty Sources only, by <i>F. Howard Collins</i> 2 0		
Twelve Charts of the Tidal Streams of the Channel Islands and Neighbouring French Coasts , by <i>F. Howard Collins</i> 4 0		

List of Nautical Works published by J. D. POTTER.

TIDES—continued.

	s.	d.
The General Direction of the Tidal Streams in the North Sea for every Hour "before" and "after," and at High Water, Dover, compiled by <i>Com. G. K. Gandy, R.N.R.</i> , from Official Publications (on one sheet, size 23 by 17 inches)	1	0
The Universal Tidal Ready Reckoner, calculated by <i>Capt. W. E. Hutchinson.</i>	1	6
The North Sea. Its Physical Characteristics, Tides, Currents and Fisheries, by <i>W. H. Wheeler, M.Inst.C.E.</i>	2	6
The Currents on the South-Eastern Coasts of Newfoundland and the Amount of Indraught into the Largest Bays on the South Coast, from Investigations of the Tidal and Current Survey in the Season of 1903, by <i>W. Bell Dawson, M.A., D.Sc., F.R.S.C., M.Inst.C.E., Superintendent.</i> Published by order of the Minister of Marine and Fisheries, Ottawa		No charge.
The Currents in the Gulf of St. Lawrence, including the Anticosti Region, Belle Isle, and Cabot Straits, condensed from the Reports of the Survey of Tides and Currents for the Seasons of 1894, 1895, and 1896. Published by order of the Minister of Marine and Fisheries, Ottawa		No charge.
The Currents at the entrance of the Bay of Fundy and on the Steamship Routes in or approaching Southern Nova Scotia, from investigations of the Tidal and Current Survey in the Season of 1904, by <i>W. Bell Dawson, M.A., D.Sc., F.R.S.C., M.Inst.C.E., Superintendent.</i> Published by the Department of Marine and Fisheries, Ottawa, Canada		No charge.
The Currents in Belle Isle Strait, from Investigations of the Tidal and Current Survey in the Seasons of 1894 and 1906. By <i>W. Bell Dawson, M.A., D.Sc., F.R.S.C., M.Inst.C.E., Superintendent.</i> Published by the Department of Marine and Fisheries, Ottawa, Canada		No charge.
Tables of Hourly Direction and Velocity of the Currents and Time of Slack Water in the Bay of Fundy and its Approaches as far as Cape Sable. From Investigations of the Tidal and Current Survey in the seasons of 1904 and 1907. By <i>W. Bell Dawson, M.A., D.Sc., M.Inst.C.E., Superintendent.</i> Published by the Department of Marine and Fisheries, Ottawa, Canada		No charge.

See also Time.

TIME.

How to Find the Time at Sea in less than a Minute, being a New and Accurate Method, with specially adapted Tables, by <i>A. C. Johnson, R.N.</i>	2	6
Time, Tide, and Distances. A handy book of reference for the Shipowner, Underwriter, or Traveller. Contains the World's Time compared with Greenwich; the Tides round the British Coasts and those from Bergen via the Eastern Route to Japan with that at London Bridge; approximate Distances from Home Ports to Home and Foreign Ports (over 13,000 references); and a Speed and Distance Table for Bates of Speed from 8 to 21 knots for distances up to 14,000 nautical miles, by <i>J. McKirdy, R.N.R.</i>	15	0
Time-Altitudes for Expediting the Calculation of Apparent-Time, &c., by <i>A. C. Johnson, R.N.</i>	4	0
The Blue Coat Boys' Clock. A dial showing the simultaneous time of day at all parts of the earth's surface, size 20 x 17 inches	5	0

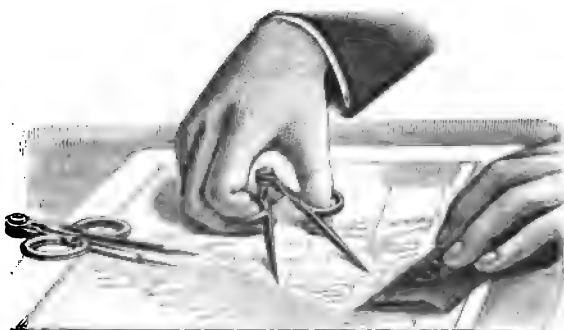
See also Azimuths, Chronometers, Tides.

WINDS.

The True Direction and Velocity of Wind, observed from Ships while Sailing, by <i>James N. Miller</i> (Member of the Liverpool Polytechnic Society), with Table for Indicating the True Direction of the Winds at Sea (1870)	0	6
The Wind in its Circuits: with the explanation of the Origin and Cause of Circular Storms and Equinoctial Gales; illustrated with numerous Diagrams and a Chart of the Prevailing Winds of the World for Spring and Summer, by <i>Lieut. R. H. Armit, R.N.</i> (1870)	7	6

See also Meteorology.

F. HOWARD COLLINS'S SINGLE-HANDED DIVIDERS.
Specially Designed for Navigators.



The advantages of these Single-handed Dividers are that they can be picked up from the table by one hand alone, and the legs opened or closed by the finger and thumb of the same hand, without any other assistance whatever.

Navigators are thus enabled to work, and retain in position, the parallel ruler with one hand, while distances are being measured with the other. It is needless to say that this enables much time to be saved in laying off courses and distances, a matter for consideration in these days of steamers travelling a mile in less than two-and-a-half minutes.

The joint itself is of an entirely new form, being made a round ball. This is found to be a great advantage, and the best form for rolling between the thumb and fore-finger when "stepping" distances; as for instance, in measuring fifty miles by the legs being set to ten miles of the chart scale.

These Dividers are of the *best make* in German-silver, price 7s. 6d. per pair in cardboard box, and with special cleat and screws for fixing to the chart-room bulk-head to hold them when not in use.

"None seem to be quite on a level of excellence with these."—*Merchant Service Review*.

"The price is certainly a reasonable one."—*The Shipping World*.

								s.	d.
BRASS DIVIDERS	6-inch, 2/6; 8-inch	3	6

FIELD'S PARALLEL RULERS.

Borwood	24-inch, 18/; 21-inch, 15/; 18-inch, 11/; 15-inch	8	0
Ebony	24-inch, 21/; 21-inch, 18/; 18-inch, 14/; 15-inch	11	6

INCORRECT CHARTS.

SPECIAL BOARD OF TRADE OFFICIAL NOTICES TO SHIPOWNERS.

NOTICE TO SHIPOWNERS AND AGENTS.

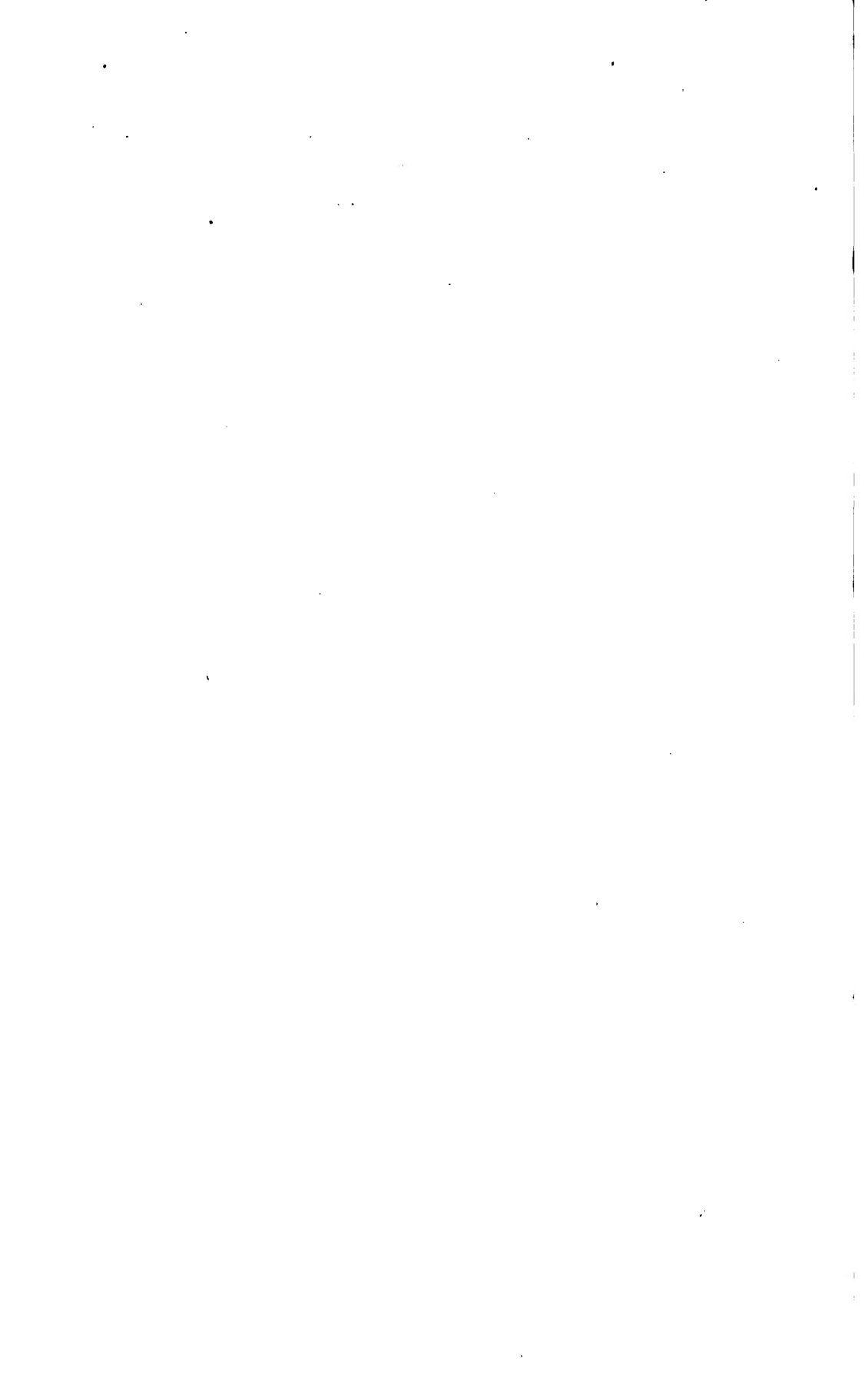
The attention of the Board of Trade has frequently been called to cases in which British vessels have been endangered or wrecked through Masters attempting to navigate them by means of antiquated or otherwise defective Charts.

The Board of Trade desire, therefore, to direct the especial attention of Shipowners and their Servants and Agents to the necessity of seeing that the Charts taken or sent on board their Ships are corrected down to the time of sailing. Neglect to supply a Ship with proper Charts will be brought prominently before the Court of Inquiry in the event of a wreck occurring from that cause.

The Official Catalogue of Charts, plans and sailing directions, published by the Admiralty (issued annually in March), can be obtained free of charge on application to the Chart Agency, 145, Minories, London, E.C., or from any of the sub-agencies at the Home or Foreign Ports.

Statement, showing the number of New British Admiralty Charts Published, Corrections made to the Chart Plates, and Quantities Printed, for the years 1885, 1890, 1895, 1900, and 1905.

	1885	1890	1895	1900	1905
New Chart Plates Engraved and Published	54	76	114	102	110
Chart Plates Improved by Additional Plans ...	32	10	34	30	36
Chart Plates Improved by Corrections and Additions	186	130	163	224	196
Corrections Made to the Chart Plates	2,750	4,750	5,300	4,520	5,320
Minor Corrections at the hands of the Draughtsmen	29,800	37,270	30,046	35,507	60,499
Total Number of Charts Printed	272,115	297,120	312,638	580,207	689,930



WILL BE ASSESSED FOR FAILURE TO RETURN
THIS BOOK ON THE DATE DUE. THE PENALTY
WILL INCREASE TO 50 CENTS ON THE FOURTH DAY
AND TO \$1.00 ON THE SEVENTH DAY
OVERDUE.

MAR 21 1938 INTERLIBRARY LOAN

ONE MONTH AFTER RECEIPT

~~FEB 23 1936~~

0722

MAY 20 1970

6-23

APR 15 1942

APR 04 1988

19 May '49 HJ

INTER-LIBRARY
LOAN

MAR 05 1988

SENT ON ILL

30 Apr 65 PM

AUG 25 2000

U. C. BERKELEY

REC'D LD

APR 29 '65-12 M

LD 21-100m-8,'34

YD 00606

U.C. BERKELEY LIBRARIES



C006155827

225301

No.

